

APPENDIX C

# Geophysical Investigation Data

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APPENDIX C.1

## **Downhole Geophysical Data**

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**SR-710 TUNNEL TECHNICAL STUDY  
BORING GEOPHYSICS**

**BORINGS Z1-B3, Z1-B5, Z1-B6,  
Z1-B7, Z2-B1, Z2-B4, Z3-B1, Z3-B3, Z3-B4,  
Z3-B6, Z3-B8, Z3-B12 AND Z4-B4**

**Report 9014-01 rev 0**

**October 5, 2009**

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Z1-B7, Z2-B1, Z2-B4, Z3-B1, Z3-B3, Z3-B4,  
Z3-B6, Z3-B8, Z3-B12 AND Z4-B4**

**Report 9014-01 rev 0**

**October 5, 2009**

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**APPENDICES**

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## INTRODUCTION

Boring geophysical measurements were collected in thirteen uncased borings located within four zones of the SR-710 tunnel technical study. Geophysical data acquisition was performed between January 14 and March 31, 2009 by Robert Steller, Charles Carter and Lauren Annis of **GEOVision**. Data analysis was performed by Robert Steller and reviewed by John Diehl of **GEOVision**. Report preparation was performed by Robert Steller and reviewed by John Diehl of **GEOVision**. The work was performed under subcontract with Cascade Drilling for CH2M Hill, Inc. (CH2M) with Ravee Raveendra serving as the point of contact for CH2M.

This report describes the field measurements, data analysis, and results of this work.

## SCOPE OF WORK

This report presents the results of boring geophysical measurements collected between January 14 and March 31, 2009, in thirteen borings, as detailed in Table 1. The purpose of these studies was to supplement stratigraphic information obtained during CH2M's soil and rock sampling program and to acquire shear wave velocities and compressional wave velocities as a function of depth, as a component of the SR-710 tunnel study.

The OYO/Robertson Suspension PS Logging System (Suspension System) was used to obtain in-situ horizontal shear ( $S_H$ ) and compressional (P) wave velocity measurements in all borings, except Z3-B8, at 1.6-foot intervals. Measurements followed **GEOVision** Procedure for P-S Suspension Seismic Velocity Logging, revision 1.3. The acquired data was analyzed and a profile of velocity versus depth was produced for both compressional and horizontally polarized shear waves.

A detailed reference for the suspension PS velocity measurement techniques used in this study is:

Guidelines for Determining Design Basis Ground Motions, Report TR-102293,  
Electric Power Research Institute, Palo Alto, California, November 1993,  
Sections 7 and 8.

The Robertson 3ACS probe was used to collect 3-arm mechanical caliper and natural gamma data at 0.05-foot intervals in all borings to aid in identification of stratigraphic transitions. Measurement procedures followed these ASTM standards:

- ASTM D5753, “Planning and Conducting Borehole Geophysical Surveys
- ASTM D6274, “Conducting Borehole Geophysical Logging – Gamma ASTM D6274-98 (Re-approved 2004), Conducting Borehole Geophysical Logging - Gamma”
- ASTM D6167-97 (Re-approved 2004) “Conducting Borehole Geophysical Logging – Mechanical Caliper”

The acquired data was combined and a profile of these parameters versus depth was produced.

The Robertson High Resolution Acoustic Televiwer (HiRAT) was used to collect deviation data and acoustic televiwer images of the rock at 0.008-foot intervals in all borings except Z3-B8. Measurements followed the **GEOVision** HiRAT Field Procedure, revision 1.0. In addition, the boring images were analyzed and planar features such as bedding planes and fractures were identified for dip, azimuth and stereonet processing to identify dominant fracture and bedding planes.

# INSTRUMENTATION

## Suspension Velocity Instrumentation

Suspension velocity measurements were performed using the suspension PS logging system, manufactured by OYO Corporation, and their subsidiary, Robertson Geologging. This system directly determines the average velocity of a 3.28-foot high segment of the soil column surrounding the boring of interest by measuring the elapsed time between arrivals of a wave propagating upward through the soil column. The receivers that detect the wave, and the source that generates the wave, are moved as a unit in the boring producing relatively constant amplitude signals at all depths.

The suspension system probe consists of a combined reversible polarity solenoid horizontal shear-wave source ( $S_H$ ) and compressional-wave source (P), joined to two biaxial receivers by a flexible isolation cylinder, as shown in Figure 1. The separation of the two receivers is 3.28 feet, allowing average wave velocity in the region between the receivers to be determined by inversion of the wave travel time between the two receivers. The total length of the probe as used in these surveys is 19 feet, with the center point of the receiver pair 12.1 feet above the bottom end of the probe.

The probe receives control signals from, and sends the digitized receiver signals to, instrumentation on the surface via an armored 4 conductor cable. The cable is wound onto the drum of a winch and is used to support the probe. Cable travel is measured to provide probe depth data, using a 3.28-foot circumference sheave fitted with a digital rotary encoder.

The entire probe is suspended in the boring by the cable, therefore, source motion is not coupled directly to the boring walls; rather, the source motion creates a horizontally propagating impulsive pressure wave in the fluid filling the boring and surrounding the source. This pressure wave is converted to P and  $S_H$ -waves in the surrounding soil and rock as it passes through the casing and grout annulus and impinges upon the wall of the boring. These waves propagate

through the soil and rock surrounding the boring, in turn causing a pressure wave to be generated in the fluid surrounding the receivers as the soil waves pass their location. Separation of the P and  $S_H$ -waves at the receivers is performed using the following steps:

1. Orientation of the horizontal receivers is maintained parallel to the axis of the source, maximizing the amplitude of the recorded  $S_H$  -wave signals.
2. At each depth,  $S_H$ -wave signals are recorded with the source actuated in opposite directions, producing  $S_H$ -wave signals of opposite polarity, providing a characteristic  $S_H$ -wave signature distinct from the P-wave signal.
3. The 7.0-foot separation of source and receiver 1 permits the P-wave signal to pass and damp significantly before the slower  $S_H$ -wave signal arrives at the receiver. In faster soils or rock, the isolation cylinder is extended to allow greater separation of the P- and  $S_H$ -wave signals.
4. In saturated soils, the received P-wave signal is typically of much higher frequency than the received  $S_H$ -wave signal, permitting additional separation of the two signals by low pass filtering.
5. Direct arrival of the original pressure pulse in the fluid is not detected at the receivers because the wavelength of the pressure pulse in fluid is significantly greater than the dimension of the fluid annulus surrounding the probe (foot versus inch scale), preventing significant energy transmission through the fluid medium.

In operation, a distinct, repeatable pattern of impulses is generated at each depth as follows:

1. The source is fired in one direction producing dominantly horizontal shear with some vertical compression, and the signals from the horizontal receivers situated parallel to the axis of motion of the source are recorded.
2. The source is fired again in the opposite direction and the horizontal receiver signals are recorded.
3. The source is fired again and the vertical receiver signals are recorded. The repeated source pattern facilitates the picking of the P and  $S_H$ -wave arrivals; reversal of the source changes the polarity of the  $S_H$ -wave pattern but not the P-wave pattern.

The data from each receiver during each source activation is recorded as a different channel on the recording system. The Suspension PS system has six channels (two simultaneous recording channels), each with a 1024 sample record. The recorded data are displayed as six channels with a common time scale. Data are stored on disk for further processing. Up to 8 sampling sequences can be summed to improve the signal to noise ratio of the signals.

Review of the displayed data on the recorder or computer screen allows the operator to set the gains, filters, delay time, pulse length (energy), sample rate, and summing number to optimize the quality of the data before recording. Verification of the calibration of the Suspension PS digital recorder is performed every twelve months using a NIST traceable frequency source and counter, as outlined in Appendix D.

## Caliper / Natural Gamma Instrumentation

Caliper and natural gamma data were collected using a Model 3ACS 3-arm caliper probe, serial number 5368, manufactured by Robertson Geologging, Ltd. With the short arm configuration used in these surveys, the probe permitted measurement of boring diameters between 1.6 and 16 inches. With this tool, caliper measurements were collected concurrent with measurement of natural gamma emission from the boring walls. The probe is 6.82 feet long, and 1.5 inches in diameter.

This probe is useful in the following studies:

- Measurement of boring diameter and volume
- Location of hard and soft formations
- Location of fissures, caving, pinching and casing damage
- Bed boundary identification
- Strata correlation between borings

The probe receives control signals from, and sends the digitized measurement values to, a Robertson Micrologger II on the surface via an armored 4 conductor cable. The cable is wound onto the drum of a winch and is used to support the probe. Cable travel is measured to provide probe depth data, using a 3.28-foot circumference sheave fitted with a digital rotary encoder. The probe and depth data are transmitted by USB link from the Micrologger unit to a laptop computer where it is displayed and stored on hard disk.

The caliper consists of three arms, each with a toothed quadrant at their base, pivoted in the lower probe body. A toothed rack engages with each quadrant, thus constraining the arms to move together. Linear movement of the rack is converted to opening and closing of the arms. Springs hold the arms open in the operating position. A motor drive is provided to retract the arms, allowing the probe to be lowered into the boring. The rack is coupled to a potentiometer which converts movement into a voltage sensed by the probe's microprocessor.

Natural gamma measurements rely upon small quantities of radioactive material contained in all soil and rocks to emit gamma radiation as they decay. Trace amounts of Uranium and Thorium are present in a few minerals, where potassium-bearing minerals such as feldspar, mica and clays will include traces of a radioactive isotope of Potassium. These emit gamma radiation as they decay with an extremely long half-life. This radiation is detected by scintillation - the production of a tiny flash of light when gamma rays strike a crystal of sodium iodide. The light is converted into an electrical pulse by a photomultiplier tube. Pulses above a threshold value of 60 thousand electron Volts (KeV) are counted by the probe's microprocessor. The measurement is useful because the radioactive elements are concentrated in certain soil and rock types e.g. clay or shale, and depleted in others e.g. sandstone or coal.

## **Acoustic Televiwer / Boring Deviation Instrumentation**

An acoustic image and boring deviation data were collected using a High Resolution Acoustic Televiwer probe (HiRAT), serial number 5174, manufactured by Robertson Geologging, Ltd. The probe is 5.2 feet long, 1.6 inches in diameter, and may be fitted with upper and lower four-band centralizers.

In this application, this probe is useful in the following studies:

- Measurement of boring inclination and deviation from vertical
- Determination of need to correct soil and geophysical log depths to true vertical depths
- Acoustic imaging of the boring wall to identify fractures, dikes, and weathered zones, and determine dip and azimuth of these features

The probe receives control signals from, and sends the digitized measurement values to, a Robertson Micrologger II on the surface via an armored 4 conductor cable. The cable is wound onto the drum of a winch and is used to support the probe. Cable travel is measured to provide probe depth data, using a 3.28-foot circumference sheave fitted with a digital rotary encoder. The probe and depth data are transmitted by USB link from the Micrologger unit to a laptop computer where it is displayed and stored on hard disk.

This system produces images of the boring wall based upon the amplitude and travel time of an ultrasonic beam reflected from the formation wall. The ultrasonic energy is generated by a piezoelectric transducer at a frequency of 1.4 MHz. A periodic acoustic energy wave is emitted by the transducer and travels through the acoustic head and boring fluid until it reaches the interface between the boring fluid and the boring wall. Here a portion of the energy is reflected back to the transducer, the remainder continuing on into the formation. By careful time sequencing, the piezoelectric transducer acts as both the transmitter of the ultrasonic pulse and receiver of the reflected wave. The travel time of the energy wave is the period between transmission of the source energy pulse and the return of the reflected wave measured at the point of maximum wave amplitude. The magnitude of the wave energy is measured in dB, a



unit-less ratio of the detected echo wave amplitude divided by the amplitude of the transmitted wave. The strength of the reflected signal depends primarily upon the impedance contrast of the boring fluid and the boring wall formation. In a number of these borings, there was significant clay “wall cake” which attenuated the acoustic signal, and created a low impedance contrast at the boring wall.

The acoustic wave propagates along the axis of the probe and then is reflected perpendicular to this axis by a reflector that focuses the beam to a 0.1-inch diameter spot about 2 inches from the central axis of the probe. This reflector is mounted on the shaft of a stepper motor enabling the position of the measurement to be rotated through 360°. Sampling rates of 90, 180 and 360 measured points per revolution are available. During these surveys, data were collected at 360 samples per revolution, providing an equivalent horizontal pixel size of approximately 0.05 inches on the boring wall. It should be noted that during logging the probe is moving in the boring, so that the measured points describe a very fine pitch spiral.

The probe contains a fluxgate magnetometer to monitor magnetic north, and all raw televiewer data are referenced to magnetic north. The processed data is referenced to true north, using a declination of 12.9 degrees east for these sites and dates, obtained from the NOAA declination web site (<http://www.ngdc.noaa.gov/geomagmodels/Declination.jsp>). Also, a three-axis accelerometer is enclosed in the probe, and boring deviation data are recorded during the logging runs, to permit correction of structure dip angle from apparent dip, (referenced to boring axis), to true dip (referenced to a vertical axis) in non-vertical borings.

The data are presented on a computer screen for operator review during the logging run, and stored on hard disk for later processing.

# MEASUREMENT PROCEDURES

## Suspension Velocity Measurement Procedures

Twelve borings (excluding Z3-B8) were logged while filled with bentonite or polymer based drilling mud. Measurements followed the **GEOVision** Procedure for P-S Suspension Seismic Velocity Logging, revision 1.31, as presented in Appendix E. These procedures were supplied and approved in advance of the work. Prior to each logging run, the probe was positioned with the top of the probe at the top of the surface casing, and the electronic depth counter was set to 8.2 feet, the distance between the mid-point of the receiver and the top of the probe, minus the height of the casing stick-up, as verified with a tape measure, and recorded on the field logs. The probe was lowered to the bottom of the boring, stopping at 1.6-foot intervals to collect data, as summarized in Table 2.

At each measurement depth the measurement sequence of two opposite horizontal records and one vertical record was performed, and the gains were adjusted as required. The data from each depth were viewed on the computer display, checked, and recorded on disk before moving to the next depth.

Upon completion of the measurements, the probe zero depth indication at the depth reference point was verified prior to removal from the boring, and after survey depth error (ASDE) was calculated, as listed in Table 3.

## Caliper / Natural Gamma Procedures

The borings were filled with bentonite or polymer based drilling mud and logged from the bottom of the boring up until the caliper entered the bottom of the surface casing or reached the surface, as listed in Table 2. Measurements followed ASTM D6167-97 (Re-approved 2004) Conducting Borehole Geophysical Logging – Mechanical Caliper.

Prior to and following each logging run, the caliper tool was verified, using the manufacturer's supplied three point calibration jig. The three point jig is a circular plate with a series of holes in the top surface into which the tips of the caliper arms fit. This has circles of diameters from 2 to 12 inches. The calibration jig is placed over a bucket with the probe standing upright with its nose section passing through the jig's central hole. The caliper probe arms are opened under program control, and a log is recorded as the tips of the arms are placed in the holes on the calibration jig. The measured dimensions, as displayed on the recording computer screen was recorded on the field log sheet, as well as in the digital files, and compared with the calibration jig dimensions. These files are presented in LAS 2.0 format in the boring specific sub-directories of the data directory on the data disk (CD-R) labeled Report 9014-02 that accompanies this report. If the verification records did not fall within +/- 0.05 inches of the calibration jig values, the caliper tool was re-calibrated, using the three point calibration jig, and the log repeated. As with the verification, the tips of the caliper arms are placed in the holes marked with the required diameter. During calibration, the value of the current calibration point, as stamped on the jig, is entered via the control computer. The system counts for 15 seconds to make an average of the response. The procedure is repeated for the second and third required openings. The computation and generation of the calibration coefficient file is entirely automatic. The calibration file is simply the set of coefficients of a quadratic curve which fits the three data points.

Natural gamma was not calibrated in the field, as it is a qualitative measurement, not a quantitative value, and is used only to assist in picking transitions between stratigraphic units, as described in ASTM D6274-98 (Re-approved 2004), Conducting Borehole Geophysical Logging - Gamma.

In each boring, the probe was positioned with the top of the probe at the top of the casing, and the electronic depth counter was set to the specified length of the probe, minus the height of the casing stick-up, as verified with a tape measure, and recorded on the field logs. The probe was lowered to the bottom of the boring, where the caliper legs were opened, and data collection begun. The probe was then returned to the surface at 10 feet/minute, collecting data continuously at 0.05-foot spacing, as summarized in Table 2.

Upon completion of the measurements, the probe zero depth indication at the depth reference point was verified prior to removal from the boring, and after survey depth error (ASDE) was calculated, as listed in Table 3.

## **Acoustic Televiewer / Boring Deviation Measurement Procedures**

Twelve borings (excluding Z3-B8) were logged while filled with bentonite or polymer based drilling mud. Measurements followed the **GEOVision** standard field procedures, as presented in Appendix E.

Prior to use, the HiRAT probe tiltmeter and compass functions were checked by comparison with a Brunton surveyors' compass, and the results recorded on the field logs.

In each boring, the HiRAT probe was positioned with the top of the probe at the top of the casing, and the electronic depth counter was set to the specified length of the probe, minus the height of the casing stick-up, as verified with a tape measure, and recorded on the field logs. The probe was lowered to the bottom of the boring, and data collection begun. The rotational scan resolution was set to 360 samples per revolution, giving a horizontal pixel size of approximately 0.05 inches. The probe was returned to the surface at a nominal rate of 3 feet/minute, with an acquisition rate of 125 samples/foot, giving an equivalent vertical pixel size of 0.008 feet (approximately 0.1 inches).

Upon completion of the measurements, the probe zero depth indication at grade was verified prior to removal from the boring, and after survey depth error (ASDE) was calculated, as listed in Table 3.

## DATA ANALYSIS

### Suspension Velocity Analysis

Using the proprietary OYO program PSLOG.EXE version 1.0, the recorded digital waveforms were analyzed to locate the most prominent first minima, first maxima, or first break on the vertical axis records, indicating the arrival of P-wave energy.

The difference in travel time between receiver 1 and receiver 2 (R1-R2) arrivals was used to calculate the P-wave velocity for that 3.28-foot segment of the soil column. When observable, P-wave arrivals on the horizontal axis records were used to verify the velocities determined from the vertical axis data. The time picks were then transferred into an EXCEL template (EXCEL version 2003 SP2) to complete the velocity calculations based upon the arrival time picks made in PSLOG. The EXCEL analysis files are included in the boring specific directories on the data disk (CD-R) labeled Report 9014-02 that accompanies this report.

The P-wave velocity over the 7.0-foot interval from source to receiver 1 (S-R1) was also picked using PSLOG, and calculated and plotted in EXCEL, for quality assurance of the velocity derived from the travel time between receivers. In this analysis, the depth values as recorded were increased by 5.2 feet to correspond to the mid-point of the 7.0-foot S-R1 interval. Travel times were obtained by picking the first break of the P-wave signal at receiver 1 and subtracting 0.3 milliseconds, the calculated and experimentally verified delay from source trigger pulse (beginning of record) to source impact. This delay corresponds to the duration of acceleration of the solenoid before impact.

As with the P-wave records, the recorded digital waveforms were analyzed to locate clear  $S_H$ -wave pulses, as indicated by the presence of opposite polarity pulses on each pair of horizontal records. Ideally, the  $S_H$ -wave signals from the 'normal' and 'reverse' source pulses are very nearly inverted images of each other. Digital Fast Fourier Transform – Inverse Fast Fourier Transform (FFT – IFFT) lowpass filtering was used to remove the higher frequency P-wave

signal from the  $S_H$ -wave signal. Different filter cutoffs were used to separate P- and  $S_H$ -waves at different depths, ranging from 600 Hz in the slowest zones to 3000 Hz in the regions of highest velocity. At each depth, the filter frequency was selected to be at least twice the fundamental frequency of the  $S_H$ -wave signal being filtered.

Generally, the first maxima were picked for the 'normal' signals and the first minima for the 'reverse' signals, although other points on the waveform were used if the first pulse was distorted. The absolute arrival time of the 'normal' and 'reverse' signals may vary by +/- 0.2 milliseconds, due to differences in the actuation time of the solenoid source caused by constant mechanical bias in the source or by boring inclination. This variation does not affect the R1-R2 velocity determinations, as the differential time is measured between arrivals of waves created by the same source actuation. The final velocity value is the average of the values obtained from the 'normal' and 'reverse' source actuations.

As with the P-wave data,  $S_H$ -wave velocity calculated from the travel time over the 7.0-foot interval from source to receiver 1 was calculated and plotted for verification of the velocity derived from the travel time between receivers. In this analysis, the depth values were increased by 5.2 feet to correspond to the mid-point of the 7.0-foot S-R1 interval. Travel times were obtained by picking the first break of the  $S_H$ -wave signal at the near receiver and subtracting 0.3 milliseconds, the calculated and experimentally verified delay from the beginning of the record at the source trigger pulse to source impact.

These data and analysis were reviewed by John Diehl as a component of **GEOVision's** in-house Quality assurance program.

Figure 2 shows an example of R1 - R2 measurements on a sample filtered suspension record. In Figure 2, the time difference over the 3.28-foot interval of 1.88 milliseconds for the horizontal signals is equivalent to an  $S_H$ -wave velocity of 1745 feet/second. Whenever possible, time differences were determined from several phase points on the  $S_H$ -waveform records to verify the data obtained from the first arrival of the  $S_H$ -wave pulse. Figure 3 displays the same record before filtering of the  $S_H$ -waveform record with a 1400 Hz FFT - IFFT digital lowpass filter,

illustrating the presence of higher frequency P-wave energy at the beginning of the record, and distortion of the lower frequency  $S_H$ -wave by residual P-wave signal.

### **Caliper / Natural Gamma Analysis**

No analysis is required with the caliper or natural gamma data; however depths to identifiable boring features on the acoustic televiewer and suspension logs were compared to verify compatible depth readings on all logs. Using Robertson Geologging Winlogger software version 1.5, build 401J, these data were converted to LAS 2.0 and PDF formats for transmittal to the client.



## Acoustic Televiewer / Boring Deviation Analysis

The acoustic televiewer data were processed using Robertson's RGLDIP software, version 6.2. Sinusoidal projections of fractures observed in the boring walls were interactively picked on the un-wrapped televiewer image, and are presented on the logs as red sinusoids superimposed over the televiewer image. Bedding features, where identifiable, were picked on the same images, and are presented on the logs as green sinusoids. The sinusoidal projections were processed using the mechanical caliper diameter data to calculate apparent dip angle. True dip was calculated, correcting for the plunge of the borings using the recorded data from the accelerometer located in the probes, and presented in arrow format, with true dip indicated by the arrow position across the plot. Azimuth of dip (not strike), is indicated by the direction of the arrow tail, with true north being "up". These values are presented with the comments to the right of the arrow plots, as dip azimuth followed by dip angle.

The televiewer images were also processed to create a simulated core image of the borings. It must be noted that the simulated core image represents a core that would have the full diameter of the boring, not the diameter of the cores removed during drilling, so that direct comparison between the two is not possible. Also, the unwrapped image is viewed from the perspective of an observer in the center of the boring looking outward. The simulated core image is viewed from the "outside" of the boring looking inward, so there is a reversal of the position of east and west relative to north between the two images.

The televiewer data were also processed to extract the deviation data and produce an ASCII file and plots of boring deviation. Stereonet analysis of the identified features was performed with Robertson's RGLDIP software, version 6.2, to assist in identifying dominant fracture and bedding planes in the borings. Concentrations of similarly oriented features were enclosed in three to five small circles on the stereonet image, and the vector mean dip and azimuth for each small circle was calculated.

# RESULTS

## Suspension Velocity Results

Suspension R1-R2 P- and  $S_H$ -wave velocities are plotted in Figures 4, 8, 12, 16, 20, 24, 28, 32, 36, 40, 45, and 49. The suspension velocity data presented in these figures are presented in Tables 5, 7, 9, 11, 13, 15, 17, 19, 21, 23, 25, and 27. The EXCEL analysis file for each boring are included in the boring specific directories on the data disk (CD-R) labeled Report 9014-02 that accompanies this report.

P- and  $S_H$ -wave velocity data from R1-R2 analysis and quality assurance analysis of S-R1 data are plotted together in Figures A-1 through A-12 to aid in visual comparison. It should be noted that R1-R2 data are an average velocity over a 3.28-foot segment of the soil column; S-R1 data are an average over 7.0 feet, creating a significant smoothing relative to the R1-R2 plots. S-R1 data are presented in Tables A-1 through A-12, and included in the EXCEL analysis files for each boring on the data disk (CD-R) labeled Report 9014-02 that accompanies this report. The EXCEL analysis files include Poisson's Ratio calculations, tabulated data and plots.

Calibration procedures and records for the suspension PS measurement system are presented in Appendix D.

The **GEOVision** standard field procedures, as provided to CH2M for approval prior to field work, are reproduced in Appendix E.

## **Caliper / Natural Gamma Results**

Caliper and natural gamma data are presented as single page logs in Figures 5, 9, 13, 17, 21, 25, 29, 33, 37, 41, 44, 46 and 50, as well as multi-page logs in Appendix B. LAS 2.0 data and Acrobat files for each boring are included in the boring specific sub-directories in the data directory on the data disk (CD-R) labeled Report 9014-02 that accompanies this report.

## **Acoustic Televiewer / Boring Deviation Results**

Acoustic televiewer amplitude images and picked sinusoids are presented in Appendix C. The same logs are presented in .pdf format in the boring specific sub-directories of the data disk (CD-R) labeled Report 9014-02 that accompanies this report. Fracture and bedding depth, dip and azimuth of dip data are provided on the multi-page log sheets in Appendix C, and in Tables 6, 8, 10, 12, 14, 16, 18, 20, 22, 24, 26 and 28 as well as in .txt and EXCEL format.

Upper hemisphere stereonet plots are presented in Figures 6, 10, 14, 18, 22, 26, 30, 34, 38, 42, 47, and 51, as well as in PDF format. These borings did not exhibit different zones of feature orientation; the feature orientations appeared to be fairly evenly distributed over the boring depths, so they were processed as single zone models.

The mean dips for each of the stereonet small circles are presented in Figures 6, 10, 14, 18, 22, 26, 30, 34, 38, 42, 47, and 51, and in ASCII format. Feature distribution histograms and Rose diagrams are presented in the boring specific sub-directories of the data disk (CD-R).

Boring deviation data is presented graphically in Figures 7, 11, 15, 19, 23, 27, 31, 35, 39, 43, 48 and 52, and summarized in Table 4. Deviation data plots in Acrobat format and deviation data at 1.0-foot stations are presented in text format in the boring specific sub-directories of the data disk (CD-R).

## **SUMMARY**

### **Discussion of Suspension Velocity Results**

Suspension PS velocity data are ideally collected in an uncased fluid filled boring, drilled with rotary mud (rotary wash) methods. The borings at these sites were well suited for collection of suspension PS velocity data, though in some cases the shallow portions of the borings were eroded out to large diameters, which degraded the quality of the velocity data.

Suspension PS velocity data quality is judged based upon 5 criteria:

1. Consistent data between receiver to receiver (R1 – R2) and source to receiver (S – R1) data.
2. Consistent relationship between P-wave and  $S_H$  -wave (excluding transition to saturated soils)
3. Consistency between data from adjacent depth intervals.
4. Clarity of P-wave and  $S_H$ -wave onset, as well as damping of later oscillations.
5. Consistency of profile between adjacent borings, if available.

Generally, these data show excellent correlation between R1 – R2 and S – R1 data, as well as excellent correlation between P-wave and  $S_H$ -wave velocities. P-wave and  $S_H$ -wave onsets are very clear, and later oscillations are well damped, with the exception of the borings that showed larger diameters due to erosion, Z1-B6, Z1-B7, Z2-B1 and Z3-B12, some which had diameters approaching 12 inches.

### **Discussion of Caliper / Natural Gamma Results**

Caliper and natural gamma data were collected in each boring. The caliper logs for these borings generally show nominal bit diameters of below about 100 feet, with the softer material above 100 feet eroded out to almost 12 inches in some locations. Natural gamma data were collected with this tool in all the borings, and shows a number of thin layers that correspond to

features on the acoustic televiewer logs. One such example is at 361 – 362 feet in Z1-B6, where there is a significant drop in natural gamma, and an apparent hard sandstone layer on the acoustic televiewer image. A significant velocity increase can be seen at the same depth.

## **Discussion of Acoustic Televiewer / Boring Deviation Results**

Despite the large nominal diameter (5.5 inches) of the Cascade Drilling borings, the acoustic televiewer data quality in borings with good diameter control and clean walls, like Z1-B3, Z1-B5 are quite clear, showing contacts between soft and harder rock units, fractures in the rock, and even spiral marks from the coring bit.

Boring Z1-B6 has good diameter control below 100 feet, but the images are not as clear due to a thick wall cake. This is illustrated by the presence of interference patterns caused by standing acoustic waves in the wall cake, similar to optical moiré patterns. These can be seen clearly in Z1-B6 at 333 – 334 feet. Heavy wall cake was a regular problem, with the probe completely covered in clay at the end of logging runs.

Boring Z2-B1 is eroded out to 8 inches or more for the entire depth, and yields almost no acoustic image. Z3-B1 does not show many planar features, but the image quality is good. This boring shows a number of hard inclusions in a softer matrix, but few planar features.

The twelve borings in which deviation data were collected were inclined at 2.0 degrees, or less, from vertical, and the maximum error in depth value was 0.3 feet in 319 feet, or less than 0.1 percent, as presented in Table 4. This error is less than depth errors from other causes, and no adjustment of log depths is indicated.

## Quality Assurance

These boring geophysical measurements were performed using industry-standard or better methods for measurements and analyses. All work was performed under **GEOVision** quality assurance procedures, which include:

- Use of NIST-traceable calibrations, where applicable, for field and laboratory instrumentation
- Use of standard field data logs
- Use of independent verification of velocity data by comparison of receiver-to-receiver and source-to-receiver velocities
- Independent review of calculations and results by a registered professional engineer, geologist, or geophysicist.

## Suspension Velocity Data Reliability

P- and  $S_H$ -wave velocity measurement using the Suspension Method gives average velocities over a 3.28-foot interval of depth. This high resolution results in the scatter of values shown in the graphs. Individual measurements are very reliable with estimated precision of +/- 5%. Standardized field procedures and quality assurance checks contribute to the reliability of these data.

## CERTIFICATION

All geophysical data, analysis, interpretations, conclusions, and recommendations in this document have been prepared under the supervision of and reviewed by a **GEOVision** California Professional Geophysicist.



7/31/09

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Antony J. Martin  
California Professional Geophysicist GP989  
**GEOVision** Geophysical Services

Date

- \* This geophysical investigation was conducted under the supervision of a California Professional Geophysicist using industry standard methods and equipment. A high degree of professionalism was maintained during all aspects of the project from the field investigation and data acquisition, through data processing interpretation and reporting. All original field data files, field notes and observations, and other pertinent information are maintained in the project files and are available for the client to review for a period of at least one year.

A professional geophysicist's certification of interpreted geophysical conditions comprises a declaration of his/her professional judgment. It does not constitute a warranty or guarantee, expressed or implied, nor does it relieve any other party of its responsibility to abide by contract documents, applicable codes, standards, regulations or ordinances.

BORING DESIGNATION	DATES LOGGED	COORDINATES (FEET, ZONE 5, NAD83) <sup>(1)</sup>		ELEVATION <sup>(1)</sup> (FEET NAVD88)
		NORTH	EAST	
Z1-B3	1/30/2009	1855594.07	6492810.43	343.23
Z1-B5	2/25/2009	1850576.02	6499981.20	442.15
Z1-B6	2/10/2009	1852836.59	6503970.85	447.22
Z1-B7	1/26/2009	1849941.30	6506175.09	480.52
Z2-B1	1/21/2009	1866308.10	6492663.29	451.02
Z2-B4	3/31/2009	1858027.66	6507350.57	558.11
Z3-B1	3/19/2009	1873601.92	6507232.68	885.14
Z3-B3	2/11/2009	1870194.48	6514774.44	801.99
Z3-B4	3/6/2009	1870813.73	6516733.49	768.04
Z3-B6	3/5/2009	1868062.70	6516722.28	750.00
Z3-B8	3/23/2009	1860993.95	6514198.81	594.27
Z3-B12	1/14/2009	1856063.15	6513380.17	501.00
Z4-B4	3/17/2009	1851895.71	6514496.46	454.42

<sup>(1)</sup> Coordinates and elevation provided by CH2M dated 6/17/09

Table 1. Boring locations and logging dates



BORING NUMBER	TOOL AND RUN NUMBER	DEPTH RANGE (FEET)	BOTTOM OF BOREHOLE CASING	SAMPLE OR MEASUREMENT INTERVAL (FEET)	DATE LOGGED
Z1-B3	CALIPER/GAMMA 1	300.7 – 71.0	86	0.05	1/30/2009
Z1-B3	ACOUSTIC TELEVIEWER 1	300.9 – 82.3	86	0.008	1/30/2009
Z1-B3	SUSPENSION PS 1	88.6 – 288.7	86	1.6	1/30/2009
Z1-B5	CALIPER/GAMMA 1	500.1 – 4.1	8	0.05	2/25/2009
Z1-B5	ACOUSTIC TELEVIEWER 1	499.4 – 35.0	8	0.008	2/25/2009
Z1-B5	SUSPENSION PS 1	11.8 – 487.2	8	1.6	2/25/2009
Z1-B6	CALIPER/GAMMA 1	400.1 – 1.0	4	0.05	2/10/2009
Z1-B6	ACOUSTIC TELEVIEWER 1	400.0 – 65.0	4	0.008	2/10/2009
Z1-B6	SUSPENSION PS 1	6.6 – 390.4	4	1.6	2/10/2009
Z1-B7	CALIPER/GAMMA 1	299.0 - 0	11	0.05	1/26/2009
Z1-B7	ACOUSTIC TELEVIEWER 1	299.0 – 145.0	11	0.008	1/26/2009
Z1-B7	SUSPENSION PS 1	13.1 – 290.4	11	1.6	1/26/2009
Z2-B1	CALIPER/GAMMA 1	149.0 – 1.0	19	0.05	1/21/2009
Z2-B1	ACOUSTIC TELEVIEWER 1	149.0 – 18.5	19	0.008	1/21/2009
Z2-B1	SUSPENSION PS 1	21.3 – 137.8	19	1.6	1/21/2009
Z2-B4	CALIPER/GAMMA 1	358.3 – 6.0	6	0.05	3/31/2009
Z2-B4	CALIPER/GAMMA 2	374.5 – 325.0	6	0.05	3/31/2009
Z2-B4	ACOUSTIC TELEVIEWER 1	358.7 – 1.8	6	0.008	3/31/2009
Z2-B4	ACOUSTIC TELEVIEWER 2	374.2 – 347.0	6	0.008	3/31/2009
Z2-B4	SUSPENSION PS 1	3.3 – 305.1	6	1.6	3/31/2009
Z2-B4	SUSPENSION PS 2	306.8 – 360.9	6	1.6	3/31/2009
Z3-B1	CALIPER/GAMMA 1	300.2 – 14.8	26	0.05	3/19/2009
Z3-B1	ACOUSTIC TELEVIEWER 1	300.2 – 22.2	26	0.008	3/19/2009
Z3-B1	SUSPENSION PS 1	4.0 – 287.1	26	1.6	3/19/2009

- PROBE DID NOT TOUCH BOTTOM OF BORING

Table 2. Logging dates and depth ranges

BORING NUMBER	TOOL AND RUN NUMBER	DEPTH RANGE (FEET)	BOTTOM OF BOREHOLE CASING	SAMPLE OR MEASUREMENT INTERVAL (FEET)	DATE LOGGED
Z3-B3	CALIPER/GAMMA 1	273.0 – 165.1	174.5	0.05	2/11/2009
Z3-B3	CALIPER/GAMMA 2	273.0 – 50.0	55	0.05	2/11/2009
Z3-B3	ACOUSTIC TELEVIEWER 1	274.0 – 173.0	174.5	0.008	2/11/2009
Z3-B3	SUSPENSION PS 1	177.2 – 262.5	174.5	1.6	2/11/2009
Z3-B3	SUSPENSION PS 2	57.4 – 183.7	55	1.6	2/11/2009
Z3-B4	CALIPER/GAMMA 1	274.9 – 2.1	3.5	0.05	3/6/2009
Z3-B4	ACOUSTIC TELEVIEWER 1	275.3 – 2.5	3.5	0.008	3/6/2009
Z3-B4	SUSPENSION PS 1	2.8 – 262.5	3.5	1.6	3/6/2009
Z3-B6	CALIPER/GAMMA 1	325.0 - 5.3	10.5	0.05	3/5/2009
Z3-B6	ACOUSTIC TELEVIEWER 1	320.4 – 308.9	10.5	0.008	3/5/2009
Z3-B6	ACOUSTIC TELEVIEWER 2	318.7 – 28.3	10.5	0.008	3/5/2009
Z3-B6	SUSPENSION PS 1	43.0 – 311.7	10.5	1.6	3/5/2009
Z3-B8	CALIPER/GAMMA 1	275.7 – 4.2	4	0.05	3/23/2009
Z3-B12	CALIPER/GAMMA 1	273.0 – 50.0	57.5	0.05	1/14/2009
Z3-B12	CALIPER/GAMMA 2	273.0 – 245.5	57.5	0.05	1/14/2009
Z3-B12	CALIPER/GAMMA 3	258.0 – 54.0	57.5	0.05	1/14/2009
Z3-B12	ACOUSTIC TELEVIEWER 1	67.5 – 186.8	57.5	0.008	1/14/2009
Z3-B12	ACOUSTIC TELEVIEWER 2	182.6 – 57.0	57.5	0.008	1/14/2009
Z3-B12	SUSPENSION PS 1	59.0 – 185.4	57.5	1.6	1/14/2009
Z3-B12	SUSPENSION PS 2	173.9 – 251.0 8.2 – 62.3	5	1.6	1/14/2009
Z4-B4	CALIPER/GAMMA 1	275.0 – 2.0	7	0.05	3/17/2009
Z4-B4	ACOUSTIC TELEVIEWER 1	275.1 – 270.3	7	0.008	3/17/2009
Z4-B4	ACOUSTIC TELEVIEWER 2	275.1 – 4.7	7	0.008	3/17/2009
Z4-B4	SUSPENSION PS 1	4.7 – 262.5	7	1.6	3/17/2009

- PROBE DID NOT TOUCH BOTTOM OF BORING

Table 2, continued. Logging dates and depth ranges

BORING NUMBER	MEAN DEVIATION AND AZIMUTH (DEGREES TN)	SURVEY DEPTH (FEET)	VERTICAL DEPTH (FEET)	DEPTH ERROR (FEET)	HORIZONTAL OFFSET (FEET)
Z1-B3	0.7 – N213	300.8	300.7	0.1	3.8
Z1-B5	0.5 – N292	499.3	499.3	0	4.7
Z1-B6	1.3 – N031	400.0	399.8	0.2	9.0
Z1-B7	1.5 – N226	299.0	298.9	0.1	7.6
Z2-B1	1.2 – N178	148.9	148.0	0	3.0
Z2-B4	0.9 – N000	374.6	374.5	0.1	6.0
Z3-B1	1.8 – N307	300.2	300.0	0.2	9.3
Z3-B3	0.5 – N265	273.9	273.9	0	2.2
Z3-B4	0.2 – N033	275.2	275.2	0	1.1
Z3-B6	2.0 – N081	318.7	318.4	0.3	11.3
Z3-B12	0.3 – N264	182.5	182.5	0	0.9
Z4-B4	0.6 – N000	275.1	275.0	0.1	2.6

Table 3. Boring Deviation Data Summary

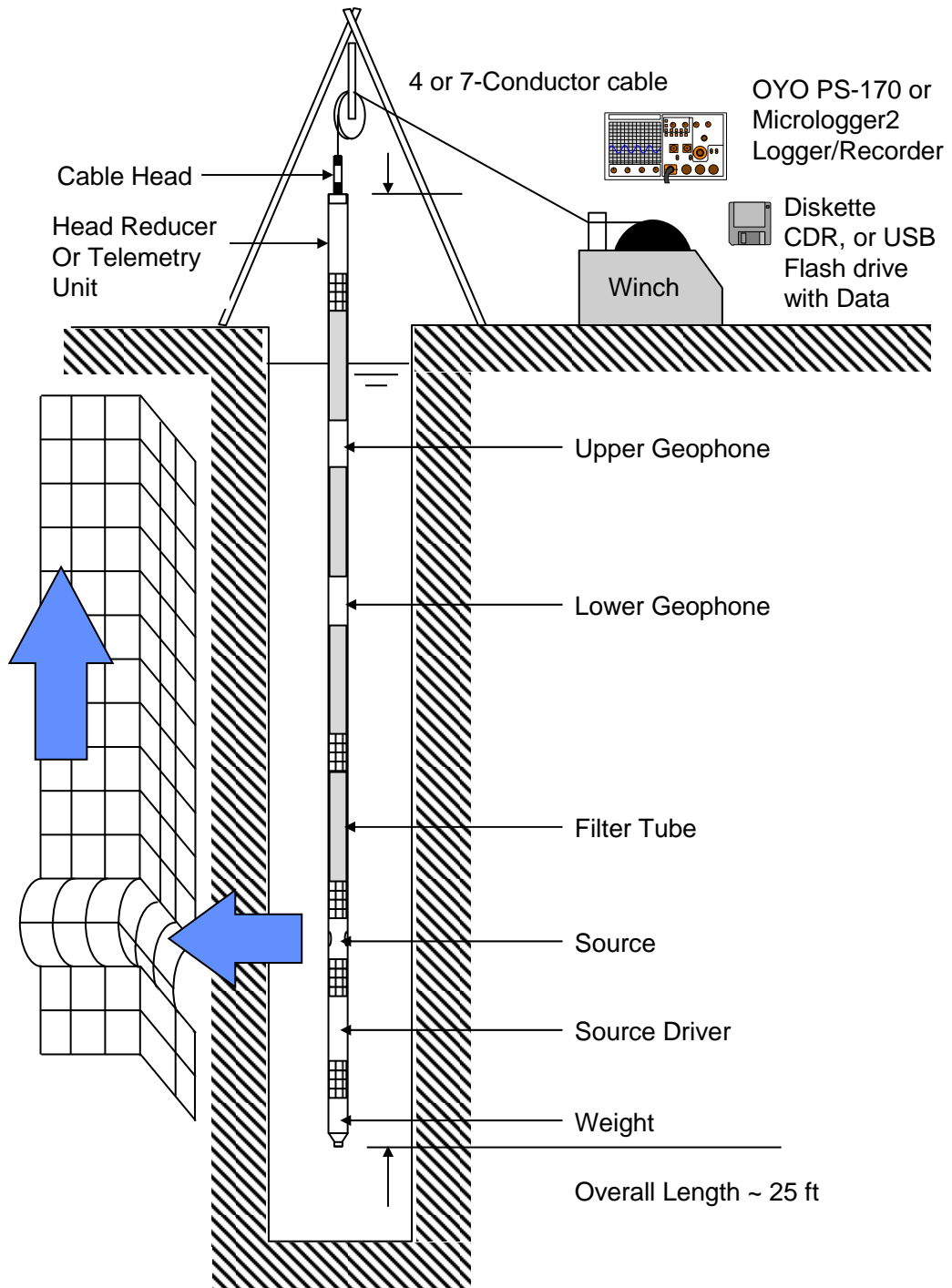


Figure 1: Concept illustration of Suspension P S logging system

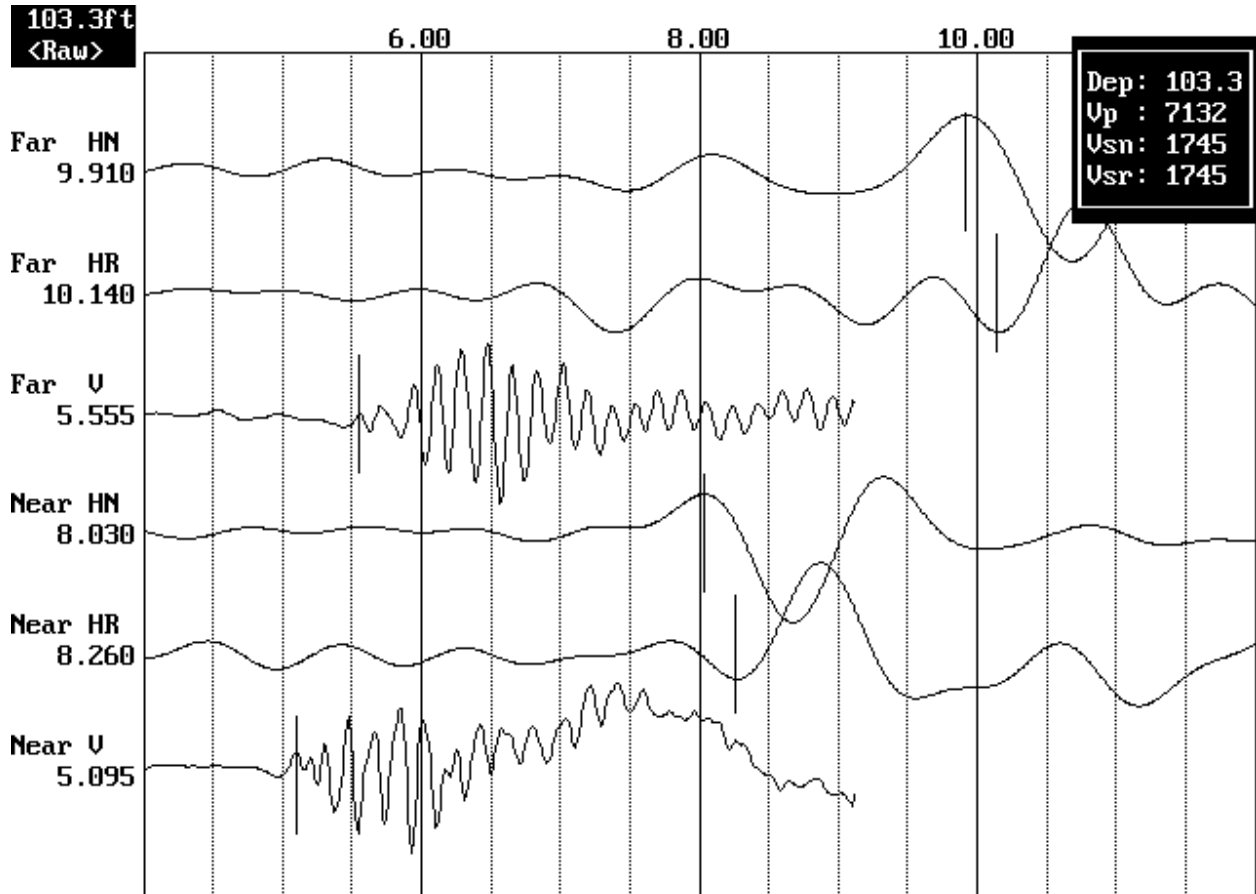


Figure 2: Example of filtered (1400 Hz lowpass) suspension record

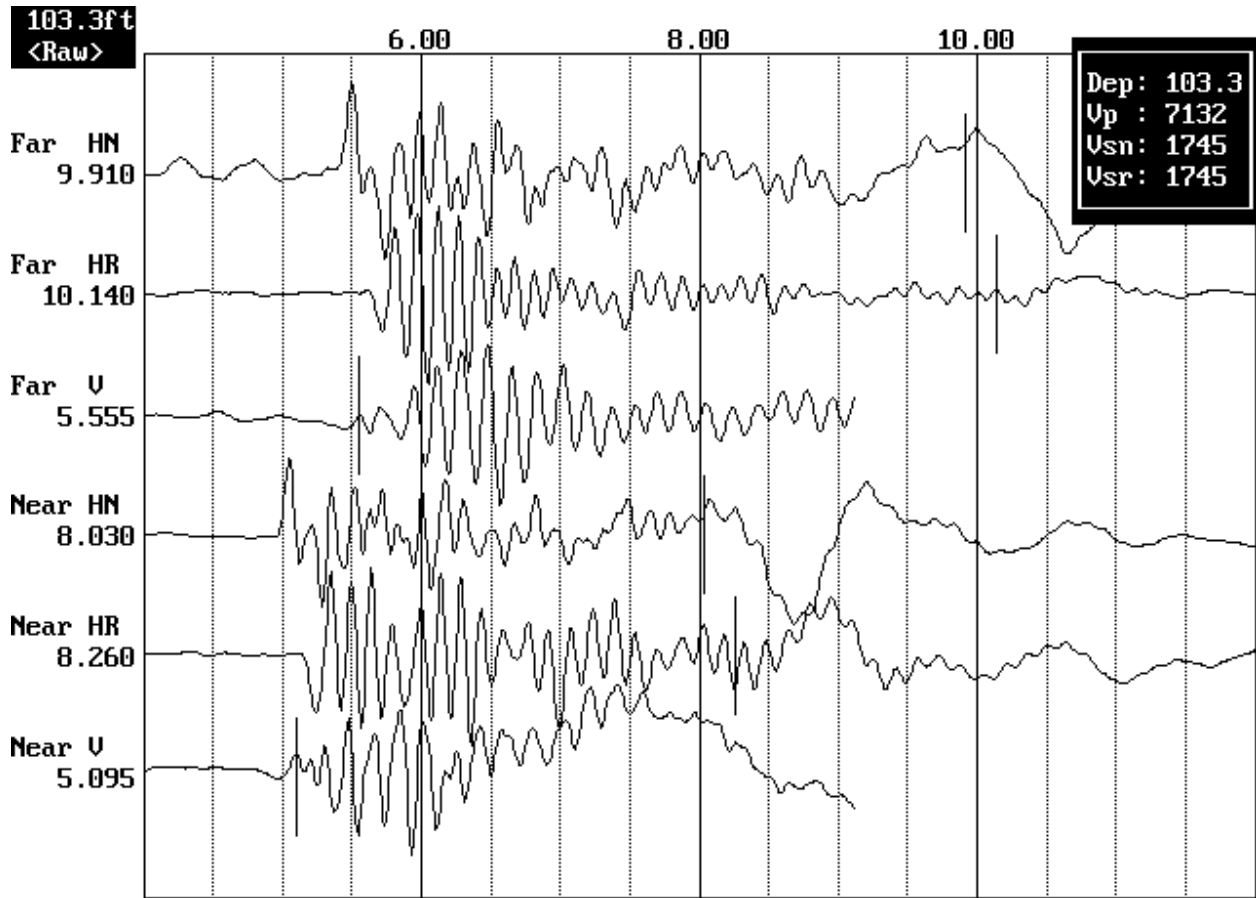


Figure 3. Example of unfiltered suspension record

# SR-710 BORING Z1-B3

## VELOCITY (METERS/SECOND)

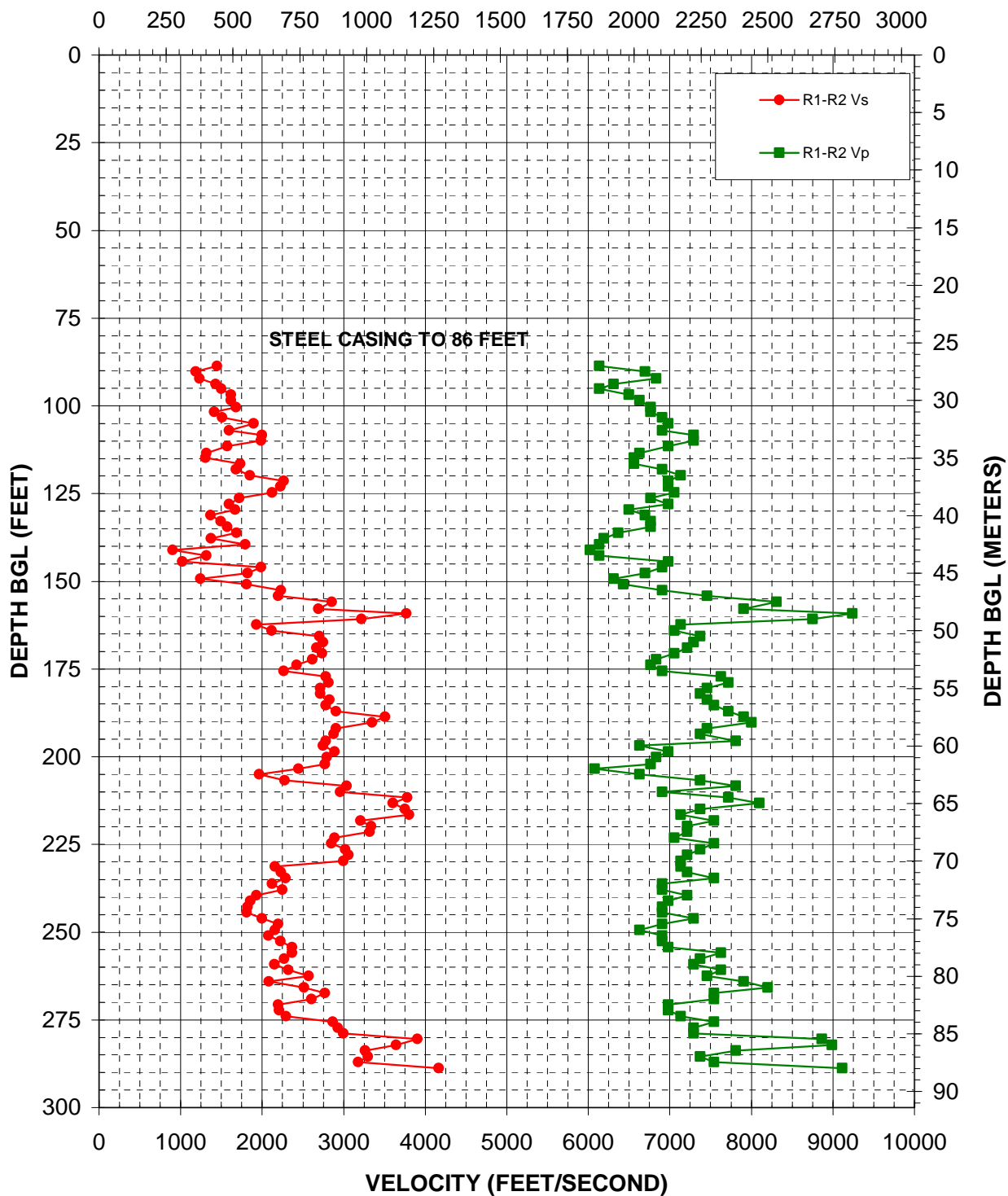


Figure 4: Boring Z1-B3, Suspension R1-R2 P- and  $S_H$ -wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
88.58	1445	6132	170.60	2734	7056	252.62	2224	6907
90.22	1189	6696	172.24	2614	6835	254.27	2369	6981
92.19	1229	6835	173.88	2421	6765	255.91	2369	7630
93.83	1433	6309	175.52	2263	6907	257.55	2270	7373
95.14	1498	6132	177.17	2780	7630	259.19	2151	7291
96.78	1616	6497	178.81	2816	7720	260.83	2319	7630
98.43	1616	6628	180.45	2711	7456	262.47	2573	7456
100.39	1682	6765	182.09	2711	7373	264.11	2083	7906
101.71	1414	6765	183.73	2828	7456	265.75	2514	8202
103.35	1512	6907	185.37	2780	7542	267.39	2769	7542
104.99	1896	6981	187.01	2903	7720	269.03	2604	7542
106.96	1593	6907	188.65	3509	7906	270.67	2195	6981
108.27	2001	7291	190.29	3348	8002	272.31	2209	6981
109.91	1988	7291	191.93	2903	7456	273.95	2294	7132
111.55	1570	6981	193.57	2878	7373	275.59	2865	7542
113.52	1318	6628	195.54	2780	7812	277.23	2929	7291
114.83	1307	6562	196.85	2745	6628	278.87	2996	7291
116.47	1731	6562	198.49	2891	6981	280.51	3906	8867
118.11	1678	6907	200.13	2792	6835	282.15	3645	8989
119.75	1848	7132	202.10	2769	6765	283.79	3265	7812
121.39	2263	6981	203.41	2448	6076	285.43	3297	7373
123.03	2224	6981	205.05	1965	6628	287.07	3178	7542
124.67	2124	7056	206.69	2278	7373	288.71	4166	9113
126.31	1722	6765	208.33	3038	7812			
127.95	1597	6981	209.97	2956	6907			
129.59	1670	6497	211.61	3782	7720			
131.23	1367	6696	213.25	3605	8101			
132.87	1491	6765	214.90	3750	7373			
134.51	1570	6765	216.54	3804	7132			
136.15	1687	6371	218.18	3209	7542			
137.80	1373	6190	219.82	3339	7211			
139.44	1793	6132	221.46	3322	7211			
141.08	901	6020	223.10	2891	7056			
142.72	1318	6132	224.74	2847	7542			
144.36	1022	6981	226.38	3017	7373			
146.00	1988	6907	228.02	3059	7211			
147.64	1823	6696	229.66	2996	7132			
149.28	1243	6309	231.30	2158	7132			
150.92	1813	6433	232.94	2232	7211			
152.56	2232	6907	234.58	2286	7542			
154.20	2195	7456	236.22	2124	6907			
155.84	2853	8306	237.86	2247	6907			
157.81	2689	7906	239.50	1930	7211			
159.12	3771	9242	241.14	1854	6981			
160.76	3217	8749	242.78	1823	6907			
162.40	1930	7132	244.42	1813	6907			
164.04	2117	7056	246.06	2001	7291			
165.68	2700	7373	247.70	2195	6907			
167.32	2745	7291	249.34	2158	6628			
168.96	2667	7211	250.98	2076	6907			

Table 4. Boring Z1-B3, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities



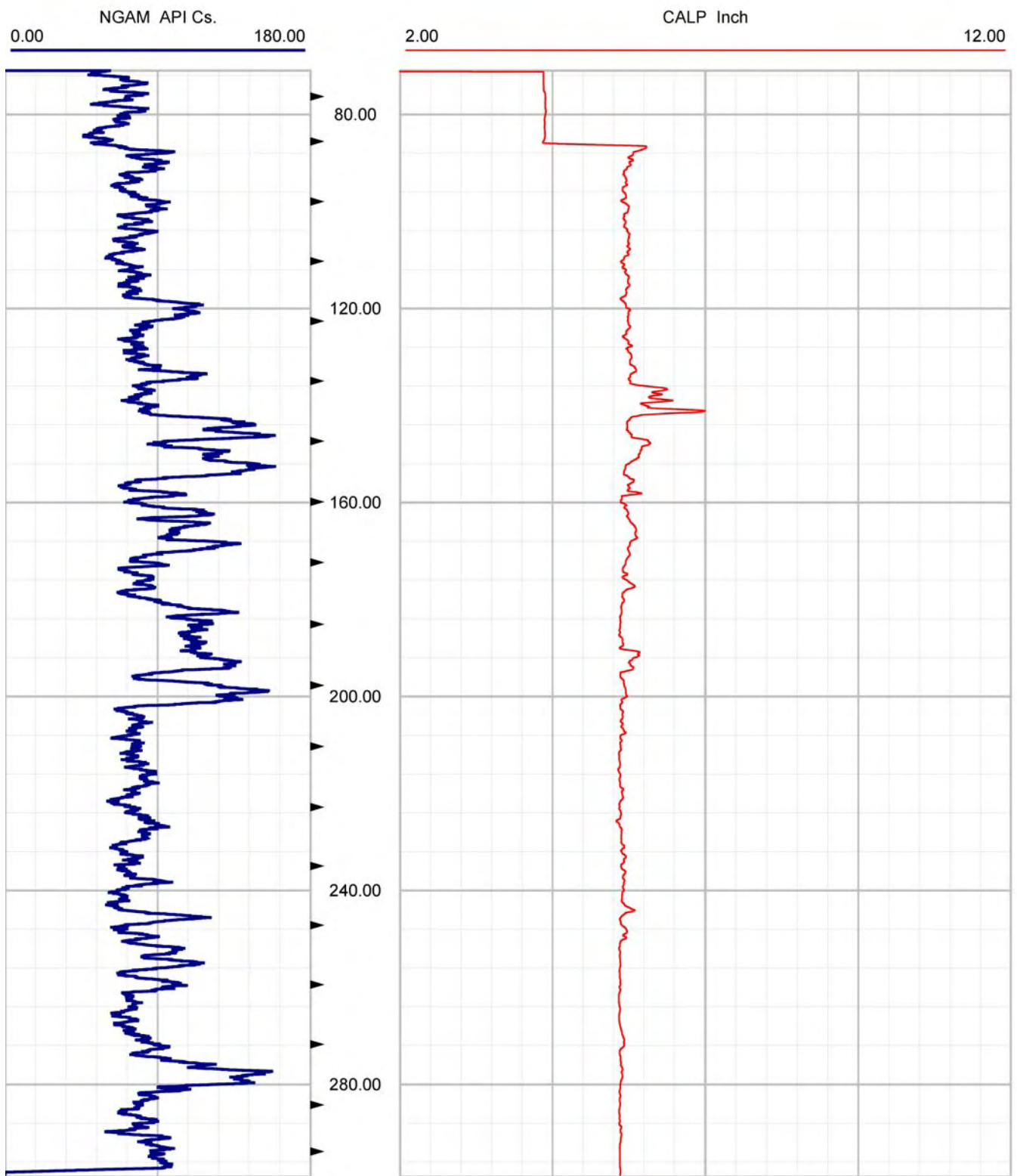


Figure 5. Boring Z1-B3, Caliper and Natural Gamma logs



CASCADE DRILLING

Borehole: Z1-B3

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 298.260 to 90.806ft  
 Mean dip format: dip-azimuth and dip

Interpretation 1

Dip data sets .....

BHTV dips

Z1-B3

Zone 0. 90.806 - 298.260ft  
 Deviation 0.80 N211.10

dipdata sets.....

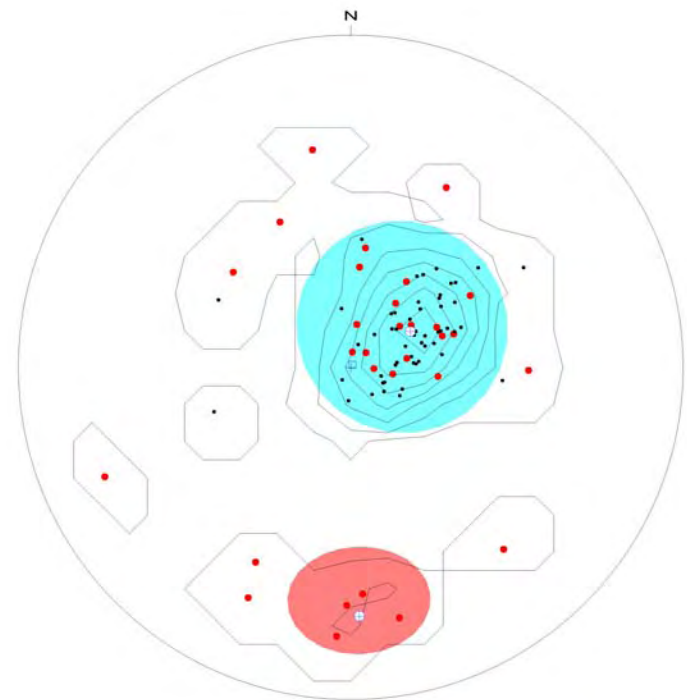
BHTV dips

• Highlighted dips: Fracture Planar Hairline-fracture

	mean dip	n	f
N059 17	N059 17	67	0.34
N178 64	N178 64	4	( 0.04)

intersections

	N059 17	N178 64
N059 17		14 N095
N178 64	14 N095	



⊕ mean dip  
 □ well axis  
 equal-area upper-hemisphere 0-90  
 contour-levels 1,3,6,10,15,21,28.

Figure 6. Boring Z1-B3, Stereonet Plot

Depth (feet)	Dip azimuth	Dip	Structure description
297.76	N039	17	Primary-structure Planar Bedding
296.77	N036	28	Primary-structure Planar Bedding
295.70	N120	14	Primary-structure Planar Bedding
294.66	N018	6	Primary-structure Planar Bedding
293.70	N142	8	Primary-structure Planar Bedding
292.24	N047	14	Primary-structure Planar Bedding
291.36	N113	14	Primary-structure Planar Bedding
290.90	N046	5	Fracture Planar Hairline-fracture
289.29	N087	11	Primary-structure Planar Bedding
283.19	N116	9	Primary-structure Planar Bedding
282.98	N080	15	Primary-structure Planar Bedding
282.62	N184	8	Primary-structure Planar Bedding
281.07	N068	24	Primary-structure Planar Bedding
280.42	N114	9	Primary-structure Planar Bedding
280.25	N081	14	Fracture Planar Hairline-fracture
279.48	N006	4	Fracture Planar Hairline-fracture
279.21	N093	6	Fracture Planar Hairline-fracture
277.41	N099	10	Fracture Planar Hairline-fracture
275.05	N070	29	Primary-structure Planar Bedding
273.23	N297	37	Primary-structure Planar Bedding
272.58	N069	14	Primary-structure Planar Bedding
265.19	N046	23	Primary-structure Planar Bedding
265.00	N038	29	Primary-structure Planar Bedding
263.87	N086	15	Primary-structure Planar Bedding
263.68	N061	18	Primary-structure Planar Bedding
259.97	N084	11	Primary-structure Planar Bedding
259.70	N071	18	Primary-structure Planar Bedding
259.27	N059	35	Fracture Planar Hairline-fracture
258.98	N065	23	Fracture Planar Hairline-fracture
254.67	N351	15	Primary-structure Planar Bedding
251.99	N106	8	Primary-structure Planar Bedding
251.65	N085	17	Primary-structure Planar Bedding
246.14	N058	18	Primary-structure Planar Bedding
245.71	N063	17	Primary-structure Planar Bedding
241.14	N037	17	Primary-structure Planar Bedding
203.70	N036	10	Primary-structure Planar Bedding
203.06	N126	10	Primary-structure Planar Bedding
200.15	N050	15	Primary-structure Planar Bedding
197.26	N087	16	Primary-structure Planar Bedding
178.99	N071	27	Primary-structure Planar Bedding
177.90	N214	4	Primary-structure Planar Bedding
169.87	N050	32	Primary-structure Planar Bedding
167.22	N056	27	Primary-structure Planar Bedding
166.67	N051	33	Primary-structure Planar Bedding
164.03	N052	40	Primary-structure Planar Bedding
161.49	N041	32	Primary-structure Planar Bedding
161.00	N033	25	Fracture Planar Hairline-fracture
160.46	N051	28	Primary-structure Planar Bedding
160.05	N206	55	Fracture Planar Hairline-fracture
159.65	N052	28	Primary-structure Planar Bedding

Table 5. Boring Z1-B3, Structure depth, dip azimuth, dip and description

Depth (feet)	Dip azimuth	Dip	Structure description
159.56	N204	65	Fracture Planar Hairline-fracture
159.42	N008	11	Fracture Planar Hairline-fracture
159.36	N177	58	Fracture Planar Hairline-fracture
159.23	N350	56	Fracture Planar Hairline-fracture
158.73	N007	30	Fracture Planar Hairline-fracture
158.50	N067	20	Primary-structure Planar Bedding
156.68	N309	38	Fracture Planar Hairline-fracture
156.03	N005	32	Primary-structure Planar Bedding
155.16	N055	18	Fracture Planar Hairline-fracture
154.75	N035	19	Fracture Planar Hairline-fracture
154.07	N334	40	Fracture Planar Hairline-fracture
152.96	N091	45	Fracture Planar Hairline-fracture
151.88	N050	16	Fracture Planar Hairline-fracture
143.95	N005	25	Fracture Planar Hairline-fracture
134.74	N028	51	Fracture Planar Hairline-fracture
131.98	N074	19	Primary-structure Planar Bedding
129.24	N181	61	Fracture Planar Hairline-fracture
123.13	N183	70	Fracture Planar Hairline-fracture
121.61	N072	27	Fracture Planar Hairline-fracture
120.20	N050	22	Primary-structure Planar Bedding
119.74	N051	19	Primary-structure Planar Bedding
119.24	N068	23	Primary-structure Planar Bedding
118.96	N071	24	Fracture Planar Hairline-fracture
118.83	N068	26	Primary-structure Planar Bedding
118.26	N074	21	Primary-structure Planar Bedding
117.97	N169	66	Fracture Planar Hairline-fracture
117.66	N082	23	Primary-structure Planar Bedding
110.46	N246	70	Fracture Planar Hairline-fracture
110.34	N058	30	Primary-structure Planar Bedding
109.77	N140	61	Fracture Planar Hairline-fracture
96.08	N252	36	Primary-structure Planar Bedding
96.08	N060	50	Primary-structure Planar Bedding
95.06	N095	38	Primary-structure Planar Bedding
91.31	N096	22	Fracture Planar Hairline-fracture

Table 5, continued. Boring Z1-B3, Structure depth, dip azimuth, dip and description

Deviated borehole in orthographic projection, viewed from N303



Figure 7. Boring Z1-B3, Deviation Projection

### SR-710 BORING Z1-B5

VELOCITY (METERS/SECOND)

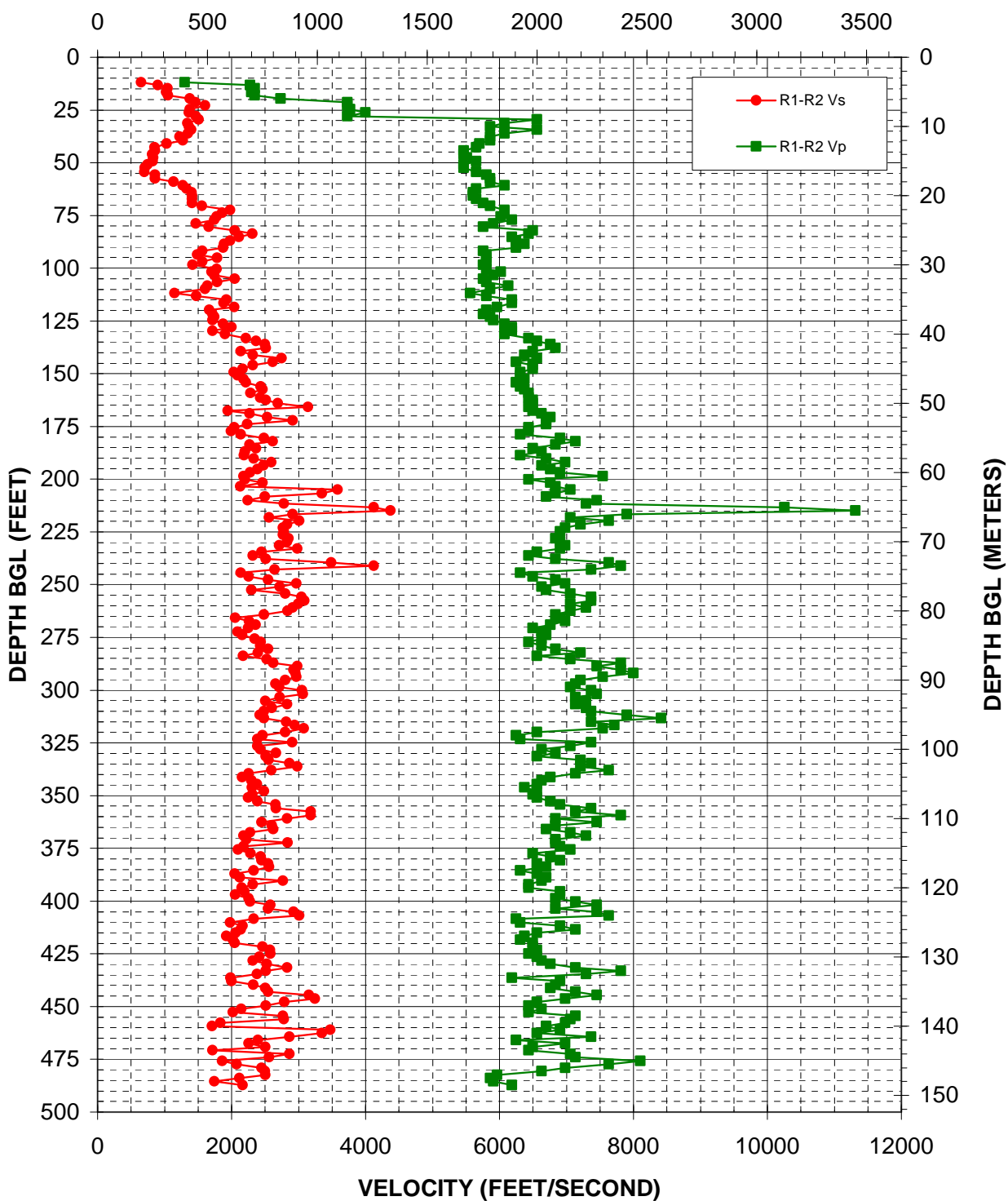


Figure 8: Boring Z1-B5, Suspension R1-R2 P- and S<sub>H</sub>-wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
11.81	651	1302	93.50	1485	5807	175.52	2044	6433
13.12	899	2278	95.14	1783	5807	177.17	1994	6433
14.76	1048	2343	96.78	1566	5807	178.81	2137	6309
16.40	1025	2294	98.43	1417	5756	180.45	2485	6907
18.04	1052	2343	100.39	1778	5807	182.09	2614	7132
19.69	1379	2734	101.71	1704	6020	183.73	2270	6835
21.33	1458	3728	103.35	1745	5911	185.37	2369	6497
22.97	1608	3728	104.99	2051	5756	187.01	2202	6628
24.61	1379	3771	106.63	1783	5807	188.65	2187	6309
26.25	1361	4001	108.27	1640	6132	190.29	2335	6696
27.89	1465	3728	109.91	1608	5859	191.93	2594	6981
29.53	1512	6562	111.88	1151	5561	193.57	2476	6628
31.17	1339	6076	113.19	1475	5807	195.21	2386	6765
32.81	1361	5859	114.83	1924	6190	196.85	2278	6907
34.45	1396	6562	116.47	1880	6190	198.49	2180	7542
36.09	1350	6076	118.44	2044	5965	200.13	2202	6433
37.73	1224	5859	119.75	1670	5807	201.77	2467	6765
39.37	1272	5859	121.72	1718	5756	203.41	2130	6835
41.01	1032	5706	123.03	1745	5859	205.05	3586	7056
42.65	854	5657	124.67	1713	5911	206.69	3348	6835
44.29	857	5468	126.31	1875	6076	208.33	2495	6696
45.93	814	5468	127.95	2001	6190	209.97	2239	7456
47.57	833	5514	129.59	1713	6190	211.61	2780	7291
49.21	822	5657	131.23	1902	6076	213.25	4127	10253
50.85	744	5468	133.20	2217	6433	214.90	4374	11313
52.49	706	5468	134.51	2369	6562	216.54	2916	7906
54.46	700	5657	136.15	2495	6765	218.18	2563	7056
55.77	857	5807	137.80	2514	6835	219.82	3010	7630
57.41	859	5859	139.44	2137	6497	221.46	2828	7211
59.06	1135	5859	141.08	2319	6371	223.10	2769	6981
60.70	1272	6076	142.72	2745	6562	224.74	2780	6907
62.34	1328	5657	144.36	2614	6249	226.38	2769	6907
63.98	1408	5608	146.00	2319	6497	228.02	2853	6835
65.62	1414	5608	147.64	2166	6497	229.66	2828	6907
67.26	1414	5657	149.28	2038	6309	231.30	2711	6981
69.23	1414	5756	150.92	2090	6309	232.94	2983	6907
70.54	1555	5859	152.56	2180	6371	234.58	2448	6562
72.51	1982	6076	154.20	2217	6249	236.22	2319	6433
73.82	1859	6076	156.17	2439	6309	237.86	2514	6835
75.46	1778	6020	157.48	2467	6371	239.50	3490	7630
77.10	1740	6190	159.12	2286	6433	241.14	4127	7812
78.74	1468	5911	161.42	2430	6433	242.78	2646	7373
80.38	1661	5756	162.40	2514	6497	244.42	2137	6309
82.02	2051	6497	164.04	2689	6497	246.06	2255	6497
83.66	2310	6433	165.68	3140	6433	247.70	2543	6835
85.30	2110	6190	167.65	1941	6497	249.34	2969	6981
86.94	1976	6249	168.96	2270	6628	250.98	2723	6628
88.58	1891	6371	170.60	2533	6765	252.62	2294	6696
90.22	1875	6249	172.24	2916	6696	254.27	2804	7056
91.86	1562	5756	173.88	2232	6696	255.91	3045	7373

Table 6. Boring Z1-B5, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
257.55	3088	7373	339.57	2255	7132	421.59	2467	6497
259.19	2996	7056	341.21	2158	6765	423.23	2573	6562
260.83	2916	7291	342.85	2294	6628	424.87	2583	6433
262.47	2841	7056	344.49	2377	6562	426.51	2412	6562
264.11	2485	6835	346.13	2302	6371	428.15	2319	6628
265.75	2057	6907	347.77	2485	6562	429.79	2524	6765
267.39	2263	6981	349.41	2310	6497	431.43	2828	7132
269.03	2360	6765	351.05	2247	6562	433.07	2514	7812
270.67	2247	6497	352.69	2386	6765	434.71	2377	7291
272.31	2090	6628	354.33	2657	6907	436.35	1988	6190
273.95	2158	6696	355.97	2667	7373	437.99	2001	6907
275.59	2343	6628	357.61	3185	7132	439.63	2327	6835
277.23	2439	6433	359.25	3185	7812	441.27	2504	6765
278.87	2430	6628	360.89	2828	6835	442.91	2543	7132
280.51	2543	6835	362.53	2448	7456	444.55	3155	7456
282.15	2395	7211	364.17	2604	6835	446.19	3248	6981
283.79	2173	6562	365.81	2625	6696	447.83	2792	6562
285.43	2524	7056	367.45	2278	7056	449.48	2514	6433
287.07	2625	7812	369.09	2180	7291	451.12	2144	6628
288.71	2983	7456	370.73	2224	6835	452.76	2019	6433
290.35	2929	7812	372.38	2841	6835	454.40	2769	7132
291.99	2956	8002	374.02	2180	6907	456.04	2780	7056
293.64	2969	7542	375.66	2096	7056	457.68	1833	6981
295.28	2804	7211	377.30	2286	6497	459.32	1709	6696
296.92	2657	7132	378.94	2439	6765	460.96	3472	6907
298.56	2711	7056	380.58	2448	6907	462.60	3348	6562
300.20	3052	7373	382.22	2543	6562	464.24	2865	7373
301.84	3066	7456	383.86	2563	6696	465.88	2395	6249
303.48	2723	7132	385.50	2335	6309	467.52	2255	6981
305.12	2504	7291	387.14	2051	6562	469.16	2504	6497
306.76	2828	7132	388.78	2124	6696	470.80	1713	6433
308.40	2604	7291	390.42	2769	6628	472.44	2865	7056
310.04	2485	7373	392.06	2319	6433	474.08	2563	7132
311.68	2421	7906	393.70	2151	6433	475.72	1859	8101
313.32	2485	8412	395.34	2195	6907	477.36	2076	7630
314.96	2816	7373	396.98	2057	6907	479.00	2448	6981
316.60	2942	7720	398.62	2255	6835	480.64	2495	6628
318.24	3081	7542	400.26	2278	7132	482.28	2504	5965
319.88	2804	6562	401.90	2583	7456	483.92	2117	5859
321.52	2467	6249	403.54	2543	6835	485.56	1740	5911
323.16	2386	6309	405.18	2929	7456	487.20	2166	6190
324.80	2903	7373	406.82	3010	7630			
326.44	2386	7056	408.46	2335	6249			
328.08	2430	6628	410.10	1982	6309			
329.72	2667	6835	411.75	2166	6907			
331.36	2514	6562	413.39	2137	7132			
333.01	2553	7211	415.03	2063	6562			
334.65	2865	7373	416.67	1924	6371			
336.29	2983	7211	418.31	2019	6309			
337.93	2594	7630	419.95	2051	6497			

Table 6, continued. Boring Z1-B5, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities



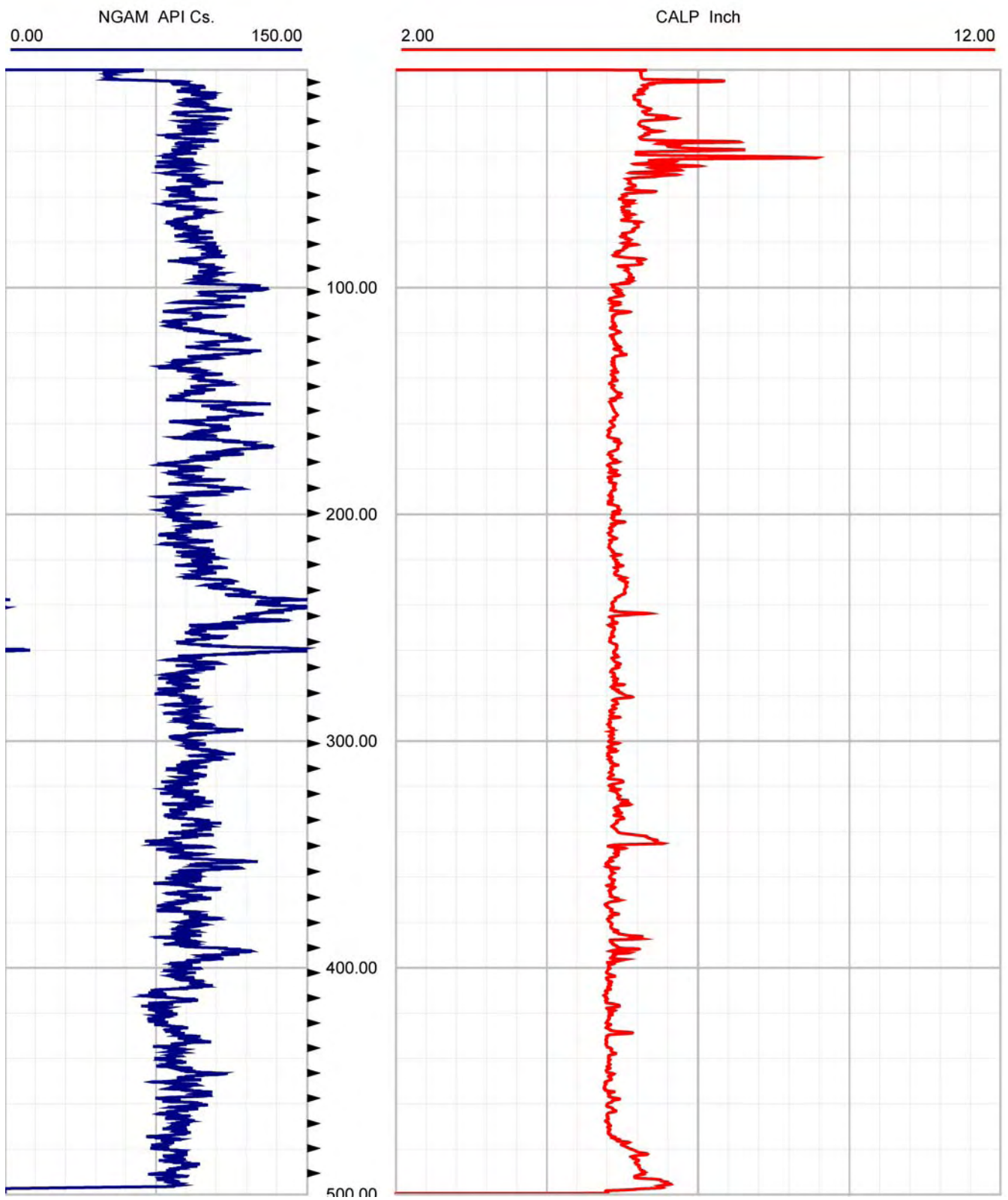


Figure 9. Boring Z1-B5, Caliper and Natural Gamma logs



CASCADE DRILLING

Borehole: Z1-B5

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 492.992 to 63.799ft  
 Mean dip format: dip-azimuth and dip

Interpretation 1

Dip data sets .....

BHTV dips

Z1-B5

Zone 0. 63.799 - 492.992ft  
 Deviation 0.50 N286.60

dipdata sets.....

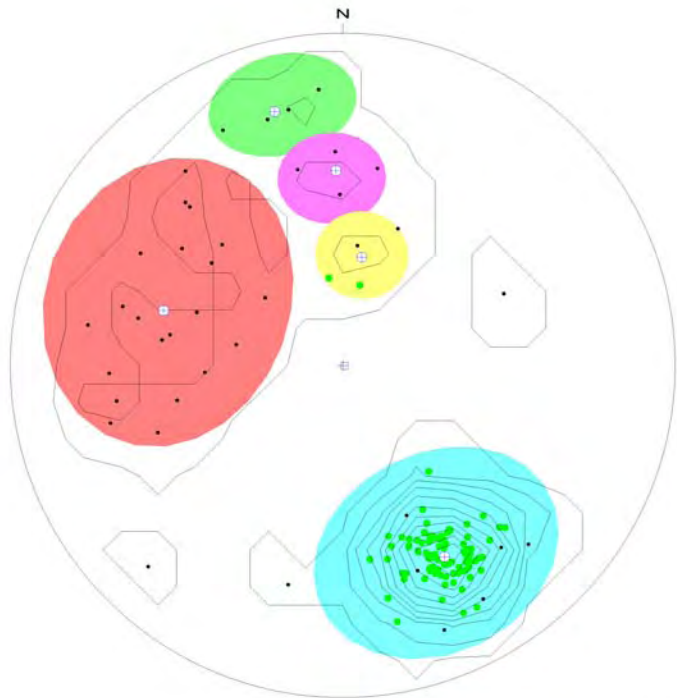
BHTV dips

Highlighted dips: Primary-structure Planar Bedding

	mean dip	n	f
N152 55	N152 55	101	0.41
N287 47	N287 47	21	( 0.07)
N345 68	N345 68	4	( 0.03)
N358 49	N358 49	4	( 0.01)
N010 27	N010 27	4	( 0.01)

Intersections

	N152 55	N287 47	N345 68	N358 49	N010 27
N152 55		25 N223	12 N070	16 N074	14 N072
N287 47	25 N223		47 N280	42 N320	26 N350
N345 68	12 N070	47 N280		25 N064	15 N069
N358 49	16 N074	42 N320	25 N064		10 N079
N010 27	14 N072	26 N350	15 N069	10 N079	



⊕ mean dip  
 □ well axis  
 equal-area upper-hemisphere 0-90  
 contour-levels 1,3,6,10,15,21,28,36,45,55,66.

Figure 10. Boring Z1-B5, Stereonet Plot

Depth (feet)	Dip azimuth	Dip	Structure description
492.49	N256	61	Fracture Planar Hairline-fracture
491.76	N139	62	Fracture Planar Hairline-fracture
491.09	N316	56	Fracture Planar Hairline-fracture
484.48	N308	42	Fracture Planar Hairline-fracture
482.56	N007	30	Fracture Planar Hairline-fracture
456.00	N351	22	Primary-structure Planar Bedding
455.47	N012	20	Primary-structure Planar Bedding
448.58	N154	72	Primary-structure Planar Bedding
444.73	N168	68	Primary-structure Planar Bedding
433.82	N157	66	Primary-structure Planar Bedding
409.76	N155	62	Primary-structure Planar Bedding
397.58	N151	72	Primary-structure Planar Bedding
394.65	N163	55	Primary-structure Planar Bedding
394.00	N224	73	Fracture Planar Hairline-fracture
389.37	N154	47	Primary-structure Planar Bedding
378.66	N152	60	Primary-structure Planar Bedding
378.28	N149	61	Primary-structure Planar Bedding
371.18	N153	63	Primary-structure Planar Bedding
370.51	N152	65	Primary-structure Planar Bedding
365.21	N164	55	Primary-structure Planar Bedding
364.16	N278	46	Fracture Planar Hairline-fracture
363.66	N281	27	Fracture Planar Hairline-fracture
363.60	N153	57	Primary-structure Planar Bedding
356.88	N137	52	Primary-structure Planar Bedding
355.81	N134	67	Fracture Planar Hairline-fracture
352.82	N147	49	Primary-structure Planar Bedding
339.13	N146	58	Primary-structure Planar Bedding
338.78	N290	39	Fracture Planar Hairline-fracture
338.67	N283	53	Fracture Planar Hairline-fracture
337.40	N147	60	Primary-structure Planar Bedding
336.92	N151	61	Primary-structure Planar Bedding
329.84	N160	55	Fracture Planar Hairline-fracture
329.12	N311	25	Fracture Planar Hairline-fracture
328.82	N066	44	Fracture Planar Hairline-fracture
328.61	N258	42	Fracture Planar Hairline-fracture
316.93	N146	55	Primary-structure Planar Bedding
316.22	N144	54	Primary-structure Planar Bedding
309.20	N140	58	Primary-structure Planar Bedding
306.25	N147	59	Primary-structure Planar Bedding
305.66	N146	57	Primary-structure Planar Bedding
302.64	N146	60	Primary-structure Planar Bedding
295.64	N148	61	Primary-structure Planar Bedding
294.97	N149	64	Primary-structure Planar Bedding
294.46	N146	64	Primary-structure Planar Bedding
292.59	N142	51	Primary-structure Planar Bedding
289.01	N152	57	Primary-structure Planar Bedding
287.53	N156	56	Primary-structure Planar Bedding
287.25	N157	57	Primary-structure Planar Bedding
282.11	N159	58	Primary-structure Planar Bedding
274.89	N359	43	Fracture Planar Hairline-fracture

Table 7. Boring Z1-B5, Structure depth, dip azimuth, dip and description

Depth (feet)	Dip azimuth	Dip	Structure description
269.78	N155	53	Primary-structure Planar Bedding
268.51	N155	53	Primary-structure Planar Bedding
264.22	N153	56	Primary-structure Planar Bedding
263.93	N152	57	Primary-structure Planar Bedding
261.91	N148	50	Primary-structure Planar Bedding
260.81	N151	57	Primary-structure Planar Bedding
260.58	N147	58	Primary-structure Planar Bedding
260.25	N136	57	Primary-structure Planar Bedding
259.01	N149	71	Fracture Planar Hairline-fracture
258.88	N172	49	Primary-structure Planar Bedding
257.37	N358	54	Fracture Planar Hairline-fracture
256.37	N169	61	Primary-structure Planar Bedding
255.42	N156	58	Primary-structure Planar Bedding
254.28	N147	57	Primary-structure Planar Bedding
253.48	N161	46	Primary-structure Planar Bedding
252.10	N145	57	Primary-structure Planar Bedding
251.25	N144	61	Primary-structure Planar Bedding
248.24	N299	59	Fracture Planar Hairline-fracture
248.00	N145	57	Primary-structure Planar Bedding
247.11	N010	50	Fracture Planar Hairline-fracture
247.09	N147	59	Primary-structure Planar Bedding
246.40	N148	59	Primary-structure Planar Bedding
241.94	N150	61	Primary-structure Planar Bedding
241.17	N154	60	Primary-structure Planar Bedding
240.07	N155	59	Primary-structure Planar Bedding
239.63	N156	58	Primary-structure Planar Bedding
237.91	N157	56	Primary-structure Planar Bedding
234.35	N267	34	Fracture Planar Hairline-fracture
232.74	N135	59	Primary-structure Planar Bedding
231.87	N150	59	Primary-structure Planar Bedding
228.24	N145	60	Primary-structure Planar Bedding
226.51	N159	74	Fracture Planar Hairline-fracture
225.75	N153	56	Primary-structure Planar Bedding
219.45	N355	72	Fracture Planar Hairline-fracture
213.65	N261	58	Fracture Planar Hairline-fracture
206.34	N280	44	Fracture Planar Hairline-fracture
203.73	N250	50	Fracture Planar Hairline-fracture
186.04	N306	50	Fracture Planar Hairline-fracture
183.20	N022	37	Fracture Planar Hairline-fracture
176.36	N141	34	Primary-structure Planar Bedding
176.05	N156	49	Primary-structure Planar Bedding
173.19	N160	49	Primary-structure Planar Bedding
171.44	N151	50	Primary-structure Planar Bedding
169.50	N167	50	Primary-structure Planar Bedding
168.40	N154	53	Primary-structure Planar Bedding
167.45	N152	52	Primary-structure Planar Bedding
164.20	N155	54	Primary-structure Planar Bedding
162.79	N147	57	Primary-structure Planar Bedding
162.58	N285	58	Fracture Planar Hairline-fracture
161.20	N157	41	Fracture Planar Hairline-fracture

Table 7, continued. Boring Z1-B5, Structure depth, dip azimuth, dip and description

Depth (feet)	Dip azimuth	Dip	Structure description
160.43	N165	47	Primary-structure Planar Bedding
156.33	N321	64	Fracture Planar Hairline-fracture
155.36	N156	52	Primary-structure Planar Bedding
153.83	N147	50	Primary-structure Planar Bedding
152.87	N152	45	Primary-structure Planar Bedding
151.94	N165	44	Primary-structure Planar Bedding
146.64	N152	49	Primary-structure Planar Bedding
144.99	N154	55	Primary-structure Planar Bedding
143.68	N156	54	Primary-structure Planar Bedding
143.32	N268	60	Fracture Planar Hairline-fracture
143.30	N279	67	Fracture Planar Hairline-fracture
143.28	N194	58	Fracture Planar Hairline-fracture
142.09	N159	47	Primary-structure Planar Bedding
133.86	N153	49	Primary-structure Planar Bedding
132.41	N150	50	Primary-structure Planar Bedding
129.57	N156	56	Primary-structure Planar Bedding
126.02	N150	51	Primary-structure Planar Bedding
125.38	N151	53	Primary-structure Planar Bedding
123.31	N315	43	Fracture Planar Hairline-fracture
123.22	N316	58	Fracture Planar Hairline-fracture
122.58	N157	48	Primary-structure Planar Bedding
121.16	N333	68	Fracture Planar Hairline-fracture
120.21	N347	51	Fracture Planar Hairline-fracture
120.11	N155	57	Primary-structure Planar Bedding
117.51	N348	68	Fracture Planar Hairline-fracture
117.26	N343	66	Fracture Planar Hairline-fracture
105.33	N164	57	Primary-structure Planar Bedding
101.18	N152	49	Primary-structure Planar Bedding
98.64	N150	52	Primary-structure Planar Bedding
95.72	N158	51	Primary-structure Planar Bedding
94.93	N160	48	Primary-structure Planar Bedding
94.55	N158	51	Primary-structure Planar Bedding
81.13	N151	41	Primary-structure Planar Bedding
79.88	N150	50	Primary-structure Planar Bedding
71.20	N146	58	Primary-structure Planar Bedding
64.61	N154	49	Primary-structure Planar Bedding
64.30	N153	48	Primary-structure Planar Bedding

Table 7, continued. Boring Z1-B5, Structure depth, dip azimuth, dip and description

Deviated borehole in orthographic projection, viewed from N22

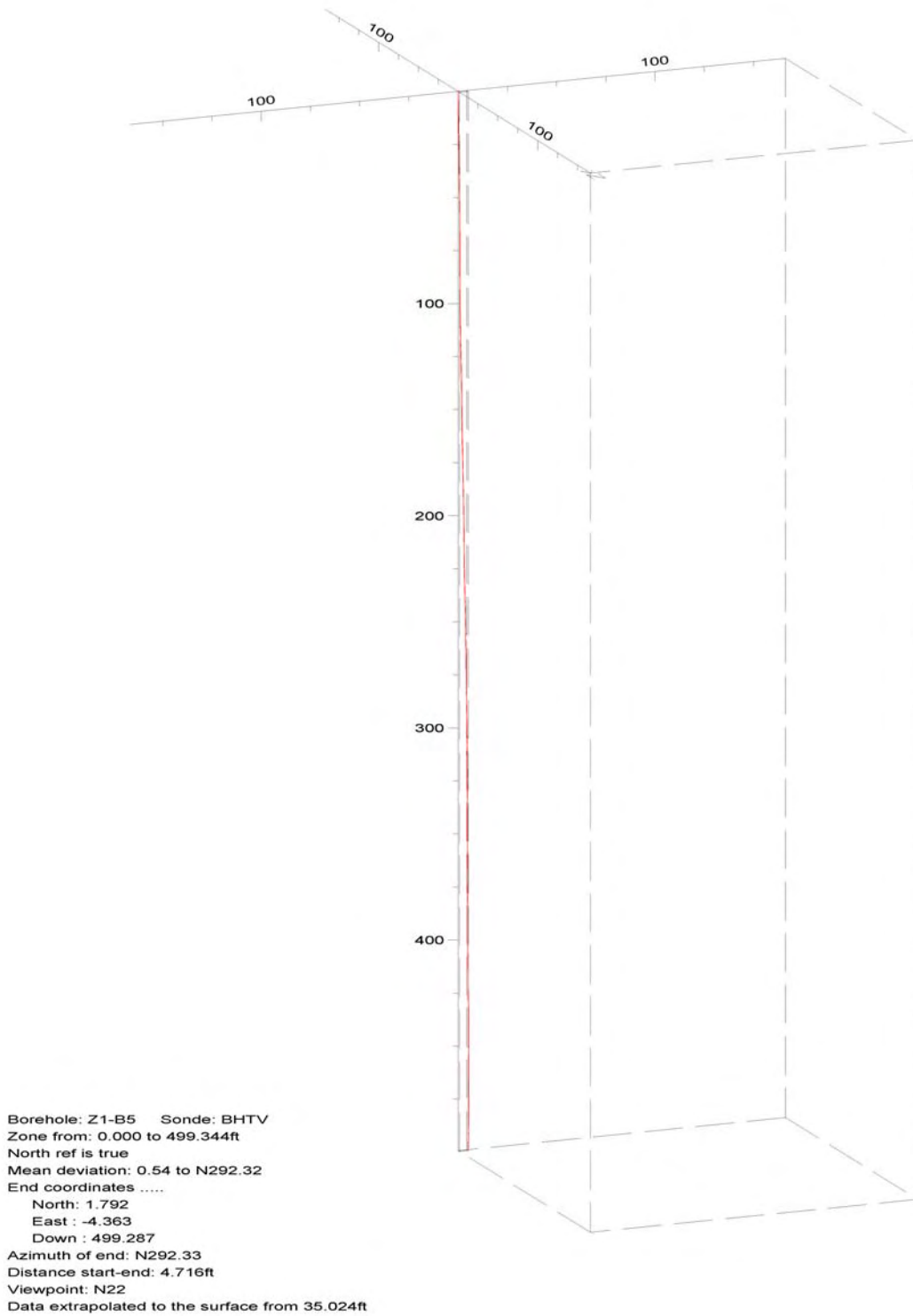


Figure 11. Boring Z1-B5, Deviation Projection

# SR-710 BORING Z1-B6

## VELOCITY (METERS/SECOND)

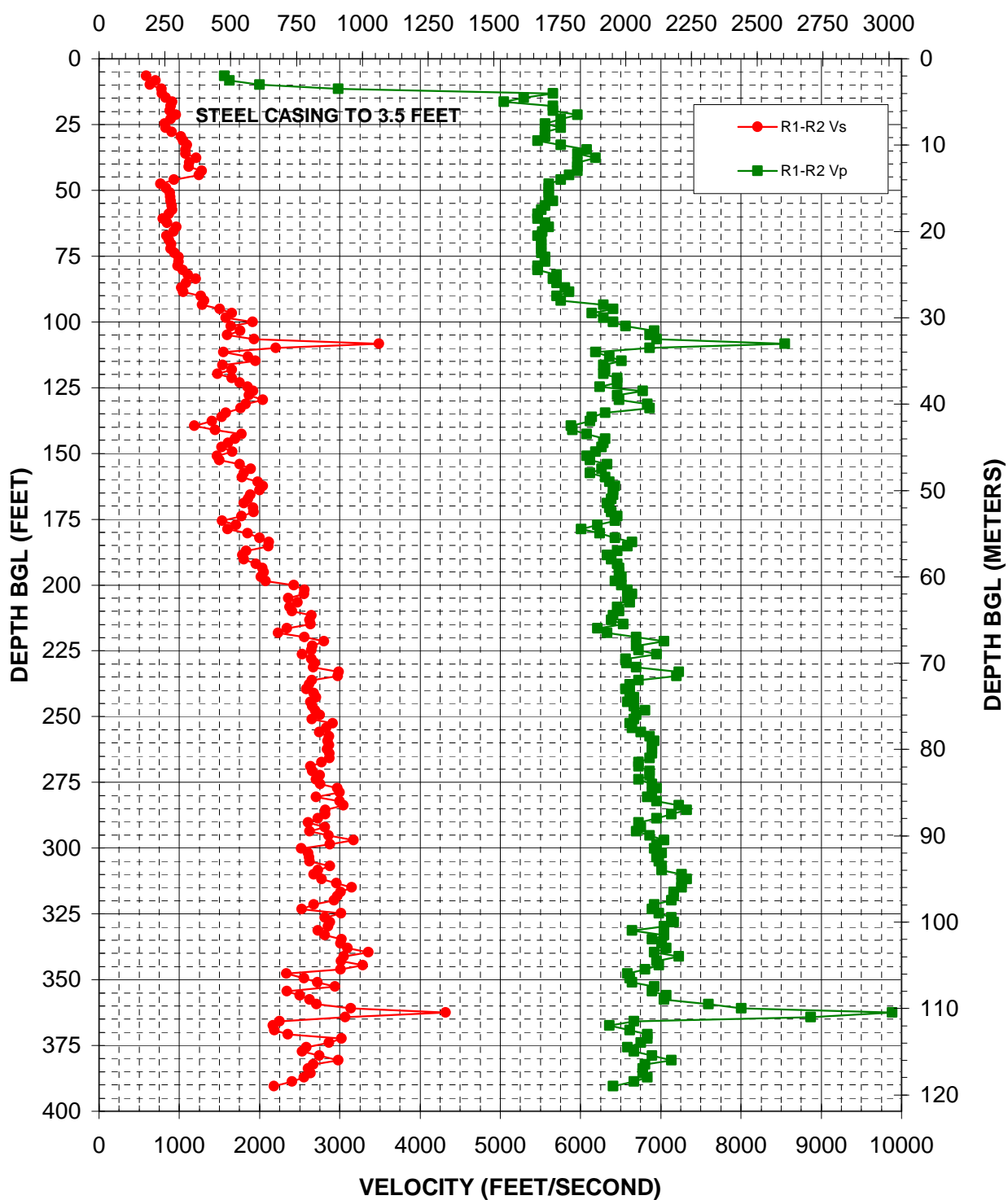


Figure 12: Boring Z1-B6, Suspension R1-R2 P- and  $S_H$ -wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
6.56	586	1562	88.58	1052	5859	170.60	1919	6358
8.20	702	1624	90.22	1267	5706	172.24	1924	6383
9.84	634	2001	91.86	1307	5756	173.88	1773	6458
11.48	777	2983	93.50	1284	6285	175.52	1537	6433
13.12	787	5657	95.14	1505	6408	177.17	1704	6214
14.76	828	5292	96.78	1653	6144	178.81	1604	6009
16.40	909	5047	98.43	1581	6285	180.45	1848	6237
18.04	894	5657	100.07	1913	6408	182.09	2001	6433
19.69	882	5657	101.71	1645	6562	183.73	2117	6641
21.33	957	5965	103.35	1759	6922	185.37	2110	6588
22.97	896	5756	104.99	1597	6864	187.01	1833	6458
24.61	818	5561	106.63	1930	6951	188.65	1788	6334
26.25	828	5756	108.27	3490	8544	190.29	1803	6383
27.89	904	5561	109.91	2202	6864	191.93	1953	6458
29.53	1022	5561	111.55	1551	6190	193.57	2038	6484
31.17	1048	5468	113.19	1859	6358	195.21	2051	6484
32.81	1094	5756	114.83	1947	6510	196.85	2019	6510
34.45	1076	6076	116.47	1540	6285	198.49	2076	6433
36.09	1079	5965	118.11	1653	6309	200.13	2430	6510
37.73	1211	6190	119.75	1475	6285	201.77	2563	6588
39.37	1127	5965	121.39	1653	6458	203.41	2553	6641
41.01	1116	5965	123.03	1754	6458	205.05	2360	6588
42.65	1282	5965	124.67	1848	6237	206.69	2476	6615
44.29	1247	5859	126.31	1919	6779	208.33	2377	6458
45.93	935	5756	127.95	1869	6458	209.97	2404	6484
47.57	767	5608	129.59	2044	6484	211.61	2646	6408
49.21	839	5608	131.23	1828	6835	213.25	2625	6383
50.85	880	5608	132.87	1764	6864	214.90	2635	6536
52.49	889	5608	134.51	1577	6309	216.54	2343	6214
54.13	896	5657	136.15	1526	6144	218.18	2232	6334
55.77	904	5561	137.80	1408	6121	219.82	2563	6696
57.41	911	5514	139.44	1189	5880	221.46	2804	7040
59.06	873	5468	141.08	1445	5901	223.10	2657	6696
60.70	798	5468	142.72	1773	6076	224.74	2646	6723
62.34	848	5561	144.36	1696	6309	226.38	2533	6951
63.98	962	5608	146.00	1608	6285	228.02	2646	6562
65.62	929	5523	147.64	1530	6261	229.66	2689	6575
67.26	843	5468	149.28	1661	6190	231.30	2667	6696
68.90	870	5514	150.92	1468	6076	232.94	2989	7227
70.54	899	5514	152.56	1498	6121	234.58	2976	7195
72.18	894	5514	154.20	1754	6334	236.22	2651	6723
73.82	943	5514	155.84	1891	6261	237.86	2619	6615
75.46	991	5561	157.48	1803	6121	239.50	2583	6562
77.10	994	5561	159.12	1783	6309	241.14	2678	6615
78.74	982	5468	160.76	1976	6358	242.78	2706	6668
80.38	1042	5468	162.40	2044	6433	244.42	2635	6588
82.02	1105	5706	164.04	2001	6408	246.06	2657	6668
83.66	1206	5657	165.68	1886	6408	247.70	2695	6807
85.30	1086	5706	167.32	1859	6383	249.34	2751	6696
86.94	1028	5807	168.96	1803	6334	250.98	2651	6668

Table 8. Boring Z1-B6, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities



Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
252.62	2910	6615	334.65	3024	6893
254.27	2834	6641	336.29	3010	7010
255.91	2745	6751	337.93	3095	7071
257.55	2865	6864	339.57	3356	6922
259.19	2847	6922	341.21	3052	7227
260.83	2865	6893	342.85	3017	6951
262.47	2841	6893	344.49	3289	6981
264.11	2872	6893	346.13	3010	6807
265.75	2872	6864	347.77	2335	6588
267.39	2774	6723	349.41	2553	6615
269.03	2635	6723	351.05	2723	6641
270.67	2657	6864	352.69	2942	6922
272.31	2751	6864	354.33	2343	6893
273.95	2706	6723	355.97	2504	7071
275.59	2757	6893	357.61	2625	7040
277.23	2969	6951	359.25	2711	7595
278.87	2996	6893	360.89	3140	8002
280.51	2706	6835	362.53	4317	9882
282.15	2996	6951	364.17	3066	8867
283.79	3045	7227	365.81	2247	6668
285.43	2822	7323	367.45	2166	6358
287.07	2822	7132	369.09	2187	6615
288.71	2728	6951	370.73	2352	6835
290.35	2604	6723	372.38	3024	6835
291.99	2816	6751	374.02	2865	6751
293.64	2625	6696	375.66	2583	6588
295.28	2859	6864	377.30	2533	6668
296.92	3170	7040	378.94	2745	6893
298.56	2878	6951	380.58	2983	7132
300.20	2519	6922	382.22	2667	6807
301.84	2604	7010	383.86	2604	6779
303.48	2619	6951	385.50	2635	6779
305.12	2625	6981	387.14	2553	6835
306.76	2878	7010	388.78	2404	6668
308.40	2728	7010	390.42	2180	6408
310.04	2678	7258			
311.68	2774	7323			
313.32	2956	7258			
314.96	3147	7258			
316.60	3010	7163			
318.24	2969	7163			
319.88	2929	7132			
321.52	2678	6922			
323.16	2524	6893			
324.80	3017	6981			
326.44	2816	7132			
328.08	2878	7163			
329.72	2853	7040			
331.36	2728	6641			
333.01	2816	7040			

Table 8, continued. Boring Z1-B6, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

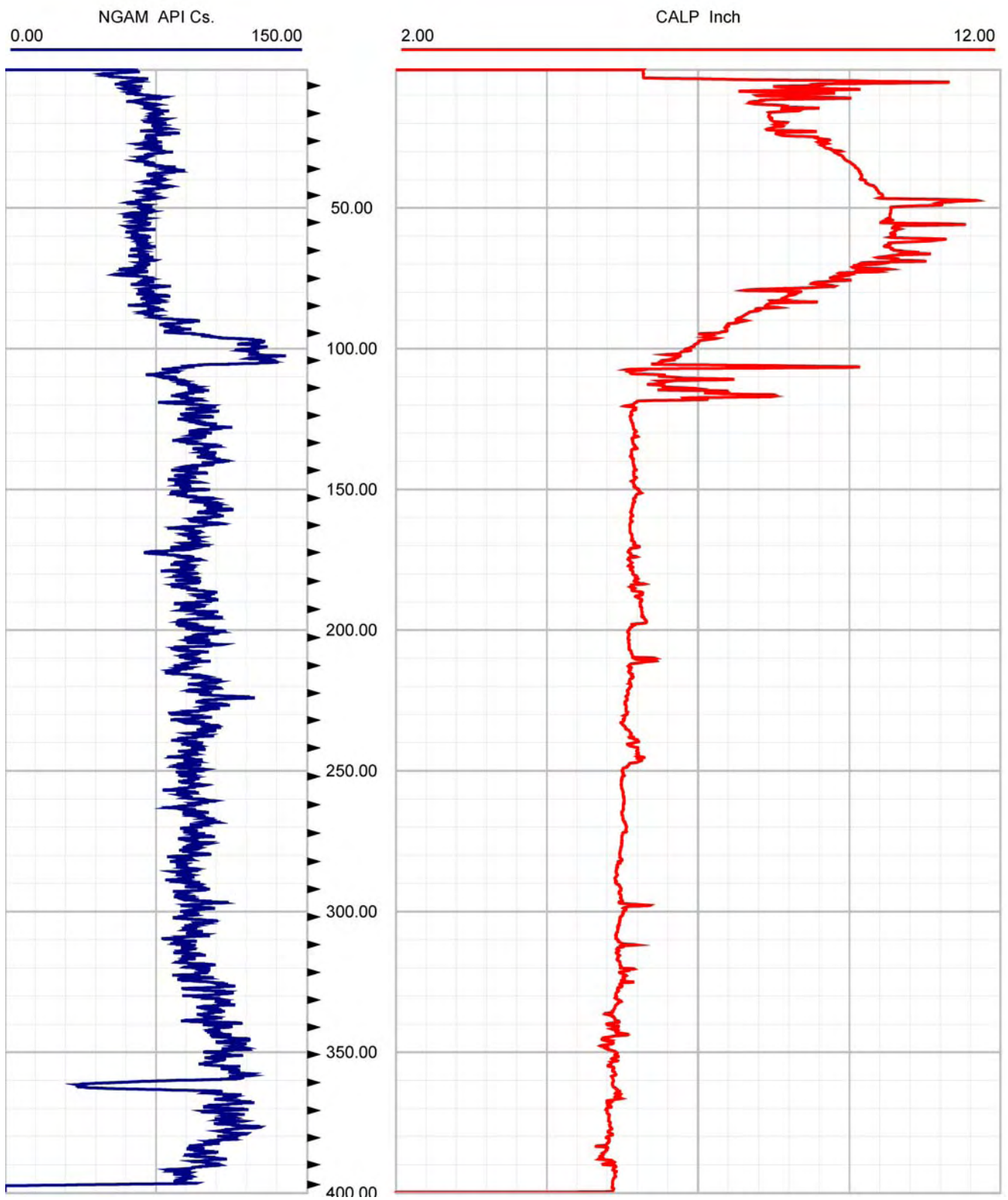


Figure 13. Boring Z1-B6 Caliper and Natural Gamma logs



CASCADE DRILLING

Borehole: Z1-B6

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 399.902 to 99.381ft  
 Mean dip format: dip-azimuth and dip

Interpretation 1

Dip data sets .....

BHTV dips

Z1-B6

Zone 0. 99.381 - 399.902ft  
 Deviation 1.20 N 19.70

dipdata sets.....

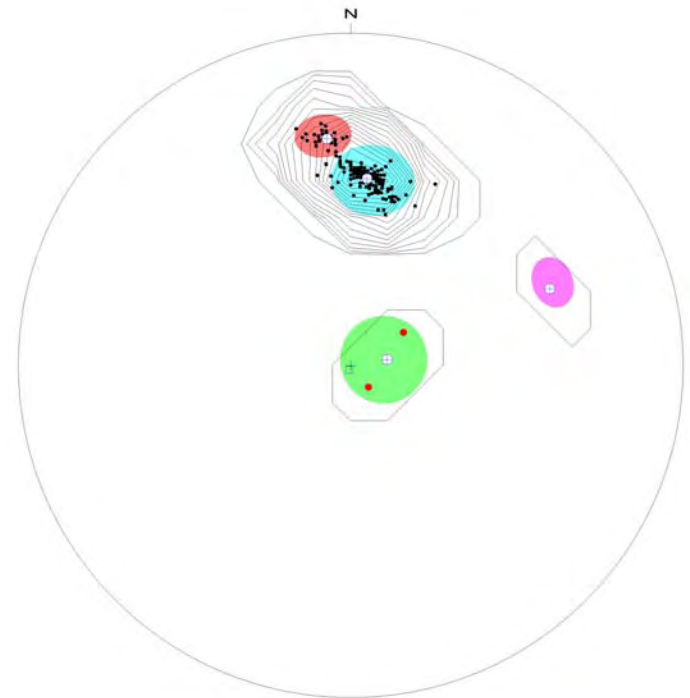
BHTV dips

• Highlighted dips: Fracture Planar Hairline-fracture

	mean dip	n	f
N005 47	N005 47	166	0.83
N354 58	N354 58	30	( 0.20)
N081 9	N081 9	2	( 0.01)
N069 54	N069 54	1	( 0.00)

intersections

	N005 47	N354 58	N081 9	N069 54
N005 47	X	29 N064	09 N087	45 N026
N354 58	29 N064	X	09 N078	49 N037
N081 9	09 N087	09 N078	X	02 N157
N069 54	45 N026	49 N037	02 N157	X



⊕ mean dip  
 □ well axis  
 equal-area upper-hemisphere 0-90  
 contour-levels 1.3,6,10,15,21,28,36,45,55,66,78,91,105,  
 120,136,153,

Figure 14. Boring Z1-B6, Stereonet Plot

Depth (feet)	Dip azimuth	Dip	Structure description
399.40	N014	43	Primary-structure Planar Bedding
398.62	N014	43	Primary-structure Planar Bedding
395.15	N016	43	Primary-structure Planar Bedding
394.89	N015	42	Primary-structure Planar Bedding
394.54	N015	44	Primary-structure Planar Bedding
394.24	N018	45	Primary-structure Planar Bedding
366.92	N022	43	Primary-structure Planar Bedding
360.52	N018	49	Primary-structure Planar Bedding
359.49	N010	51	Primary-structure Planar Bedding
351.68	N011	53	Primary-structure Planar Bedding
341.58	N010	46	Primary-structure Planar Bedding
340.43	N013	38	Primary-structure Planar Bedding
339.94	N012	40	Primary-structure Planar Bedding
339.16	N013	46	Primary-structure Planar Bedding
337.68	N010	44	Primary-structure Planar Bedding
336.75	N008	45	Primary-structure Planar Bedding
334.58	N354	45	Primary-structure Planar Bedding
332.26	N000	47	Primary-structure Planar Bedding
329.73	N002	47	Primary-structure Planar Bedding
329.28	N008	44	Primary-structure Planar Bedding
328.49	N069	54	Fracture Planar Hairline-fracture
327.66	N001	42	Primary-structure Planar Bedding
327.08	N005	41	Primary-structure Planar Bedding
325.88	N013	43	Primary-structure Planar Bedding
323.85	N007	43	Primary-structure Planar Bedding
322.62	N009	46	Primary-structure Planar Bedding
320.69	N013	45	Primary-structure Planar Bedding
320.46	N010	49	Primary-structure Planar Bedding
318.21	N008	44	Primary-structure Planar Bedding
316.24	N008	45	Primary-structure Planar Bedding
315.11	N009	44	Primary-structure Planar Bedding
314.34	N011	42	Primary-structure Planar Bedding
312.82	N012	45	Primary-structure Planar Bedding
311.07	N012	45	Primary-structure Planar Bedding
310.73	N008	44	Primary-structure Planar Bedding
309.98	N014	42	Primary-structure Planar Bedding
309.15	N012	42	Primary-structure Planar Bedding
308.20	N010	45	Primary-structure Planar Bedding
305.46	N006	43	Primary-structure Planar Bedding
303.83	N025	50	Primary-structure Planar Bedding
303.31	N010	39	Primary-structure Planar Bedding
300.74	N141	7	Fracture Planar Hairline-fracture
300.61	N008	48	Primary-structure Planar Bedding
300.02	N009	50	Primary-structure Planar Bedding
299.23	N006	45	Primary-structure Planar Bedding
298.28	N005	49	Primary-structure Planar Bedding
297.61	N006	48	Primary-structure Planar Bedding
297.02	N008	47	Primary-structure Planar Bedding
296.21	N006	45	Primary-structure Planar Bedding
295.97	N006	45	Primary-structure Planar Bedding

Table 9. Boring Z1-B6, Structure depth, dip azimuth, dip and description

Depth (feet)	Dip azimuth	Dip	Structure description
294.81	N005	46	Primary-structure Planar Bedding
294.37	N005	48	Primary-structure Planar Bedding
293.88	N005	47	Primary-structure Planar Bedding
293.51	N009	47	Primary-structure Planar Bedding
292.76	N006	46	Primary-structure Planar Bedding
291.99	N006	47	Primary-structure Planar Bedding
291.38	N002	47	Primary-structure Planar Bedding
290.83	N003	48	Primary-structure Planar Bedding
289.95	N007	47	Primary-structure Planar Bedding
288.90	N006	46	Primary-structure Planar Bedding
288.22	N009	44	Primary-structure Planar Bedding
287.54	N010	47	Primary-structure Planar Bedding
287.02	N008	45	Primary-structure Planar Bedding
285.48	N008	49	Primary-structure Planar Bedding
284.73	N008	46	Primary-structure Planar Bedding
284.34	N004	49	Primary-structure Planar Bedding
284.00	N008	47	Primary-structure Planar Bedding
282.91	N009	47	Primary-structure Planar Bedding
281.99	N007	48	Primary-structure Planar Bedding
281.70	N006	48	Primary-structure Planar Bedding
281.45	N008	45	Primary-structure Planar Bedding
281.00	N005	46	Primary-structure Planar Bedding
280.56	N008	47	Primary-structure Planar Bedding
278.88	N005	46	Primary-structure Planar Bedding
278.38	N005	46	Primary-structure Planar Bedding
277.00	N010	46	Primary-structure Planar Bedding
276.52	N008	47	Primary-structure Planar Bedding
275.60	N009	47	Primary-structure Planar Bedding
273.86	N006	48	Primary-structure Planar Bedding
272.07	N005	45	Primary-structure Planar Bedding
271.49	N009	47	Primary-structure Planar Bedding
270.23	N006	48	Primary-structure Planar Bedding
269.09	N009	48	Primary-structure Planar Bedding
268.95	N007	49	Primary-structure Planar Bedding
268.30	N007	49	Primary-structure Planar Bedding
267.98	N006	47	Primary-structure Planar Bedding
267.52	N007	47	Primary-structure Planar Bedding
266.81	N007	48	Primary-structure Planar Bedding
264.73	N007	49	Primary-structure Planar Bedding
264.49	N008	48	Primary-structure Planar Bedding
264.23	N004	49	Primary-structure Planar Bedding
262.88	N004	46	Primary-structure Planar Bedding
262.29	N006	47	Primary-structure Planar Bedding
261.89	N004	48	Primary-structure Planar Bedding
260.18	N008	47	Primary-structure Planar Bedding
259.22	N005	47	Primary-structure Planar Bedding
258.76	N005	47	Primary-structure Planar Bedding
258.32	N007	45	Primary-structure Planar Bedding
255.61	N002	49	Primary-structure Planar Bedding
254.61	N003	47	Primary-structure Planar Bedding

Table 9, continued. Boring Z1-B6, Structure depth, dip azimuth, dip and description

Depth (feet)	Dip azimuth	Dip	Structure description
253.28	N003	45	Primary-structure Planar Bedding
252.66	N003	48	Primary-structure Planar Bedding
251.34	N006	48	Primary-structure Planar Bedding
251.02	N000	45	Primary-structure Planar Bedding
249.76	N004	48	Primary-structure Planar Bedding
248.71	N004	50	Primary-structure Planar Bedding
247.72	N006	48	Primary-structure Planar Bedding
246.84	N008	48	Primary-structure Planar Bedding
246.11	N007	51	Primary-structure Planar Bedding
245.01	N006	47	Primary-structure Planar Bedding
243.33	N006	50	Primary-structure Planar Bedding
241.37	N008	48	Primary-structure Planar Bedding
239.96	N002	48	Primary-structure Planar Bedding
238.23	N010	49	Primary-structure Planar Bedding
237.50	N003	50	Primary-structure Planar Bedding
235.34	N006	47	Primary-structure Planar Bedding
234.85	N005	46	Primary-structure Planar Bedding
232.74	N356	46	Primary-structure Planar Bedding
232.39	N006	48	Primary-structure Planar Bedding
229.86	N003	50	Primary-structure Planar Bedding
229.00	N002	49	Primary-structure Planar Bedding
228.70	N002	49	Primary-structure Planar Bedding
226.87	N002	48	Primary-structure Planar Bedding
225.00	N003	48	Primary-structure Planar Bedding
221.60	N003	46	Primary-structure Planar Bedding
221.31	N000	48	Primary-structure Planar Bedding
219.50	N002	49	Primary-structure Planar Bedding
216.63	N001	47	Primary-structure Planar Bedding
216.11	N002	48	Primary-structure Planar Bedding
214.95	N360	49	Primary-structure Planar Bedding
214.32	N001	49	Primary-structure Planar Bedding
212.63	N001	50	Primary-structure Planar Bedding
209.61	N005	47	Primary-structure Planar Bedding
207.20	N004	48	Primary-structure Planar Bedding
206.57	N001	48	Primary-structure Planar Bedding
204.89	N001	49	Primary-structure Planar Bedding
201.54	N001	49	Primary-structure Planar Bedding
197.68	N005	49	Primary-structure Planar Bedding
196.80	N360	51	Primary-structure Planar Bedding
194.95	N003	51	Primary-structure Planar Bedding
192.84	N001	50	Primary-structure Planar Bedding
191.22	N002	49	Primary-structure Planar Bedding
189.90	N003	49	Primary-structure Planar Bedding
189.05	N001	50	Primary-structure Planar Bedding
188.07	N360	50	Primary-structure Planar Bedding
186.45	N001	48	Primary-structure Planar Bedding
184.33	N357	50	Primary-structure Planar Bedding
182.87	N357	52	Primary-structure Planar Bedding
181.27	N001	49	Primary-structure Planar Bedding
179.84	N001	49	Primary-structure Planar Bedding

Table 9, continued. Boring Z1-B6, Structure depth, dip azimuth, dip and description

Depth (feet)	Dip azimuth	Dip	Structure description
178.52	N002	50	Primary-structure Planar Bedding
176.20	N358	50	Primary-structure Planar Bedding
175.51	N350	49	Primary-structure Planar Bedding
174.39	N002	49	Primary-structure Planar Bedding
172.42	N357	51	Primary-structure Planar Bedding
171.55	N357	50	Primary-structure Planar Bedding
170.48	N354	48	Primary-structure Planar Bedding
169.66	N001	50	Primary-structure Planar Bedding
168.25	N058	15	Fracture Planar Hairline-fracture
166.95	N003	50	Primary-structure Planar Bedding
165.58	N002	49	Primary-structure Planar Bedding
164.51	N001	49	Primary-structure Planar Bedding
163.60	N360	51	Primary-structure Planar Bedding
162.54	N358	49	Primary-structure Planar Bedding
160.88	N003	48	Primary-structure Planar Bedding
159.74	N357	50	Primary-structure Planar Bedding
158.43	N360	50	Primary-structure Planar Bedding
157.47	N002	49	Primary-structure Planar Bedding
156.46	N357	51	Primary-structure Planar Bedding
154.82	N359	51	Primary-structure Planar Bedding
154.00	N357	53	Primary-structure Planar Bedding
152.88	N357	51	Primary-structure Planar Bedding
152.36	N356	53	Primary-structure Planar Bedding
149.94	N004	49	Primary-structure Planar Bedding
148.61	N360	49	Primary-structure Planar Bedding
146.74	N353	51	Primary-structure Planar Bedding
143.94	N356	54	Primary-structure Planar Bedding
142.99	N353	51	Primary-structure Planar Bedding
142.29	N354	55	Primary-structure Planar Bedding
140.89	N356	56	Primary-structure Planar Bedding
140.54	N356	57	Primary-structure Planar Bedding
140.19	N356	56	Primary-structure Planar Bedding
137.53	N358	58	Primary-structure Planar Bedding
136.31	N354	60	Primary-structure Planar Bedding
135.80	N356	58	Primary-structure Planar Bedding
134.95	N351	60	Primary-structure Planar Bedding
134.77	N353	60	Primary-structure Planar Bedding
133.64	N349	58	Primary-structure Planar Bedding
133.49	N351	58	Primary-structure Planar Bedding
132.63	N354	58	Primary-structure Planar Bedding
132.25	N351	56	Primary-structure Planar Bedding
131.67	N352	58	Primary-structure Planar Bedding
131.27	N349	60	Primary-structure Planar Bedding
130.64	N352	59	Primary-structure Planar Bedding
130.00	N355	59	Primary-structure Planar Bedding
129.39	N356	60	Primary-structure Planar Bedding
129.17	N353	61	Primary-structure Planar Bedding
128.88	N354	60	Primary-structure Planar Bedding
126.96	N352	58	Primary-structure Planar Bedding
125.48	N354	57	Primary-structure Planar Bedding

Table 9, continued. Boring Z1-B6, Structure depth, dip azimuth, dip and description

Depth (feet)	Dip azimuth	Dip	Structure description
125.12	N353	58	Primary-structure Planar Bedding
123.49	N354	60	Primary-structure Planar Bedding
122.27	N359	58	Primary-structure Planar Bedding
120.71	N355	57	Primary-structure Planar Bedding
117.50	N353	62	Primary-structure Planar Bedding
108.96	N348	59	Primary-structure Planar Bedding
107.77	N354	62	Primary-structure Planar Bedding
99.88	N347	62	Primary-structure Planar Bedding

Table 9, continued. Boring Z1-B6, Structure depth, dip azimuth, dip and description



Deviated borehole in orthographic projection, viewed from N121

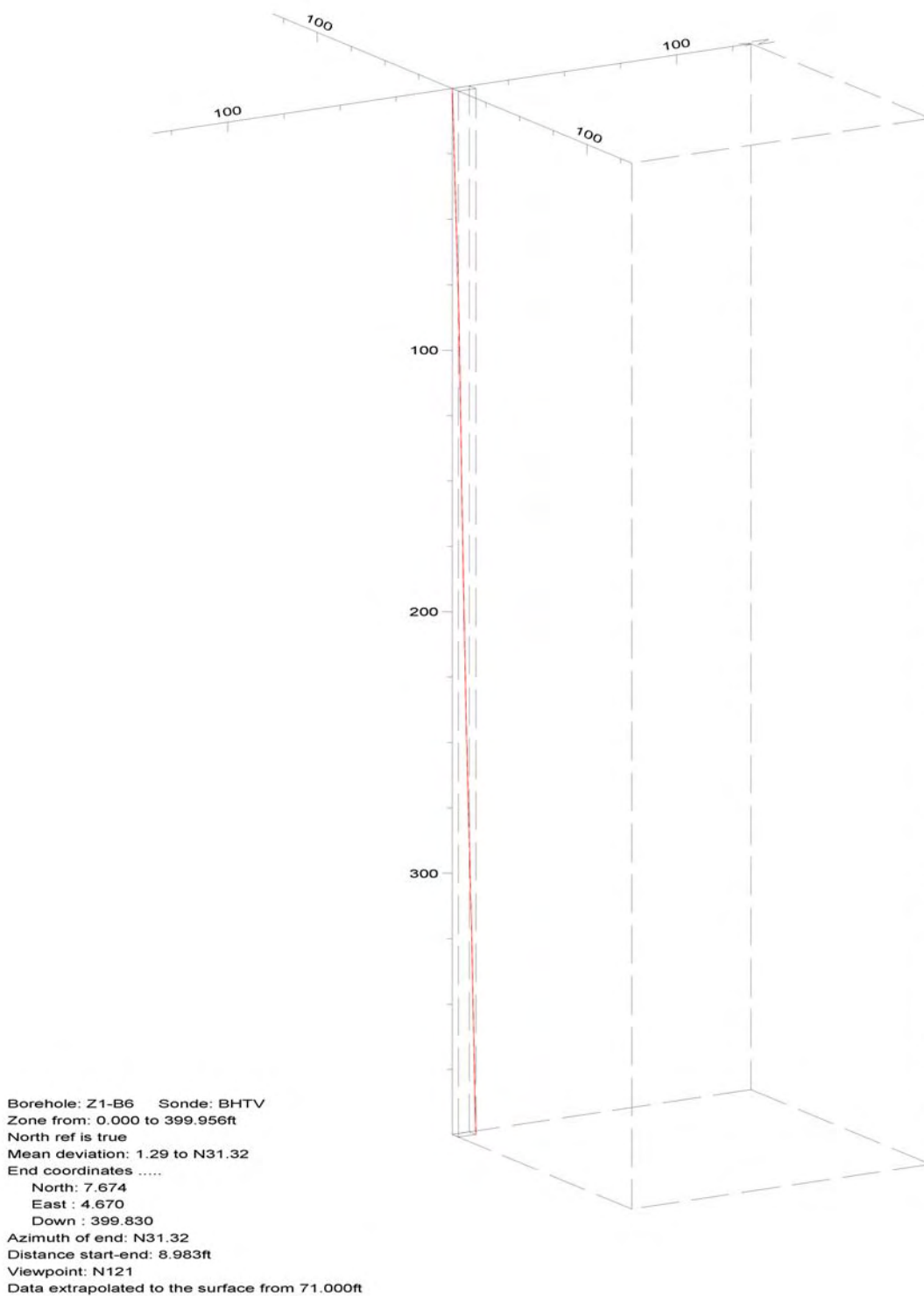


Figure 15. Boring Z1-B6, Deviation Projection

# SR-710 BORING Z1-B7

## VELOCITY (METERS/SECOND)

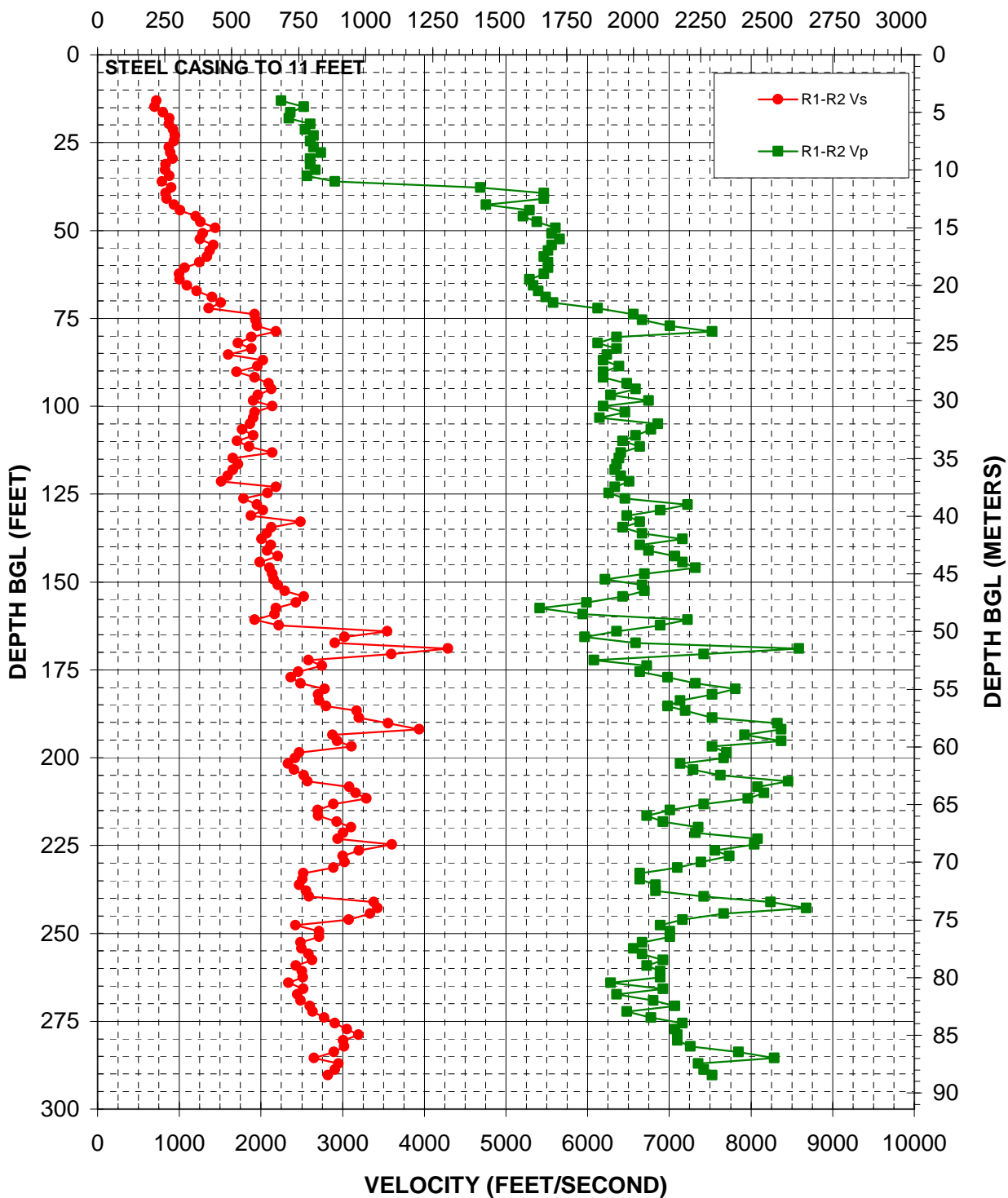


Figure 16: Boring Z1-B7, Suspension R1-R2 P- and S<sub>H</sub>-wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
13.12	721	2247	95.14	2130	6588	177.17	2369	6981
14.76	697	2524	96.78	1965	6285	178.81	2485	7323
16.40	802	2360	98.43	1907	6751	180.45	2780	7812
18.04	882	2343	100.07	2137	6190	182.09	2700	7525
19.69	875	2604	101.71	1924	6458	183.73	2711	7132
21.33	924	2543	103.35	1907	6144	185.37	2798	6981
22.97	948	2646	104.99	1869	6864	186.68	3170	7195
24.61	937	2604	106.63	1773	6779	188.65	3201	7525
26.25	875	2646	108.27	1907	6588	190.29	3556	8327
27.89	889	2734	109.91	1709	6433	191.93	3941	8369
29.53	922	2604	111.55	1854	6641	193.57	2878	7925
31.17	833	2604	113.19	2137	6408	195.21	2936	8369
32.81	831	2667	114.83	1657	6383	196.85	3110	7525
34.45	877	2563	116.47	1722	6358	198.49	2471	7701
36.09	789	2903	118.11	1657	6334	200.13	2417	7666
37.73	904	4687	119.75	1593	6408	201.77	2335	7132
39.37	837	5468	121.39	1515	6510	203.41	2404	7291
41.01	846	5468	123.03	2187	6334	205.05	2524	7630
42.65	935	4755	124.67	2083	6261	206.69	2573	8456
44.29	1009	5292	126.31	1788	6458	208.33	3081	8081
45.93	1202	5208	127.95	1953	7227	209.97	3162	8161
47.57	1262	5378	129.59	2025	6893	211.61	3289	7963
49.21	1442	5608	131.23	1880	6484	213.25	2891	7423
50.85	1289	5561	132.87	2485	6641	214.90	2695	7010
52.49	1252	5657	134.51	2130	6433	216.54	2700	6723
54.13	1417	5561	136.15	2070	6668	218.18	2929	6922
55.77	1376	5514	137.80	2007	7163	219.82	3102	7356
57.41	1339	5468	139.44	2124	6641	221.46	3010	7323
59.06	1247	5514	141.08	2076	6751	223.10	2942	8081
60.70	1069	5514	142.72	2209	7071	224.74	3605	8041
62.34	999	5468	144.36	1988	7163	226.38	3201	7560
63.98	1005	5292	146.00	2103	7323	228.02	3003	7738
65.62	1097	5335	147.64	2137	6696	229.66	3024	7389
67.26	1213	5396	149.28	2158	6214	231.30	2891	7101
68.90	1399	5486	150.92	2209	6668	232.94	2519	6641
70.54	1512	5580	152.56	2294	6696	234.58	2509	6641
72.18	1364	6121	154.20	2524	6433	236.22	2471	6835
73.82	1924	6562	155.84	2430	5987	237.86	2552	6835
75.46	1936	6668	157.48	2187	5414	239.50	2588	7423
77.10	1953	7010	159.12	2166	5944	241.14	3382	8243
78.74	2187	7525	160.76	1921	7227	242.78	3426	8679
80.38	1886	6358	162.40	2221	6893	244.42	3339	7666
82.02	1722	6121	164.04	3547	6358	246.06	3073	7163
83.66	1886	6358	165.68	3024	5965	247.70	2421	6893
85.30	1600	6237	167.32	2903	6588	249.34	2711	7010
86.94	2025	6190	168.96	4289	8589	250.98	2711	7010
88.58	1959	6383	170.60	3595	7423	252.62	2485	6668
90.22	1704	6190	172.24	2583	6076	254.27	2495	6562
91.86	1924	6190	173.88	2745	6723	255.91	2583	6668
93.50	2096	6484	175.52	2458	6641	257.55	2630	6922

Table 10. Boring Z1-B7, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
259.19	2430	6723
260.83	2504	6893
262.47	2514	6893
264.11	2339	6285
265.75	2519	6922
267.39	2444	6358
269.03	2485	6807
270.67	2599	7071
272.31	2635	6484
273.95	2774	6779
275.59	2903	7163
277.23	3052	7071
278.87	3193	7101
280.51	3010	7101
282.15	3017	7258
283.79	2897	7849
285.43	2649	8285
287.07	2949	7356
288.71	2903	7423
290.35	2822	7525

Table 10, continued. Boring Z1-B7, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

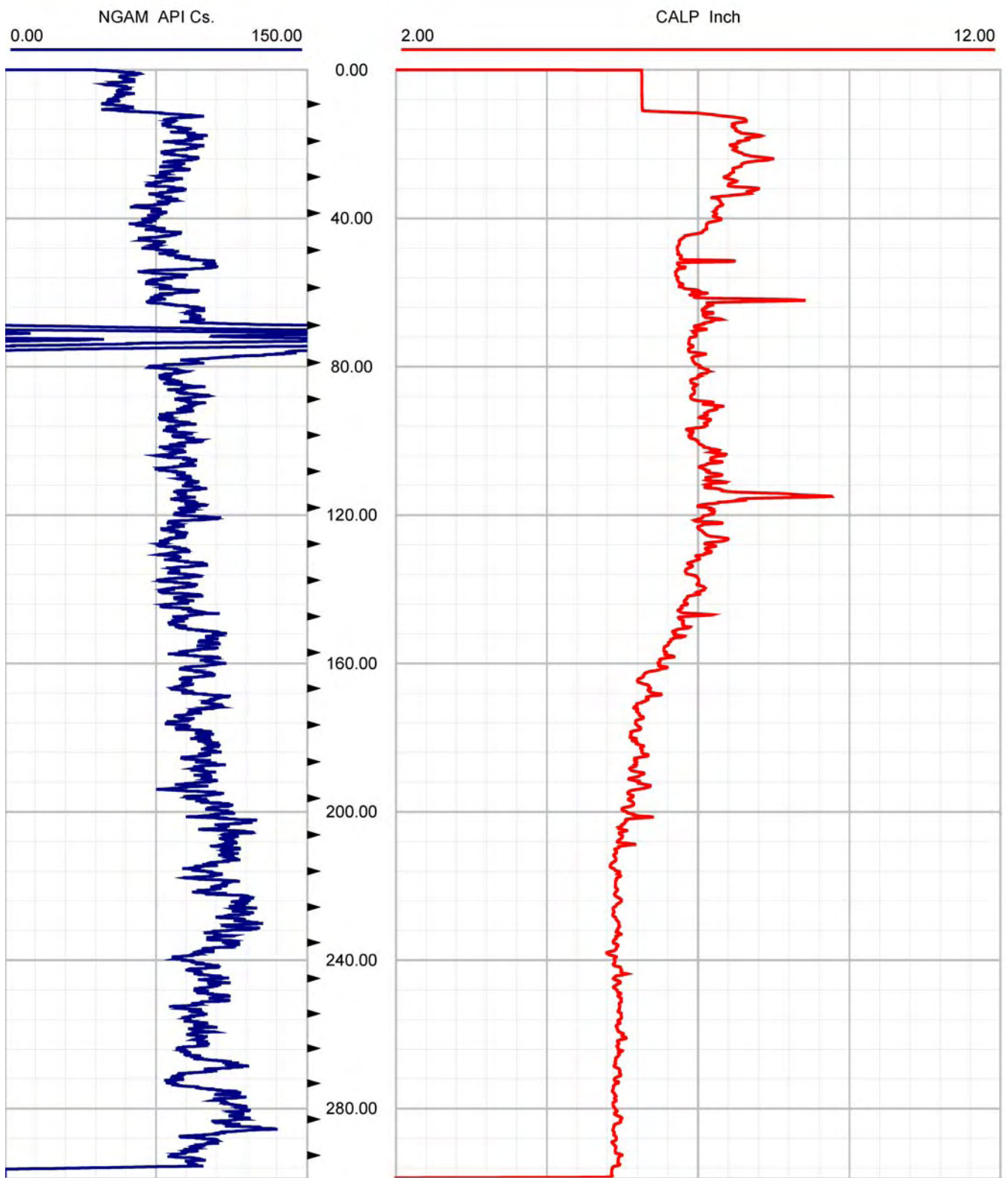


Figure 17. Boring Z1-B7, Caliper and Natural Gamma logs



CASCADE DRILLING

Borehole: Z1-B7

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 290.606 to 162.911ft  
 Mean dip format: dip-azimuth and dip

Interpretation 1

Dip data sets .....  
 BHTV dips

Z1-B7  
 Zone 0. 162.911 - 290.606ft  
 Deviation 1.50 N221.40

dipdata sets.....  
 BHTV dips  
 • Highlighted dips: Fracture Planar Open-fracture

	mean dip	n	f
N183 71	N183 71	41	1.04

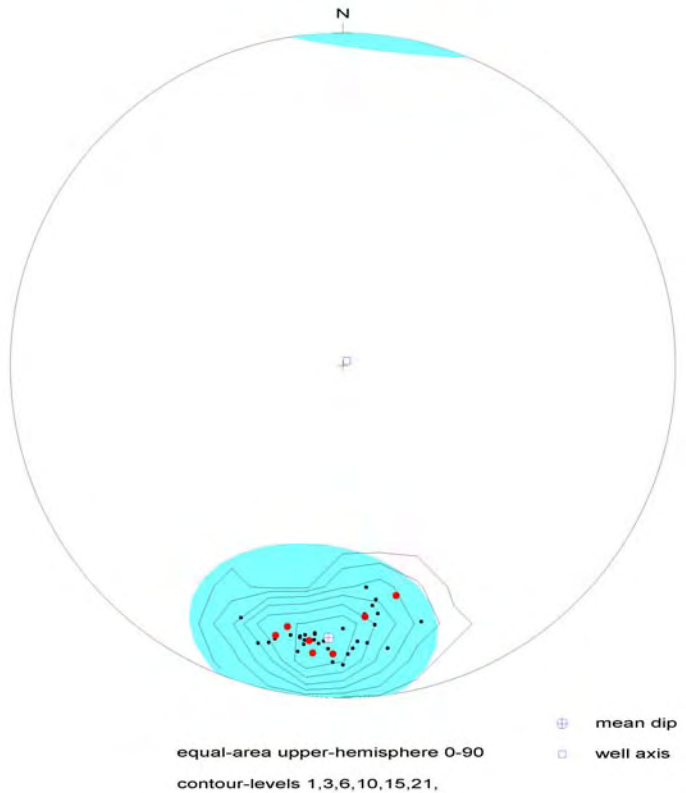


Figure 18. Boring Z1-B7, Stereonet Plot

Depth (feet)	Dip azimuth	Dip	Structure description
290.11	N202	71	Primary-structure Planar Bedding
282.71	N189	76	Fracture Planar Hairline-fracture
282.42	N195	75	Fracture Planar Hairline-fracture
280.36	N180	68	Fracture Planar Hairline-fracture
279.66	N175	65	Fracture Planar Open-fracture
278.85	N192	69	Fracture Planar Open-fracture
278.03	N167	60	Fracture Planar Open-fracture
276.57	N174	57	Fracture Planar Hairline-fracture
276.19	N172	60	Fracture Planar Hairline-fracture
275.75	N172	65	Fracture Planar Hairline-fracture
275.56	N175	64	Fracture Planar Hairline-fracture
275.06	N173	62	Primary-structure Planar Bedding
268.22	N171	75	Primary-structure Planar Bedding
267.36	N189	71	Primary-structure Planar Bedding
262.11	N182	78	Primary-structure Planar Bedding
261.05	N175	73	Primary-structure Planar Bedding
255.56	N163	70	Primary-structure Planar Bedding
254.78	N173	68	Primary-structure Planar Bedding
245.34	N183	74	Primary-structure Planar Bedding
235.53	N188	71	Primary-structure Planar Bedding
232.08	N186	70	Fracture Planar Hairline-fracture
231.10	N186	70	Fracture Planar Hairline-fracture
230.79	N186	70	Fracture Planar Hairline-fracture
230.32	N189	72	Fracture Planar Hairline-fracture
229.95	N191	72	Fracture Planar Hairline-fracture
228.85	N188	72	Fracture Planar Hairline-fracture
227.30	N189	72	Fracture Planar Hairline-fracture
222.05	N194	73	Fracture Planar Open-fracture
212.15	N177	72	Fracture Planar Hairline-fracture
211.98	N185	73	Fracture Planar Hairline-fracture
211.37	N184	72	Fracture Planar Hairline-fracture
210.95	N186	72	Fracture Planar Hairline-fracture
209.03	N187	72	Fracture Planar Open-fracture
202.06	N182	76	Fracture Planar Open-fracture
196.97	N186	76	Fracture Planar Open-fracture
195.89	N179	76	Fracture Planar Hairline-fracture
194.99	N178	74	Fracture Planar Hairline-fracture
194.36	N188	74	Primary-structure Planar Bedding
184.79	N180	79	Primary-structure Planar Bedding
165.17	N197	76	Primary-structure Planar Bedding
163.41	N194	74	Primary-structure Planar Bedding

Table 11. Boring Z1-B7, Structure depth, dip azimuth, dip and description

Deviated borehole in orthographic projection, viewed from N316

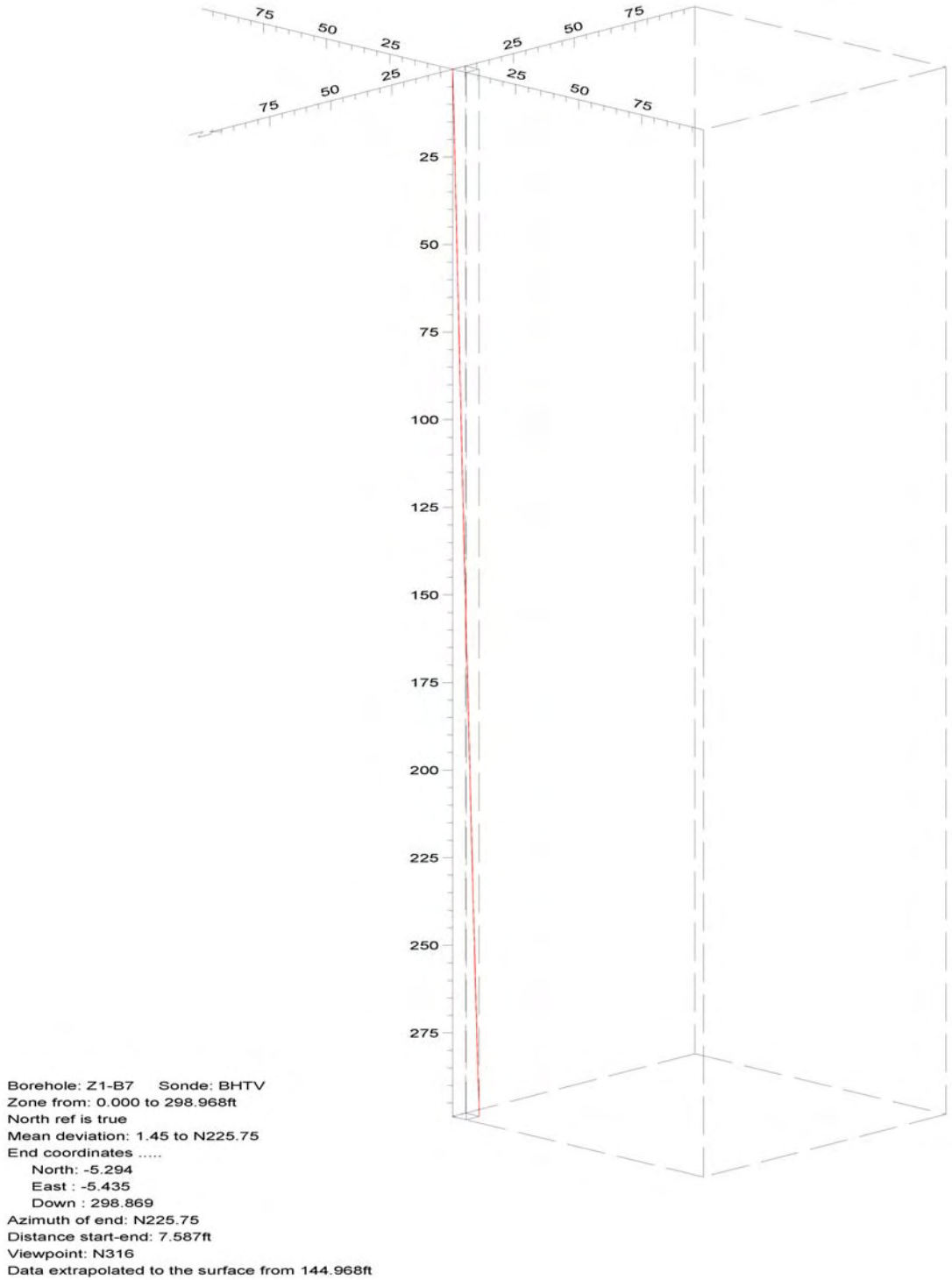


Figure 19. Boring Z1-B7, Deviation Projection



# SR-710 BORING Z2-B1

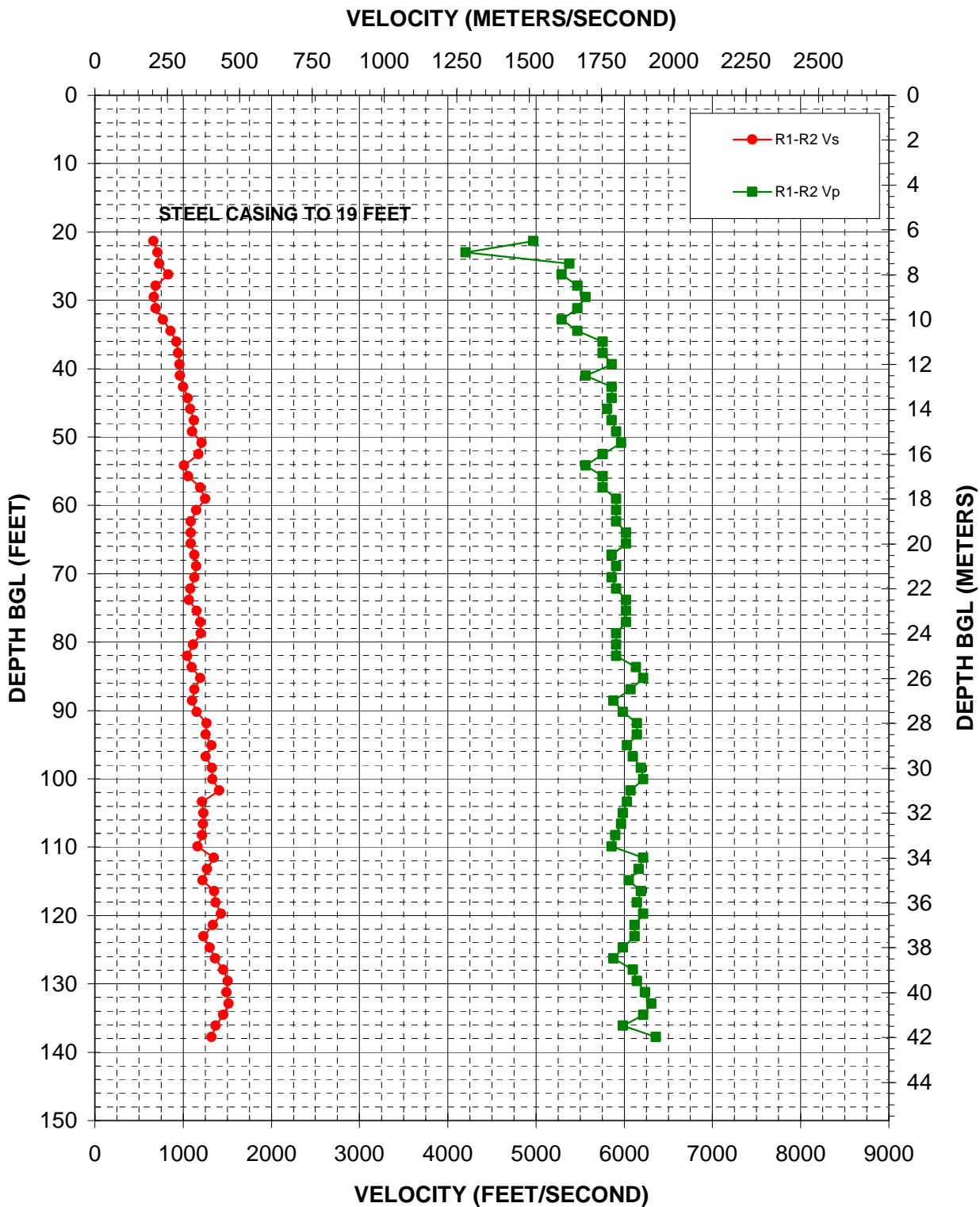


Figure 20: Boring Z2-B1, Suspension R1-R2 P- and  $S_H$ -wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
21.33	666	4971	103.35	1215	6031
22.97	712	4206	104.99	1229	5987
24.61	732	5378	106.63	1224	5965
26.25	835	5292	108.27	1215	5901
27.89	691	5468	109.91	1163	5859
29.53	671	5561	111.55	1350	6214
31.17	691	5468	113.19	1272	6167
32.81	770	5292	114.83	1220	6053
34.45	859	5468	116.47	1356	6190
36.09	927	5756	118.11	1367	6144
37.73	943	5756	119.75	1433	6214
39.37	962	5859	121.39	1339	6121
41.01	968	5561	123.03	1229	6121
42.65	1000	5859	124.67	1302	5987
44.29	1052	5859	126.31	1361	5880
45.93	1085	5807	127.95	1458	6098
47.57	1124	5859	129.59	1505	6144
49.21	1105	5911	131.23	1491	6237
50.85	1211	5965	132.87	1519	6309
52.49	1176	5756	134.51	1458	6214
54.13	1009	5561	136.15	1367	5987
55.77	1055	5756	137.80	1323	6358
57.41	1193	5756			
59.06	1252	5911			
60.70	1147	5911			
62.34	1086	5911			
63.98	1086	6020			
65.62	1086	6020			
67.26	1131	5859			
68.90	1147	5911			
70.54	1131	5859			
72.18	1083	5911			
73.82	1069	6020			
75.46	1155	6020			
77.10	1197	6020			
78.74	1202	5911			
80.38	1112	5911			
82.02	1045	5911			
83.66	1097	6132			
85.30	1193	6214			
86.94	1131	6076			
88.58	1101	5880			
90.22	1155	5987			
91.86	1267	6144			
93.50	1257	6144			
95.14	1323	6031			
96.78	1257	6098			
98.43	1328	6190			
100.07	1334	6214			
101.71	1408	6076			

Table 12. Boring Z2-B1, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

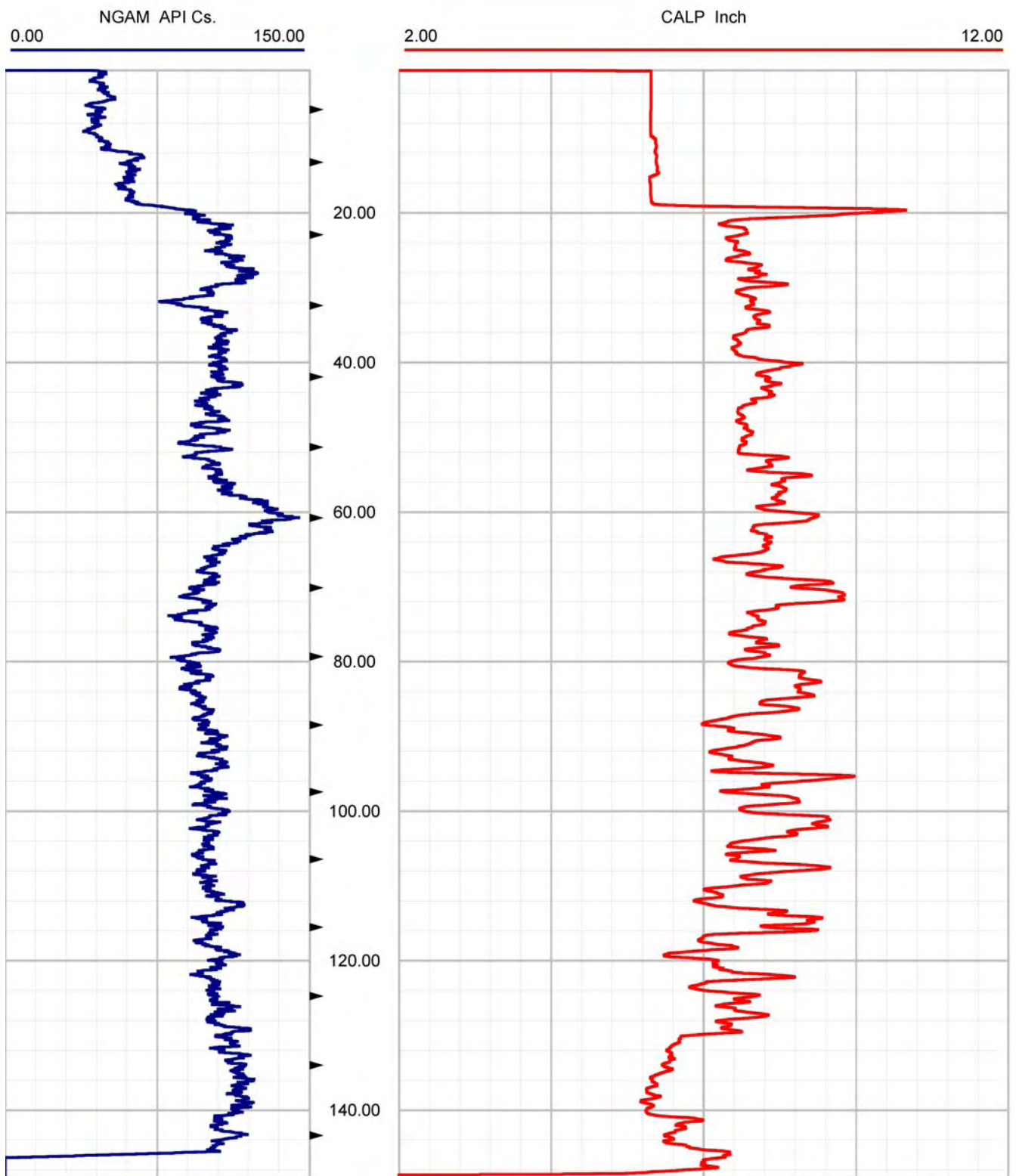


Figure 21. Boring Z2-B1, Caliper and Natural Gamma logs



DIP DATA INTERPRETATION  
 RGLDIP vsn 6.2  
 FRACTURE ANALYSIS STEREOGRAMS

CASCADE DRILLING

Borehole: Z2-B1

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 142.728 to 141.728ft  
 Mean dip format: dip-azimuth and dip

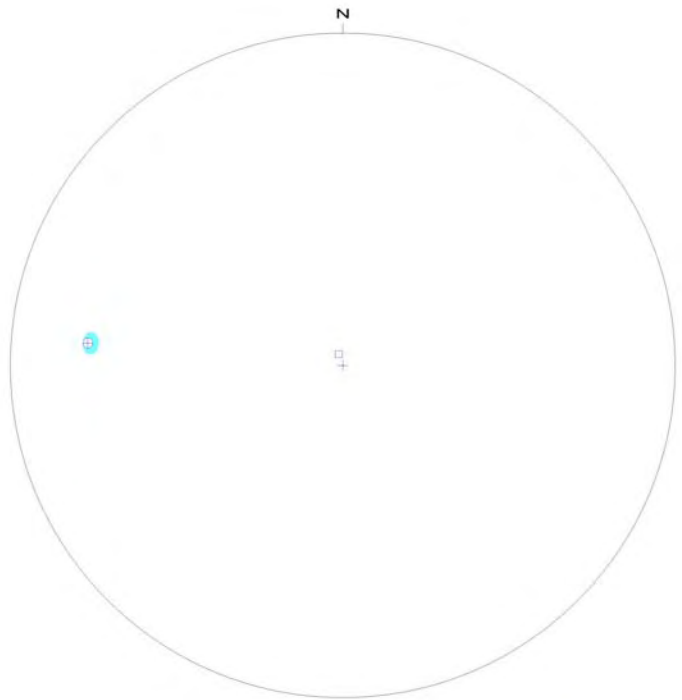
Interpretation 1

Dip data sets .....  
 BHTV dips

Z2-B1  
 Zone 0. 141.728 - 142.718ft  
 Deviation 2.90 N159,20

dipdata sets.....  
 BHTV dips  
 • Highlighted dips: Fracture Planar Hairline-fracture

	mean dip	n	f
N275 66	N275 66	1	0.00



equal-area upper-hemisphere 0-90  
 contour-levels

⊕ mean dip  
 □ well axis

Z2-B1, Interpretation 1

142.718 to 141.728ft

1

Figure 22. Boring Z2-B1, Stereonet Plot

Depth (feet)	Dip azimuth	Dip	Structure description
142.23	N275	66	Primary-structure Planar Bedding

Table 13. Boring Z2-B1, Structure depth, dip azimuth, dip and description

Deviated borehole in orthographic projection, viewed from N268

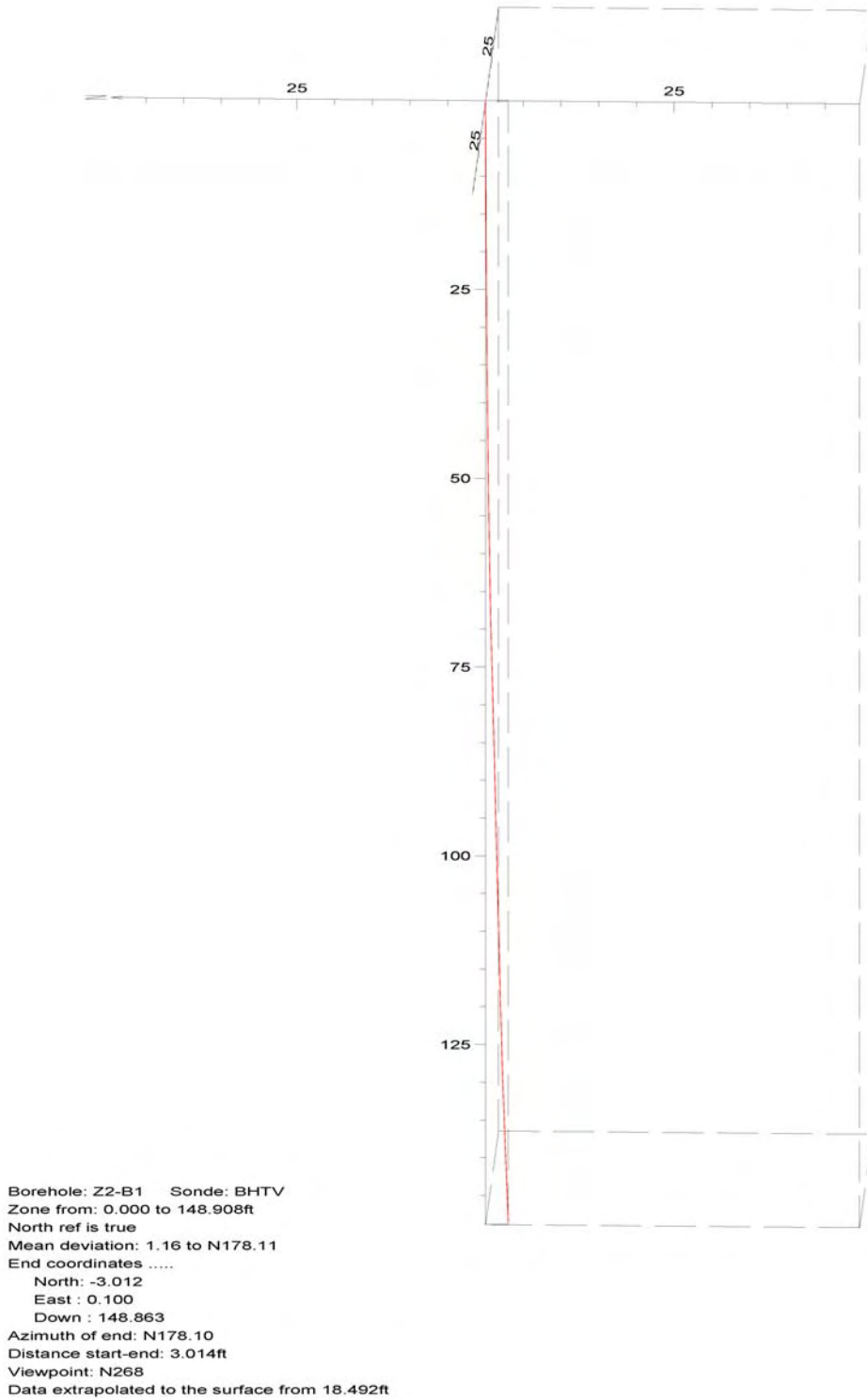


Figure 23. Boring Z2-B1, Deviation Projection

# SR-710 BORING Z2-B4

## VELOCITY (METERS/SECOND)

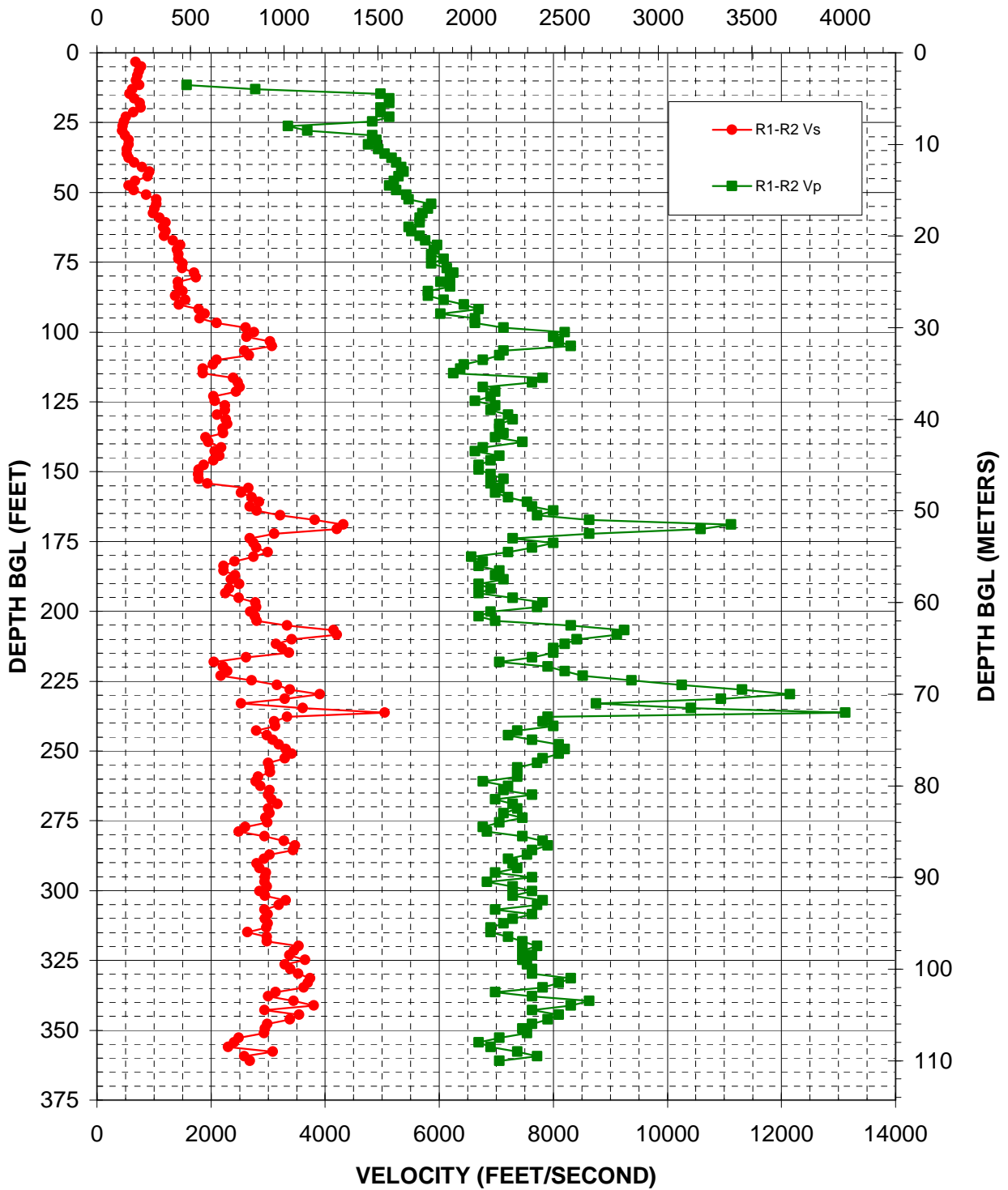


Figure 24: Boring Z2-B4, Suspension R1-R2 P- and  $S_H$ -wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
3.28	676		85.30	1505	5807	167.32	3815	8634
4.92	772		86.94	1373	5807	168.96	4317	11121
6.56	737		88.58	1548	6076	170.60	4206	10583
8.20	713		90.22	1439	6433	172.24	3110	8634
9.84	687		91.86	1783	6696	173.88	2678	7291
11.48	741	1577	93.50	1886	6020	175.52	2745	8002
13.12	622	2780	95.14	1803	6628	177.17	2792	7630
14.76	571	4971	96.78	2103	6628	178.81	2996	7211
16.40	656	5126	98.43	2604	7132	180.45	2745	6562
18.04	754	5126	100.07	2757	8202	182.09	2412	6765
19.69	763	4971	101.71	2625	8002	183.73	2224	6696
21.33	640	4971	103.35	3038	8101	185.37	2217	7056
22.97	513	5126	104.99	3066	8306	187.01	2421	6981
24.61	475	4825	106.63	2583	7132	188.65	2352	7132
26.25	456	3348	108.27	2667	7056	190.29	2495	6696
27.89	448	3686	109.91	2103	6765	191.93	2319	6907
29.53	492	4825	111.55	2038	6433	193.57	2255	6696
31.17	554	4897	113.19	1859	6371	195.21	2485	7291
32.81	558	4755	114.83	1854	6249	196.85	2780	7812
34.45	523	4934	116.47	2386	7812	198.49	2792	7720
36.09	527	5047	118.11	2467	7630	200.13	2689	6907
37.73	554	5167	119.75	2504	6765	201.77	2769	6696
39.37	656	5249	121.39	2439	6981	203.41	2804	6981
41.01	791	5335	123.03	2044	6907	205.05	3331	8306
42.65	924	5378	124.67	2063	6628	206.69	4153	9242
44.29	887	5292	126.31	2247	6981	208.33	4206	9113
45.93	672	5208	127.95	2247	6907	209.97	3418	8412
47.57	556	5126	129.59	2110	7211	211.61	3140	8202
49.21	645	5249	131.23	2263	7291	213.25	3248	8002
50.85	861	5423	132.87	2286	7056	214.90	3365	8002
52.49	1042	5468	134.51	2202	7056	216.54	2614	7630
54.13	1038	5859	136.15	2209	7132	218.18	2051	7056
55.77	1006	5807	137.80	1907	6981	219.82	2209	7906
57.41	982	5706	139.44	1953	7456	221.46	2286	8202
59.06	1101	5657	141.08	2180	6765	223.10	2173	8522
60.70	1206	5657	142.72	2070	6628	224.74	2711	9374
62.34	1163	5468	144.36	2151	7056	226.38	3155	10253
63.98	1202	5514	146.00	2044	6907	228.02	3382	11313
65.62	1180	5657	147.64	1875	6696	229.66	3906	12151
67.26	1334	5756	149.28	1788	6696	231.30	3297	10936
68.90	1465	5965	150.92	1773	6907	232.94	2524	8749
70.54	1408	5911	152.56	1783	7132	234.58	3605	10415
72.18	1433	5859	154.20	1941	6907	236.22	5047	13123
73.82	1426	6076	155.84	2657	7056	237.86	3331	7906
75.46	1498	5859	157.48	2524	6981	239.50	3110	7812
77.10	1491	6132	159.12	2711	7211	241.14	3125	8002
78.74	1700	6249	160.76	2841	7542	242.78	2792	7373
80.38	1736	6190	162.40	2678	7630	244.42	2983	7211
82.02	1420	6020	164.04	2804	8002	246.06	3081	7630
83.66	1433	6190	165.68	3217	7720	247.70	3185	8101

NOTE: "blank" space indicates data of insufficient quality for good pick.

Table 14. Boring Z2-B4, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities



Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
249.34	3314	8202	331.36	3739	8306
250.98	3418	8101	333.01	3697	8101
252.62	3297	7812	334.65	3625	7812
254.27	3003	7720	336.29	3132	6981
255.91	3024	7373	337.93	3003	7630
257.55	3038	7373	339.57	3444	8634
259.19	2828	7373	341.21	3804	8306
260.83	2786	6765	342.85	2936	7630
262.47	2865	7211	344.49	3547	8101
264.11	3024	7132	346.13	3382	7906
265.75	3003	7630	347.77	2989	7630
267.39	3059	6981	349.41	2949	7456
269.03	3162	7291	351.05	2929	7542
270.67	3003	7373	352.69	2485	7056
272.31	3024	7132	354.33	2404	6696
273.95	2956	7456	355.97	2302	6907
275.59	2989	7056	357.61	3081	7373
277.23	2599	6765	359.25	2583	7720
278.87	2485	6835	360.89	2678	7056
280.51	2942	7456			
282.15	3281	7812			
283.79	3472	7906			
285.43	3435	7630			
287.07	3024	7542			
288.71	2929	7211			
290.35	2804	7291			
291.99	2853	7373			
293.64	2962	6981			
295.28	2949	7630			
296.92	2942	6835			
298.56	2976	7291			
300.20	2847	7630			
301.84	2949	7291			
303.48	3314	7812			
305.12	3193	7720			
306.76	2942	6981			
308.40	2996	7630			
310.04	2949	7291			
311.68	2996	7132			
313.32	2969	6907			
314.96	2641	6907			
316.60	2976	7211			
318.24	2976	7456			
319.88	3537	7720			
321.52	3454	7456			
323.16	3374	7630			
324.80	3645	7456			
326.44	3297	7542			
328.08	3391	7630			
329.72	3528	7630			

Table 14, continued. Boring Z2-B4, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

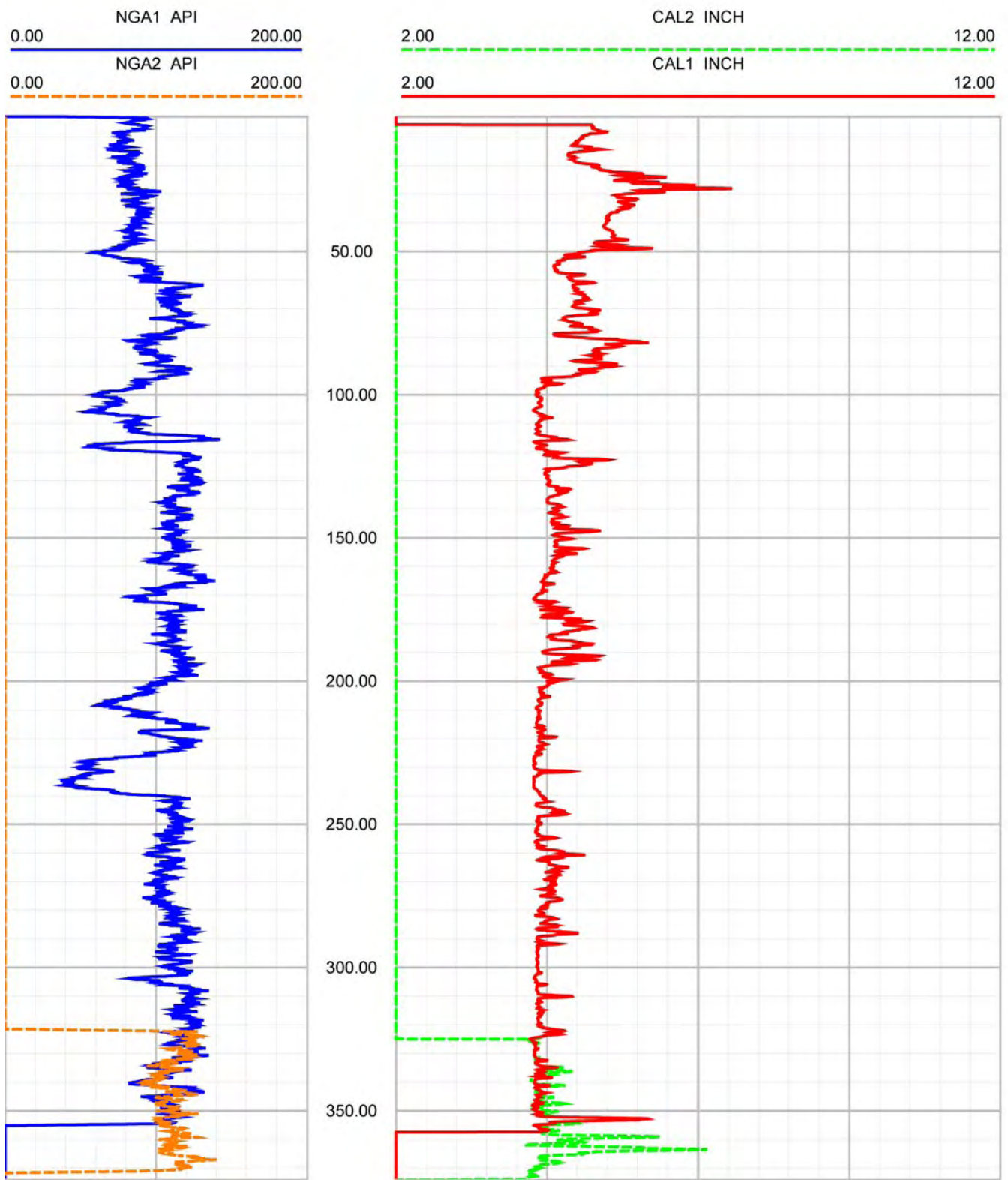


Figure 25. Boring Z2-B4, Caliper and Natural Gamma logs



CASCADE DRILLING

Borehole: Z2-B4

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 372.508 to 63.101ft  
 Mean dip format: dip-azimuth and dip

Interpretation 1

Dip data sets .....

BHTV dips

Z2-B4

Zone 0. 63.101 - 372.498ft  
 Deviation 1.20 N355.10

dipdata sets.....

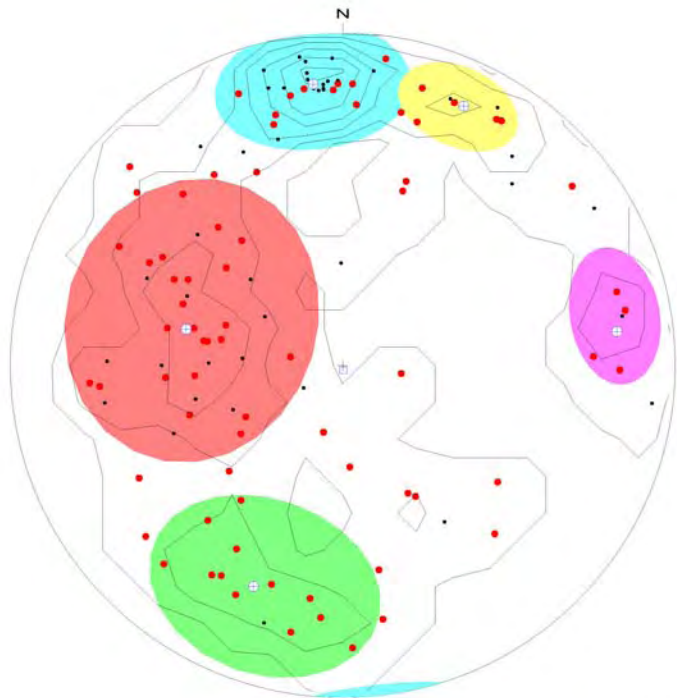
BHTV dips

• Highlighted dips: Fracture Planar Hairline-fracture

	mean dip	n	f
N354 74	N354 74	30	( 0.38)
N283 40	N283 40	37	0.16
N202 61	N202 61	13	( 0.08)
N083 72	N083 72	5	( 0.05)
N025 75	N025 75	7	( 0.09)

intersections

	N354 74	N283 40	N202 61	N083 72	N025 75
N354 74		40 N278	30 N273	67 N042	74 N003
N283 40	40 N278		39 N266	13 N357	38 N307
N202 61	30 N273	39 N266		49 N151	04 N114
N083 72	67 N042	13 N357	49 N151		71 N064
N025 75	74 N003	38 N307	04 N114	71 N064	



equal-area upper-hemisphere 0-90  
 contour-levels 1,3,6,10,15,21.  
 ⊕ mean dip  
 □ well axis

Figure 26. Boring Z2-B4, Stereonet Plot

Depth (feet)	Dip azimuth	Dip	Structure description
372.01	N310	70	Fracture Planar Hairline-fracture
371.64	N297	48	Fracture Planar Hairline-fracture
358.32	N229	68	Fracture Planar Hairline-fracture
355.82	N344	60	Primary-structure Planar Bedding
353.21	N335	60	Primary-structure Planar Bedding
351.36	N019	46	Fracture Planar Hairline-fracture
347.18	N301	53	Fracture Planar Hairline-fracture
346.92	N298	56	Fracture Planar Hairline-fracture
340.12	N345	67	Fracture Planar Hairline-fracture
335.30	N354	73	Primary-structure Planar Bedding
333.92	N356	74	Primary-structure Planar Bedding
332.78	N356	72	Primary-structure Planar Bedding
332.48	N355	72	Primary-structure Planar Bedding
332.28	N356	72	Primary-structure Planar Bedding
331.62	N354	73	Primary-structure Planar Bedding
329.41	N353	76	Primary-structure Planar Bedding
326.88	N357	75	Primary-structure Planar Bedding
324.88	N359	75	Primary-structure Planar Bedding
322.72	N002	74	Fracture Planar Hairline-fracture
321.26	N003	68	Fracture Planar Hairline-fracture
319.15	N075	74	Fracture Planar Hairline-fracture
318.02	N298	65	Fracture Planar Hairline-fracture
317.58	N171	66	Fracture Planar Hairline-fracture
316.66	N282	45	Fracture Planar Hairline-fracture
316.23	N280	35	Fracture Planar Hairline-fracture
315.75	N294	43	Fracture Planar Bedding
315.28	N312	49	Fracture Planar Bedding
312.60	N270	45	Fracture Planar Open-fracture
311.03	N291	43	Fracture Planar Hairline-fracture
309.49	N284	38	Fracture Planar Hairline-fracture
308.08	N321	40	Fracture Planar Hairline-fracture
306.82	N240	11	Fracture Planar Open-fracture
306.55	N313	31	Fracture Planar Open-fracture
304.96	N302	23	Fracture Planar Open-fracture
301.89	N310	38	Fracture Planar Hairline-fracture
301.36	N282	31	Fracture Planar Hairline-fracture
300.88	N318	47	Fracture Planar Hairline-fracture
300.21	N178	74	Fracture Planar Hairline-fracture
300.05	N317	60	Fracture Planar Hairline-fracture
299.48	N289	31	Fracture Planar Hairline-fracture
299.05	N280	34	Fracture Planar Hairline-fracture
297.35	N222	69	Fracture Planar Hairline-fracture
297.11	N248	29	Primary-structure Planar Bedding
296.16	N151	37	Fracture Planar Hairline-fracture
296.09	N274	25	Primary-structure Planar Bedding
294.36	N313	77	Fracture Planar Hairline-fracture
293.43	N266	44	Fracture Planar Hairline-fracture
292.43	N294	54	Fracture Planar Open-fracture
291.74	N299	44	Fracture Planar Hairline-fracture
290.23	N212	64	Fracture Planar Hairline-fracture

Table 15. Boring Z2-B4, Structure depth, dip azimuth, dip and description

Depth (feet)	Dip azimuth	Dip	Structure description
287.54	N265	63	Fracture Planar Hairline-fracture
278.90	N016	76	Fracture Planar Hairline-fracture
278.82	N033	77	Fracture Planar Hairline-fracture
277.31	N127	49	Fracture Planar Hairline-fracture
276.54	N138	58	Fracture Planar Hairline-fracture
262.81	N147	47	Primary-structure Planar Bedding
260.29	N031	80	Fracture Planar Open-fracture
258.50	N032	76	Fracture Planar Hairline-fracture
257.53	N326	59	Fracture Planar Hairline-fracture
252.83	N221	52	Fracture Planar Hairline-fracture
252.20	N349	72	Fracture Planar Hairline-fracture
250.80	N336	54	Fracture Planar Hairline-fracture
250.61	N339	77	Fracture Planar Hairline-fracture
248.47	N039	70	Primary-structure Planar Bedding
245.68	N097	83	Fracture Planar Open-fracture
243.08	N043	64	Primary-structure Planar Bedding
242.02	N197	70	Primary-structure Planar Bedding
239.17	N279	13	Fracture Planar Hairline-fracture
235.45	N153	36	Fracture Planar Hairline-fracture
234.66	N242	27	Fracture Planar Hairline-fracture
233.82	N271	33	Primary-structure Planar Bedding
230.68	N236	30	Fracture Planar Hairline-fracture
230.67	N210	54	Fracture Planar Hairline-fracture
230.37	N227	39	Fracture Planar Hairline-fracture
228.17	N266	37	Fracture Planar Hairline-fracture
227.88	N252	40	Fracture Planar Hairline-fracture
227.81	N266	65	Fracture Planar Hairline-fracture
226.68	N022	75	Primary-structure Planar Bedding
224.18	N013	67	Fracture Planar Hairline-fracture
223.83	N017	66	Fracture Planar Hairline-fracture
222.73	N098	14	Fracture Planar Hairline-fracture
221.57	N079	76	Fracture Planar Hairline-fracture
220.56	N188	60	Fracture Planar Hairline-fracture
219.40	N217	42	Fracture Planar Hairline-fracture
218.07	N170	53	Fracture Planar Hairline-fracture
217.72	N205	65	Fracture Planar Hairline-fracture
217.23	N052	77	Fracture Planar Hairline-fracture
216.54	N196	17	Fracture Planar Hairline-fracture
214.54	N091	72	Fracture Planar Hairline-fracture
210.95	N176	25	Fracture Planar Hairline-fracture
208.84	N088	65	Fracture Planar Hairline-fracture
207.87	N348	74	Primary-structure Planar Bedding
205.72	N345	75	Primary-structure Planar Bedding
204.29	N185	65	Fracture Planar Hairline-fracture
203.48	N358	72	Fracture Planar Hairline-fracture
203.02	N352	73	Fracture Planar Hairline-fracture
200.58	N345	81	Primary-structure Planar Bedding
198.71	N354	74	Primary-structure Planar Bedding
197.32	N353	78	Primary-structure Planar Bedding
197.04	N198	59	Fracture Planar Hairline-fracture

Table 15, continued. Boring Z2-B4, Structure depth, dip azimuth, dip and description

Depth (feet)	Dip azimuth	Dip	Structure description
196.55	N210	62	Fracture Planar Hairline-fracture
192.65	N019	49	Fracture Planar Hairline-fracture
191.15	N344	64	Fracture Planar Hairline-fracture
182.49	N058	78	Primary-structure Planar Bedding
172.51	N191	71	Fracture Planar Hairline-fracture
170.53	N008	82	Fracture Planar Hairline-fracture
167.26	N359	74	Fracture Planar Hairline-fracture
153.62	N358	82	Primary-structure Planar Bedding
150.93	N353	81	Primary-structure Planar Bedding
142.63	N006	78	Primary-structure Planar Bedding
134.65	N352	83	Primary-structure Planar Bedding
120.06	N327	68	Primary-structure Planar Bedding
116.80	N359	25	Primary-structure Planar Bedding
116.14	N023	75	Fracture Planar Hairline-fracture
114.10	N354	75	Primary-structure Planar Bedding
104.93	N080	74	Primary-structure Planar Bedding
99.39	N248	46	Primary-structure Planar Bedding
96.06	N261	62	Primary-structure Planar Bedding
79.11	N257	38	Primary-structure Planar Bedding
72.91	N271	60	Primary-structure Planar Bedding
63.60	N241	59	Fracture Planar Hairline-fracture

Table 15, continued. Boring Z2-B4, Structure depth, dip azimuth, dip and description

Deviated borehole in orthographic projection, viewed from N90

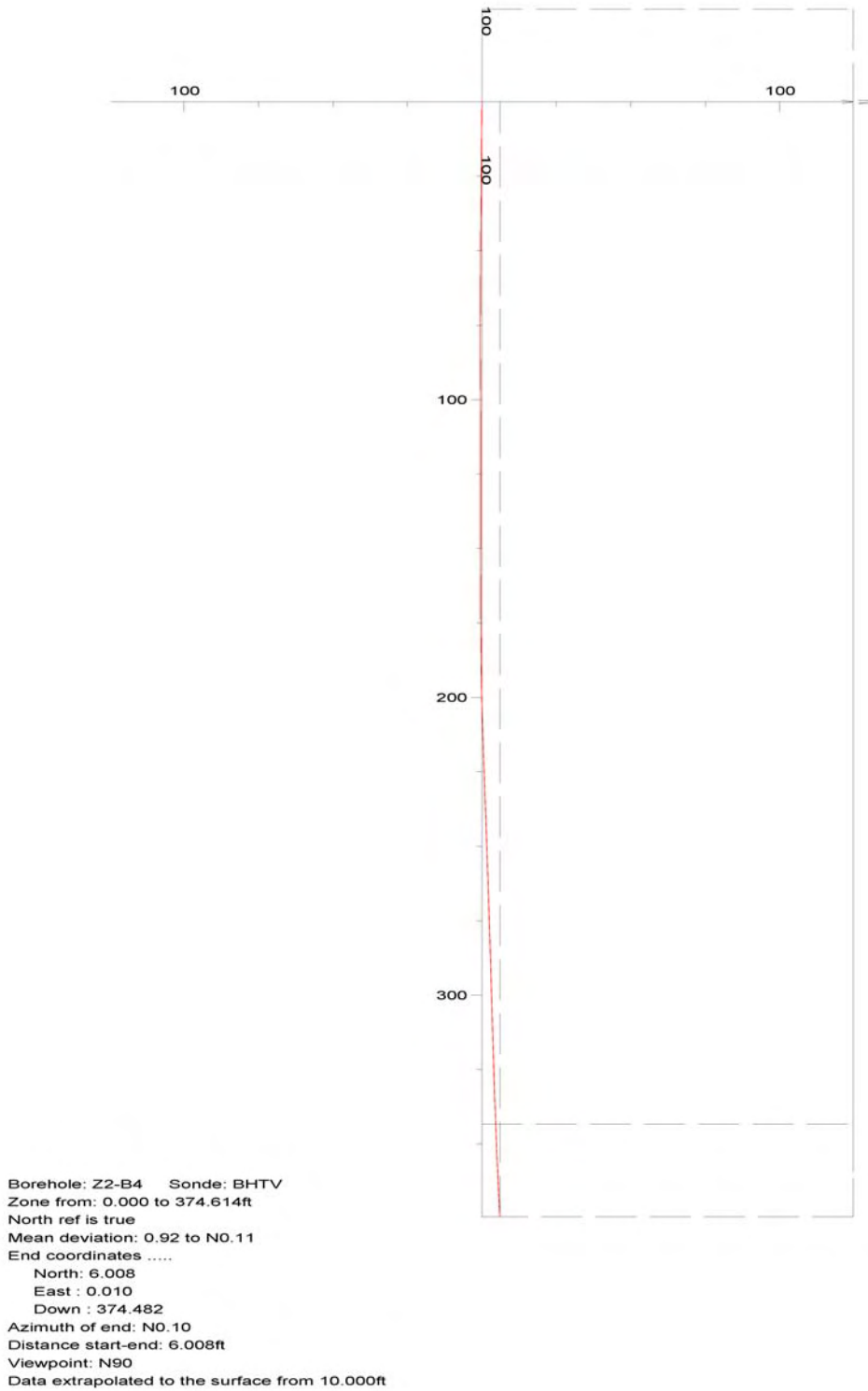


Figure 27. Boring Z2-B4, Deviation Projection

# SR-710 BORING Z3-B1

## VELOCITY (METERS/SECOND)

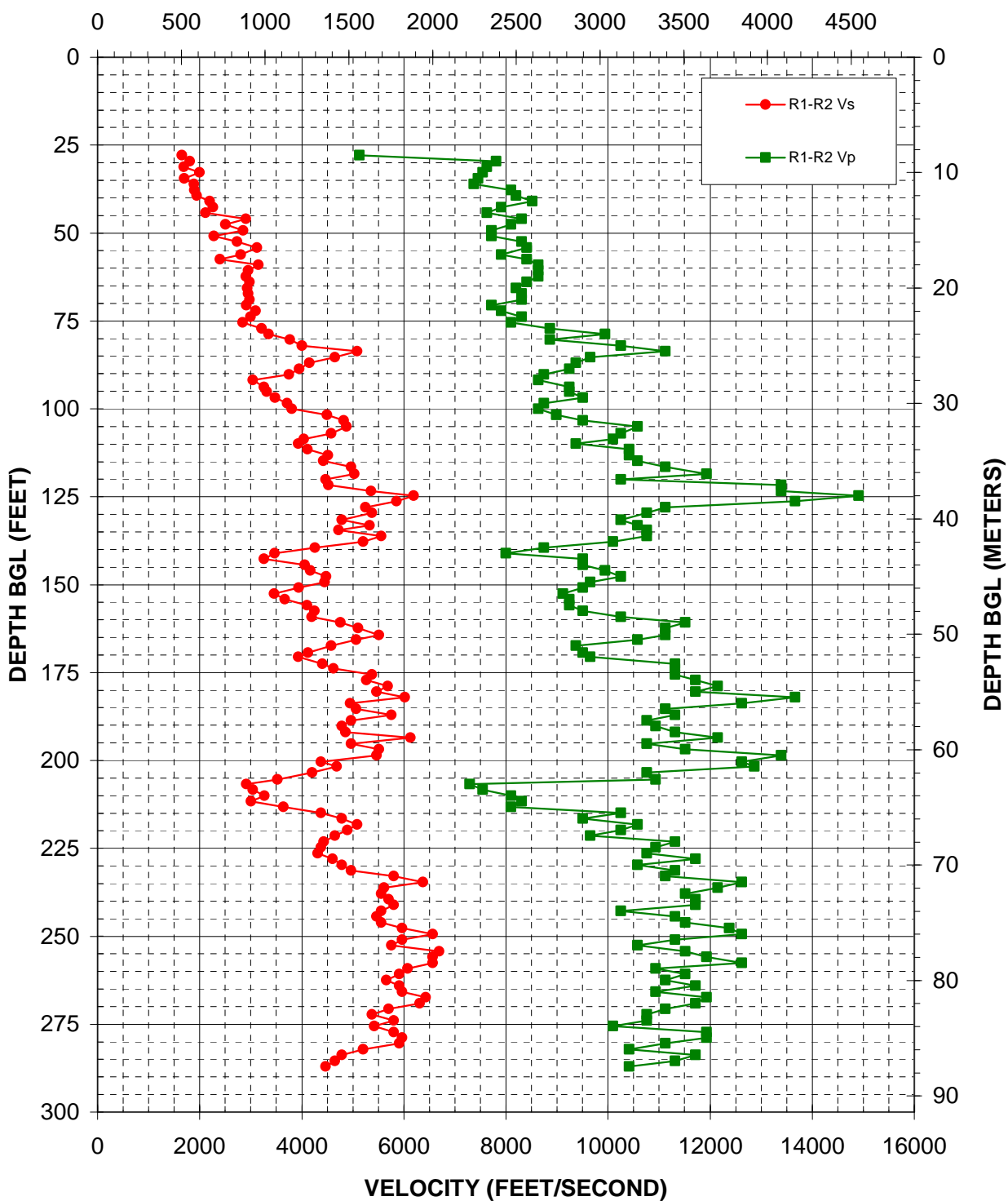


Figure 28: Boring Z3-B1, Suspension R1-R2 P- and  $S_H$ -wave velocities



Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
27.89	1649	5126	109.91	3929	9374	191.93	4861	11313
29.53	1803	7812	111.55	4114	10415	193.57	6132	12151
31.17	1691	7630	113.19	4510	10415	195.21	4971	10757
32.81	2001	7542	114.83	4419	10583	196.85	5514	11512
34.45	1700	7456	116.47	4971	11121	198.49	5468	13391
36.09	1886	7373	118.44	5028	11930	200.46	4374	12619
37.73	1896	8101	120.08	4464	10253	201.77	4687	12866
39.37	1941	8202	121.72	4525	13391	203.41	4206	10757
41.01	2202	8522	123.36	5356	13391	205.38	3528	10936
42.65	2263	7906	124.67	6190	14913	206.69	2916	7291
44.29	2117	7630	126.31	5859	13670	208.33	3038	7542
45.93	2903	8306	127.95	5249	11121	209.97	3265	8101
47.57	2504	8101	129.59	5378	10757	211.61	3010	8306
49.21	2853	7720	131.56	4790	10253	213.25	3645	8101
50.85	2278	7720	133.20	5335	10583	214.90	4374	10253
52.49	2734	8306	134.51	4721	10757	216.54	4790	9510
54.13	3125	8412	136.15	5561	10757	218.18	5087	10583
56.10	2804	7906	137.80	5208	10095	219.82	4897	10253
57.41	2395	8412	139.44	4261	8749	221.46	4654	9650
59.06	3155	8634	141.08	3472	8002	223.10	4434	11313
60.70	2956	8634	142.72	3256	9510	224.74	4374	10936
62.34	2903	8634	144.36	4063	9510	226.38	4317	10757
63.98	2983	8412	146.00	4166	9942	228.02	4605	11717
65.62	2929	8202	147.64	4479	10253	229.66	4790	10583
67.26	2956	8306	149.28	4449	9650	231.30	4971	11313
68.90	2983	8306	150.92	3941	9510	232.94	5807	11121
70.54	2916	7720	152.56	3463	9113	234.58	6371	12619
72.18	3095	7906	154.20	3666	9242	236.22	5608	12151
73.82	2996	8306	155.84	4101	9242	237.86	5561	11512
75.46	2841	8101	157.48	4247	9510	239.50	5706	11717
77.10	3217	8867	159.12	4193	10253	241.14	5807	11717
78.74	3348	9942	160.76	4755	11512	242.78	5561	10253
80.38	3771	8867	162.40	5106	11121	244.42	5468	11313
82.02	4001	10253	164.37	5514	11121	246.06	5561	11512
83.66	5087	11121	165.68	5067	10583	247.70	5965	12381
85.30	4654	9650	167.32	4573	9374	249.34	6562	12619
86.94	4153	9374	169.29	4127	9510	250.98	5965	11313
88.58	3953	9242	170.60	3929	9650	252.62	5756	10583
90.22	3750	8749	172.57	4404	11313	254.27	6696	11512
91.86	3038	8634	173.88	4621	11313	255.91	6562	11930
93.83	3256	9242	175.52	5378	11313	257.55	6562	12619
95.14	3314	9242	177.17	5270	11717	259.19	6076	10936
96.78	3481	9510	178.81	5681	12151	260.83	5911	11512
98.43	3718	8749	180.45	5468	11717	262.47	5657	11121
100.07	3804	8634	182.09	6020	13670	264.11	5911	11717
101.71	4494	8989	183.73	4952	12619	265.75	5965	10936
103.35	4825	9510	185.37	5067	11121	267.39	6433	11930
104.99	4879	10583	187.01	5756	11313	269.03	6309	11717
106.96	4573	10253	188.65	4971	10757	270.67	5706	11121
108.60	4038	10095	190.29	4790	10936	272.31	5378	10757

Table 16. Boring Z3-B1, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
273.95	5807	10757
275.59	5423	10095
277.23	5807	11930
278.87	5965	11930
280.51	5911	11121
282.15	5208	10415
283.79	4790	11717
285.43	4654	11313
287.07	4464	10415

Table 16, continued. Boring Z3-B1, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

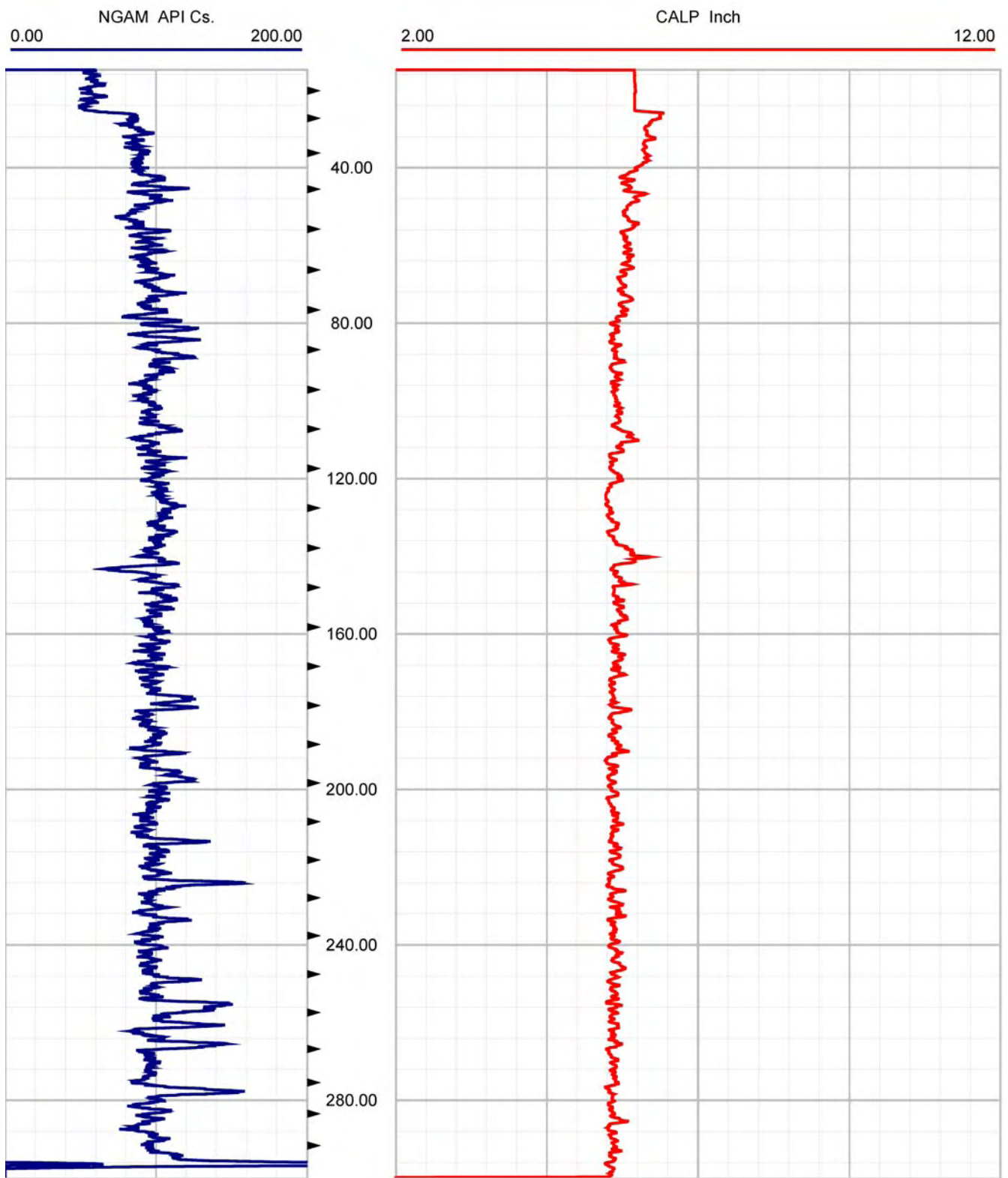


Figure 29. Boring Z3-B1, Caliper and Natural Gamma logs



CASCADE DRILLING

Borehole: Z3-B1

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 274.689 to 36.716ft  
 Mean dip format: dip-azimuth and dip

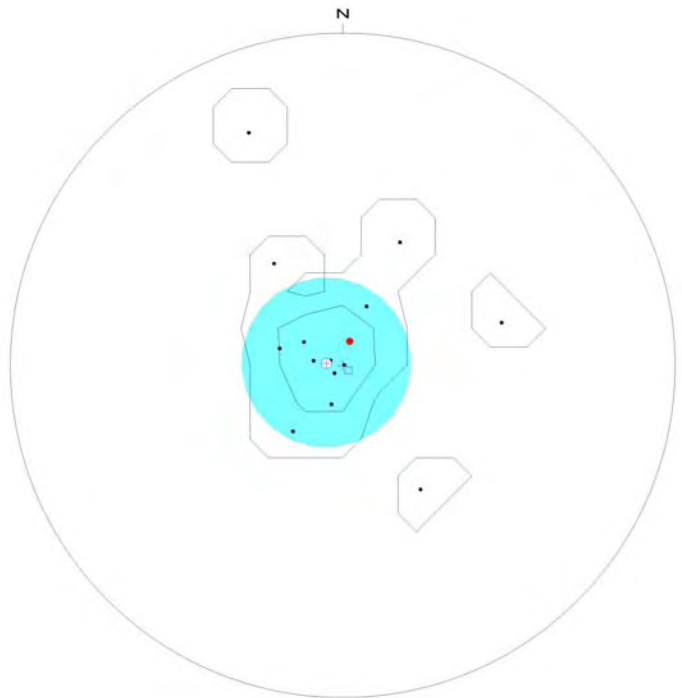
Interpretation 1

Dip data sets .....  
 BHTV dips

Z3-B1  
 Zone 0. 36.716 - 274.679ft  
 Deviation 1.90 N310.30

dipdata sets.....  
 BHTV dips  
 • Highlighted dips: Fracture Planar Hairline-fracture

	mean dip	n	f
N277 4	N277 4	10	( 0.04)



equal-area upper-hemisphere 0-90  
 contour-levels 1,3,  
 ⊕ mean dip  
 □ well axis

Figure 30. Boring Z3-B1, Stereonet Plot

Depth (feet)	Dip azimuth	Dip	Structure description
274.19	N226	3	Primary-structure Planar Bedding
267.32	N025	34	Primary-structure Planar Bedding
266.61	N196	10	Primary-structure Planar Bedding
255.39	N285	16	Primary-structure Planar Bedding
254.45	N217	20	Primary-structure Planar Bedding
230.38	N279	7	Primary-structure Planar Bedding
230.06	N292	3	Primary-structure Planar Bedding
206.30	N075	41	Primary-structure Planar Bedding
193.65	N326	30	Primary-structure Planar Bedding
192.12	N148	36	Primary-structure Planar Bedding
146.99	N338	65	Primary-structure Planar Bedding
125.67	N301	11	Primary-structure Planar Bedding
123.19	N022	16	Primary-structure Planar Bedding
55.52	N075	0	Primary-structure Planar Bedding
37.22	N016	6	Fracture Planar Hairline-fracture

Table 17. Boring Z3-B1, Structure depth, dip azimuth, dip and description

Deviated borehole in orthographic projection, viewed from N37

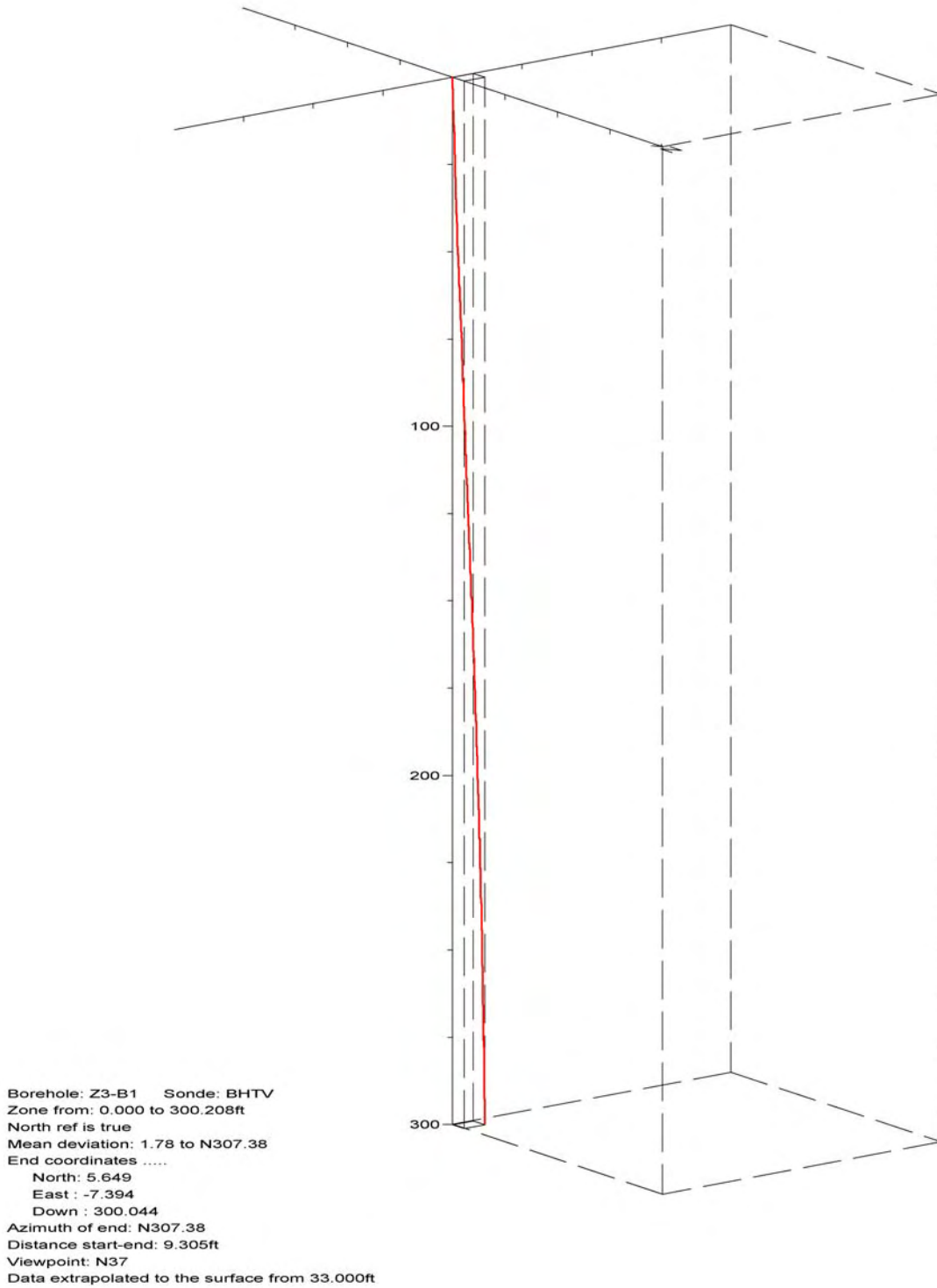


Figure 31. Boring Z3-B1, Deviation Projection

### SR-710 BORING Z3-B3

VELOCITY (METERS/SECOND)

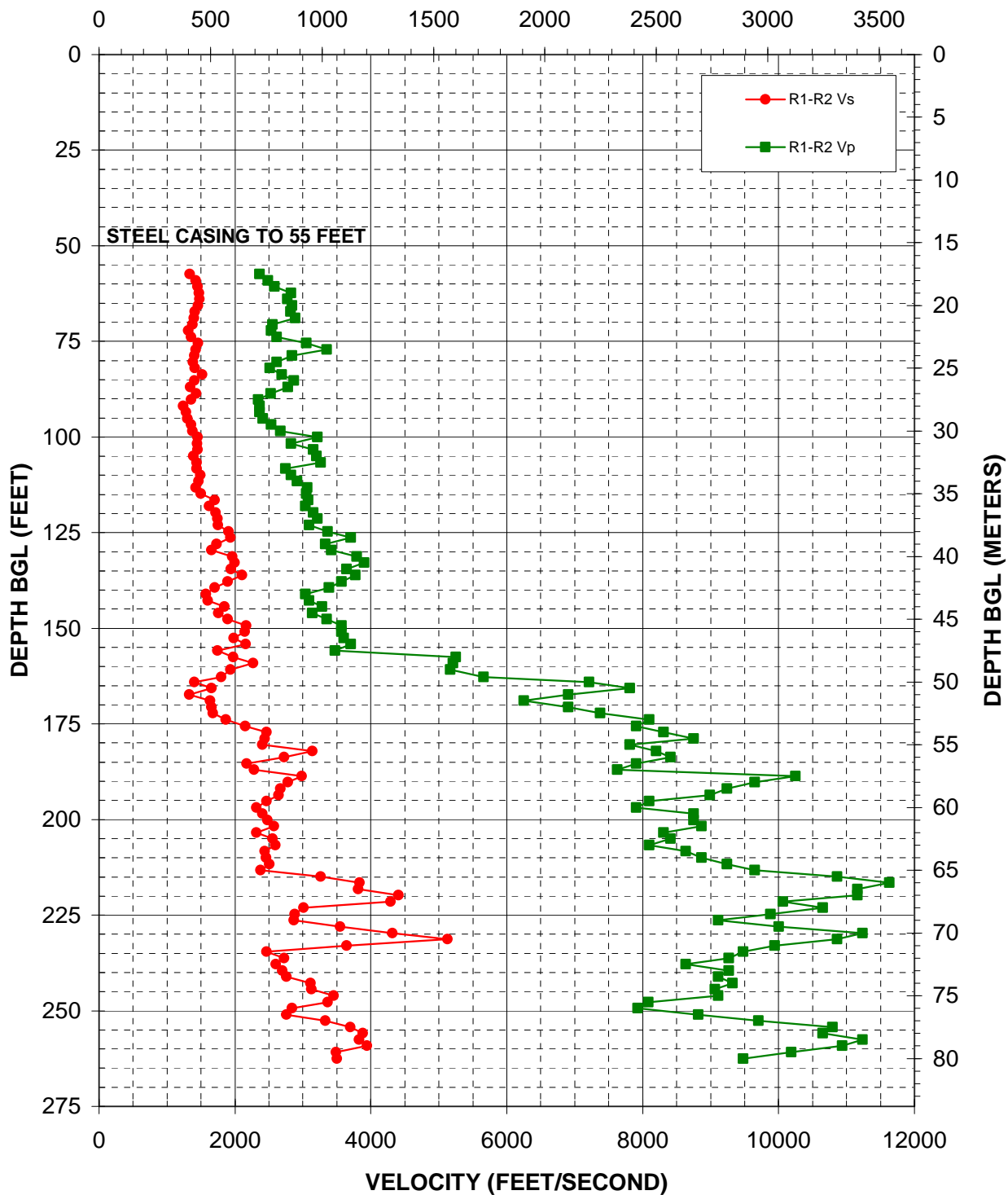


Figure 32: Boring Z3-B3, Suspension R1-R2 P- and S<sub>H</sub>-wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
57.41	1334	2360	139.44	1700	3382	221.46	4289	10064
59.06	1426	2485	141.08	1574	3038	223.10	3010	10652
60.70	1448	2583	142.72	1600	3095	224.74	2878	9882
62.34	1468	2828	144.36	1848	3281	226.38	2865	9113
63.98	1481	2769	146.00	1759	3140	228.02	3547	10003
65.62	1458	2841	147.64	1896	3348	229.66	4317	11236
67.26	1408	2816	149.28	2166	3566	231.30	5126	10864
68.90	1393	2891	150.92	2144	3566	232.94	3645	9942
70.54	1379	2553	152.56	1982	3605	234.58	2467	9482
72.18	1312	2533	154.20	2158	3707	236.22	2723	9268
73.82	1353	2614	155.84	1745	3472	237.86	2604	8634
75.46	1455	3052	157.48	1976	5249	239.50	2700	9268
77.10	1423	3348	159.12	2270	5208	241.14	2757	9113
78.74	1402	2841	160.76	1936	5167	242.78	3110	9321
80.38	1384	2614	162.73	1798	5657	244.42	3125	9063
82.02	1411	2514	164.04	1402	7211	246.06	3454	9113
83.66	1515	2689	165.68	1657	7812	247.70	3365	8081
85.30	1405	2865	167.32	1331	6907	249.34	2841	7925
86.94	1345	2780	168.96	1632	6249	250.98	2757	8819
88.58	1433	2524	170.60	1657	6907	252.62	3331	9707
90.22	1353	2343	172.24	1674	7373	254.27	3697	10792
91.86	1240	2360	173.88	1864	8101	255.91	3883	10652
93.50	1282	2360	175.52	2151	7906	257.55	3826	11236
95.14	1299	2412	177.17	2467	8306	259.19	3941	10936
96.78	1356	2533	178.81	2439	8749	260.83	3490	10189
98.43	1379	2667	180.45	2404	7812	262.47	3500	9482
100.07	1452	3217	182.09	3140	8202			
101.71	1445	2828	183.73	2723	8412			
103.35	1448	3155	185.37	2173	7906			
104.99	1387	3201	187.01	2278	7630			
106.63	1439	3265	188.65	2983	10253			
108.27	1439	2745	190.29	2780	9650			
109.91	1491	2828	191.93	2667	9242			
111.55	1465	2916	193.57	2646	8989			
113.19	1426	3066	195.21	2467	8101			
114.83	1498	3052	196.85	2319	7906			
116.47	1704	3081	198.49	2404	8749			
118.11	1624	3038	200.13	2476	8749			
119.75	1713	3155	201.77	2573	8867			
121.39	1740	3217	203.41	2319	8306			
123.03	1750	3095	205.05	2553	8412			
124.67	1907	3365	206.69	2594	8101			
126.31	1936	3707	208.33	2439	8634			
127.95	1731	3331	209.97	2458	8867			
129.59	1657	3418	211.61	2504	9242			
131.23	1959	3793	213.25	2377	9650			
132.87	1994	3906	214.90	3265	10864			
134.51	1941	3645	216.54	3837	11634			
136.15	2103	3771	218.18	3815	11159			
137.80	1896	3566	219.82	4404	11159			

Table 18. Boring Z3-B3, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities



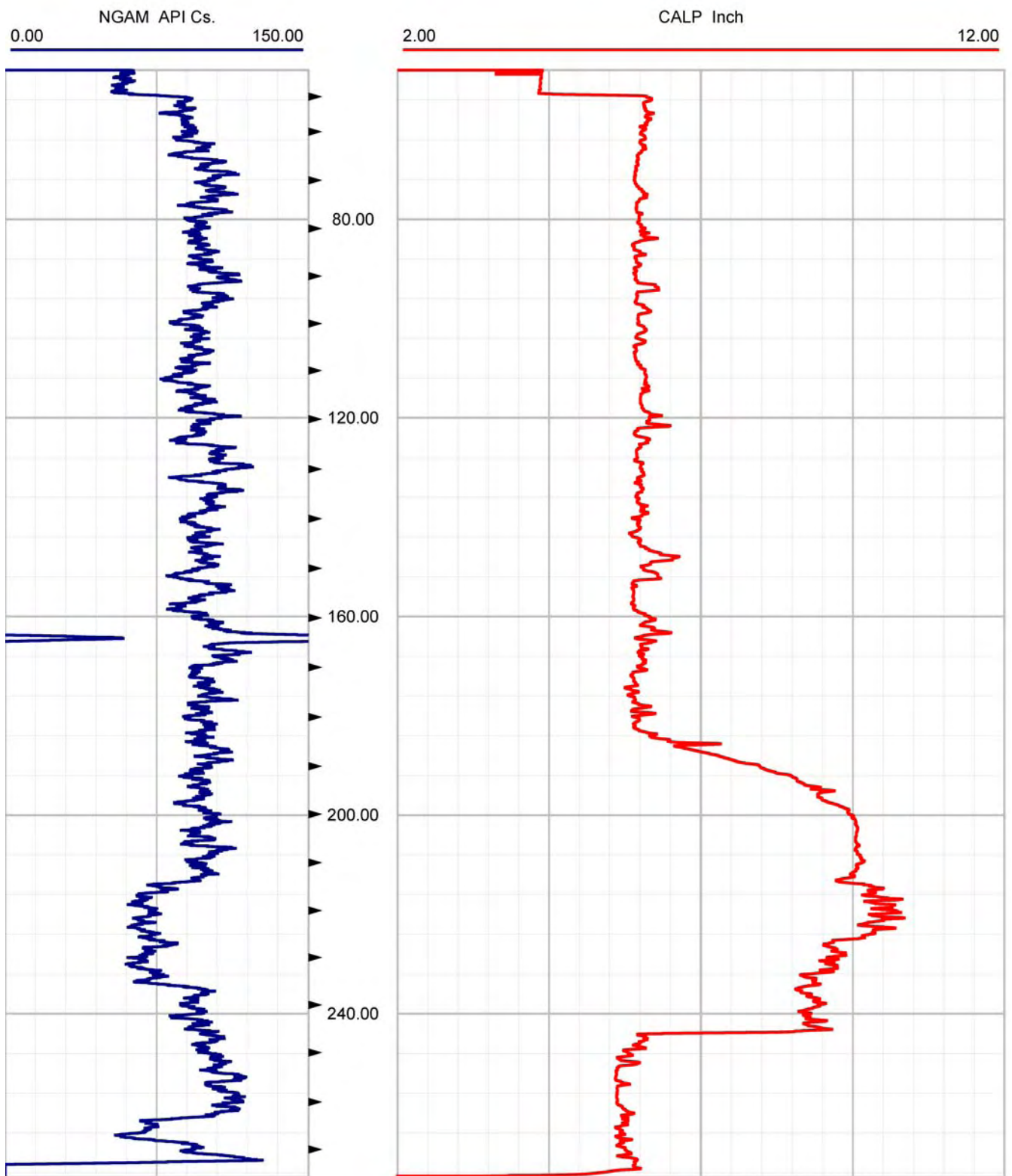


Figure 33. Boring Z3-B3, Caliper and Natural Gamma logs



CASCADE DRILLING

Borehole: Z3-B3

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 273.652 to 271.984ft  
 Mean dip format: dip-azimuth and dip

Interpretation 1

Dip data sets .....  
 BHTV dips

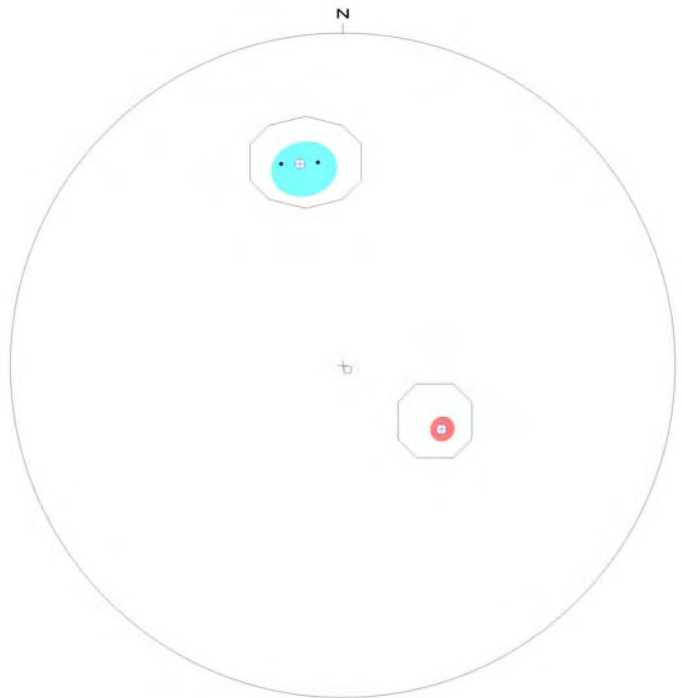
Z3-B3  
 Zone 0. 271.984 - 273.642ft  
 Deviation 1.60 N308.50

dipdata sets.....  
 BHTV dips  
 • Highlighted dips: Fracture Planar Hairline-fracture

	mean dip	n	f
N348 52	N348 52	2	2.04
N123 29	N123 29	1	( 0.00)

intersections

	N348 52	N123 29
N348 52		16 N065
N123 29	16 N065	



equal-area upper-hemisphere 0-90  
 contour-levels 1,  
 ⊕ mean dip  
 □ well axis

Figure 34. Boring Z3-B3, Stereonet Plot

Depth (feet)	Dip azimuth	Dip	Structure description
273.15	N343	53	Primary-structure Planar Bedding
272.68	N353	52	Primary-structure Planar Bedding
272.48	N123	29	Fracture Planar Hairline-fracture

Table 19. Boring Z3-B3, Structure depth, dip azimuth, dip and description

Deviated borehole in orthographic projection, viewed from N355

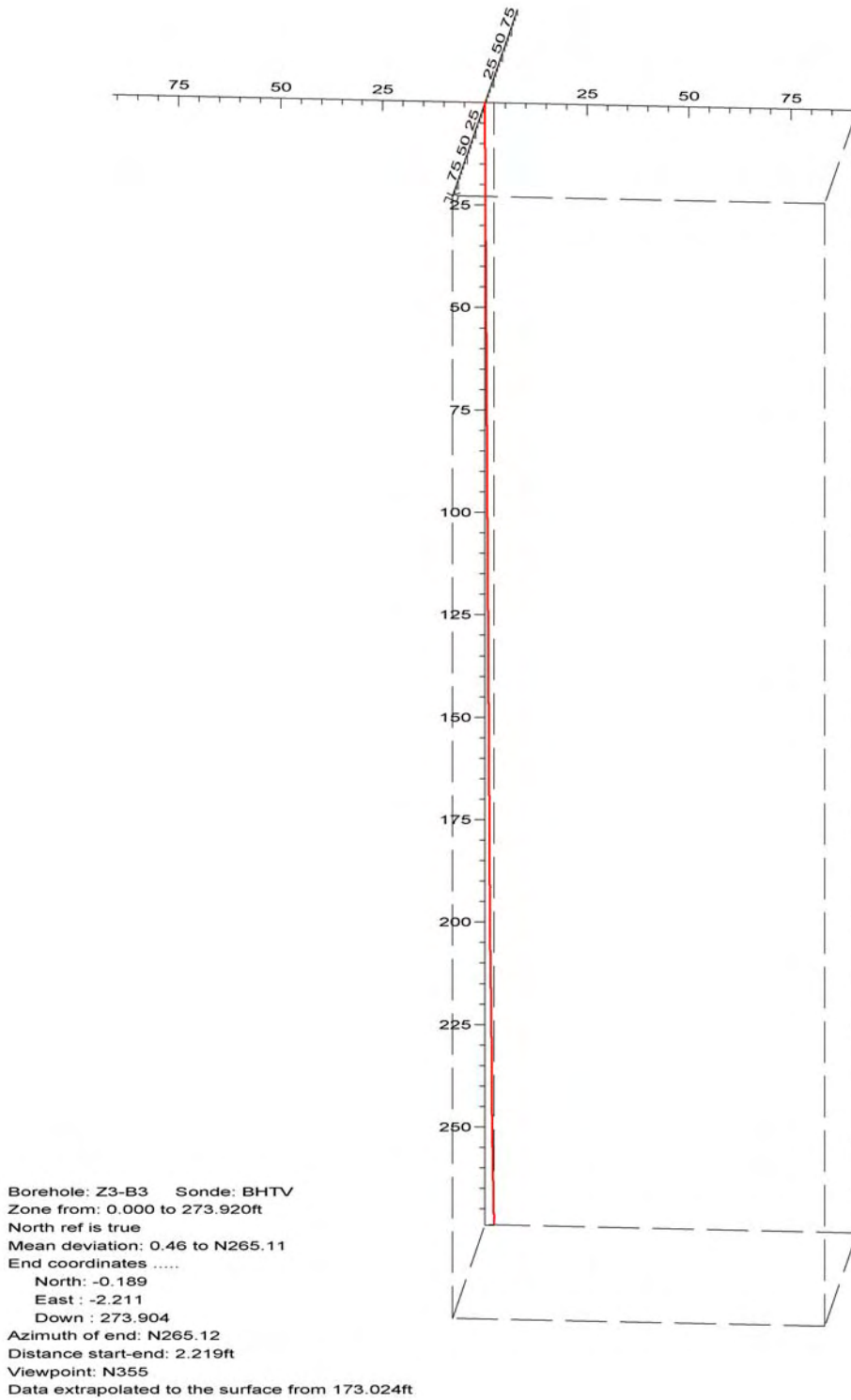


Figure 35. Boring Z3-B3, Deviation Projection

# SR-710 BORING Z3-B4

## VELOCITY (METERS/SECOND)

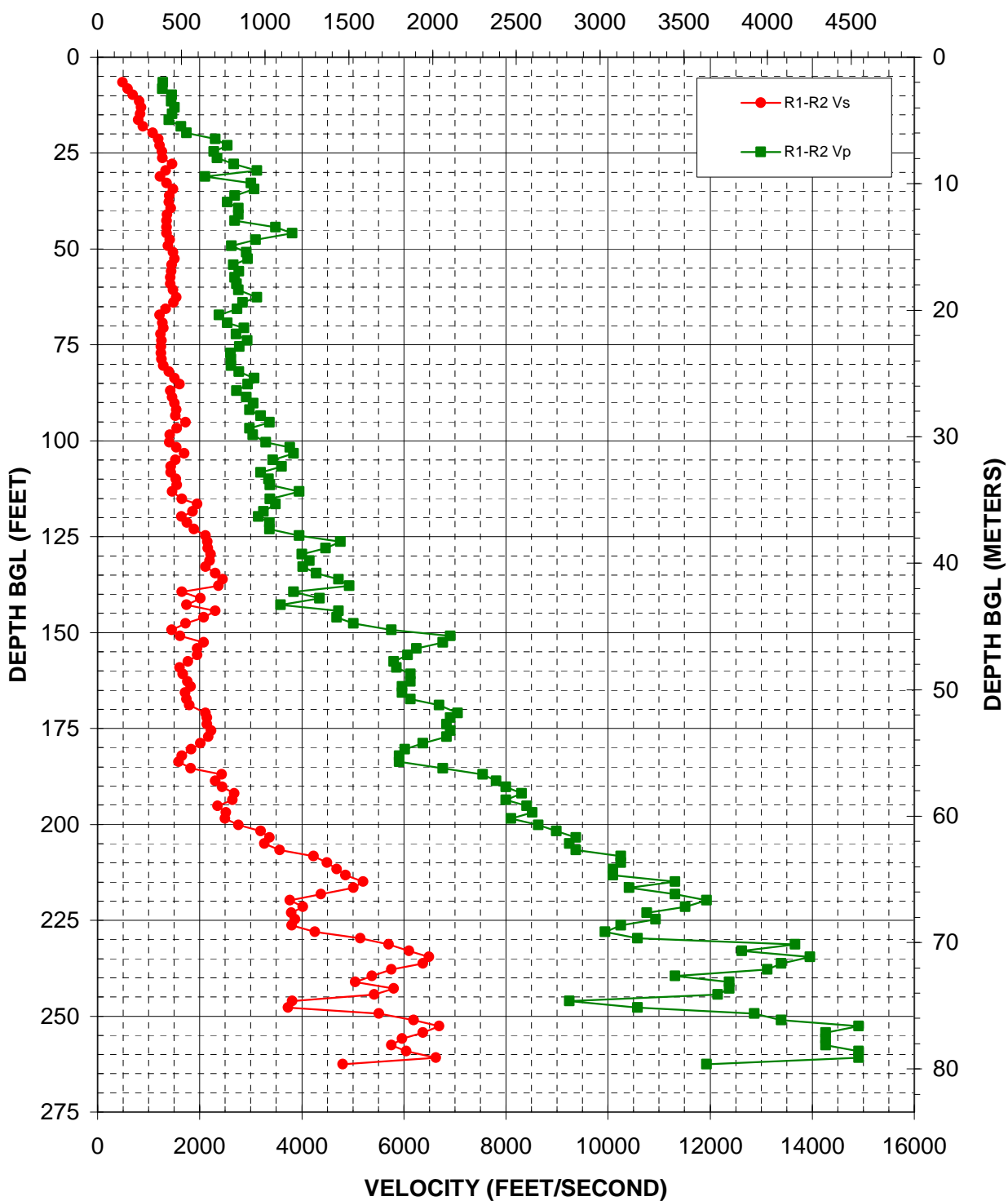


Figure 36: Boring Z3-B4, Suspension R1-R2 P- and  $S_H$ -wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
6.56	489	1277	88.58	1465	2916	170.93	2117	7056
8.20	594	1272	90.22	1512	3052	172.24	2144	6907
9.84	689	1452	91.86	1548	2983	173.88	2144	6835
11.48	814	1445	93.50	1526	3201	175.52	2224	6907
13.12	857	1505	95.14	1727	3365	177.17	2173	6835
14.76	833	1458	96.78	1555	2983	178.81	2019	6371
16.40	800	1402	98.43	1414	3038	180.45	1838	6020
18.04	894	1632	100.39	1408	3297	182.09	1657	5911
19.69	1079	1745	101.71	1540	3771	183.73	1589	5911
21.33	1189	2310	103.35	1700	3837	185.37	1823	6765
22.97	1215	2543	104.99	1526	3435	187.01	2430	7542
24.61	1267	2278	106.63	1433	3605	188.65	2310	7812
26.25	1272	2343	108.27	1433	3201	190.29	2439	8002
27.89	1458	2667	109.91	1533	3348	191.93	2678	8306
29.53	1334	3125	111.55	1555	3382	193.57	2646	8002
31.17	1224	2103	113.19	1458	3953	195.21	2352	8412
32.81	1356	3010	115.16	1649	3382	196.85	2514	8522
34.45	1485	3066	116.47	1953	3490	198.49	2495	8101
36.09	1408	2689	118.44	1864	3248	200.13	2757	8634
37.73	1396	2543	119.75	1640	3155	201.77	3201	8989
39.37	1433	2757	121.39	1754	3365	203.41	3365	9374
41.01	1361	2757	123.03	1886	3365	205.05	3265	9242
42.65	1356	2689	124.67	2117	3953	206.69	3566	9374
44.29	1350	3490	126.31	2151	4755	208.33	4233	10253
45.93	1356	3815	127.95	2158	4464	209.97	4494	10253
47.57	1420	3095	129.59	2217	4001	211.61	4687	10095
49.21	1384	2625	131.23	2202	4153	213.25	4861	10095
50.85	1478	2916	132.87	2117	4026	214.90	5208	11313
52.49	1505	2942	134.51	2310	4289	216.54	5009	10415
54.13	1452	2657	136.15	2448	4721	218.18	4374	11313
55.77	1445	2769	137.80	2369	4934	219.82	3771	11930
57.41	1426	2689	139.44	1649	3837	221.46	4026	11512
59.06	1426	2723	141.08	2013	4345	223.10	3793	10757
60.70	1478	2757	142.72	1745	3586	224.74	3871	10936
62.66	1540	3125	144.36	2310	4721	226.38	3804	10253
63.98	1491	2841	146.00	2076	4687	228.02	4261	9942
65.62	1334	2734	147.64	1727	5009	229.66	5146	10583
67.26	1215	2377	149.28	1452	5756	231.30	5706	13670
69.23	1272	2543	150.92	1620	6907	232.94	6104	12619
70.54	1287	2865	152.56	2083	6765	234.58	6497	13961
72.18	1233	2711	154.20	1953	6249	236.22	6371	13391
73.82	1252	2929	155.84	1953	6076	237.86	5756	13123
75.46	1247	2780	157.48	1773	5807	239.50	5378	11313
77.10	1247	2604	159.12	1608	5859	241.14	5047	12381
78.74	1252	2614	160.76	1674	6132	242.78	5807	12381
80.38	1292	2614	162.73	1759	6132	244.42	5423	12151
82.02	1402	2769	164.04	1828	5965	246.06	3815	9242
83.66	1512	3066	165.68	1713	5965	247.70	3728	10583
85.30	1608	2942	167.32	1745	6132	249.34	5514	12866
86.94	1426	2723	168.96	1798	6696	250.98	6190	13391

Table 20. Boring Z3-B4, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

<b>Depth (feet)</b>	<b>V<sub>s</sub> (feet/sec)</b>	<b>V<sub>p</sub> (feet/sec)</b>
252.62	6696	14913
254.27	6371	14265
255.91	5965	14265
257.55	5756	14265
259.19	6048	14913
260.83	6628	14913
262.47	4807	11930

Table 20, continued. Boring Z3-B4, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

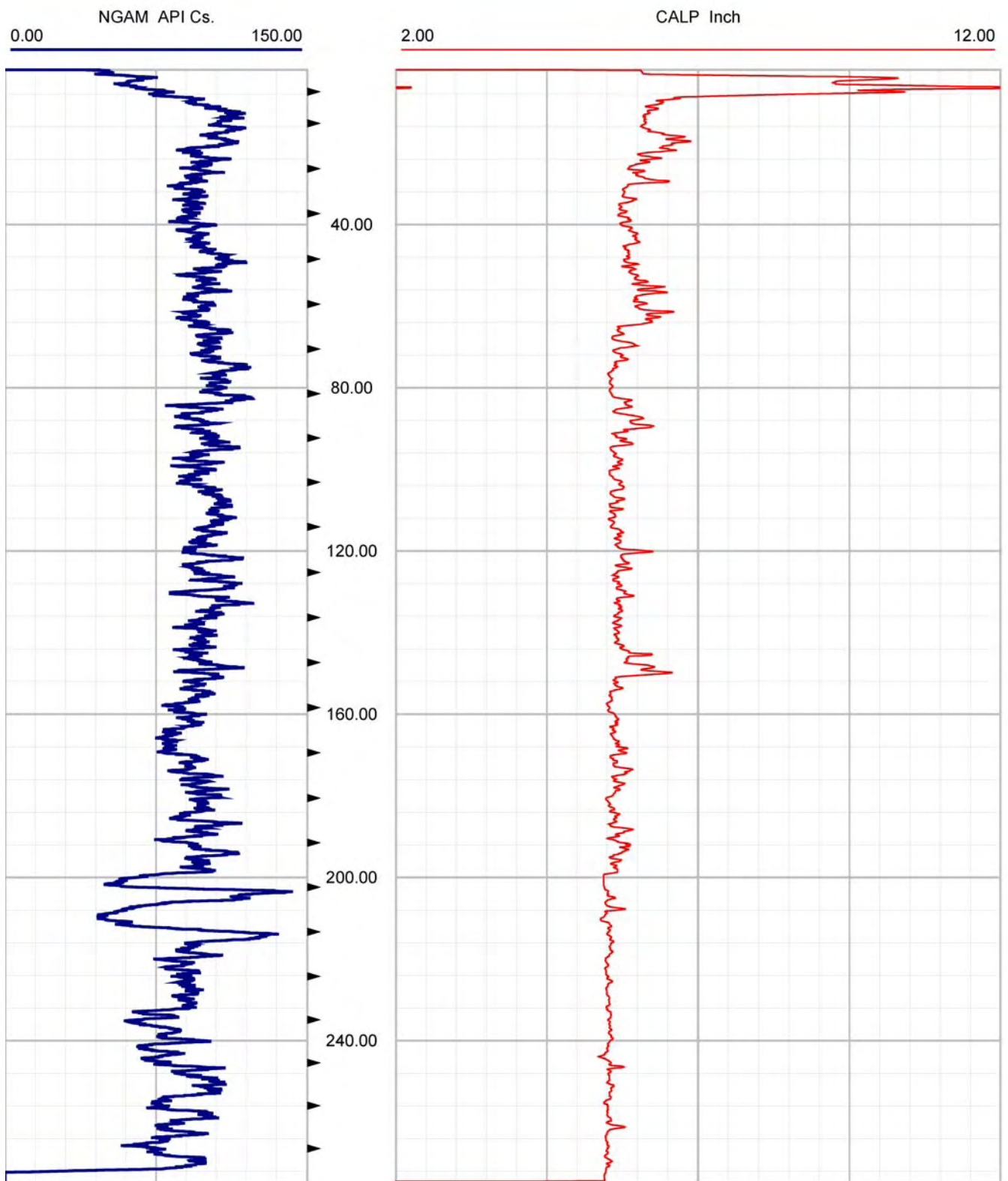


Figure 37. Boring Z3-B4, Caliper and Natural Gamma logs





CASCADE DRILLING

Borehole: Z3-B4

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 275.196 to 64.540ft  
 Mean dip format: dip-azimuth and dip

Interpretation 1

Dip data sets .....  
 BHTV dips

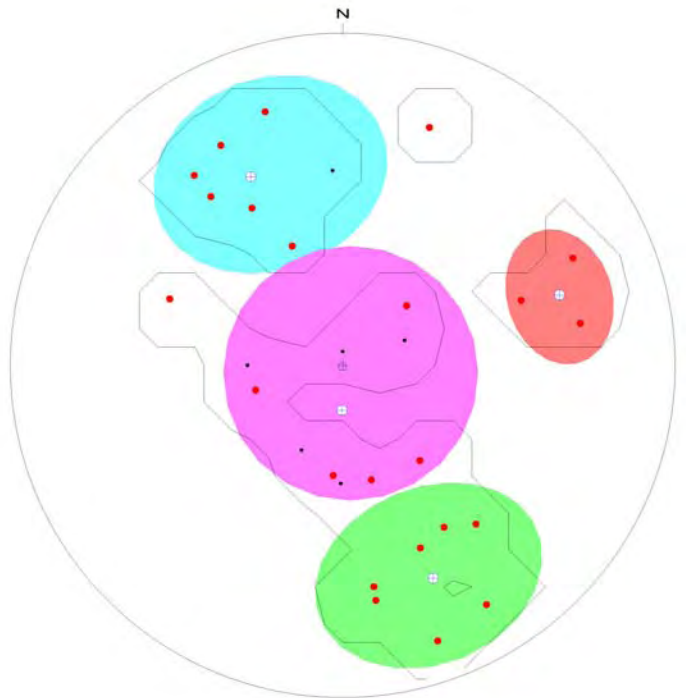
Z3-B4  
 Zone 0. 64.540 - 275.196ft  
 Deviation 0.30 N 25.80

dipdata sets.....  
 BHTV dips  
 • Highlighted dips: Fracture Planar Hairline-fracture

	mean dip	n	f
N334 53	N334 53	7	( 0.06)
N072 58	N072 58	3	( 0.03)
N157 59	N157 59	7	( 0.06)
N181 11	N181 11	10	( 0.05)

intersections

	N334 53	N072 58	N157 59	N181 11
N334 53	X	43 N018	02 N246	04 N247
N072 58	43 N018	X	50 N113	10 N156
N157 59	02 N246	50 N113	X	05 N244
N181 11	04 N247	10 N156	05 N244	X



equal-area upper-hemisphere 0-90  
 contour-levels 1,  
 ⊕ mean dip  
 □ well axis

Figure 38. Boring Z3-B4, Stereonet Plot

Depth (feet)	Dip azimuth	Dip	Structure description
274.74	N141	30	Fracture Planar Hairline-fracture
274.42	N065	65	Fracture Planar Hairline-fracture
274.33	N020	65	Fracture Planar Hairline-fracture
273.39	N331	65	Fracture Planar Hairline-fracture
273.13	N080	62	Fracture Planar Hairline-fracture
271.88	N185	27	Fracture Planar Hairline-fracture
271.42	N157	50	Fracture Planar Hairline-fracture
271.18	N148	48	Fracture Planar Hairline-fracture
270.43	N161	77	Fracture Planar Hairline-fracture
270.26	N181	29	Primary-structure Planar Bedding
267.93	N149	73	Fracture Planar Hairline-fracture
265.43	N166	29	Fracture Planar Hairline-fracture
265.05	N343	69	Fracture Planar Hairline-fracture
259.99	N330	45	Fracture Planar Hairline-fracture
258.86	N322	54	Fracture Planar Hairline-fracture
258.15	N291	47	Fracture Planar Hairline-fracture
257.82	N047	21	Fracture Planar Hairline-fracture
252.67	N070	48	Fracture Planar Hairline-fracture
250.25	N254	22	Fracture Planar Hairline-fracture
248.28	N172	61	Fracture Planar Hairline-fracture
247.64	N359	3	Primary-structure Planar Bedding
245.30	N322	62	Fracture Planar Hairline-fracture
236.66	N172	57	Fracture Planar Hairline-fracture
215.95	N140	52	Fracture Planar Hairline-fracture
199.28	N337	32	Fracture Planar Hairline-fracture
191.94	N357	49	Primary-structure Planar Bedding
190.56	N206	23	Primary-structure Planar Bedding
133.02	N270	23	Primary-structure Planar Bedding
65.04	N068	16	Primary-structure Planar Bedding

Table 21. Boring Z3-B4, Structure depth, dip azimuth, dip and description

Deviated borehole in orthographic projection, viewed from N123

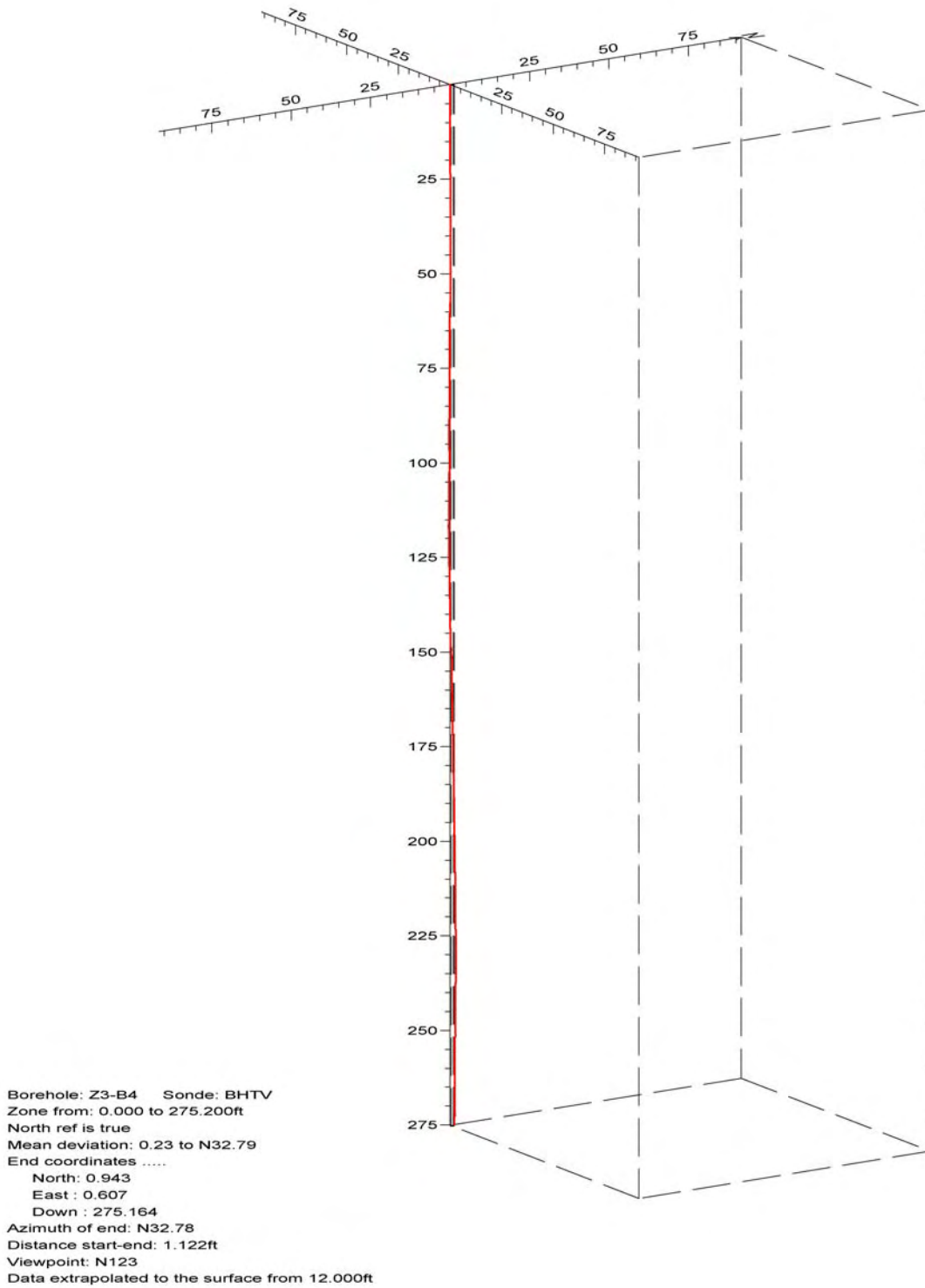


Figure 39. Boring Z3-B4, Deviation Projection

# SR-710 BORING Z3-B6

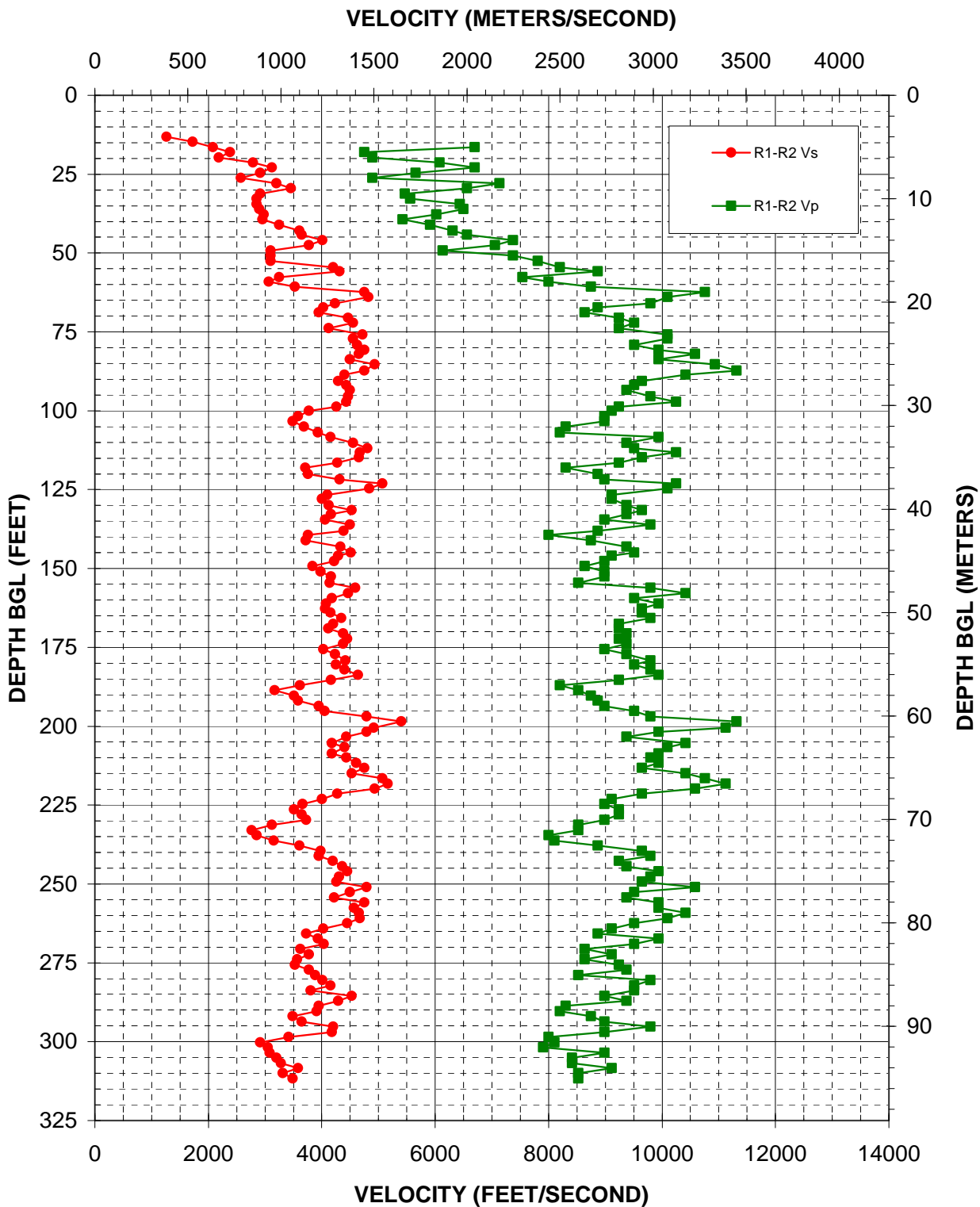


Figure 40: Boring Z3-B6, Suspension R1-R2 P- and S<sub>H</sub>-wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
13.12	1262		95.47	4464	9794	177.17	4233	9374
14.76	1727		97.11	4434	10253	179.13	4419	9794
16.40	2083	6696	98.75	4261	9242	180.45	4247	9510
18.04	2386	4755	100.07	3771	9113	182.09	4404	9794
19.69	2187	4897	101.71	3586	8989	183.73	4637	9942
21.33	2792	6076	103.35	3490	8989	185.37	4166	9242
22.97	3125	6696	104.99	3686	8306	187.01	3615	8202
24.61	2916	5657	106.96	3929	8202	188.65	3170	8522
26.25	2573	4897	108.27	4153	9942	190.29	3509	8749
27.89	3201	7132	110.24	4557	9374	191.93	3586	8867
29.53	3454	6562	111.88	4807	9510	193.57	3953	8989
31.17	2916	5468	113.19	4670	10253	195.21	4050	9510
32.81	2853	5561	114.83	4654	9650	196.85	4790	9794
34.45	2853	6433	116.47	4275	9242	198.49	5401	11313
36.09	2903	6497	118.11	3707	8306	200.46	4915	11121
37.73	2983	6020	120.08	3760	8867	201.77	4790	9942
39.37	2956	5423	121.72	4317	8989	203.41	4434	9374
41.01	3248	5911	123.03	5067	10253	205.38	4179	10415
42.98	3605	6309	124.67	4843	10095	206.69	4404	10095
44.29	3645	6562	126.64	4101	9113	208.66	4179	9942
45.93	4013	7373	127.95	4001	9113	209.97	4434	9794
47.57	3771	7056	129.92	4127	9374	211.61	4605	9942
49.21	3095	6132	131.56	4525	9650	213.25	4755	9650
50.85	3095	7373	132.87	4166	9374	214.90	4525	10415
52.49	3095	7812	134.51	4063	8989	216.54	5067	10757
54.46	4206	8202	136.15	4494	9794	218.18	5167	11121
55.77	4317	8867	138.12	4389	8867	219.82	4934	10583
57.74	3248	7542	139.44	3760	8002	221.46	4275	9650
59.06	3066	8002	141.08	3718	8749	223.10	4001	9113
60.70	3528	8749	143.04	4331	9374	224.74	3666	8989
62.34	4755	10757	145.01	4510	9510	226.38	3509	9242
63.98	4825	10095	146.00	4289	9113	228.02	3645	9242
65.94	4233	9794	147.64	4220	8989	229.66	3728	8989
67.26	4026	8867	149.28	3837	8634	231.30	3125	8522
68.90	3953	8634	150.92	3977	8989	232.94	2769	8522
70.54	4464	9242	152.56	4166	8989	234.58	2853	8002
72.18	4557	9510	154.53	4140	8522	236.22	3155	8101
73.82	4127	9242	156.17	4589	9794	237.86	3605	8867
75.79	4721	10095	157.81	4464	10415	239.50	3977	9650
77.10	4557	10095	159.45	4179	9510	241.14	3953	9794
79.07	4621	9510	161.09	4076	9942	242.78	4193	9242
80.71	4755	9942	162.73	4063	9650	244.42	4360	9374
82.02	4654	10583	164.04	4153	9650	246.06	4449	9942
83.66	4494	9942	165.68	4345	9794	247.70	4303	9794
85.30	4934	10936	167.65	4206	9242	249.34	4261	9650
87.27	4755	11313	168.96	4114	9242	250.98	4790	10583
88.58	4404	10415	170.60	4374	9374	252.62	4494	9510
90.55	4289	9650	172.24	4449	9242	254.27	4220	9374
91.86	4434	9510	173.88	4374	9374	255.91	4755	9942
93.50	4494	9374	175.52	4026	8989	257.55	4573	9942

Table 22. Boring Z3-B6, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

<b>Depth (feet)</b>	<b>V<sub>s</sub> (feet/sec)</b>	<b>V<sub>p</sub> (feet/sec)</b>
259.19	4654	10415
260.83	4670	10095
262.47	4449	9510
264.11	4026	9113
265.75	3728	8867
267.39	3929	9942
269.03	4038	9510
270.67	3625	8634
272.31	3771	9113
273.95	3566	8634
275.59	3528	9242
277.23	3771	9374
278.87	3883	8522
280.51	4013	9794
282.15	4153	9510
283.79	3804	9510
285.43	4525	8989
287.07	4289	9374
288.71	3953	8306
290.35	3906	8202
291.99	3490	8749
293.64	3645	8989
295.28	4206	9794
296.92	4179	8989
298.56	3418	8002
300.20	2916	8101
301.84	3052	7906
303.48	3081	8989
305.12	3201	8412
306.76	3281	8412
308.40	3586	9113
310.04	3314	8522
311.68	3490	8522

Table 22, continued. Boring Z3-B6, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

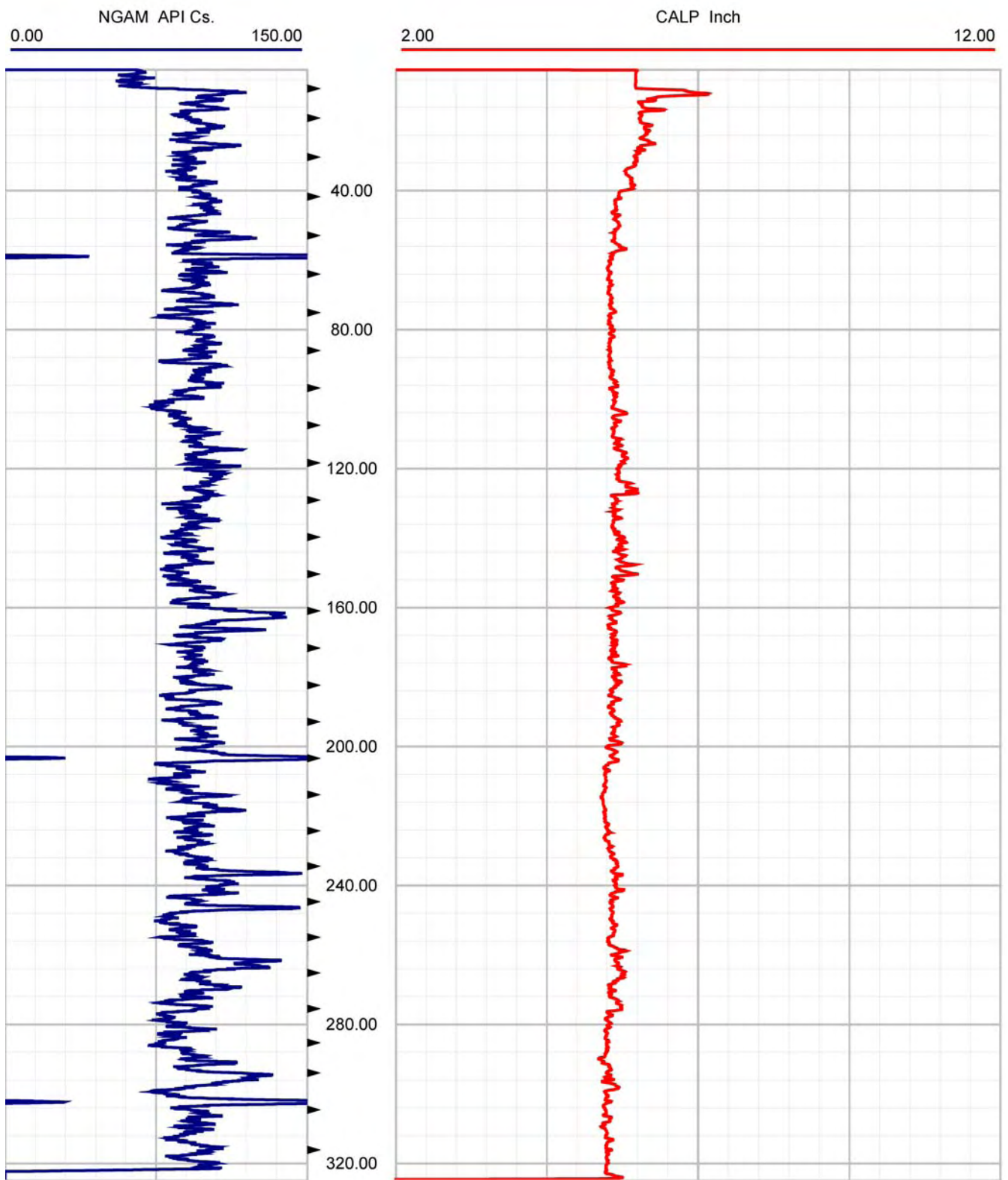


Figure 41. Boring Z3-B6, Caliper and Natural Gamma logs



CASCADE DRILLING

Borehole: Z3-B6

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 285.973 to 45.665ft  
 Mean dip format: dip-azimuth and dip

Interpretation 1

Dip data sets .....

BHTV dips

Z3-B6

Zone 0. 45.665 - 285.973ft  
 Deviation 2.10 N 78.30

dipdata sets.....

BHTV dips

Highlighted dips: Fracture Planar Hairline-fracture

	mean dip	n	f
N293 51	N293 51	7	( 0.04)
N347 35	N347 35	4	( 0.02)

intersections

	N293 51	N347 35
N293 51		35 N348
N347 35	35 N348	

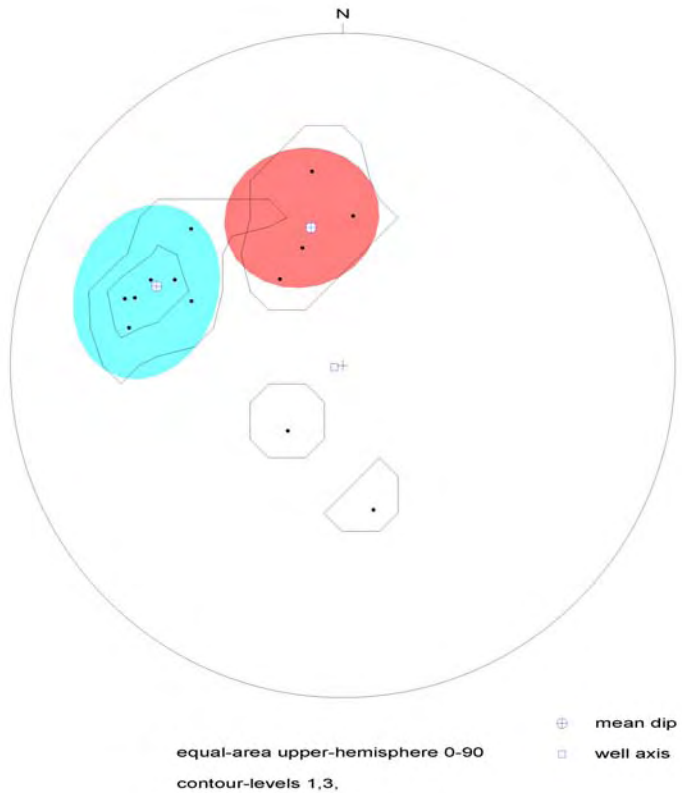


Figure 42. Boring Z3-B6, Stereonet Plot



Depth (feet)	Dip azimuth	Dip	Structure description
285.47	N351	49	Primary-structure Planar Bedding
267.80	N324	26	Primary-structure Planar Bedding
256.46	N004	37	Primary-structure Planar Bedding
255.27	N341	31	Primary-structure Planar Bedding
219.30	N312	52	Primary-structure Planar Bedding
108.50	N280	55	Primary-structure Planar Bedding
108.43	N288	56	Primary-structure Planar Bedding
97.24	N294	53	Primary-structure Planar Bedding
97.13	N287	58	Primary-structure Planar Bedding
63.31	N168	37	Primary-structure Planar Bedding
61.26	N220	21	Primary-structure Planar Bedding
46.68	N293	41	Primary-structure Planar Bedding
46.17	N297	47	Primary-structure Planar Bedding

Table 23. Boring Z3-B6, Structure depth, dip azimuth, dip and description

Deviated borehole in orthographic projection, viewed from N171

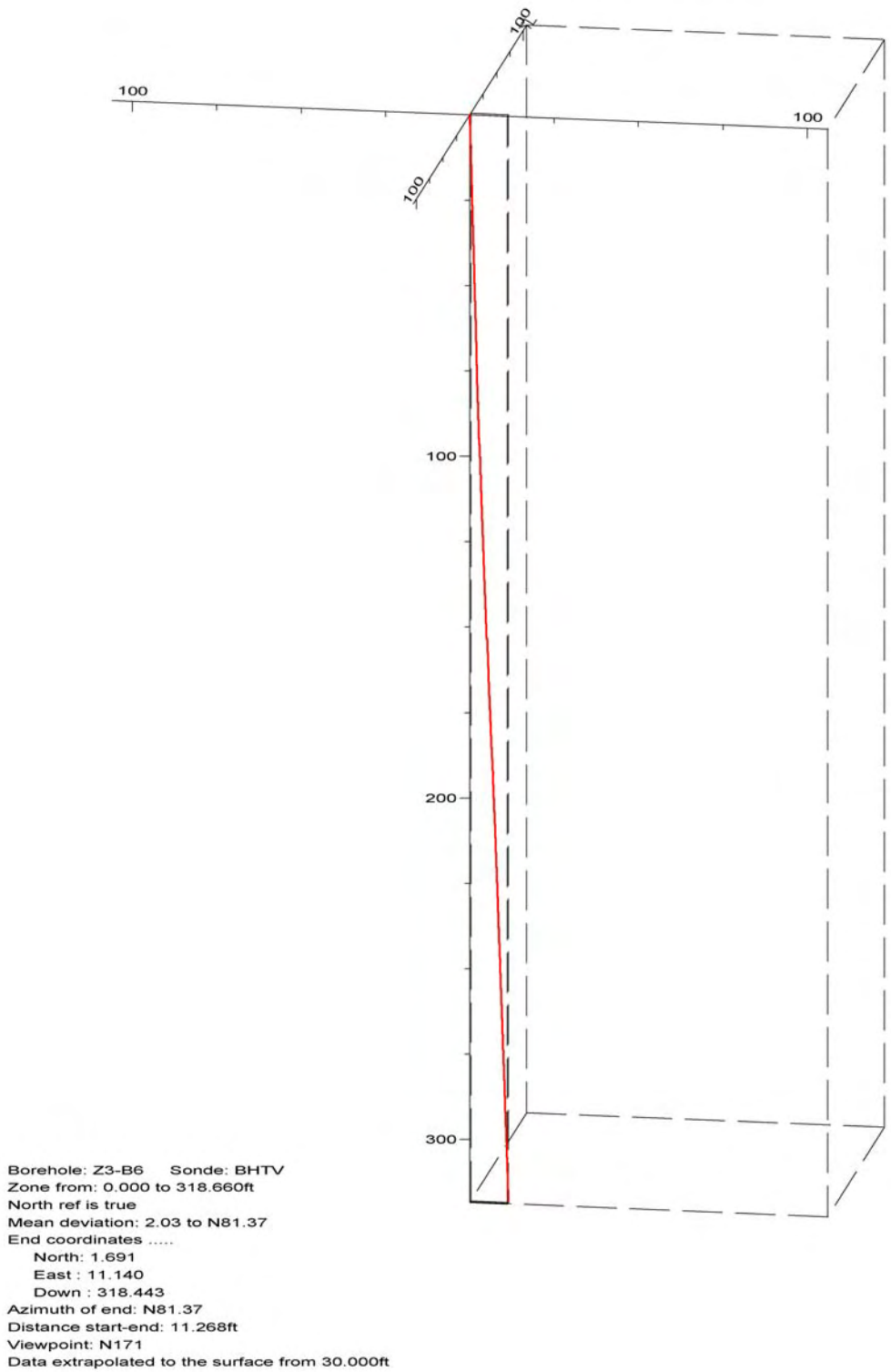


Figure 43. Boring Z3-B6, Deviation Projection

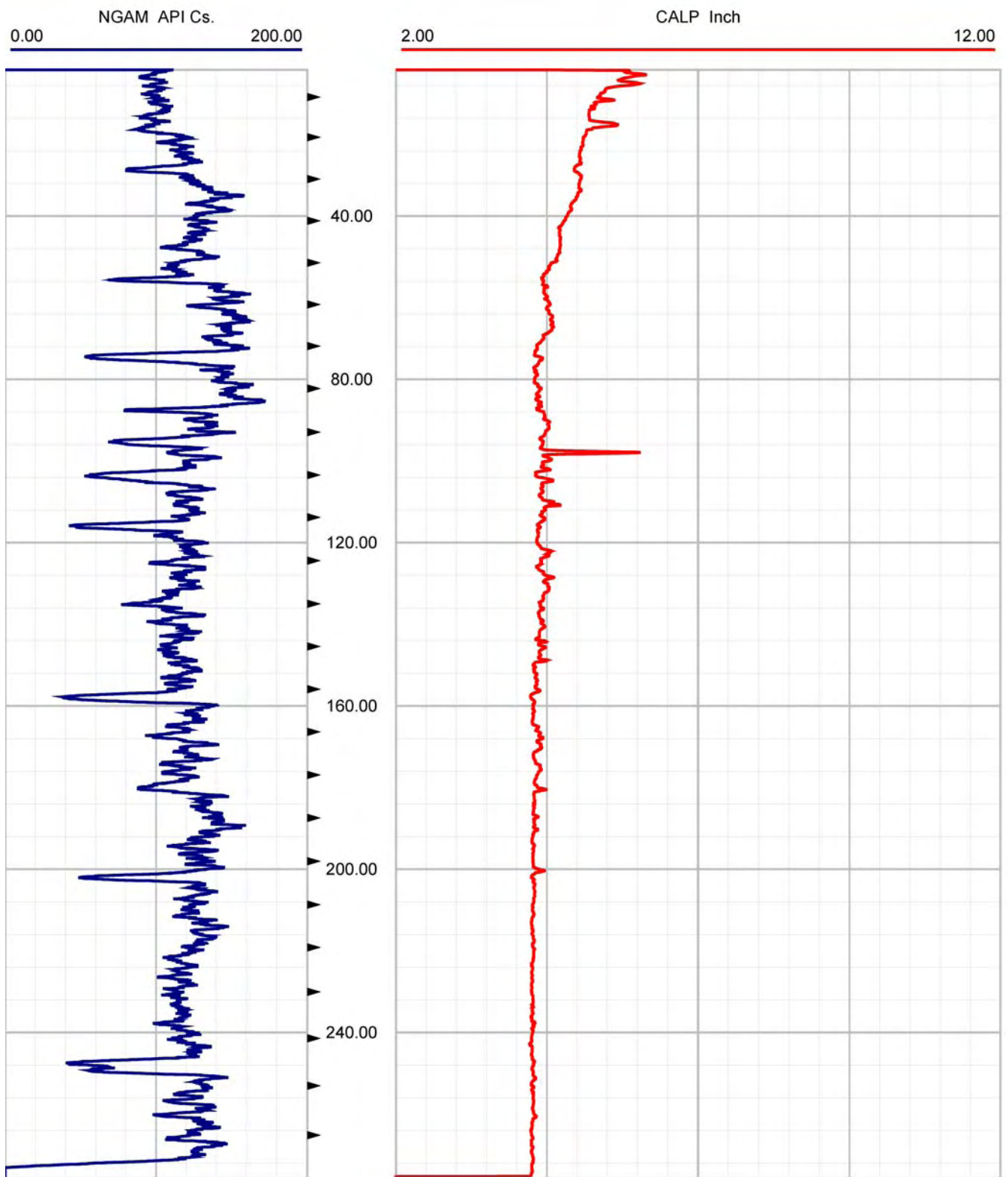


Figure 44. Boring Z3-B8, Caliper and Natural Gamma logs

# SR-710 BORING Z3-B12

## VELOCITY (METERS/SECOND)

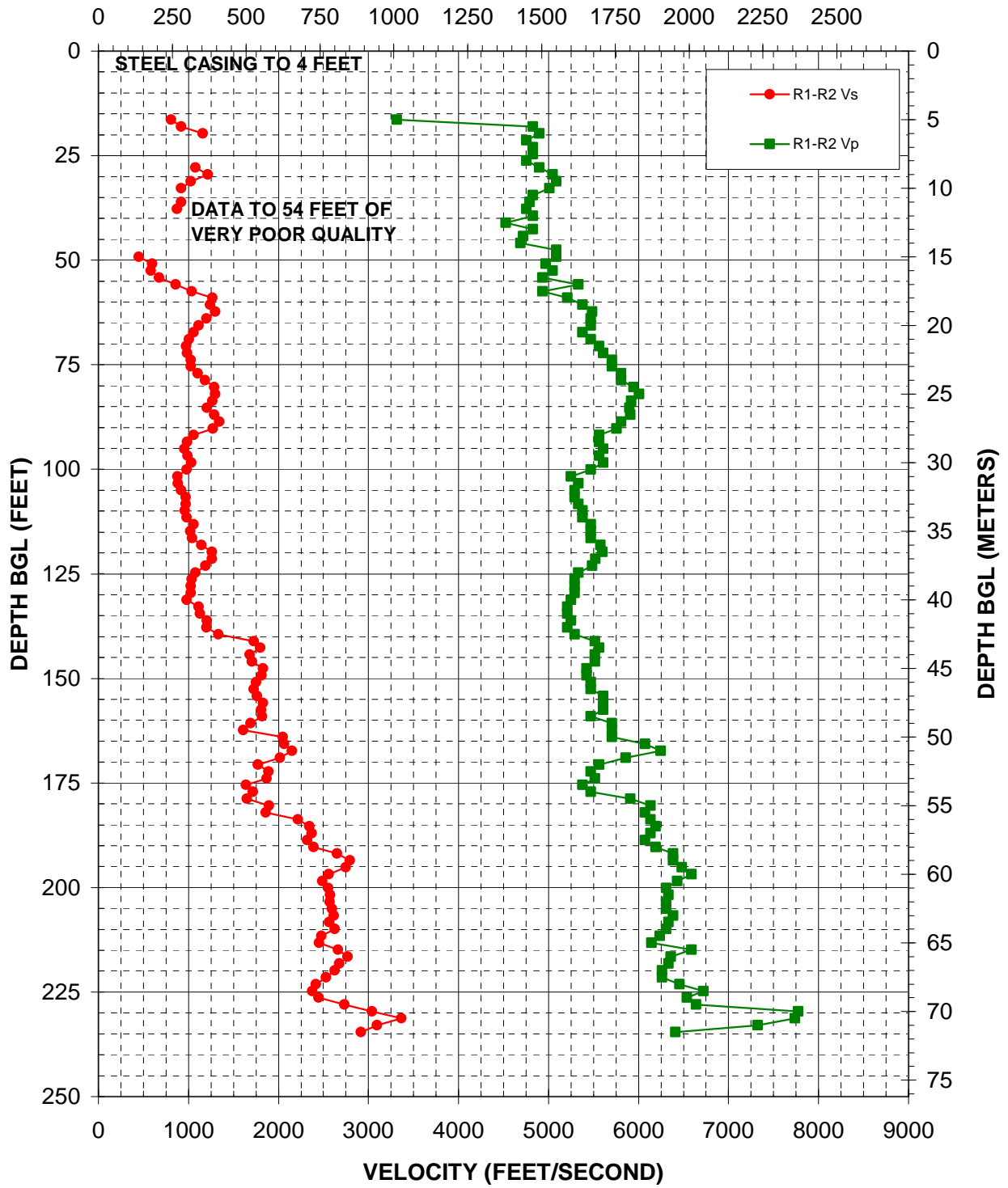


Figure 45: Boring Z3-B12, Suspension R1-R2 P- and S<sub>H</sub>-wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
8.20			96.78	991	5561	178.81	1649	5911
16.40	805	3314	98.43	1032	5608	180.45	1896	6132
18.04	918	4825	100.07	982	5468	182.09	1859	6076
19.69	1161	4897	101.71	877	5249	183.73	2217	6132
21.33		4755	103.35	882	5335	185.37	2343	6190
22.97		4825	104.99	922	5292	187.01	2369	6132
24.61		4825	106.63	971	5292	188.65	2319	6076
26.25		4755	108.27	971	5335	190.29	2390	6190
27.89	1076	4897	109.91	959	5378	191.93	2651	6383
29.53	1215	5047	111.55	979	5378	193.57	2792	6383
31.17	1025	5087	113.19	1058	5468	195.21	2745	6484
32.81	918	5009	114.83	1020	5468	196.85	2558	6588
34.45		4825	116.47	1043	5468	198.49	2485	6433
36.09	918	4790	118.11	1143	5580	200.13	2553	6309
37.73	875	4755	119.75	1262	5599	201.77	2573	6334
39.37		4825	121.39	1259	5523	203.41	2568	6309
41.01		4525	123.03	1191	5486	205.05	2594	6309
42.65		4825	124.67	1079	5335	206.69	2614	6383
44.29		4721	126.31	1035	5292	208.33	2563	6334
45.93		4687	127.95	1025	5292	209.97	2625	6309
47.57		5087	129.59	1028	5292	211.61	2476	6237
49.21	449	5087	131.23	982	5249	213.25	2453	6144
50.85	599	4971	132.87	1112	5208	214.90	2662	6588
52.49	583	5047	134.51	1131	5208	216.54	2769	6358
54.13	676	4934	136.15	1206	5249	218.18	2678	6334
55.77	859	5335	137.80	1202	5208	219.82	2625	6261
57.41	1038	4934	139.44	1334	5292	221.46	2529	6261
59.06	1267	5208	141.08	1727	5514	223.10	2417	6458
60.70	1243	5378	142.72	1798	5561	224.74	2377	6723
62.34	1297	5486	144.36	1682	5514	226.38	2448	6536
63.98	1202	5468	146.00	1704	5514	228.02	2734	6641
65.62	1116	5468	147.64	1828	5423	229.66	3038	7774
67.26	1055	5378	149.28	1813	5423	231.30	3365	7738
68.90	1006	5468	150.92	1750	5468	232.94	3095	7323
70.54	976	5561	152.56	1727	5468	234.58	2916	6408
72.18	988	5608	154.20	1764	5608			
73.82	1028	5706	155.84	1828	5608			
75.46	1025	5706	157.48	1808	5608			
77.10	1105	5807	159.12	1818	5468			
78.74	1184	5807	160.76	1691	5706			
80.38	1289	5944	162.40	1608	5706			
82.02	1299	6009	164.04	2051	5706			
83.66	1267	5922	165.68	2063	6076			
85.30	1206	5901	167.32	2151	6249			
86.94	1287	5911	168.96	2019	5859			
88.58	1345	5807	170.60	1773	5561			
90.22	1272	5756	172.24	1891	5468			
91.86	1058	5561	173.88	1869	5514			
93.50	988	5561	175.52	1640	5378			
95.14	954	5608	177.17	1718	5468			

NOTE: "blank" space indicates data of insufficient quality for good pick. See Appendix A for Source-to-Receiver measurement.

Table 24. Boring Z3-B12, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

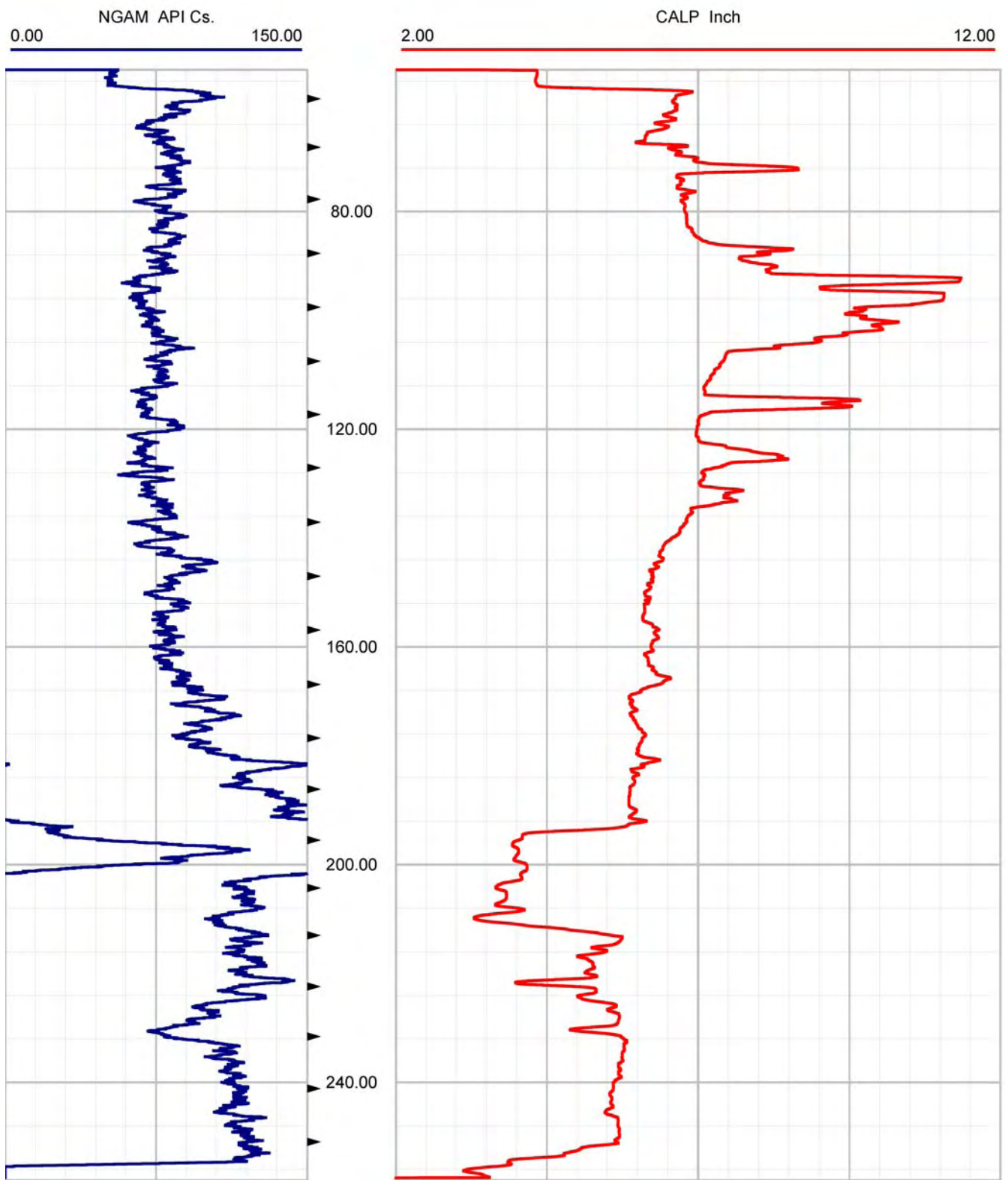


Figure 46. Boring Z3-B12, Caliper and Natural Gamma logs



CASCADE DRILLING

Borehole: Z3-B12

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 179.361 to 113.631ft  
 Mean dip format: dip-azimuth and dip

Interpretation 1

Dip data sets .....  
 BHTV dips

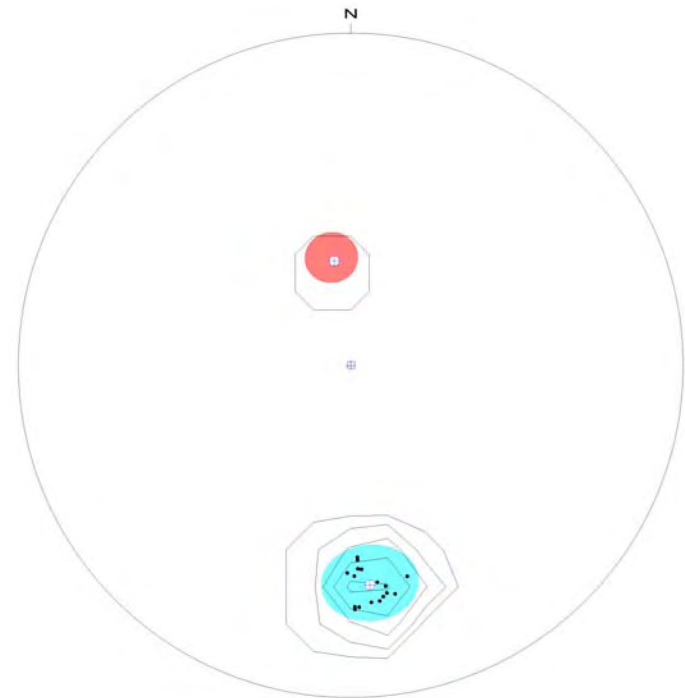
Z3-B12  
 Zone 0. 113.631 - 179.351ft  
 Deviation 0.20 N234.00

dipdata sets.....  
 BHTV dips  
 • Highlighted dips: Fracture Planar Open-fracture

	mean dip	n	f
N175 56	N175 56	17	0.47
N351 26	N351 26	1	( 0.00)

intersections

	N175 56	N351 26
N175 56		01 N264
N351 26	01 N264	



equal-area upper-hemisphere 0-90  
 contour-levels 1,3,6,10,15,  
 ⊕ mean dip  
 □ well axis

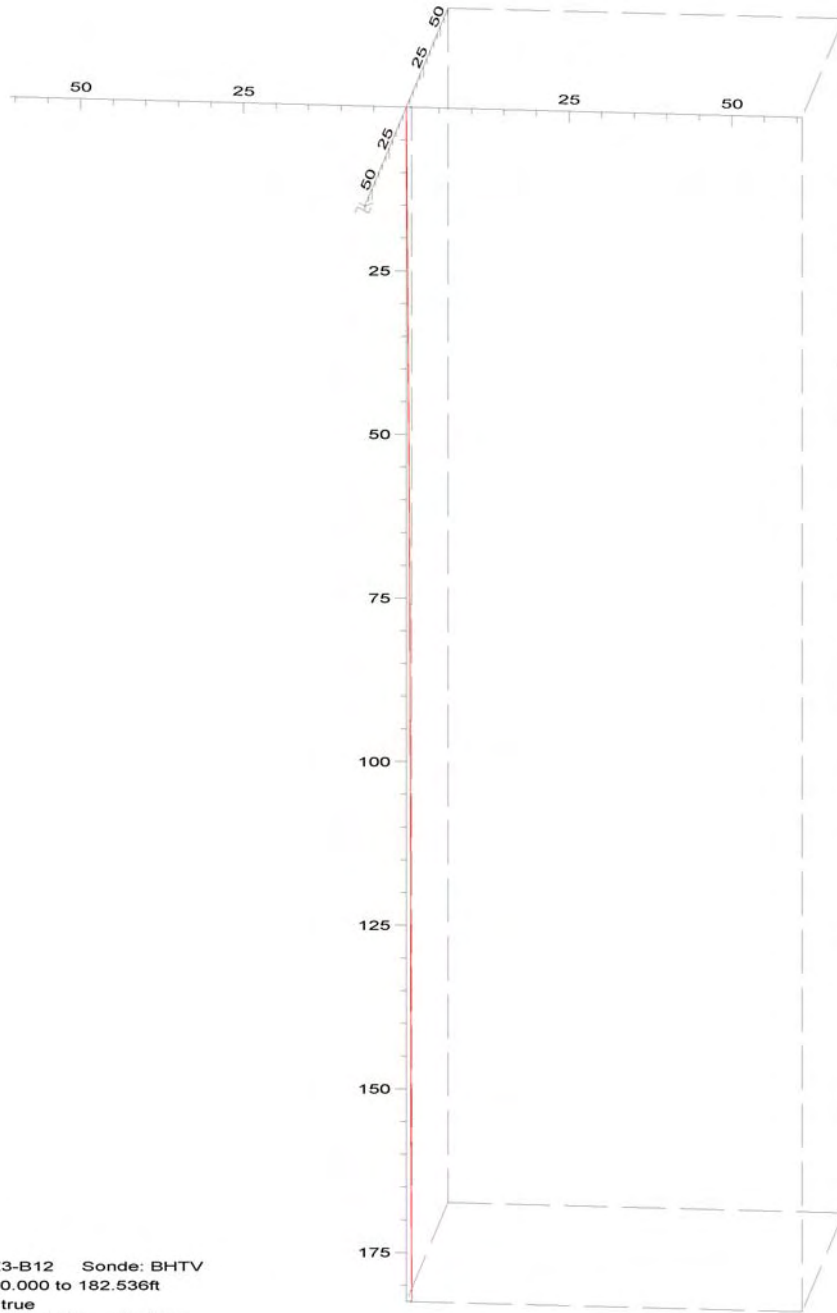
Figure 47. Boring Z3-B12, Stereonet Plot

Depth (feet)	Dip azimuth	Dip	Structure description
178.86	N179	62	Primary-structure Planar Bedding
178.55	N179	63	Primary-structure Planar Bedding
177.99	N178	62	Primary-structure Planar Bedding
176.93	N175	61	Primary-structure Planar Bedding
176.29	N173	61	Primary-structure Planar Bedding
174.71	N172	60	Primary-structure Planar Bedding
162.82	N171	57	Primary-structure Planar Bedding
162.36	N169	59	Primary-structure Planar Bedding
161.74	N165	55	Primary-structure Planar Bedding
159.94	N171	59	Primary-structure Planar Bedding
157.05	N179	53	Primary-structure Planar Bedding
156.16	N173	55	Primary-structure Planar Bedding
152.02	N178	49	Primary-structure Planar Bedding
150.86	N178	48	Primary-structure Planar Bedding
148.50	N178	51	Primary-structure Planar Bedding
146.45	N181	53	Primary-structure Planar Bedding
131.08	N177	52	Primary-structure Planar Bedding
114.13	N351	26	Primary-structure Planar Bedding

Table 25. Boring Z3-B12, Structure depth, dip azimuth, dip and description



Deviated borehole in orthographic projection, viewed from N354



Borehole: Z3-B12 Sonde: BHTV  
 Zone from: 0.000 to 182.536ft  
 North ref is true  
 Mean deviation: 0.27 to N263.66  
 End coordinates .....  
 North: -0.094  
 East : -0.846  
 Down : 182.516  
 Azimuth of end: N263.66  
 Distance start-end: 0.852ft  
 Viewpoint: N354  
 Data extrapolated to the surface from 57.000ft

Distances in feet, Deviation and Azimuths in degrees

Figure 48. Boring Z3-B12, Deviation Projection

# SR-710 BORING Z4-B4

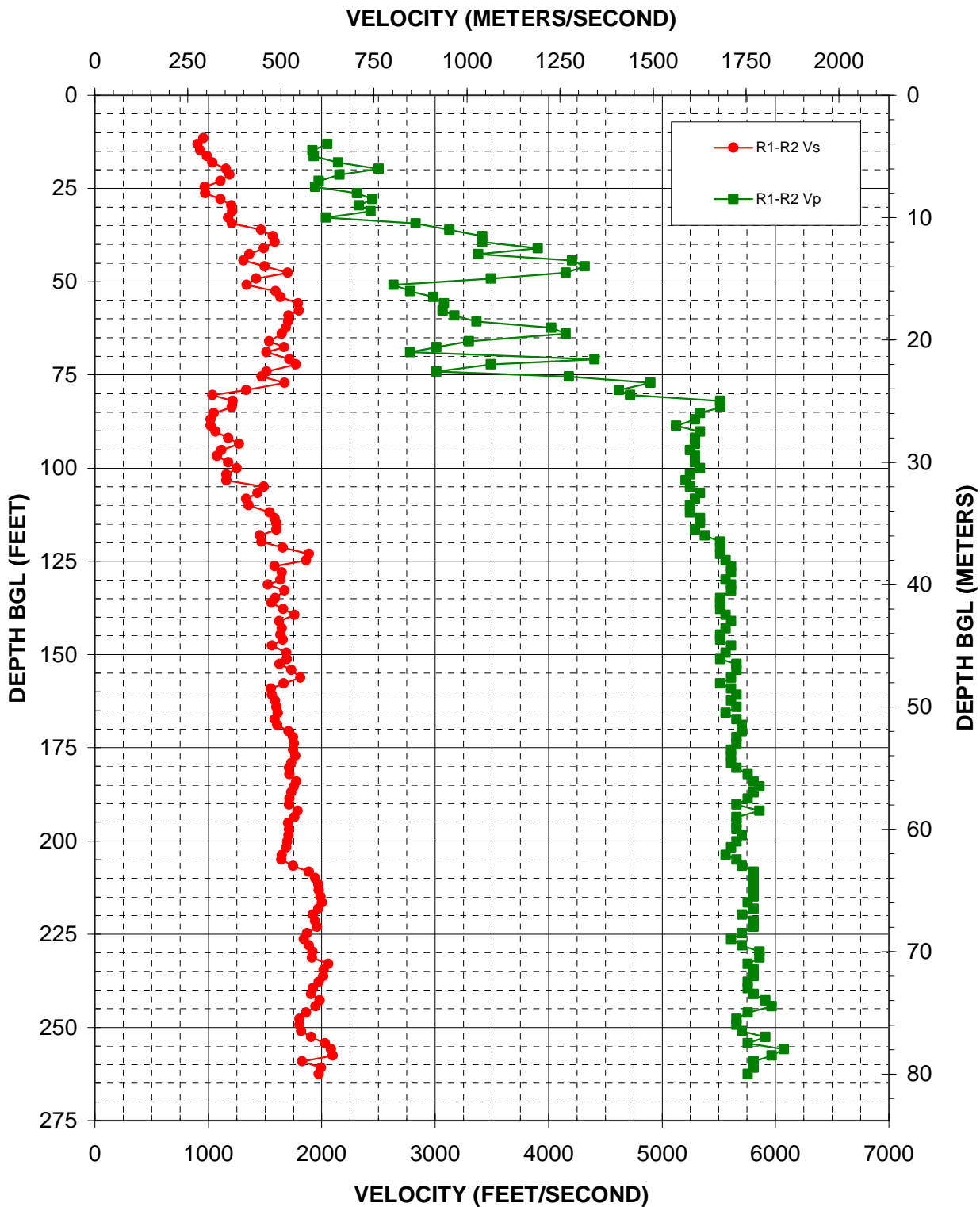


Figure 49: Boring Z4-B4, Suspension R1-R2 P- and S<sub>H</sub>-wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
11.48	958		93.50	1272	5292	175.52	1750	5608
13.12	904	2051	95.14	1116	5249	177.17	1769	5608
14.76	929	1919	96.78	1076	5292	179.13	1731	5608
16.40	991	1930	98.43	1176	5292	180.45	1713	5657
18.04	1035	2144	100.07	1252	5335	182.09	1718	5756
19.69	1155	2504	101.71	1159	5249	184.06	1776	5807
21.33	1189	2158	103.35	1159	5208	185.37	1754	5859
22.97	1108	1976	104.99	1491	5249	187.01	1731	5807
24.61	968	1941	106.63	1433	5335	188.65	1718	5756
26.25	974	2310	108.27	1334	5292	190.29	1713	5657
27.89	1108	2448	109.91	1356	5249	191.93	1788	5859
29.53	1202	2327	111.88	1540	5249	193.57	1759	5657
31.17	1211	2430	113.52	1585	5335	195.21	1704	5657
32.81	1176	2038	114.83	1600	5335	196.85	1713	5657
34.45	1206	2828	116.47	1600	5292	198.49	1709	5706
36.09	1465	3125	118.11	1455	5378	200.13	1696	5657
37.73	1570	3418	119.75	1468	5514	201.77	1687	5608
39.37	1585	3418	121.39	1657	5514	203.74	1649	5561
41.01	1491	3906	123.03	1886	5514	205.05	1645	5657
42.65	1361	3382	124.67	1864	5561	206.69	1750	5706
44.29	1312	4206	126.31	1585	5608	208.33	1886	5807
45.93	1498	4317	127.95	1649	5608	209.97	1941	5807
47.57	1700	4153	129.92	1636	5561	211.61	1970	5807
49.21	1420	3490	131.23	1526	5608	213.25	1976	5807
50.85	1339	2635	132.87	1674	5608	214.90	1988	5807
52.49	1593	2780	134.84	1589	5514	216.54	2001	5756
54.13	1636	2983	136.15	1559	5514	218.18	1970	5807
55.77	1793	3081	137.80	1661	5514	219.82	1924	5706
57.74	1798	3066	139.44	1759	5561	221.46	1941	5807
59.06	1709	3170	141.08	1624	5608	223.10	1959	5807
60.70	1704	3365	143.04	1649	5561	224.74	1869	5706
62.34	1682	4026	144.69	1636	5514	226.38	1843	5608
63.98	1649	4153	146.00	1657	5514	228.02	1886	5706
65.94	1537	3297	147.64	1562	5608	229.66	1919	5859
67.59	1670	3010	149.61	1687	5561	231.30	1913	5859
68.90	1512	2780	151.25	1691	5514	232.94	2057	5756
70.87	1718	4404	152.56	1628	5657	234.58	2019	5807
72.18	1773	3490	154.20	1731	5657	236.22	2013	5807
74.15	1512	3010	156.17	1813	5608	237.86	1976	5756
75.46	1471	4179	157.81	1665	5514	239.50	1924	5756
77.10	1674	4897	159.12	1555	5608	241.14	1907	5807
79.07	1334	4621	160.76	1562	5657	242.78	1982	5911
80.38	1038	4721	162.40	1589	5608	244.42	1947	5965
82.02	1215	5514	164.04	1600	5657	246.06	1864	5756
83.66	1206	5514	165.68	1612	5561	247.70	1803	5657
85.30	1048	5335	167.32	1585	5657	249.34	1803	5657
86.94	1022	5292	168.96	1608	5706	250.98	1818	5706
88.58	1022	5126	170.60	1709	5706	252.62	1907	5911
90.22	1065	5335	172.24	1750	5657	254.27	2031	5756
91.86	1176	5292	173.88	1754	5657	255.91	2083	6076

Table 26. Boring Z4-B4, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
257.55	2096	5965
259.19	1828	5807
260.83	1994	5807
262.47	1976	5756

Table 26, continued. Boring Z4-B4, Suspension R1-R2 depths and P- and S<sub>H</sub>-wave velocities

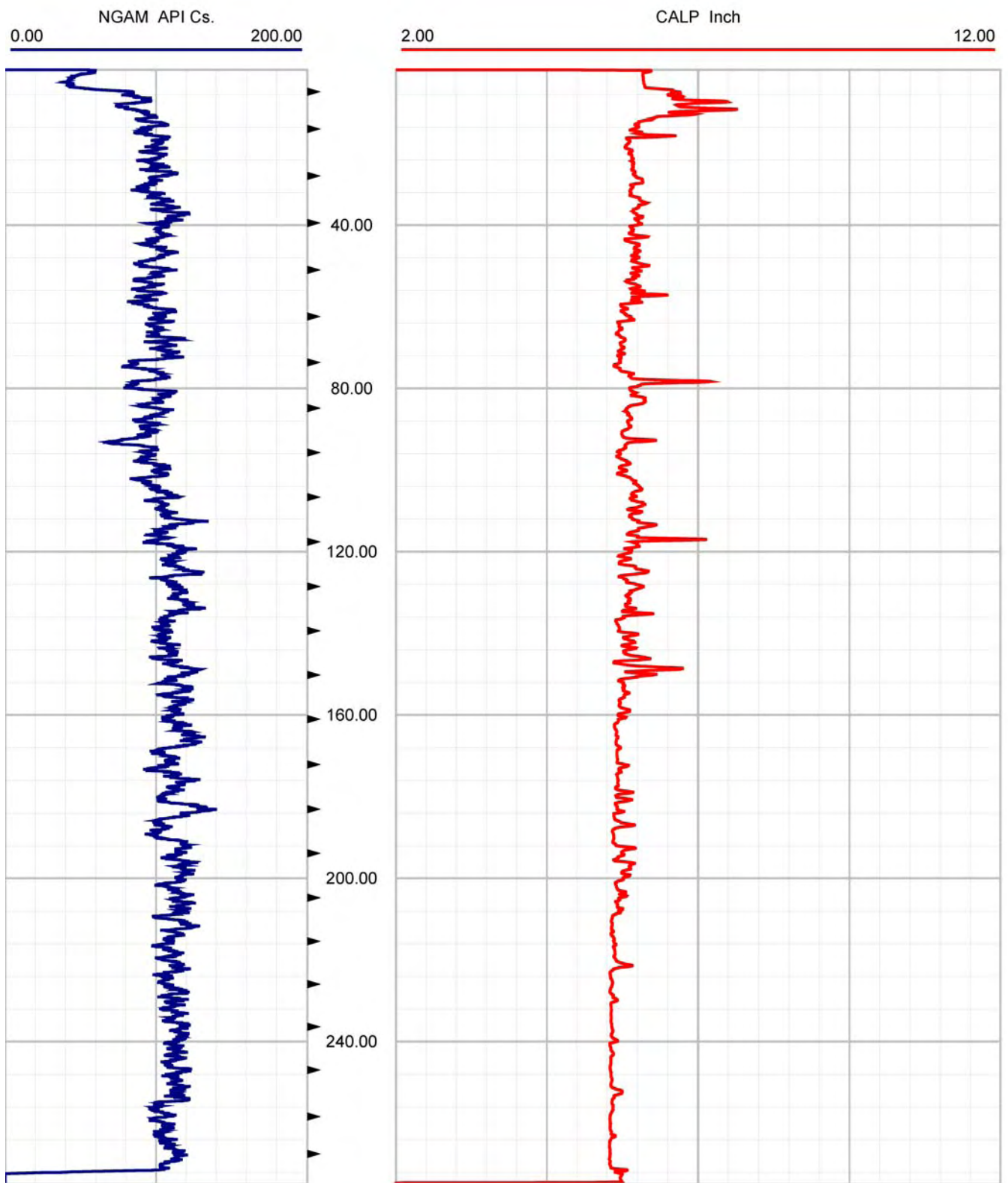


Figure 50. Boring Z4-B4, Caliper and Natural Gamma logs



CASCADE DRILLING

Borehole: Z4-B4

SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref: true  
 Depth units are feet

Zone from 274.222 to 17.723ft  
 Mean dip format: dip-azimuth and dip

Interpretation 1

Dip data sets .....  
 BHTV dips

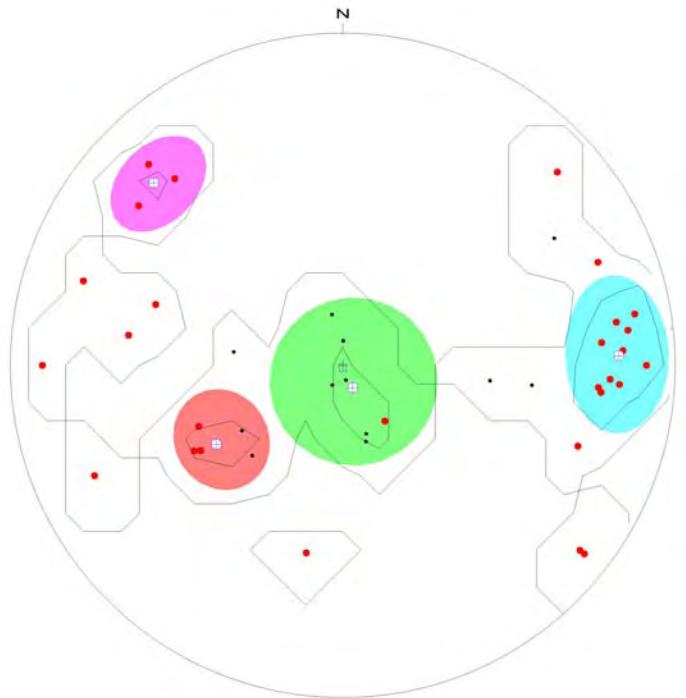
Z4-B4  
 Zone 0. 17.723 - 274.222ft  
 Deviation 0.60 N356.10

dipdata sets.....  
 BHTV dips  
 • Highlighted dips: Fracture Planar Hairline-fracture

	mean dip	n	f
N088 72	N088 72	10	( 0.13)
N238 37	N238 37	5	( 0.02)
N156 6	N156 6	7	( 0.03)
N314 68	N314 68	3	( 0.03)

intersections

	N088 72	N238 37	N156 6	N314 68
N088 72	X	17 N172	06 N176	47 N018
N238 37	17 N172	X	06 N156	37 N242
N156 6	06 N176	06 N156	X	02 N225
N314 68	47 N018	37 N242	02 N225	X



equal-area upper-hemisphere 0-90  
 contour-levels 1,3.  
 ⊕ mean dip  
 □ well axis

Figure 51. Boring Z4-B4, Stereonet Plot

Depth (feet)	Dip azimuth	Dip	Structure description
273.72	N318	65	Fracture Planar Hairline-fracture
273.28	N316	73	Fracture Planar Hairline-fracture
269.47	N308	67	Fracture Planar Hairline-fracture
257.47	N239	41	Fracture Planar Hairline-fracture
245.93	N109	64	Fracture Planar Hairline-fracture
208.70	N143	17	Fracture Planar Hairline-fracture
187.06	N001	6	Primary-structure Planar Bedding
182.56	N128	81	Fracture Planar Hairline-fracture
173.49	N128	80	Fracture Planar Hairline-fracture
172.05	N068	72	Fracture Planar Hairline-fracture
168.70	N208	6	Primary-structure Planar Bedding
168.04	N168	4	Primary-structure Planar Bedding
159.96	N083	75	Fracture Planar Hairline-fracture
159.55	N240	43	Fracture Planar Hairline-fracture
155.97	N247	39	Fracture Planar Hairline-fracture
152.85	N288	50	Fracture Planar Hairline-fracture
152.03	N191	48	Fracture Planar Hairline-fracture
150.23	N094	72	Fracture Planar Hairline-fracture
146.46	N085	67	Fracture Planar Hairline-fracture
145.99	N081	72	Fracture Planar Hairline-fracture
144.45	N246	71	Fracture Planar Hairline-fracture
142.84	N087	73	Fracture Planar Hairline-fracture
140.85	N288	71	Fracture Planar Hairline-fracture
121.97	N080	78	Fracture Planar Hairline-fracture
121.13	N095	66	Fracture Planar Hairline-fracture
120.84	N096	67	Fracture Planar Hairline-fracture
120.50	N093	69	Fracture Planar Hairline-fracture
118.41	N090	81	Fracture Planar Hairline-fracture
118.05	N278	55	Fracture Planar Hairline-fracture
117.53	N225	32	Primary-structure Planar Bedding
117.11	N096	37	Primary-structure Planar Bedding
114.88	N277	27	Primary-structure Planar Bedding
113.08	N270	80	Fracture Planar Hairline-fracture
112.28	N048	76	Fracture Planar Hairline-fracture
98.48	N059	63	Primary-structure Planar Bedding
78.32	N096	48	Primary-structure Planar Bedding
43.39	N237	30	Primary-structure Planar Bedding
35.14	N348	13	Primary-structure Planar Bedding
18.61	N161	18	Primary-structure Planar Bedding
18.22	N163	20	Primary-structure Planar Bedding

Table 27. Boring Z4-B4, Structure depth, dip azimuth, dip and description

Deviated borehole in orthographic projection, viewed from N90

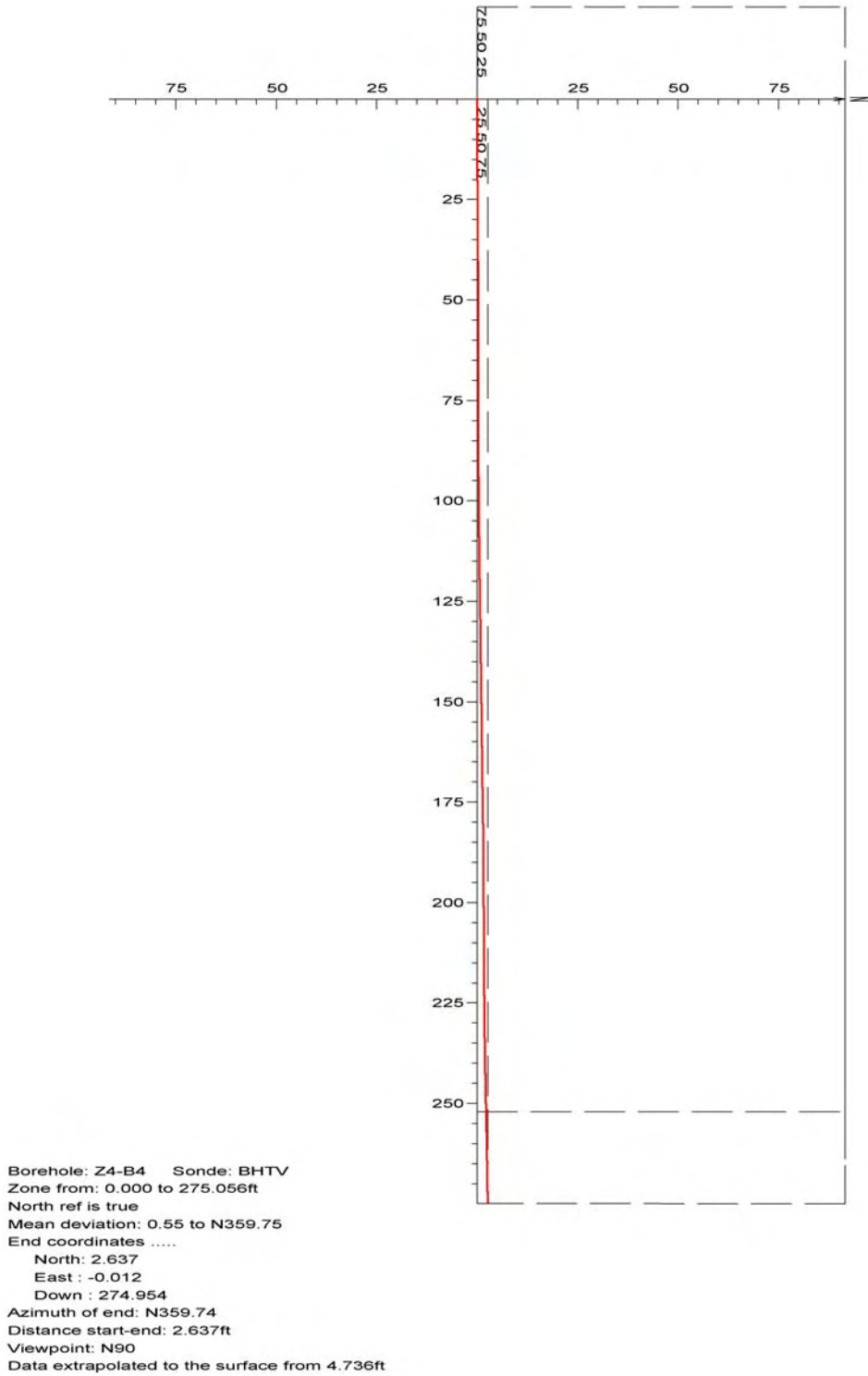


Figure 52. Boring Z4-B4, Deviation Projection



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**APPENDIX A**

**SUSPENSION VELOCITY MEASUREMENT  
QUALITY ASSURANCE SUSPENSION SOURCE  
TO RECEIVER ANALYSIS RESULTS**

# SR-710 BORING Z1-B3

## VELOCITY (METERS/SECOND)

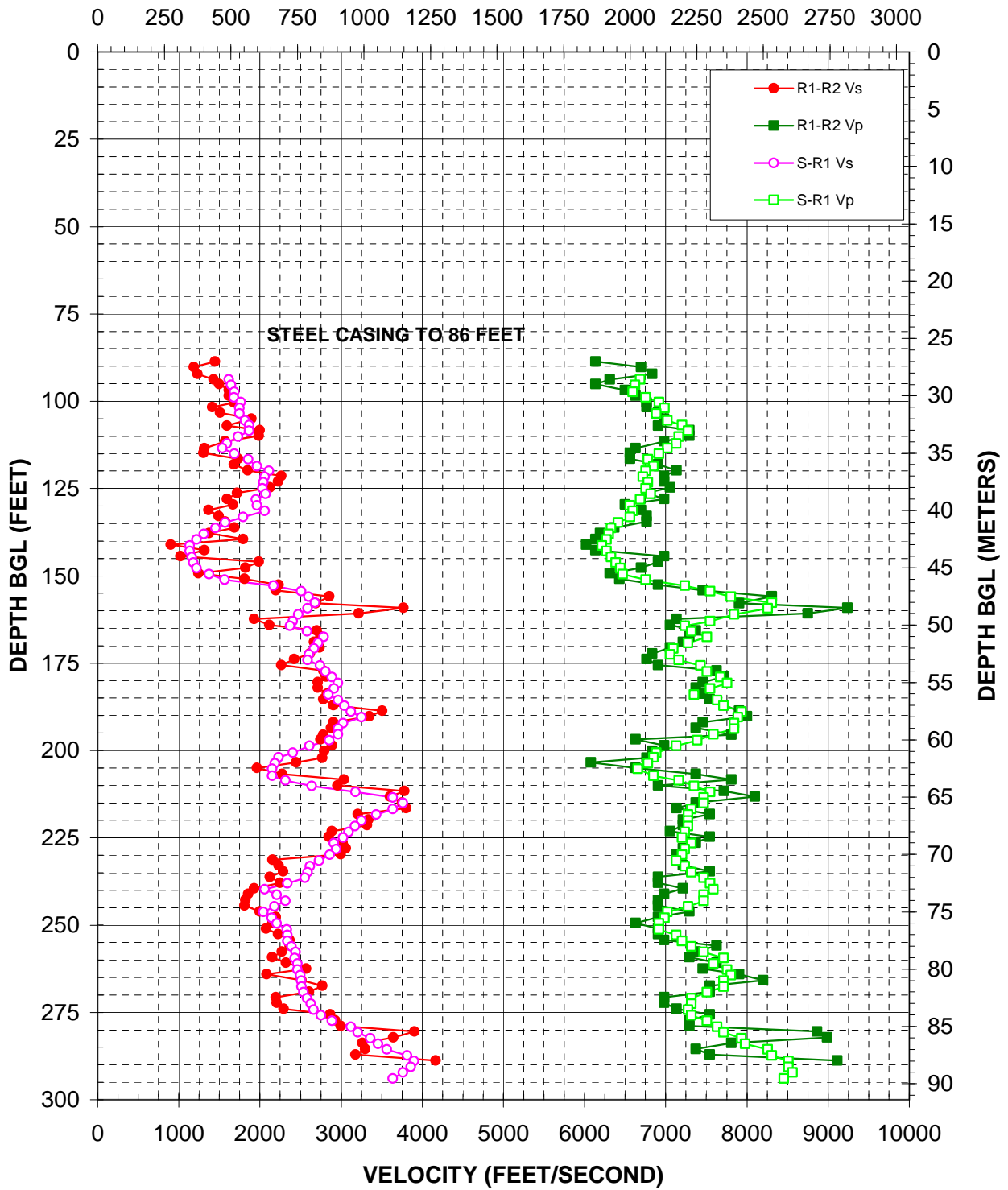


Figure A-1. Boring Z1-B3, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
93.73	1618	6687
95.37	1648	6624
97.34	1688	6592
98.98	1680	6751
100.30	1764	6917
101.94	1747	6986
103.58	1747	6883
105.54	1819	7021
106.86	1867	7201
108.50	1867	7276
110.14	1729	7164
112.11	1596	7128
113.42	1540	7021
115.06	1688	6917
116.70	1857	6784
118.67	1961	6850
119.98	2108	6751
121.62	2059	6719
123.26	2044	6784
124.90	2032	6751
126.54	2071	6817
128.18	1950	6687
129.82	1961	6562
131.46	2059	6592
133.10	1796	6562
134.74	1571	6412
136.38	1451	6325
138.02	1310	6297
139.67	1220	6269
141.31	1132	6213
142.95	1134	6269
144.59	1166	6325
146.23	1182	6383
147.87	1219	6441
149.51	1371	6471
151.15	1567	6751
152.79	2167	7238
154.43	2507	7549
156.07	2600	7801
157.71	2680	8309
159.35	2591	8260
160.99	2472	7845
162.96	2404	7549
164.27	2372	7238
165.91	2581	7314
167.55	2786	7509
169.19	2721	7276
170.83	2670	7092
172.47	2605	7056
174.11	2591	7164

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
175.75	2743	7430
177.40	2808	7509
179.04	2889	7673
180.68	2962	7758
182.32	2913	7549
183.96	2843	7352
185.60	2962	7632
187.24	3039	7715
188.88	3120	7933
190.52	3250	7889
192.16	3026	7845
193.80	2962	7845
195.44	2962	7590
197.08	2854	7391
198.72	2610	7128
200.69	2404	6883
202.00	2229	6850
203.64	2187	6784
205.28	2154	6655
207.25	2154	6850
208.56	2317	7164
210.20	2639	7352
211.84	3177	7549
213.48	3638	7469
215.12	3765	7469
216.77	3638	7314
218.41	3433	7276
220.05	3250	7276
221.69	3170	7276
223.33	3093	7238
224.97	3026	7201
226.61	2913	7314
228.25	2938	7238
229.89	2860	7201
231.53	2732	7128
233.17	2615	7238
234.81	2591	7314
236.45	2553	7469
238.09	2340	7549
239.73	2059	7590
241.37	2208	7469
243.01	2317	7469
244.65	2180	7276
246.29	2041	7021
247.93	2147	6986
249.57	2208	6917
251.21	2333	6917
252.85	2336	7128
254.49	2336	7201
256.14	2388	7314

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
257.78	2438	7469
259.42	2429	7715
261.06	2464	7590
262.70	2464	7758
264.34	2499	7801
265.98	2507	7715
267.62	2516	7715
269.26	2535	7509
270.90	2581	7314
272.54	2630	7314
274.18	2659	7276
275.82	2753	7314
277.46	2889	7509
279.10	3120	7632
280.74	3206	7715
282.38	3359	7933
284.02	3459	7978
285.66	3564	8260
287.30	3816	8309
288.94	3901	8510
290.58	3858	8510
292.22	3765	8562
293.86	3638	8459

Table A-1. Boring Z1-B3, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

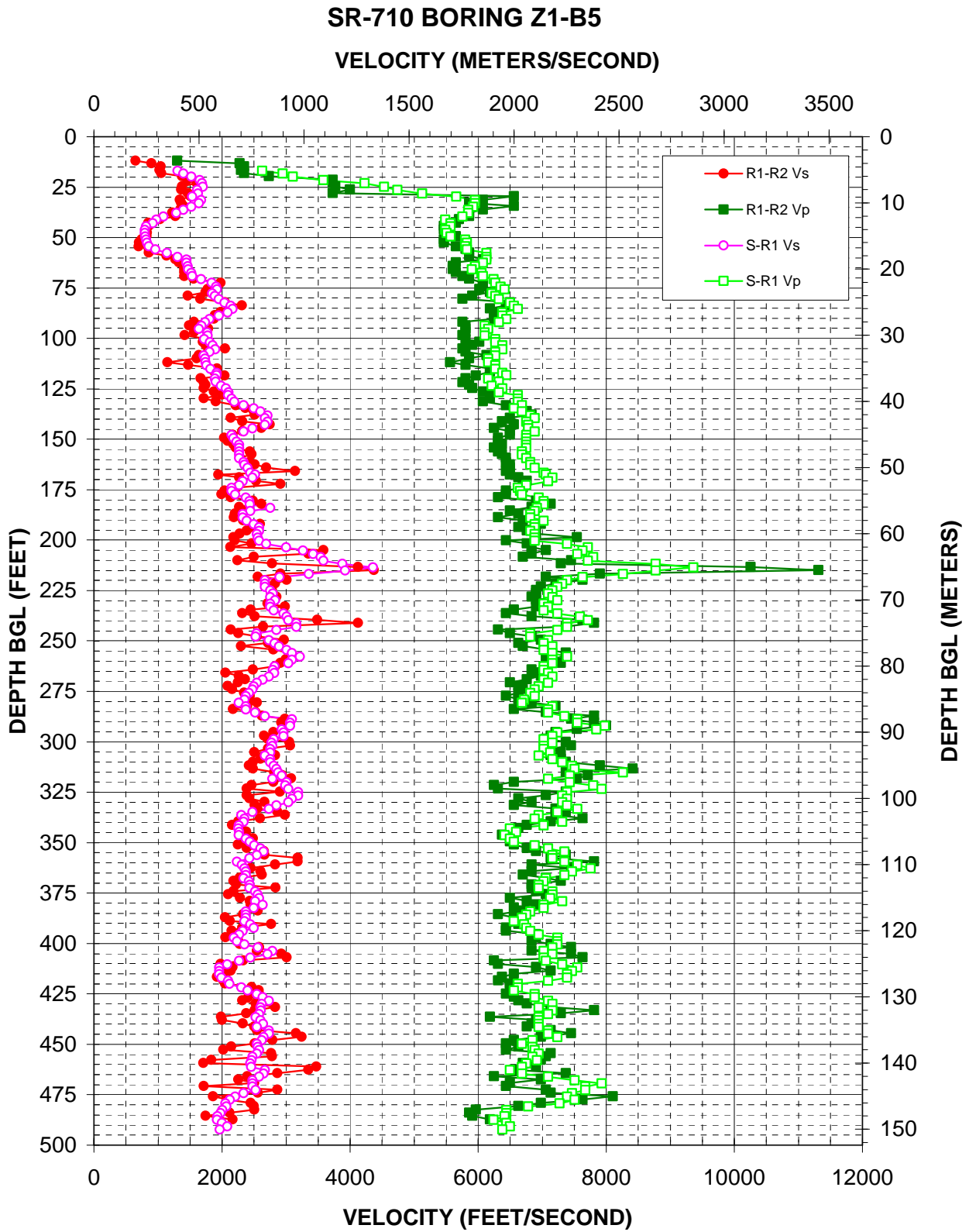


Figure A-2. Boring Z1-B5, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
16.96	1305	2630
18.27	1399	2950
19.91	1523	3107
21.56	1656	3582
23.20	1688	4230
24.84	1704	4530
26.48	1610	4744
28.12	1625	5125
29.76	1533	5662
31.40	1672	5950
33.04	1640	5950
34.68	1520	5925
36.32	1399	5851
37.96	1286	5851
39.60	1083	5755
41.24	975	5485
42.88	919	5572
44.52	818	5572
46.16	796	5485
47.80	796	5507
49.44	803	5572
51.08	818	5802
52.72	834	5827
54.36	858	5802
56.00	964	5827
57.64	1142	6132
59.61	1305	6132
60.93	1445	6132
62.57	1445	6079
64.21	1470	5950
65.85	1475	5900
67.49	1520	6053
69.13	1540	6079
70.77	1672	6241
72.41	1838	6269
74.38	1908	6354
75.69	1924	6412
77.66	1848	6213
78.97	1887	6269
80.61	1950	6325
82.25	2041	6501
83.89	2141	6562
85.53	2167	6624
87.17	2090	6383
88.81	1950	6383
90.45	1810	6441
92.09	1734	6325
93.73	1680	6105
95.37	1639	6159
97.01	1773	6105

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
98.65	1782	6105
100.30	1725	6269
101.94	1814	6269
103.58	1853	6383
105.54	1898	6383
106.86	1805	6269
108.50	1717	6269
110.14	1738	6159
111.78	1747	6159
113.42	1755	6269
115.06	1819	6269
117.03	1918	6383
118.34	1918	6441
119.98	1892	6159
121.62	1903	6325
123.59	1989	6213
124.90	2065	6383
126.87	2102	6325
128.18	2096	6624
129.82	2154	6624
131.46	2194	6624
133.10	2340	6687
134.74	2499	6562
136.38	2600	6687
138.35	2711	6817
139.67	2670	6883
141.31	2711	6751
142.95	2670	6784
144.59	2481	6784
146.23	2340	6883
147.87	2154	6751
149.51	2180	6751
151.15	2229	6751
152.79	2272	6751
154.43	2272	6751
156.07	2272	6687
157.71	2272	6687
159.35	2272	6751
161.32	2340	6817
162.63	2356	6817
164.27	2404	6883
166.57	2446	7021
167.55	2516	7056
169.19	2481	7164
170.83	2325	7092
172.80	2272	6751
174.11	2154	6624
175.75	2154	6655
177.40	2208	6687
179.04	2372	6951

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
180.68	2429	7021
182.32	2438	7021
183.96	2753	6917
185.60	2446	6883
187.24	2325	6817
188.88	2325	6817
190.52	2388	7021
192.16	2499	6883
193.80	2581	6883
195.44	2581	6817
197.08	2544	6883
198.72	2562	6883
200.36	2581	6883
202.00	2690	7391
203.64	3000	7715
205.28	3266	7632
206.92	3425	7549
208.56	3546	7801
210.20	3582	7715
211.84	3879	8776
213.48	4361	9361
215.12	3922	8776
216.77	3359	8260
218.41	2901	7632
220.05	2670	7391
221.69	2670	7314
223.33	2670	7238
224.97	2753	7164
226.61	2797	7092
228.25	2753	7164
229.89	2831	7238
231.53	2753	7021
233.17	2753	7092
234.81	2808	7021
236.45	2962	7238
238.09	3013	7590
239.73	3039	7715
241.37	3163	7391
243.01	3163	7391
244.65	2854	7238
246.29	2539	6817
247.93	2526	6817
249.57	2732	7092
251.21	2825	7021
252.85	2889	7164
254.49	3013	7021
256.14	3093	7164
257.78	3221	7391
259.42	3093	7164
261.06	3039	7164

Table A-2. Boring Z1-B5, S - R1 quality assurance analysis  
P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
262.70	2825	7021
264.34	2797	7021
265.98	2820	7092
267.62	2732	7164
269.26	2639	7021
270.90	2544	7092
272.54	2499	6951
274.18	2481	6883
275.82	2421	6817
277.46	2372	6883
279.10	2356	6719
280.74	2265	6687
282.38	2372	7164
284.02	2372	7092
285.66	2516	7092
287.30	2670	7352
288.94	3093	7549
290.58	3066	7549
292.22	3066	7978
293.86	2938	7845
295.51	2962	7238
297.15	2962	7164
298.79	2808	7021
300.43	2775	7164
302.07	2786	7021
303.71	2753	7021
305.35	2753	7128
306.99	2670	6951
308.63	2753	7164
310.27	2753	7314
311.91	2808	7469
313.55	2854	7509
315.19	2877	8260
316.83	2938	7430
318.47	2786	7092
320.11	3013	7430
321.75	2988	7801
323.39	3039	7933
325.03	3191	7391
326.67	3191	7314
328.31	3093	7391
329.95	3039	7314
331.59	2854	7391
333.23	2732	7549
334.88	2481	7238
336.52	2302	6951
338.16	2356	6883
339.80	2340	7314
341.44	2265	7021
343.08	2258	6501

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
344.72	2272	6592
346.36	2265	6412
348.00	2372	6501
349.64	2438	6562
351.28	2507	6883
352.92	2600	7092
354.56	2649	7352
356.20	2544	7164
357.84	2429	7164
359.48	2236	7352
361.12	2310	7549
362.76	2356	7758
364.40	2372	7469
366.04	2372	7352
367.68	2340	7056
369.32	2421	7021
370.96	2438	6951
372.60	2429	6951
374.25	2516	7164
375.89	2562	7164
377.53	2581	7128
379.17	2516	7314
380.81	2639	7021
382.45	2499	7021
384.09	2372	6817
385.73	2372	6751
387.37	2372	6687
389.01	2356	6562
390.65	2446	6719
392.29	2499	6751
393.93	2325	6817
395.57	2272	6951
397.21	2187	7238
398.85	2236	7238
400.49	2356	7238
402.13	2562	7164
403.77	2786	7021
405.41	2711	7164
407.05	2446	7021
408.69	2272	7056
410.33	2083	7314
411.98	1956	7549
413.62	1956	7469
415.26	1956	7391
416.90	1995	7391
418.54	2096	7092
420.18	2115	6624
421.82	2302	6624
423.46	2404	6562
425.10	2544	6883

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
426.74	2639	6883
428.38	2732	7092
430.02	2620	7164
431.66	2600	6951
433.30	2610	7164
434.94	2581	7092
436.58	2526	6951
438.22	2600	6951
439.86	2644	6951
441.50	2544	6951
443.14	2732	7092
444.78	2732	7092
446.42	2649	7238
448.06	2620	6850
449.70	2544	6687
451.35	2562	6850
452.99	2581	6883
454.63	2544	6951
456.27	2481	6850
457.91	2464	6917
459.55	2446	6751
461.19	2455	6687
462.83	2670	6501
464.47	2649	6687
466.11	2581	7092
467.75	2481	7509
469.39	2481	7933
471.03	2481	7673
472.67	2526	7673
474.31	2340	7469
475.95	2208	7391
477.59	2121	7509
479.23	2053	7276
480.87	2071	6784
482.51	2006	6441
484.15	1978	6441
485.79	1934	6412
487.43	1924	6241
489.07	2000	6441
490.72	2083	6501
492.36	1967	6383

Table A-2, continued. Boring Z1-B5, S - R1 quality assurance analysis  
P- and S<sub>H</sub>-wave data

# SR-710 BORING Z1-B6

## VELOCITY (METERS/SECOND)

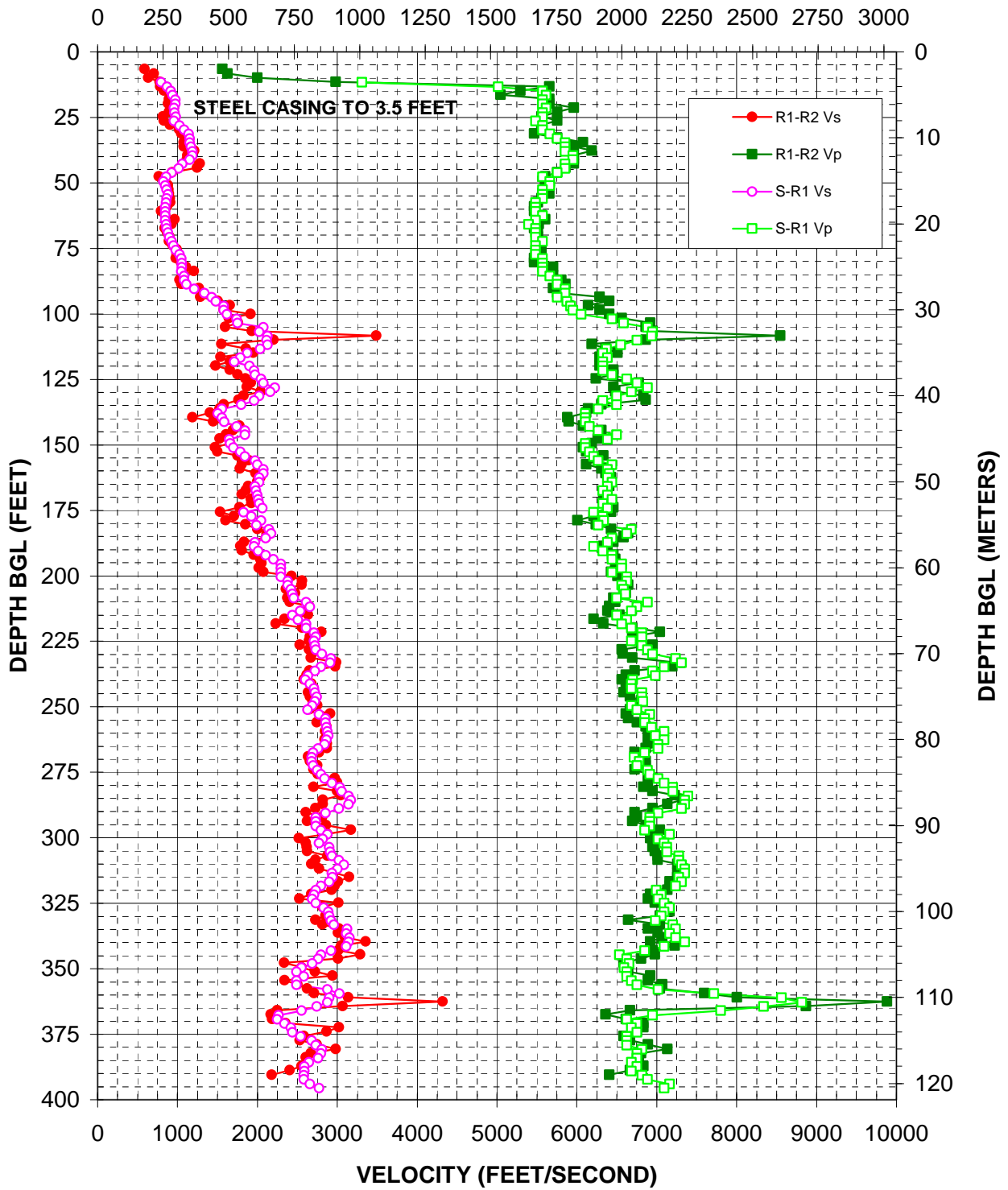


Figure A-3. Boring Z1-B6, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data



Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
11.71	798	3312	93.73	1433	5755	175.75	1828	6213
13.35	873	5015	95.37	1484	5875	177.40	1929	6325
14.99	919	5572	97.01	1578	5925	179.04	2047	6337
16.63	942	5617	98.65	1581	5950	180.68	1989	6269
18.27	974	5572	100.30	1618	6053	182.32	2147	6687
19.91	974	5572	101.94	1742	6441	183.96	2174	6624
21.56	957	5617	103.58	1751	6586	185.60	2102	6441
23.20	962	5572	105.22	2077	6883	187.24	1972	6383
24.84	978	5572	106.86	2023	6951	188.88	1961	6213
26.48	959	5485	108.50	2128	6938	190.52	2012	6325
28.12	1026	5572	110.14	2115	6751	192.16	2102	6441
29.76	1087	5572	111.78	2128	6549	193.80	2201	6441
31.40	1143	5662	113.42	2035	6371	195.44	2294	6562
33.04	1155	5755	115.06	1872	6325	197.08	2294	6562
34.68	1155	5851	116.70	1787	6383	198.72	2294	6441
36.32	1170	5851	118.34	1712	6325	200.36	2294	6624
37.96	1186	5851	119.98	1903	6325	202.00	2380	6624
39.60	1186	5950	121.62	1961	6325	203.64	2380	6562
41.24	1151	5950	123.26	1972	6441	205.28	2421	6586
42.88	1064	5851	124.90	2047	6624	206.92	2438	6611
44.52	1015	5851	126.54	2076	6751	208.56	2455	6501
46.16	931	5755	128.18	2218	6883	210.20	2610	6883
47.80	858	5572	129.82	2160	6687	211.84	2659	6751
49.44	826	5662	131.46	2023	6501	213.48	2535	6687
51.08	846	5662	133.10	1962	6325	215.12	2438	6501
52.72	865	5572	134.74	1800	6501	216.77	2507	6624
54.36	884	5572	136.38	1557	6269	218.41	2610	6562
56.00	863	5572	138.02	1503	6105	220.05	2610	6687
57.64	858	5485	139.67	1557	6105	221.69	2711	6817
59.28	848	5485	141.31	1585	6105	223.33	2732	6817
60.93	848	5485	142.95	1742	6159	224.97	2711	6687
62.57	848	5572	144.59	1848	6269	226.61	2721	6817
64.21	846	5485	146.23	1848	6501	228.25	2732	6883
65.85	860	5401	147.87	1652	6383	229.89	2808	6951
67.49	863	5485	149.51	1660	6105	231.53	2925	7238
69.13	882	5485	151.15	1704	6105	233.17	2913	7314
70.77	898	5485	152.79	1787	6159	234.81	2797	7092
72.41	926	5572	154.43	1848	6213	236.45	2721	6951
74.05	951	5485	156.07	1972	6269	238.09	2635	6986
75.69	981	5485	157.71	2000	6441	239.73	2600	6699
77.33	1026	5485	159.35	2077	6383	241.37	2659	6687
78.97	1048	5572	160.99	2077	6406	243.01	2711	6687
80.61	1057	5572	162.63	2023	6383	244.65	2721	6817
82.25	1057	5572	164.27	2023	6441	246.29	2743	6817
83.89	1051	5572	165.91	1974	6383	247.93	2721	6830
85.53	1087	5662	167.55	1987	6325	249.57	2690	6687
87.17	1087	5755	169.19	2000	6383	251.21	2630	6751
88.81	1114	5755	170.83	2012	6441	252.85	2775	6917
90.45	1212	5851	172.47	2023	6325	254.49	2854	6850
92.09	1340	5851	174.11	2065	6383	256.14	2854	6850

Table A-3. Boring Z1-B6, S - R1 quality assurance analysis  
P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
257.78	2866	6938	339.80	3141	7352
259.42	2877	7092	341.44	3114	7092
261.06	2889	6986	343.08	2925	6850
262.70	2866	7092	344.72	2797	6531
264.34	2843	7021	346.36	2764	6624
265.98	2764	7021	348.00	2690	6655
267.62	2700	6850	349.64	2553	6592
269.26	2680	6719	351.28	2490	6624
270.90	2680	6784	352.92	2581	6624
272.54	2700	6751	354.56	2491	6687
274.18	2753	6883	356.20	2490	6751
275.82	2797	6917	357.84	2877	7021
277.46	2843	7021	359.48	3026	7715
279.10	2938	7092	361.12	2899	8562
280.74	3033	7201	362.76	2877	8820
282.38	3059	7201	364.40	2743	8338
284.02	3143	7391	366.04	2555	7801
285.66	3171	7352	367.68	2265	6951
287.30	3141	7352	369.32	2250	6624
288.94	3020	7314	370.96	2340	6751
290.58	2854	7021	372.60	2421	6687
292.22	2732	6917	374.25	2438	6751
293.86	2732	6917	375.89	2544	6624
295.51	2732	6917	377.53	2680	6624
297.15	2797	6850	379.17	2732	6624
298.79	2877	7164	380.81	2808	6817
300.43	2820	7021	382.45	2797	6751
302.07	2775	7092	384.09	2764	6751
303.71	2901	7128	385.73	2649	6687
305.35	2913	7128	387.37	2591	6751
306.99	2938	7276	389.01	2591	6687
308.63	3020	7276	390.65	2581	6817
310.27	3086	7314	392.29	2581	6883
311.91	3007	7352	393.93	2659	7164
313.55	2938	7352	395.57	2775	7092
315.19	2944	7276			
316.83	2899	7314			
318.47	2797	7238			
320.11	2732	6993			
321.75	2711	7056			
323.39	2690	7021			
325.03	2732	7092			
326.67	2831	7164			
328.31	2889	7092			
329.95	2901	7056			
331.59	2925	6986			
333.23	2956	7201			
334.88	3127	7238			
336.52	3114	7164			
338.16	3156	7238			

Table A-3, continued. Boring Z1-B6, S - R1 quality assurance analysis  
P- and S<sub>H</sub>-wave data

# SR-710 BORING Z1-B7

## VELOCITY (METERS/SECOND)

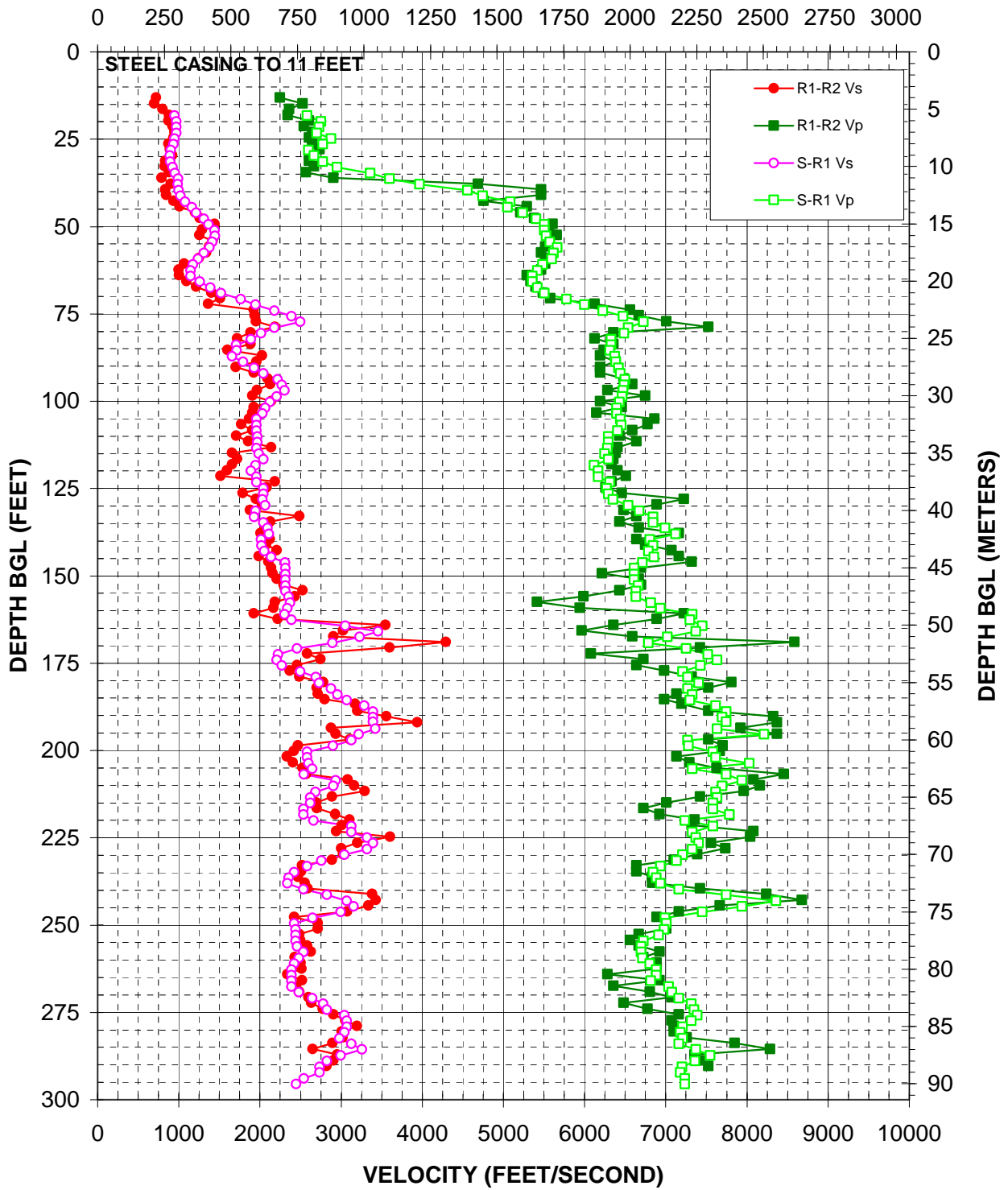


Figure A-4. Boring Z1-B7, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
18.27	945	2581	100.30	2121	6429	182.32	2877	7268
19.91	968	2753	101.94	2067	6394	183.96	2956	7329
21.56	968	2732	103.58	2029	6394	185.60	3073	7298
23.20	970	2700	105.22	1956	6441	187.24	3289	7615
24.84	948	2877	106.86	1956	6453	188.88	3392	7749
26.48	936	2775	108.50	1956	6406	190.52	3392	7698
28.12	904	2600	110.14	1967	6291	191.83	3392	7749
29.76	890	2670	111.78	1967	6291	193.80	3425	7632
31.40	894	2775	113.42	1956	6280	195.44	3221	8212
33.04	923	2950	115.06	1989	6246	197.08	3127	7268
34.68	955	3359	116.70	2041	6291	198.72	2901	7283
36.32	996	3601	118.34	1945	6116	200.36	2581	7582
37.96	985	3967	119.98	1887	6170	202.00	2581	7615
39.60	1002	4559	121.62	1956	6170	203.64	2600	8033
41.24	1022	4744	123.26	1956	6314	205.28	2644	7329
42.88	1078	5088	124.90	2041	6269	206.92	2544	7749
44.52	1164	5051	126.54	2041	6291	208.56	2932	7942
46.16	1217	5240	128.18	2029	6348	210.20	2904	7698
47.80	1312	5401	129.82	2065	6537	211.84	2685	7615
49.44	1366	5507	131.46	1945	6674	213.48	2620	7632
51.08	1442	5507	133.10	1929	6843	215.12	2620	7582
52.72	1448	5528	134.74	2041	6843	216.77	2538	7582
54.36	1416	5572	136.38	2096	6993	218.41	2539	7784
56.00	1379	5662	138.02	2108	7121	220.05	2665	7238
57.64	1312	5617	139.67	2014	6803	221.69	3127	7582
59.28	1236	5594	141.31	2020	6843	223.33	3127	7329
60.93	1174	5485	142.95	2053	6790	224.97	3320	7375
62.57	1149	5422	144.59	2138	6856	226.61	3392	7406
64.21	1149	5360	146.23	2310	6712	228.25	3320	7329
65.85	1261	5360	147.87	2317	6611	229.89	3039	7208
67.49	1390	5422	149.51	2317	6611	231.53	2759	7135
69.13	1523	5507	151.15	2317	6611	233.17	2583	6938
70.77	1764	5779	152.79	2317	6661	234.81	2421	6843
72.41	1945	6001	154.43	2317	6636	236.45	2356	6883
74.05	2180	6224	156.07	2356	6636	238.09	2339	6938
75.69	2388	6477	157.71	2372	6817	239.73	2535	7164
77.33	2499	6725	159.35	2340	6938	241.37	2825	7749
78.97	2180	6537	160.99	2302	7329	243.01	3073	8358
80.61	2018	6489	162.63	2388	7298	244.65	3156	7942
82.25	1887	6325	164.27	3053	7453	246.29	2994	7453
83.89	1708	6325	165.91	3455	7375	247.93	2649	6993
85.53	1717	6314	167.55	3228	7021	249.57	2425	7007
87.17	1656	6371	169.19	2895	6790	251.21	2442	6979
88.81	1791	6383	170.83	2455	7253	252.85	2442	6910
90.45	1929	6418	172.47	2225	7517	254.49	2443	6725
92.09	2041	6441	174.11	2208	7632	256.14	2459	6699
93.73	2222	6501	175.75	2272	7430	257.78	2539	6699
95.37	2272	6489	177.40	2499	7208	259.42	2481	6712
97.01	2302	6477	179.04	2690	7268	261.06	2425	6803
98.65	2208	6465	180.68	2732	7406	262.70	2388	6883

Table A-4. Boring Z1-B7, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

<b>Depth (feet)</b>	<b>V<sub>s</sub> (feet/sec)</b>	<b>V<sub>p</sub> (feet/sec)</b>
264.34	2388	6883
265.98	2388	6817
267.62	2388	7035
269.26	2481	7078
270.90	2644	7164
272.54	2781	7314
274.18	2825	7352
275.82	3039	7391
277.46	3073	7314
279.10	3073	7208
280.74	3039	7179
282.38	2981	7208
284.02	3127	7164
285.66	3258	7375
287.30	2994	7549
288.94	2825	7360
290.58	2737	7201
292.22	2737	7179
293.86	2544	7238
295.51	2446	7238

Table A-4, continued. Boring Z1-B7, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

# SR-710 BORING Z2-B1

## VELOCITY (METERS/SECOND)

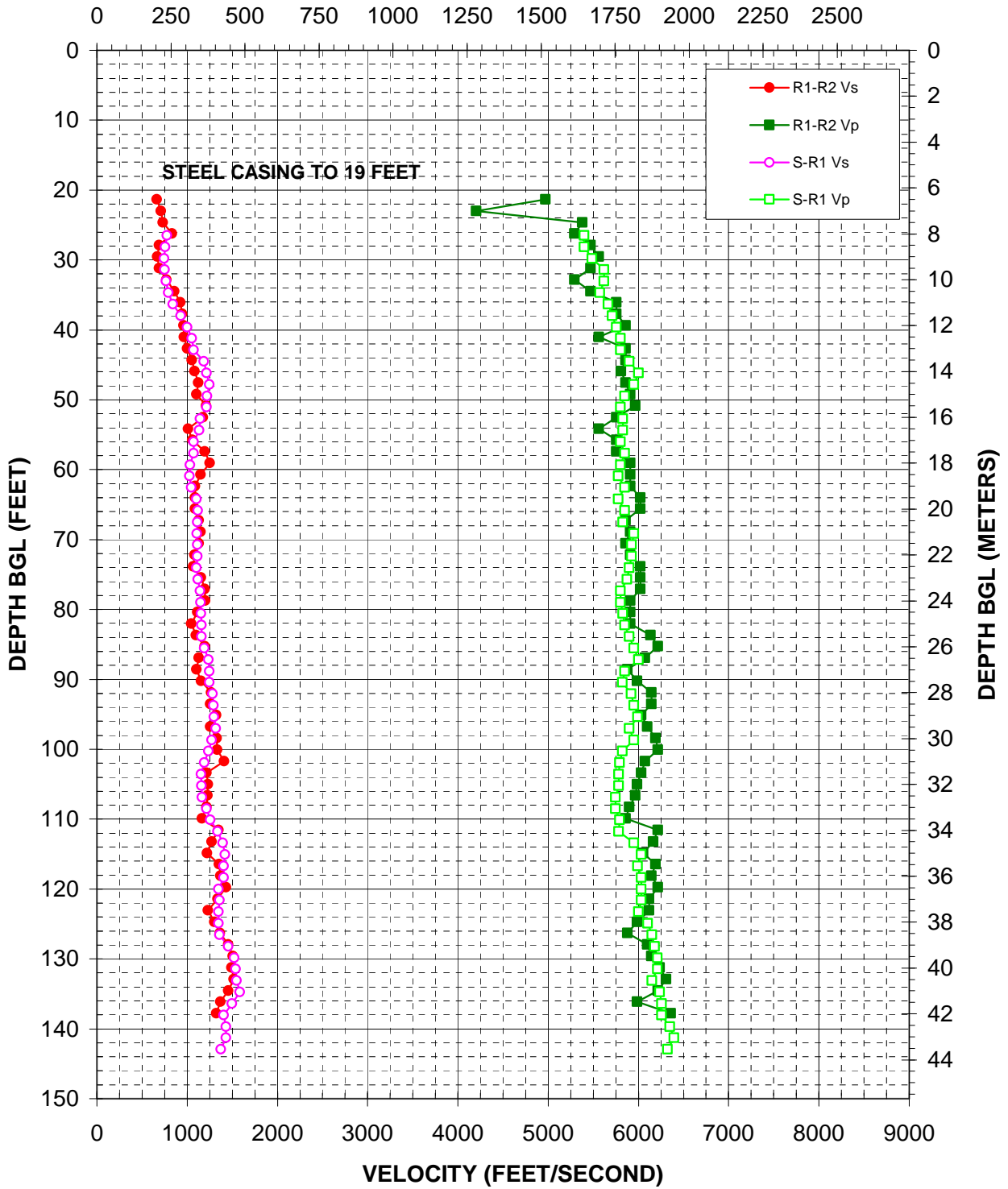


Figure A-5. Boring Z2-B1, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
26.48	774	5401	108.50	1217	5745
28.12	756	5401	110.14	1256	5793
29.76	746	5485	111.78	1337	5783
31.40	751	5617	113.42	1396	5950
33.04	767	5617	115.06	1418	6032
34.68	790	5572	116.70	1407	5991
36.32	843	5662	118.34	1407	6032
37.96	927	5708	119.98	1348	6032
39.60	1002	5755	121.62	1358	6032
41.24	1053	5802	123.26	1348	6001
42.88	1075	5802	124.90	1348	6105
44.52	1184	5900	126.54	1358	6148
46.16	1217	6001	128.18	1454	6180
47.80	1247	5950	129.82	1523	6213
49.44	1223	5851	131.46	1536	6213
51.08	1215	5802	133.10	1550	6148
52.72	1142	5827	134.74	1585	6235
54.36	1134	5827	136.38	1497	6258
56.00	1075	5802	138.02	1407	6258
57.64	1075	5851	139.67	1430	6348
59.28	1034	5802	141.31	1430	6394
60.93	1028	5779	142.95	1374	6325
62.57	1046	5851			
64.21	1102	5779			
65.85	1120	5851			
67.49	1113	5827			
69.13	1107	5950			
70.77	1113	5925			
72.41	1113	5925			
74.05	1102	5900			
75.69	1120	5875			
77.33	1142	5802			
78.97	1149	5802			
80.61	1157	5827			
82.25	1160	5851			
83.89	1160	5900			
85.53	1192	5950			
87.17	1238	6001			
88.81	1247	5851			
90.45	1247	5822			
92.09	1284	5920			
93.73	1293	5950			
95.37	1298	5991			
97.01	1317	5900			
98.65	1274	5950			
100.30	1238	5822			
101.94	1192	5793			
103.58	1157	5783			
105.22	1160	5783			
106.86	1162	5745			

Table A-5. Boring Z2-B1, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

# SR-710 BORING Z2-B4

VELOCITY (METERS/SECOND)

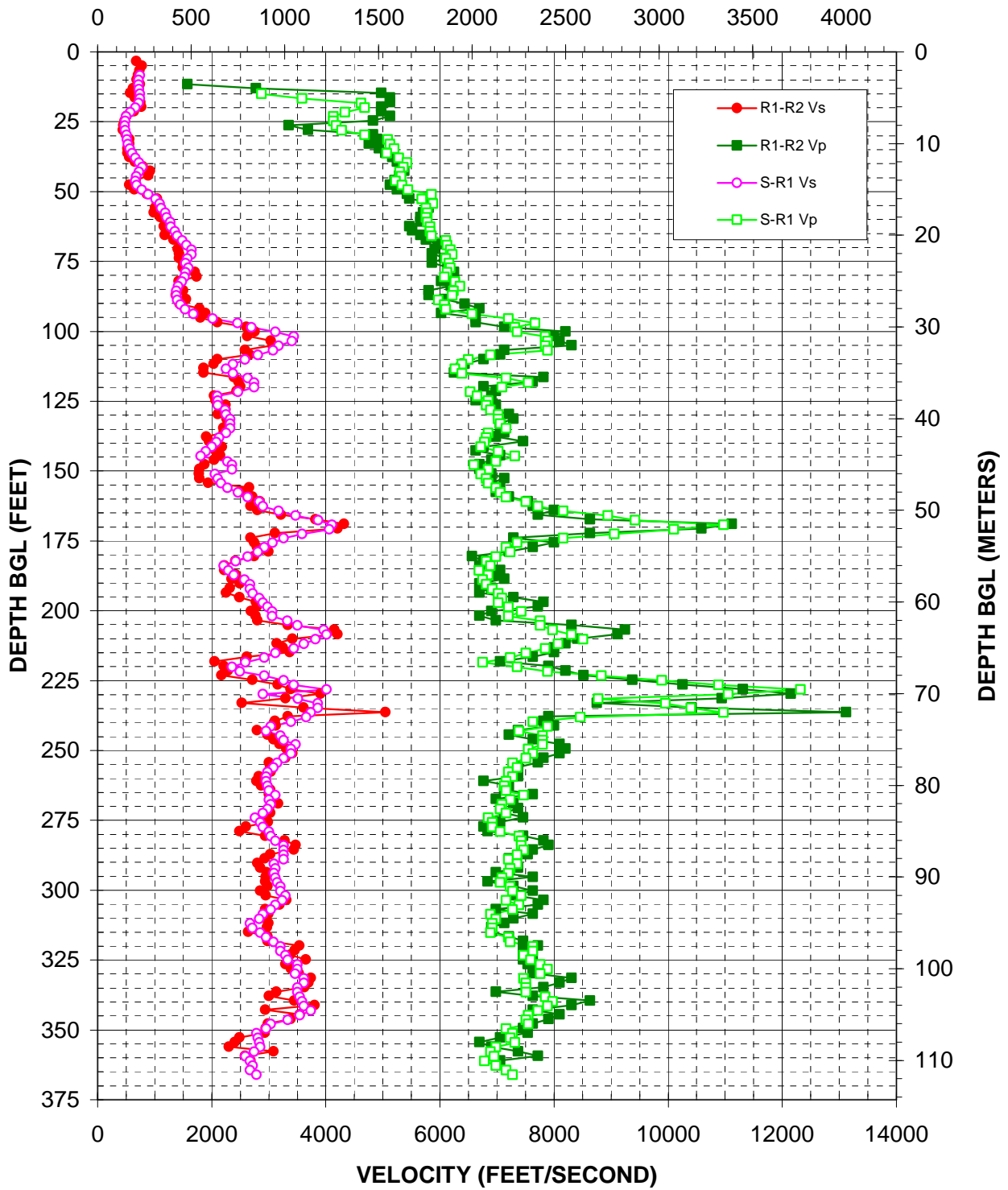


Figure A-6. Boring Z2-B4, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data



Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
8.43	742	
10.07	719	
11.71	721	
13.35	727	
14.99	742	2877
16.63	742	3582
18.27	719	4619
19.91	662	4681
21.56	573	4334
23.20	498	4130
24.84	482	4130
26.48	474	4179
28.12	484	4281
29.76	507	4681
31.40	516	5088
33.04	531	5125
34.68	568	5201
36.32	605	5069
37.96	659	5279
39.60	723	5422
41.24	784	5360
42.88	723	5299
44.52	681	5319
46.16	659	5220
47.80	686	5339
49.44	772	5443
51.08	889	5851
52.72	1020	5685
54.36	1094	5875
56.00	1114	5755
57.64	1186	5779
59.28	1215	5755
60.93	1272	5779
62.57	1281	5827
64.21	1355	5827
65.85	1399	5851
67.49	1487	6105
69.13	1560	6132
70.77	1648	6186
72.41	1648	6213
74.05	1574	6105
75.69	1540	6159
77.33	1588	6186
78.97	1540	6132
80.61	1526	6079
82.25	1475	6269
83.89	1410	6354
85.53	1382	6241
87.17	1377	6213
88.81	1399	5975

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
90.45	1457	6079
92.09	1535	6105
93.73	1680	6562
95.37	2018	7201
97.01	2455	7673
98.65	2700	7314
100.30	3120	7352
101.94	3442	7845
103.58	3408	7889
105.22	3177	7845
106.86	3079	7889
108.50	2808	6883
110.14	2581	6501
111.78	2372	6383
113.42	2250	6269
115.06	2372	6383
116.70	2635	7164
118.34	2743	7549
119.98	2743	7092
121.62	2464	6531
123.26	2096	6655
124.90	2108	6850
126.54	2108	6817
128.18	2236	6883
129.82	2250	7021
131.46	2325	7021
133.10	2325	7056
134.74	2325	7164
136.38	2250	6850
138.02	2134	6817
139.67	2083	6784
141.31	2006	6719
142.95	1898	7021
144.59	1805	7314
146.56	2280	6986
147.87	2356	6592
149.51	2356	6850
151.15	2059	6719
152.79	2108	6817
154.43	2160	6850
156.07	2280	6986
157.71	2464	7056
159.35	2630	7164
160.99	2831	7509
162.63	2901	7715
164.27	3177	8164
165.91	3476	8944
167.55	3868	9424
169.19	4106	10970
170.83	4058	10102

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
172.47	3582	9059
174.11	3266	8164
175.75	3066	7352
177.40	2925	7164
179.04	2808	7238
180.68	2630	6986
182.32	2421	6817
183.96	2215	6883
185.60	2294	6687
187.24	2388	6850
188.88	2572	6751
190.52	2670	6817
192.16	2670	6917
193.80	2721	7021
195.44	2831	7092
197.08	2901	7021
198.72	2981	7201
200.36	3059	7430
202.00	3059	7201
203.64	3327	7758
205.28	3502	7758
206.92	3967	7978
208.56	4012	8309
210.20	3816	8510
211.84	3619	8070
213.48	3442	7845
215.12	3120	7509
216.77	2925	7238
218.41	2591	6751
220.05	2356	7352
221.69	2499	7889
223.33	2925	8831
224.97	3266	9889
226.61	3442	10885
228.25	4012	12318
229.89	2901	11057
231.53	3510	8776
233.17	3858	9959
234.81	3858	10401
236.45	3735	10970
238.09	3657	8459
239.73	3392	7632
241.37	3039	7889
243.01	2956	7391
244.65	3206	7801
246.29	3266	7801
247.93	3476	7801
249.57	3392	7549
251.21	3392	7632
252.85	3266	7509

NOTE: "blank" space indicates data of insufficient quality for good pick.

Table A-6. Boring Z2-B4, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
254.49	3148	7276	336.52	3502	7509
256.14	3086	7352	338.16	3546	7845
257.78	2981	7201	339.80	3582	7978
259.42	2956	7276	341.44	3619	7889
261.06	2956	7164	343.08	3735	7715
262.70	2981	7128	344.72	3546	7549
264.34	3007	7164	346.36	3335	7509
265.98	3120	7469	348.00	3033	7549
267.62	3007	7238	349.64	2956	7164
269.26	3033	7092	351.28	2786	7276
270.90	2981	7056	352.92	2808	7238
272.54	2901	7164	354.56	2831	7314
274.18	2759	6850	356.20	2854	6986
275.82	2854	6917	357.84	2743	6883
277.46	2901	6917	359.48	2591	6951
279.10	3007	7056	361.12	2670	6784
280.74	3033	7391	362.76	2721	6986
282.38	3120	7430	364.40	2670	7164
284.02	3266	7430	366.04	2786	7276
285.66	3266	7469			
287.30	3266	7352			
288.94	3266	7201			
290.58	3093	7352			
292.22	3120	7238			
293.86	3093	7201			
295.51	3120	7092			
297.15	3148	7056			
298.79	3206	7238			
300.43	3206	7276			
302.07	3296	7430			
303.71	3235	7164			
305.35	3120	7391			
306.99	3033	7276			
308.63	2901	6883			
310.27	2831	6986			
311.91	2675	6917			
313.55	2716	6917			
315.19	2854	6883			
316.83	2956	7201			
318.47	3086	7238			
320.11	3206	7632			
321.75	3206	7632			
323.39	3296	7469			
325.03	3335	7590			
326.67	3502	7758			
328.31	3502	7889			
329.95	3467	7758			
331.59	3619	7469			
333.23	3619	7509			
334.88	3502	7509			

Table A-6, continued. Boring Z2-B4, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

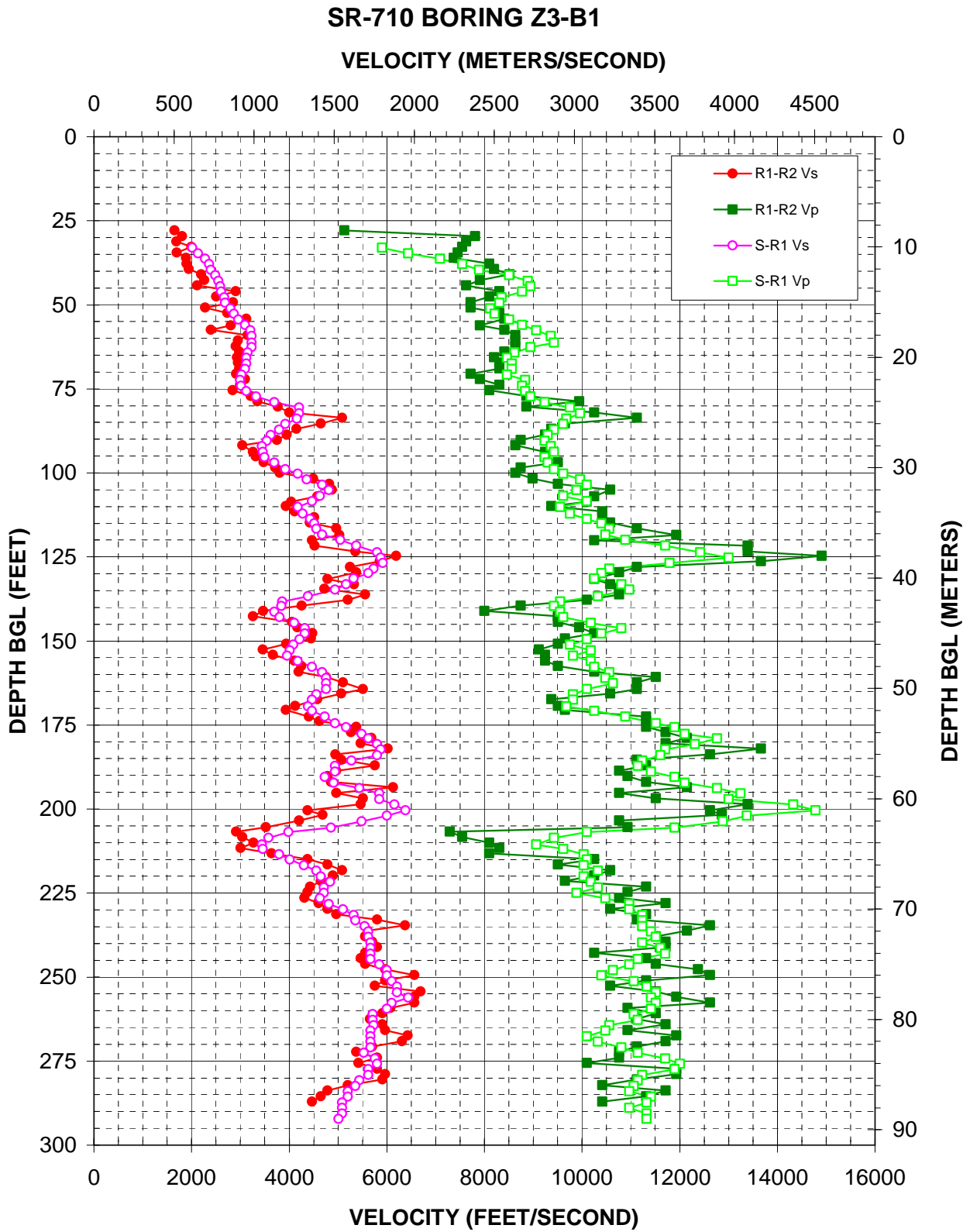


Figure A-7. Boring Z3-B1, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
33.04	2012	5900	115.06	4515	10401	197.08	5851	13002
34.68	2134	6441	116.70	4559	10558	198.72	6159	14329
36.32	2276	7092	118.34	4681	10479	200.36	6383	14781
37.96	2364	7549	119.98	5051	10885	202.00	6001	13373
39.60	2396	7889	121.62	5380	11702	203.64	5485	12883
41.24	2485	8510	123.59	5802	12427	205.61	4859	11900
42.88	2553	8887	125.23	5875	13002	206.92	3989	10102
44.52	2591	8944	126.87	5925	11800	208.56	3582	9424
46.16	2610	8776	128.51	5731	10558	210.53	3442	9059
47.80	2670	8358	129.82	5617	10401	211.84	3459	9618
49.44	2690	8309	131.46	5319	10250	213.48	3795	10030
51.08	2797	8117	133.10	5162	10802	215.12	4012	10102
52.72	2866	8212	134.74	4944	10970	216.77	4307	10030
54.36	2962	8510	136.71	4388	10325	218.41	4559	10325
56.00	3093	8776	138.35	3858	9552	220.05	4650	10030
57.64	3206	9059	139.67	3837	9424	221.69	4842	10175
59.28	3235	9361	141.31	3695	9552	223.33	4712	10325
61.25	3235	9424	142.95	3805	9618	224.97	4712	9889
62.57	3235	8944	144.59	4106	10175	226.61	4634	10479
64.21	3148	8615	146.23	4321	10802	228.25	4809	10970
65.85	3120	8459	147.87	4321	10401	229.89	5106	10970
67.49	3120	8562	149.51	4217	10102	231.53	5319	11234
69.13	3093	8562	151.15	4082	9751	233.17	5360	11234
70.77	3026	8459	152.79	4012	10175	234.81	5550	11234
72.41	3000	8831	154.43	3955	9820	236.45	5617	11416
74.05	3013	8776	156.07	4179	10175	238.09	5617	11510
75.69	3120	8831	157.71	4472	10250	239.73	5662	11234
77.33	3327	8944	159.35	4681	10558	241.37	5662	11605
78.97	3695	9238	160.99	4760	10479	243.01	5662	11702
80.61	4204	9751	162.63	4760	10638	244.65	5662	11144
82.25	4204	9959	164.27	4760	10102	246.29	5851	10970
83.89	4154	9684	165.91	4559	9820	247.93	6001	10638
85.53	3922	9618	167.55	4472	9820	249.57	6001	10401
87.17	3795	9424	169.52	4388	9684	251.21	6105	11057
88.81	3619	9299	170.83	4472	10250	252.85	6213	11324
90.45	3546	9238	172.47	4728	10885	254.49	6213	11510
92.09	3442	9361	174.44	4944	11510	256.14	6441	11416
93.73	3459	9424	175.75	5162	11900	257.78	6105	11510
95.37	3493	9238	177.72	5485	12105	259.42	6001	11416
97.01	3695	9299	179.04	5617	12765	261.06	5708	11057
98.98	3922	9424	180.68	5802	12318	262.70	5708	11144
100.30	4179	9618	182.32	5875	11702	264.34	5731	10558
101.94	4361	9959	183.96	5802	11605	265.98	5662	10479
103.58	4681	10102	185.60	5279	11234	267.62	5662	10102
105.22	4809	9889	187.24	4944	11144	269.26	5662	10325
106.86	4634	9618	188.88	4944	11416	270.90	5662	10802
108.50	4472	10102	190.52	4728	11900	272.54	5528	11144
110.14	4179	9552	192.16	4910	12105	274.18	5755	11702
112.11	4281	9751	193.80	5443	12765	275.82	5802	12002
113.75	4430	10102	195.44	5851	13247	277.46	5617	11900

Table A-7. Boring Z3-B1, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

<b>Depth (feet)</b>	<b>V<sub>s</sub> (feet/sec)</b>	<b>V<sub>p</sub> (feet/sec)</b>
279.10	5617	11234
280.74	5443	11144
282.38	5360	11057
284.02	5201	10970
285.66	5201	11416
287.30	5088	11324
288.94	5088	10970
290.58	5088	11324
292.22	5015	11324

Table A-7, continued. Boring Z3-B1, S - R1 quality assurance analysis  
P- and S<sub>H</sub>-wave data

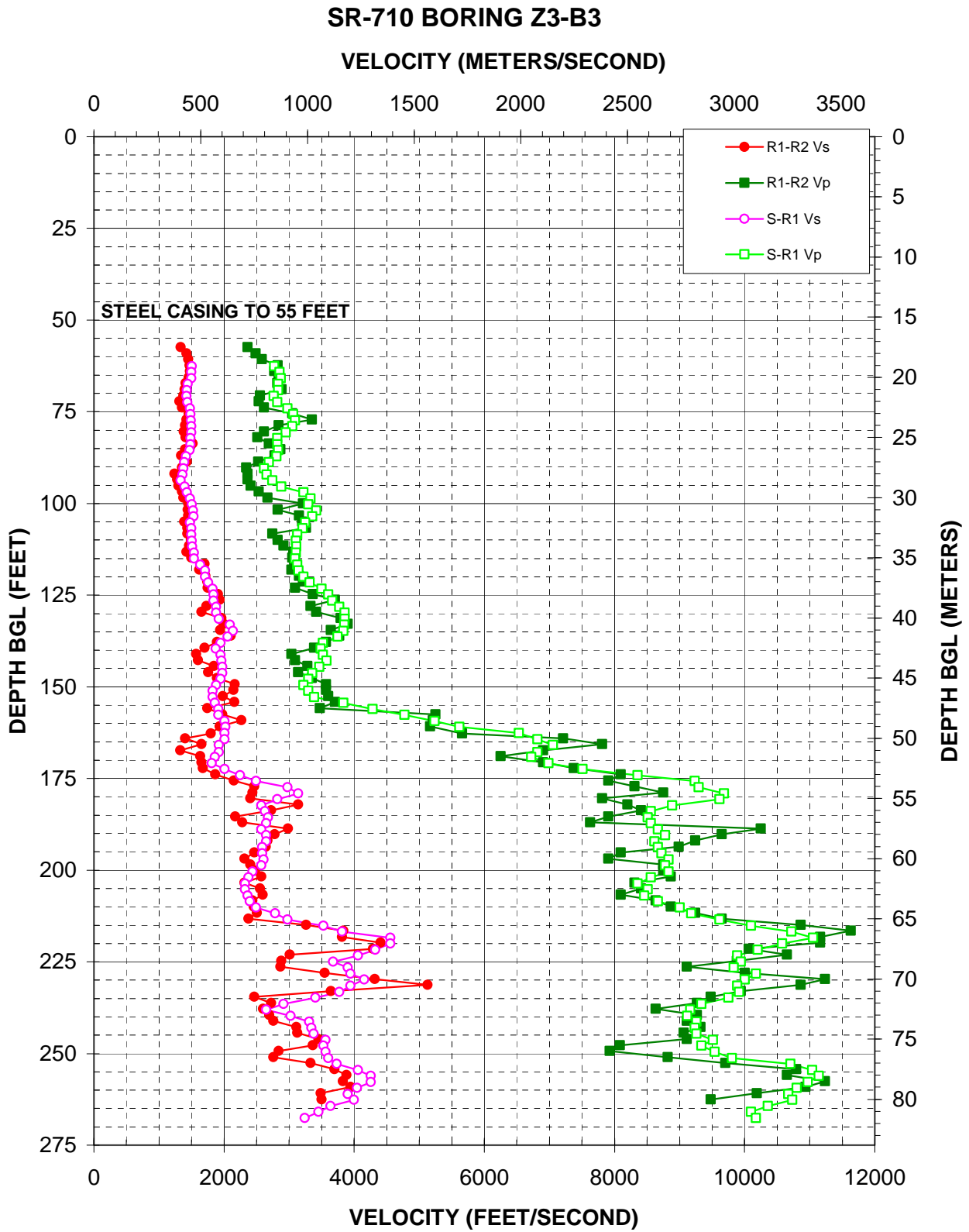


Figure A-8. Boring Z3-B3, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
62.57	1503	2775
64.21	1497	2854
65.85	1497	2872
67.49	1445	2831
69.13	1430	2831
70.77	1424	2764
72.41	1437	2820
74.05	1478	2975
75.69	1484	3066
77.33	1491	3093
78.97	1497	3053
80.61	1497	2950
82.25	1484	2820
83.89	1484	2820
85.53	1469	2831
87.17	1418	2803
88.81	1388	2690
90.45	1377	2615
92.09	1363	2654
93.73	1337	2743
95.37	1399	2877
97.01	1430	3221
98.65	1478	3327
100.30	1503	3296
101.94	1526	3417
103.58	1533	3359
105.22	1478	3250
106.86	1497	3206
108.50	1497	3127
110.14	1505	3107
111.78	1510	3114
113.42	1540	3107
115.06	1540	3093
116.70	1633	3127
118.34	1712	3148
119.98	1712	3221
121.62	1760	3320
123.26	1828	3502
124.90	1838	3601
126.54	1838	3666
128.18	1882	3775
129.82	1882	3858
131.46	1924	3858
133.10	2090	3847
134.74	2141	3837
136.38	2059	3745
138.02	1950	3519
139.67	1872	3484
141.31	1950	3519
142.95	1961	3573

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
144.59	1972	3467
146.23	1972	3359
147.87	1950	3296
149.51	1882	3221
151.15	1828	3296
152.79	1828	3384
154.43	1857	3837
156.07	1913	4281
157.71	1913	4776
159.35	2012	5240
160.99	2023	5617
162.63	2012	6531
164.27	2012	6817
165.91	1924	7056
167.88	1924	6817
169.19	1857	6719
170.83	1810	6986
172.47	2012	7509
174.11	2250	8358
175.75	2490	9238
177.40	2975	9299
179.04	3141	9684
180.68	2820	9618
182.32	2572	8887
183.96	2630	8562
185.60	2675	8510
187.24	2649	8562
188.88	2572	8668
190.52	2649	8776
192.16	2649	8615
193.80	2591	8668
195.44	2591	8722
197.08	2610	8831
198.72	2572	8776
200.36	2438	8831
202.00	2380	8562
203.64	2325	8358
205.28	2325	8510
206.92	2364	8459
208.56	2396	8668
210.20	2490	9001
211.84	2786	9178
213.48	2975	9618
215.12	3528	10102
216.77	3816	10719
218.41	4559	11057
220.05	4559	10574
221.69	4323	10205
223.33	4058	9889
224.97	3676	9945

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
226.61	3901	9833
228.25	3944	10175
229.89	4154	10001
231.53	3944	9889
233.17	3775	9917
234.81	3408	9751
236.45	2913	9336
238.09	2649	9166
239.73	3026	9118
241.37	3312	9263
243.01	3343	9238
244.65	3375	9263
246.29	3564	9514
247.93	3528	9336
249.57	3564	9539
251.21	3601	9806
252.85	3735	10703
254.49	4058	11039
256.14	4255	11144
257.78	4255	10970
259.42	4047	10802
261.06	3901	10670
262.70	4001	10735
264.34	3638	10355
265.98	3450	10102
267.62	3243	10175

Table A-8. Boring Z3-B3, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

# SR-710 BORING Z3-B4

VELOCITY (METERS/SECOND)

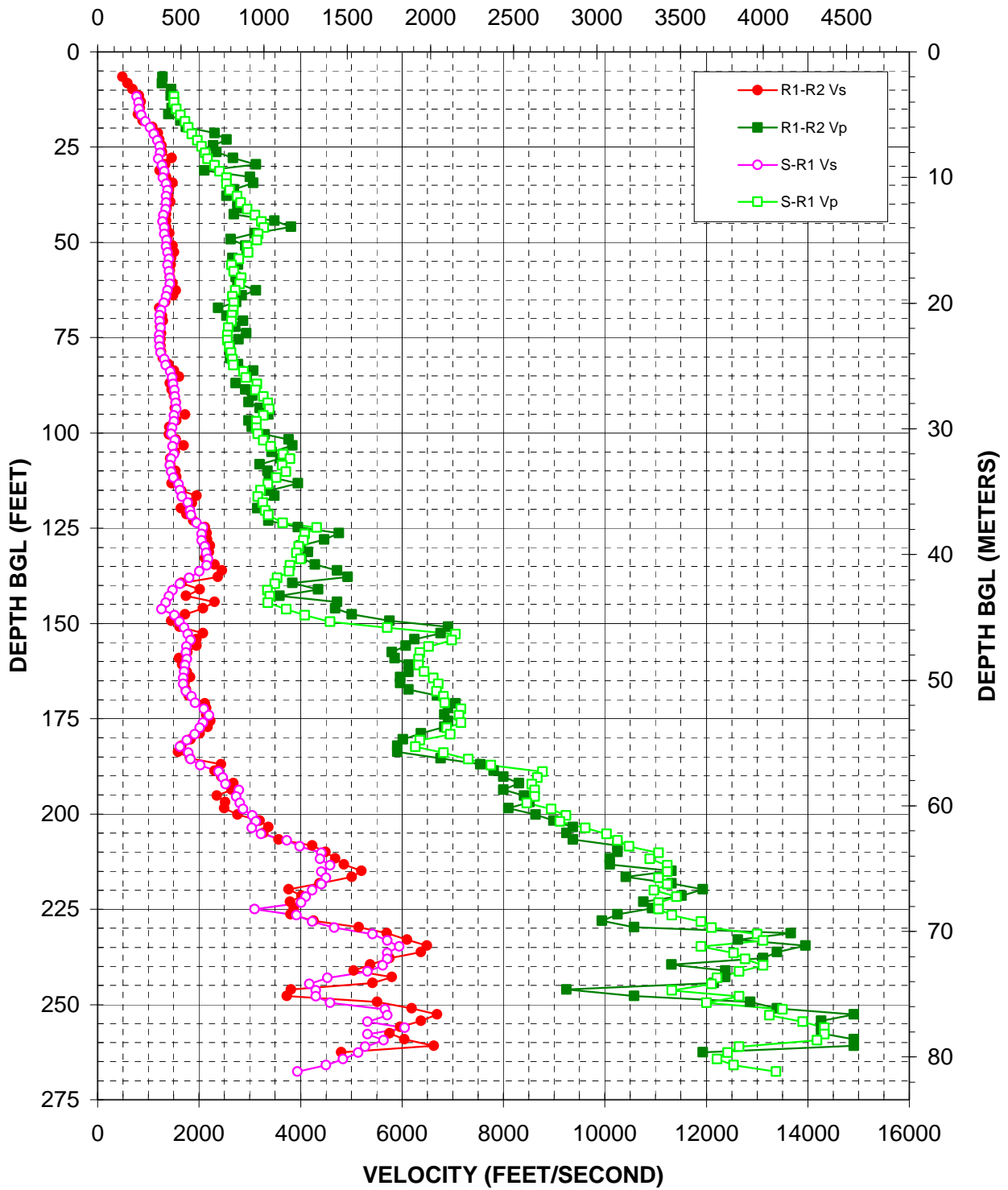


Figure A-9. Boring Z3-B4, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data



Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
11.71	767	1510	93.73	1553	3384	176.08	2077	7164
13.35	807	1510	95.37	1507	3273	177.40	2012	6883
14.99	815	1550	97.01	1507	3134	179.04	1918	6951
16.63	858	1633	98.65	1469	3134	180.68	1764	6354
18.27	941	1721	100.30	1451	3163	182.32	1621	6269
19.91	1034	1791	101.94	1526	3273	183.96	1791	6817
21.56	1111	1862	103.58	1481	3417	185.60	1833	7314
23.20	1182	1972	105.54	1507	3657	187.24	2023	7758
24.84	1227	2053	106.86	1457	3795	188.88	2388	8776
26.48	1236	2128	108.50	1427	3638	190.52	2472	8668
28.12	1198	2174	110.14	1451	3715	192.16	2526	8562
29.76	1272	2302	111.78	1500	3519	193.80	2786	8615
31.40	1315	2404	113.42	1596	3359	195.44	2732	8615
33.04	1286	2544	115.06	1625	3213	197.08	2808	8459
34.68	1350	2544	116.70	1664	3163	198.72	2866	8944
36.32	1382	2610	118.34	1782	3258	200.36	3053	9238
37.96	1355	2753	120.31	1828	3304	202.00	3120	9118
39.60	1355	2820	121.62	1848	3367	203.64	3039	9618
41.24	1340	2950	123.59	1950	3647	205.28	3221	10030
42.88	1295	3107	124.90	2077	4321	206.92	3735	10250
44.52	1281	3235	126.54	2053	4082	208.56	3989	10479
46.16	1315	3281	128.18	2053	4058	210.20	4416	11057
47.80	1315	3170	129.82	2115	3967	211.84	4388	10885
49.44	1361	3141	131.46	2141	3922	213.48	4589	11234
51.08	1355	2950	133.10	2180	4001	215.12	4416	11234
52.72	1377	2969	134.74	2154	3795	216.77	4501	11057
54.36	1410	2786	136.38	2006	3775	218.41	4416	11234
56.00	1377	2644	138.02	1810	3546	220.05	4230	10970
57.64	1410	2690	139.67	1625	3493	221.69	4106	11416
59.28	1427	2837	141.31	1478	3351	223.33	4012	11057
60.93	1427	2803	142.95	1404	3400	224.97	3093	11057
62.57	1377	2711	144.59	1348	3359	226.61	3922	11324
64.21	1350	2659	146.23	1258	3725	228.25	4230	11900
65.85	1305	2690	147.87	1513	4082	229.89	4665	12105
67.81	1254	2680	149.51	1618	4589	231.53	5422	13002
69.13	1227	2654	151.15	1704	5708	233.17	5708	13123
70.77	1227	2639	152.79	1782	7056	234.81	5950	11900
72.41	1240	2581	154.43	1838	6986	236.45	5708	12537
74.38	1219	2562	156.07	1755	6531	238.09	5708	12765
75.69	1219	2562	157.71	1747	6354	239.73	5617	13123
77.33	1227	2600	159.35	1760	6325	241.37	5319	12650
78.97	1245	2630	160.99	1721	6325	243.01	4530	12210
80.61	1315	2659	162.63	1708	6441	244.65	4179	12105
82.25	1345	2675	164.27	1688	6624	246.29	4307	11324
83.89	1433	2877	165.91	1692	6719	247.93	4307	12650
85.53	1469	2925	167.88	1747	6687	249.57	4589	12002
87.17	1487	3141	169.19	1853	6817	251.21	5662	13502
88.81	1513	3114	170.83	1924	6850	252.85	5708	13247
90.45	1526	3273	172.47	2102	7164	254.49	5319	13903
92.09	1540	3359	174.11	2194	7128	256.14	6053	14329

Table A-9. Boring Z3-B4, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

<b>Depth (feet)</b>	<b>V<sub>s</sub> (feet/sec)</b>	<b>V<sub>p</sub> (feet/sec)</b>
257.78	5319	14329
259.42	5639	14184
261.06	5279	12650
262.70	5144	12427
264.34	4842	12210
265.98	4501	12537
267.62	3944	13373

Table A-9, continued. Boring Z3-B4, S - R1 quality assurance analysis  
P- and S<sub>H</sub>-wave data

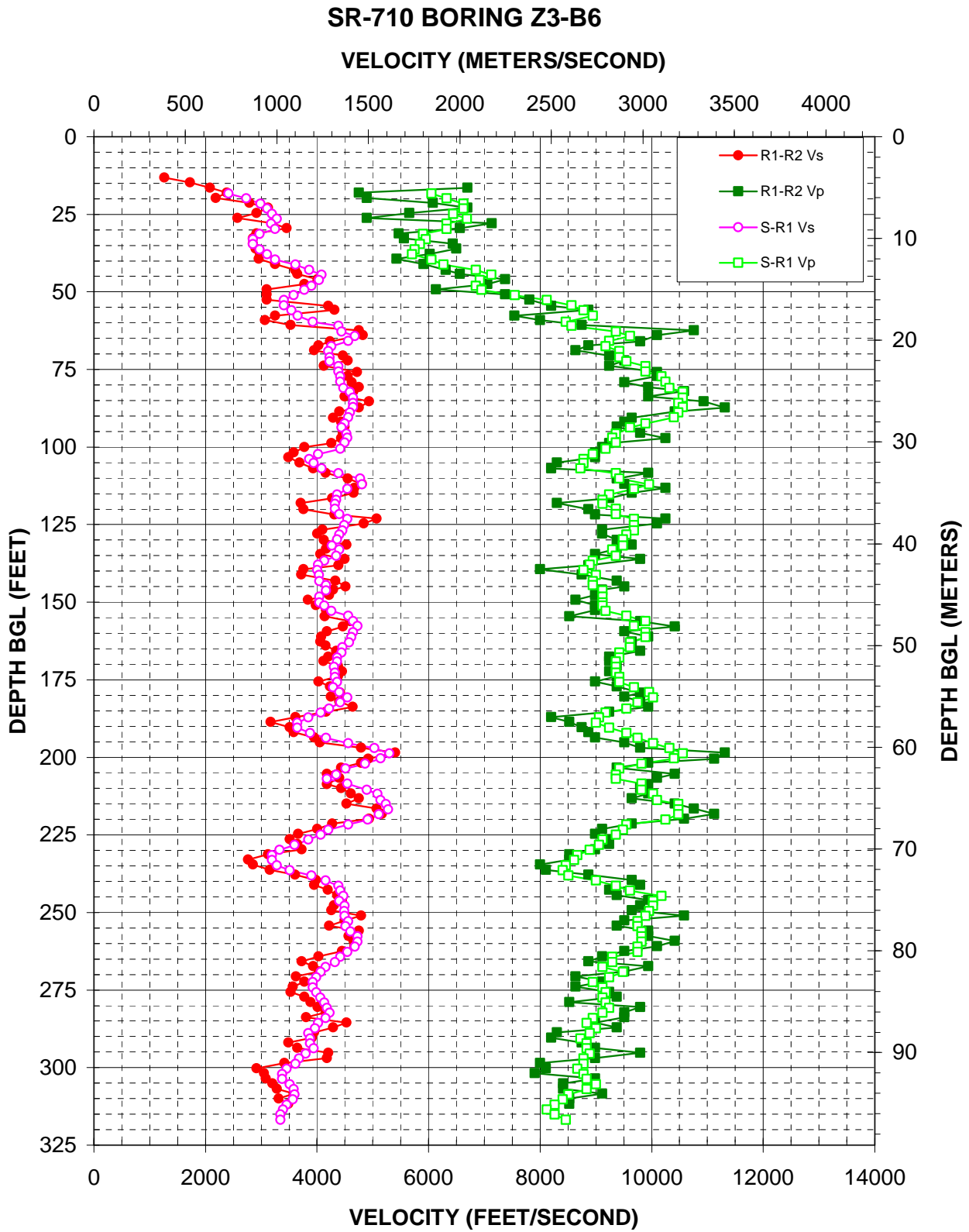


Figure A-10. Boring Z3-B6, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
18.27	2413	6053	100.62	4416	9178	182.32	4416	9751
19.91	2732	6325	102.26	4023	8944	184.28	4217	9552
21.56	2988	6624	103.90	3858	8776	185.60	4070	9178
23.20	3107	6624	105.22	3944	8776	187.24	3847	9059
24.84	3191	6441	106.86	4082	8722	188.88	3647	9001
26.48	3281	6687	108.50	4388	9361	190.52	3647	9238
28.12	3177	6325	110.14	4776	9424	192.16	3879	9552
29.76	3250	6325	112.11	4809	9959	193.80	4167	9751
31.40	2975	5900	113.42	4544	9684	195.44	4559	10030
33.04	2854	5950	115.39	4361	9238	197.08	5033	10325
34.68	2854	5851	117.03	4347	9118	198.72	5299	10558
36.32	2975	5755	118.34	4321	9118	200.36	5144	10401
37.96	3107	5708	119.98	4321	9361	202.00	4859	9820
39.60	3250	6053	121.62	4402	9361	203.64	4515	9424
41.24	3619	6269	123.26	4544	9684	205.61	4347	9361
42.88	3858	6850	125.23	4486	9684	206.92	4179	9361
44.52	4082	7128	126.87	4458	9684	208.56	4544	9820
46.16	4035	6917	128.18	4402	9552	210.53	4893	9820
48.13	3901	6850	129.82	4361	9488	211.84	5088	10030
49.44	3775	6951	131.79	4268	9488	213.81	5144	10102
51.08	3582	7549	133.10	4402	9299	215.12	5240	10479
52.72	3408	8117	135.07	4347	9361	216.77	5279	10479
54.36	3408	8562	136.71	4130	8944	218.41	5106	10479
56.00	3546	8776	138.02	4023	8887	220.05	4910	10250
57.64	3657	8944	139.67	4001	8776	221.69	4559	9552
59.61	3922	8459	141.31	4035	9001	223.33	4204	9488
60.93	4388	8562	143.27	4047	8944	224.97	4070	9361
62.89	4444	9361	144.59	4167	8944	226.61	3847	9118
64.21	4681	9618	146.23	4167	9118	228.25	3601	9059
65.85	4559	9238	148.20	4047	9118	229.89	3327	8887
67.49	4255	9178	150.16	4047	9118	231.53	3191	8668
69.13	4204	9424	151.15	4130	9118	233.17	3191	8615
71.10	4230	9424	152.79	4255	9178	234.81	3281	8459
72.41	4230	9552	154.43	4559	9552	236.45	3510	8408
74.05	4388	9889	156.07	4650	9889	238.09	3901	8510
75.69	4388	9889	157.71	4728	9684	239.73	4154	9001
77.33	4416	10175	159.68	4650	9889	241.37	4388	9361
78.97	4416	10250	161.32	4619	9889	243.01	4416	9618
80.94	4472	10325	162.96	4574	9618	244.65	4472	10175
82.25	4589	10558	164.60	4458	9618	246.29	4402	10030
84.22	4650	10558	166.24	4444	9424	247.93	4501	10030
85.86	4650	10479	167.88	4361	9424	249.57	4486	9959
87.17	4650	10558	169.19	4361	9361	251.21	4501	9889
88.81	4589	10479	170.83	4307	9361	252.85	4559	9751
90.45	4559	10401	172.80	4321	9361	254.49	4515	9751
92.42	4501	9889	174.11	4321	9424	256.14	4604	9820
93.73	4444	9618	175.75	4361	9424	257.78	4728	9820
95.70	4530	9361	177.40	4294	9684	259.42	4728	9820
97.01	4544	9299	179.04	4402	9959	261.06	4681	9751
98.65	4501	9361	180.68	4544	10030	262.70	4544	9751

Table A-10. Boring Z3-B6, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
264.34	4416	9299
265.98	4321	9299
267.62	4154	9118
269.26	4070	9488
270.90	3989	9238
272.54	3922	8944
274.18	3922	9118
275.82	3989	9178
277.46	4058	9118
279.10	4130	9178
280.74	4179	9238
282.38	4230	9118
284.02	4154	8944
285.66	4023	8831
287.30	3967	9001
288.94	3847	8887
290.58	3879	8722
292.22	3879	8831
293.86	3944	8831
295.51	3795	8887
297.15	3676	8776
298.79	3619	8776
300.43	3459	8668
302.07	3375	8776
303.71	3375	8831
305.35	3510	9001
306.99	3582	8831
308.63	3601	8510
310.27	3564	8408
311.91	3459	8260
313.55	3392	8117
315.19	3343	8260
316.83	3343	8459

Table A-10, continued. Boring Z3-B6, S - R1 quality assurance analysis  
P- and S<sub>H</sub>-wave data

# SR-710 BORING Z3-B12

## VELOCITY (METERS/SECOND)

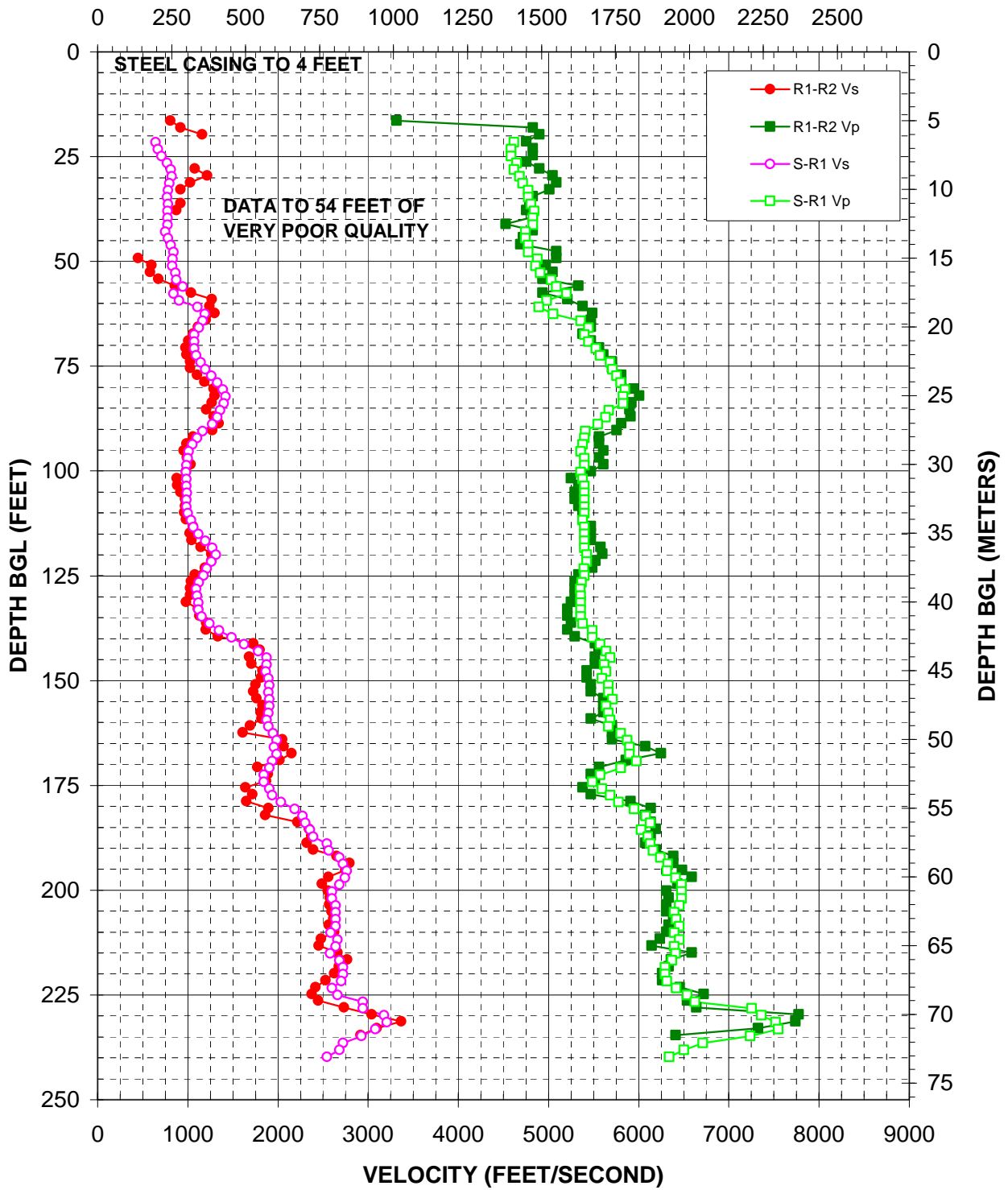


Figure A-11. Boring Z3-B12, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
13.35		
21.56	645	4619
23.20	669	4589
24.84	711	4589
26.48	769	4650
28.12	814	4619
29.76	823	4681
31.40	795	4712
33.04	782	4776
34.68	773	4776
36.32	782	4809
37.96	778	4842
39.60	778	4825
41.24	778	4825
42.88	749	4744
44.52	782	4744
46.16	814	4776
47.80	843	4776
49.44	833	4876
51.08	828	4859
52.72	864	4910
54.36	874	5033
56.00	945	5088
57.64	843	5201
59.28	906	4979
60.93	1111	4893
62.57	1188	5051
64.21	1164	5360
65.85	1122	5443
67.49	1072	5401
69.13	1072	5443
70.77	1072	5528
72.41	1092	5572
74.05	1142	5685
75.69	1196	5708
77.33	1261	5755
78.97	1327	5802
80.61	1390	5851
82.25	1418	5827
83.89	1401	5827
85.53	1358	5671
87.17	1327	5635
88.81	1272	5546
90.45	1164	5409
92.09	1102	5401
93.73	1053	5380
95.37	1010	5360
97.01	1002	5401
98.65	985	5401
100.30	979	5360

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
101.94	985	5380
103.58	985	5401
105.22	993	5401
106.86	985	5401
108.50	985	5401
110.14	1002	5401
111.78	1037	5380
113.42	1062	5401
115.06	1120	5401
116.70	1196	5401
118.34	1274	5401
119.98	1312	5426
121.62	1261	5426
123.26	1211	5392
124.90	1174	5401
126.54	1122	5368
128.18	1092	5351
129.82	1102	5360
131.46	1120	5360
133.10	1120	5360
134.74	1153	5360
136.38	1244	5380
138.02	1348	5485
139.67	1484	5485
141.31	1625	5572
142.95	1782	5639
144.59	1872	5685
146.23	1872	5617
147.87	1862	5639
149.51	1892	5594
151.15	1903	5662
152.79	1892	5662
154.43	1903	5708
156.07	1903	5639
157.71	1892	5662
159.35	1872	5685
160.99	1892	5662
162.63	1945	5802
164.27	1989	5875
165.91	1956	5900
167.55	1989	5900
169.19	1934	5975
170.83	1903	5802
172.47	1843	5572
174.11	1845	5485
175.75	1903	5594
177.40	1934	5685
179.04	2035	5779
180.68	2187	5950
182.32	2272	6079

Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
183.96	2302	6132
185.60	2356	6027
187.24	2388	6105
188.88	2544	6132
190.52	2562	6159
192.16	2680	6241
193.80	2721	6325
195.44	2764	6314
197.08	2743	6412
198.72	2680	6477
200.36	2600	6477
202.00	2600	6477
203.64	2639	6453
205.28	2639	6394
206.92	2639	6418
208.56	2639	6453
210.20	2583	6394
211.84	2659	6453
213.48	2639	6394
215.12	2581	6412
216.77	2680	6371
218.41	2721	6291
220.05	2721	6291
221.69	2700	6314
223.33	2600	6418
224.97	2659	6537
226.61	2944	6624
228.25	2944	7253
229.89	3177	7360
231.53	3206	7517
233.17	3079	7549
234.81	2925	7238
236.45	2721	6712
238.09	2680	6501
239.73	2544	6337

Table A-11. Boring Z3-B12, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

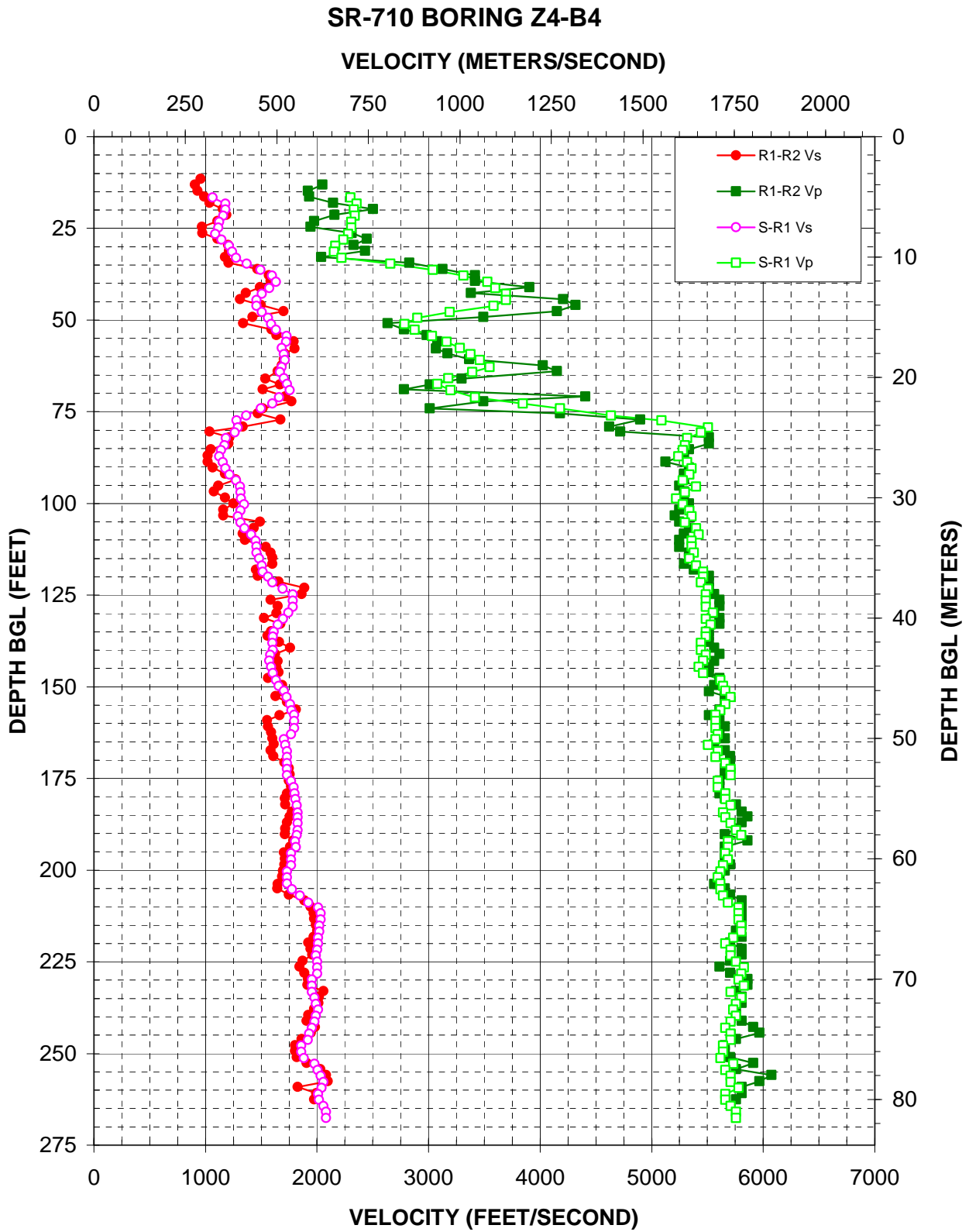


Figure A-12. Boring Z4-B4, R1 - R2 high resolution analysis and S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data



Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)	Depth (feet)	V <sub>s</sub> (feet/sec)	V <sub>p</sub> (feet/sec)
16.63	1064	2302	98.65	1320	5220	180.68	1810	5662
18.27	1178	2356	100.30	1348	5279	182.32	1819	5708
19.91	1178	2333	101.94	1315	5339	184.28	1828	5639
21.56	1159	2340	103.58	1291	5360	185.60	1828	5662
23.20	1125	2310	105.22	1315	5299	187.24	1828	5708
24.84	1114	2310	106.86	1350	5401	189.21	1828	5755
26.48	1087	2280	108.50	1410	5422	190.52	1819	5802
28.12	1143	2236	110.14	1451	5360	192.16	1803	5685
29.76	1211	2167	111.78	1457	5360	193.80	1812	5685
31.40	1240	2154	113.42	1457	5380	195.44	1769	5662
33.04	1277	2222	115.06	1481	5339	197.08	1766	5685
34.68	1371	2659	117.03	1507	5401	198.72	1766	5639
36.32	1494	3039	118.67	1513	5464	200.36	1734	5617
37.96	1596	3312	119.98	1560	5464	202.00	1734	5594
39.60	1633	3528	121.62	1599	5443	203.64	1734	5617
41.24	1574	3601	123.26	1692	5507	205.28	1777	5617
42.88	1507	3695	124.90	1782	5485	206.92	1848	5639
44.52	1457	3695	126.54	1782	5485	208.89	1924	5685
46.16	1457	3582	128.18	1782	5485	210.20	2012	5779
47.80	1507	3191	129.82	1742	5550	211.84	2035	5779
49.44	1560	2901	131.46	1696	5485	213.48	2035	5779
51.08	1588	2786	133.10	1650	5528	215.12	2023	5802
52.72	1633	2877	135.07	1614	5485	216.77	2023	5802
54.36	1729	3033	136.38	1607	5485	218.41	2012	5731
56.00	1723	3163	138.02	1599	5443	220.05	2012	5662
57.64	1686	3281	139.99	1607	5443	221.69	2000	5708
59.28	1704	3375	141.31	1583	5485	223.33	1989	5708
60.93	1712	3459	142.95	1574	5464	224.97	2000	5755
62.89	1686	3546	144.59	1588	5422	226.61	2000	5827
64.21	1668	3392	146.23	1607	5464	228.25	2000	5802
65.85	1704	3177	148.20	1633	5617	229.89	1956	5779
67.49	1734	3079	149.84	1656	5639	231.53	1956	5827
69.13	1755	3199	151.15	1704	5662	233.17	1956	5708
71.10	1660	3417	152.79	1729	5708	234.81	1978	5802
72.74	1599	3847	154.76	1760	5662	236.45	1989	5755
74.05	1497	4179	156.40	1773	5617	238.09	2012	5731
76.02	1366	4634	157.71	1796	5572	239.73	1989	5755
77.33	1281	5088	159.35	1796	5572	241.37	1978	5708
79.30	1291	5507	161.32	1796	5572	243.01	1956	5662
80.61	1263	5443	162.96	1769	5594	244.65	1929	5708
82.25	1182	5319	164.27	1704	5572	246.29	1918	5708
84.22	1170	5299	165.91	1717	5507	247.93	1857	5639
85.53	1140	5279	167.55	1734	5594	249.57	1857	5639
87.17	1125	5240	169.19	1734	5572	251.21	1882	5617
88.81	1155	5319	170.83	1734	5662	252.85	1978	5731
90.45	1178	5360	172.47	1734	5708	254.49	2006	5662
92.09	1215	5339	174.11	1734	5708	256.14	2035	5708
93.73	1277	5279	175.75	1769	5594	257.78	2059	5708
95.37	1310	5401	177.40	1791	5594	259.42	2041	5779
97.01	1314	5299	179.04	1800	5662	261.06	2012	5662

Table A-12. Boring Z4-B4, S - R1 quality assurance analysis P- and S<sub>H</sub>-wave data

<b>Depth (feet)</b>	<b>V<sub>s</sub> (feet/sec)</b>	<b>V<sub>p</sub> (feet/sec)</b>
262.70	2018	5662
264.34	2059	5708
265.98	2083	5755
267.62	2083	5755

Table A-12, continued. Boring Z4-B4, S - R1 quality assurance analysis  
P- and S<sub>H</sub>-wave data

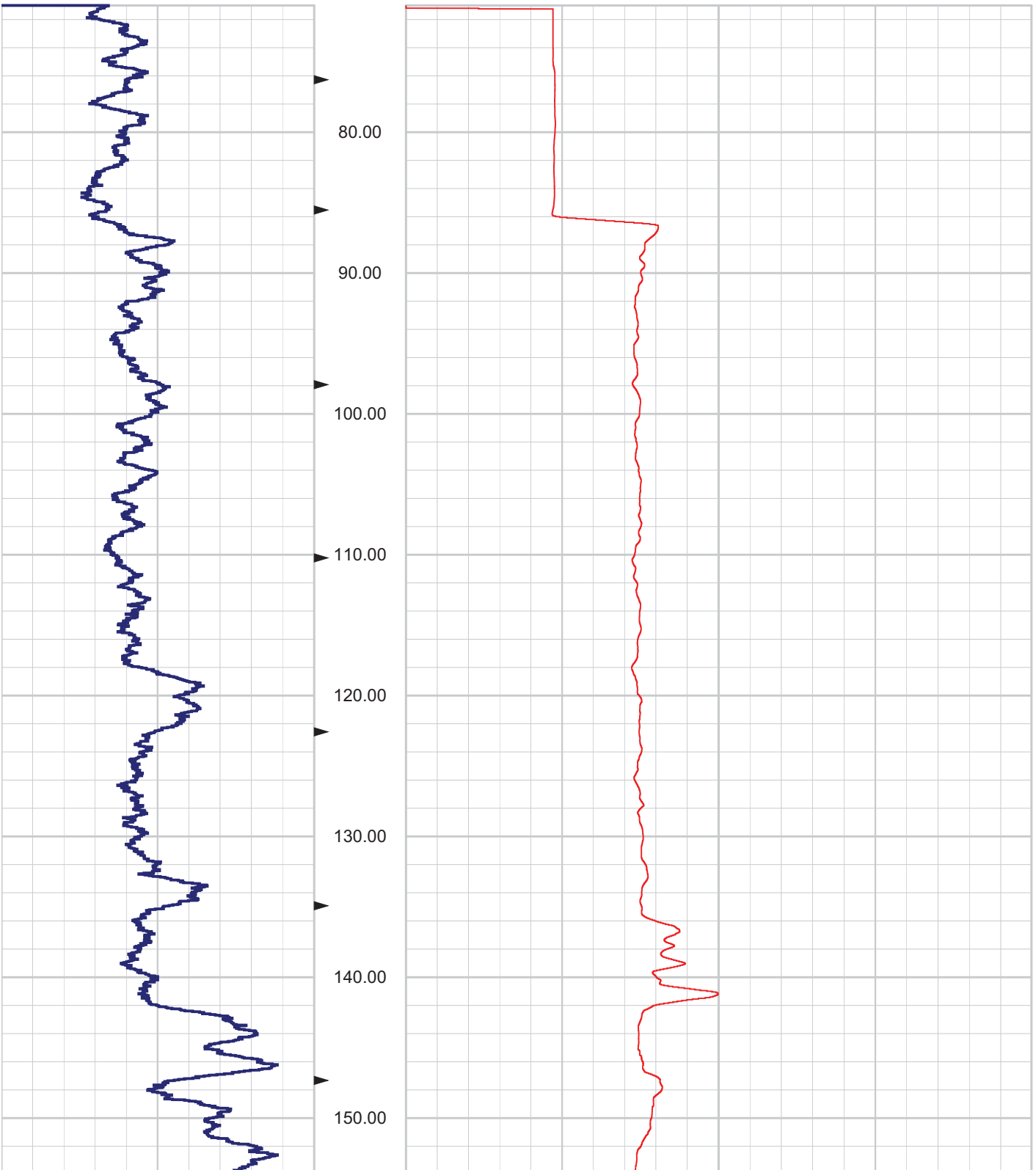
**APPENDIX B**

**CALIPER AND**

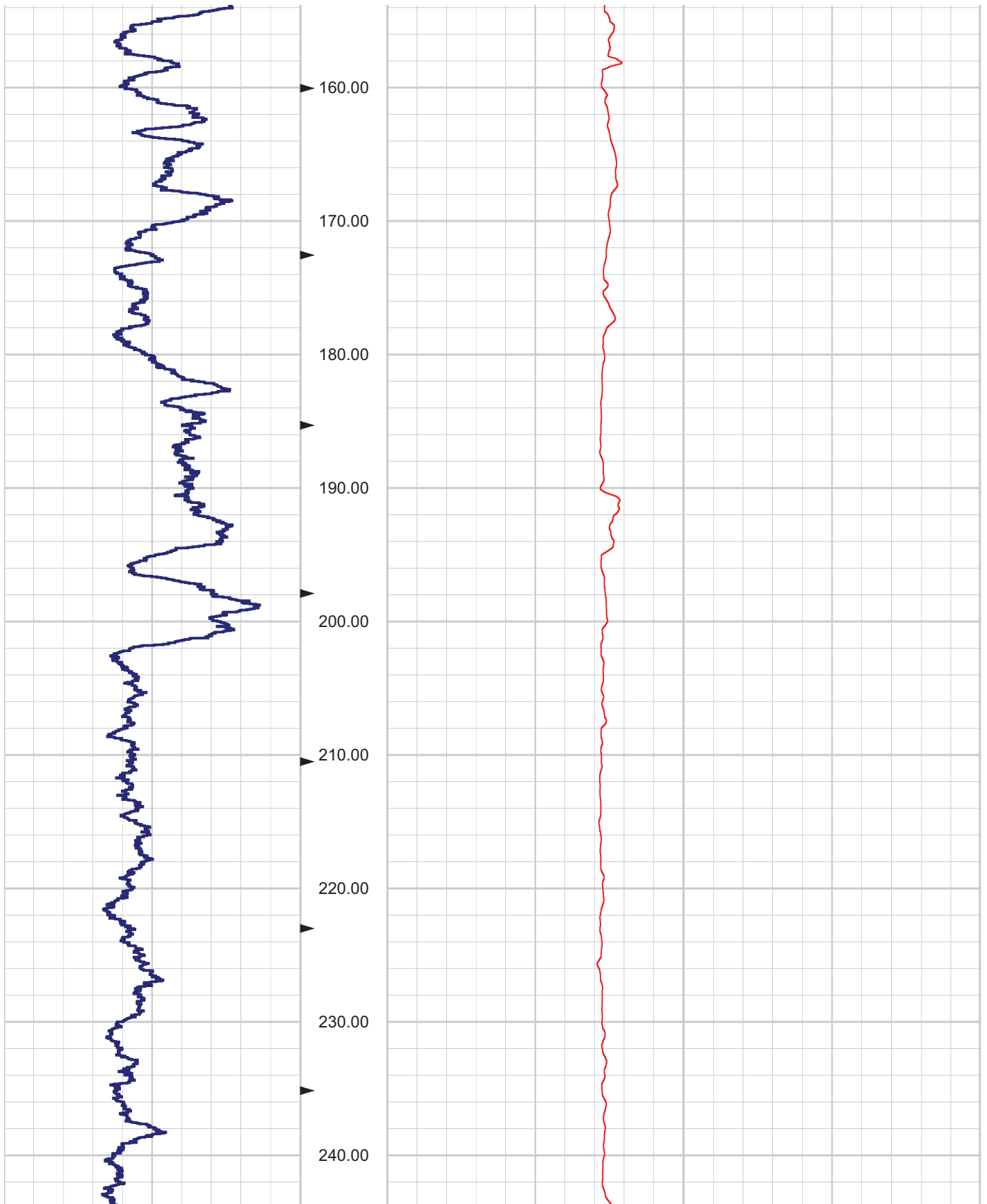
**NATURAL GAMMA LOGS**

0.00 NGAM API Cs. 11 0.00

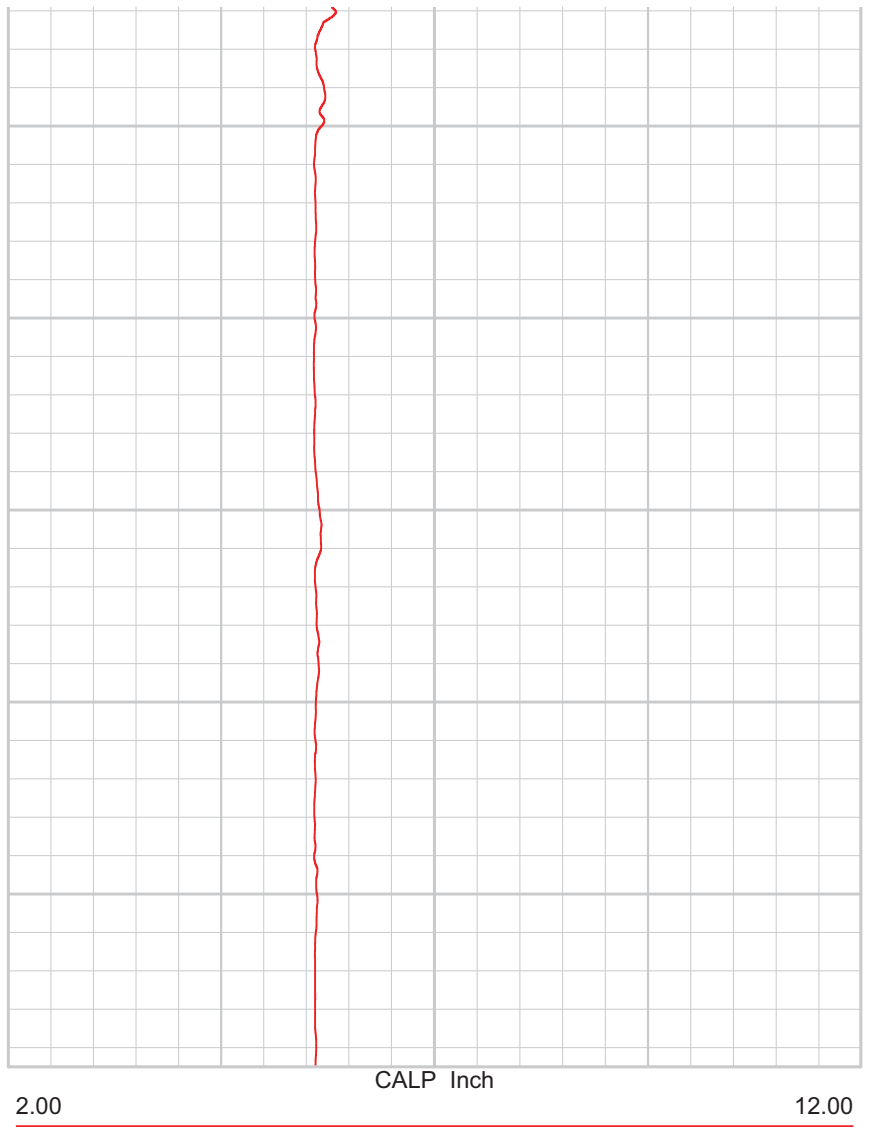
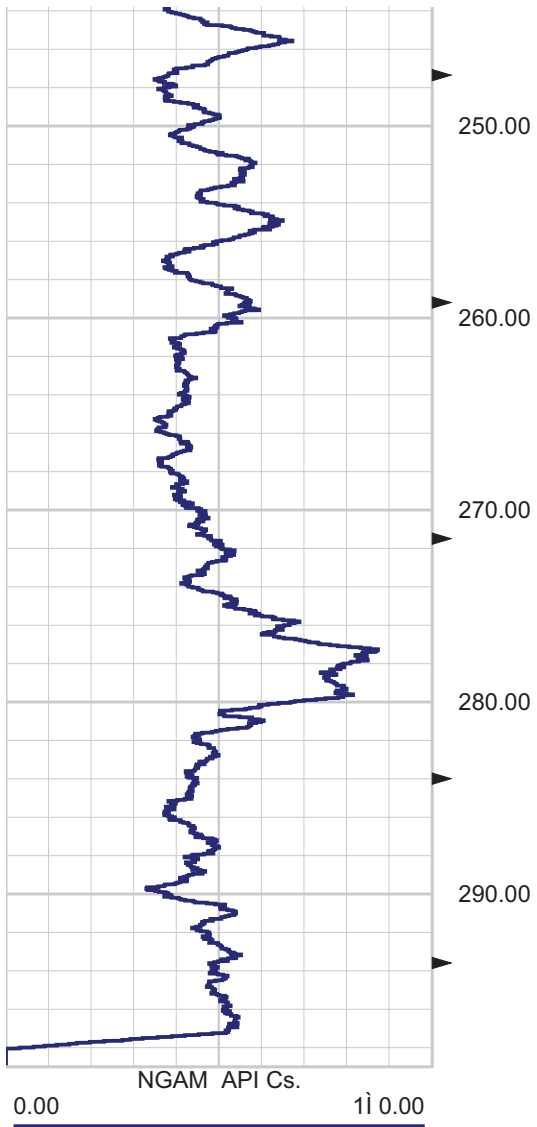
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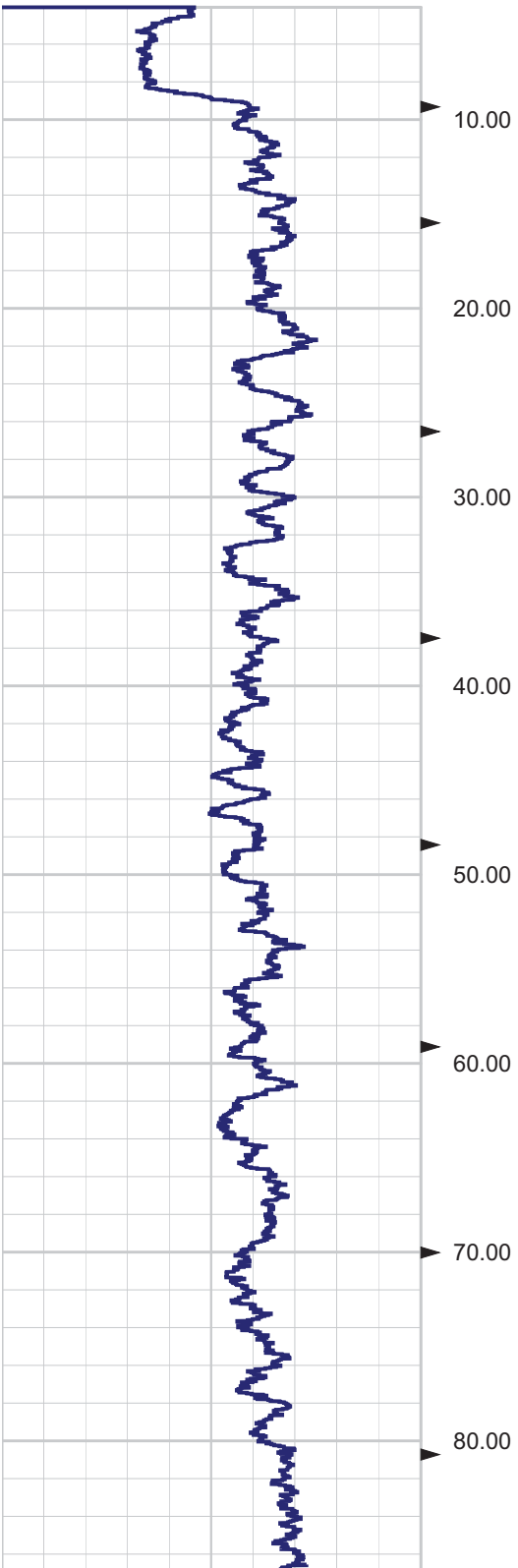
SR-710 Boring Z1-B3 Caliper and Natural Gamma rev 1.1 Sheet 1 of 3



SR-710 Boring Z1-B3 Caliper and Natural Gamma rev 1.1 Sheet 2 of 3



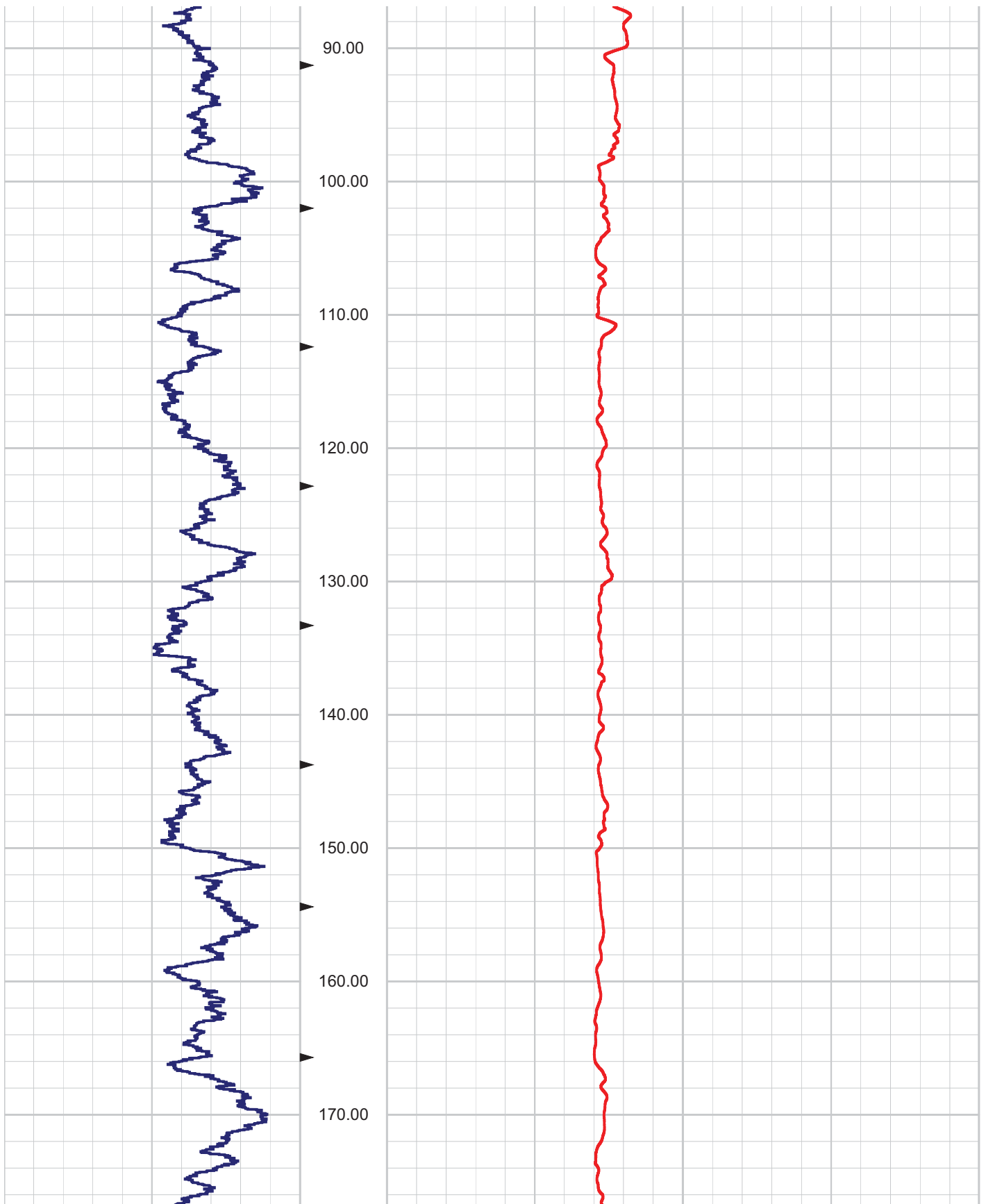
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2.00 CALP Inch 12.00

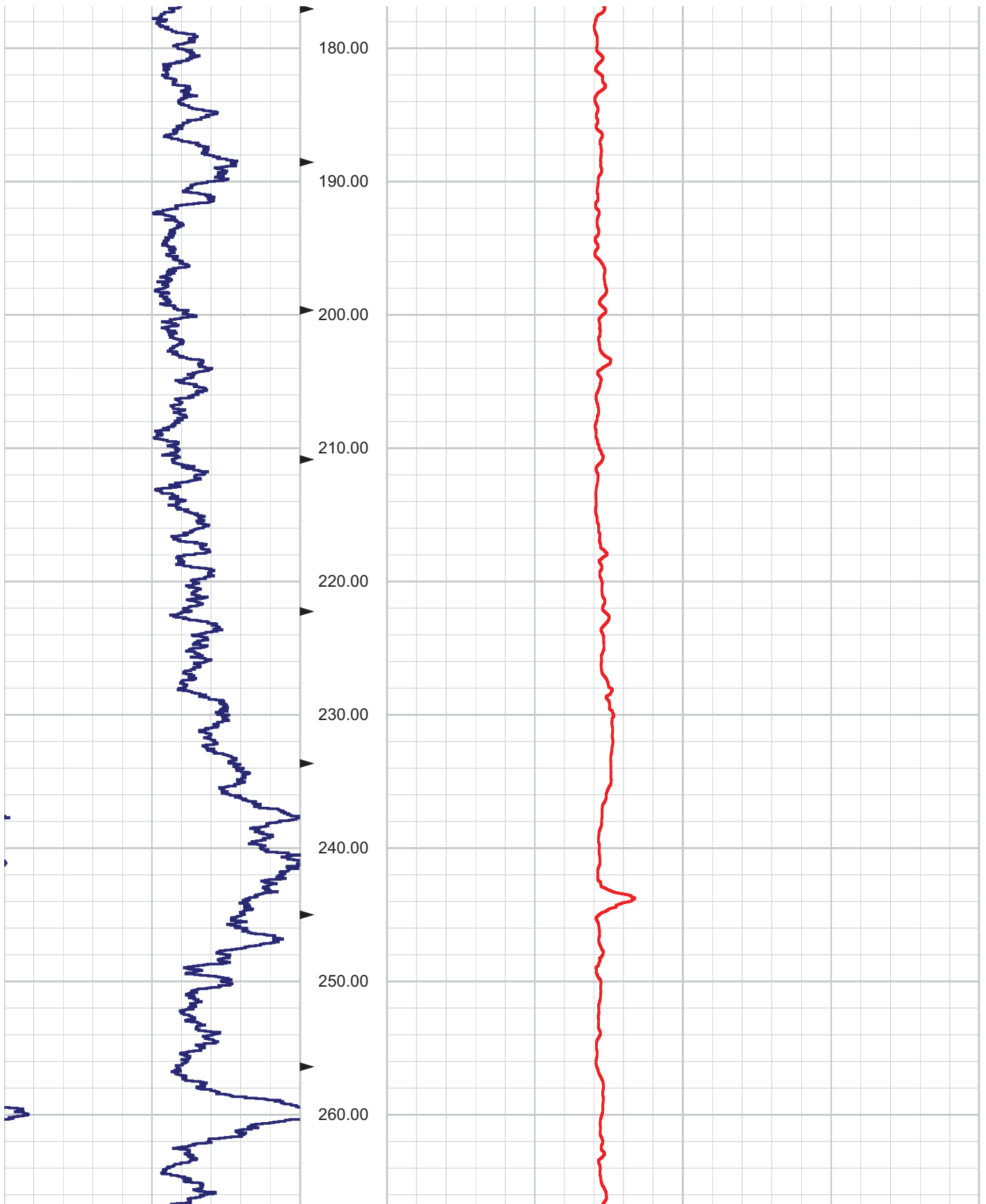


SR-710 Boring Z1-B5 Caliper and Natural Gamma rev 1.1 Sheet 1 of 6

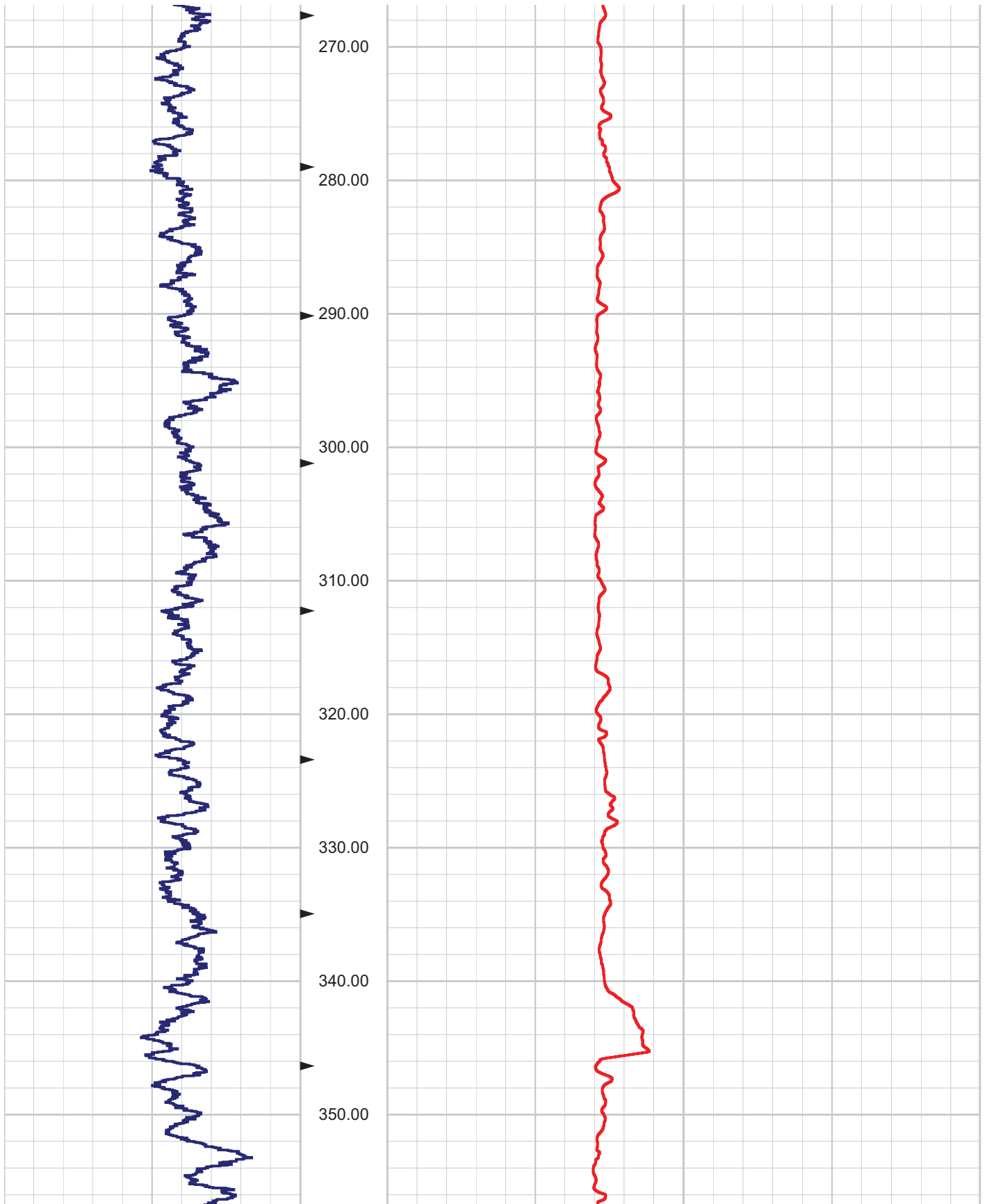


SR-710 Boring Z1-B5 Caliper and Natural Gamma rev 1.1 Sheet 2 of 6

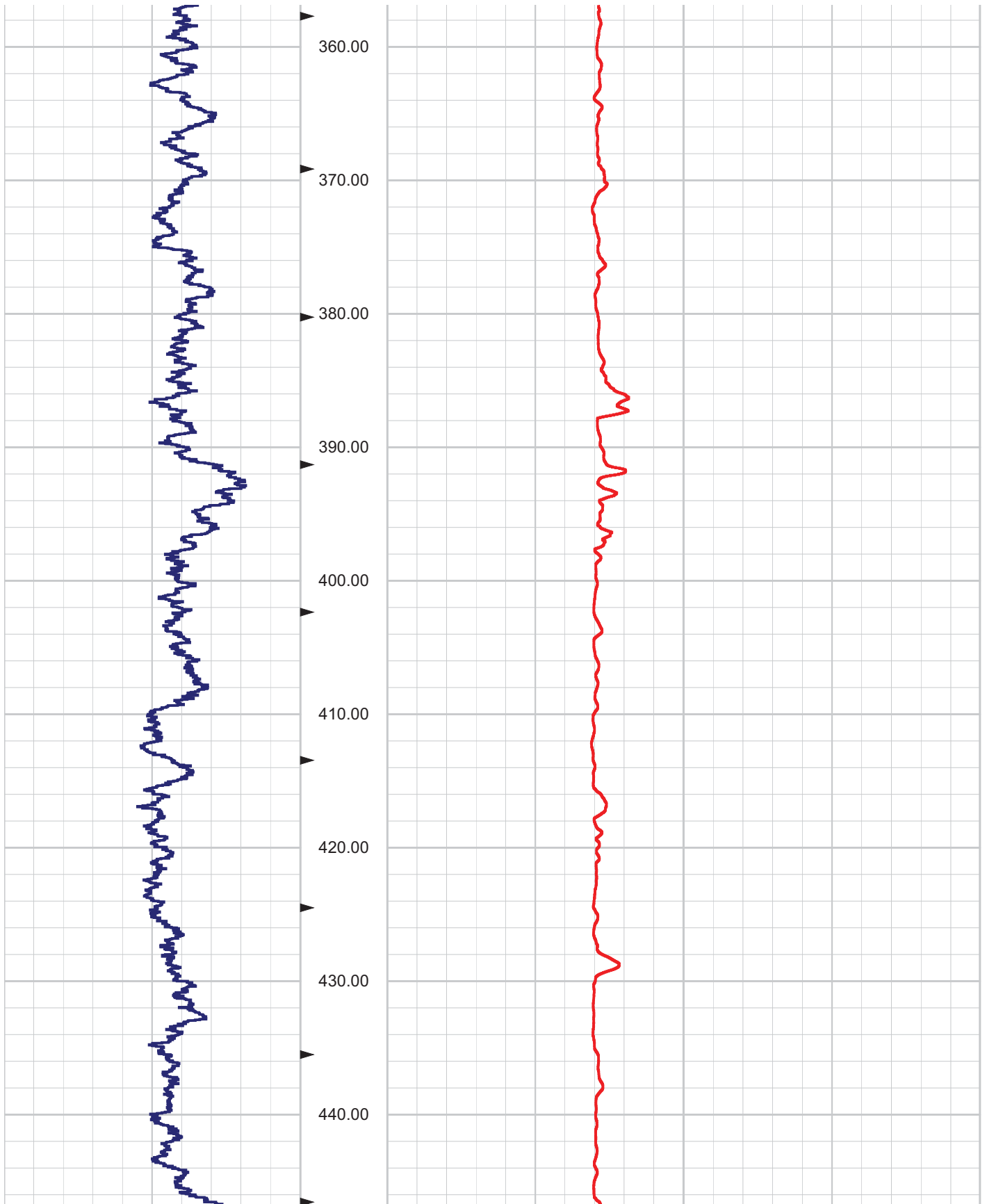




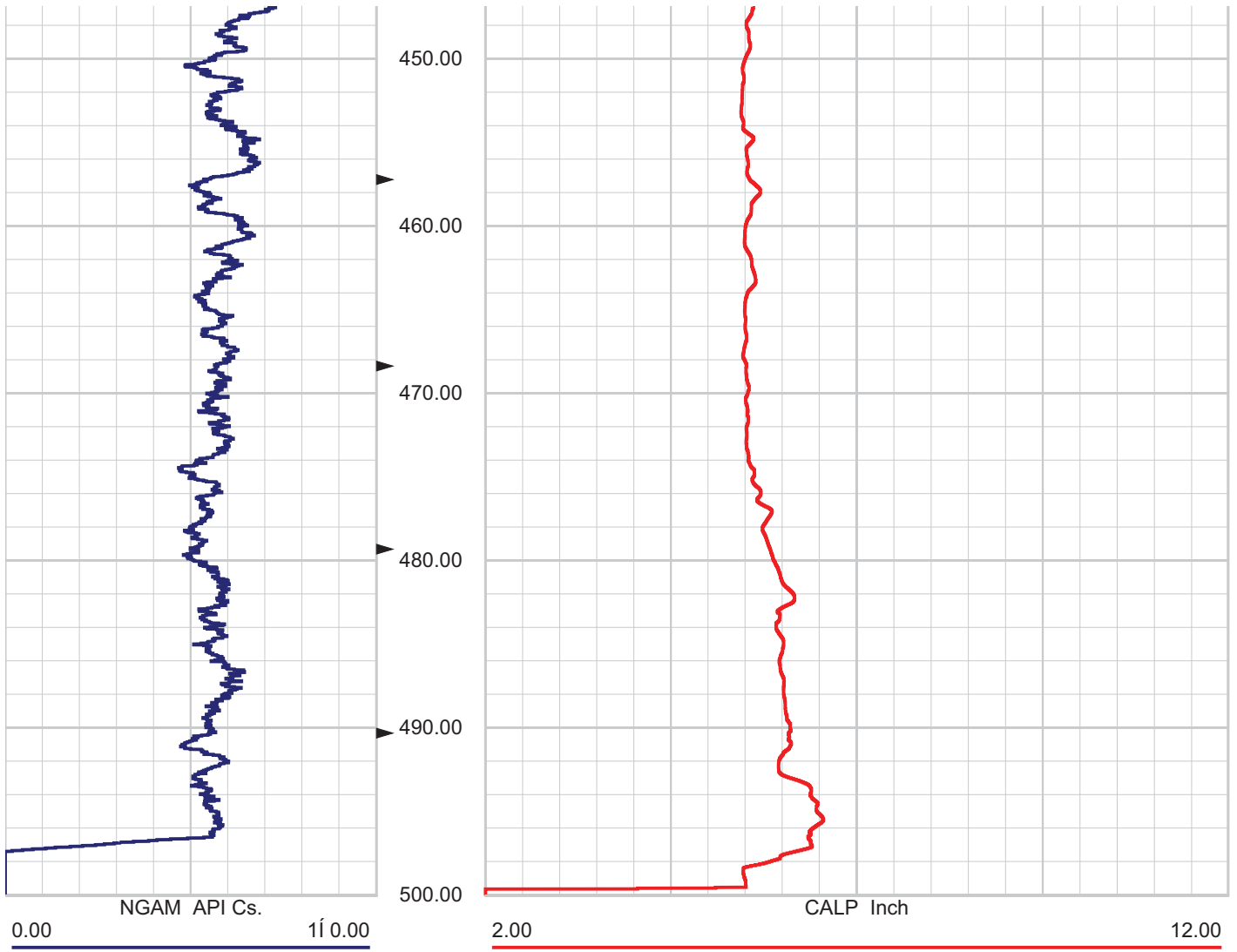
SR-710 Boring Z1-B5 Caliper and Natural Gamma rev 1.1 Sheet 3 of 6



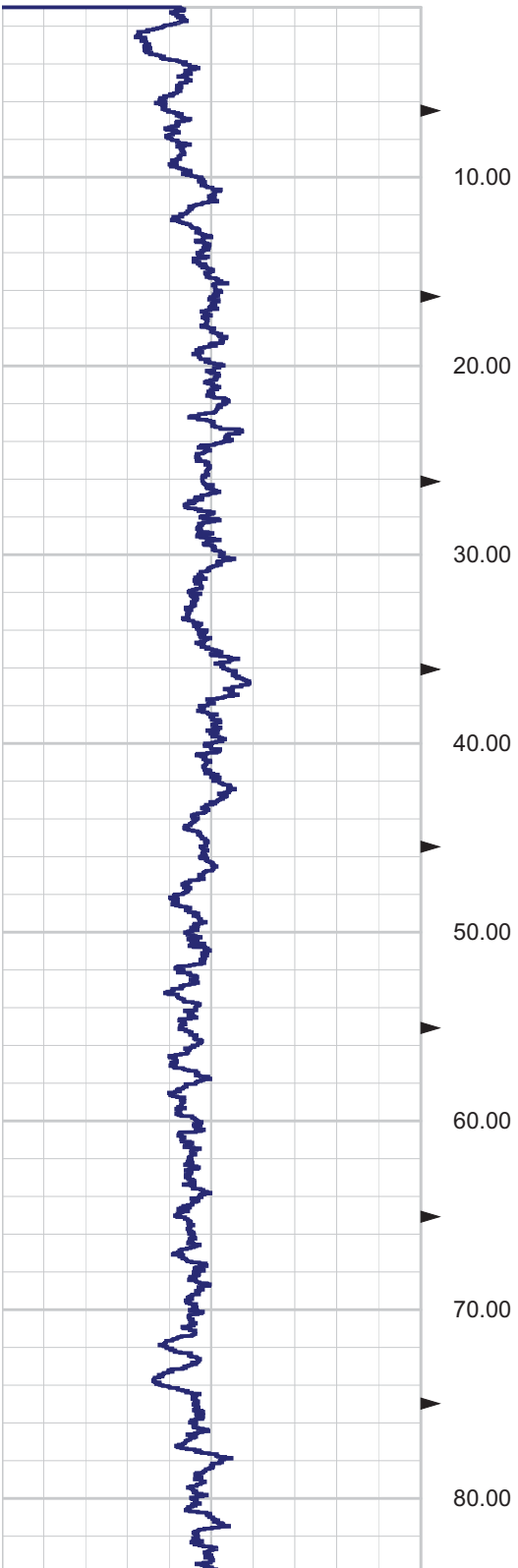
SR-710 Boring Z1-B5 Caliper and Natural Gamma rev 1.1 Sheet 4 of 6



SR-710 Boring Z1-B5 Caliper and Natural Gamma rev 1.1 Sheet 5 of 6

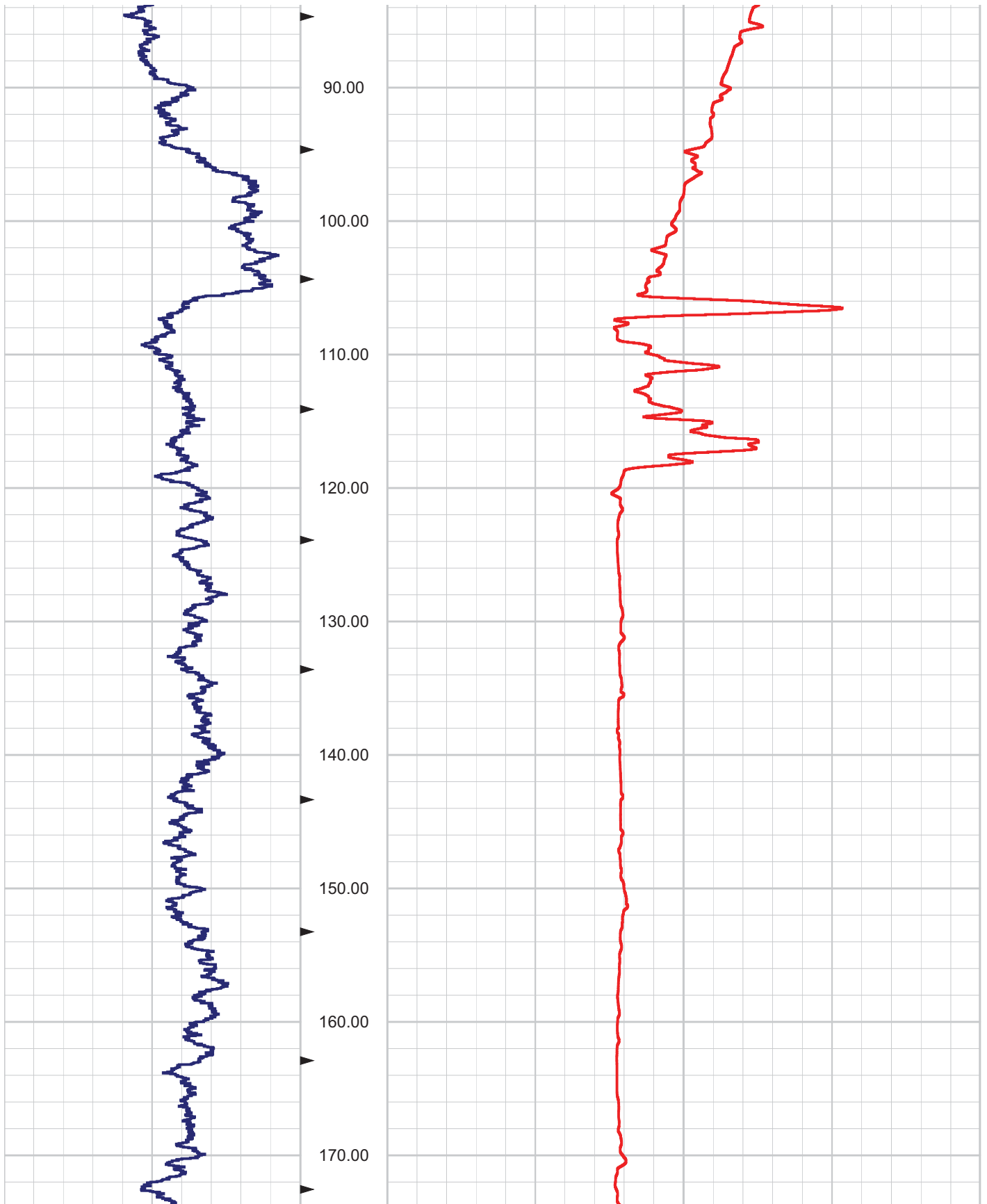


0.00 NGAM API Cs. 11 0.00

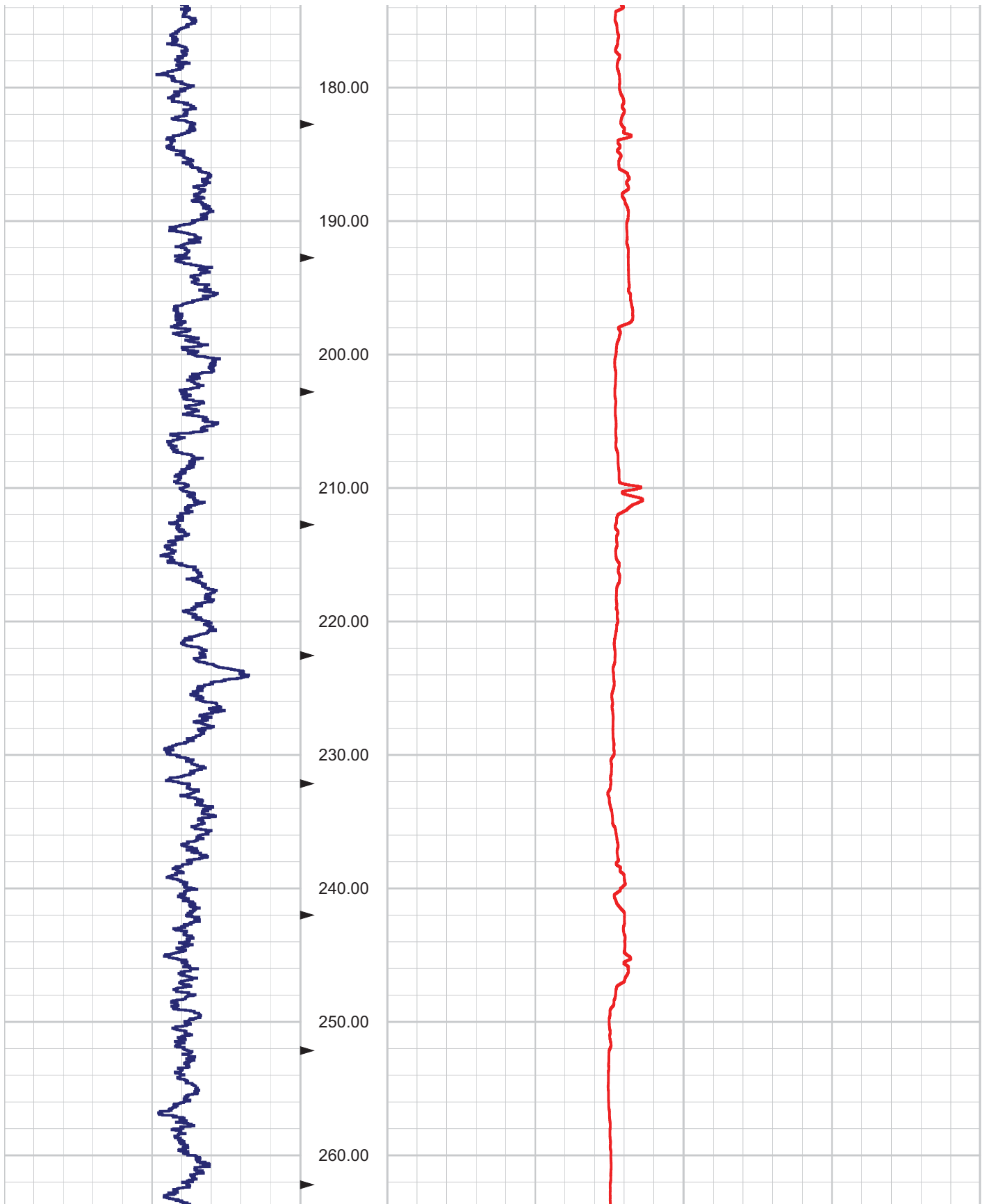


2.00 CALP Inch 12.00

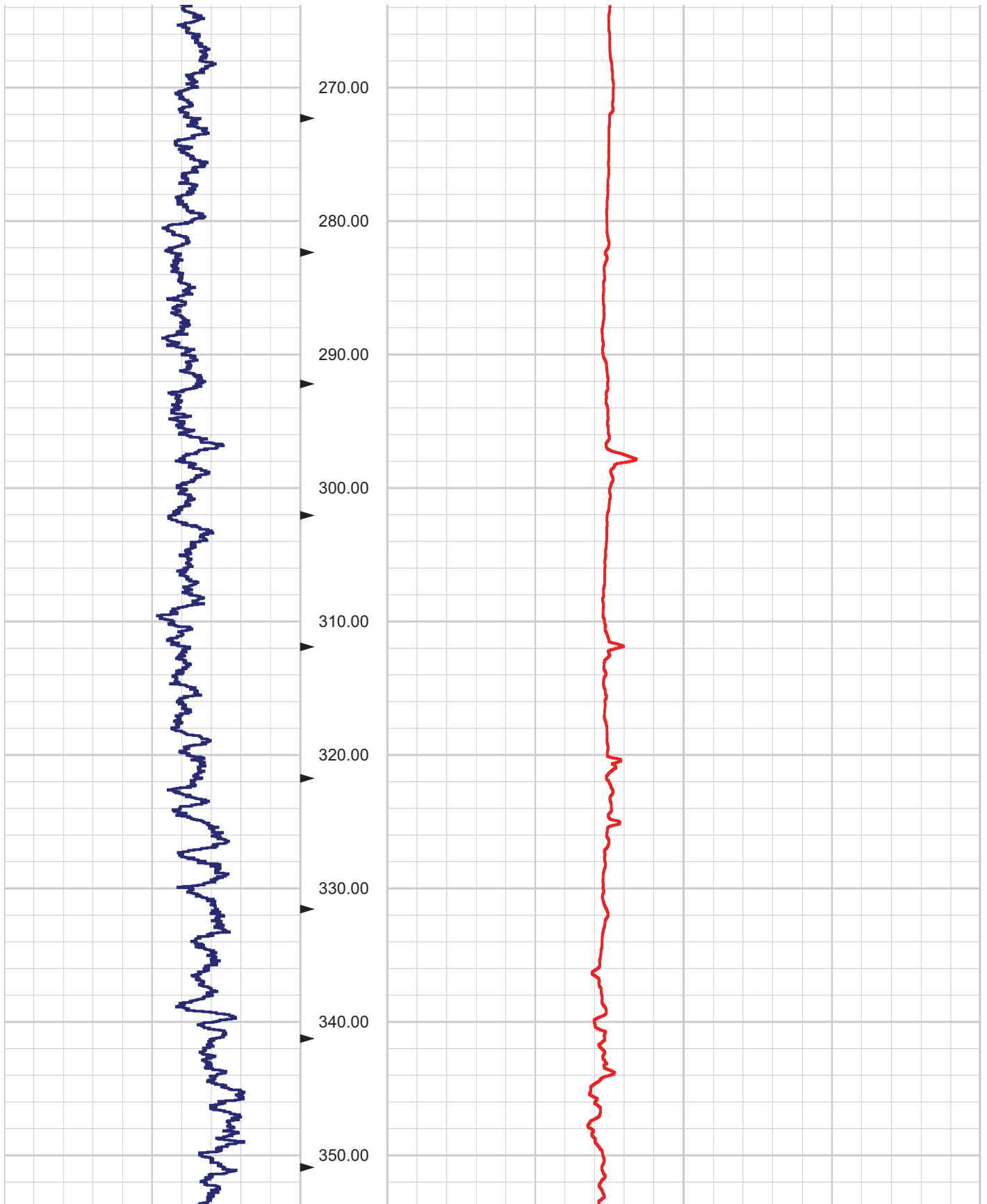




SR-710 Boring Z1-B6 Caliper and Natural Gamma rev 1.1 Sheet 2 of 5

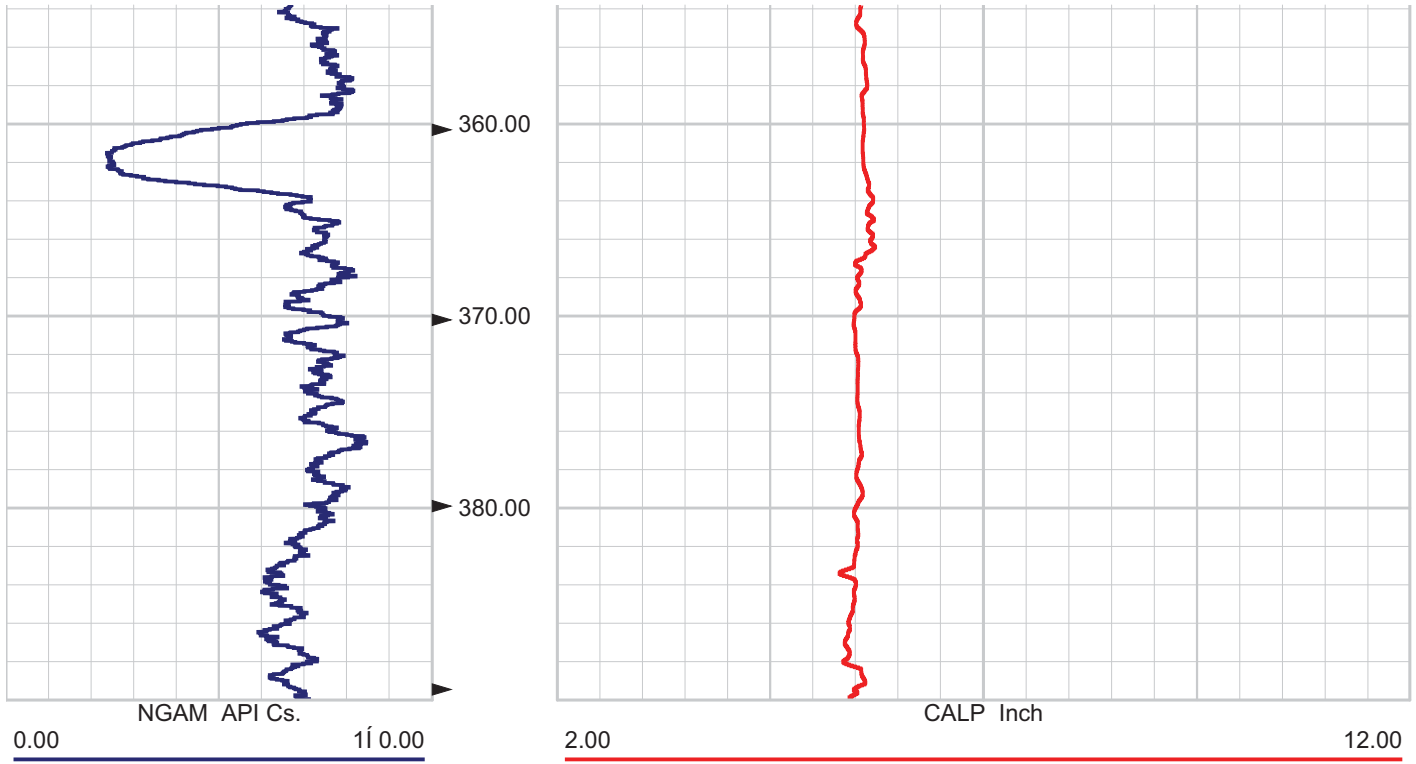


SR-710 Boring Z1-B6 Caliper and Natural Gamma rev 1.1 Sheet 3 of 5

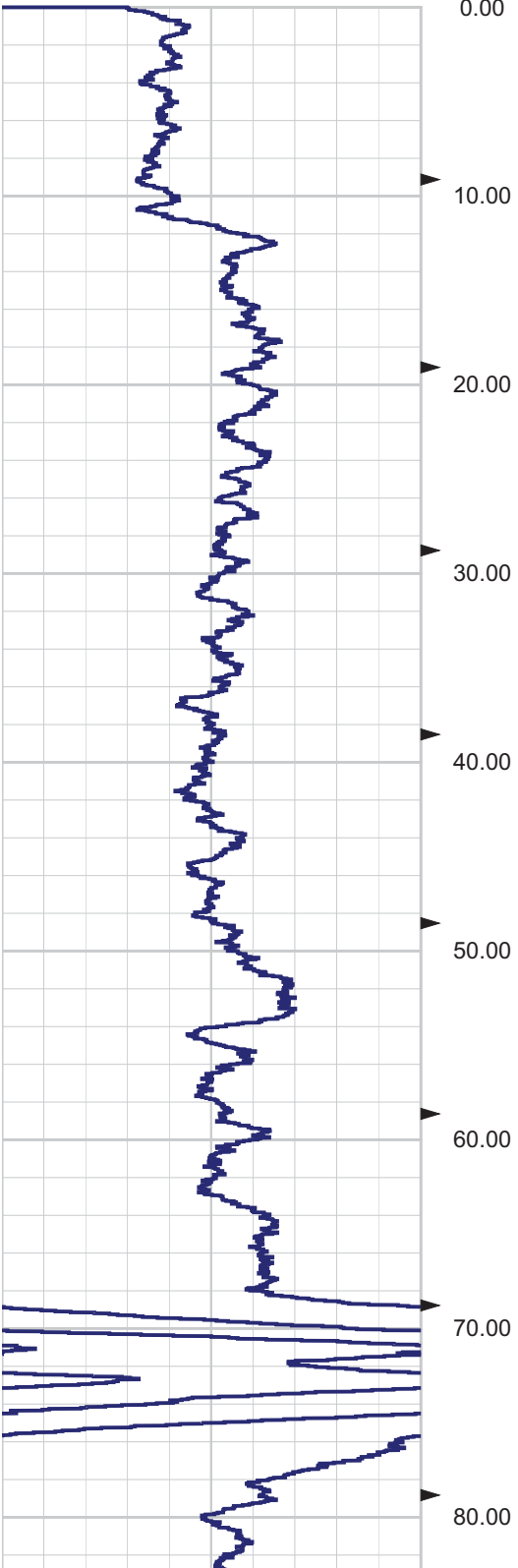


SR-710 Boring Z1-B6 Caliper and Natural Gamma rev 1.1 Sheet 4 of 5

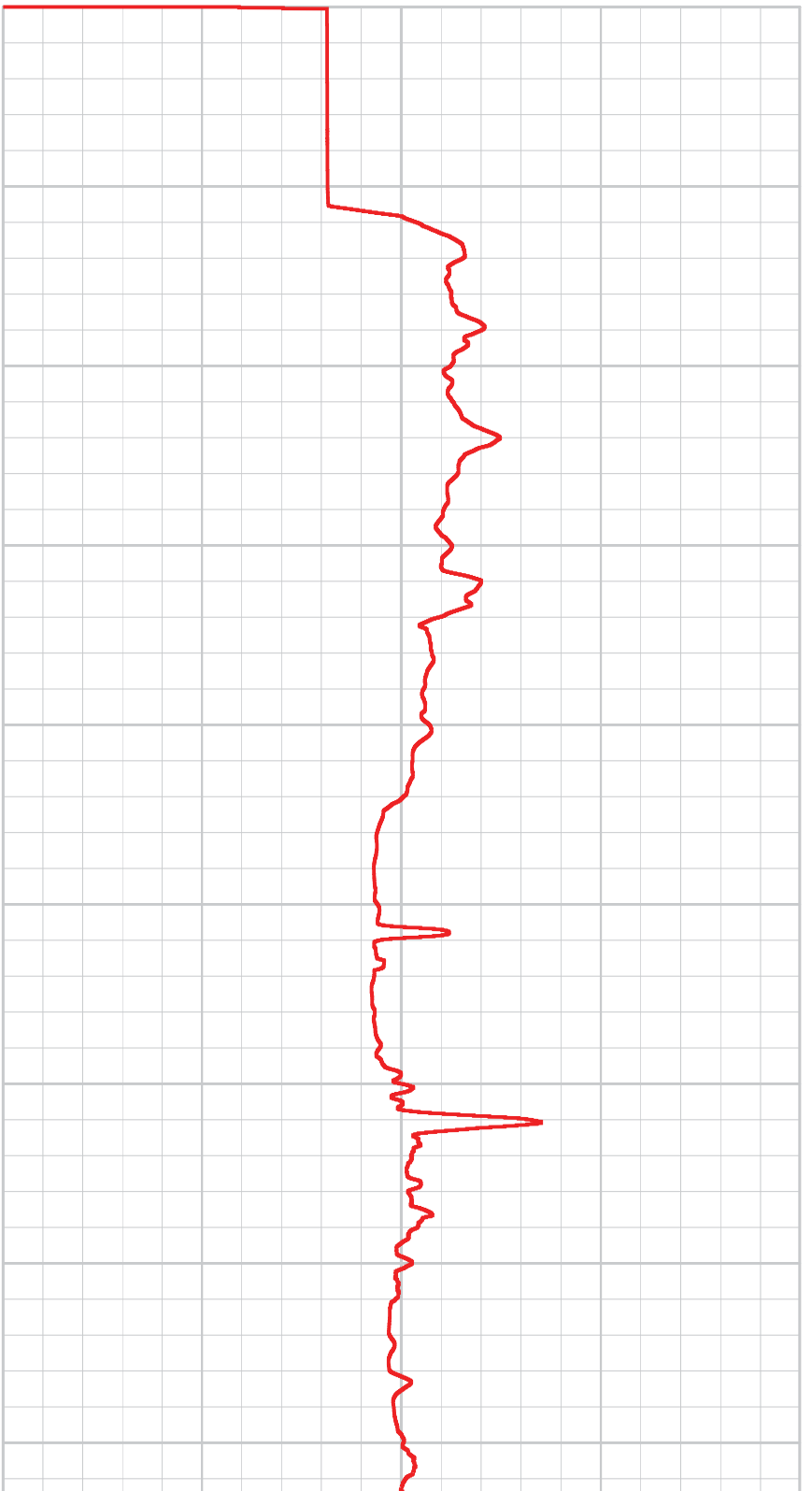




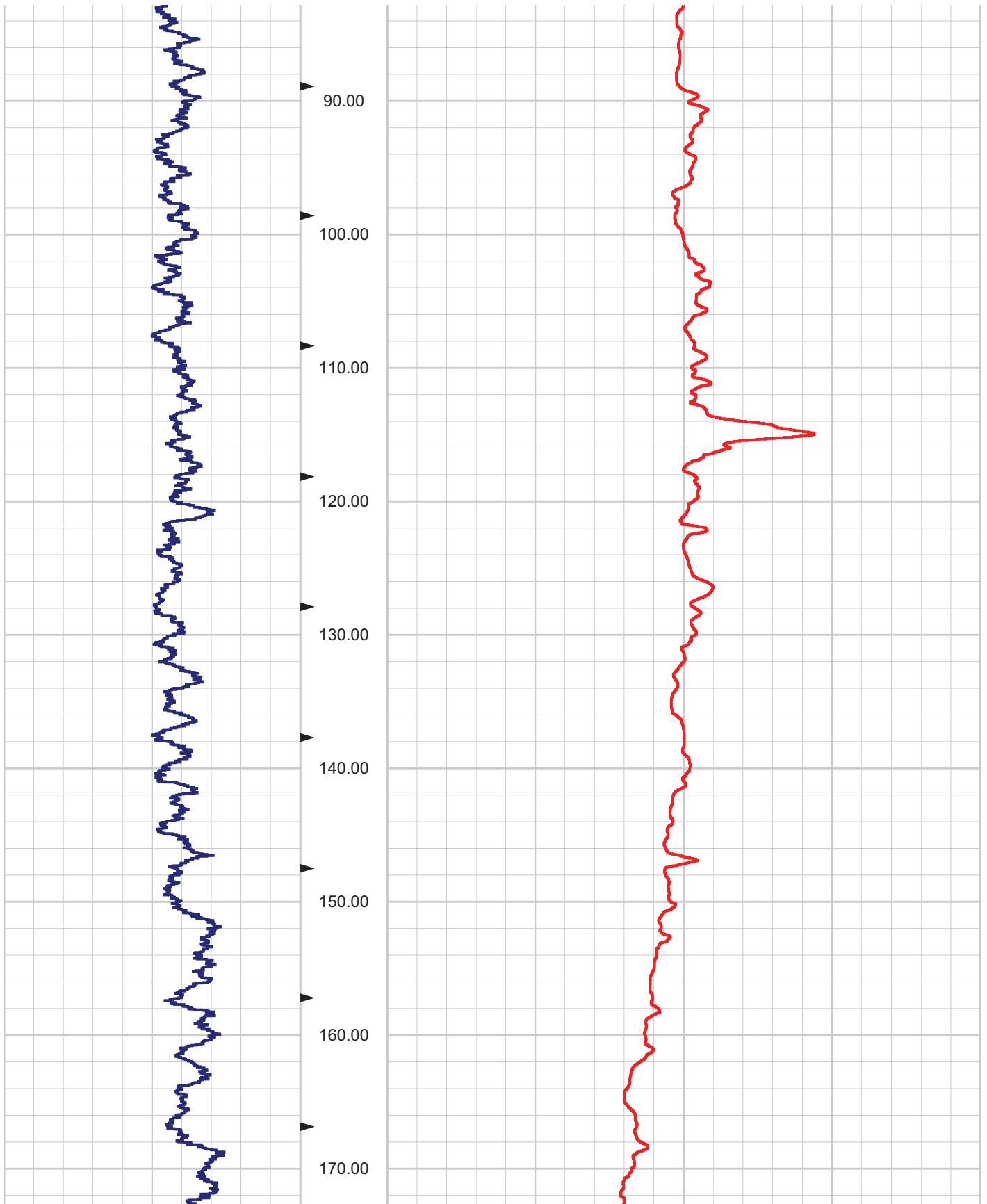
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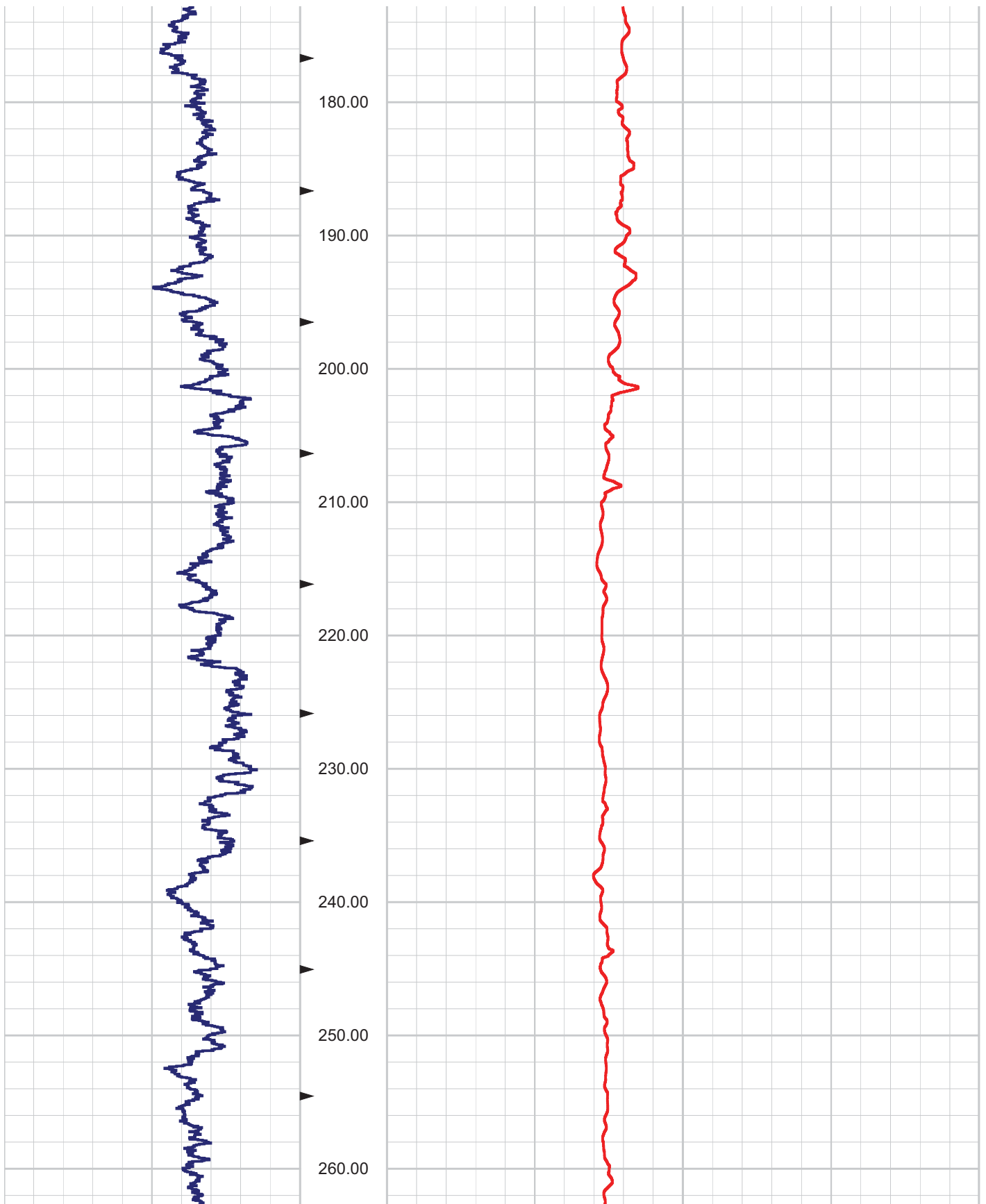
2.00 CALP Inch 12.00



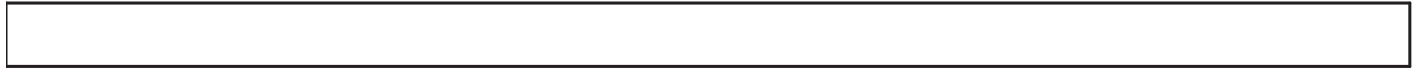
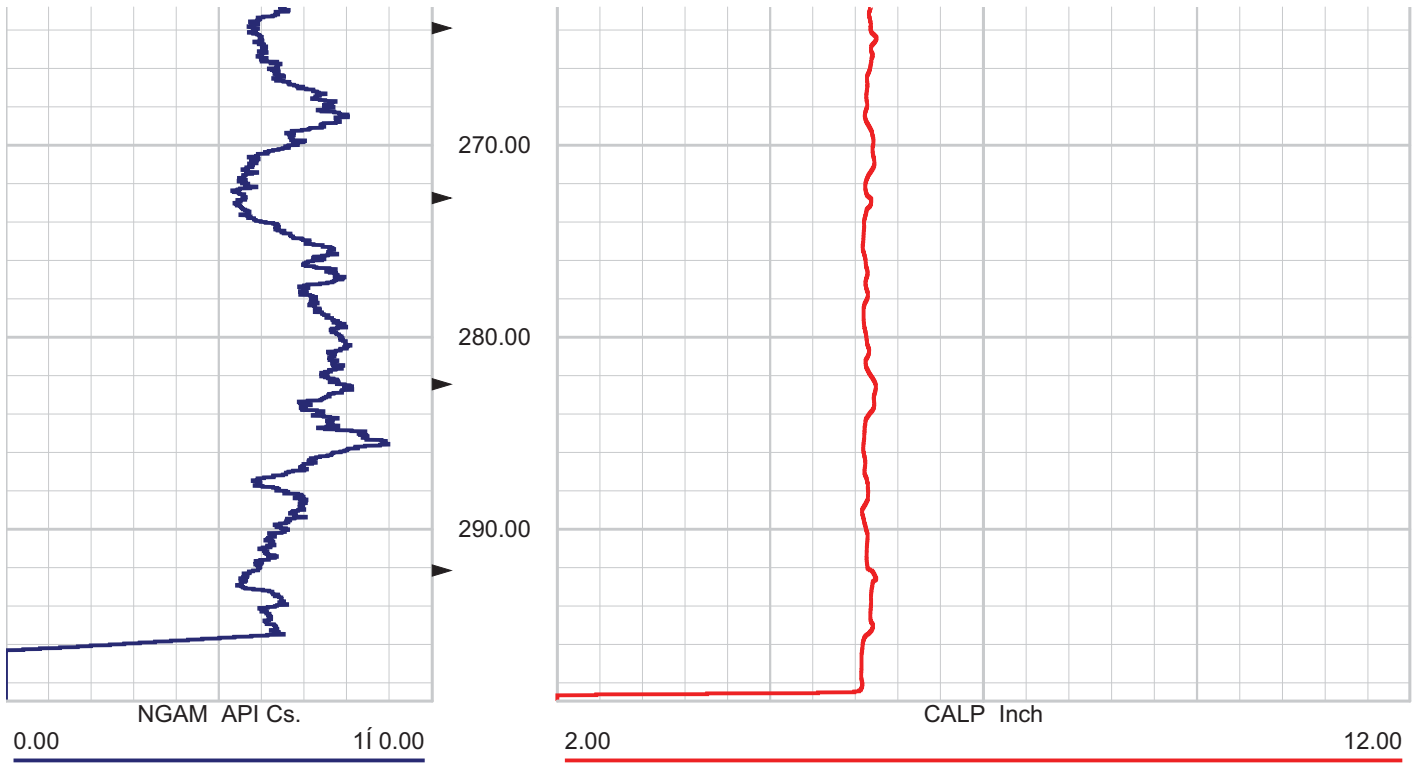
SR-710 Boring Z1-B7 Caliper and Natural Gamma rev 1.1 Sheet 1 of 4



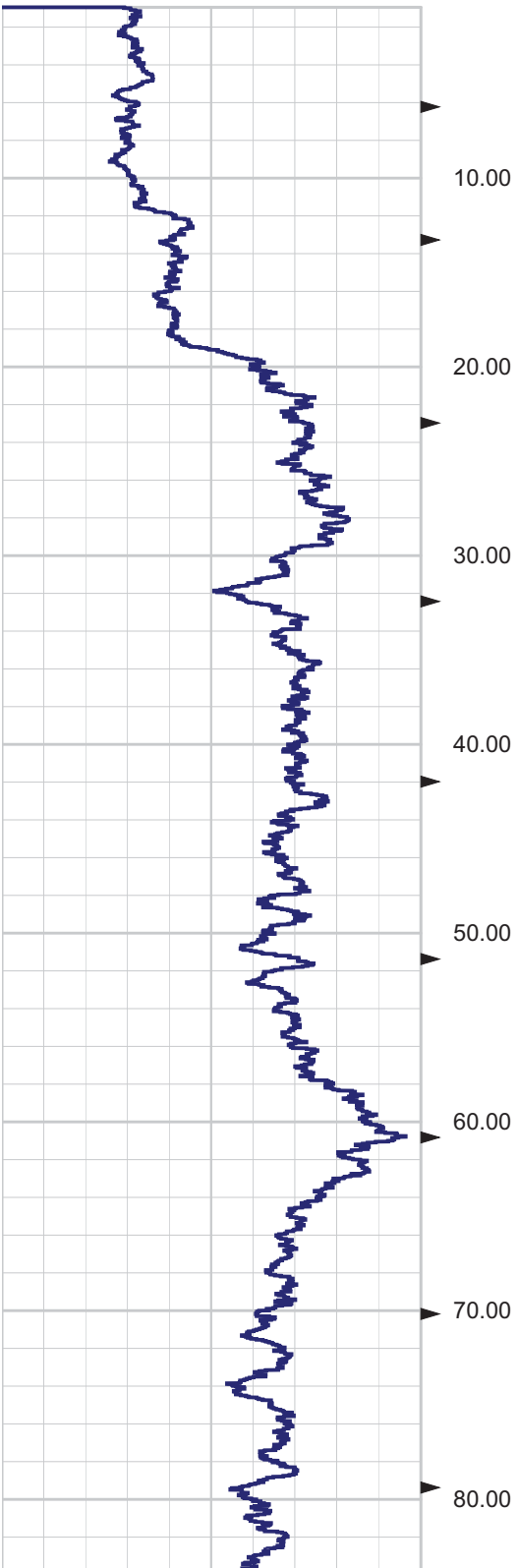
SR-710 Boring Z1-B7 Caliper and Natural Gamma rev 1.1 Sheet 2 of 4



SR-710 Boring Z1-B7 Caliper and Natural Gamma rev 1.1 Sheet 3 of 4



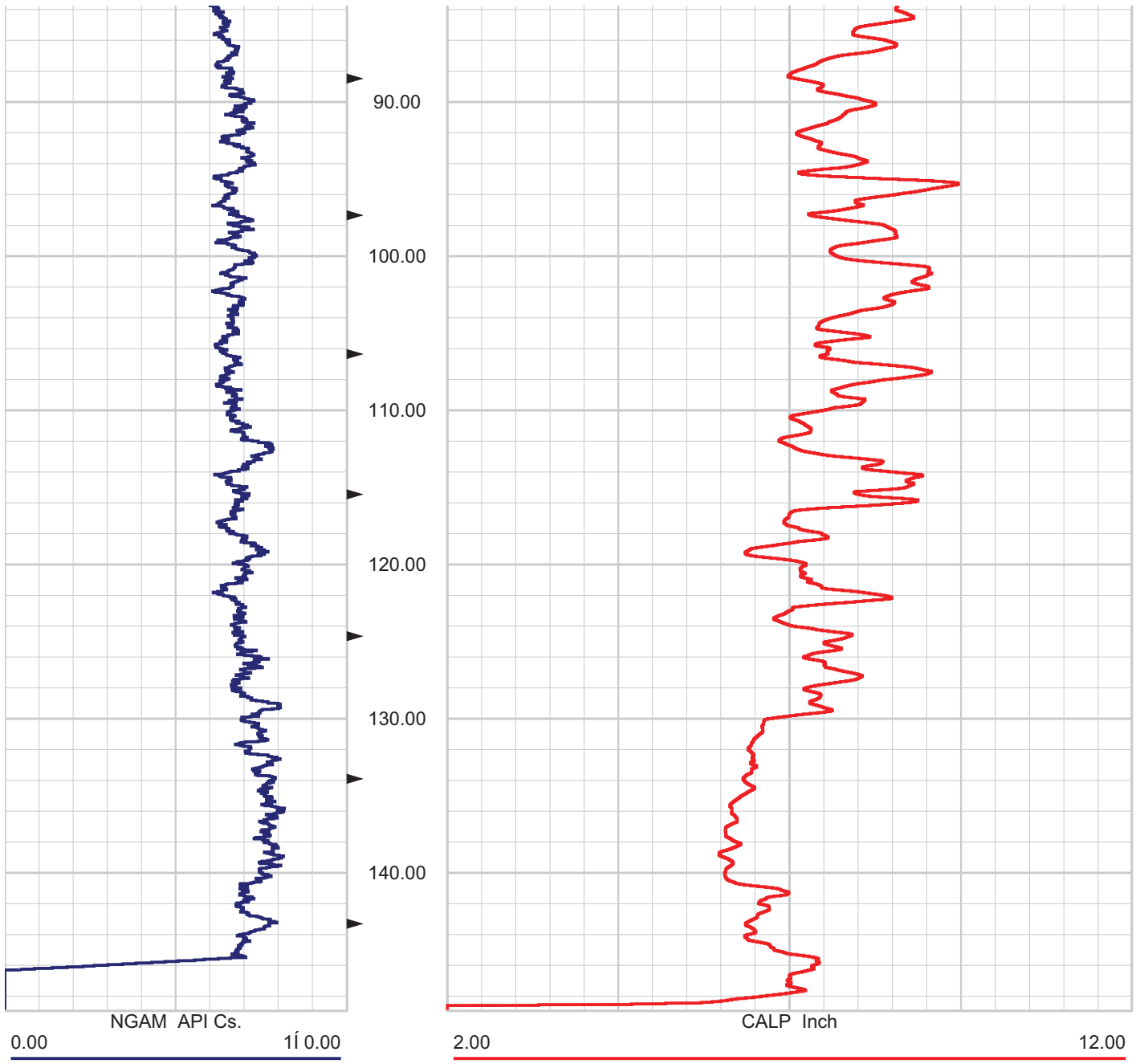
0.00 NGAM API Cs. 11 0.00



2.00 CALP Inch 12.00

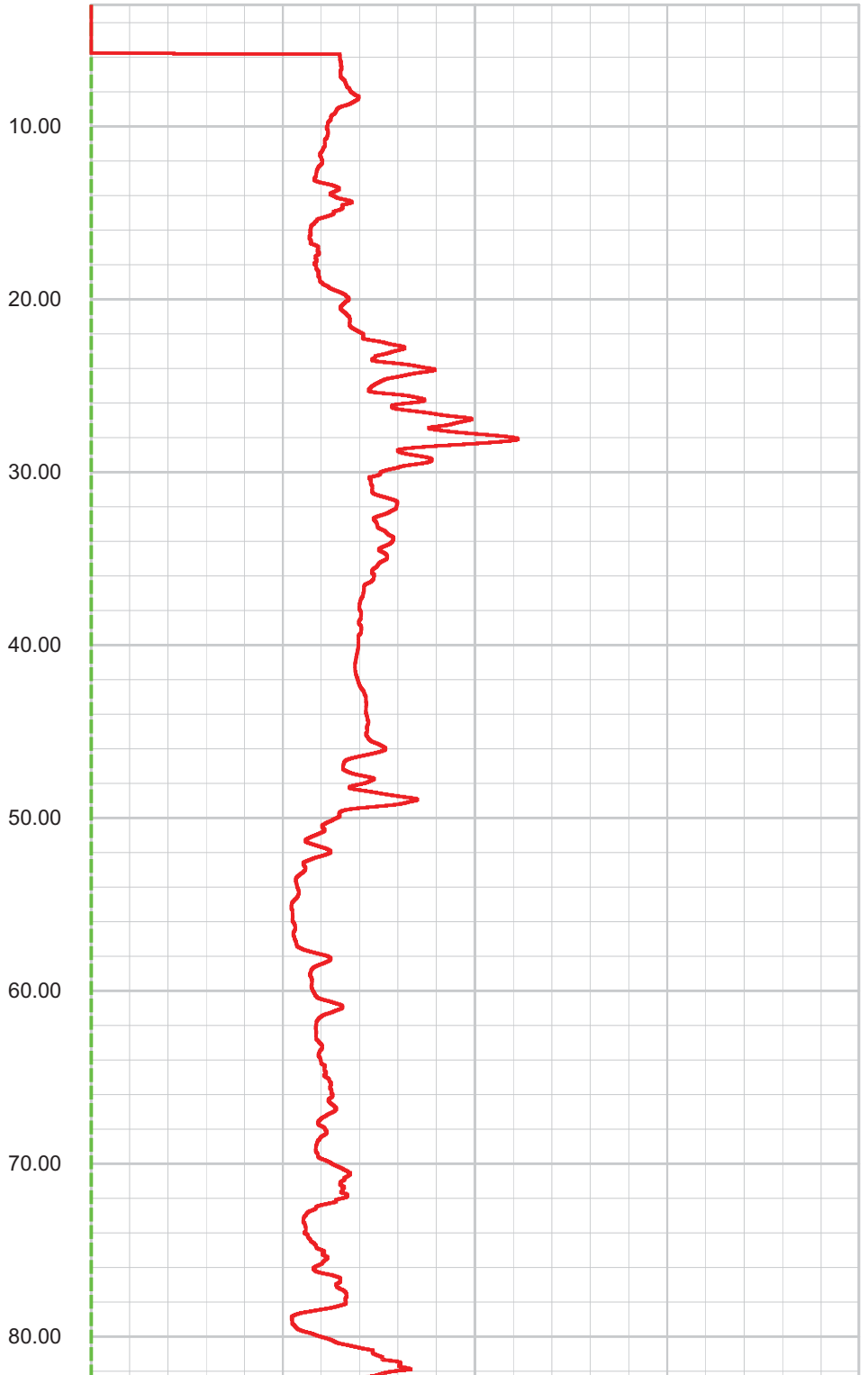
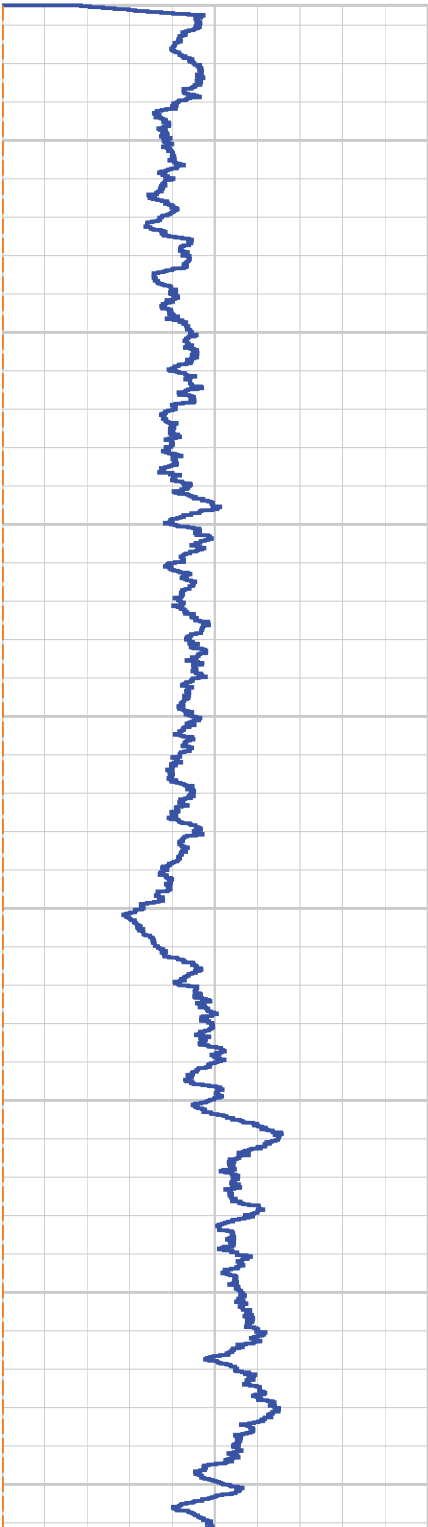


SR-710 Boring Z2-B1 Caliper and Natural Gamma rev 1.1 Sheet 1 of 2



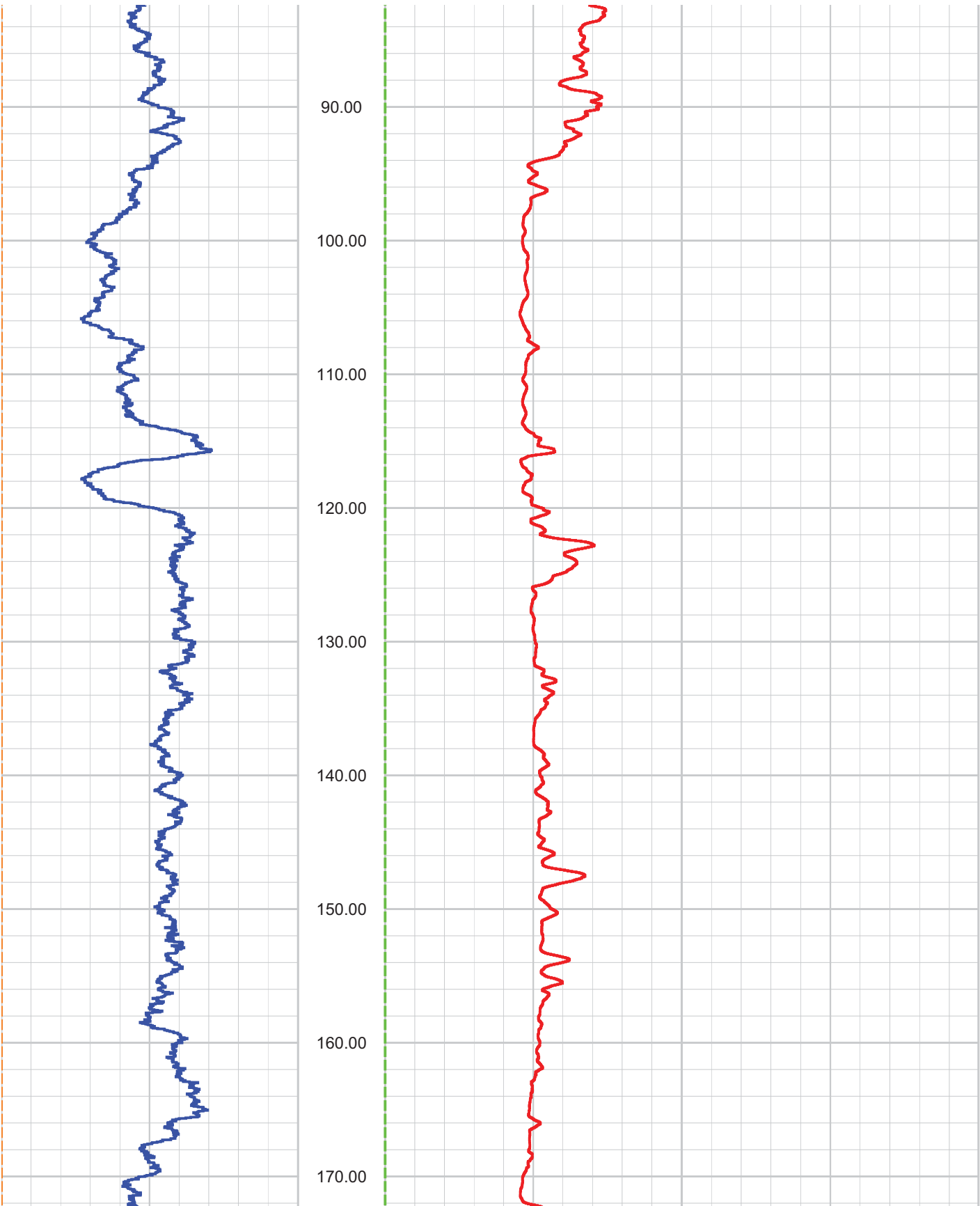
0.00	NGA1 API	200.00
<hr/>		
0.00	NGA2 API	200.00
<hr/>		

2.00	CAL2 INCH	12.00
<hr/>		
2.00	CAL1 INCH	12.00
<hr/>		

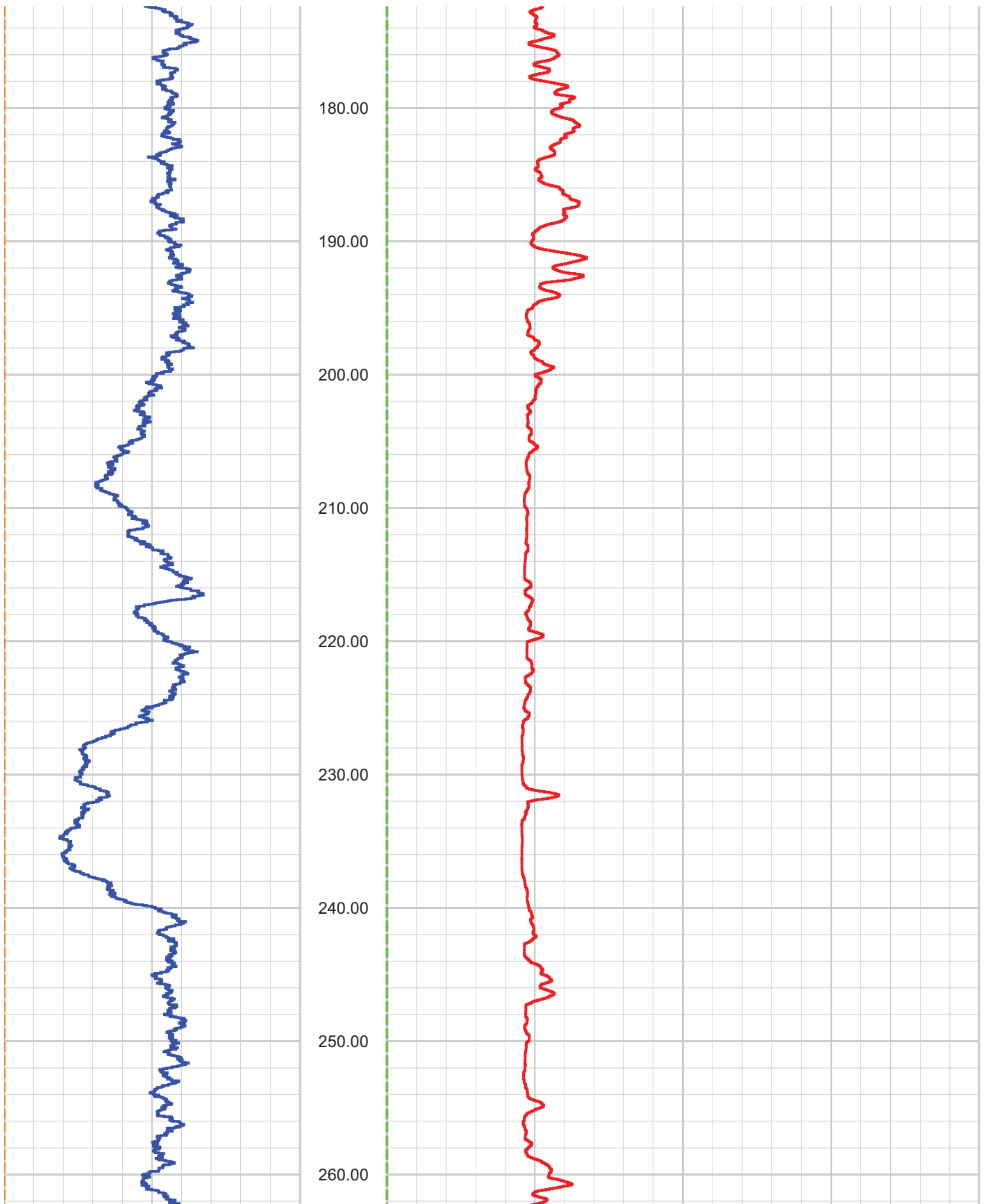


SR-710 Boring Z2-B4 Caliper and Natural Gamma rev 1.1 Sheet 1 of 5

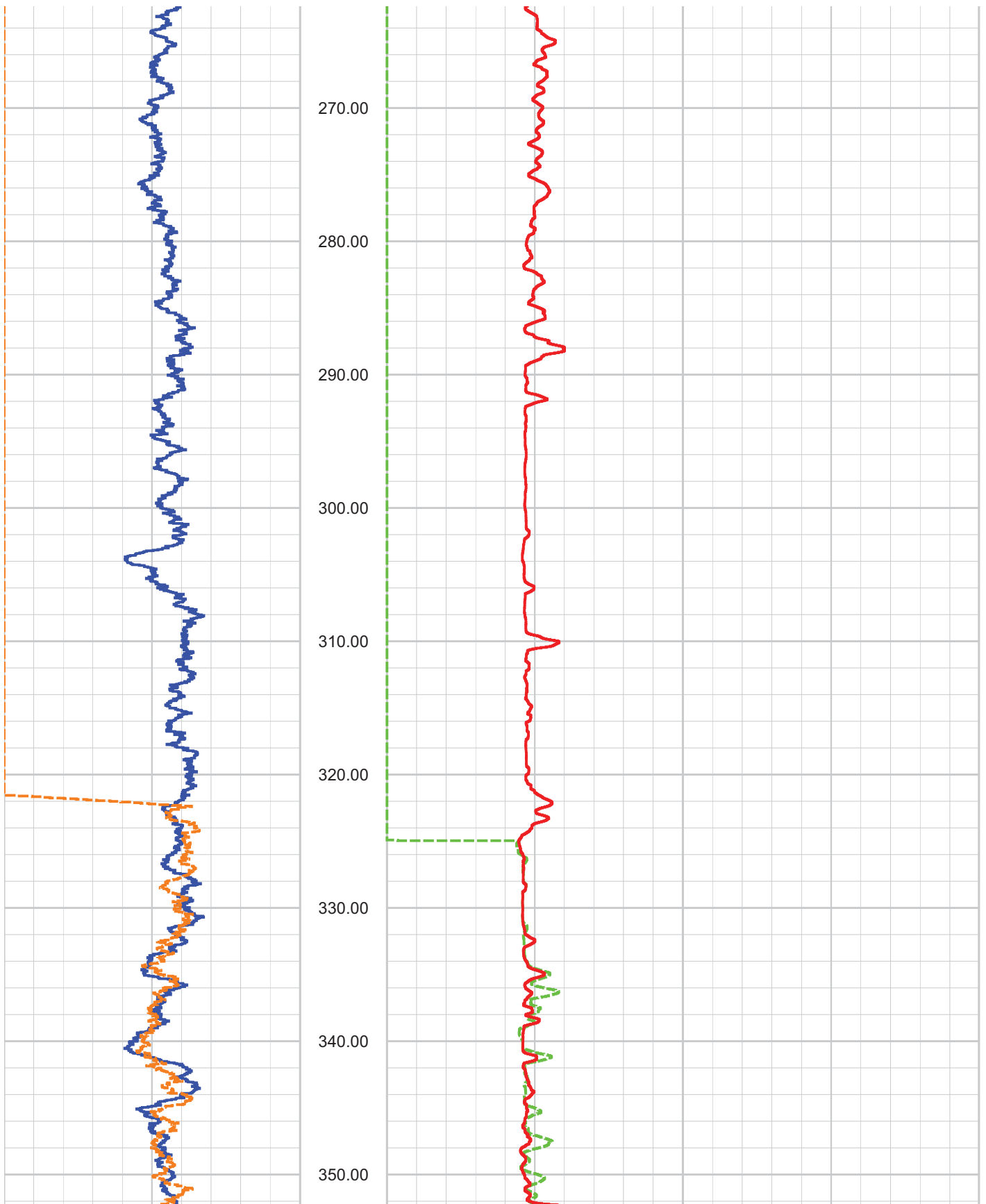




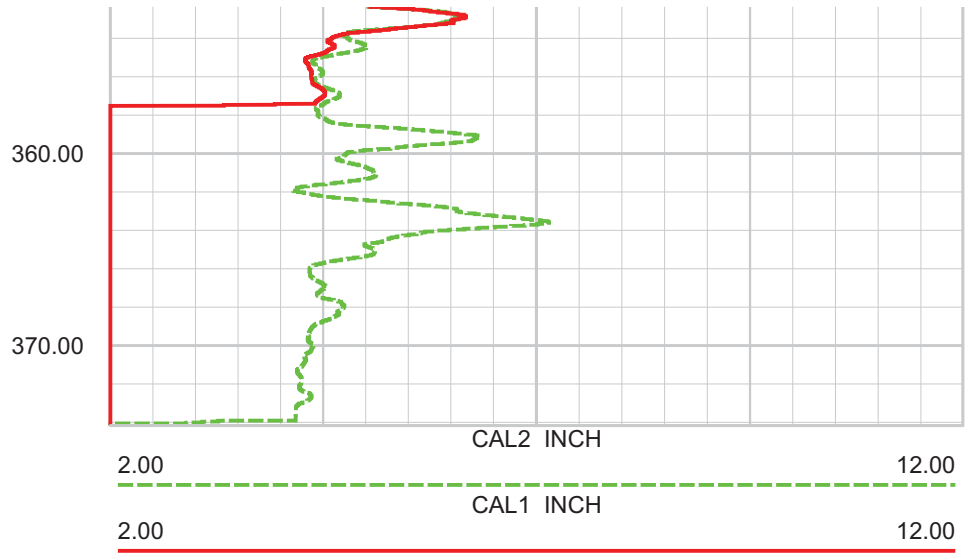
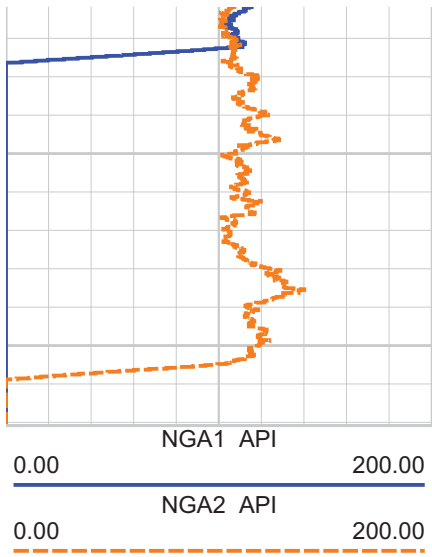
SR-710 Boring Z2-B4 Caliper and Natural Gamma rev 1.1 Sheet 2 of 5



SR-710 Boring Z2-B4 Caliper and Natural Gamma rev 1.1 Sheet 3 of 5

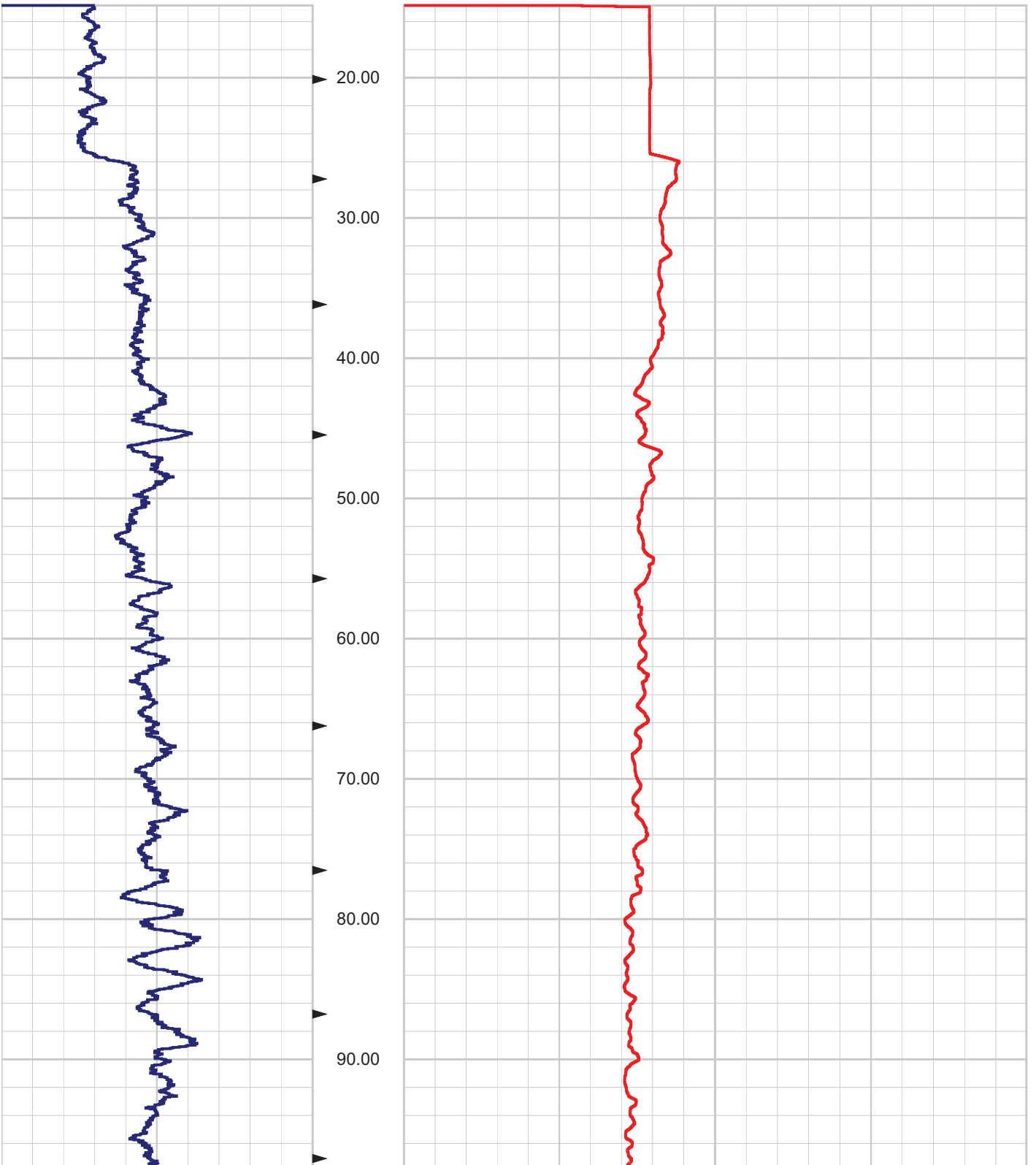


SR-710 Boring Z2-B4 Caliper and Natural Gamma rev 1.1 Sheet 4 of 5

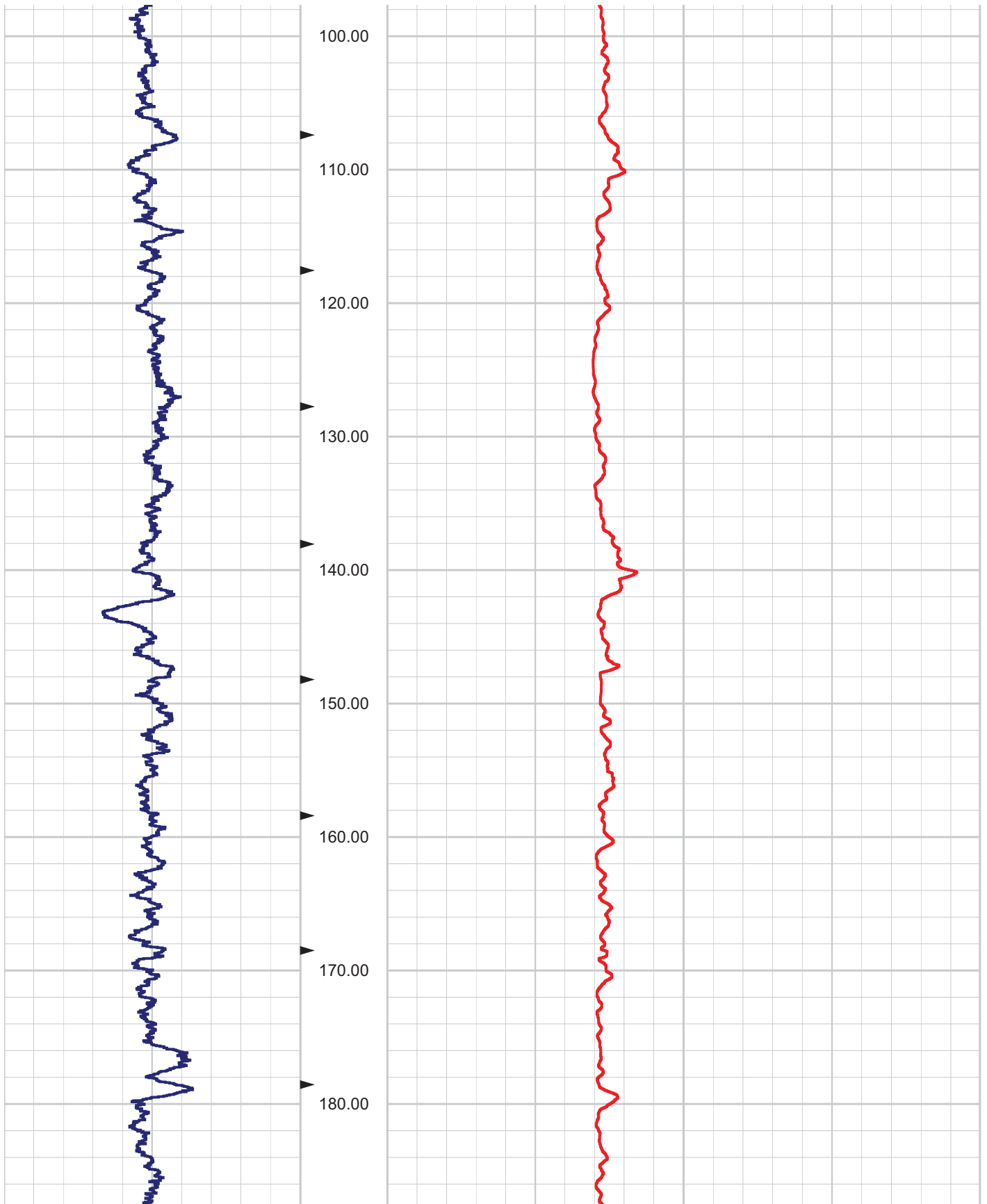


0.00 NGAM API Cs. 200.00

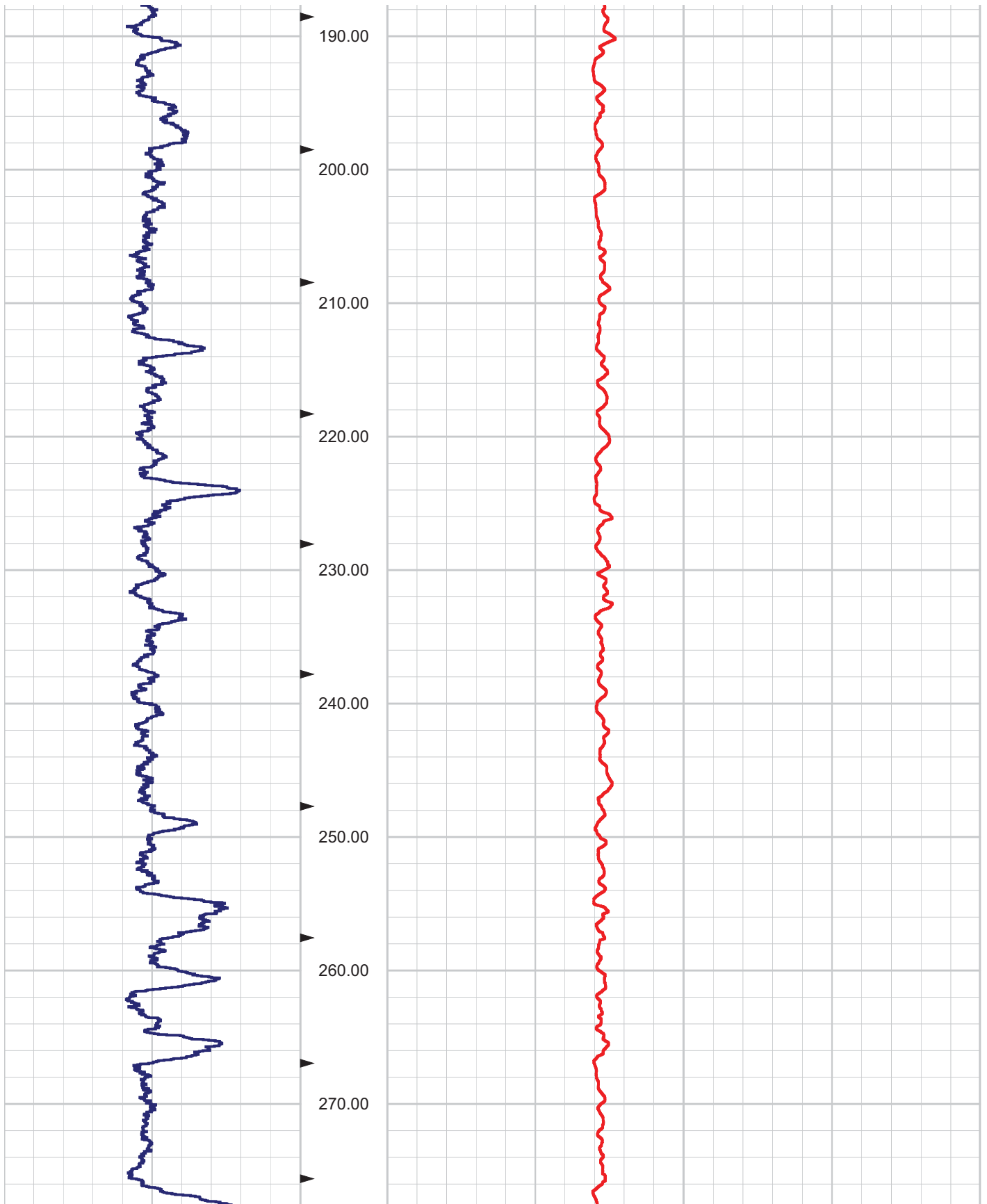
2.00 CALP Inch 12.00



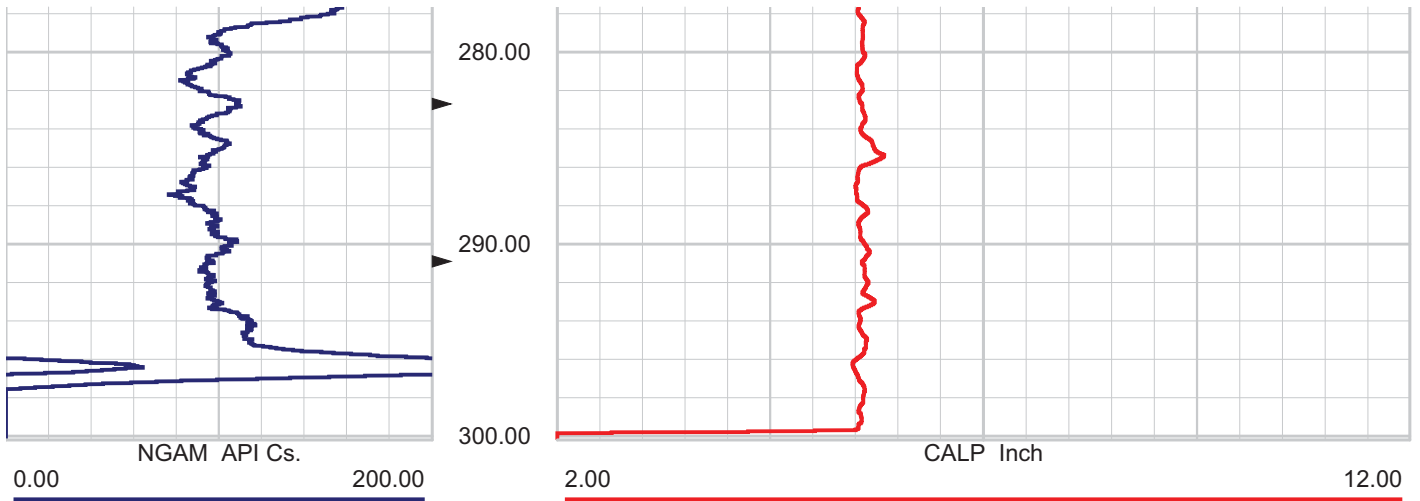
SR-710 Boring Z3-B1 Caliper and Natural Gamma rev 1.1 Sheet 1 of 4



SR-710 Boring Z3-B1 Caliper and Natural Gamma rev 1.1 Sheet 2 of 4



SR-710 Boring Z3-B1 Caliper and Natural Gamma rev 1.1 Sheet 3 of 4

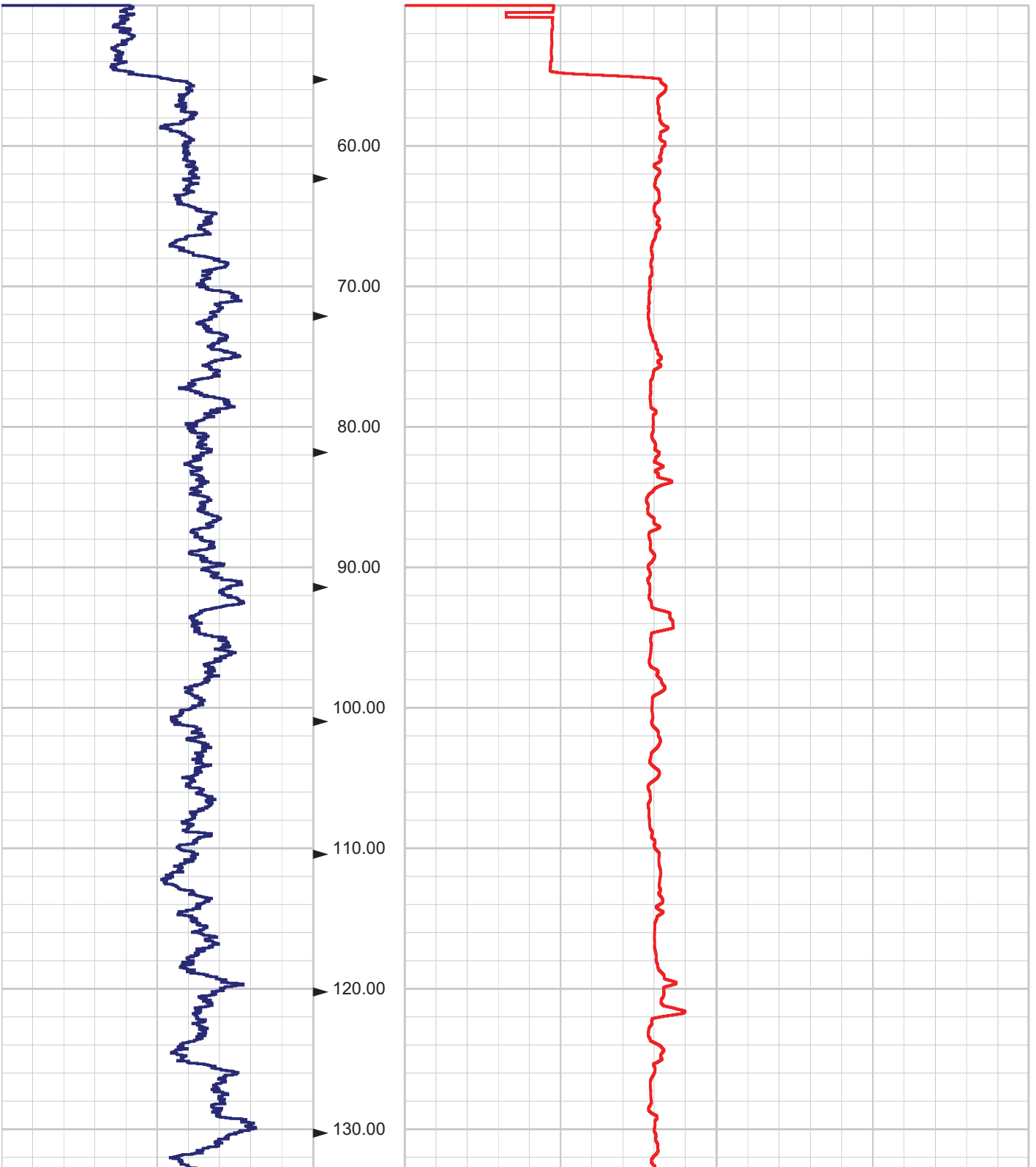


Depth: 14.00 ft Date: 19 Mar 2009 Time: 09:20:44 File: "C:\Winlogger401\Data\SR710\Z3-B1\Z3B1CALUP01.LOG"

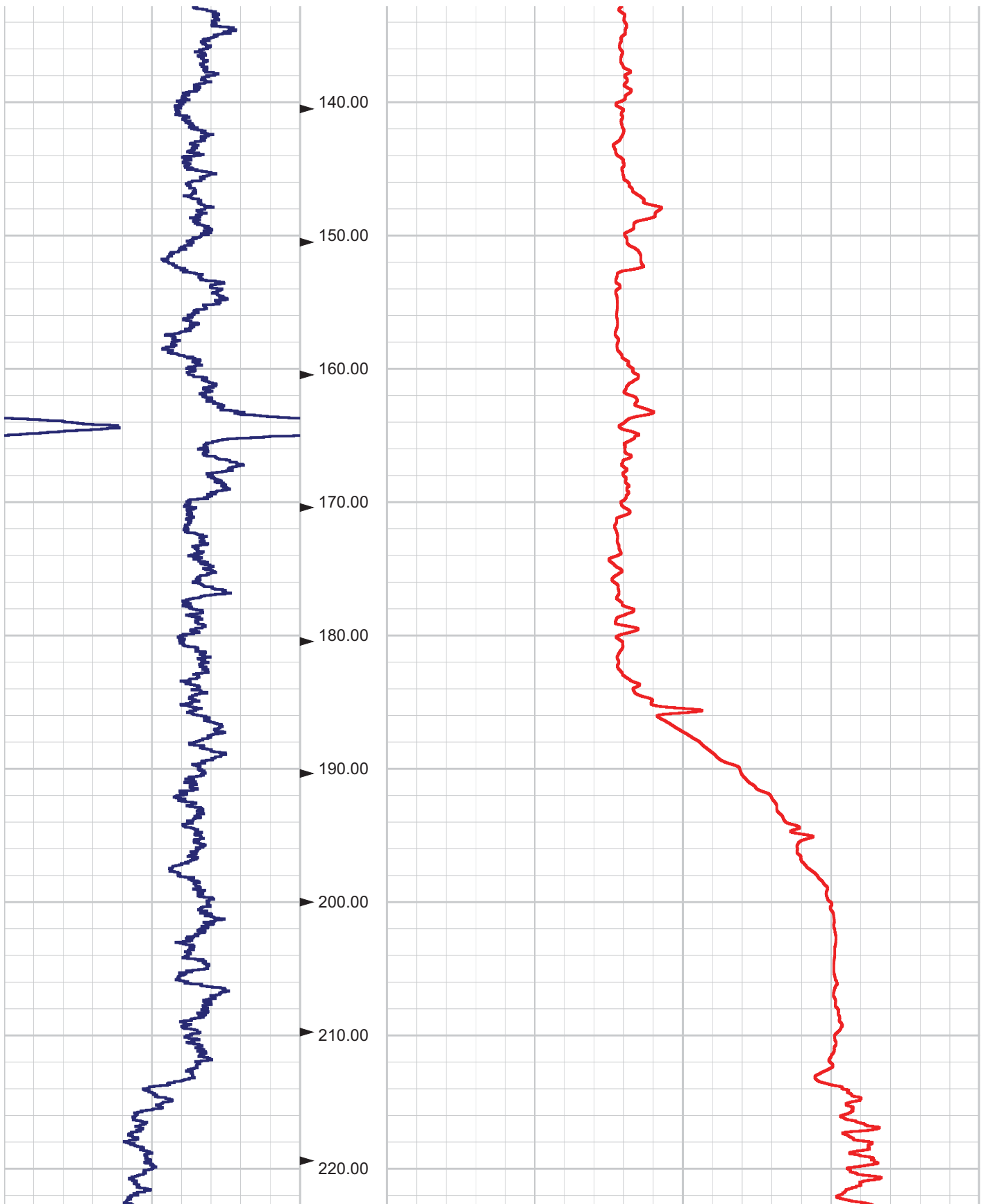


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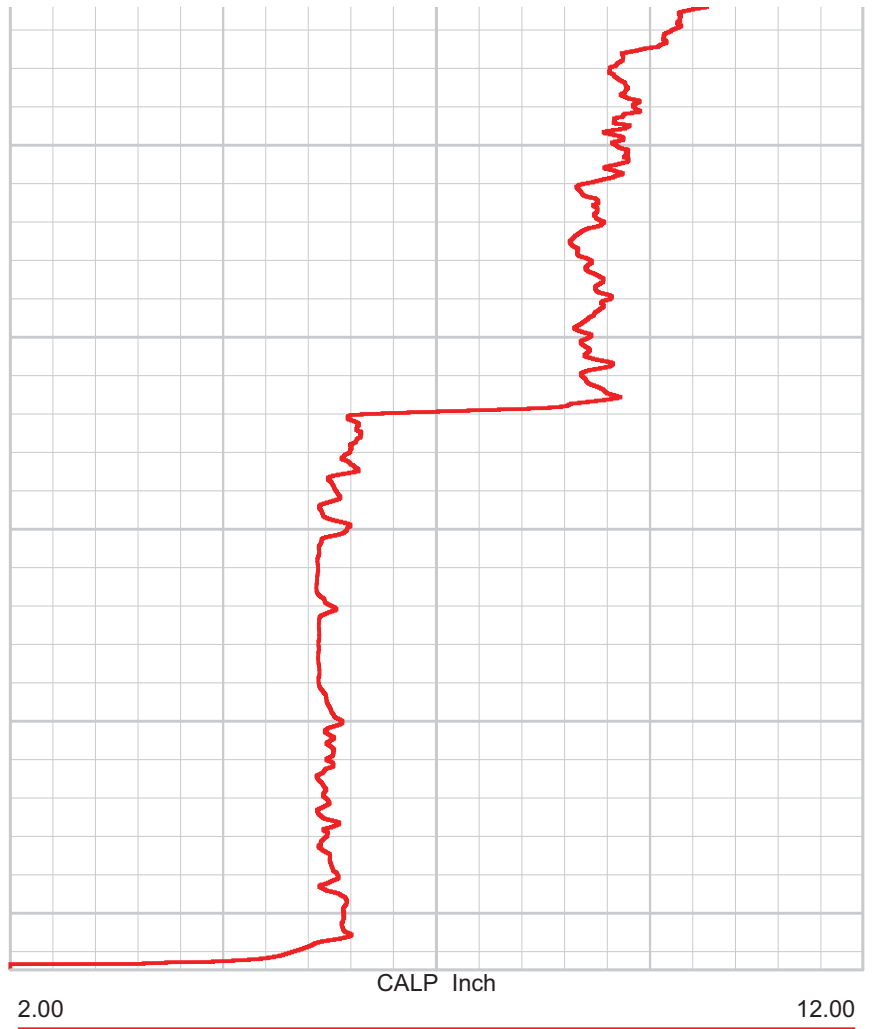
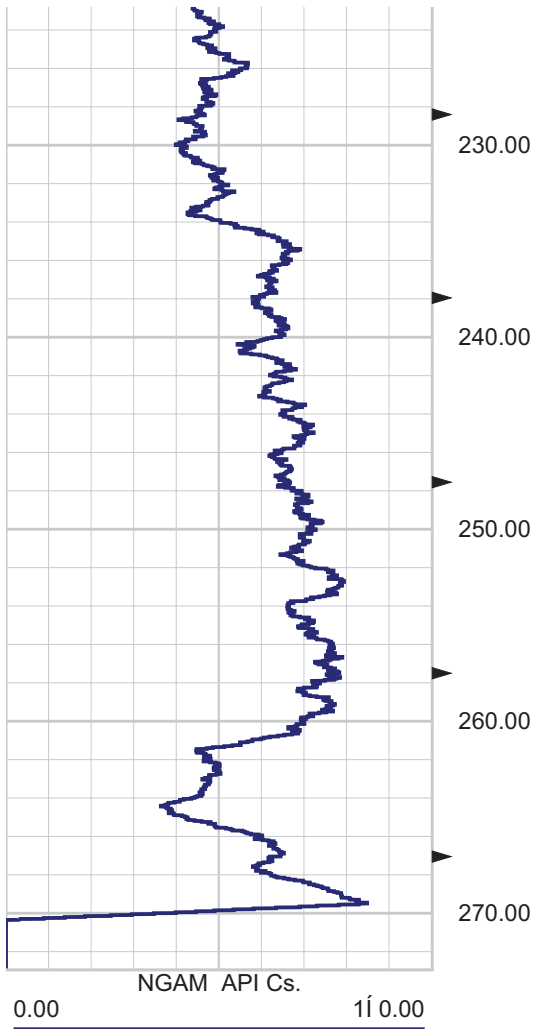
2.00 CALP Inch 12.00



SR-710 Boring Z3-B3 Caliper and Natural Gamma rev 1.1 Sheet 1 of 3

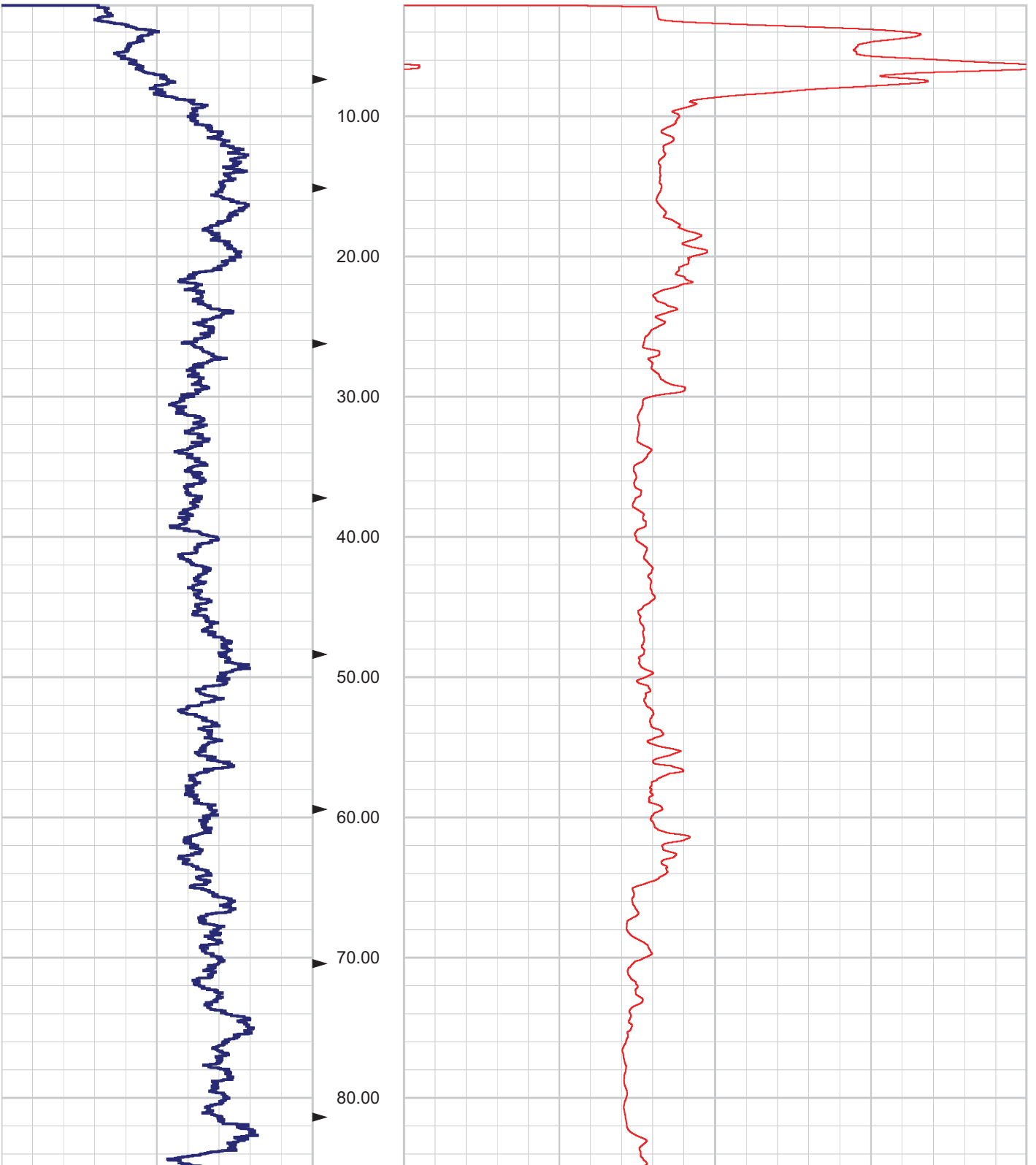


SR-710 Boring Z3-B3 Caliper and Natural Gamma rev 1.1 Sheet 2 of 3

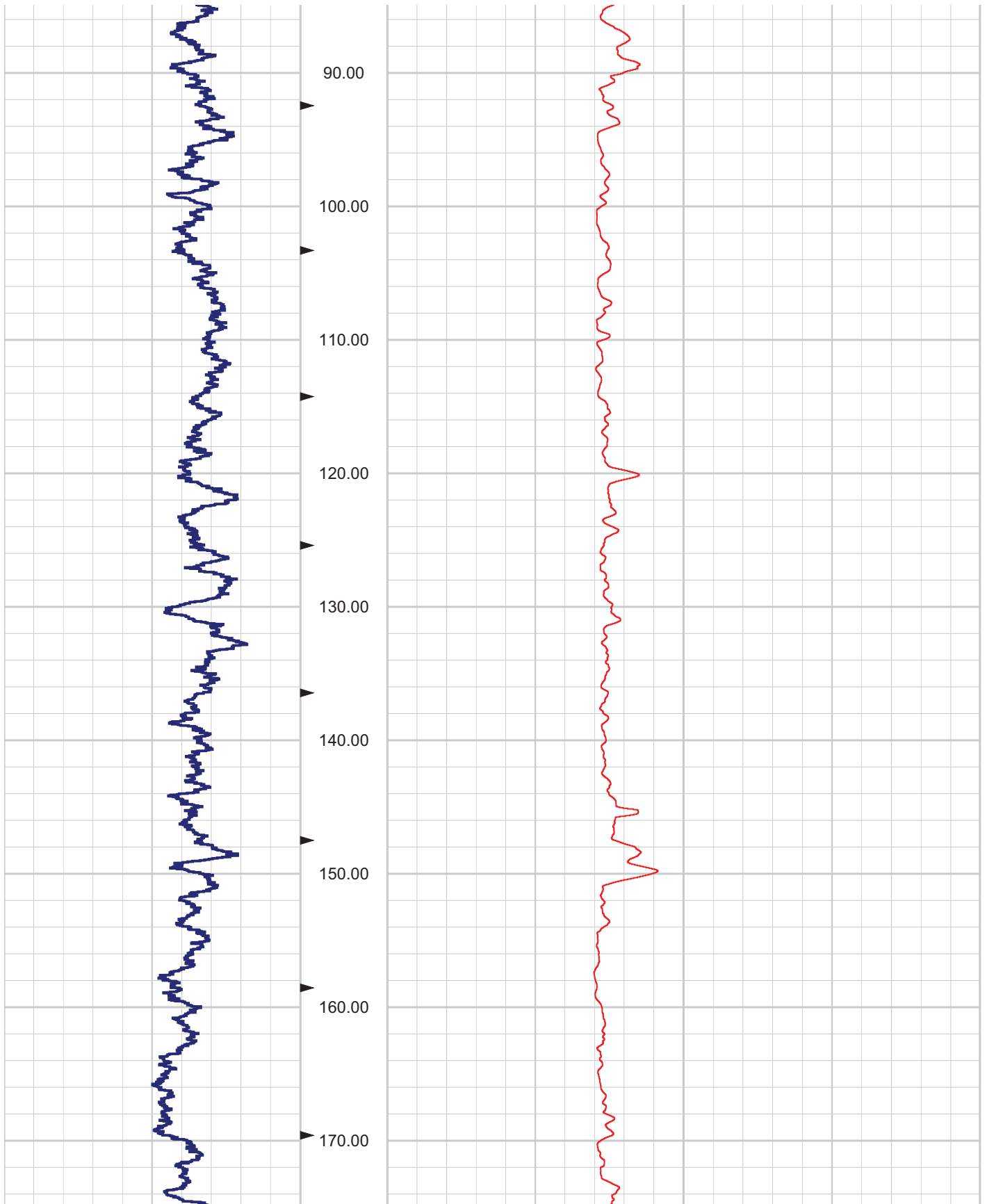


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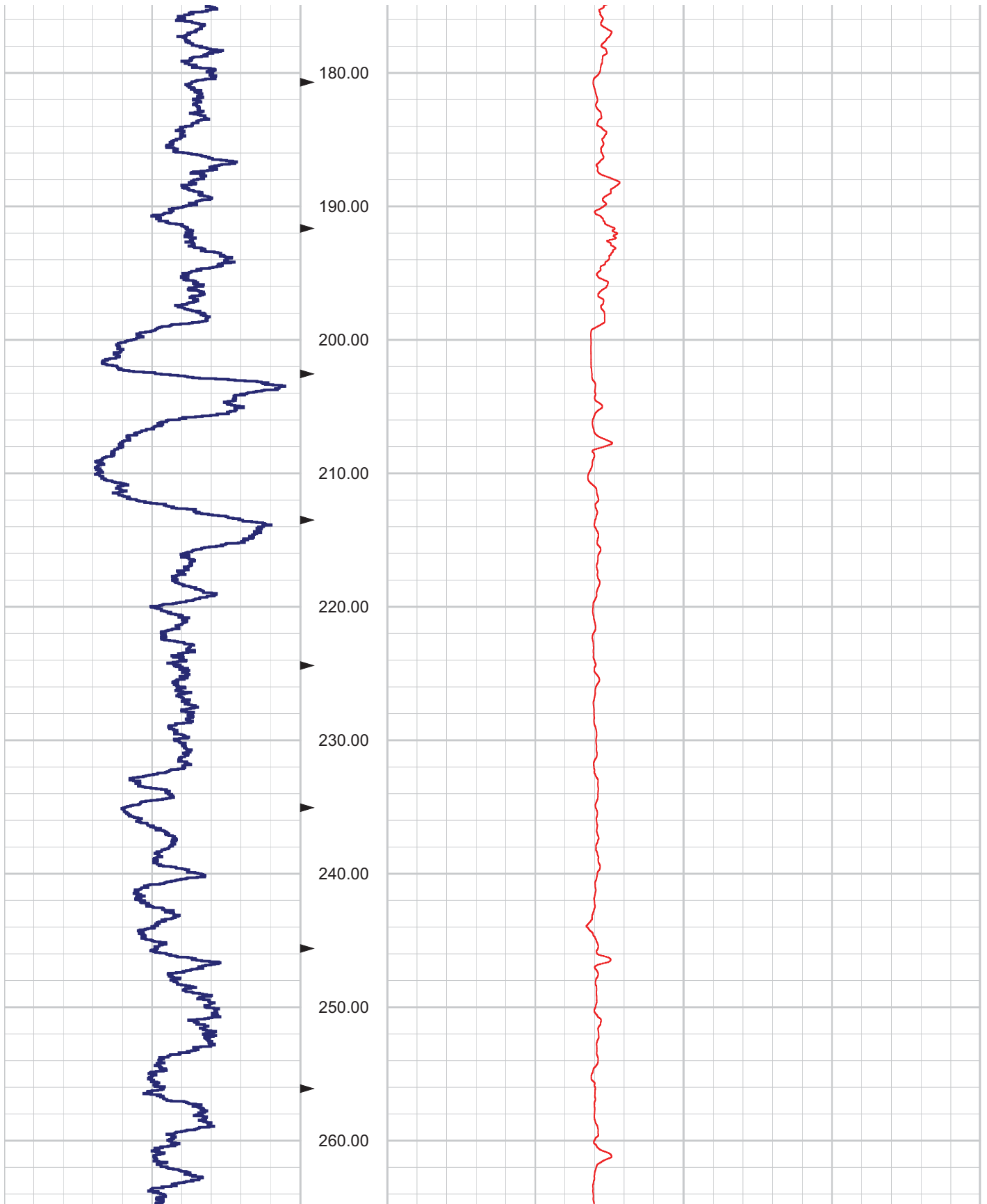
2.00 CALP Inch 12.00



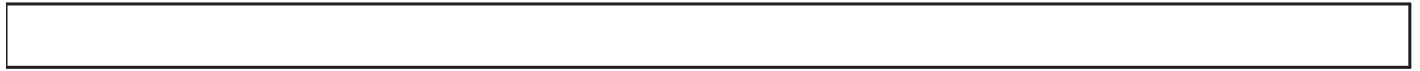
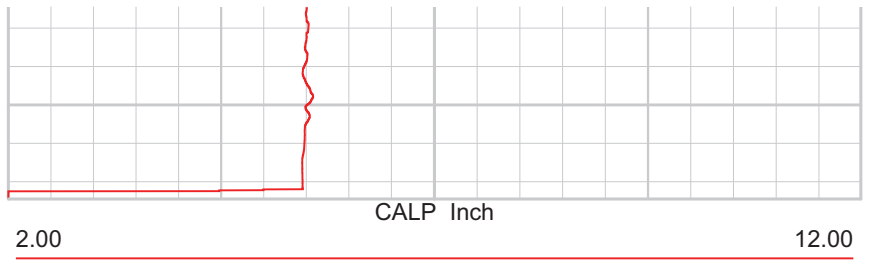
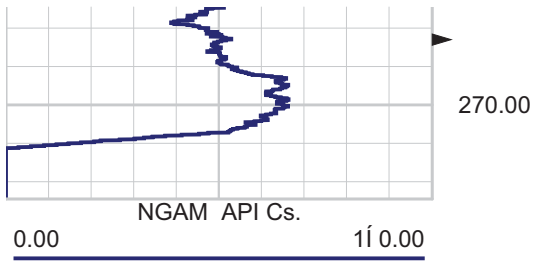
SR-710 Boring Z3-B4 Caliper and Natural Gamma rev 1.1 Sheet 1 of 4



SR-710 Boring Z3-B4 Caliper and Natural Gamma rev 1.1 Sheet 2 of 4

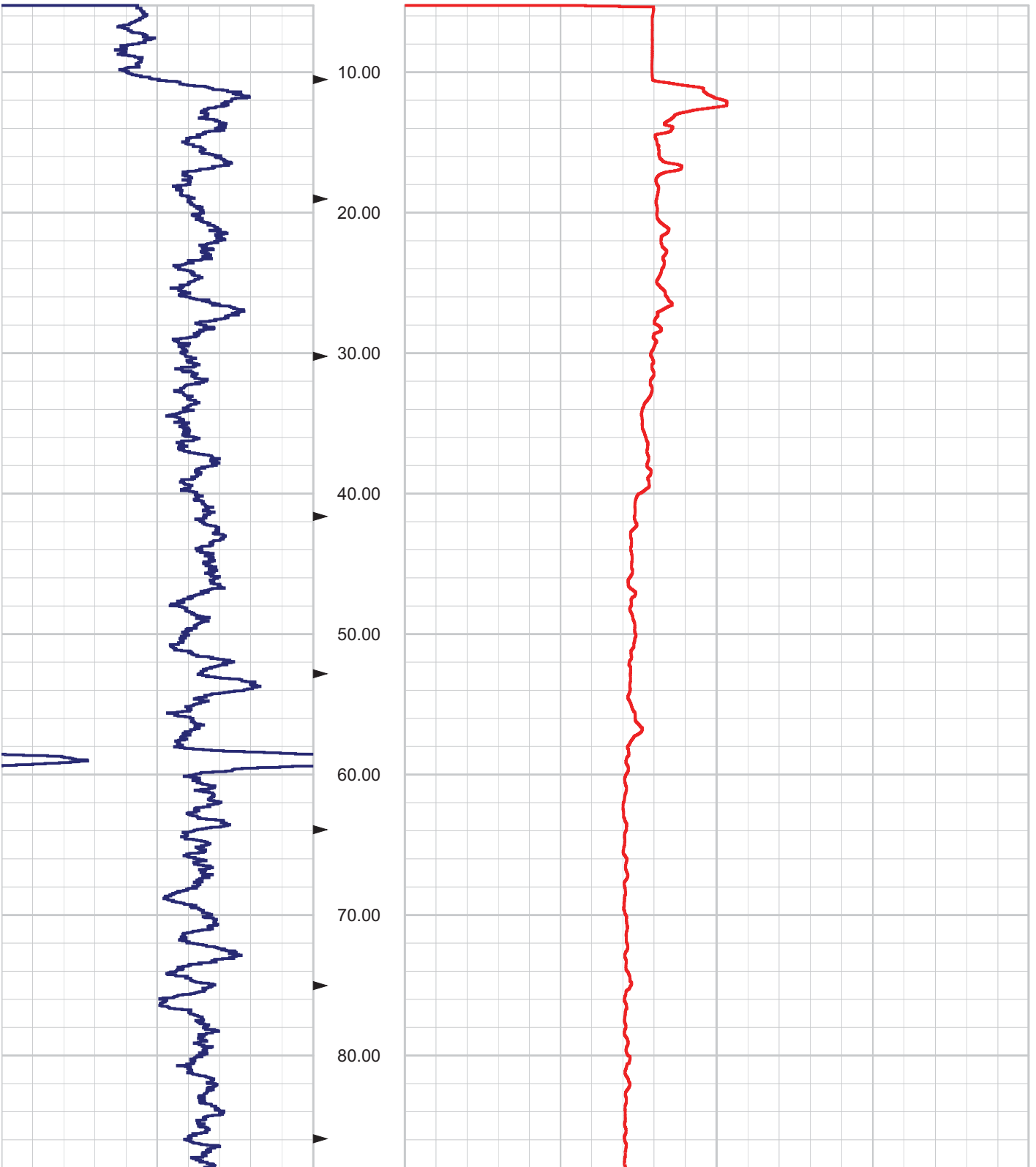


SR-710 Boring Z3-B4 Caliper and Natural Gamma rev 1.1 Sheet 3 of 4



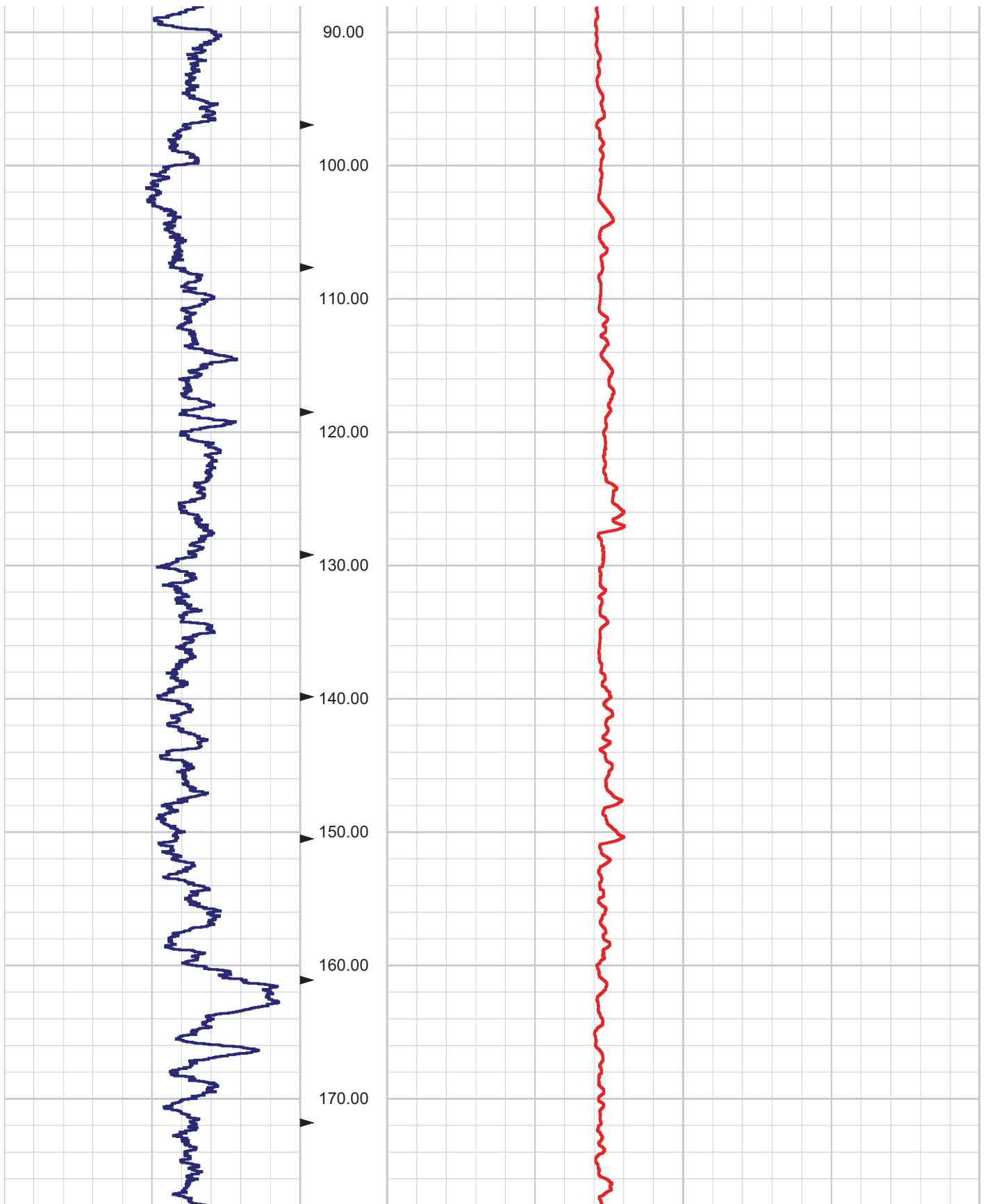
0.00 NGAM API Cs. 11 0.00

2.00 CALP Inch 12.00

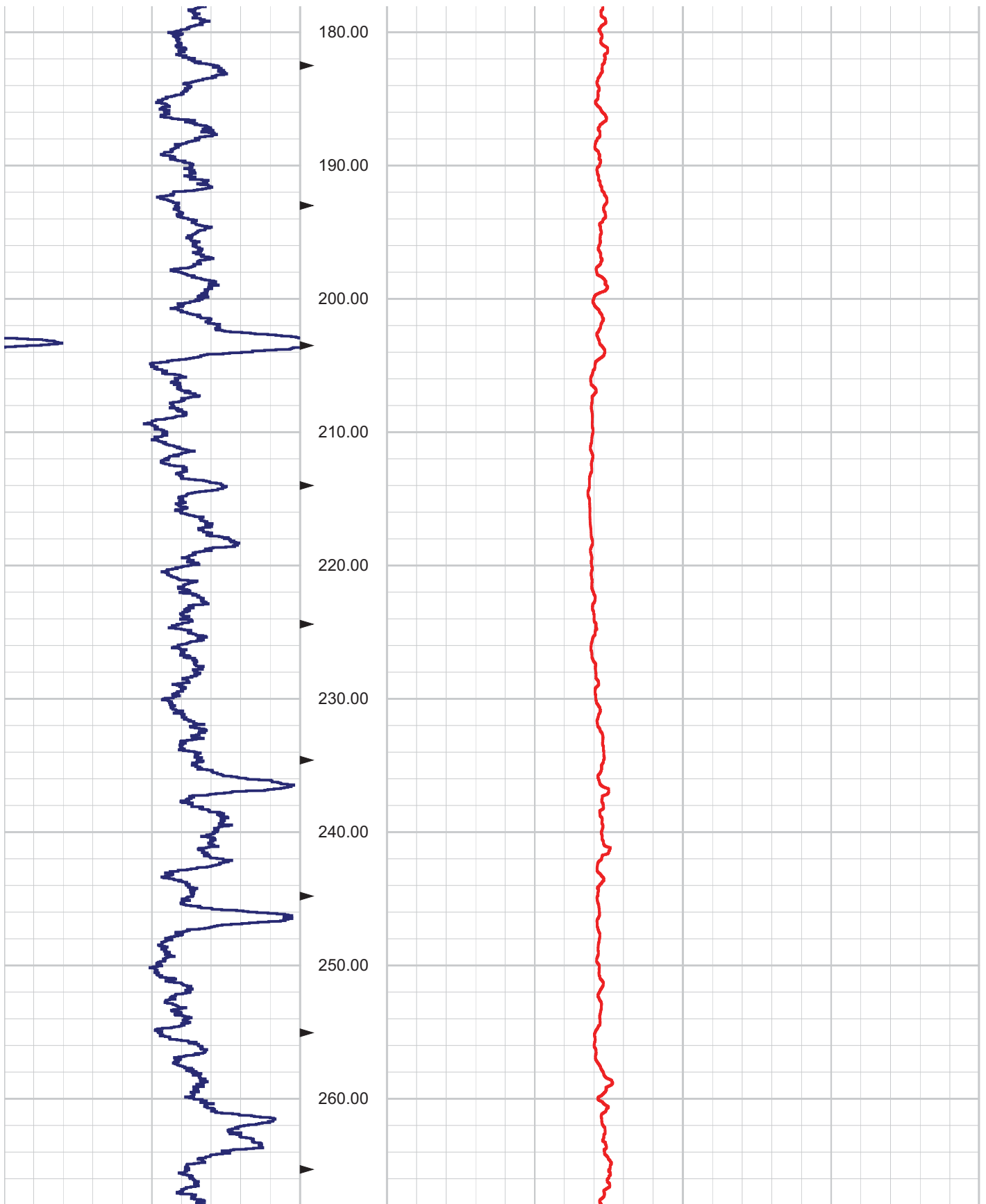


SR-710 Boring Z3-B6 Caliper and Natural Gamma rev 1.1 Sheet 1 of 4

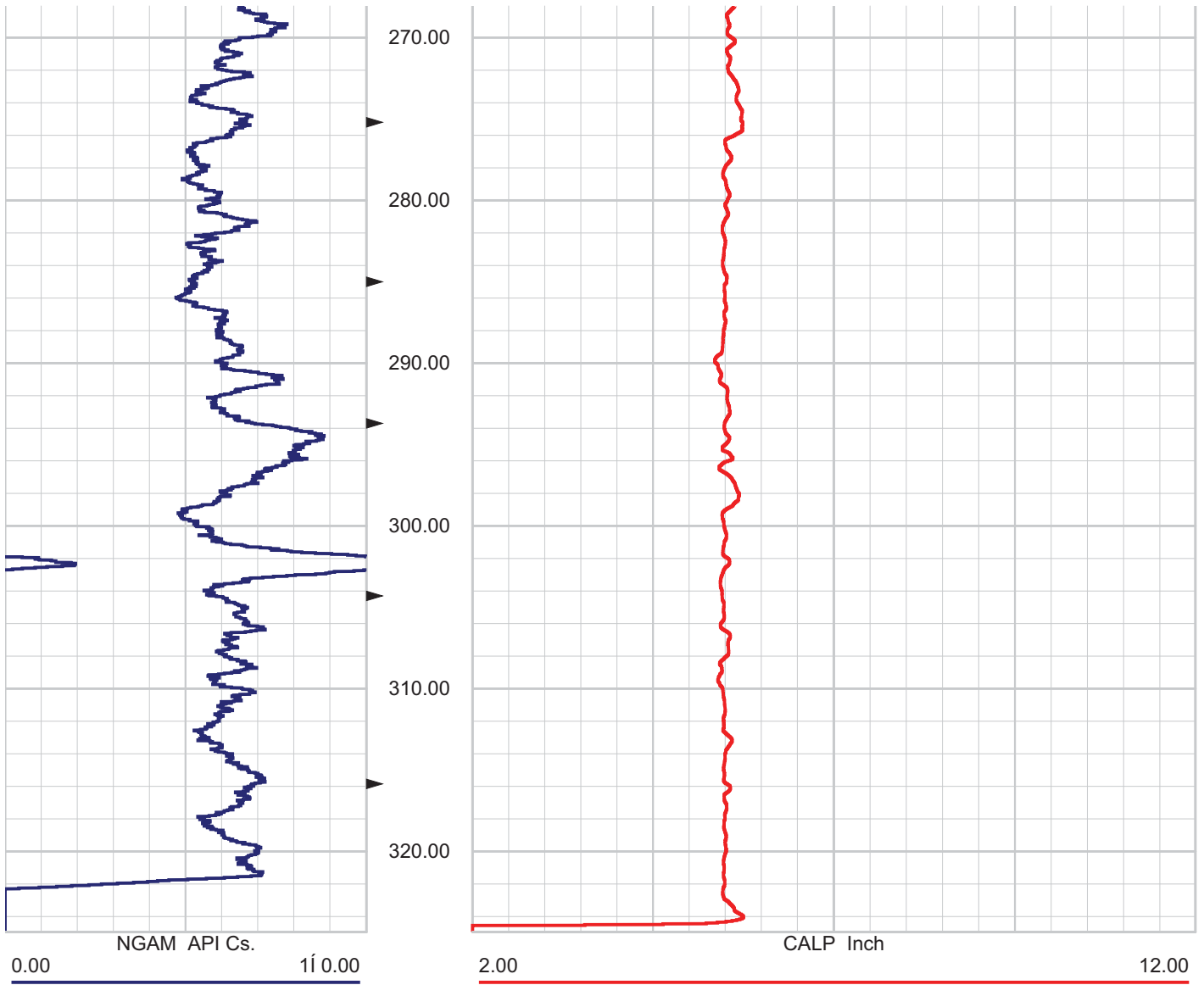




SR-710 Boring Z3-B6 Caliper and Natural Gamma rev 1.1 Sheet 2 of 4

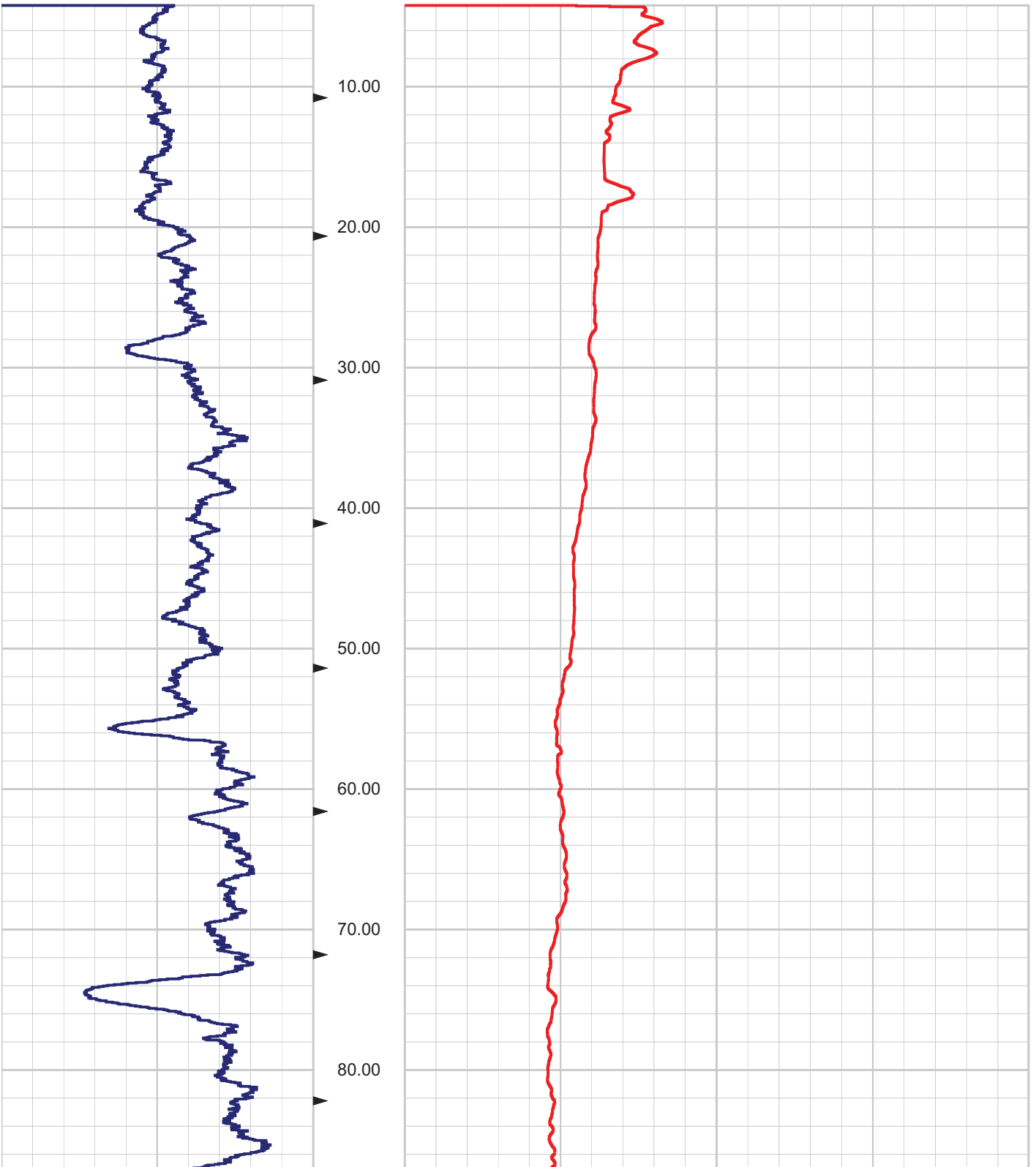


SR-710 Boring Z3-B6 Caliper and Natural Gamma rev 1.1 Sheet 3 of 4

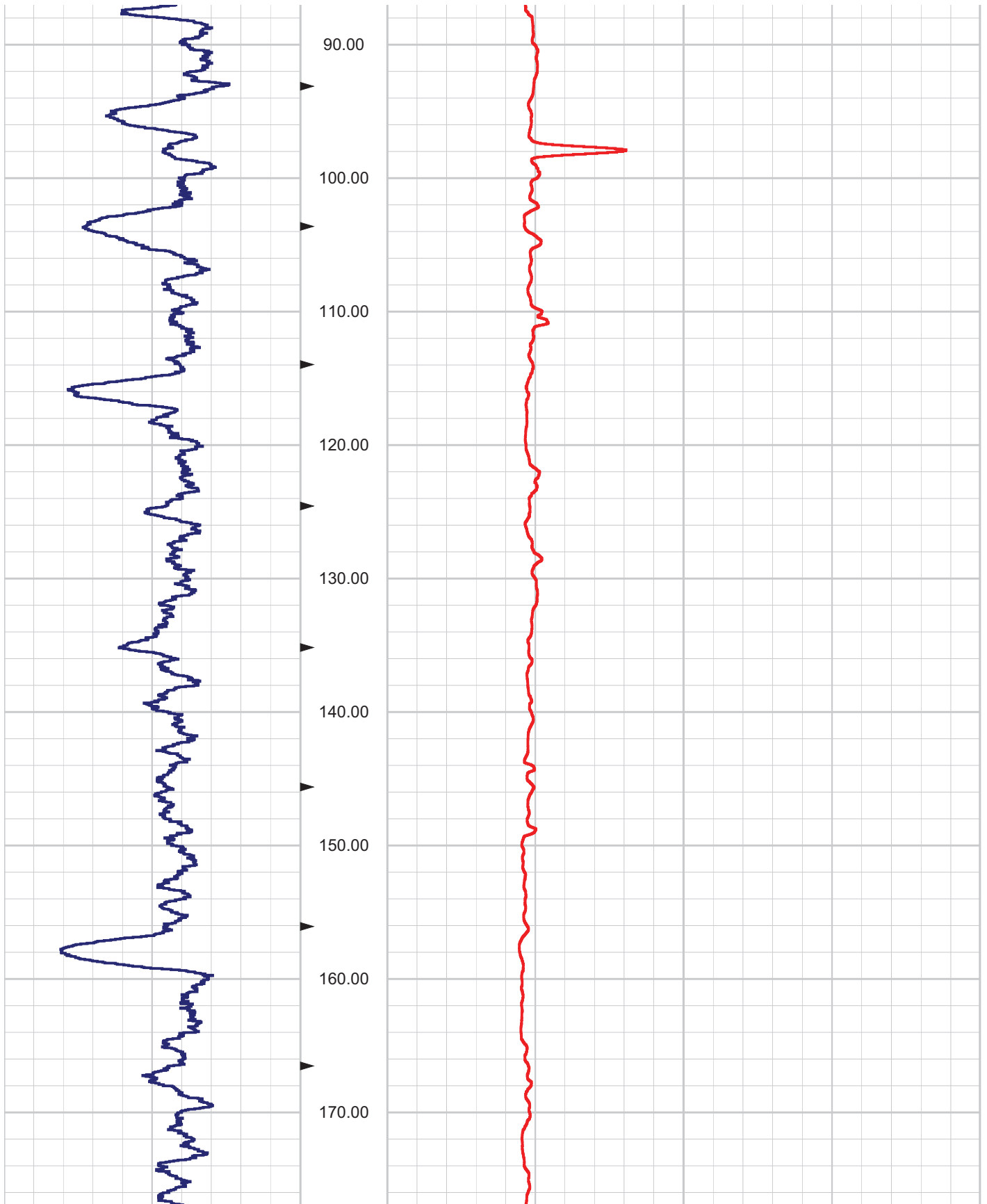


0.00 NGAM API Cs. 200.00

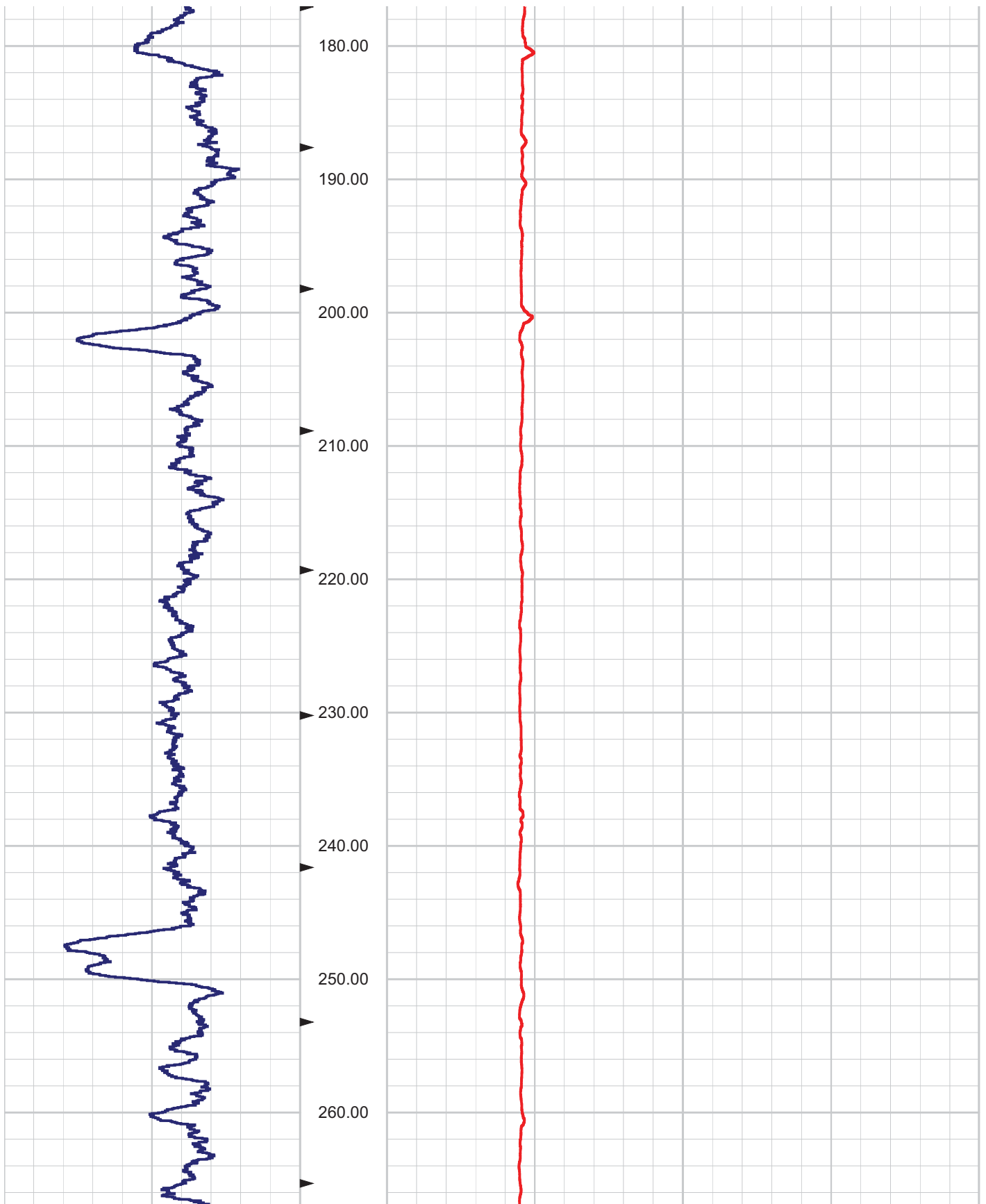
2.00 CALP Inch 12.00



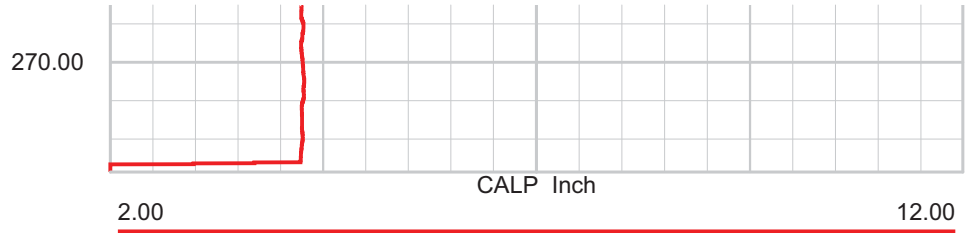
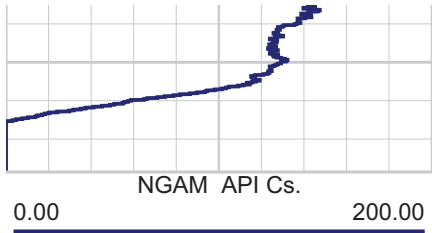
SR-710 Boring Z3-B8 Caliper and Natural Gamma rev 1.1 Sheet 1 of 4



SR-710 Boring Z3-B8 Caliper and Natural Gamma rev 1.1 Sheet 2 of 4

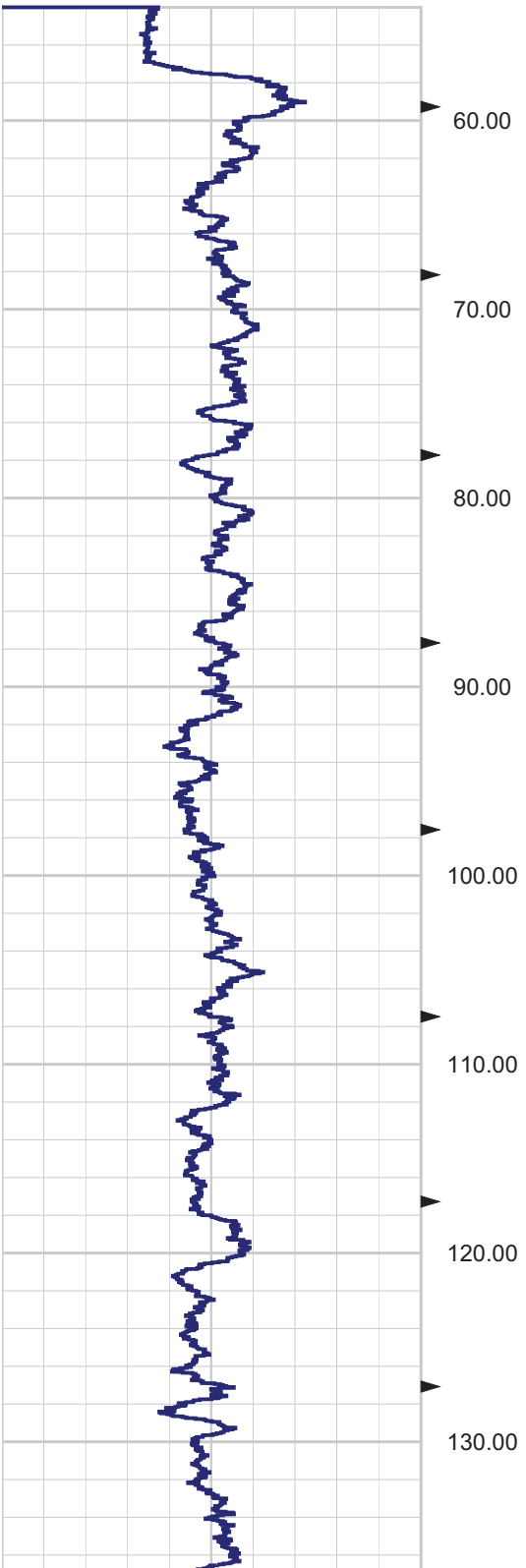


SR-710 Boring Z3-B8 Caliper and Natural Gamma rev 1.1 Sheet 3 of 4

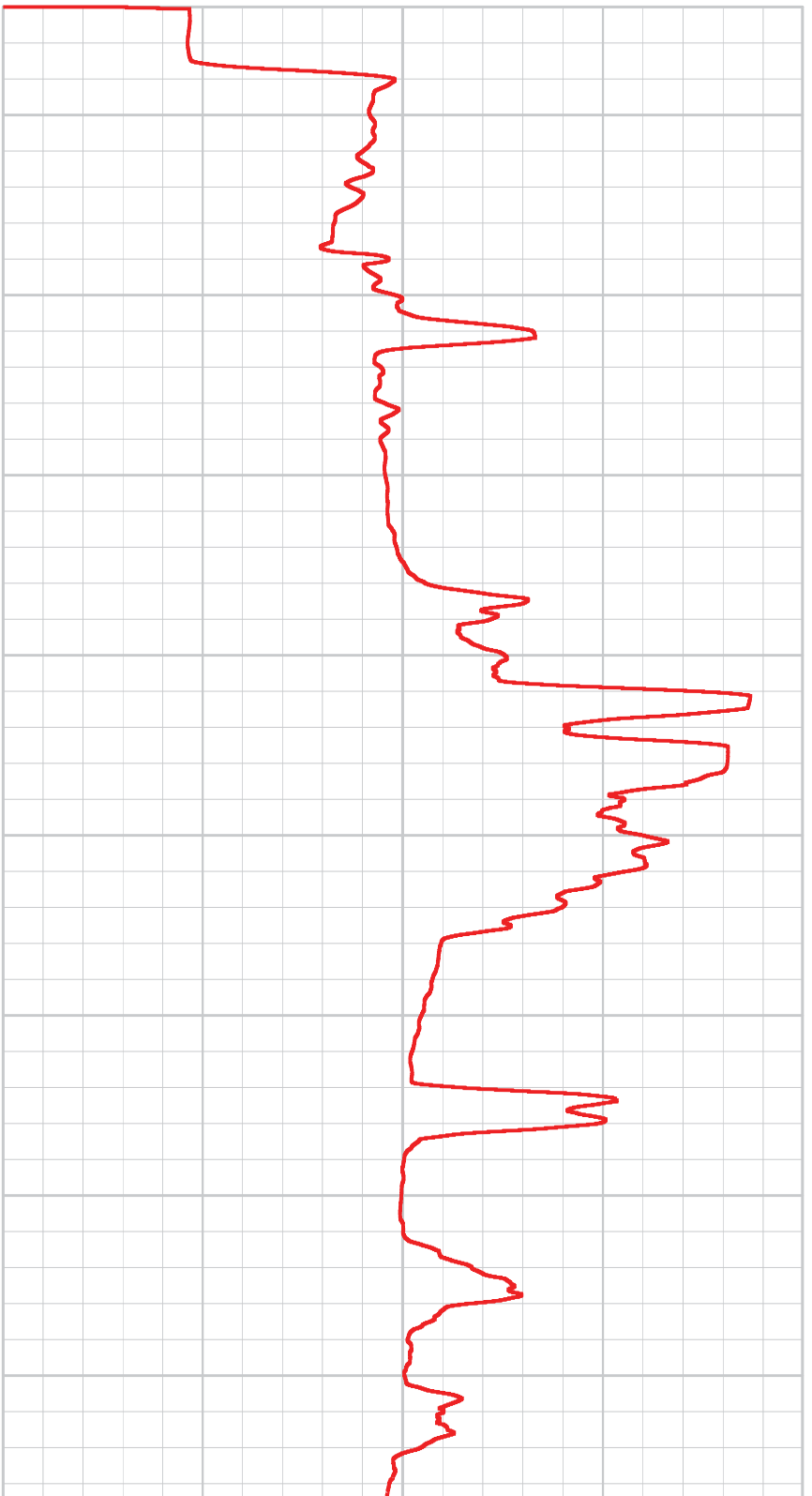


Depth: 3.00 ft Date: 23 Mar 2009 Time: 14:16:54 File: "C:\Winlogger401\Data\SR710\Z3-B8\Z3B8CALUP01.LOG"

0.00 NGAM API Cs. 11 0.00

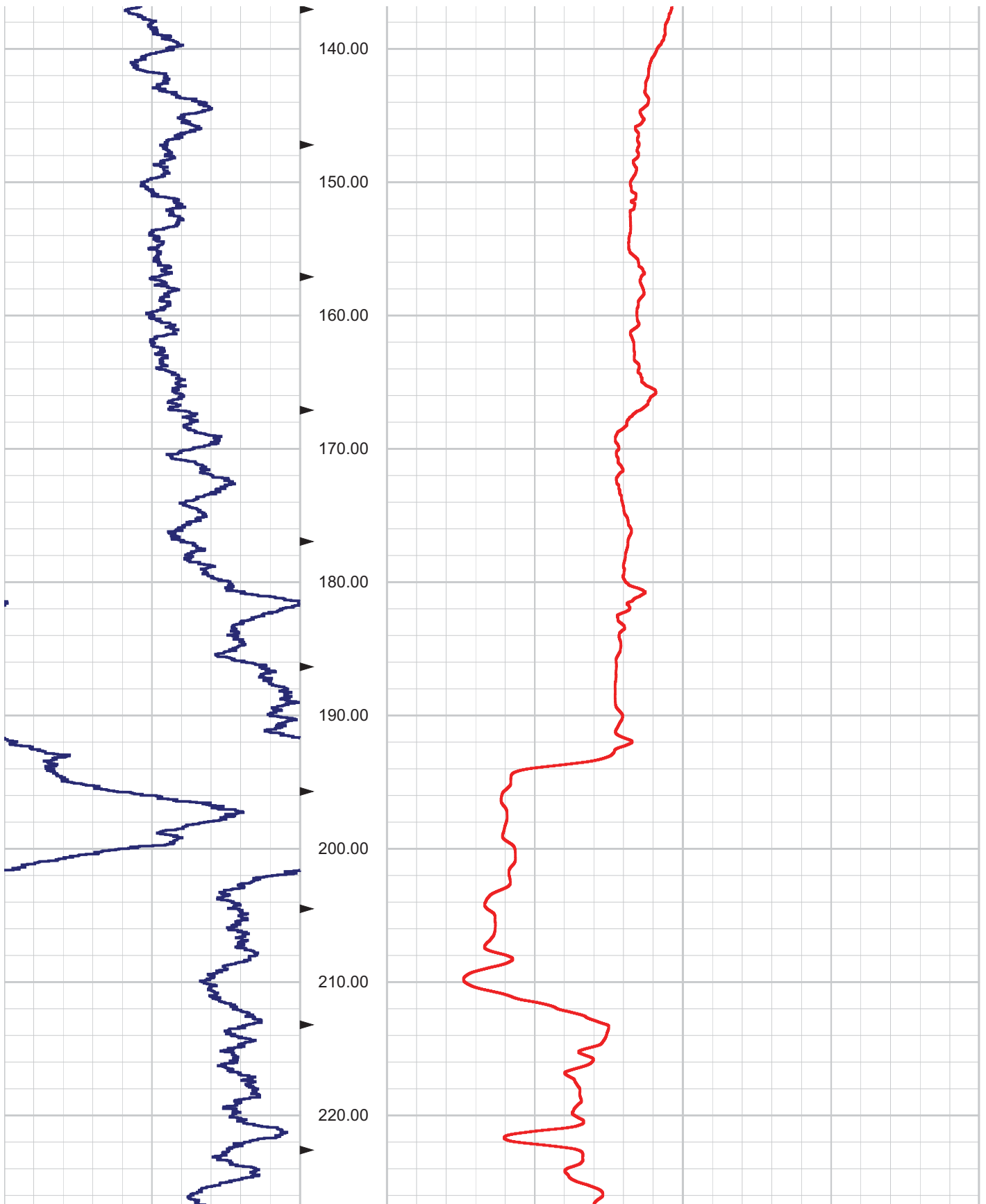


2.00 CALP Inch 12.00

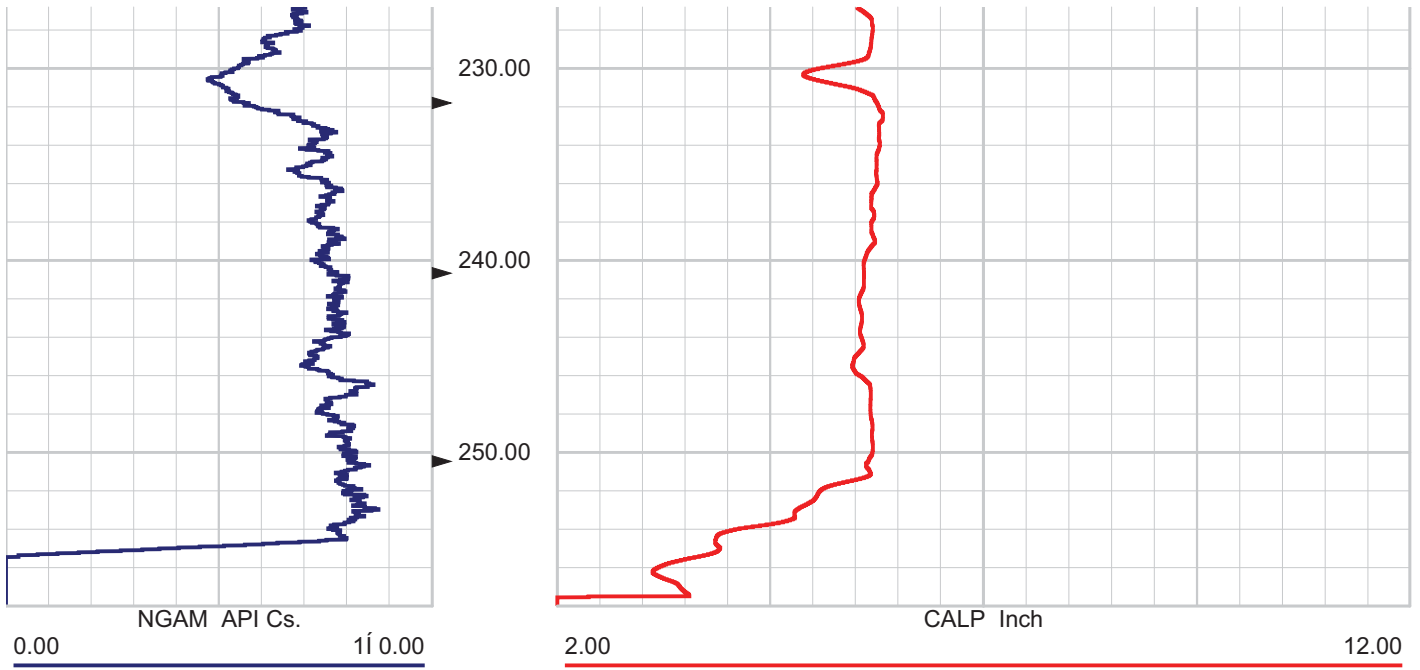


SR-710 Boring Z3-B12 Caliper and Natural Gamma rev 1.1 Sheet 1 of 3



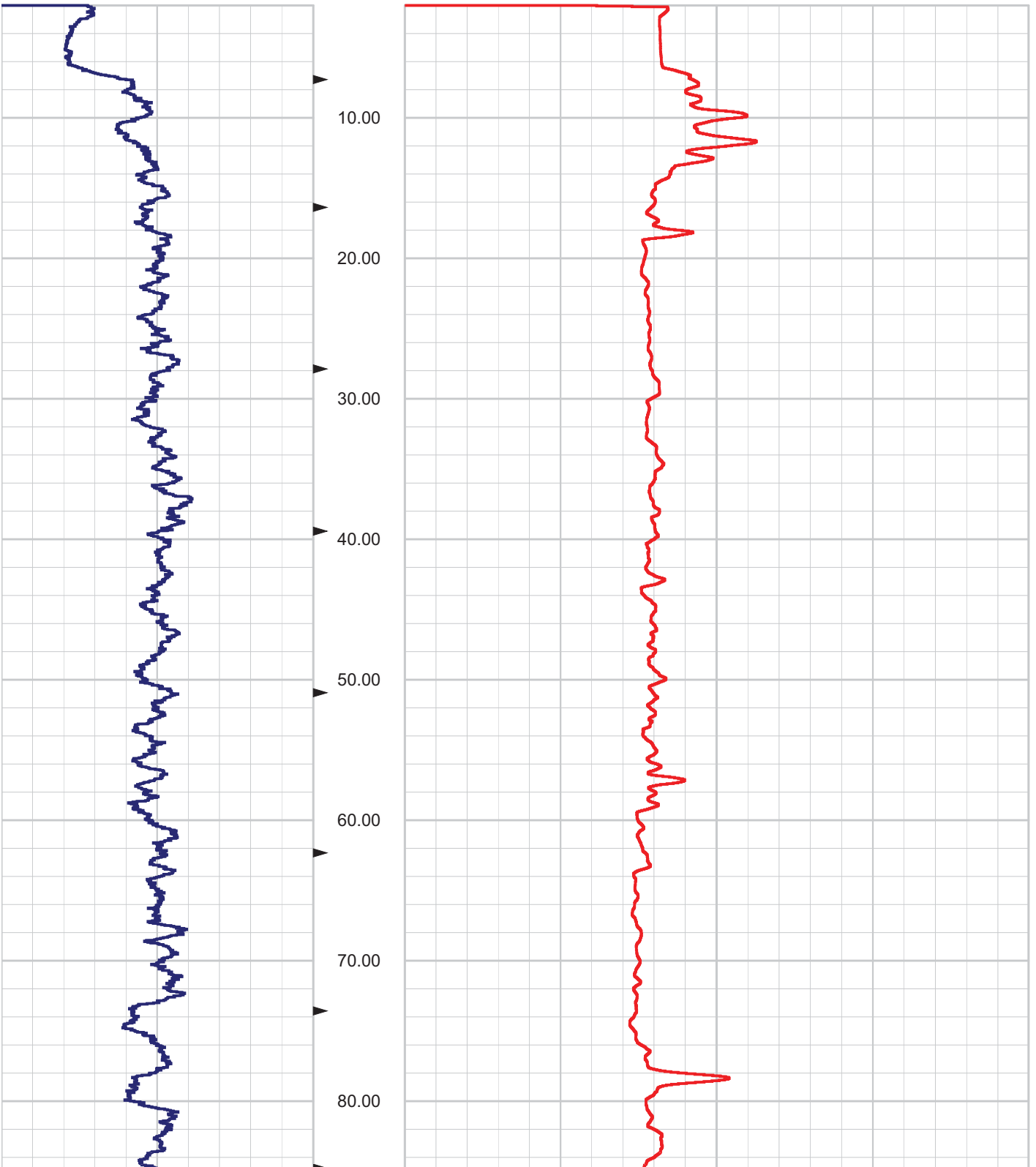


SR-710 Boring Z3-B12 Caliper and Natural Gamma rev 1.1 Sheet 2 of 3

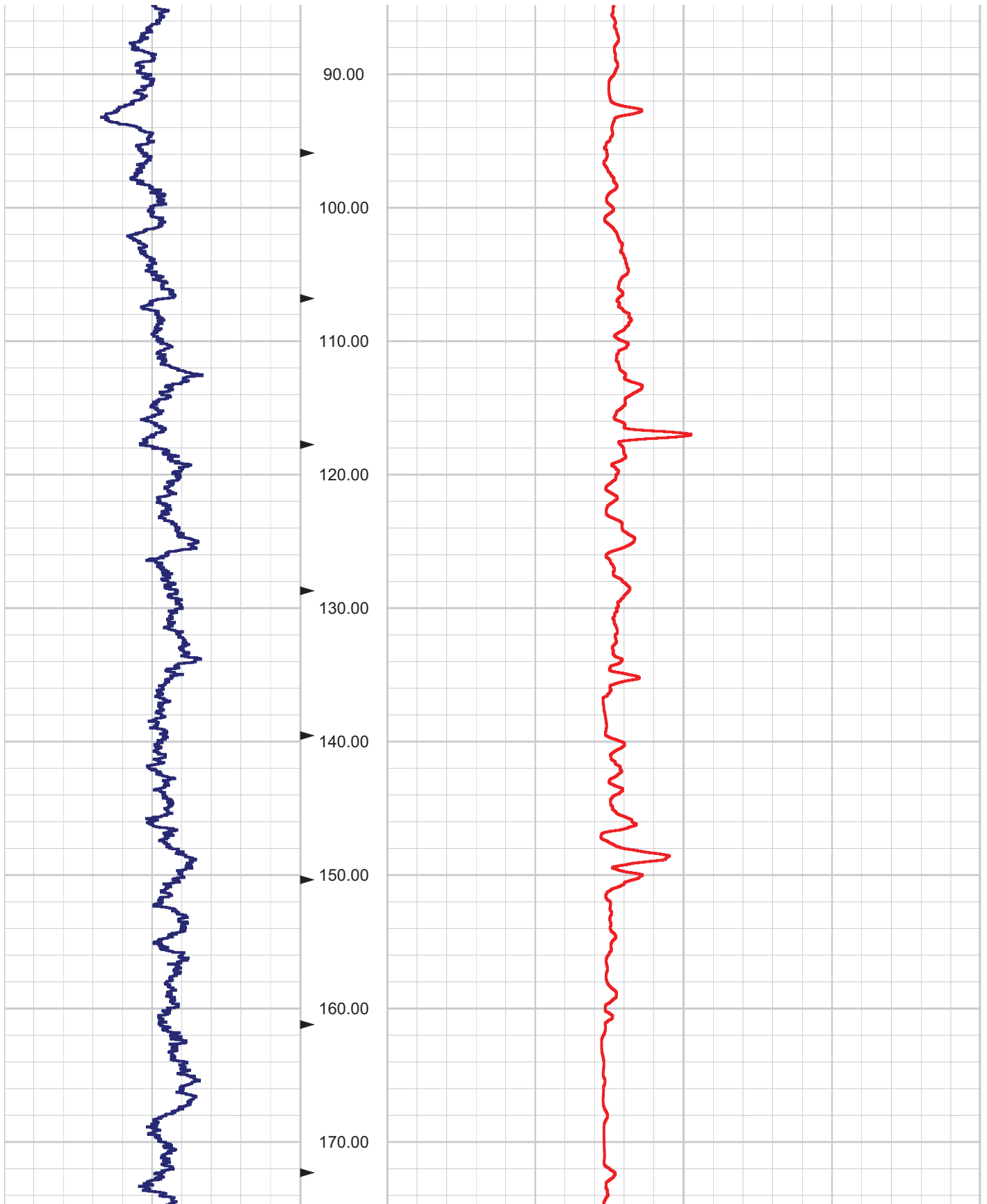


0.00 NGAM API Cs. 200.00

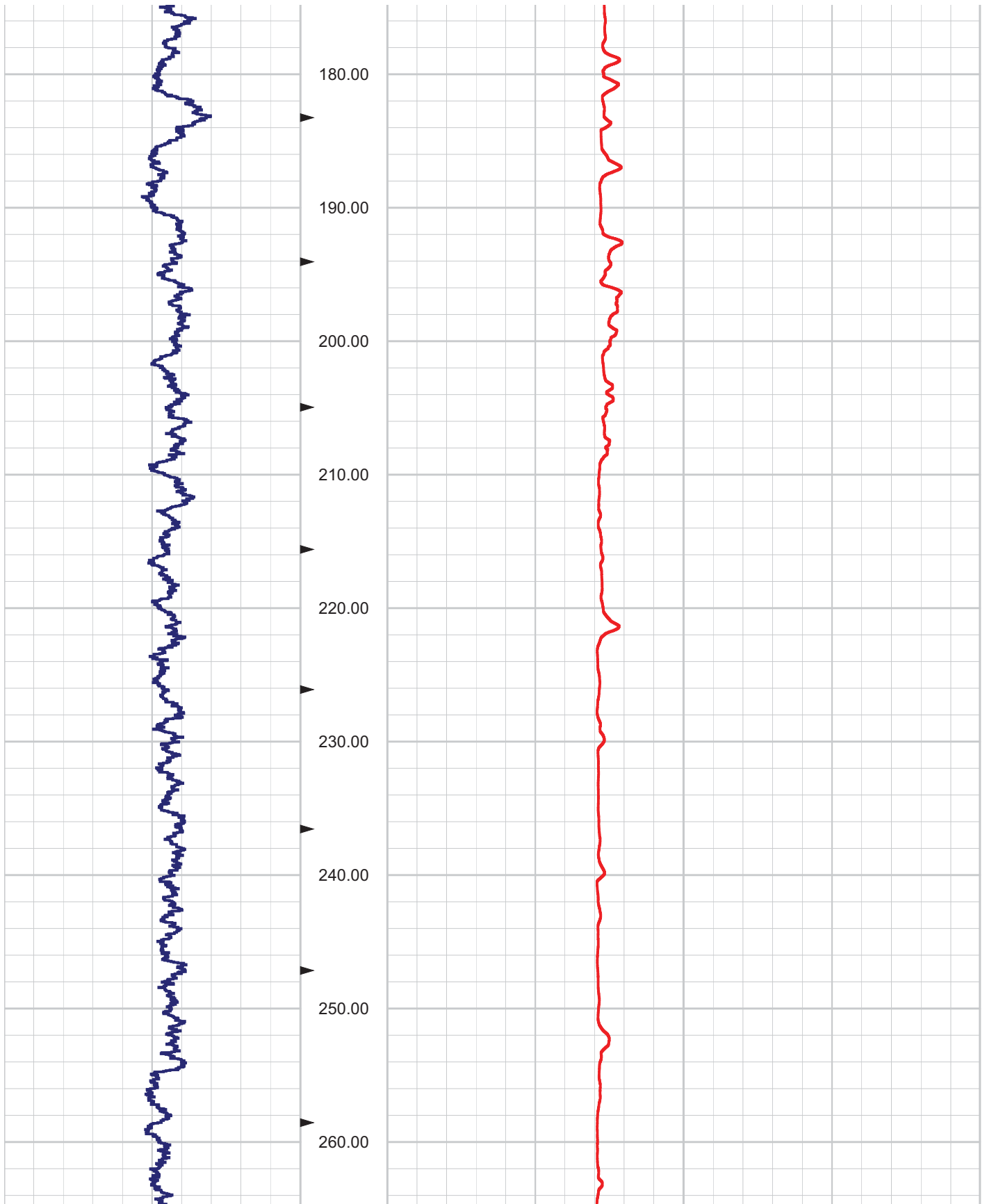
2.00 CALP Inch 12.00



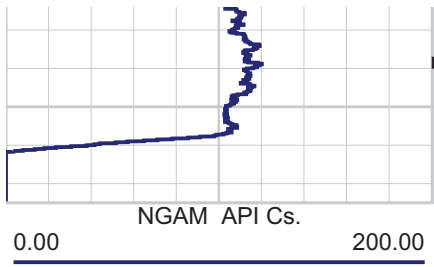
SR-710 Boring Z4-B4 Caliper and Natural Gamma rev 1.1 Sheet 1 of 4



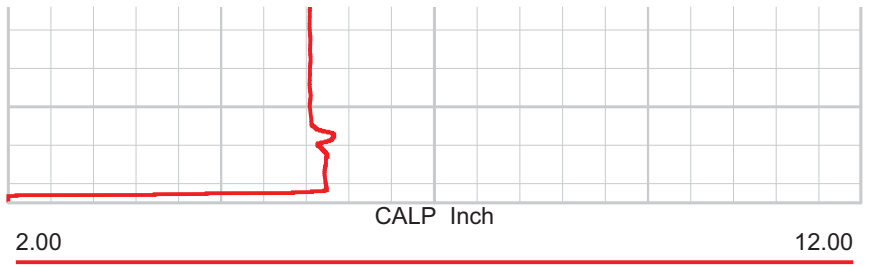
SR-710 Boring Z4-B4 Caliper and Natural Gamma rev 1.1 Sheet 2 of 4



SR-710 Boring Z4-B4 Caliper and Natural Gamma rev 1.1 Sheet 3 of 4



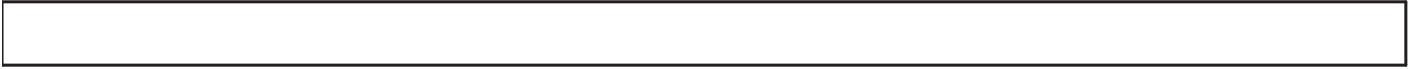
270.00



CALP Inch

0.00 200.00

2.00 12.00



**APPENDIX C**

**ACOUSTIC TELEVIEWER DIPS LOGS**



CASCADE DRILLING

Borehole: Z1-B3

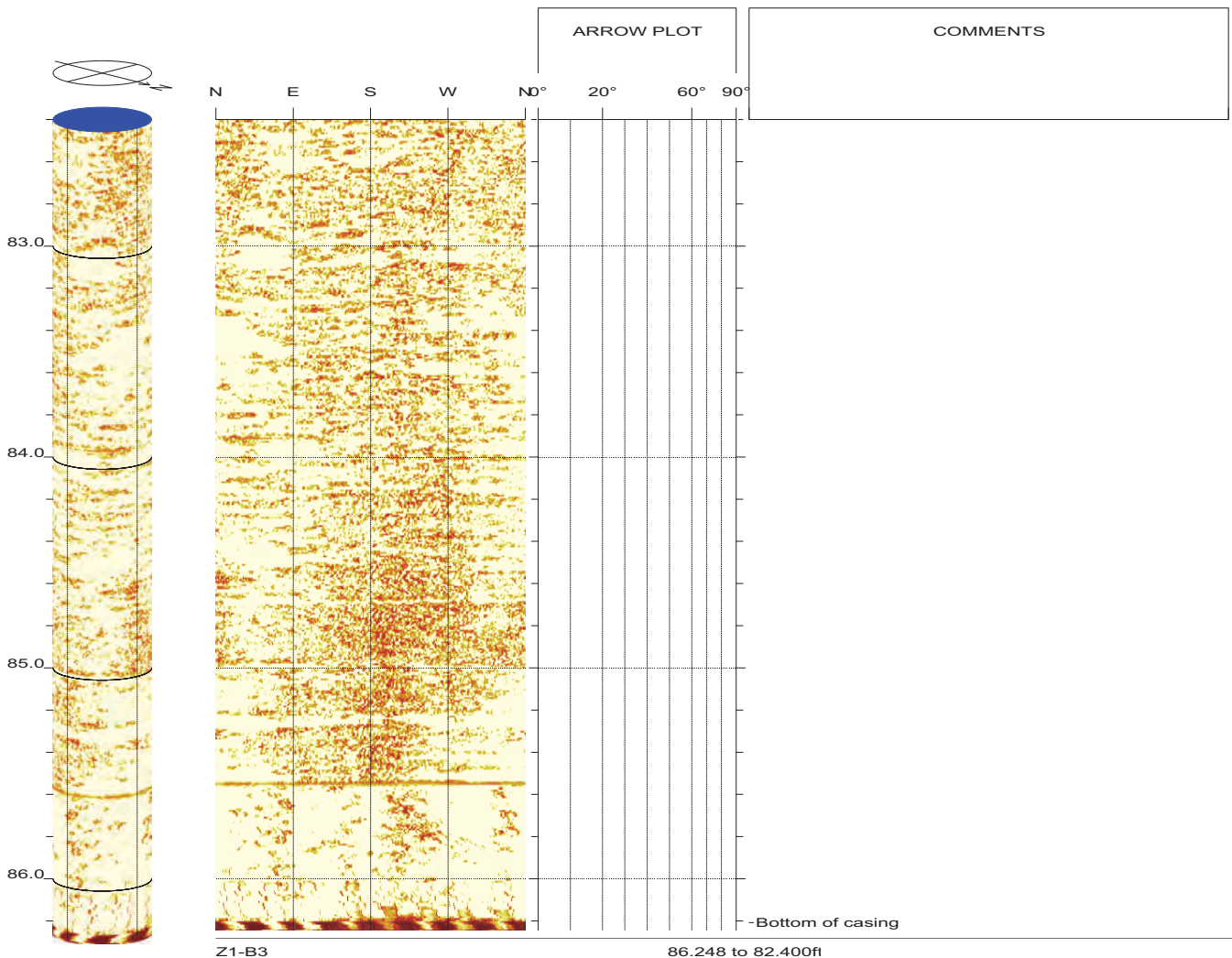
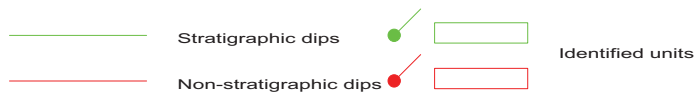
SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

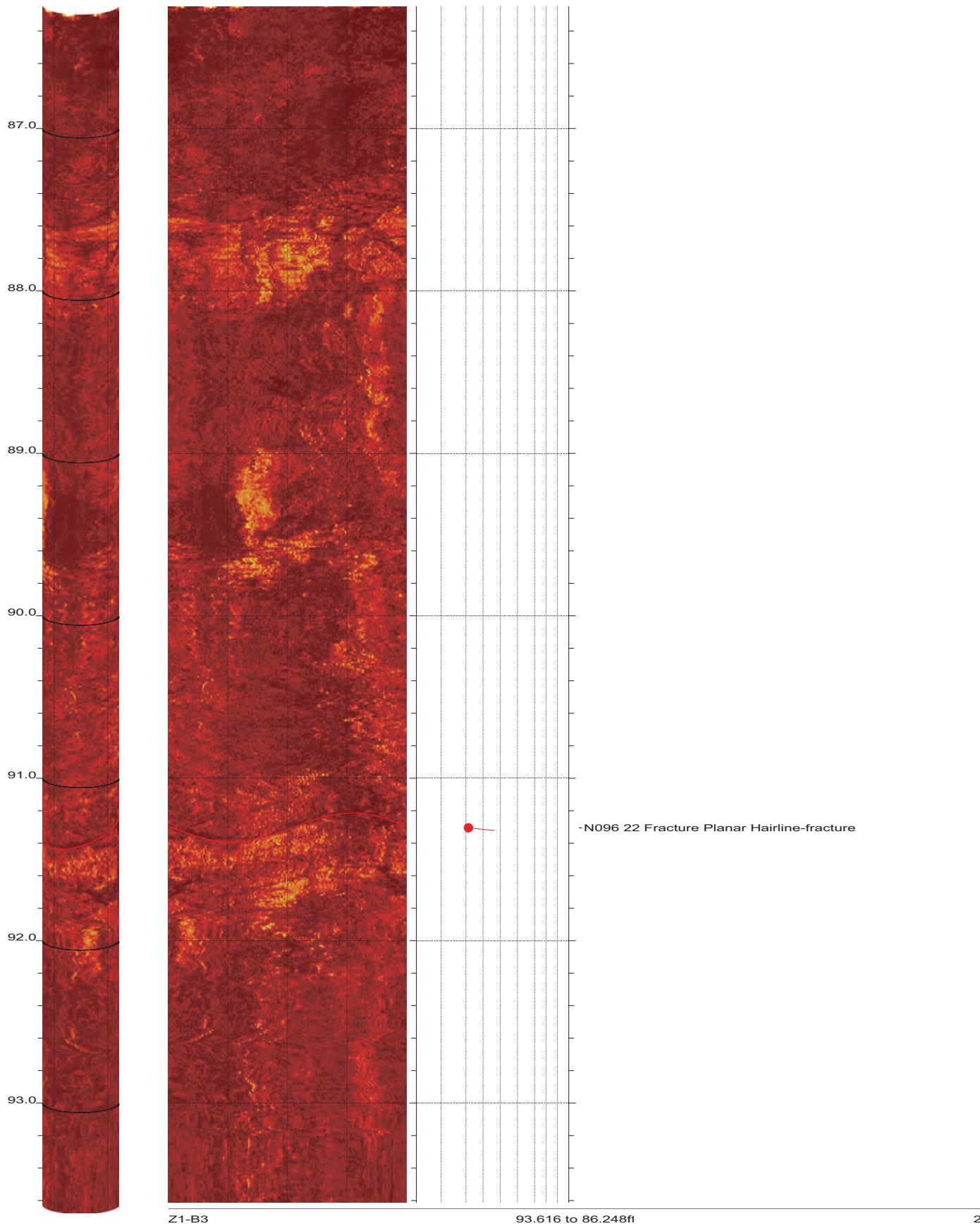
North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

Zone from 300.600 to 82.400ft  
 Format: BHTV-NESWN

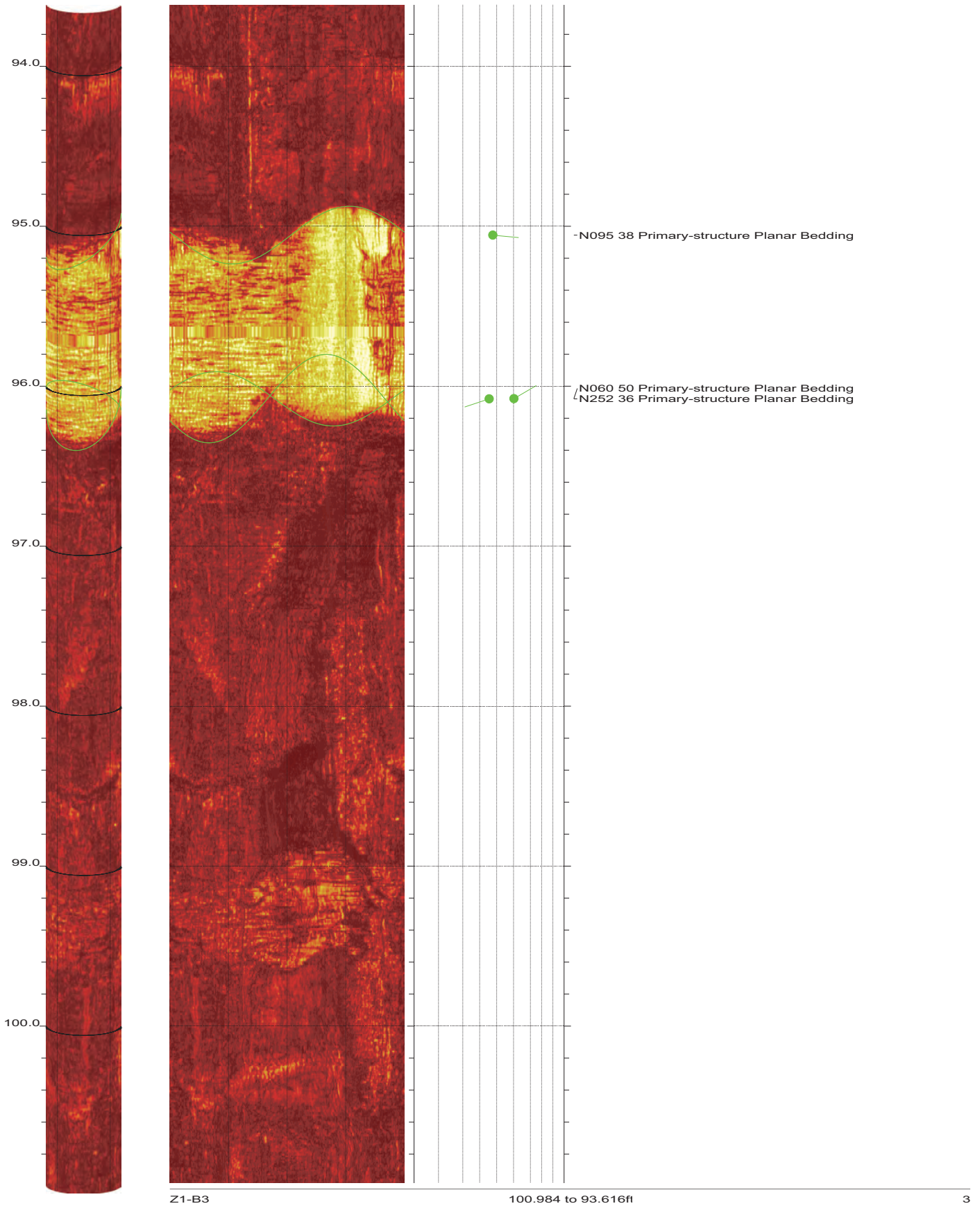
Borehole diam: 5.600inch  
 Vertical = borehole-axis  
 Image: Amplitude



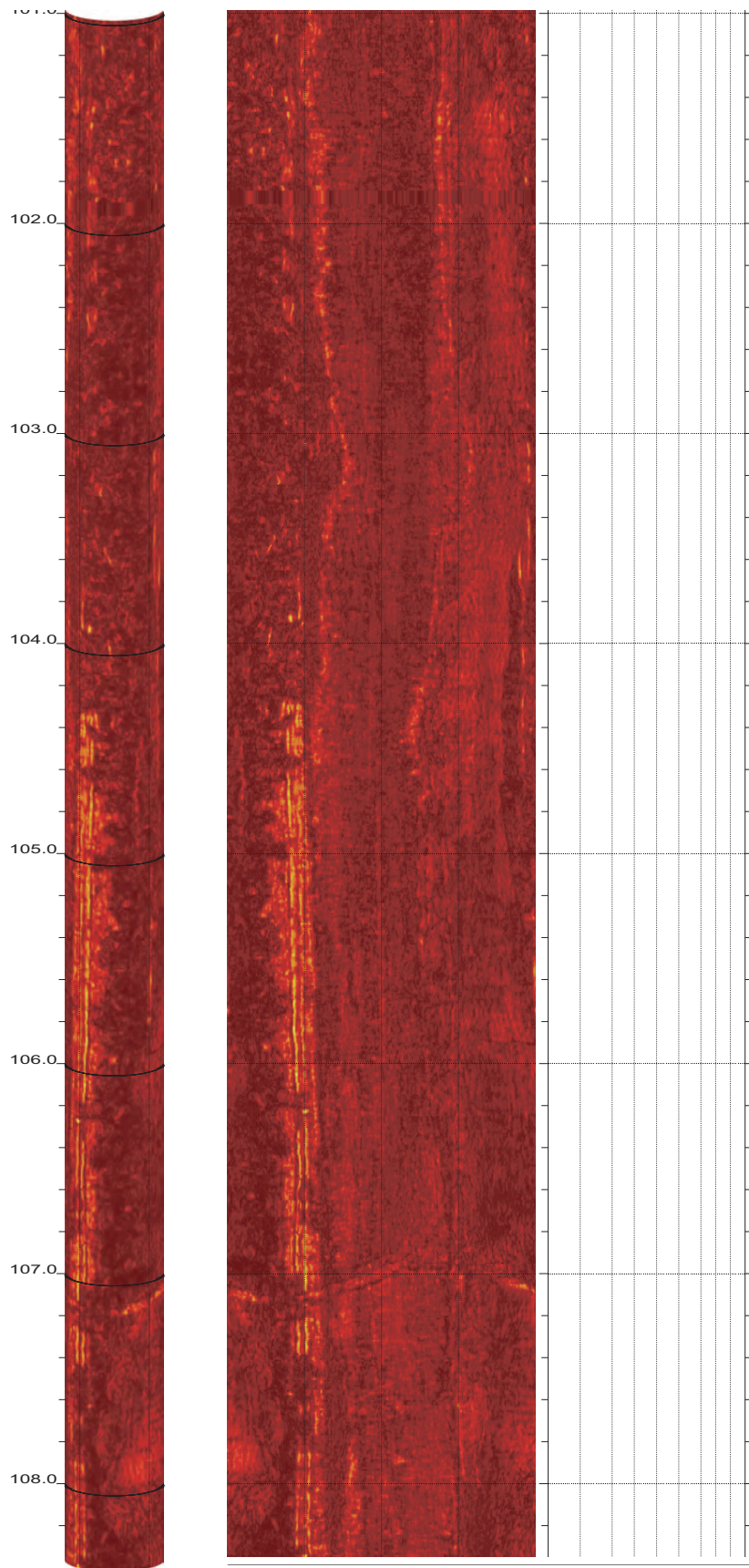




SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 2 of 31



SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 3 of 31

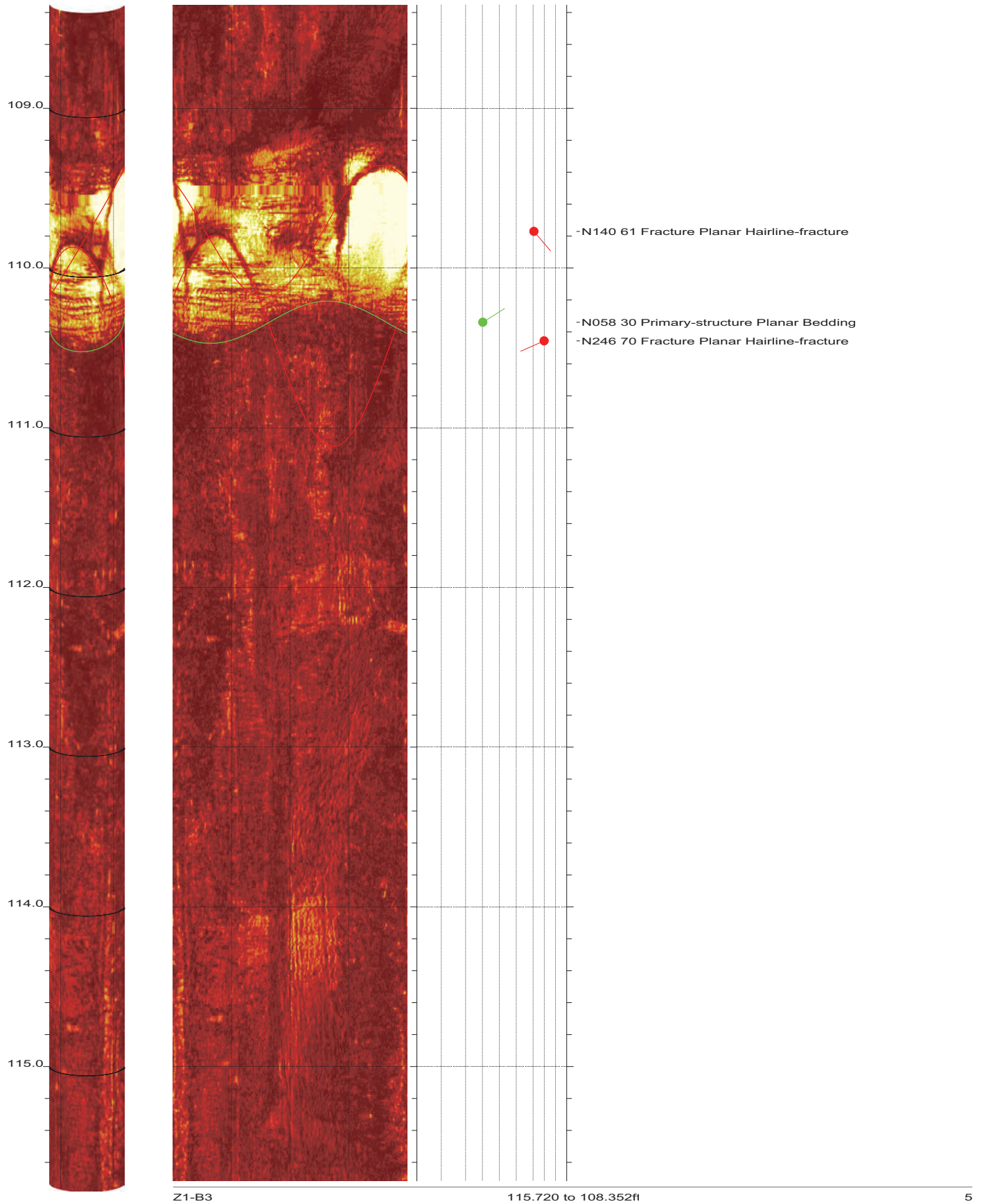


Z1-B3

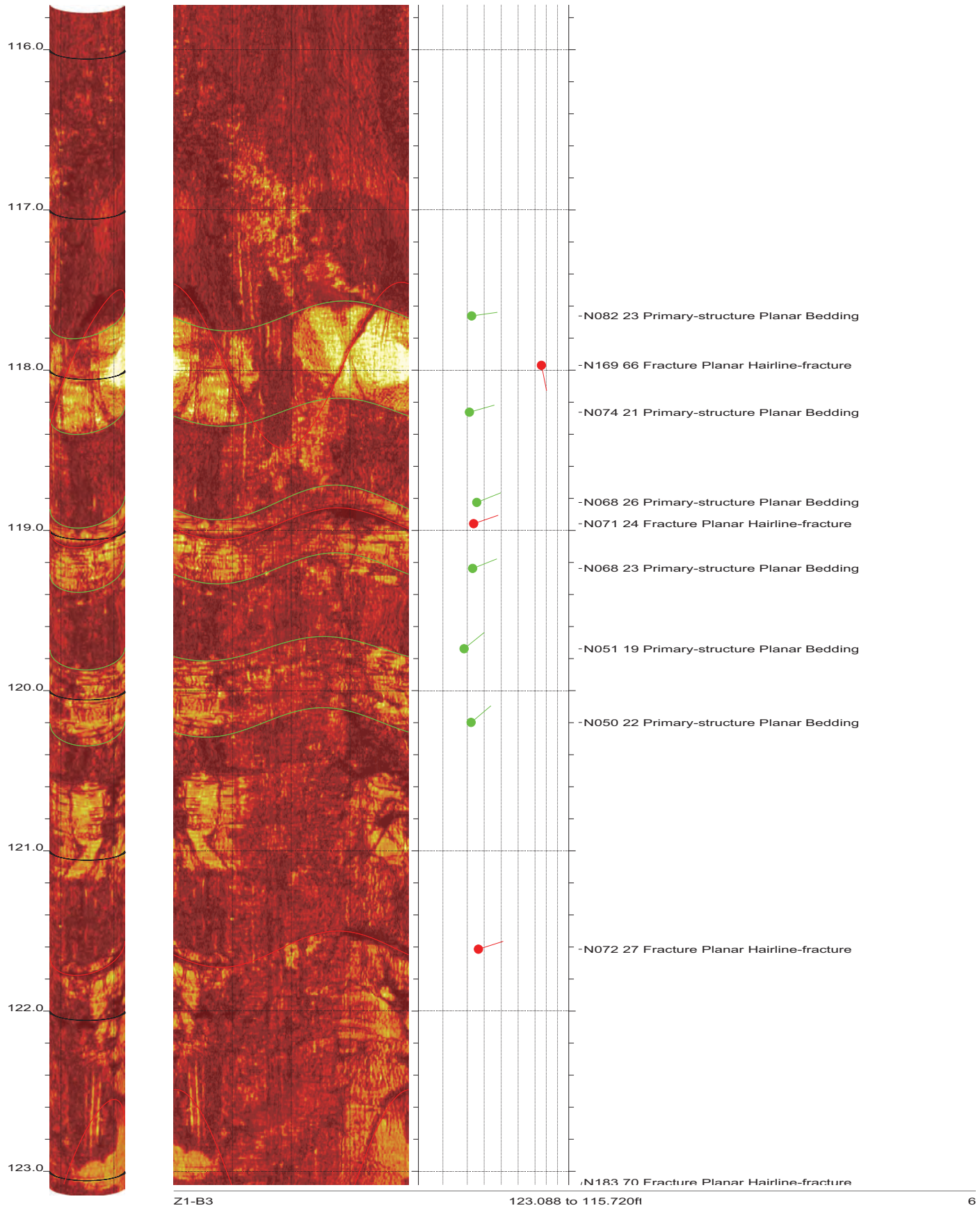
108.352 to 100.984ft

4

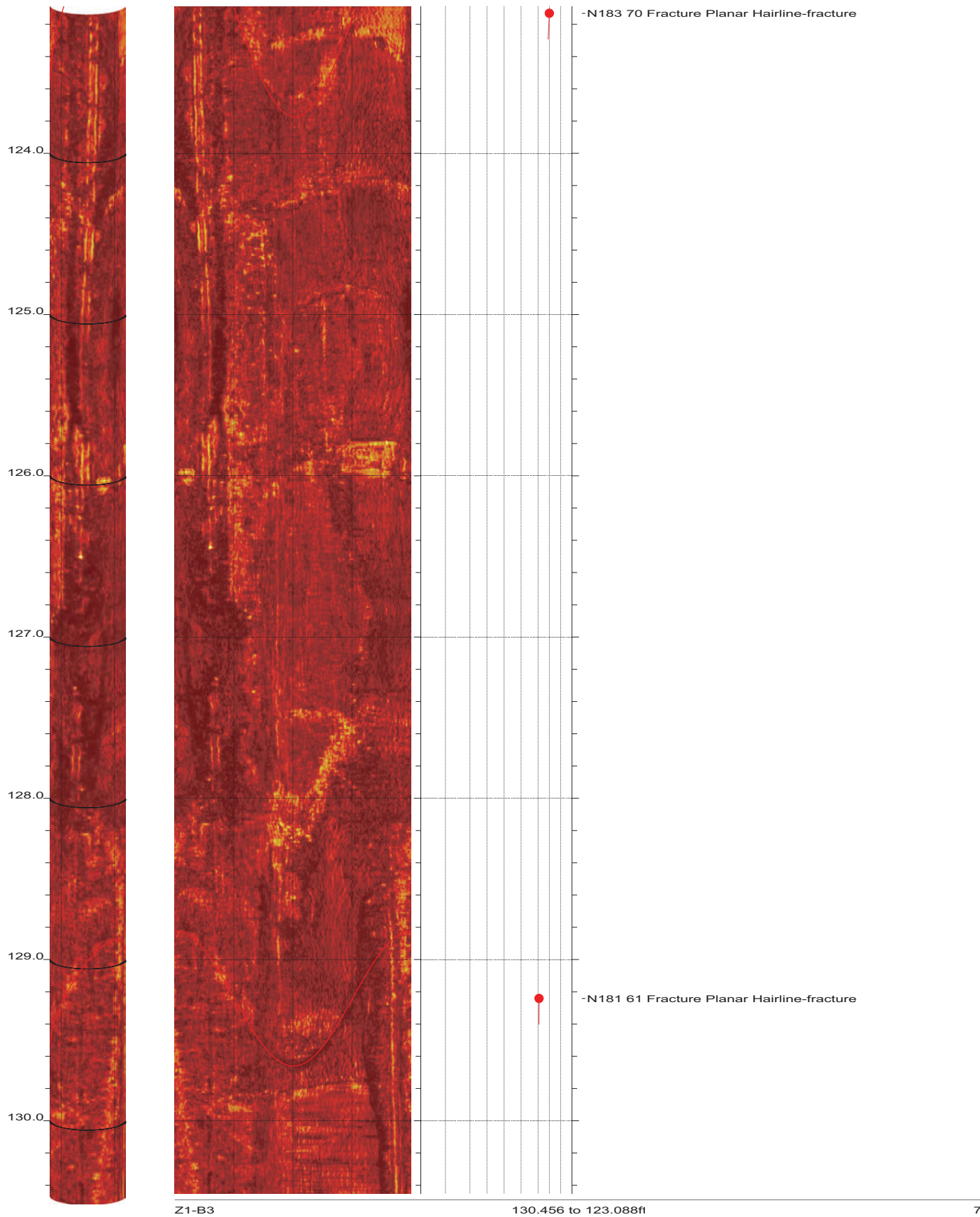
SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 4 of 31



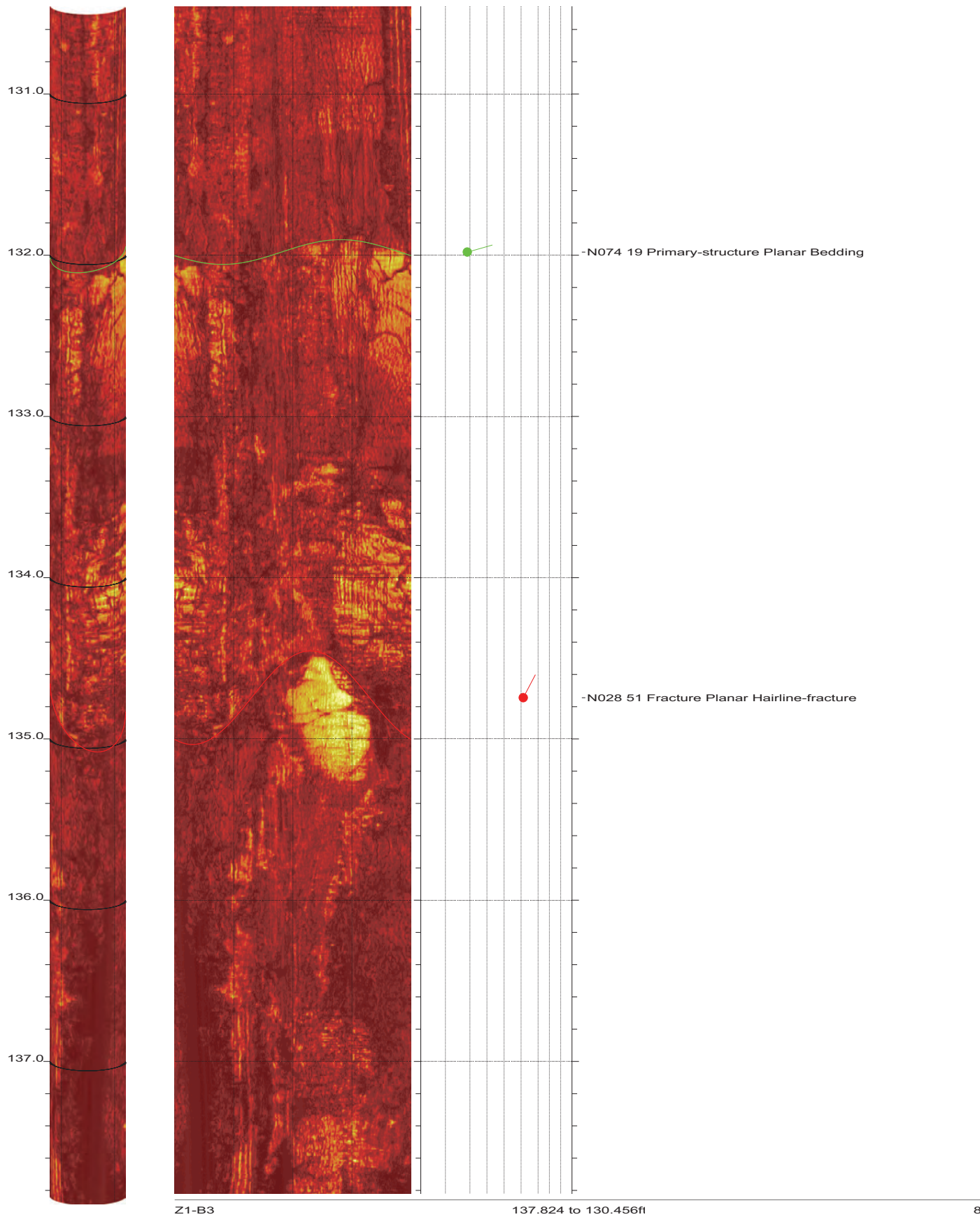
SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 5 of 31



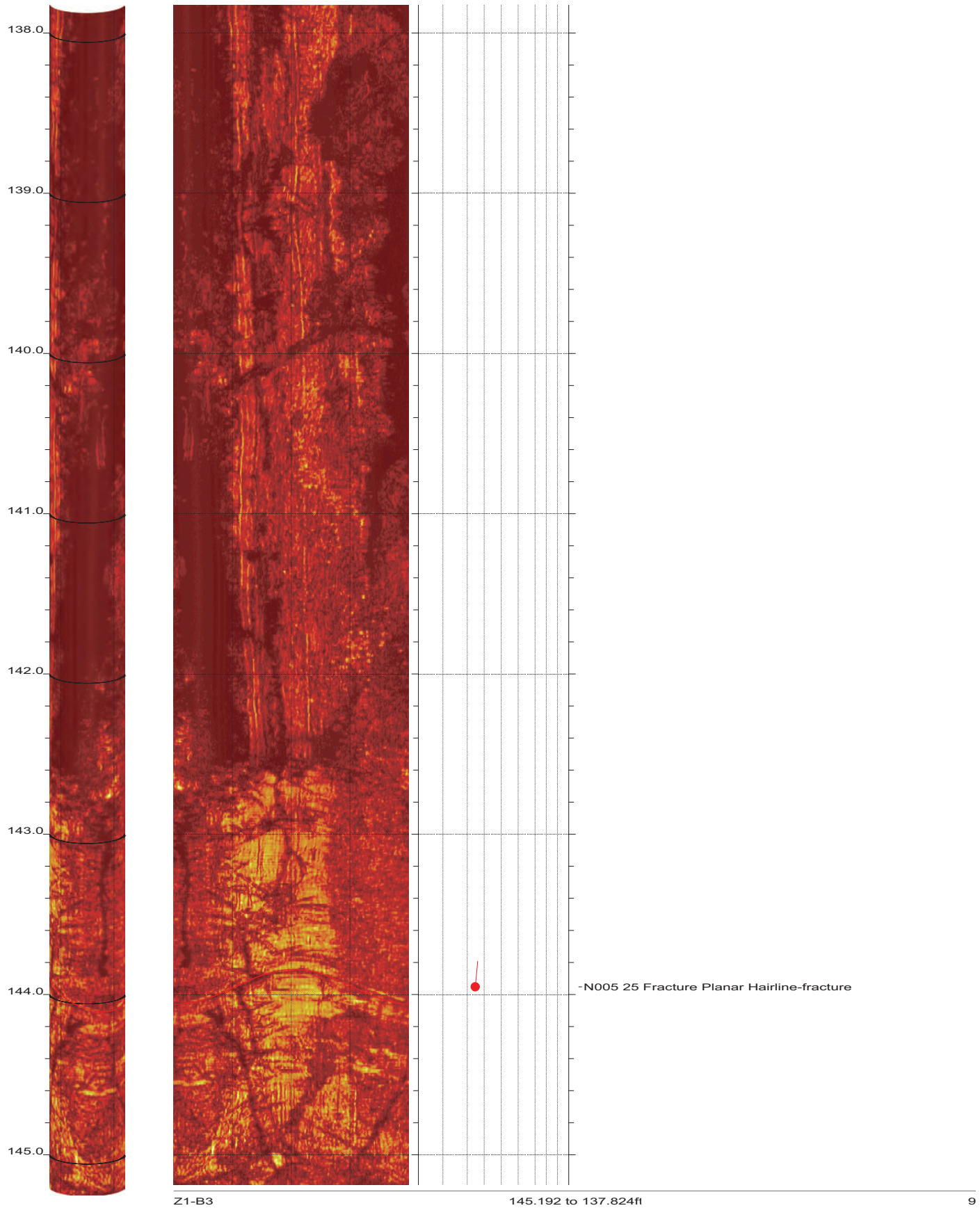
SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 6 of 31



SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 7 of 31

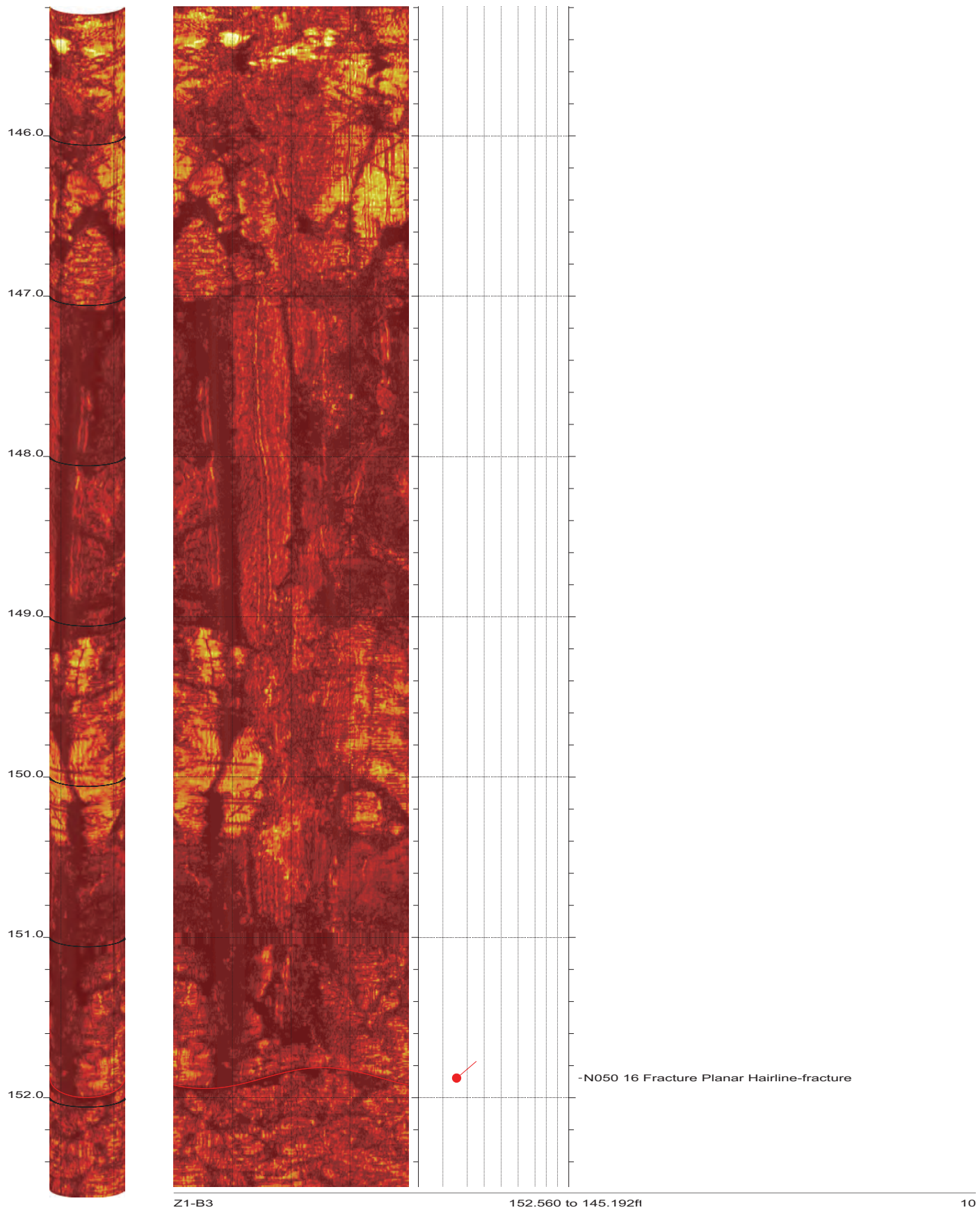


SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 8 of 31

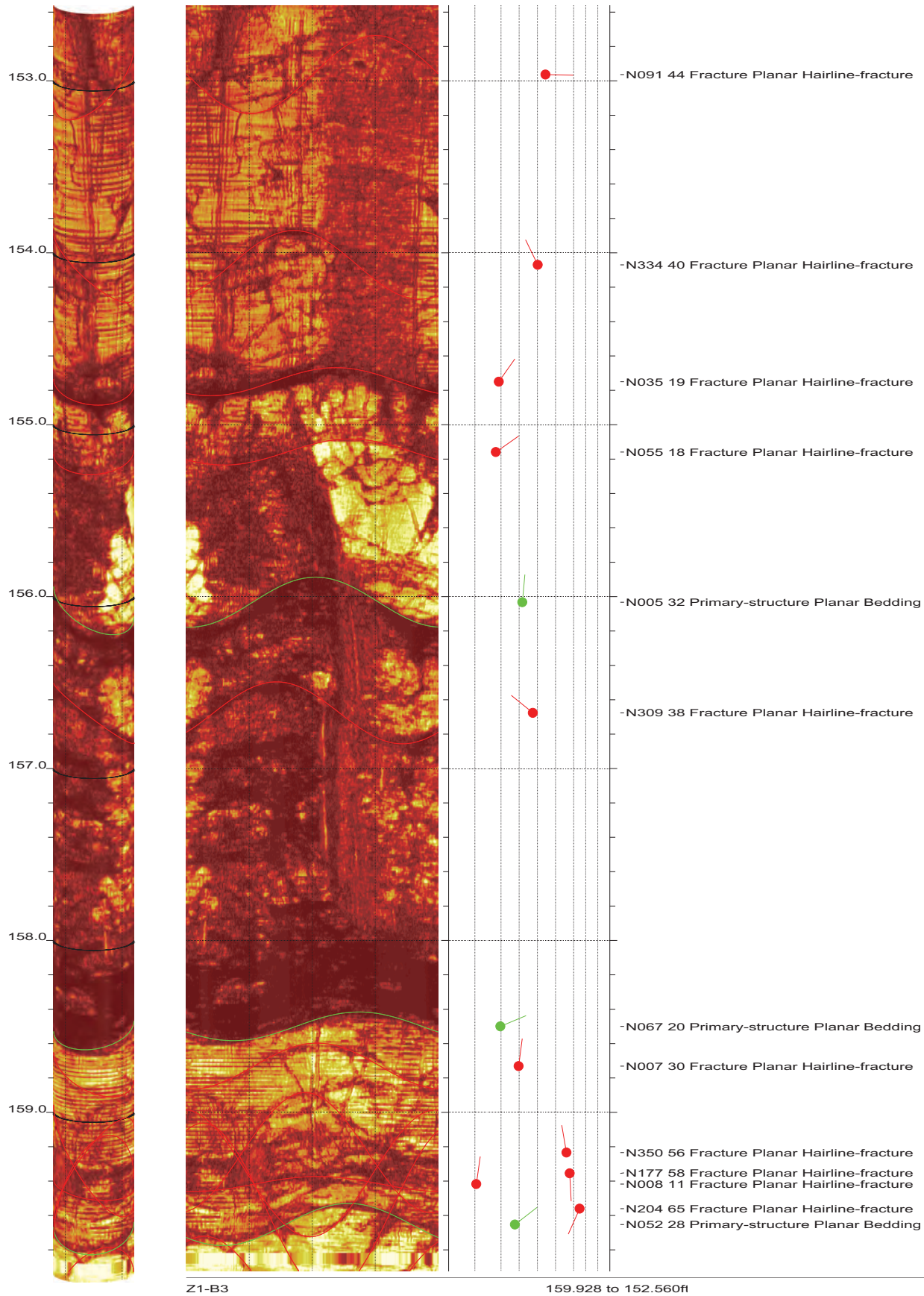


SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 9 of 31

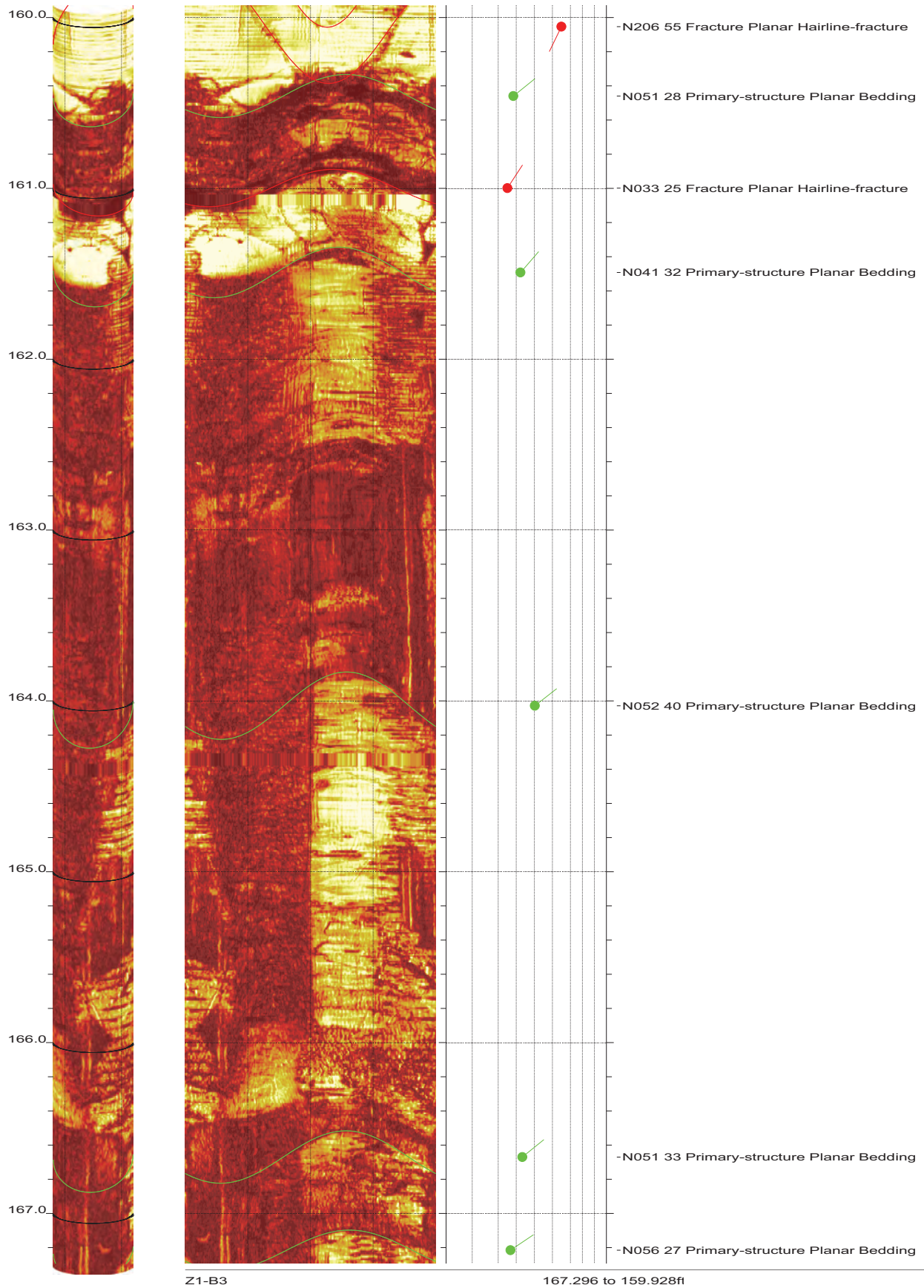




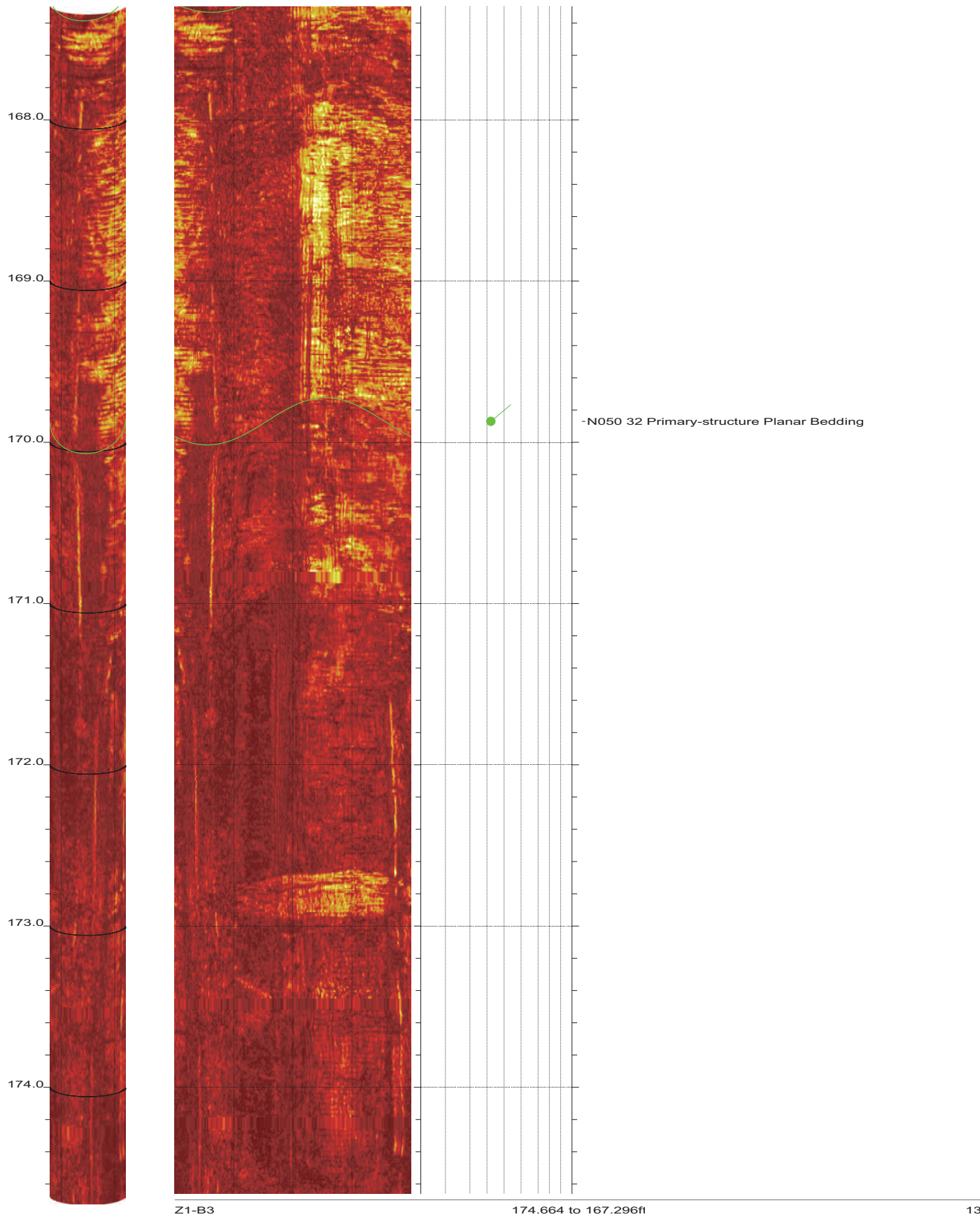
SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 10 of 31

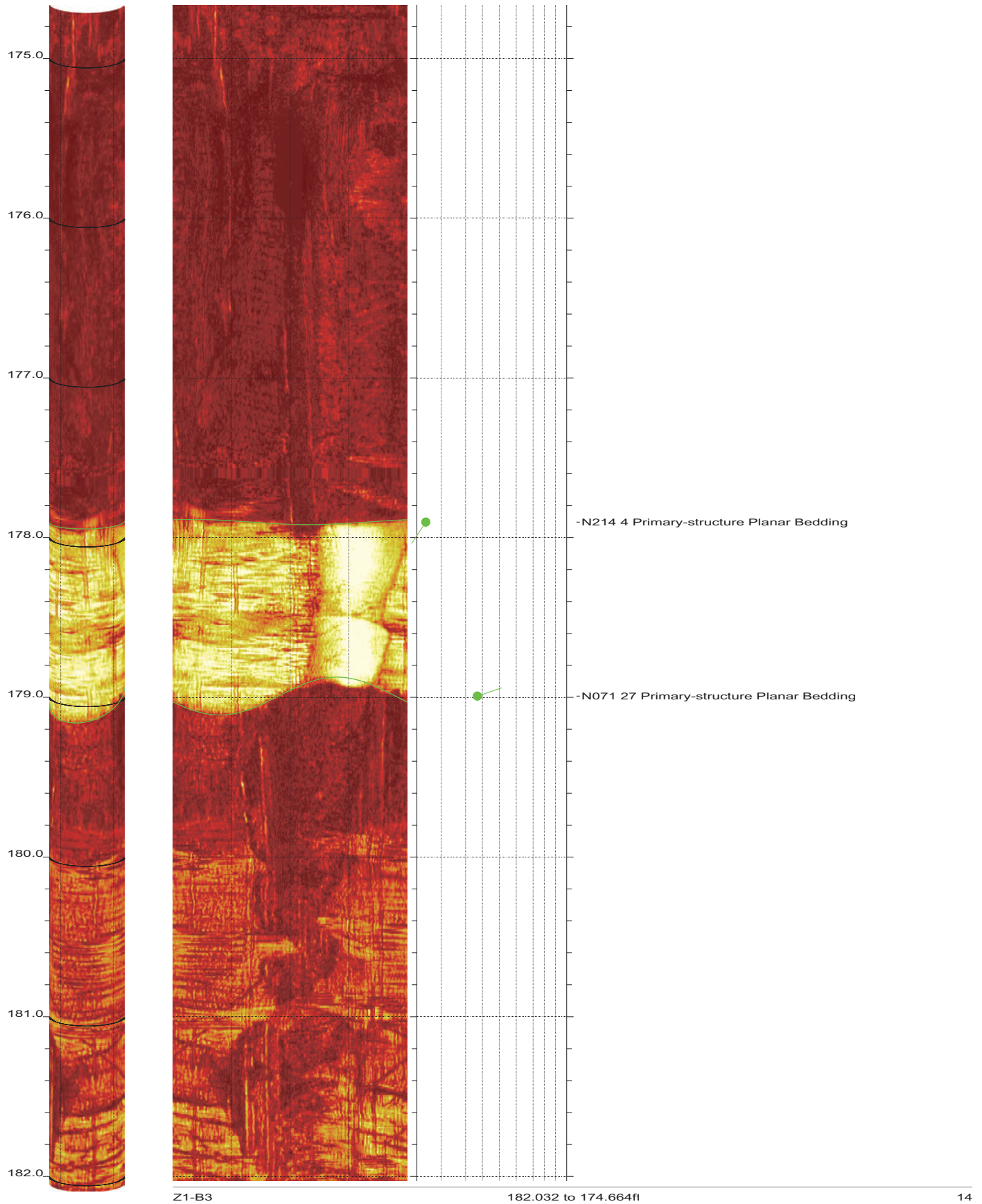


SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 11 of 31

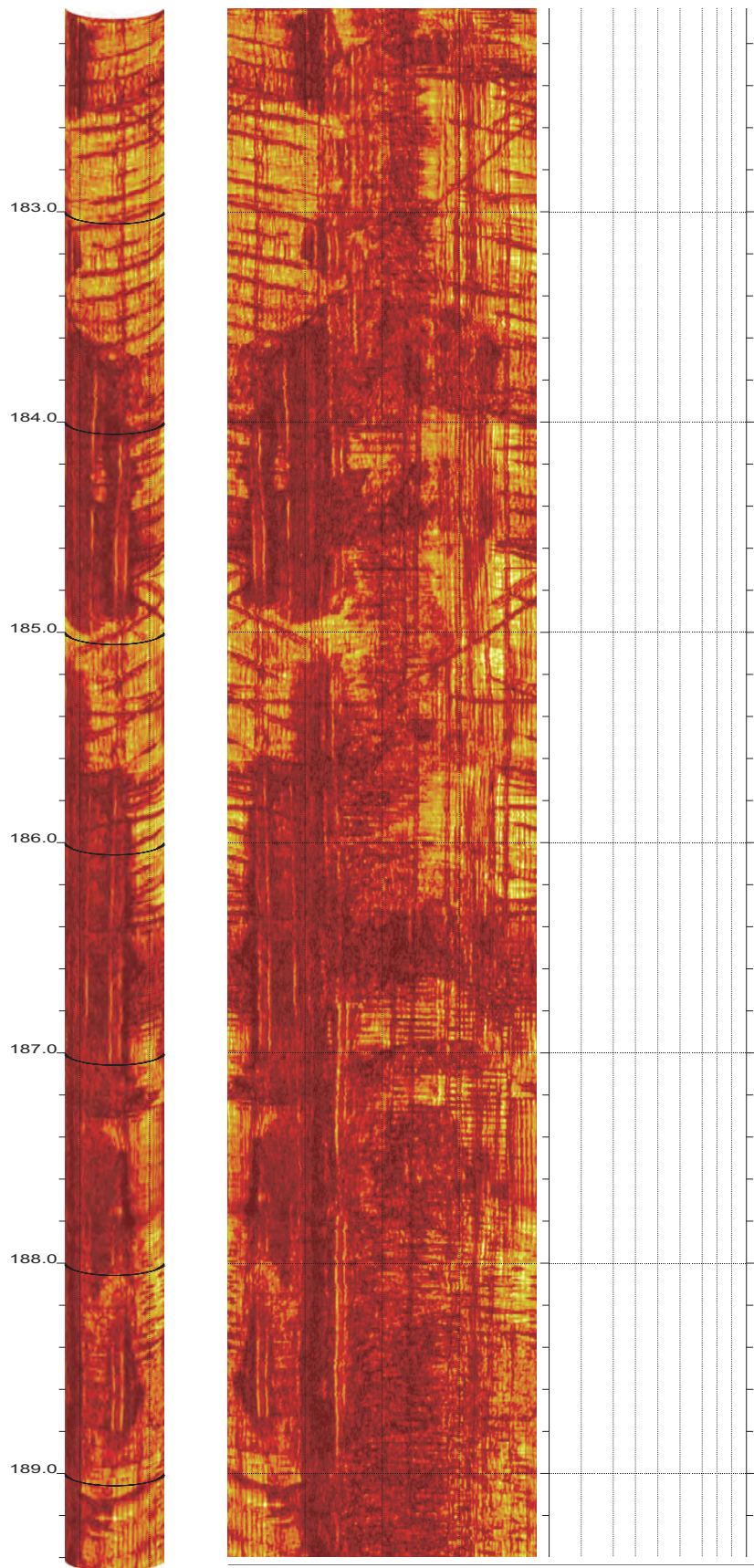


SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 12 of 31





SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 14 of 31

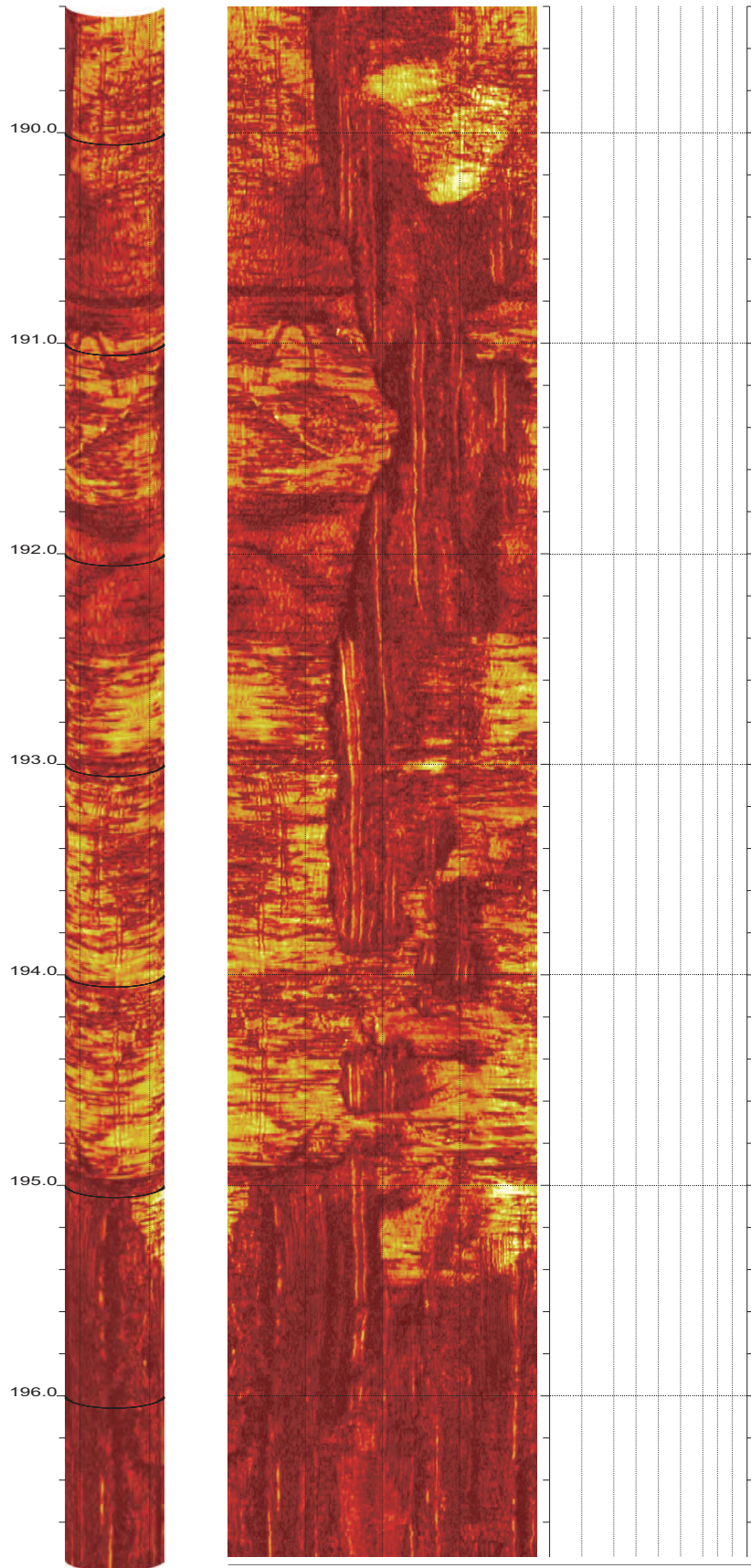


Z1-B3

189.400 to 182.032ft

15

SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 15 of 31

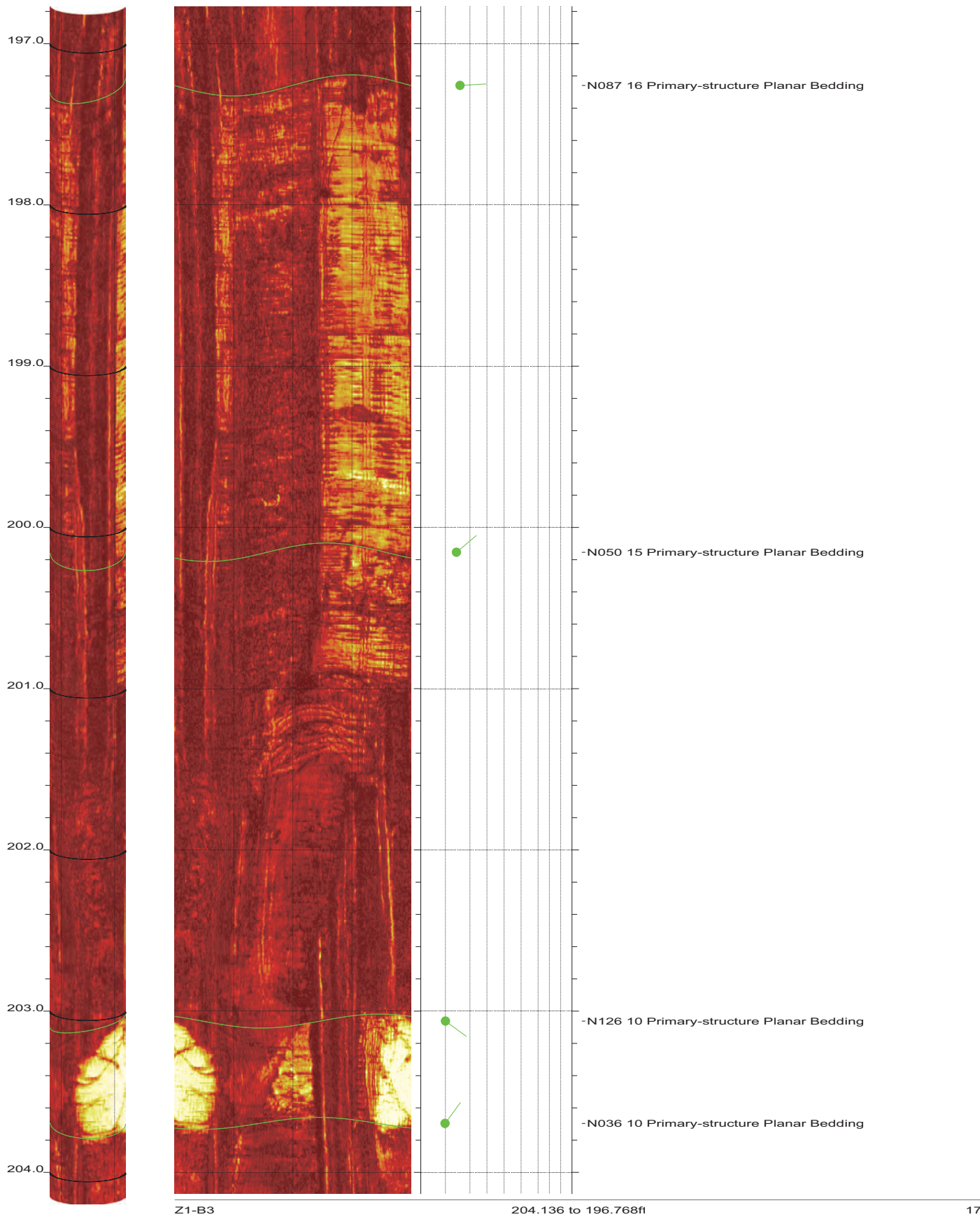


Z1-B3

196.768 to 189.400ft

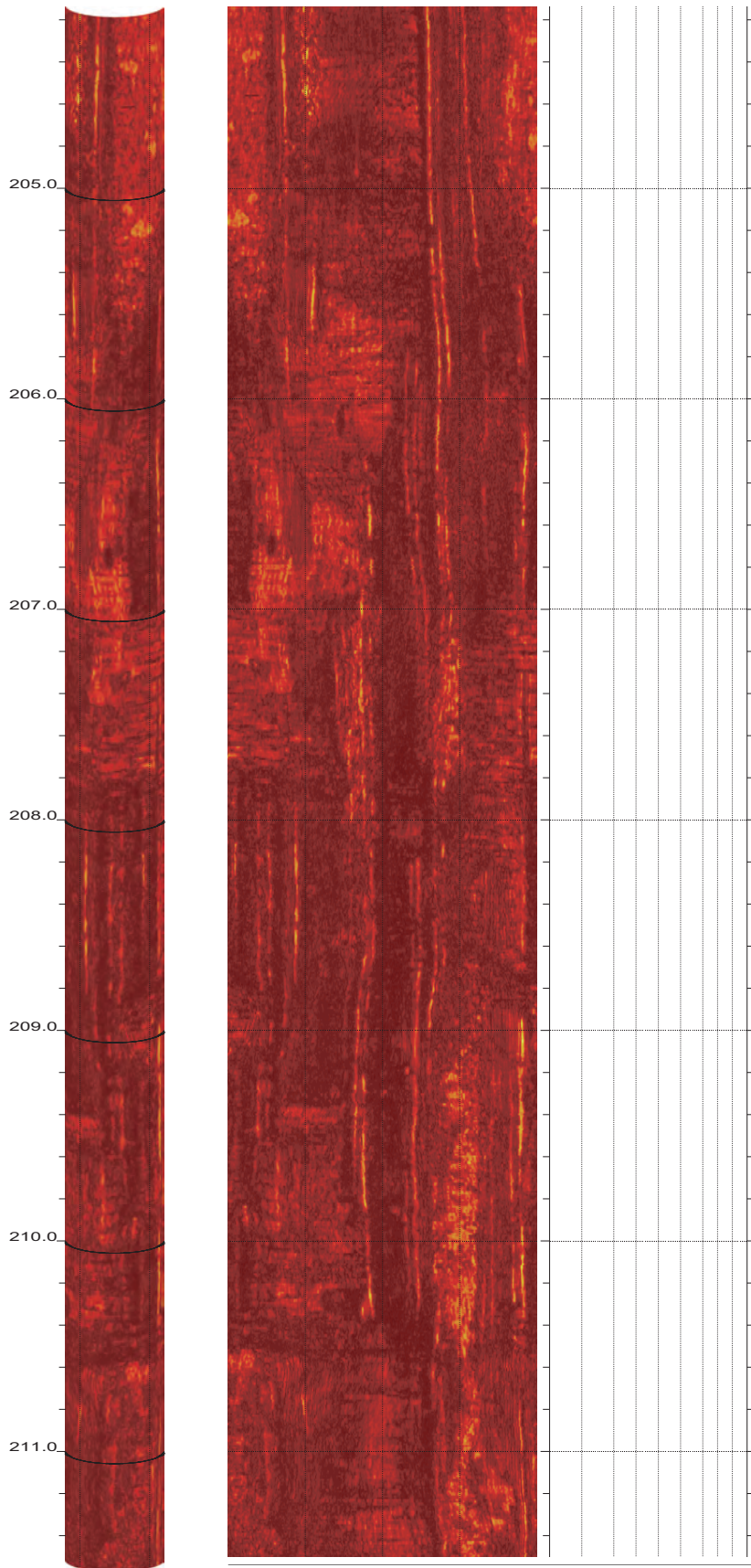
16

SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 16 of 31



SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 17 of 31



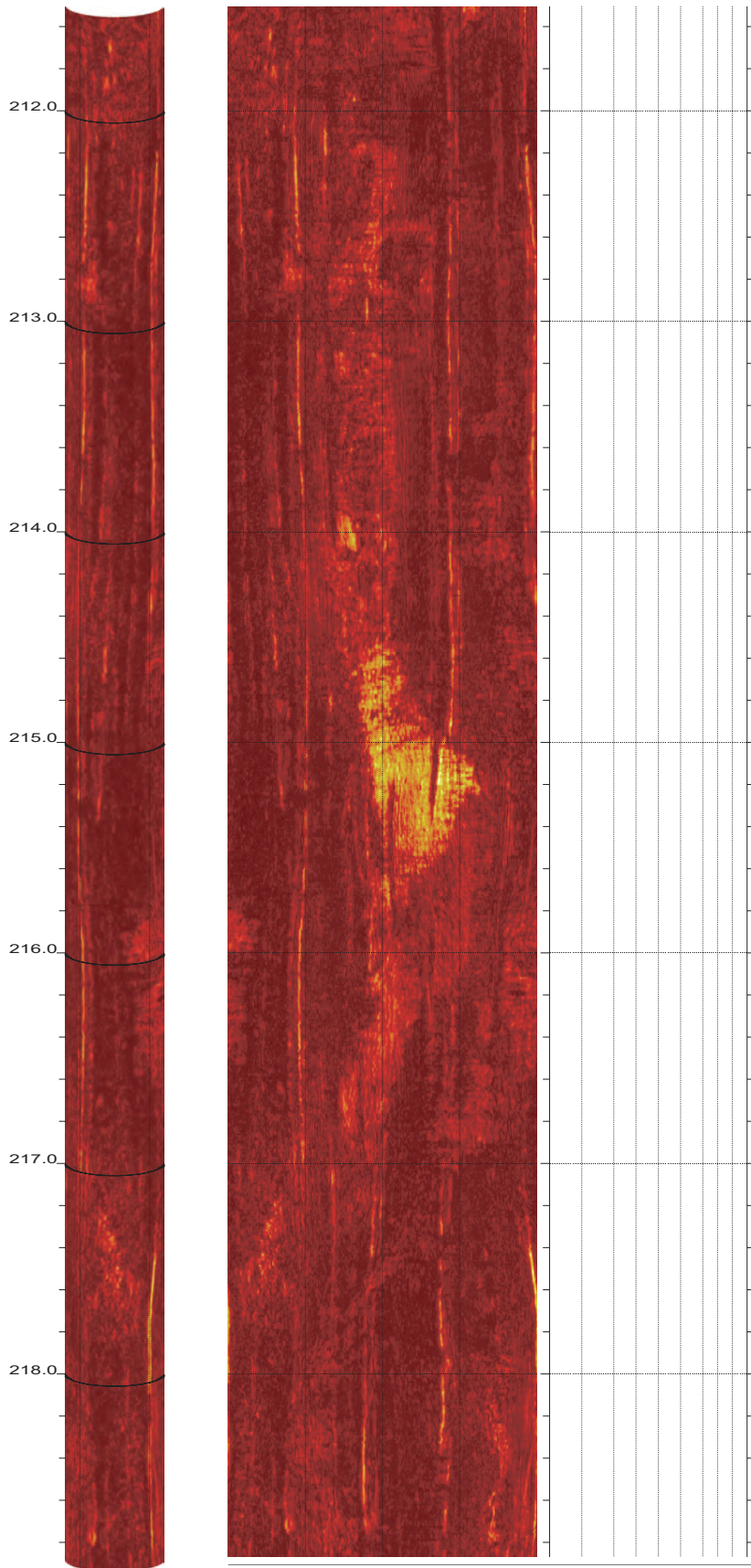


Z1-B3

211.504 to 204.136ft

18

SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 18 of 31

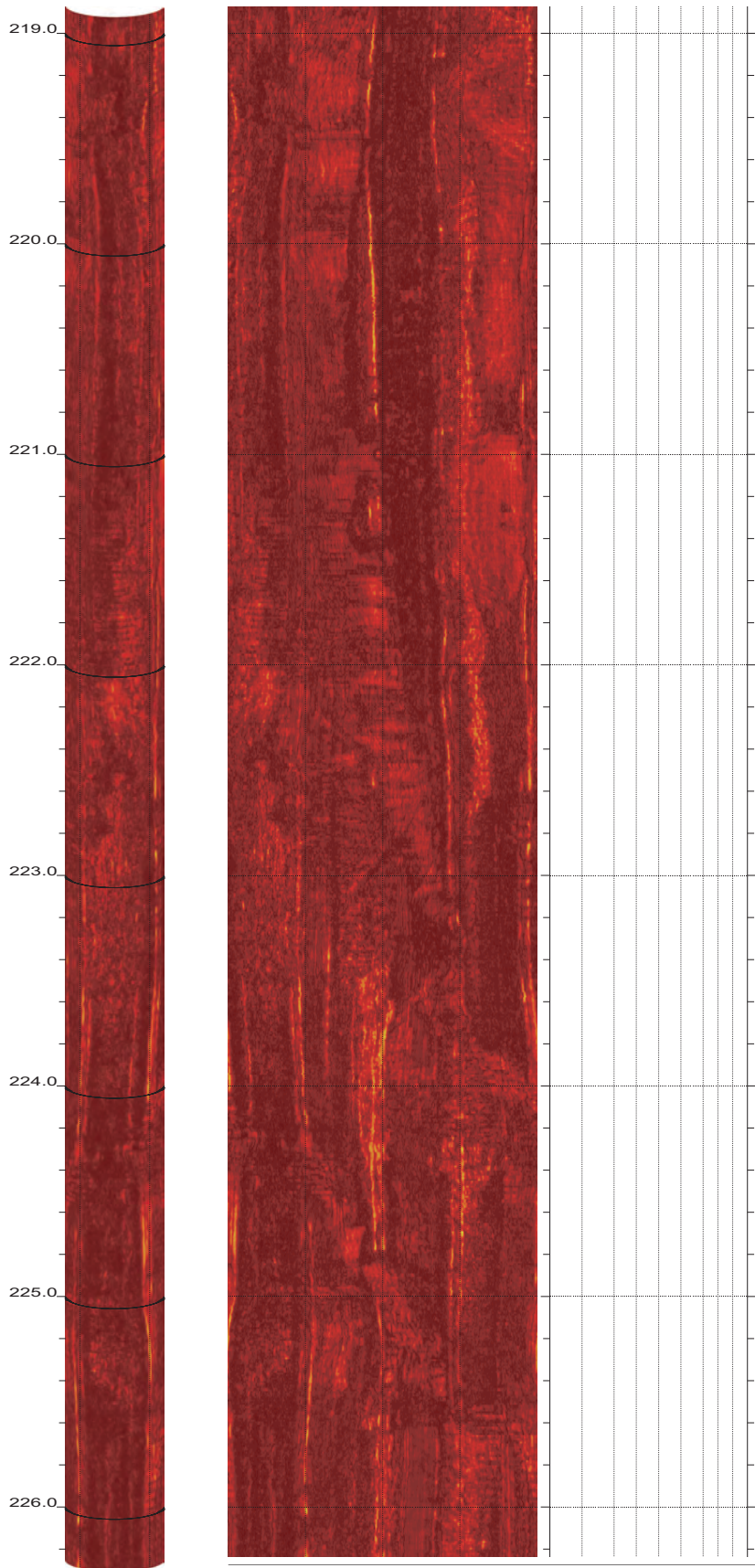


Z1-B3

218.872 to 211.504ft

19

SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 19 of 31

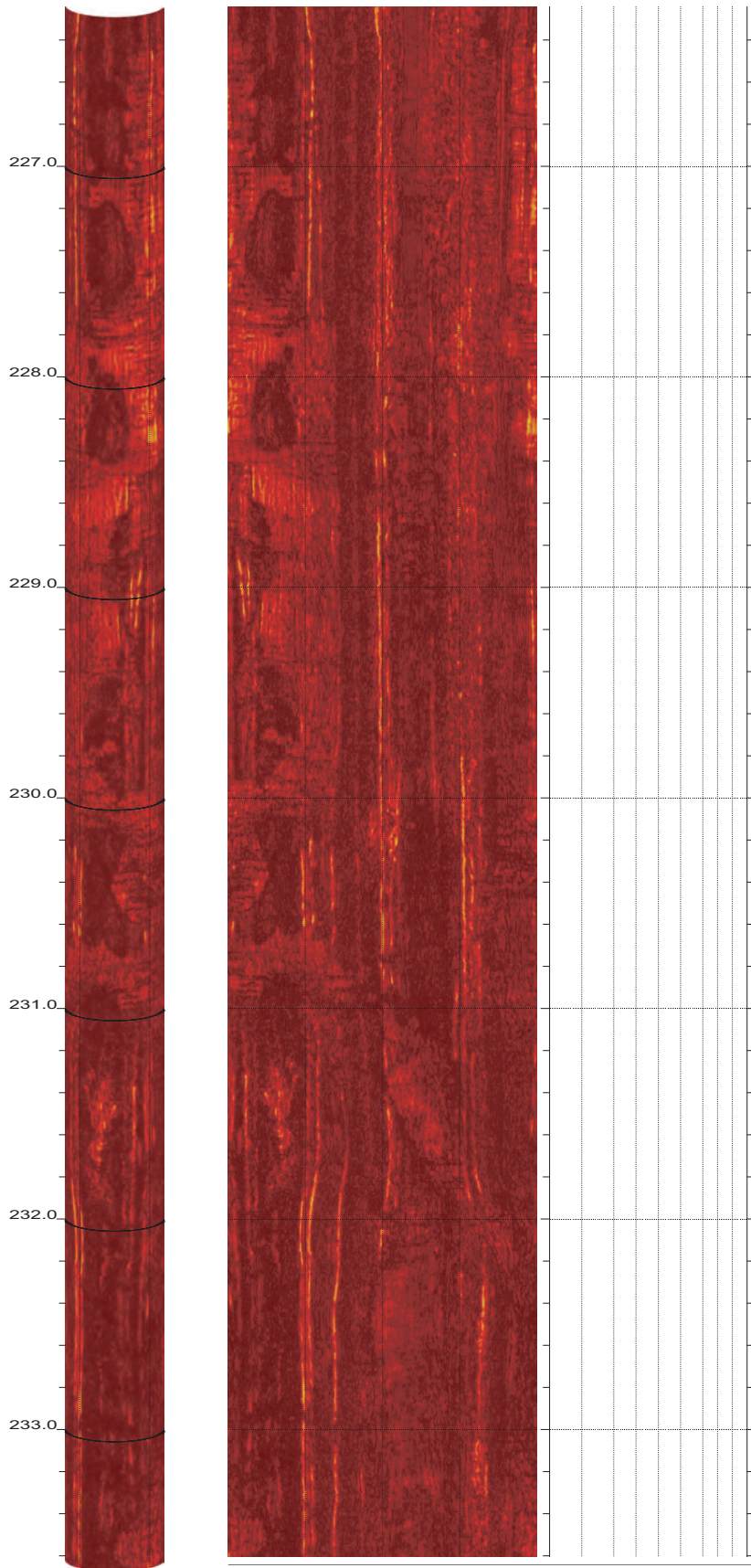


Z1-B3

226.240 to 218.872ft

20

SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 20 of 31

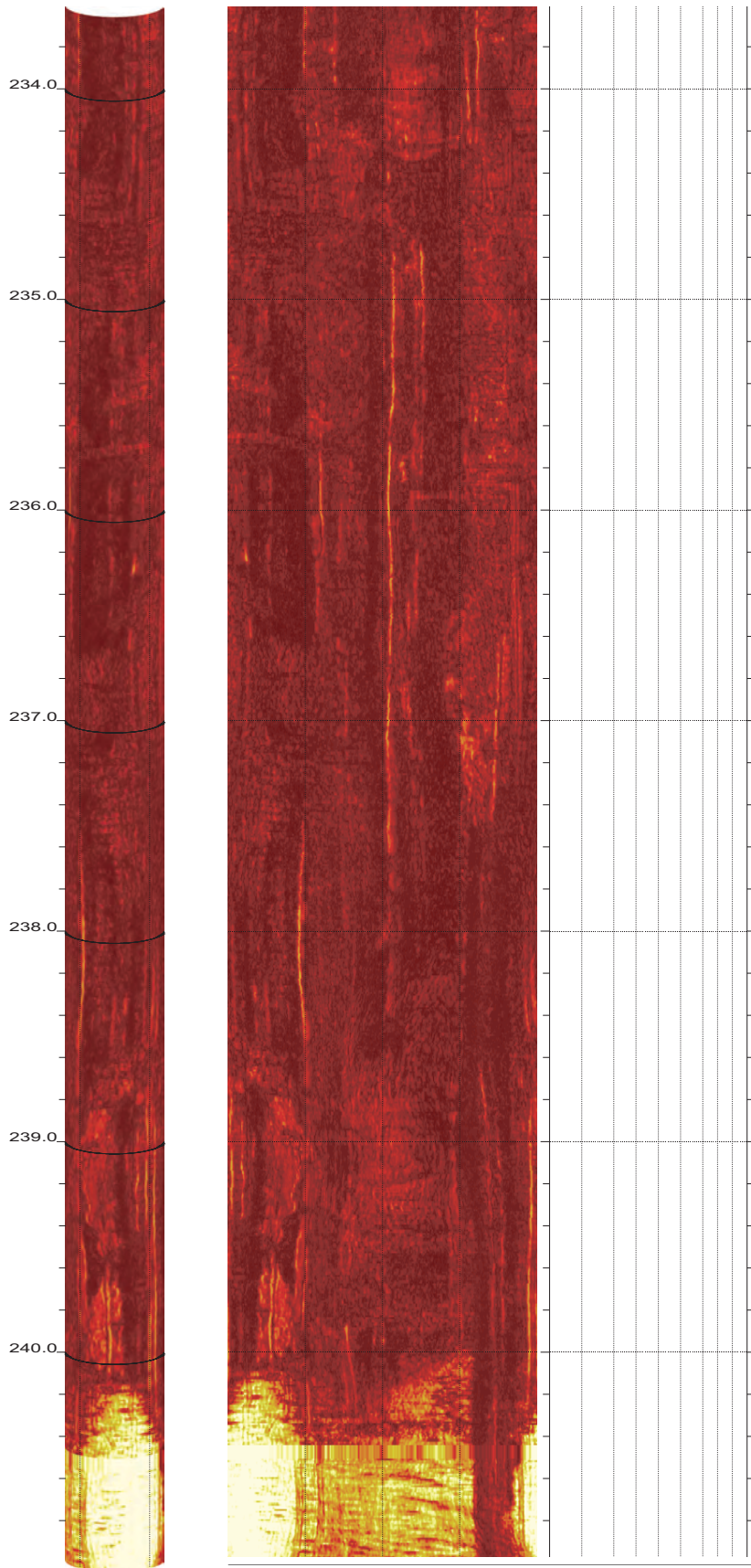


Z1-B3

233.608 to 226.240ft

21

SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 21 of 31

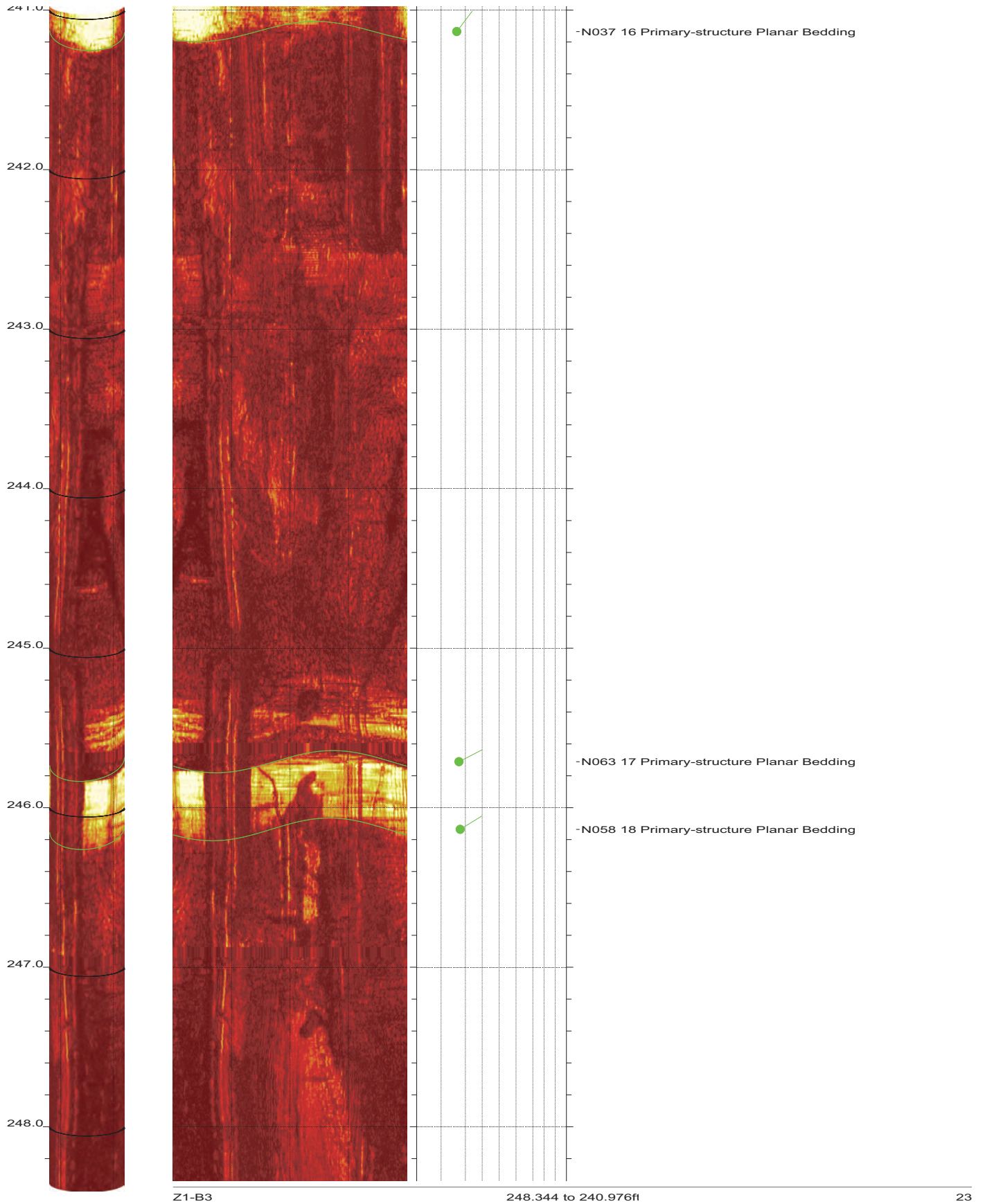


Z1-B3

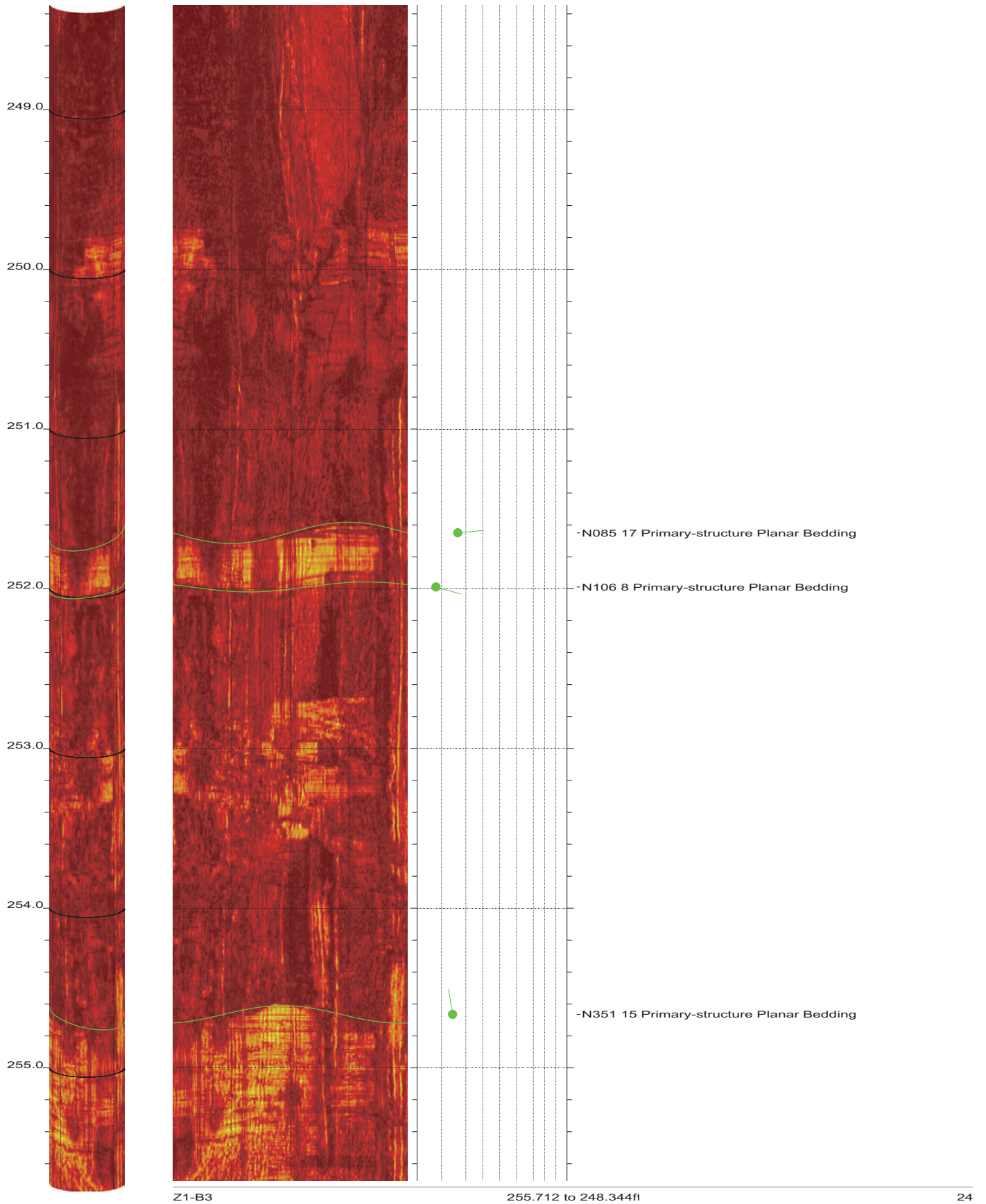
240.976 to 233.608ft

22

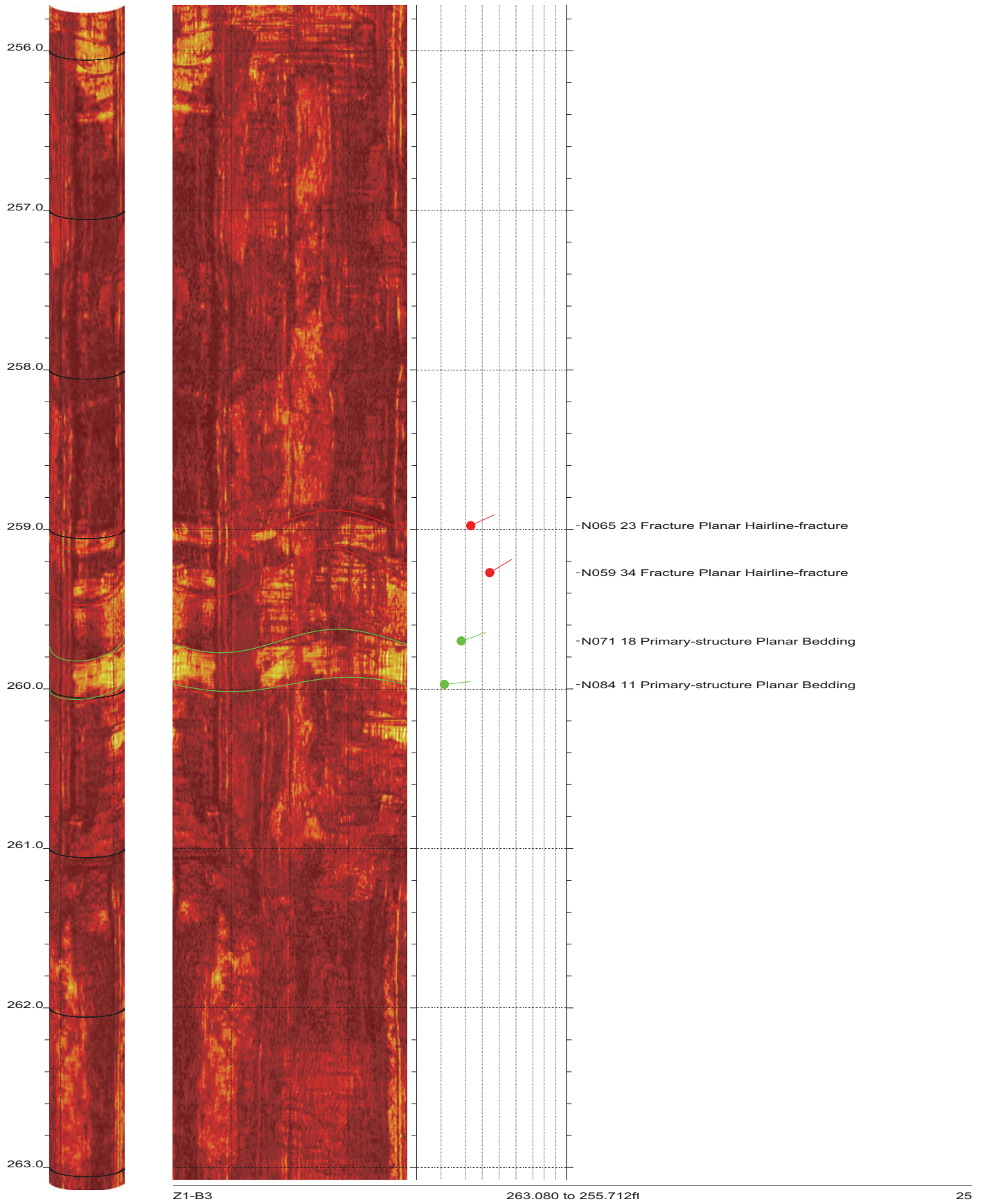
SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 22 of 31



SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 23 of 31

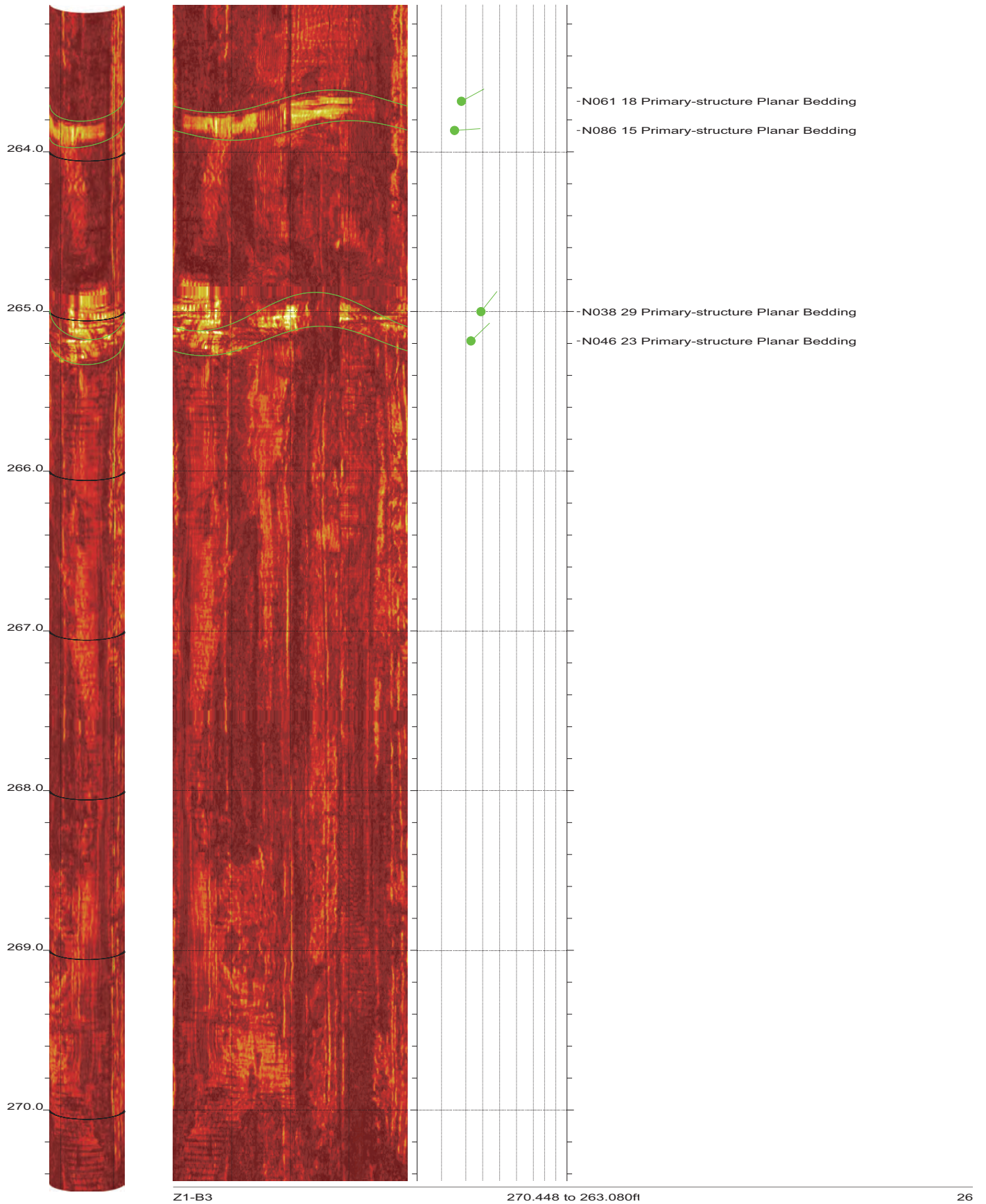


SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 24 of 31

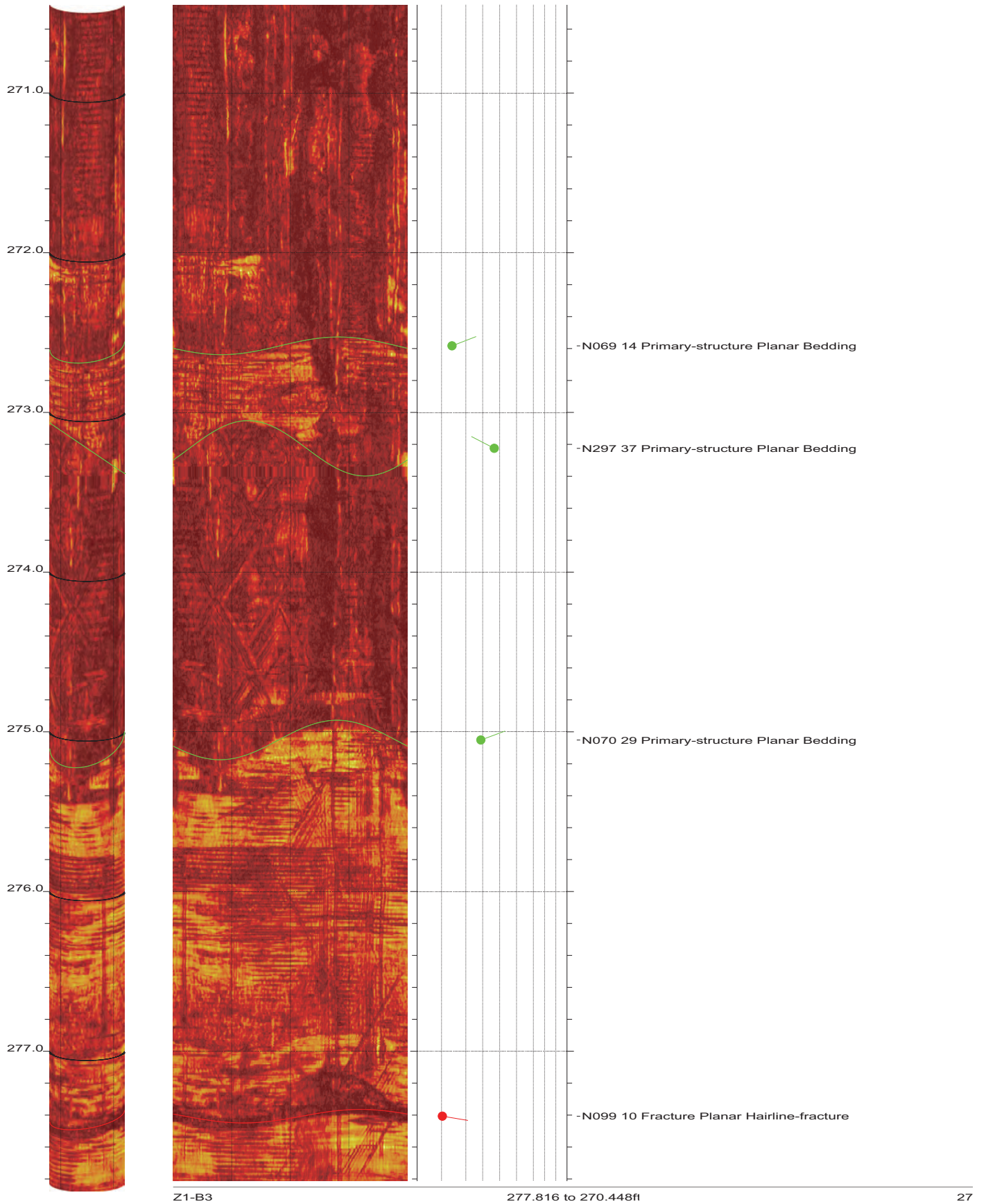


SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 25 of 31

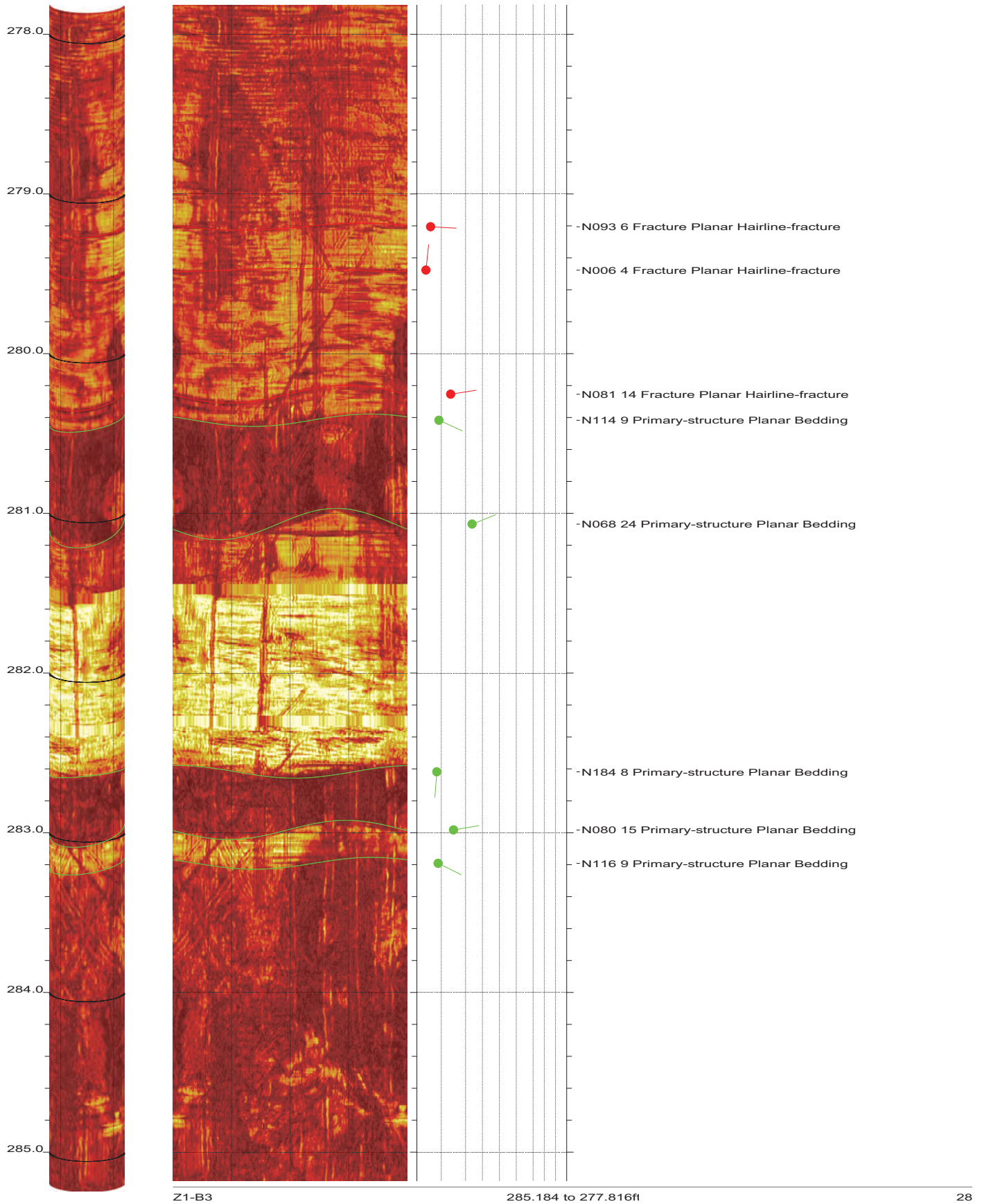




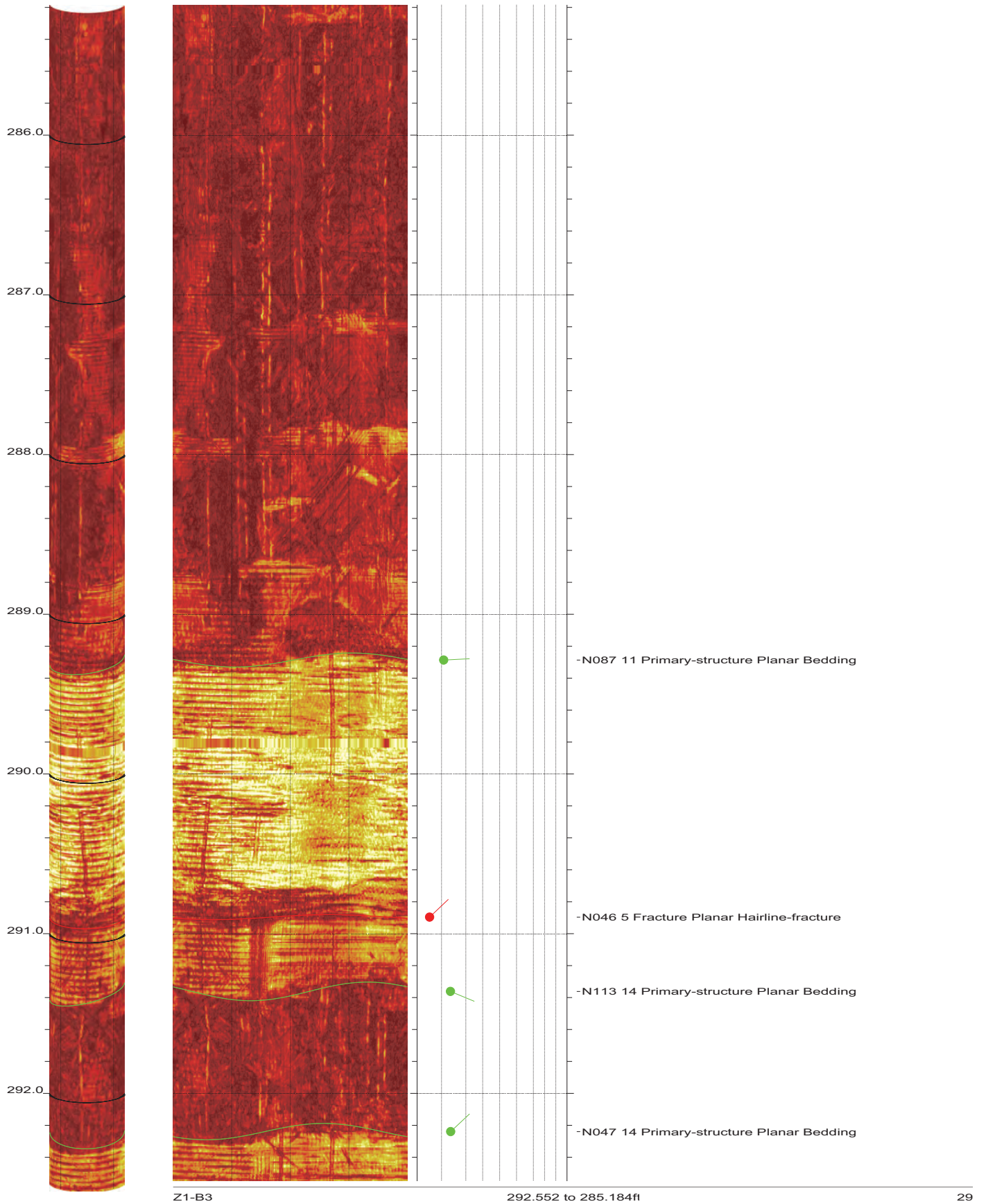
SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 26 of 31



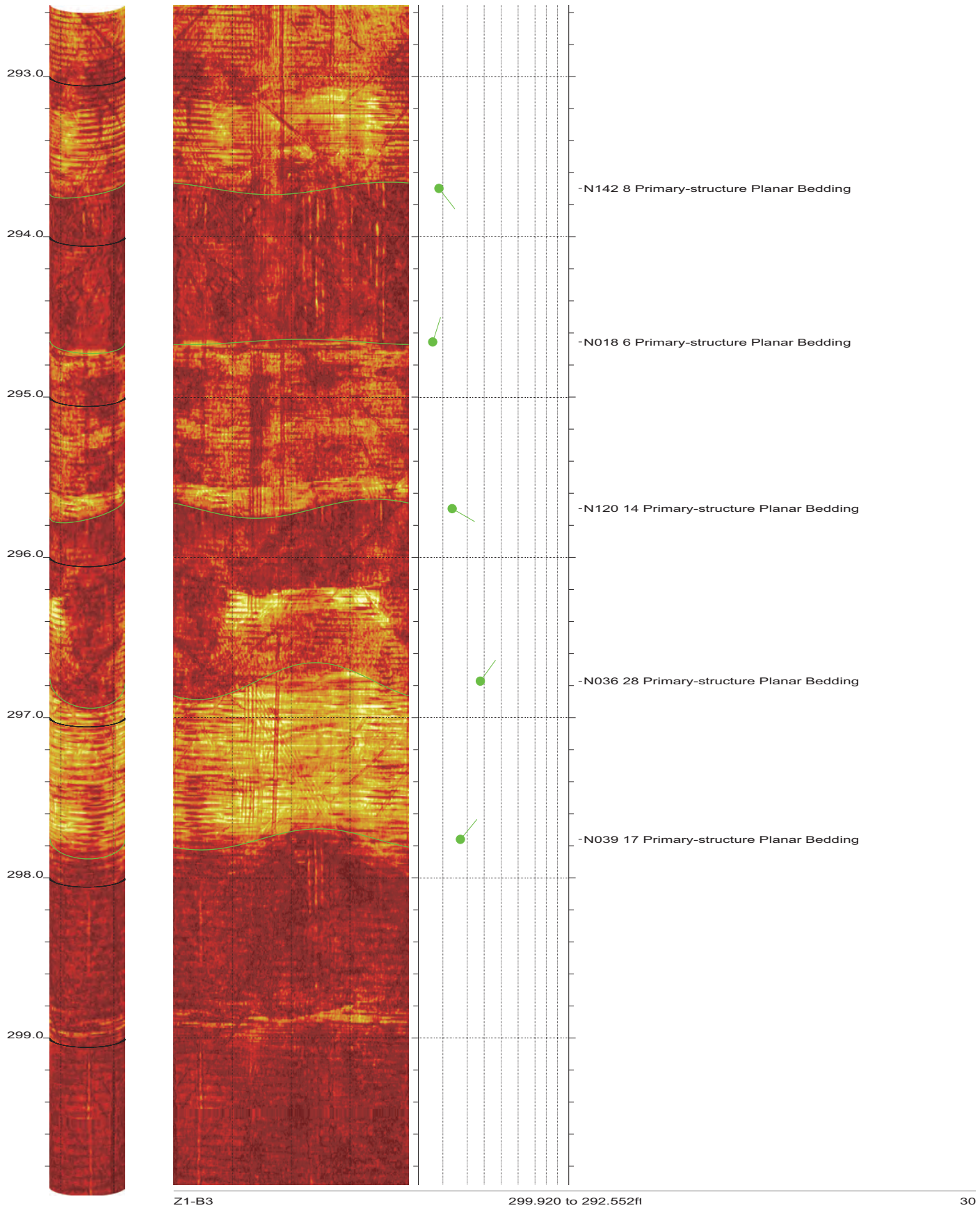
SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 27 of 31



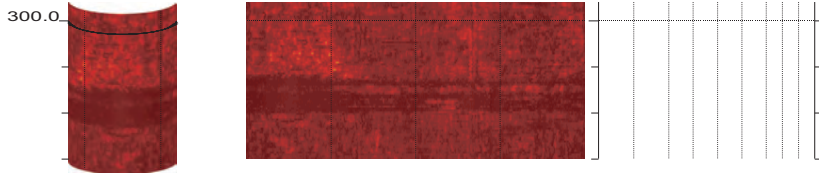
SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 28 of 31



SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 29 of 31



SR-710 Boring Z1-B3 Acoustic Televiewer Dips rev 1 Sheet 30 of 31





BHTV DATA PROCESSING  
 RGLDIP vsn 6.2  
 INTERPRETED BHTV DIPS LOG

CASCADE DRILLING

Borehole: Z1-B5

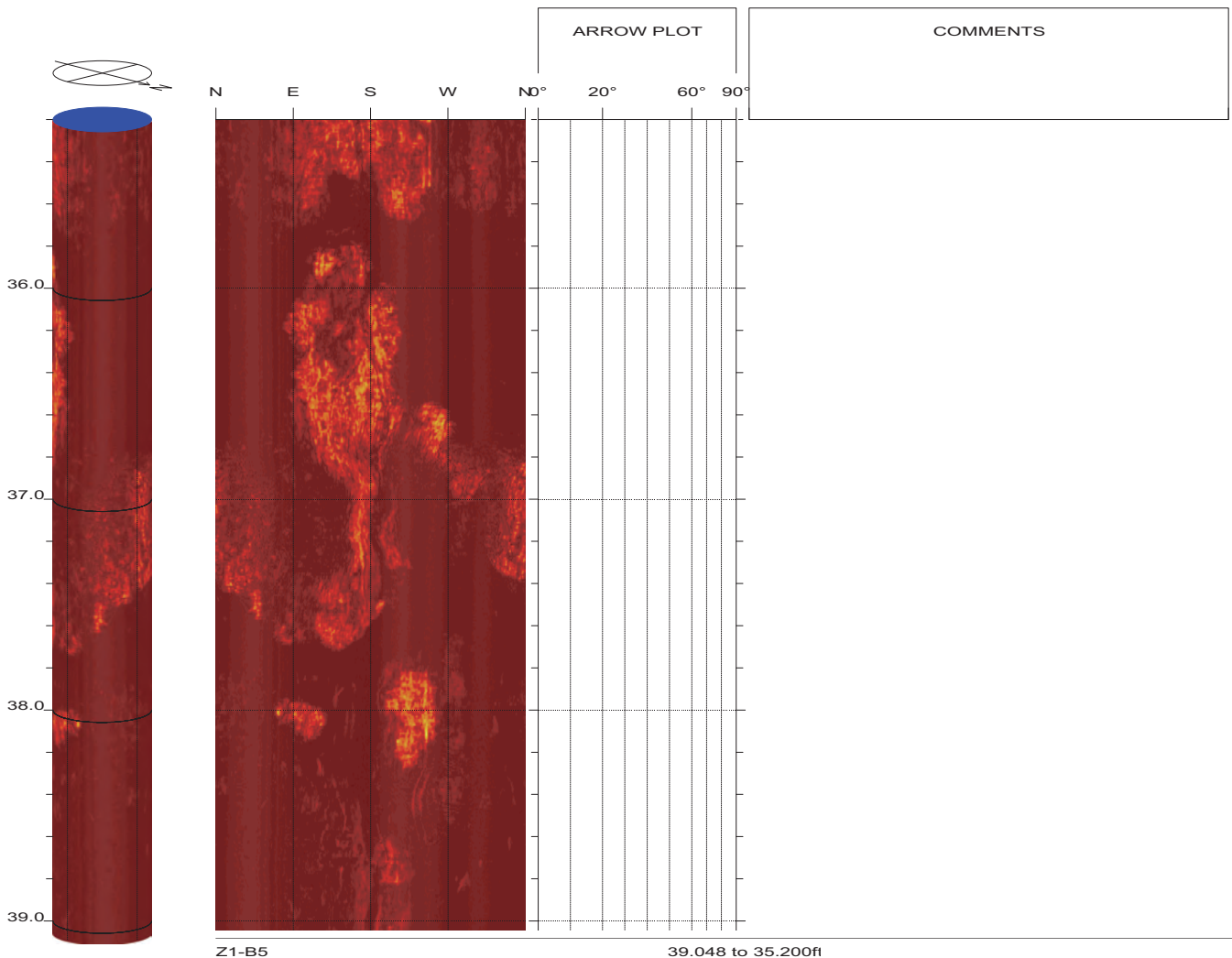
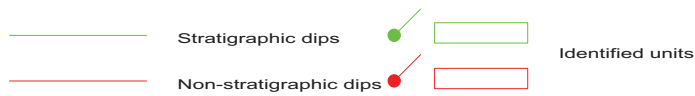
SR-710 TUNNEL INVESTIGATION

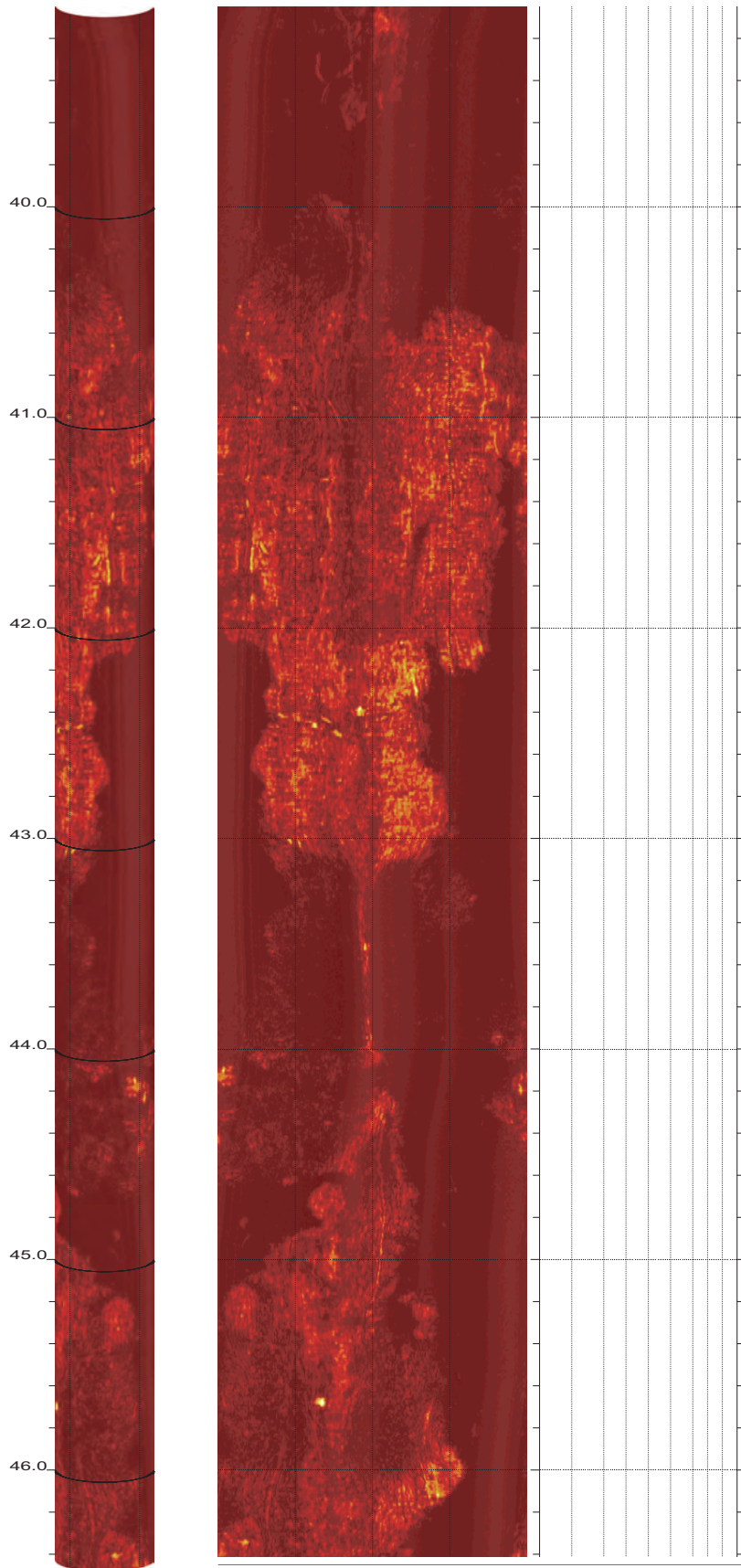
top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

Zone from 499.200 to 35.200ft  
 Format: BHTV-NESWN

Borehole diam: 5.600inch  
 Vertical = borehole-axis  
 Image: Amplitude





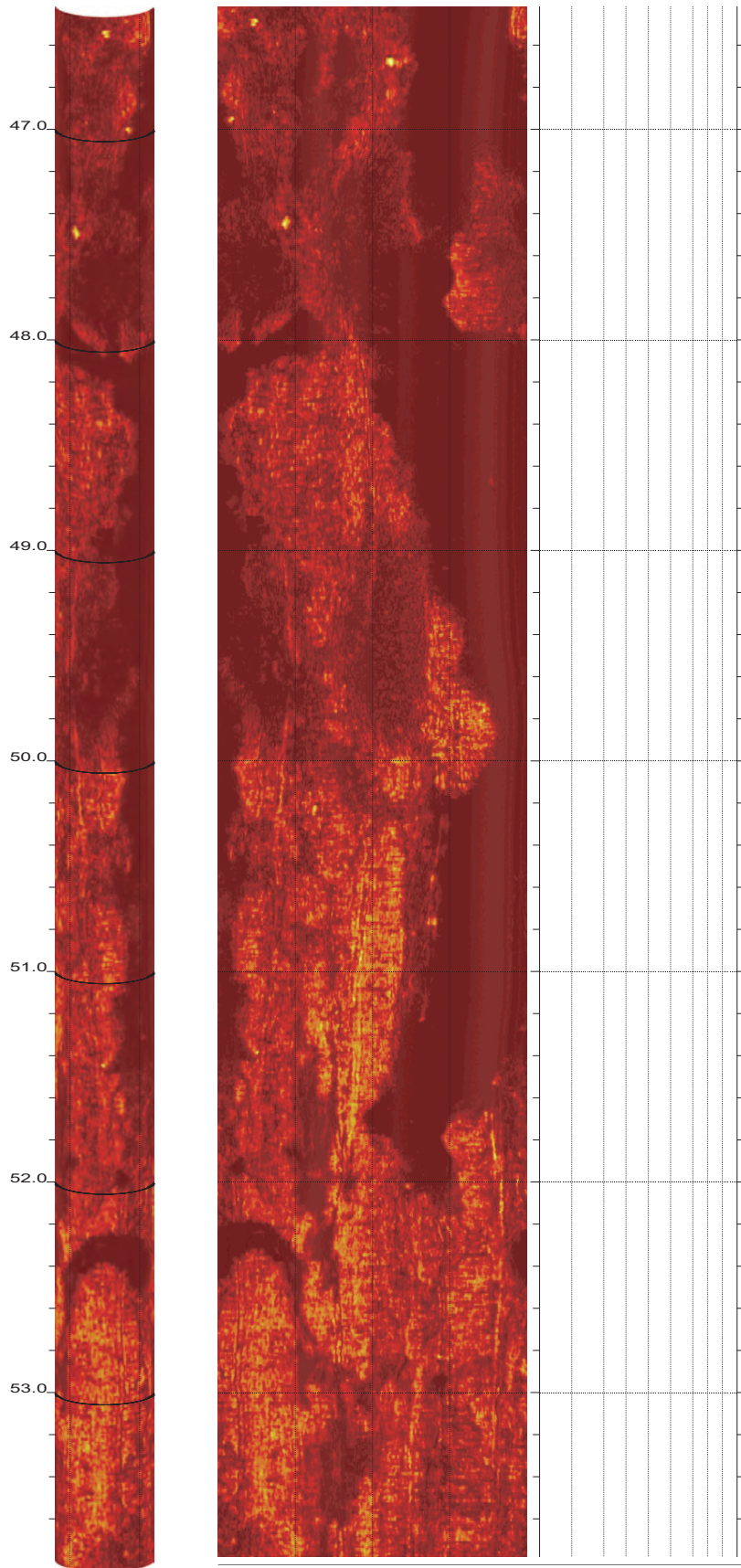
Z1-B5

46.416 to 39.048ft

2

SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 2 of 64



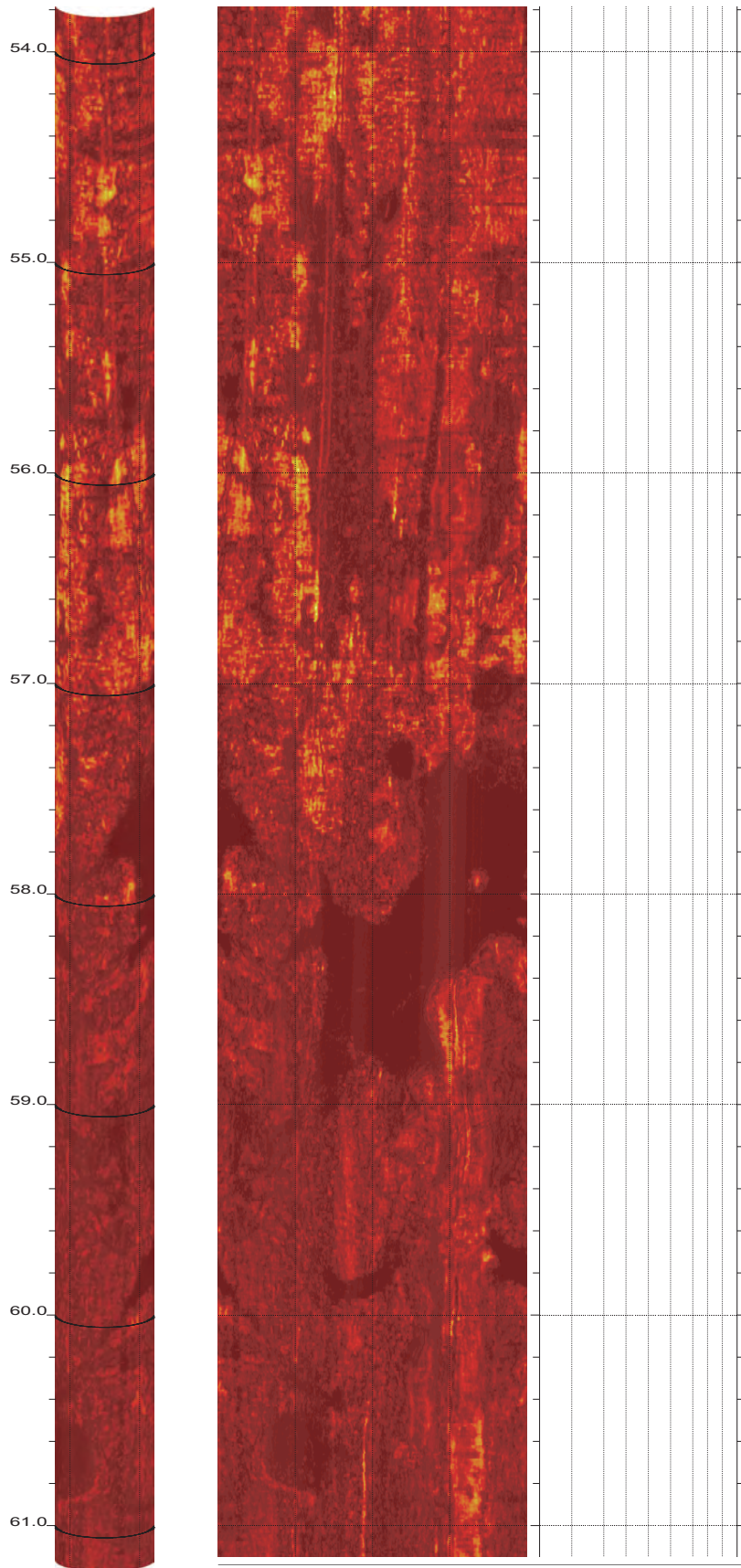


Z1-B5

53.784 to 46.416ft

3

SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 3 of 64

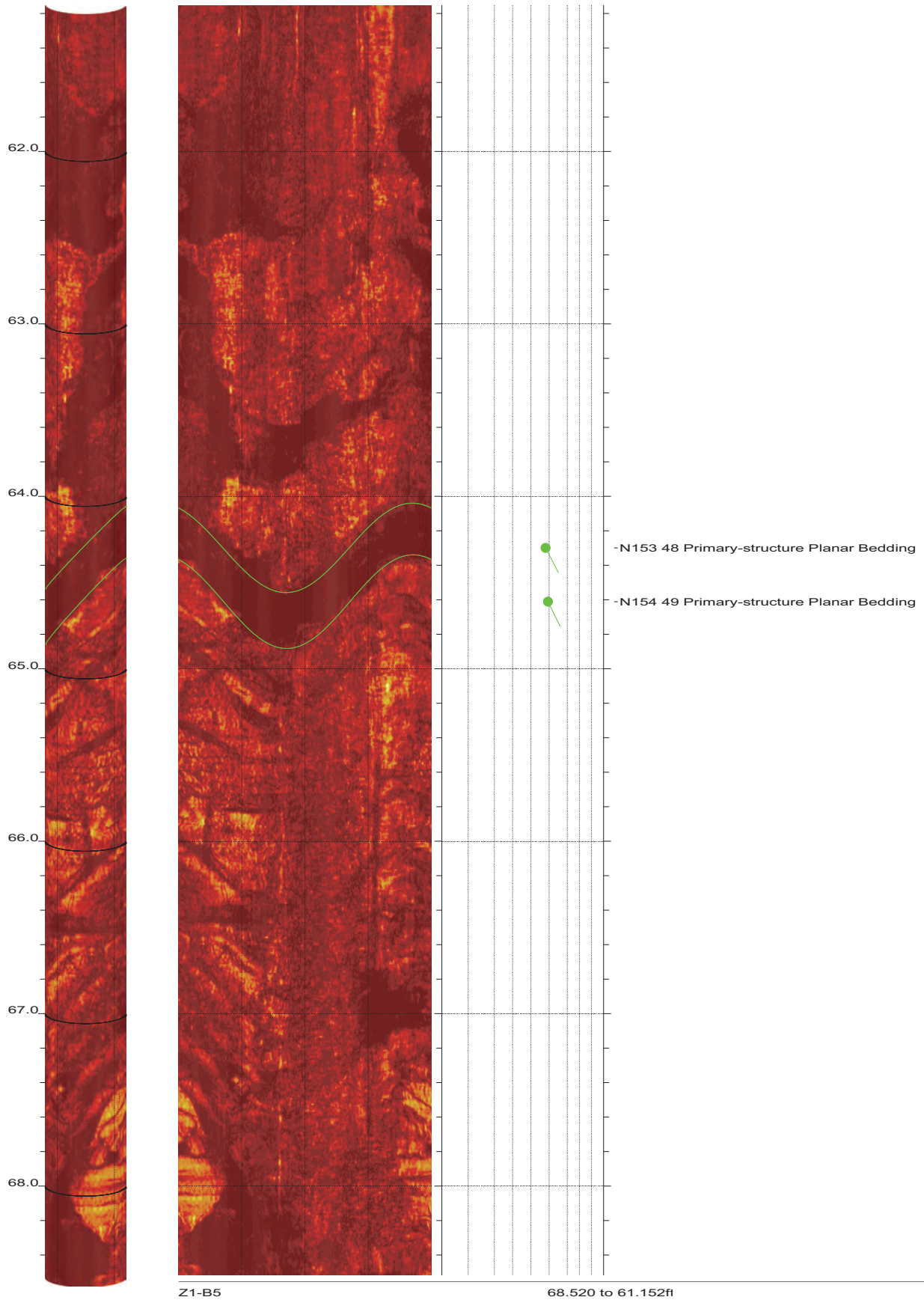


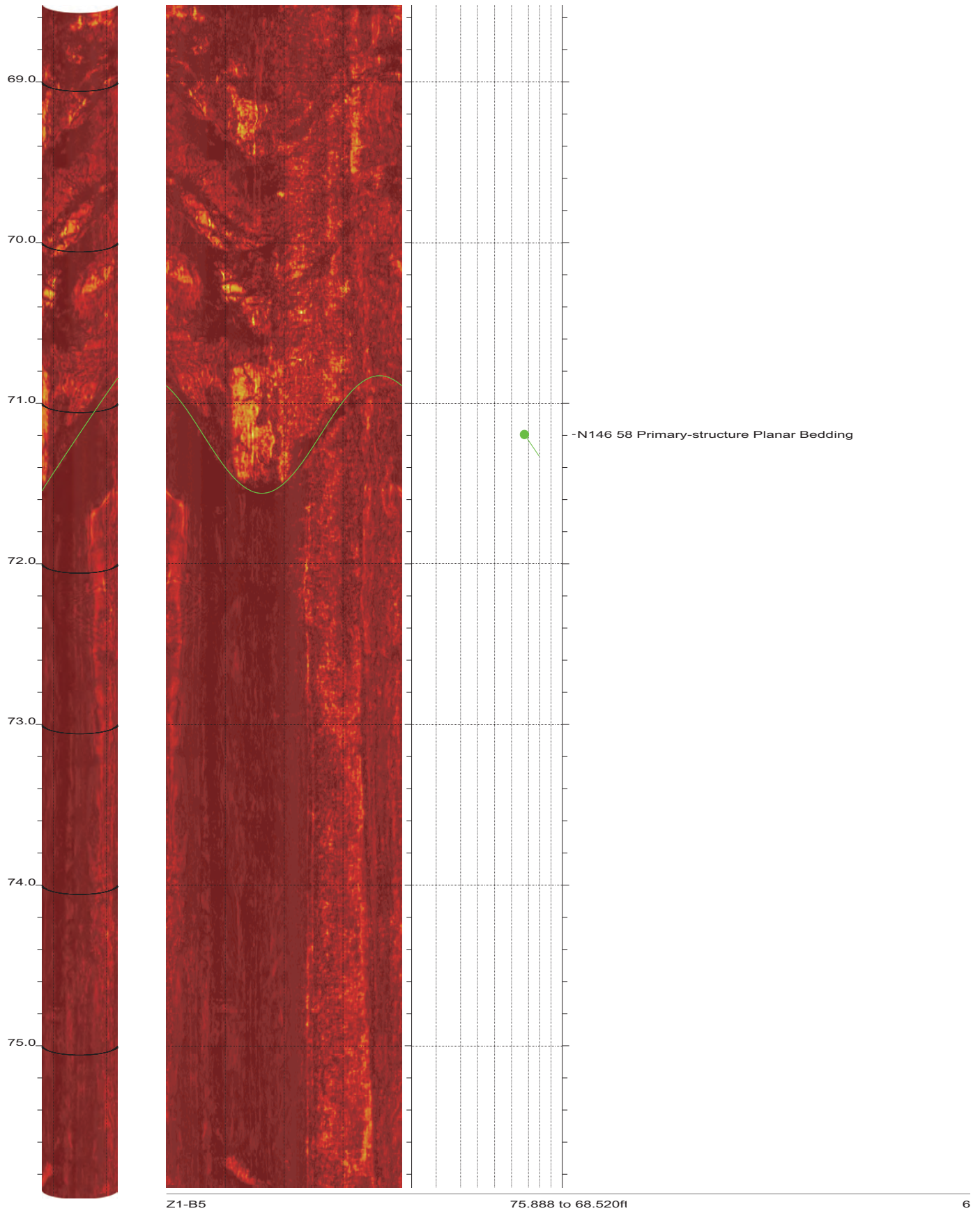
Z1-B5

61.152 to 53.784ft

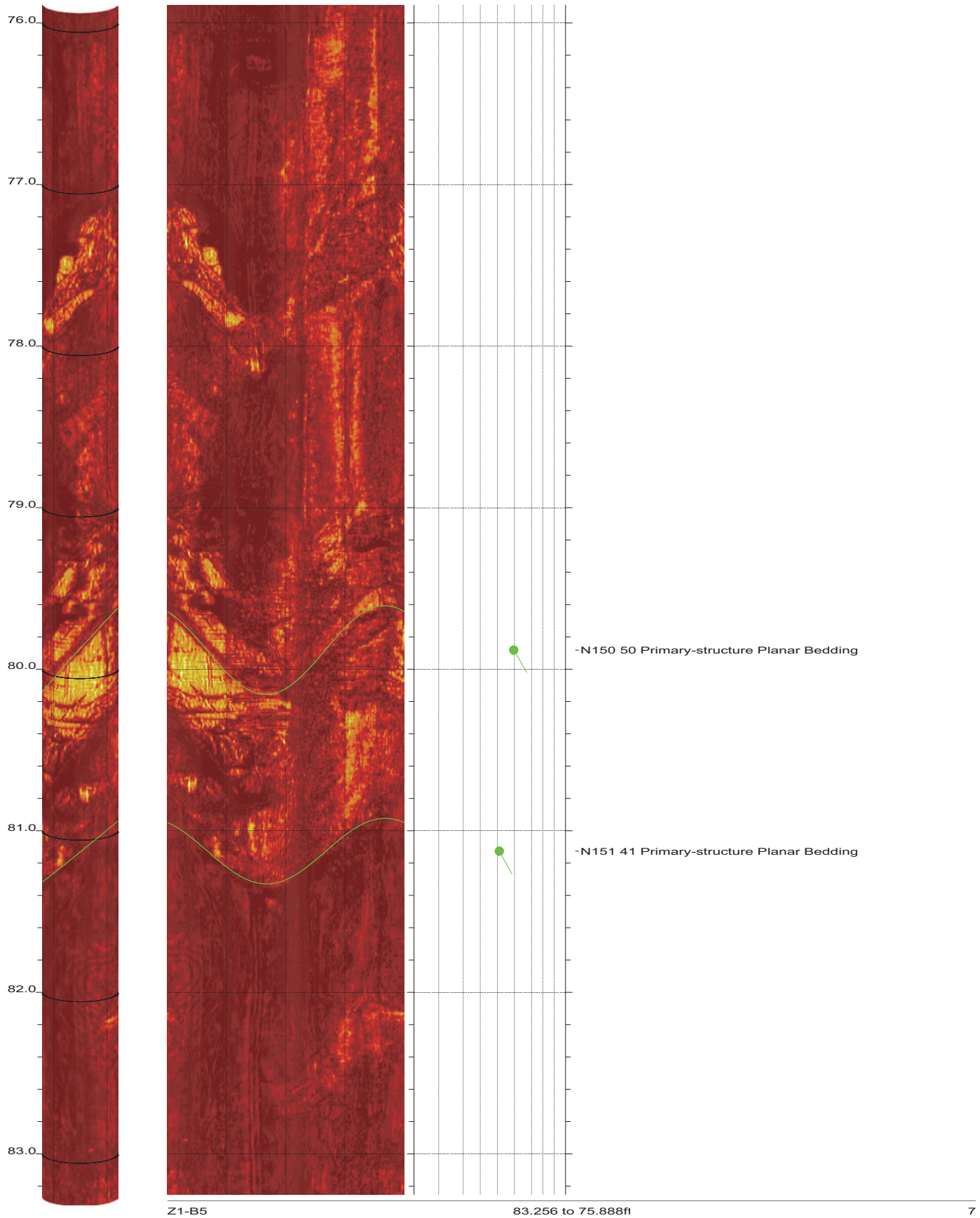
4

SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 4 of 64

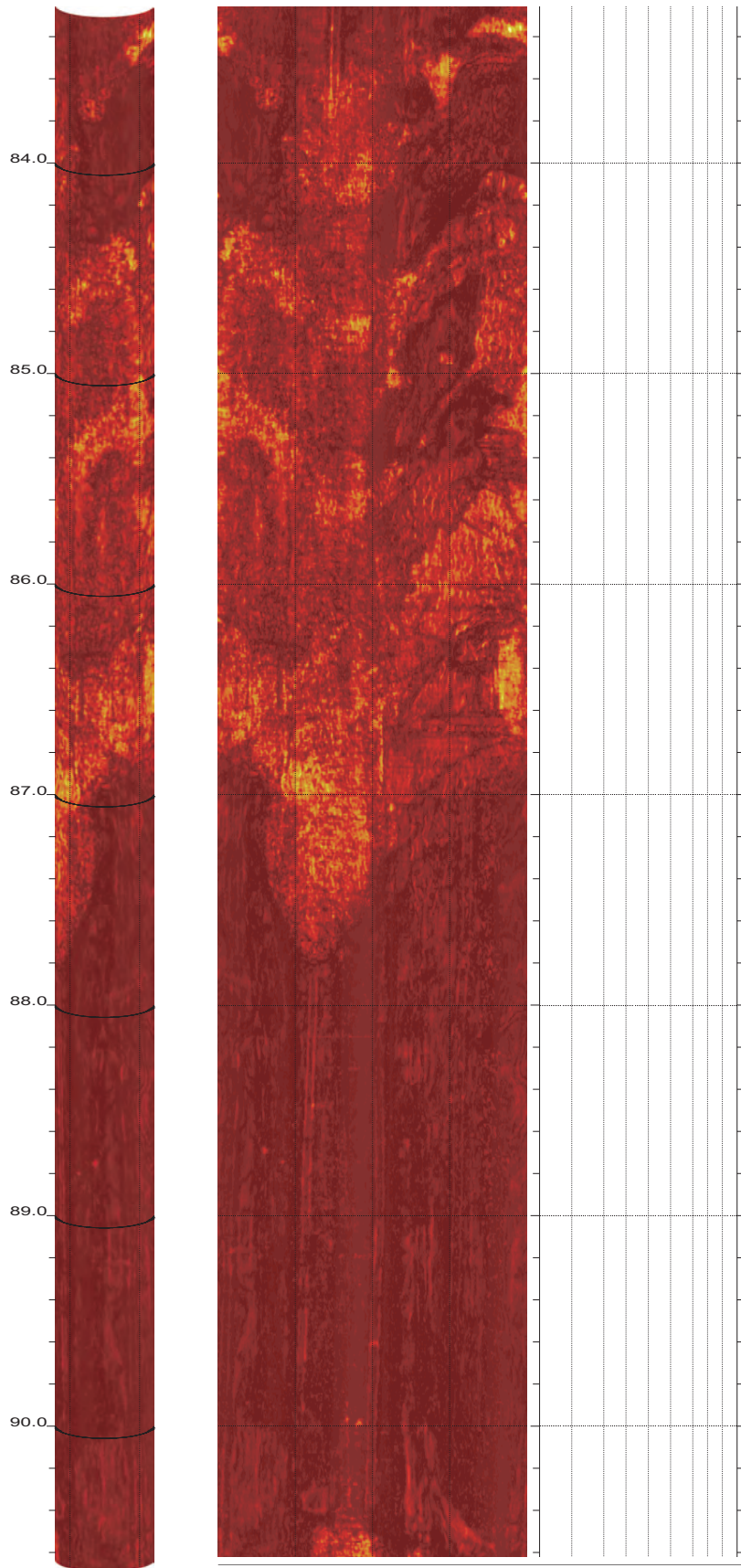




SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 6 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 7 of 64

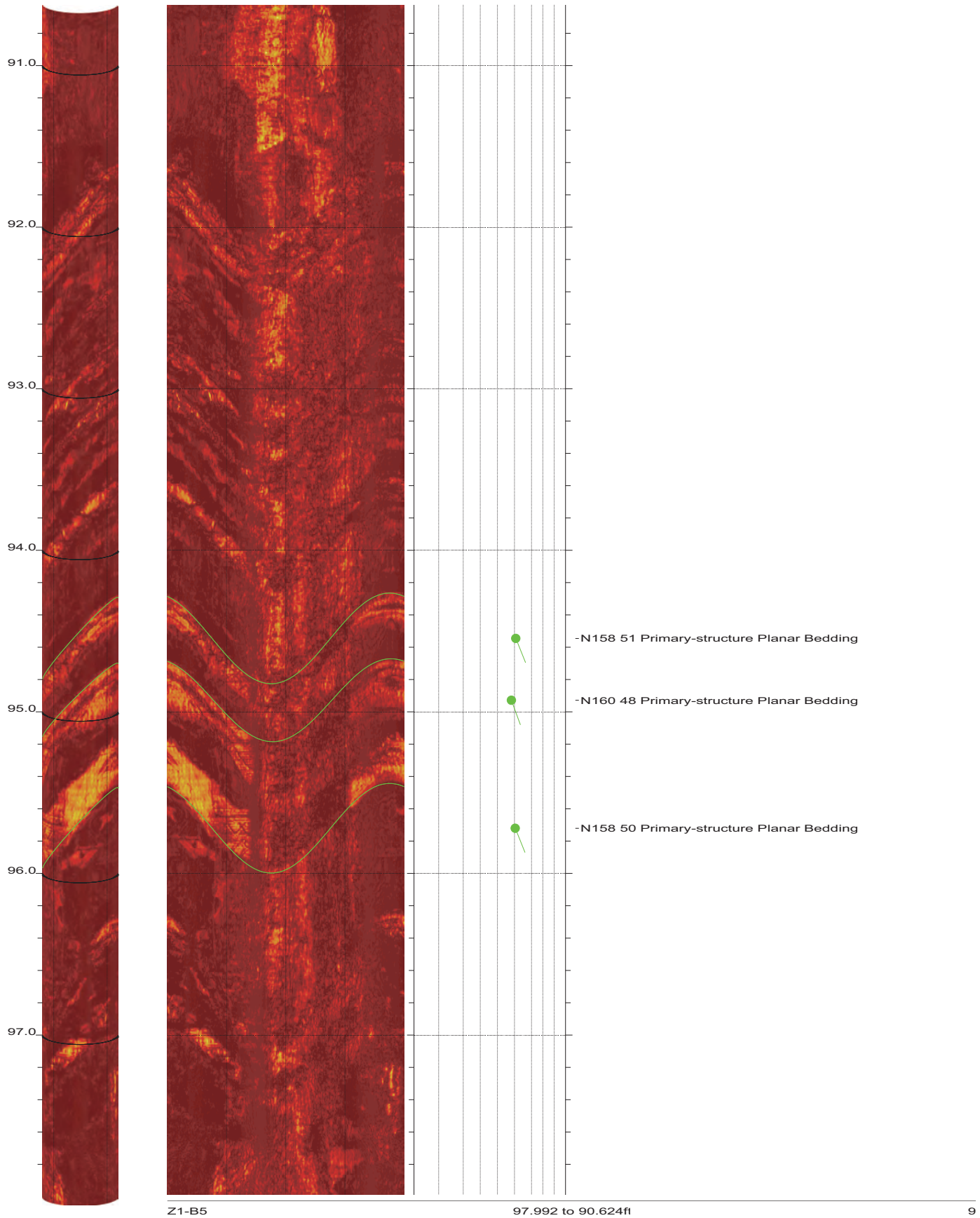


Z1-B5

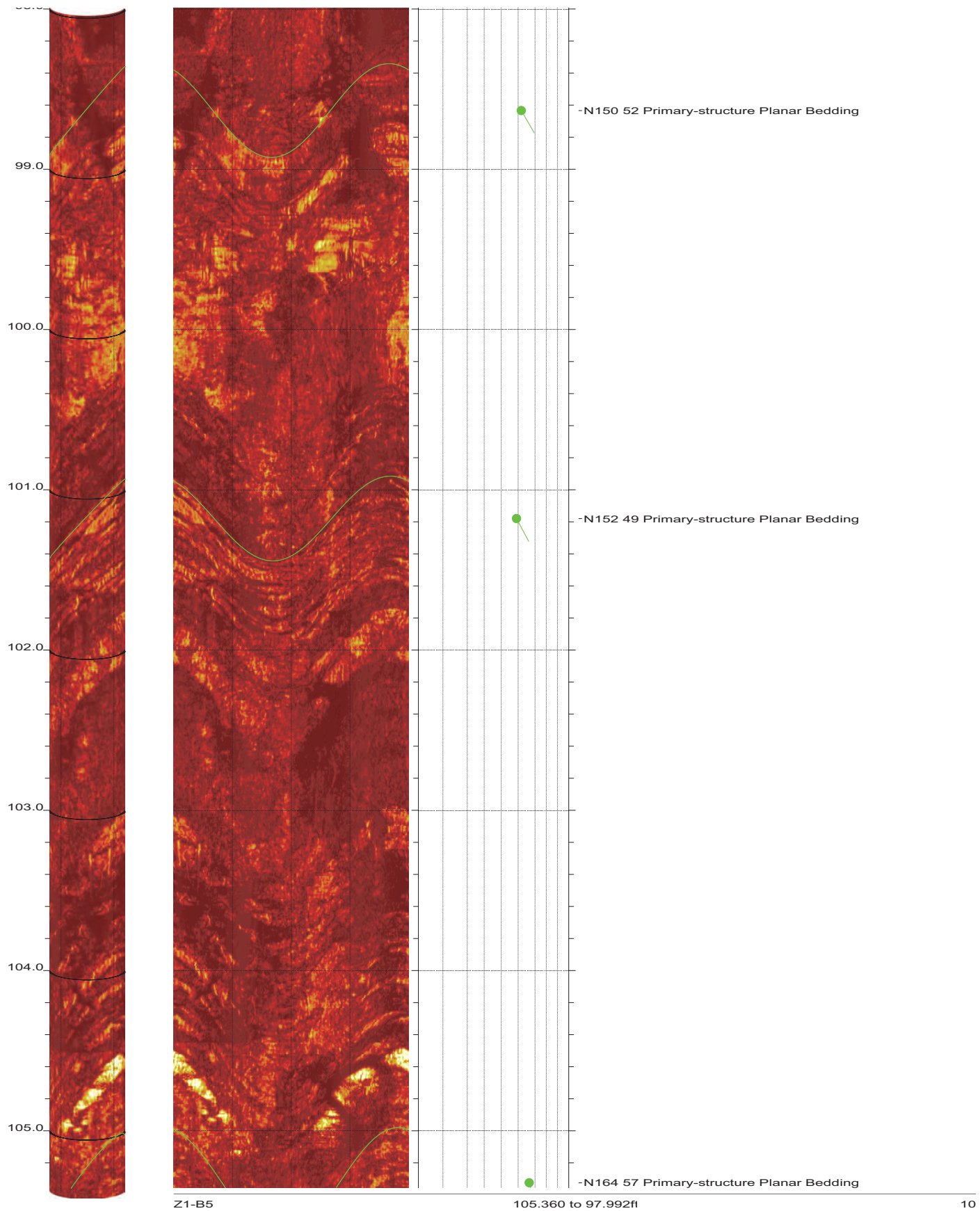
90.624 to 83.256ft

8

SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 8 of 64

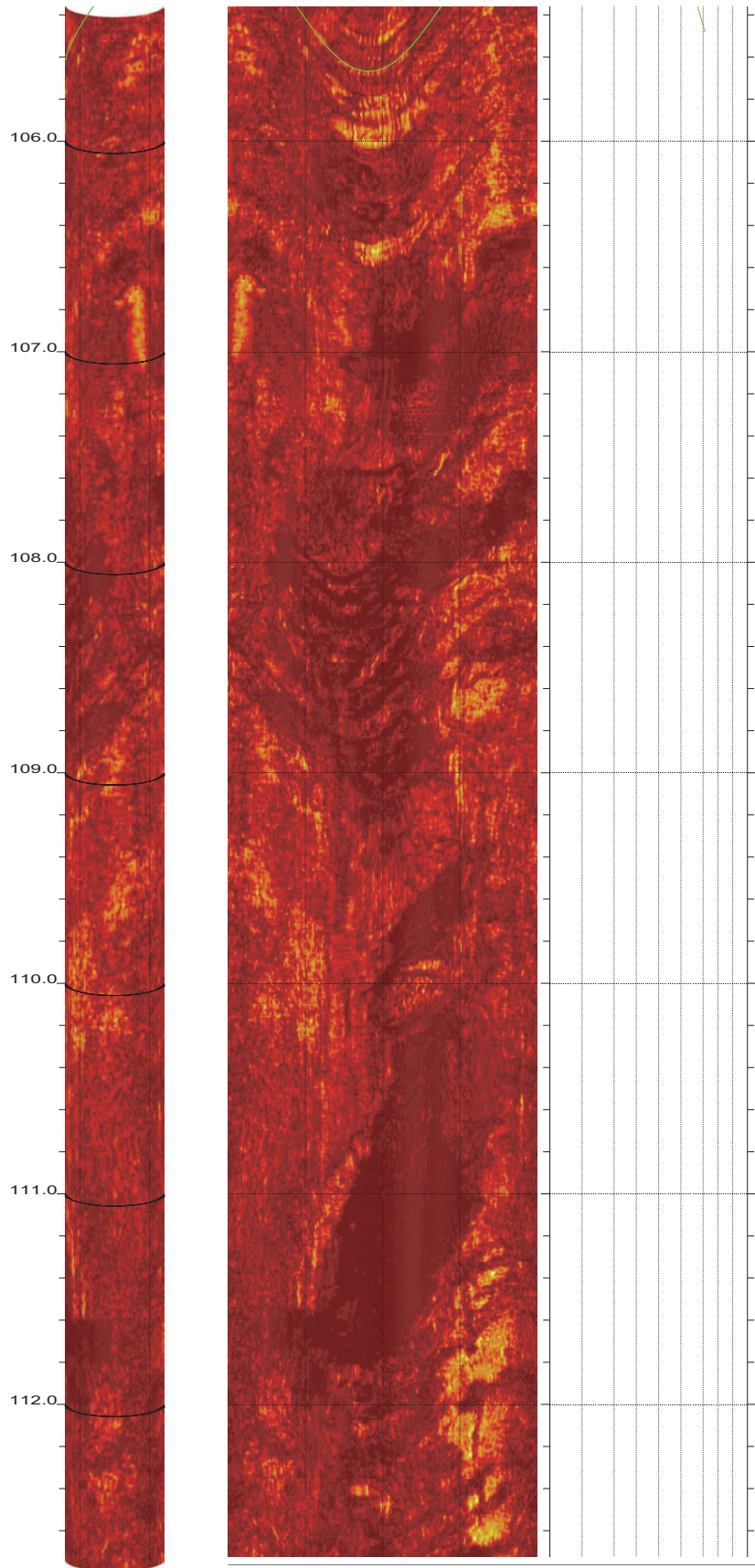


SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 9 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 10 of 64



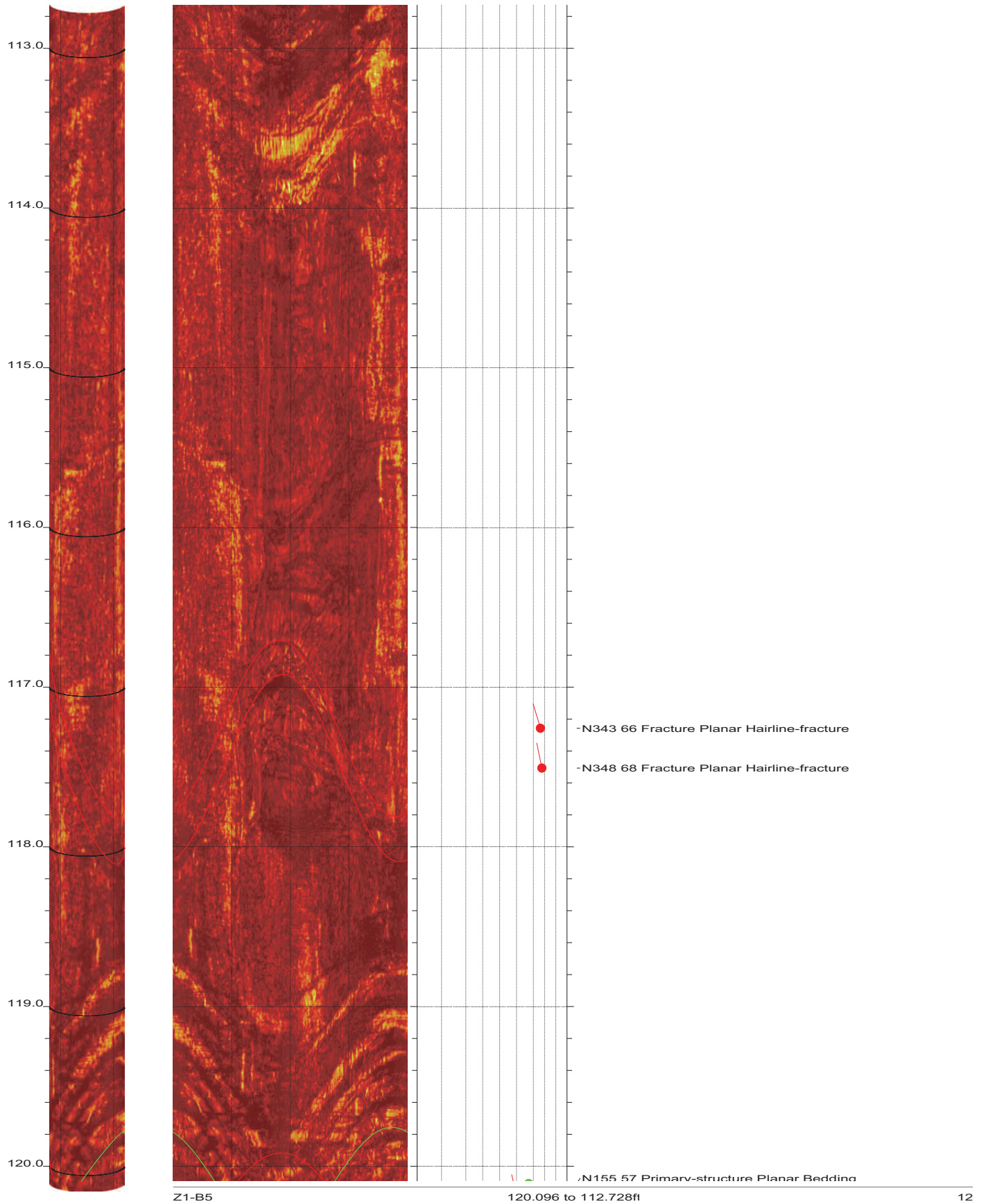


Z1-B5

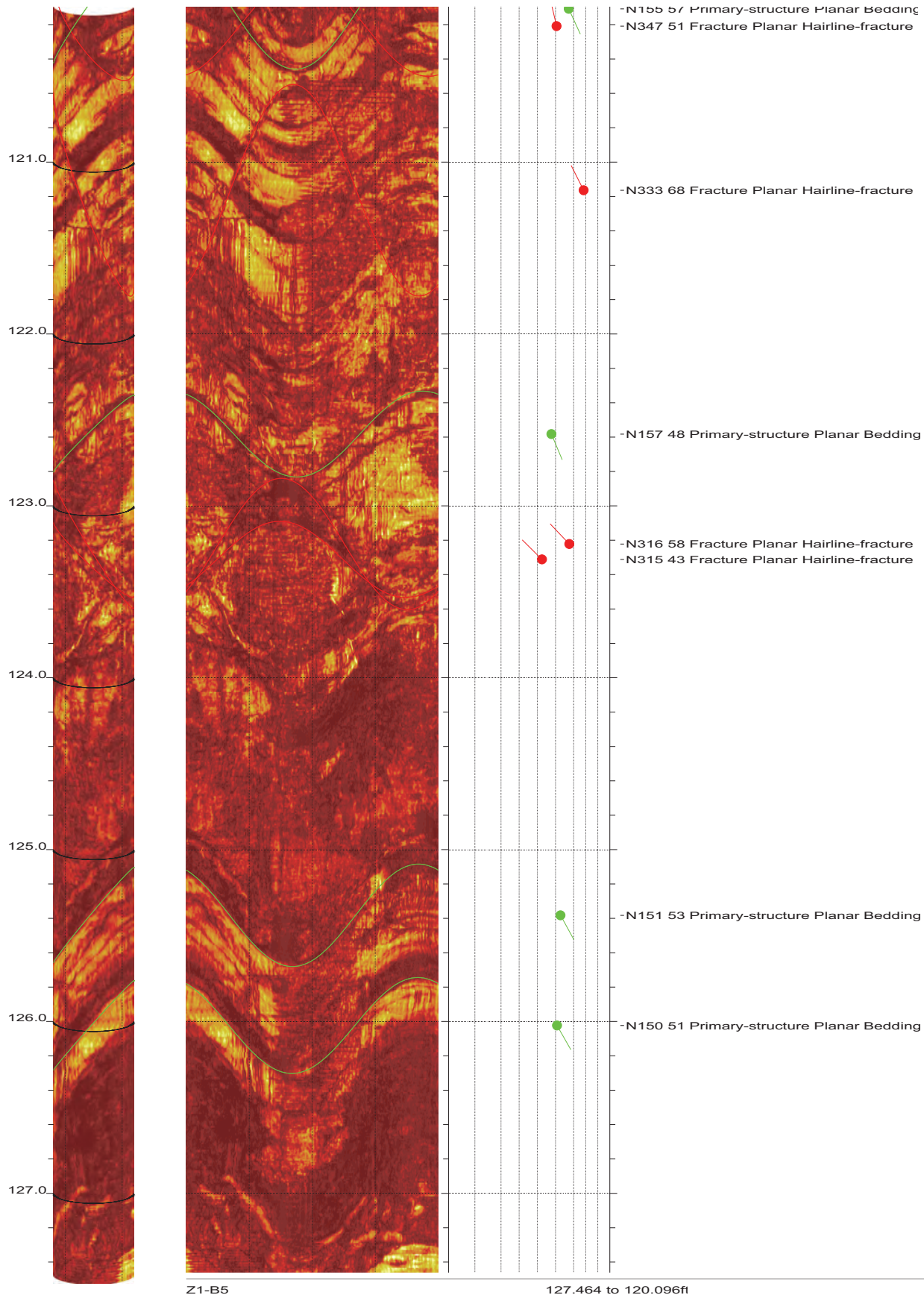
112.728 to 105.360ft

11

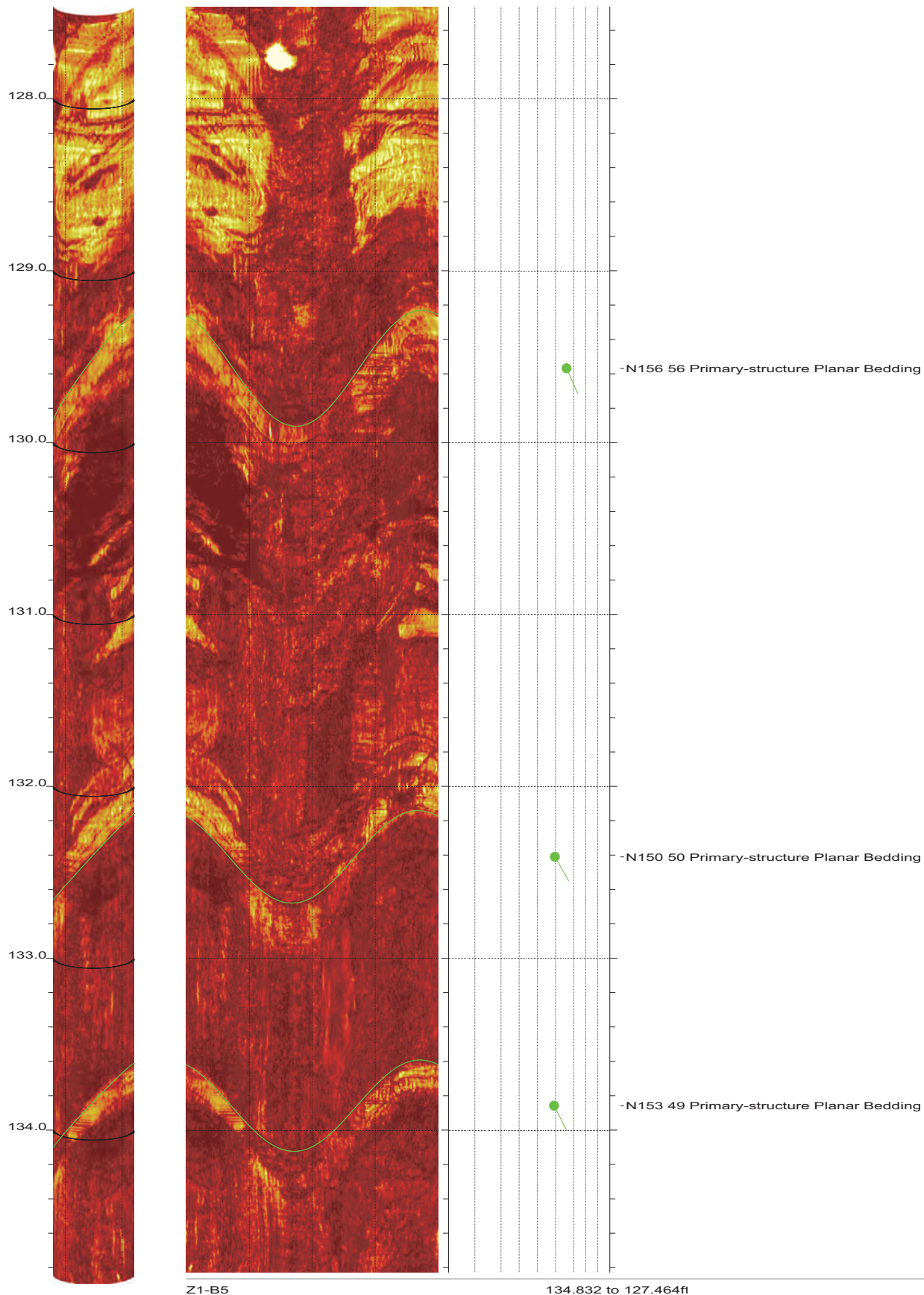
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 11 of 64



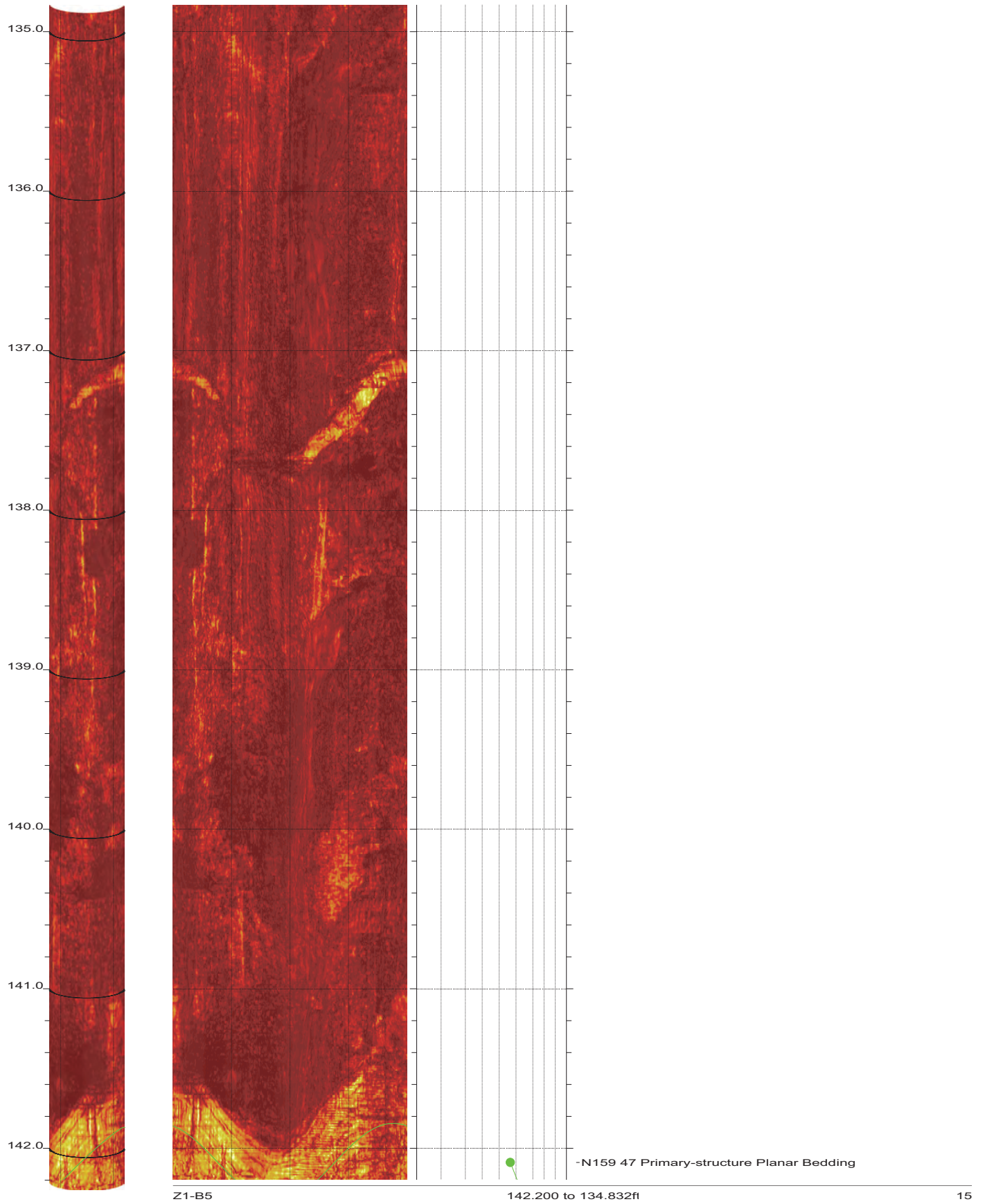
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 12 of 64



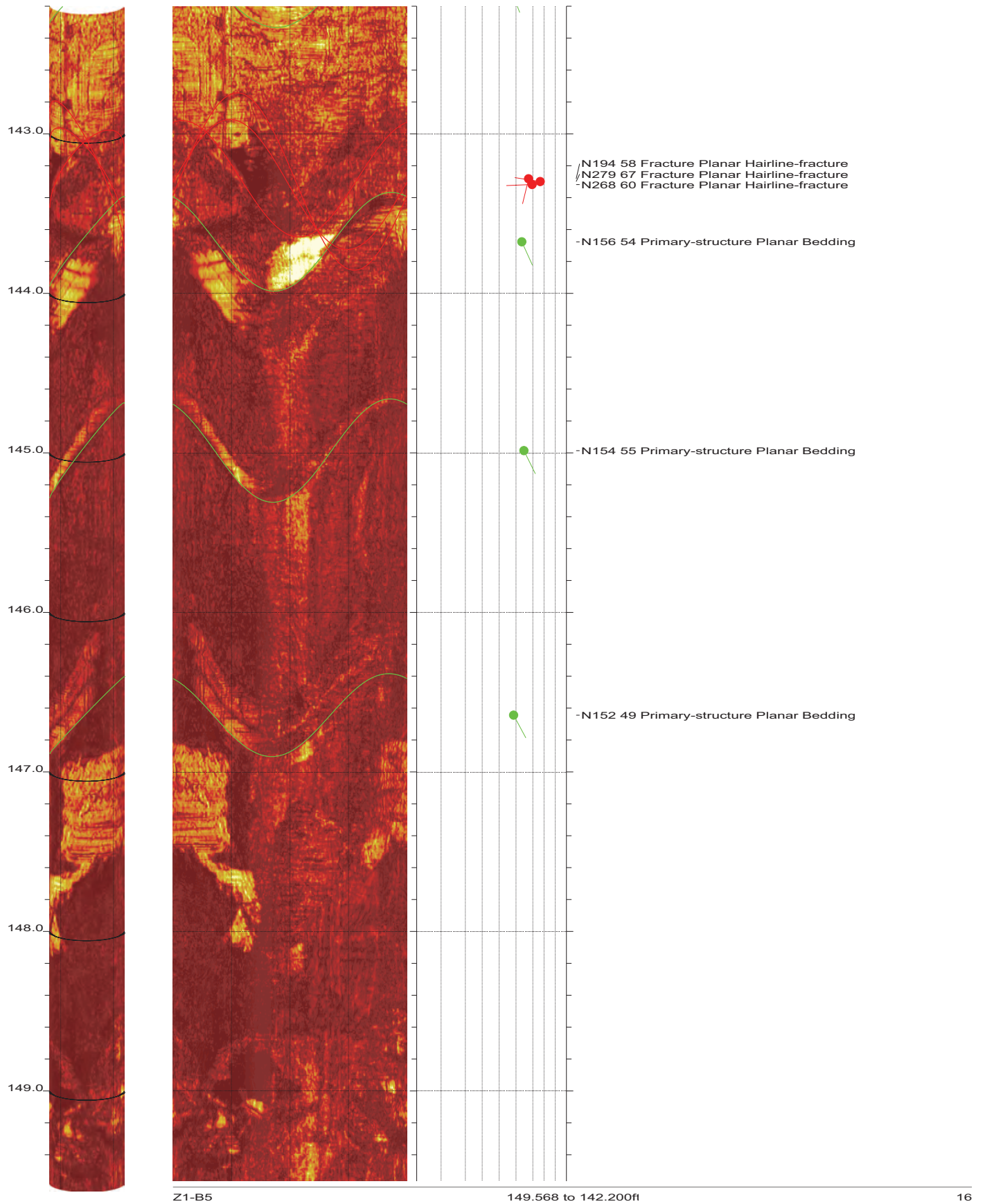
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 13 of 64



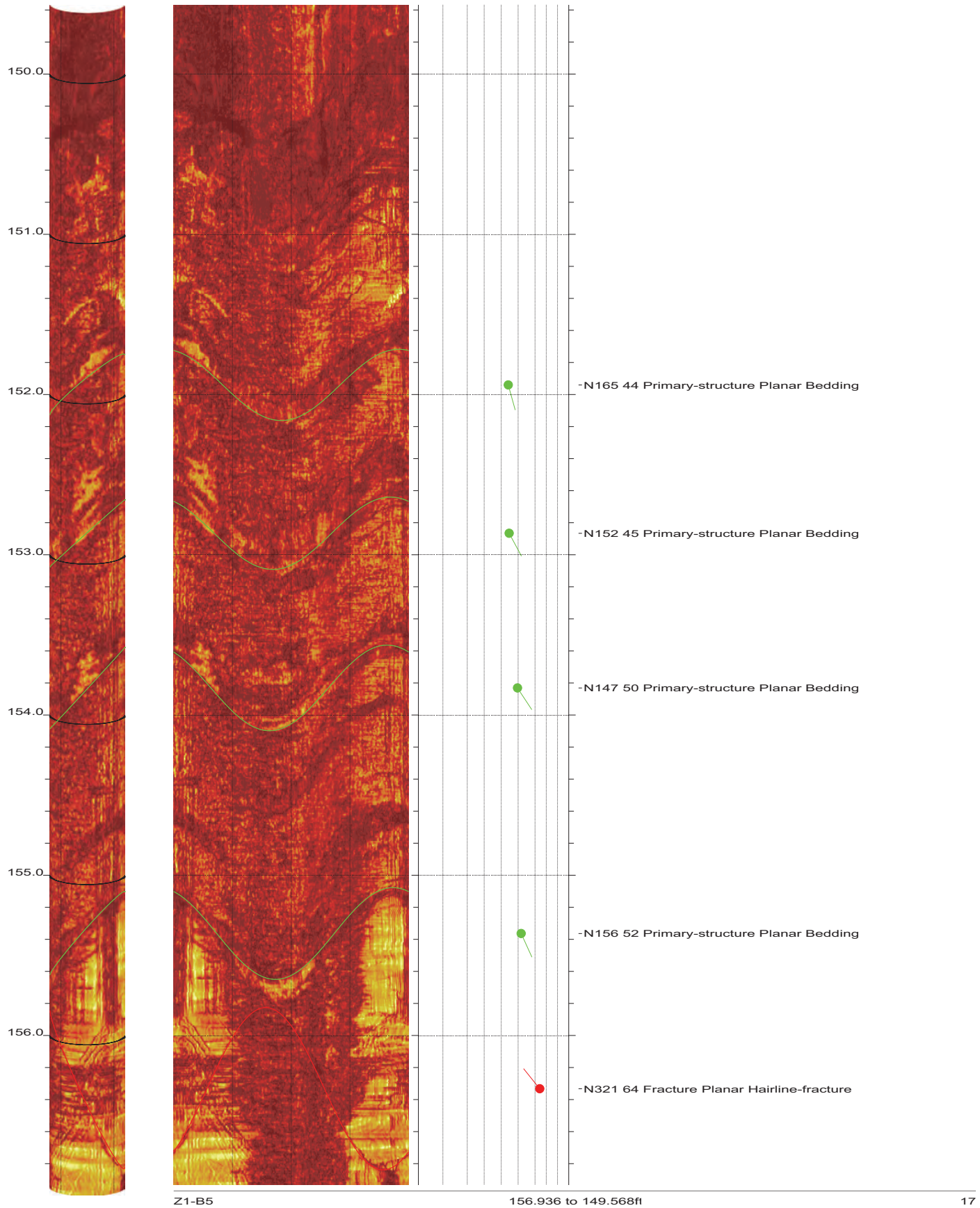
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 14 of 64



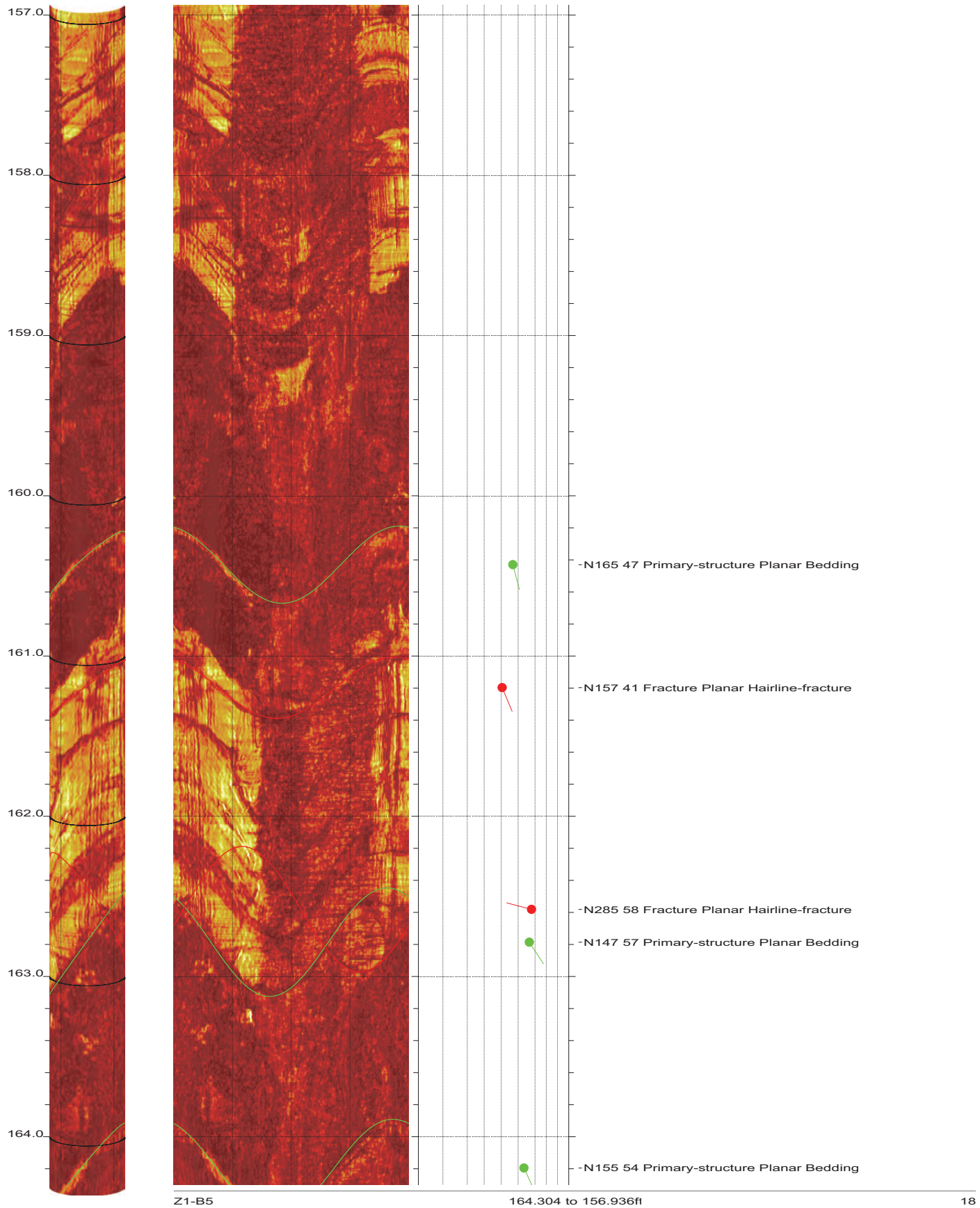
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 15 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 16 of 64

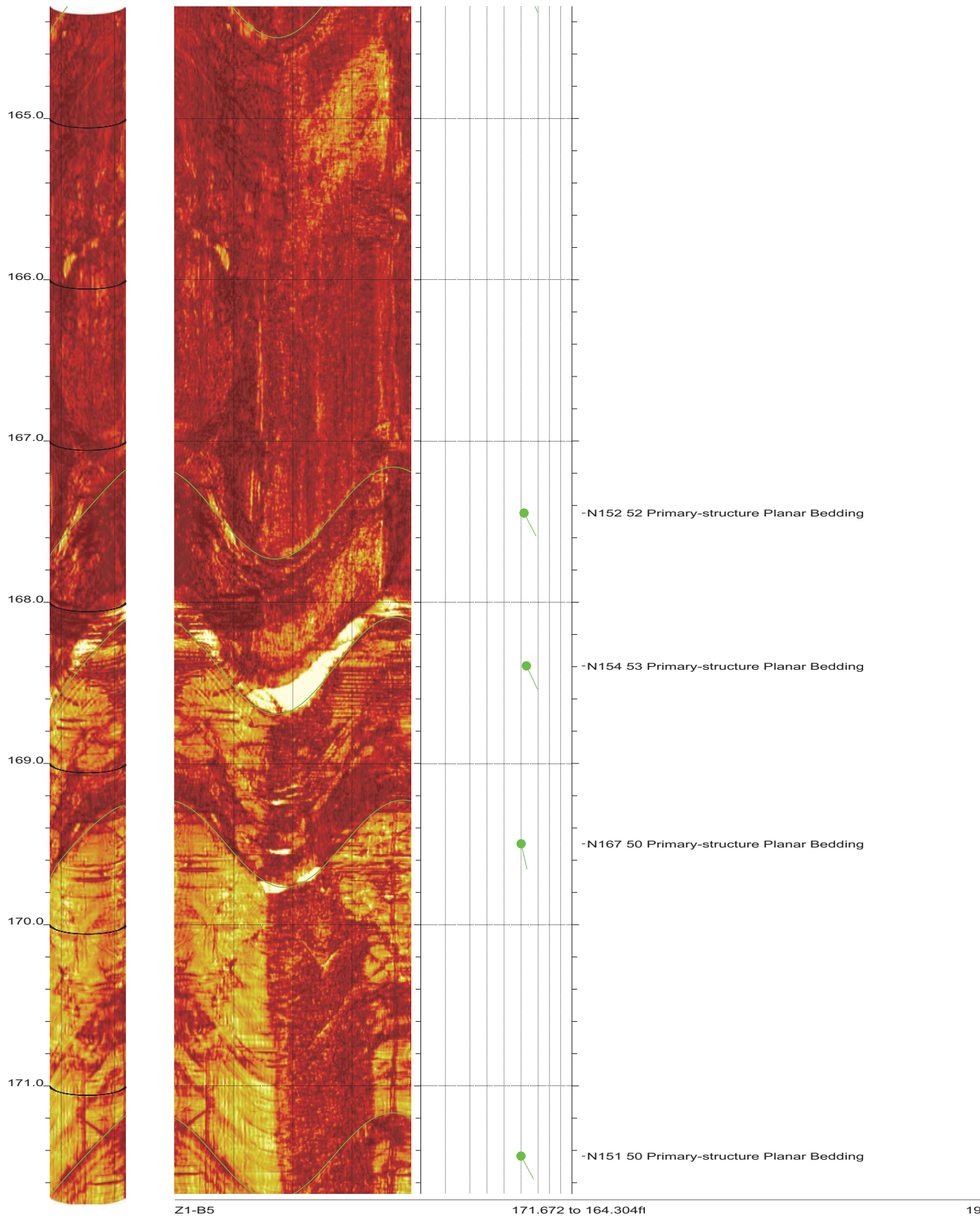


SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 17 of 64

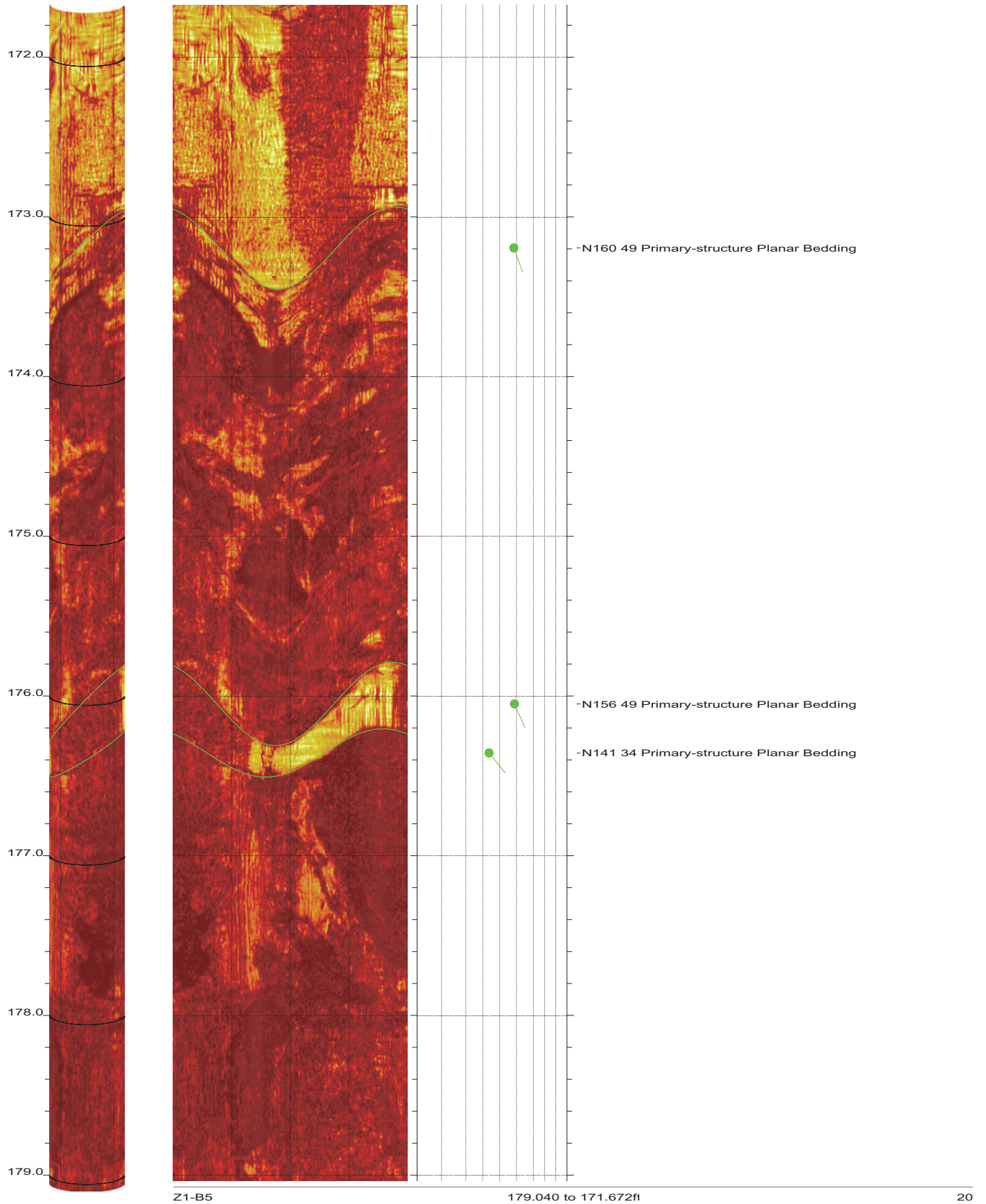


SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 18 of 64

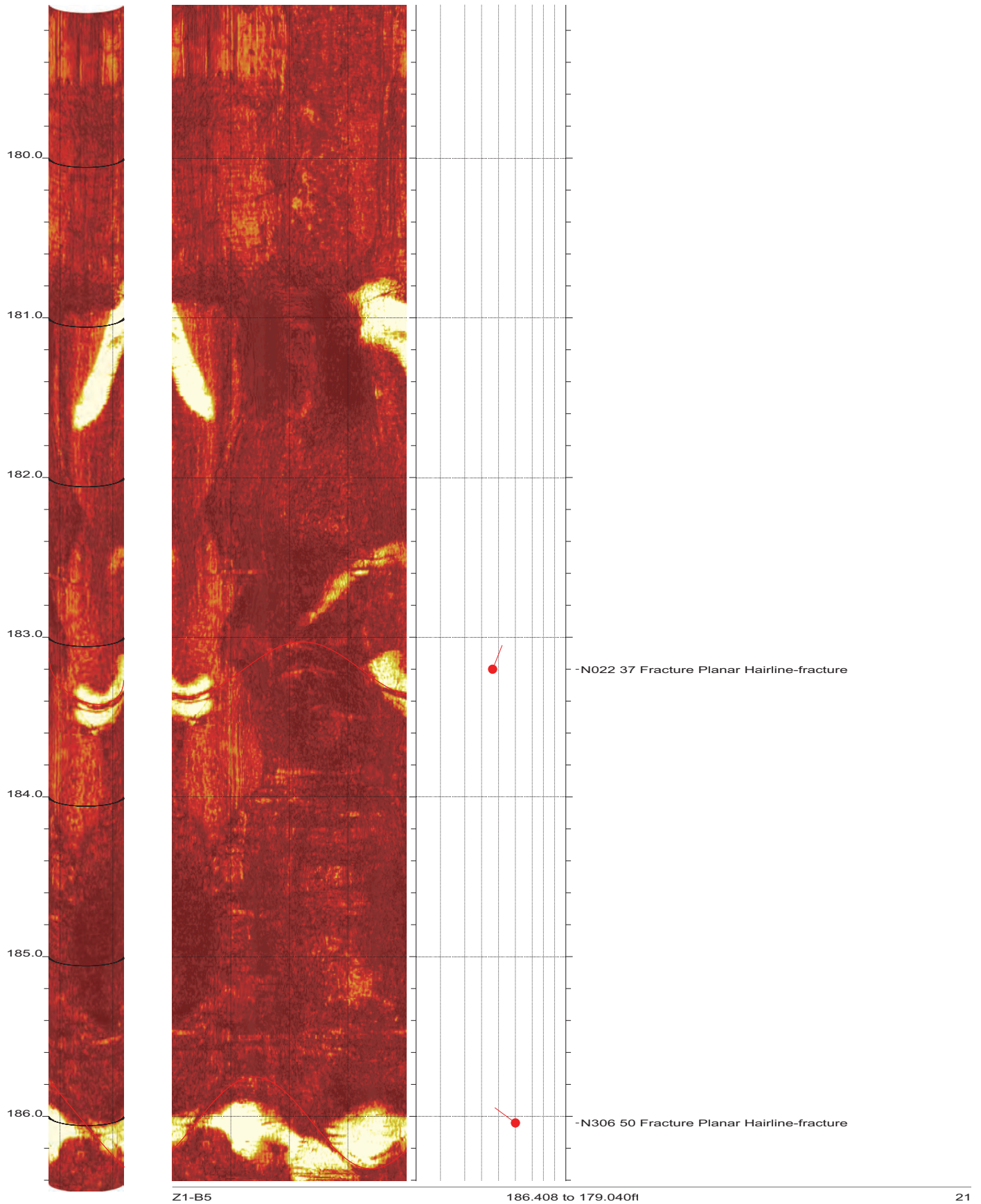




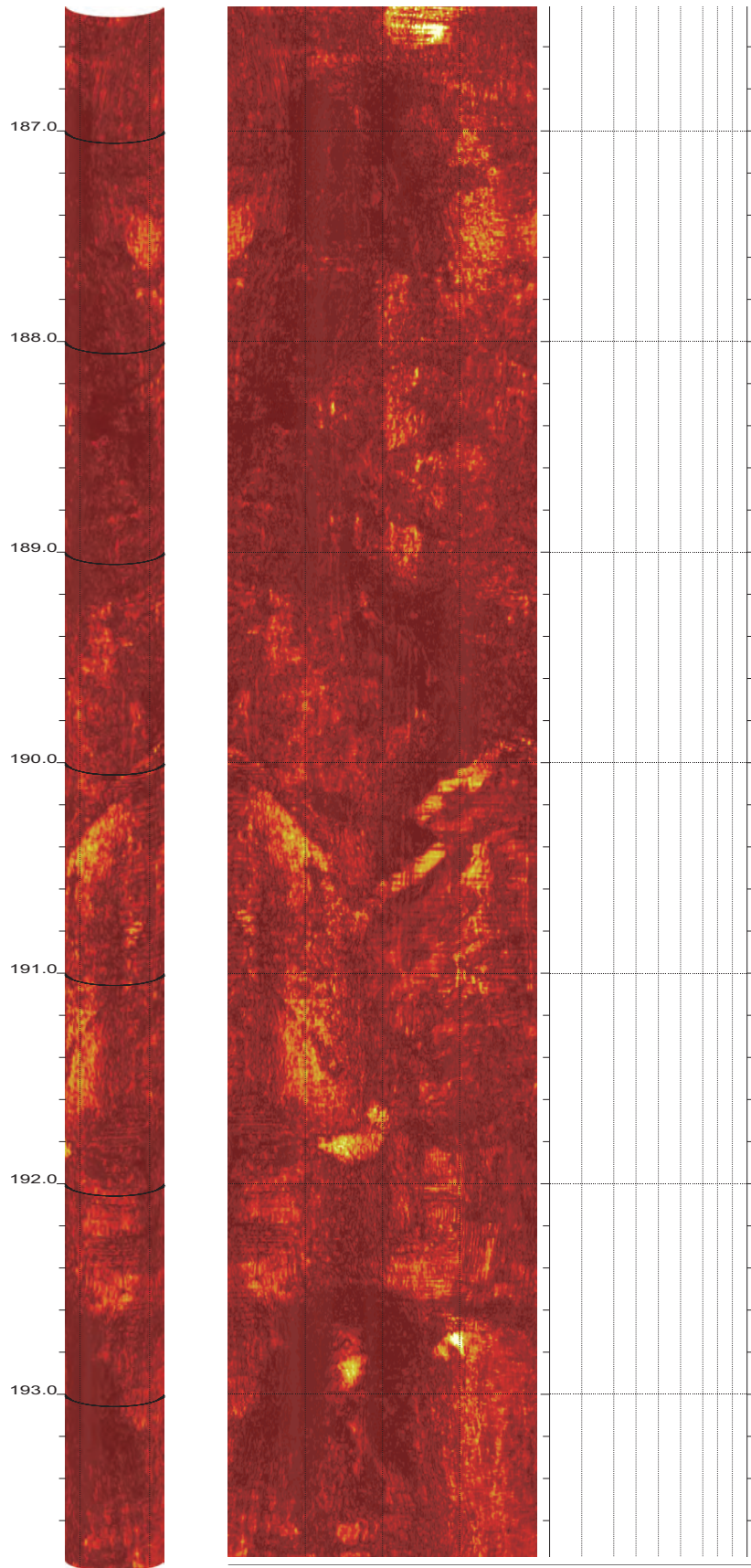
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 19 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 20 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 21 of 64

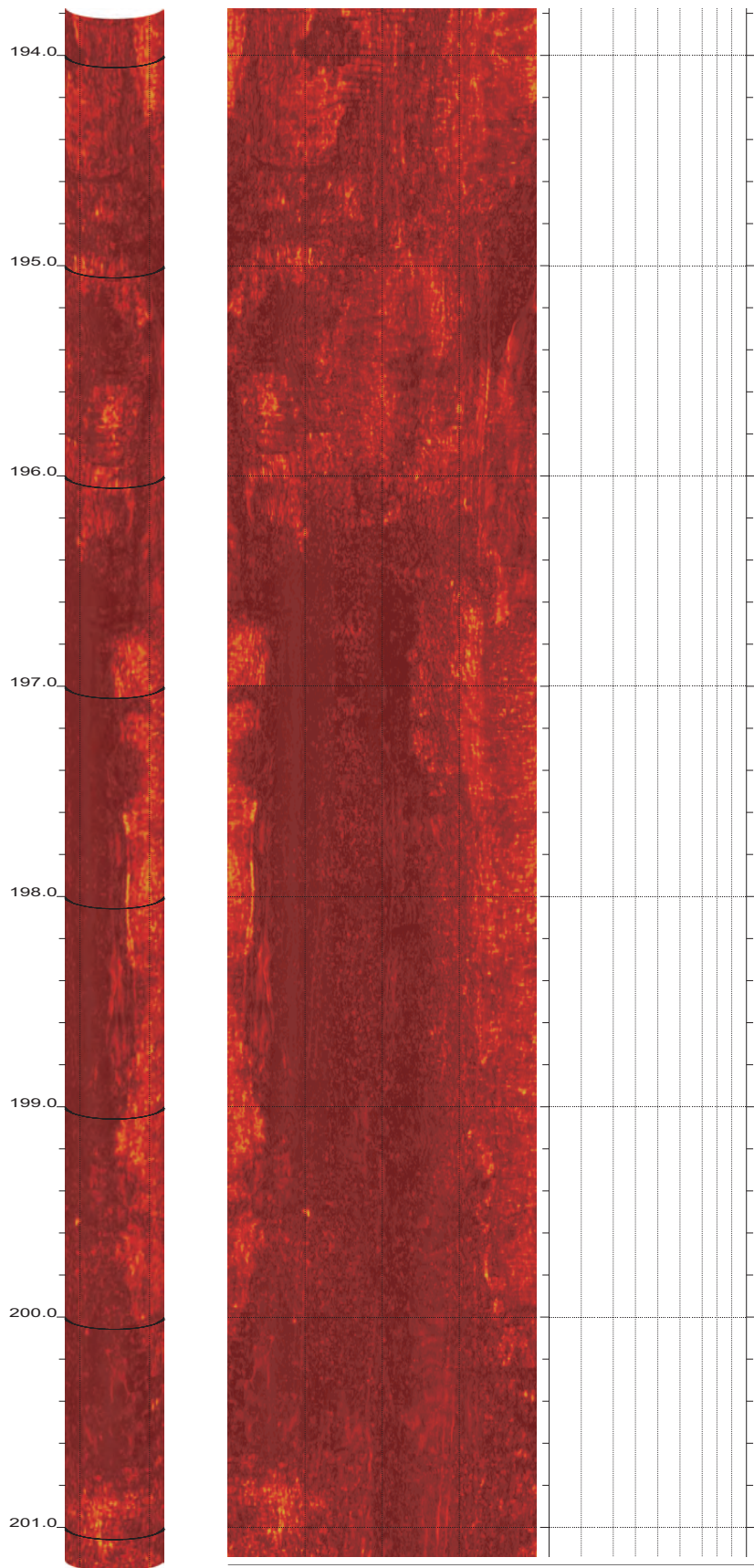


Z1-B5

193.776 to 186.408ft

22

SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 22 of 64

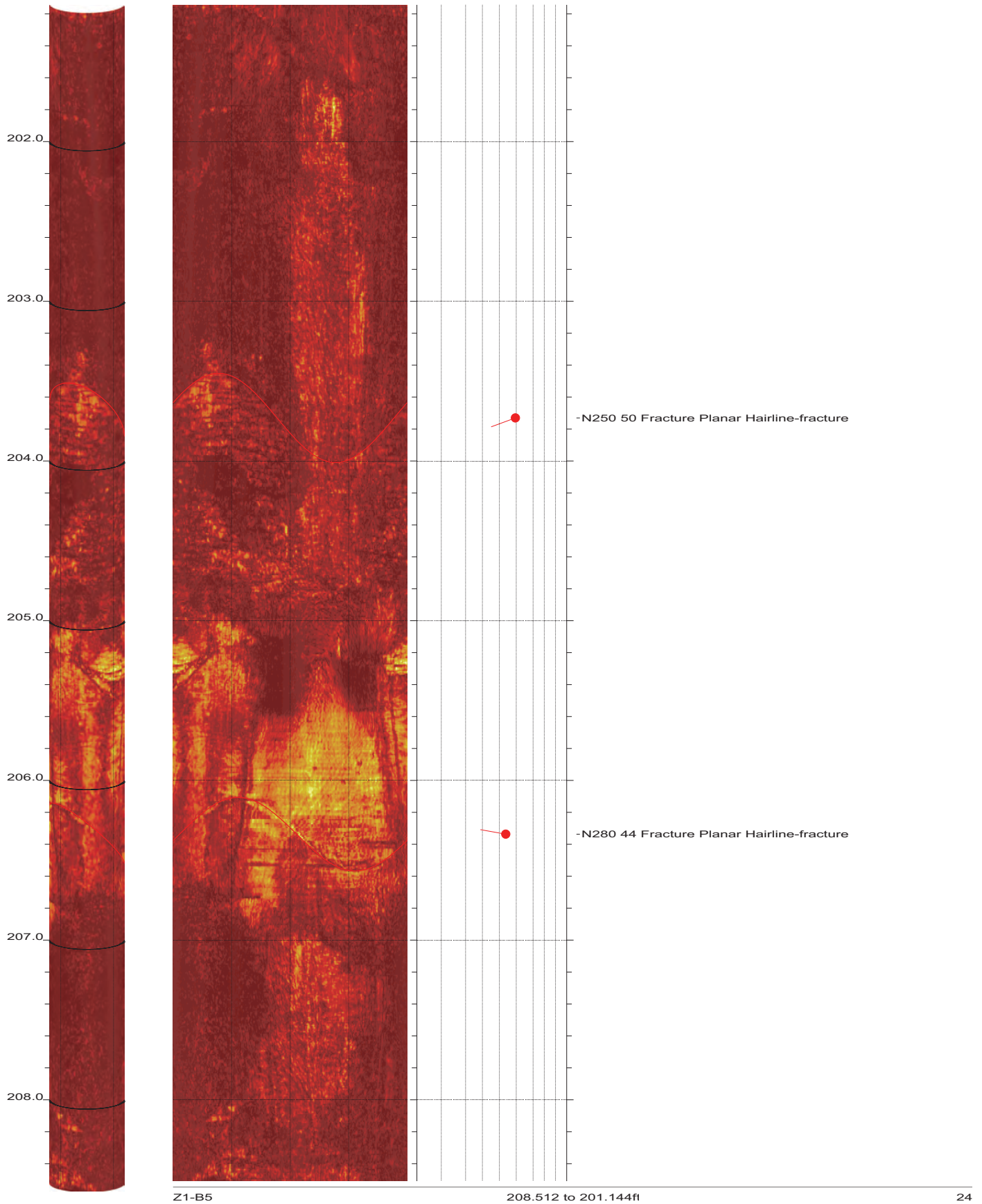


Z1-B5

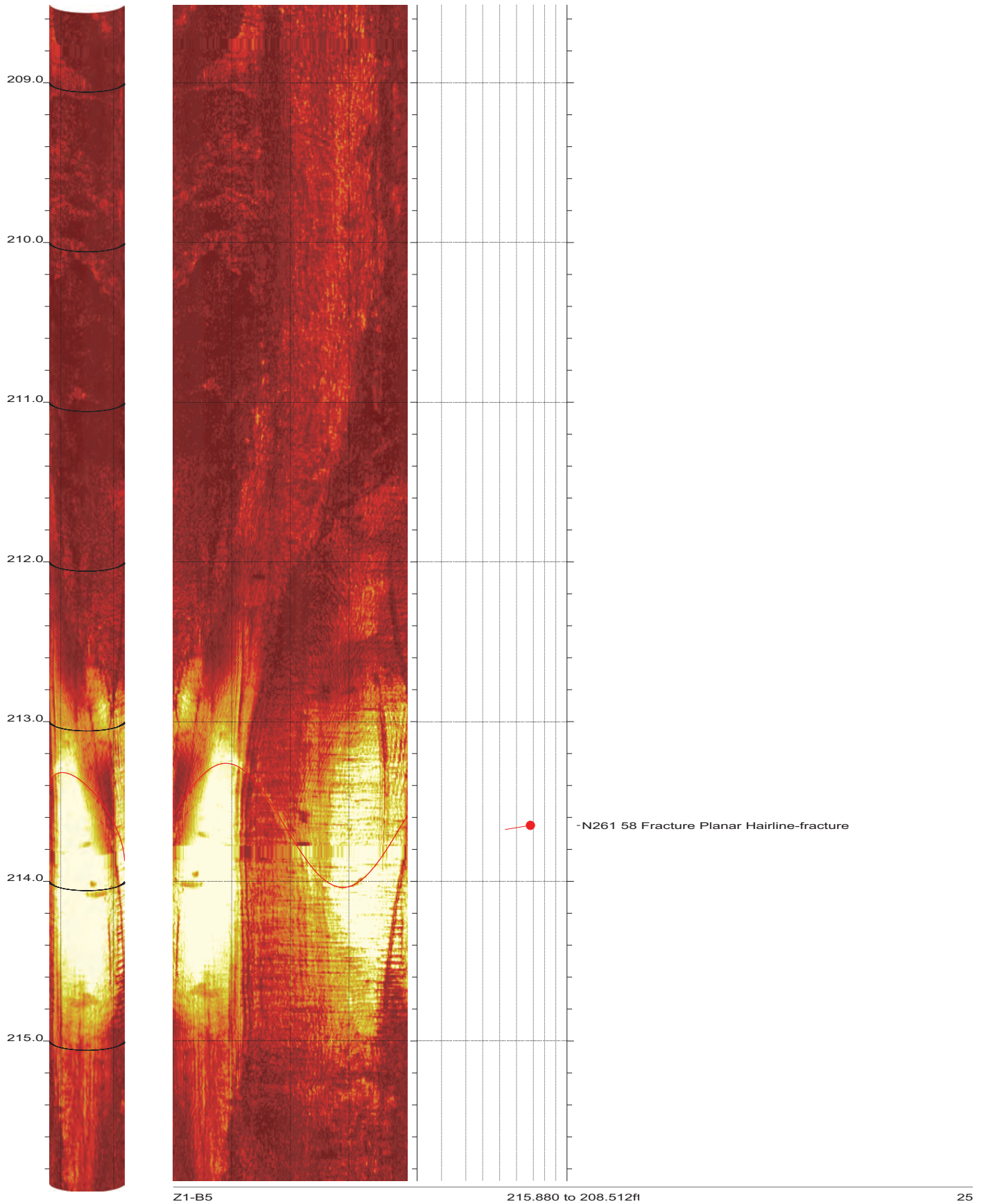
201.144 to 193.776ft

23

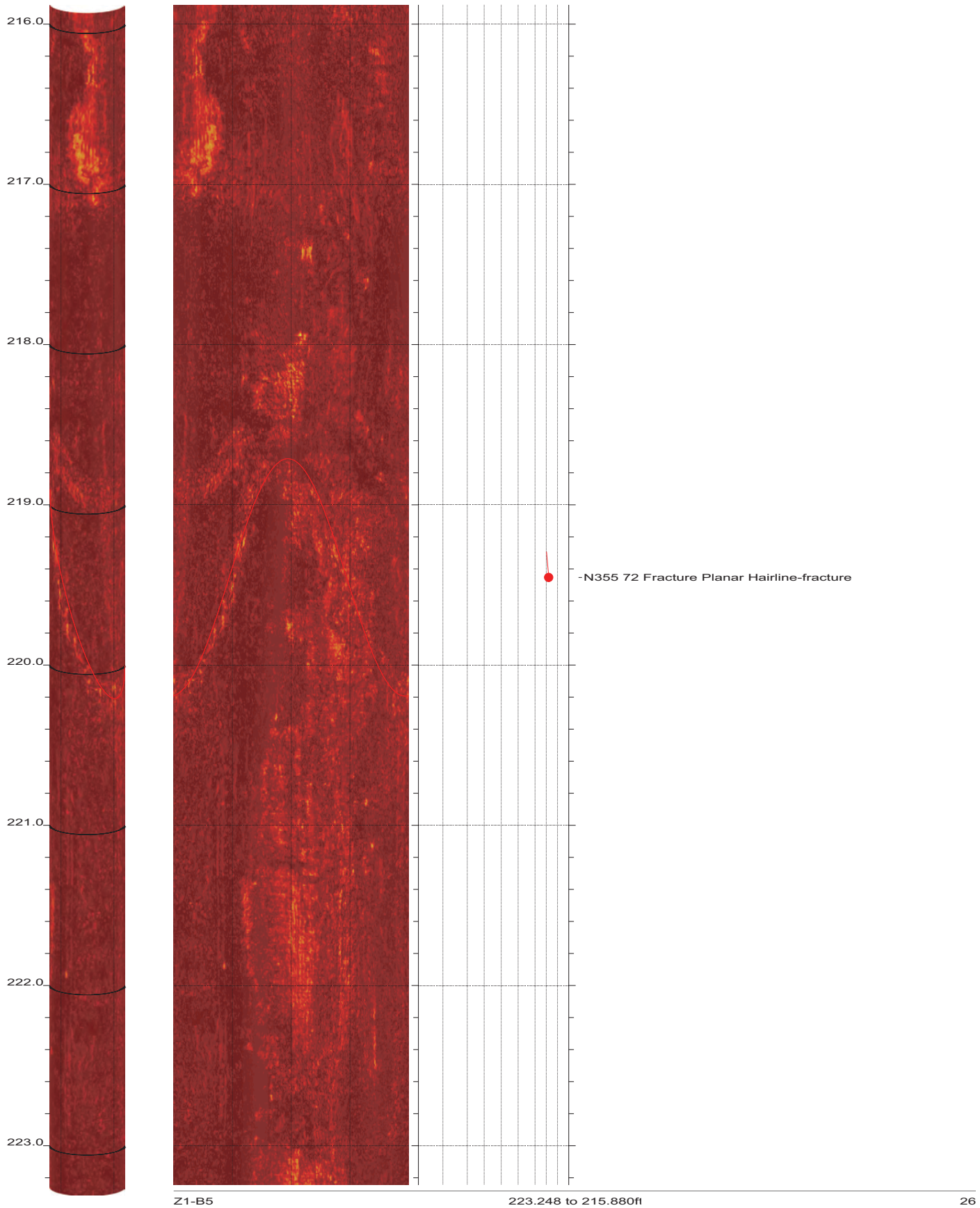
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 23 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 24 of 64

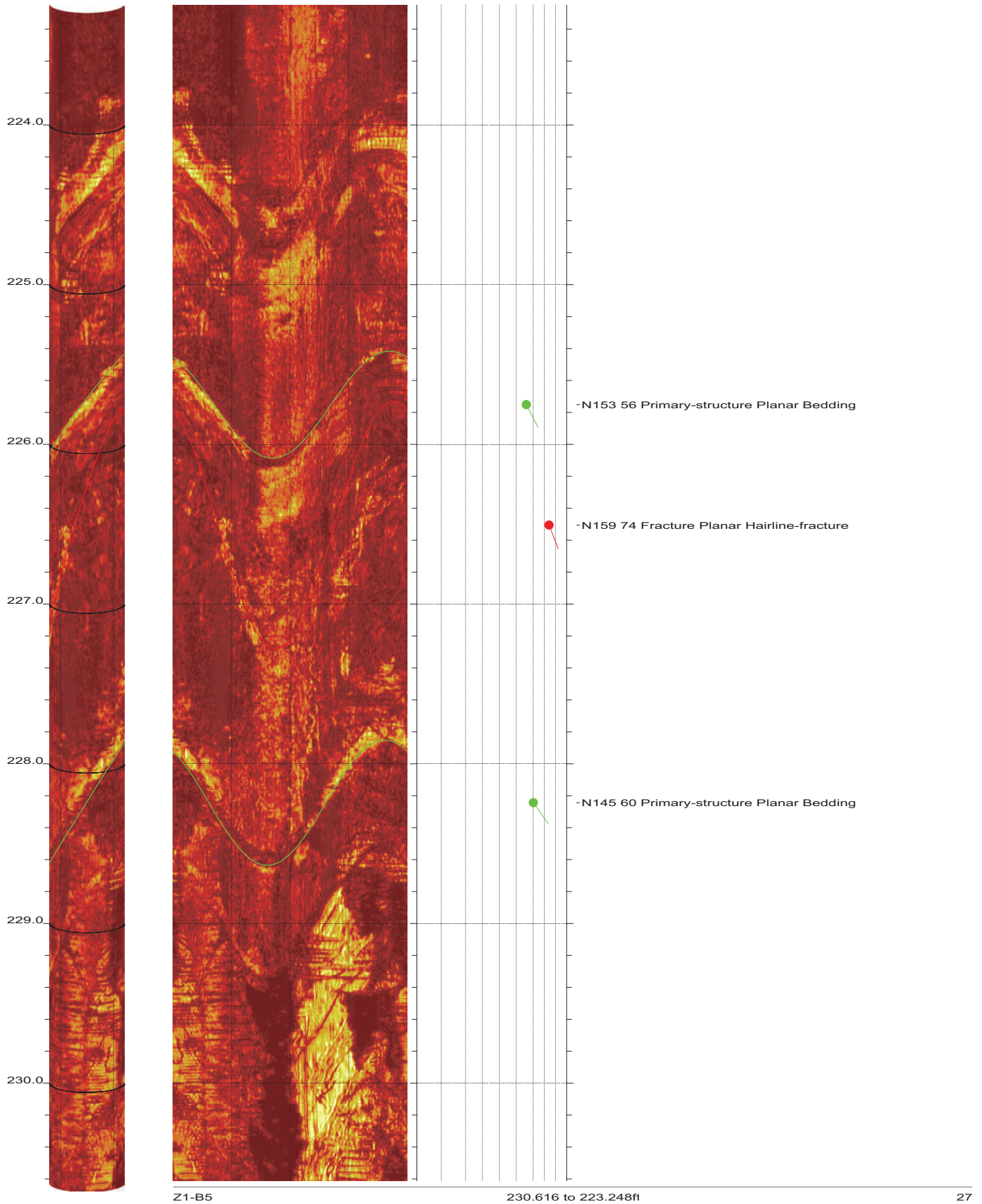


SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 25 of 64

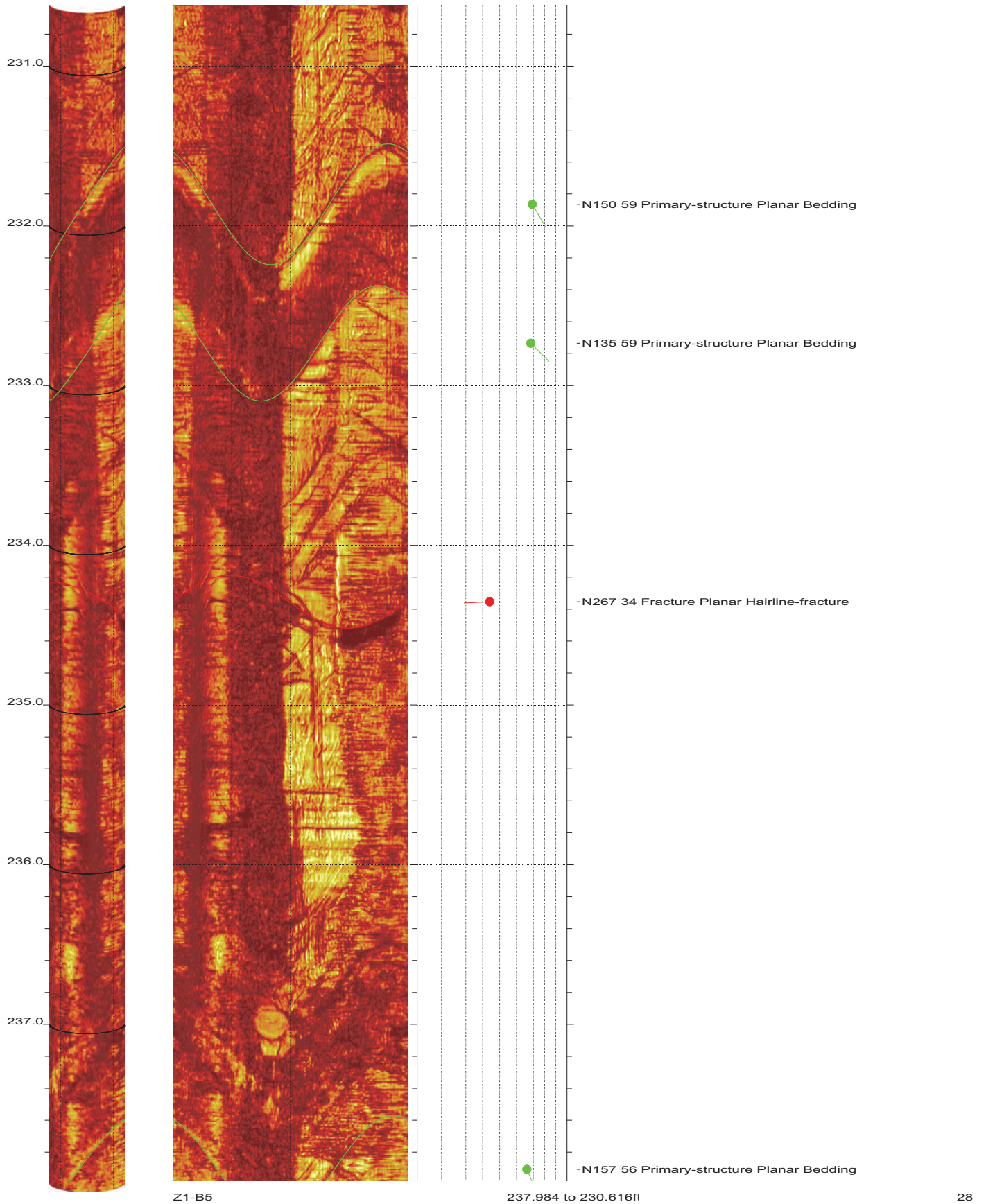


SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 26 of 64

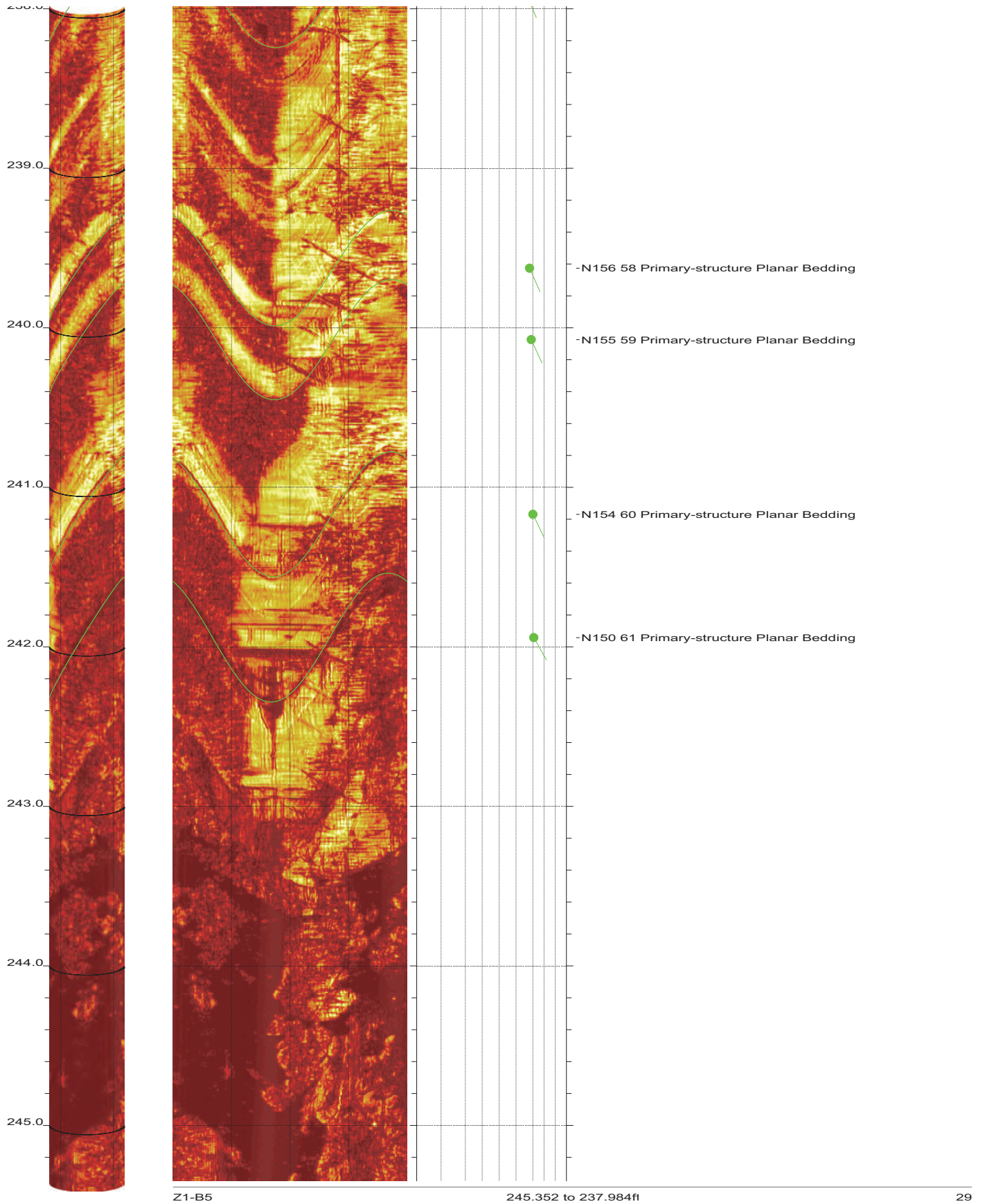




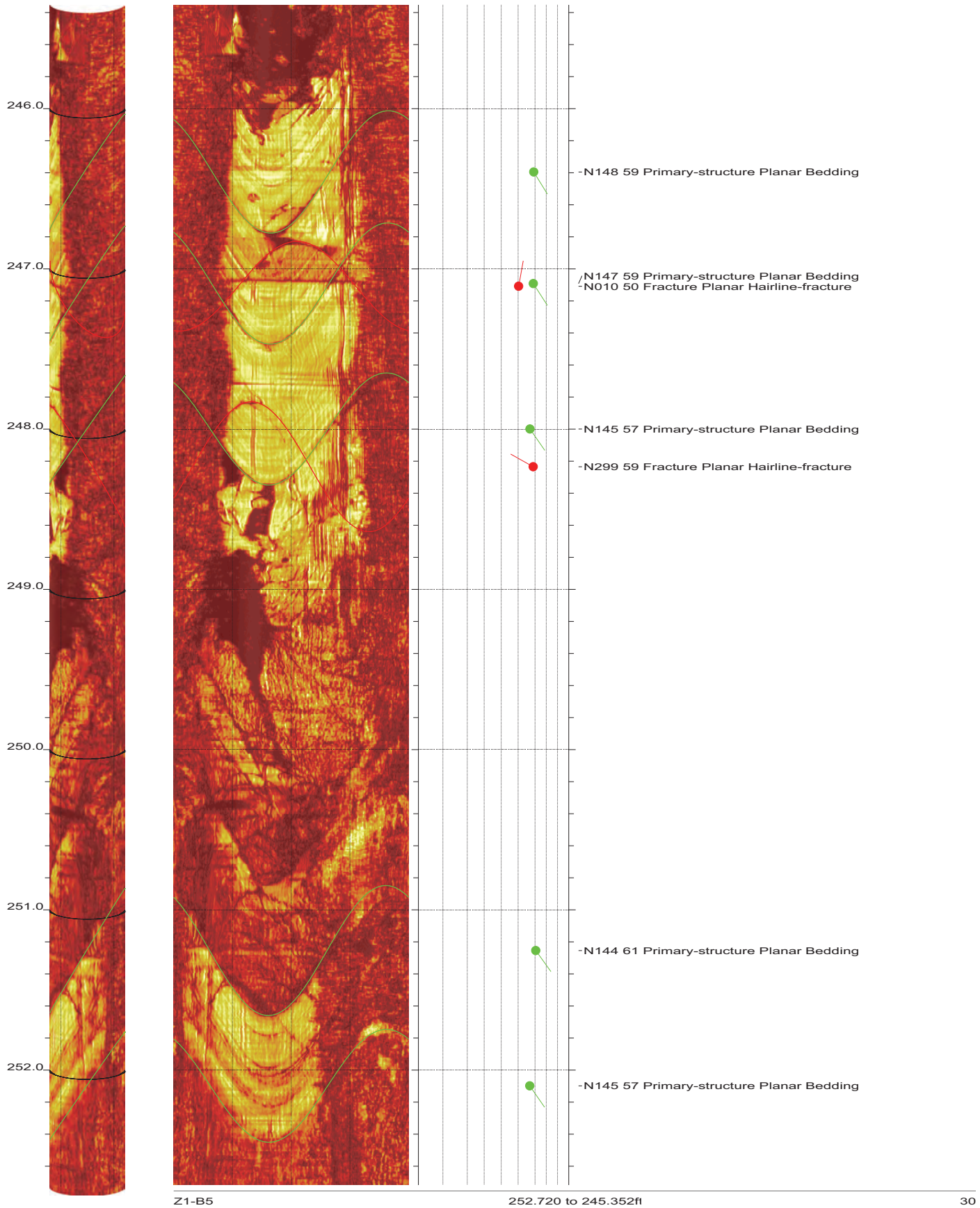
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 27 of 64



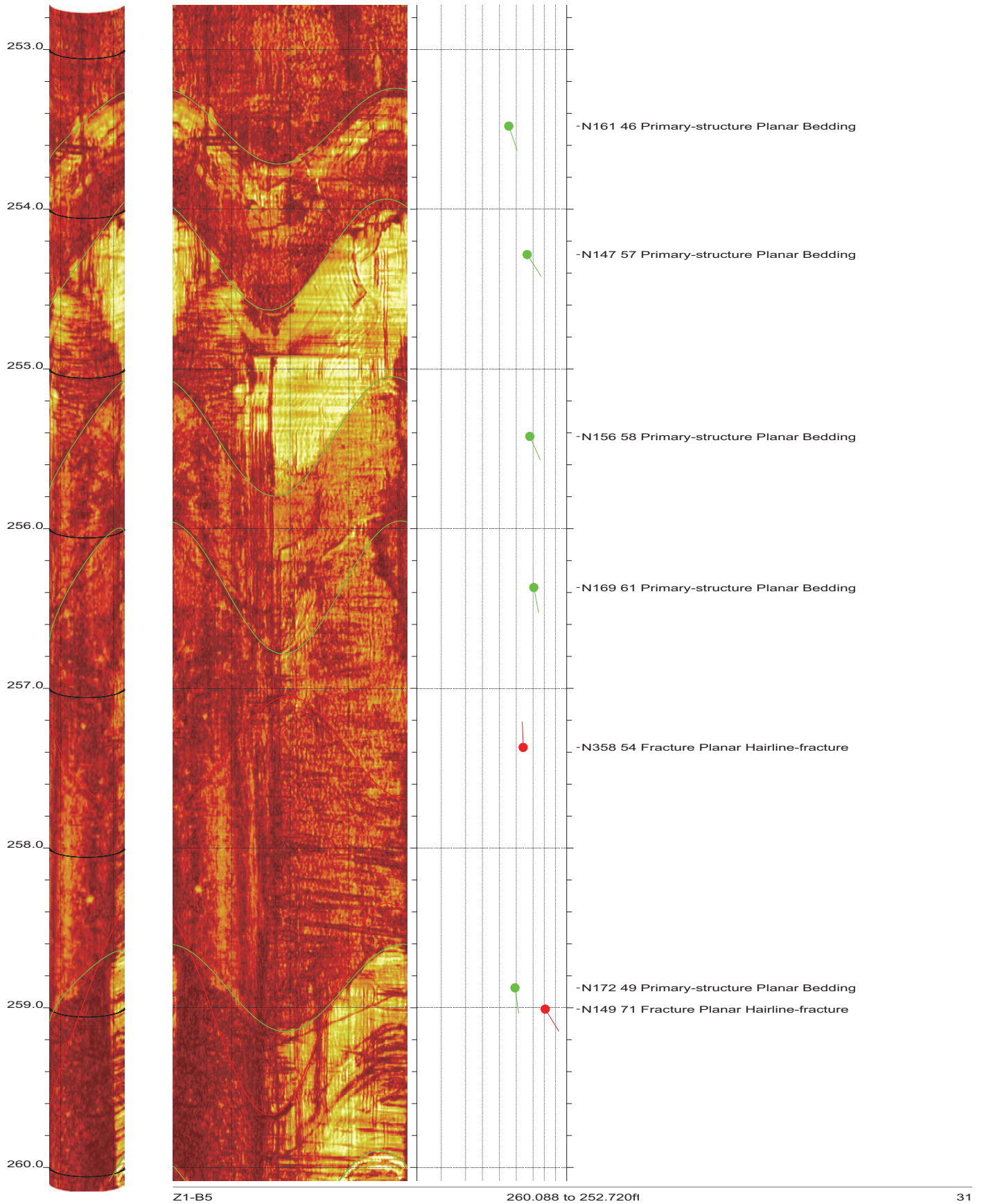
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 28 of 64



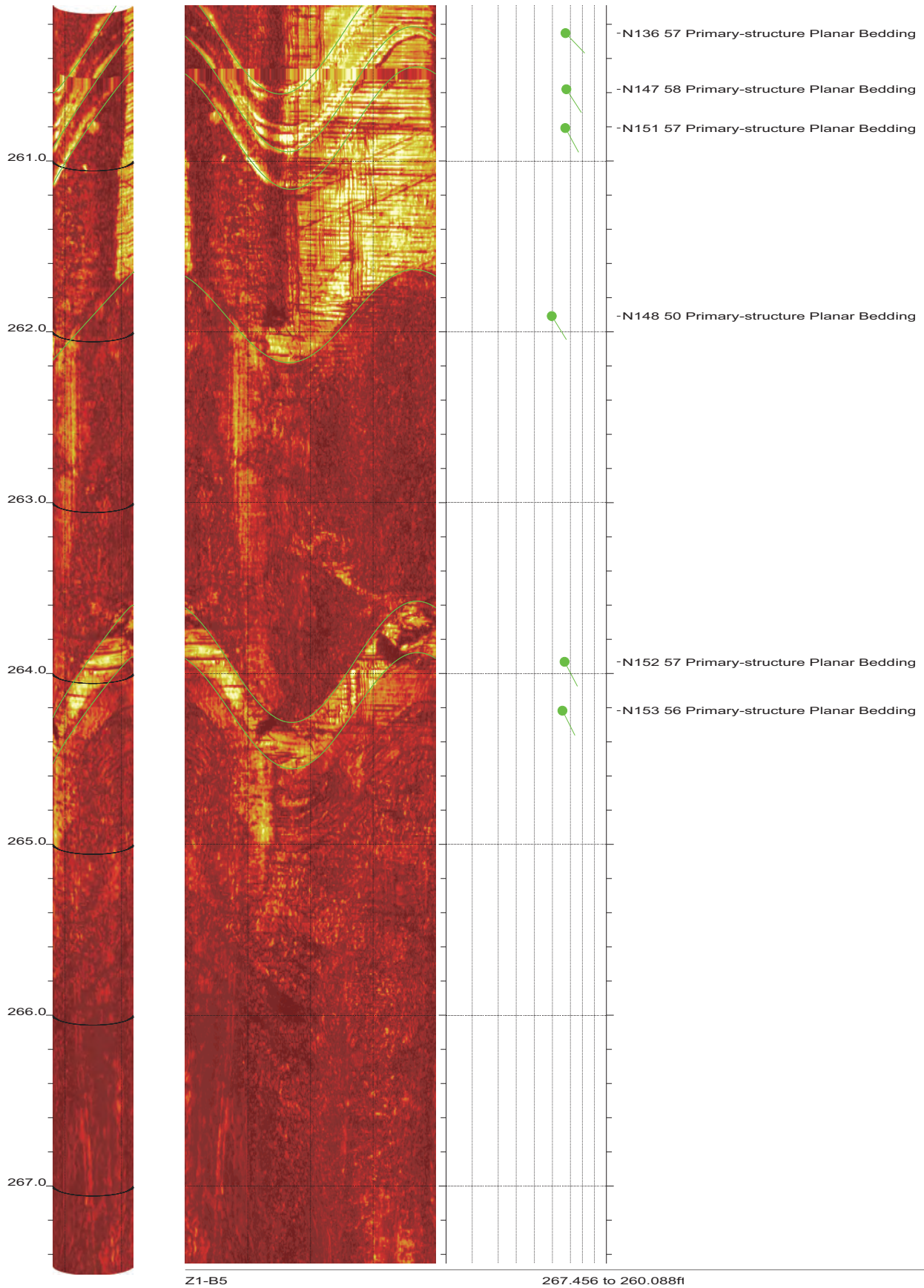
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 29 of 64



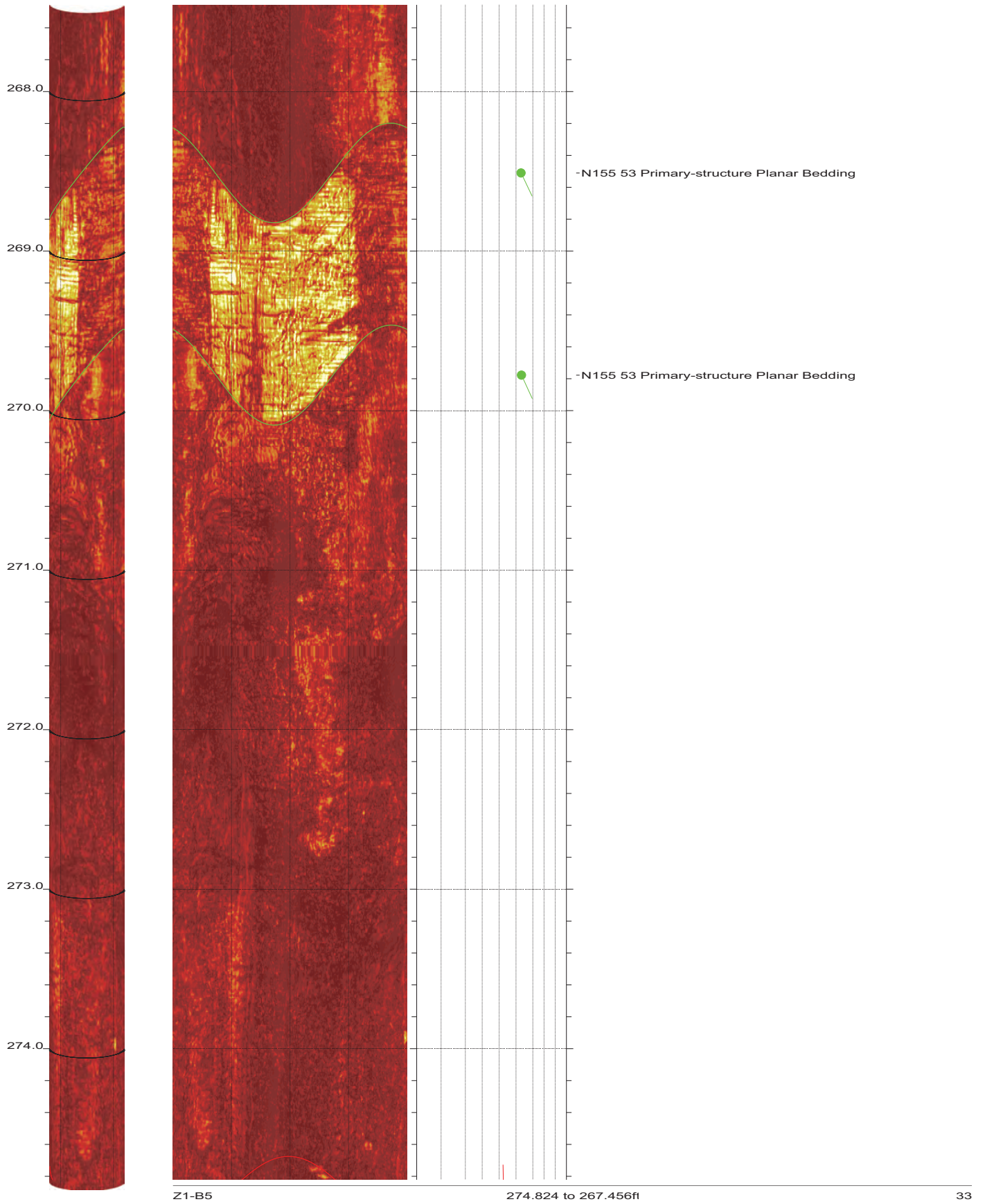
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 30 of 64



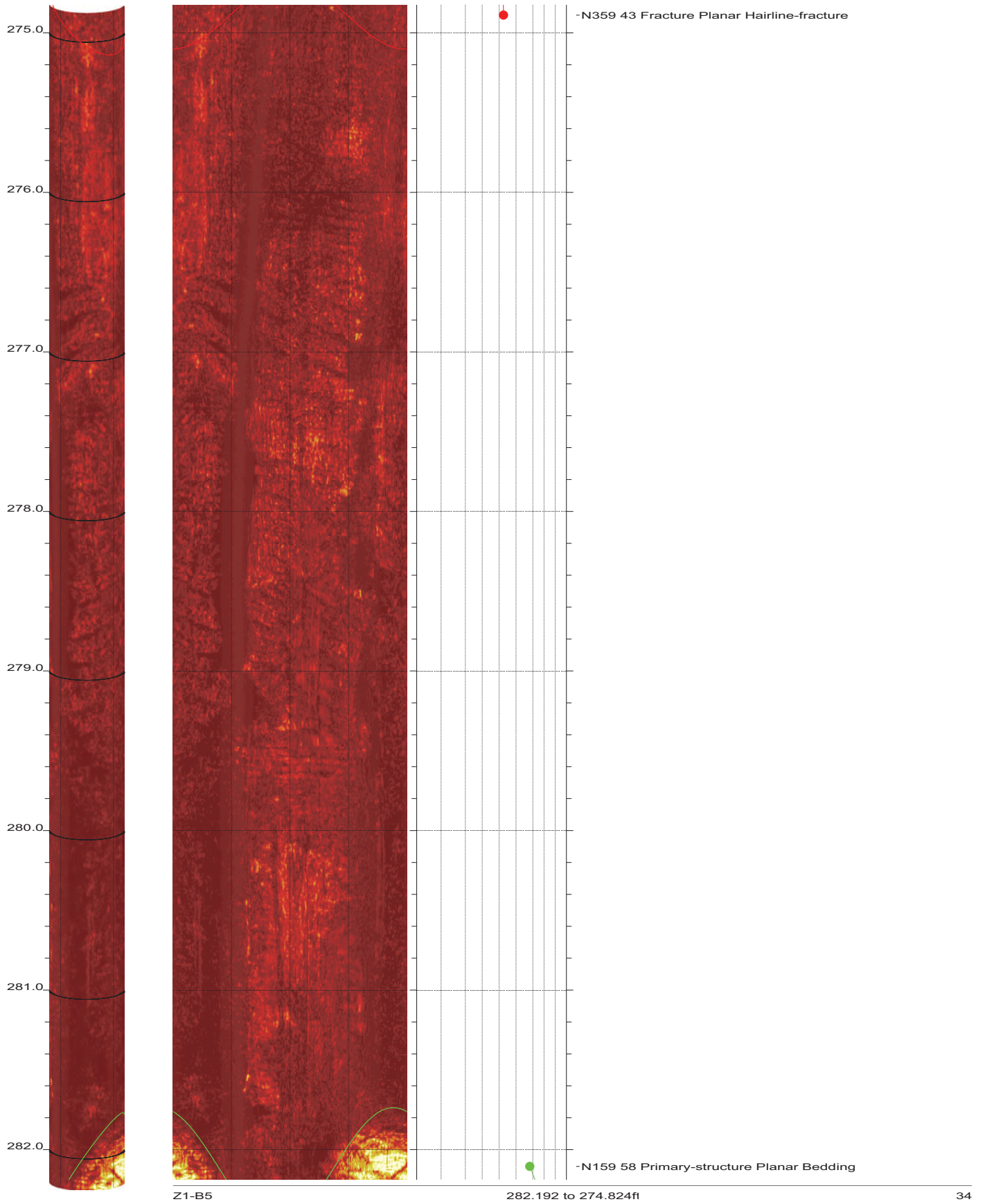
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 31 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 32 of 64

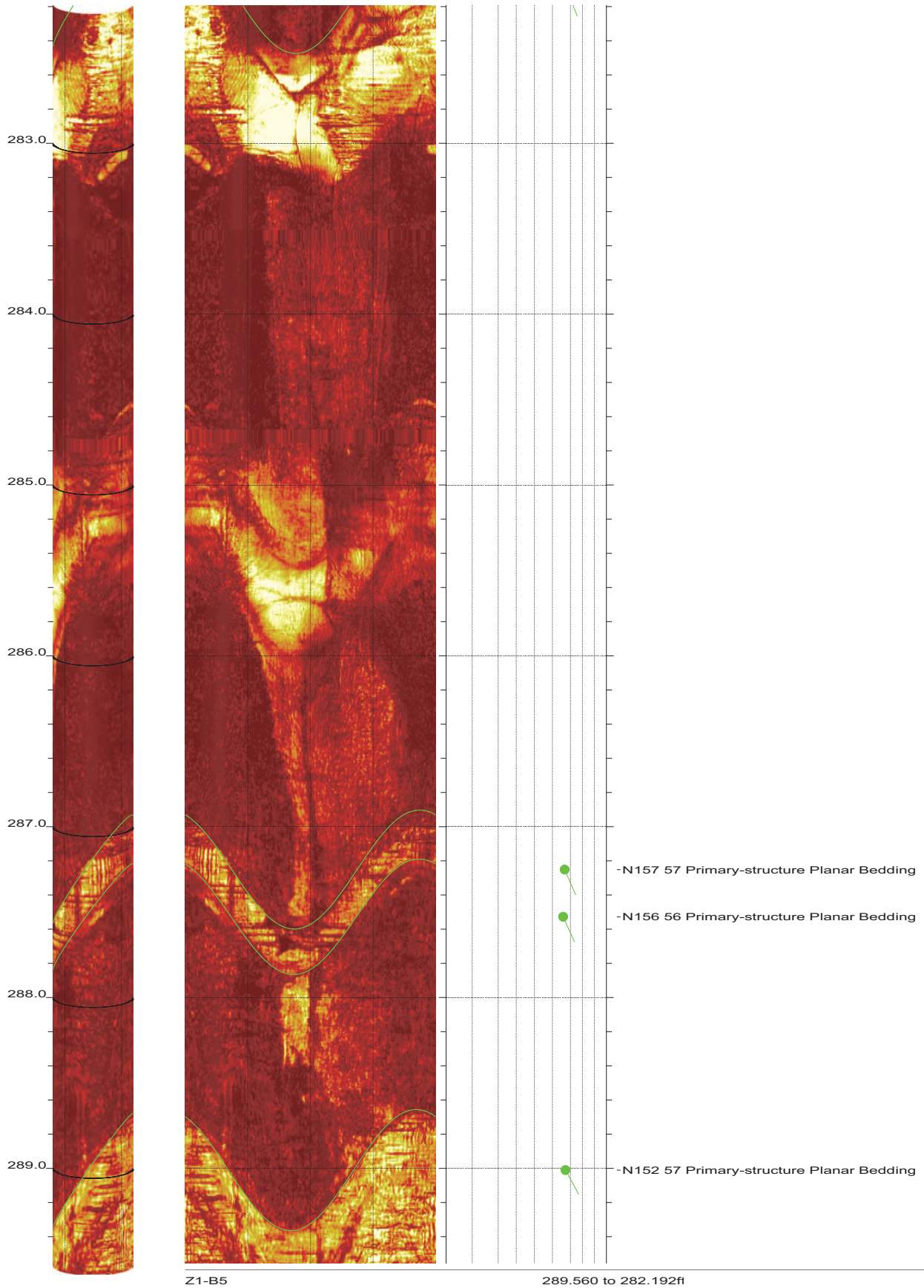


SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 33 of 64

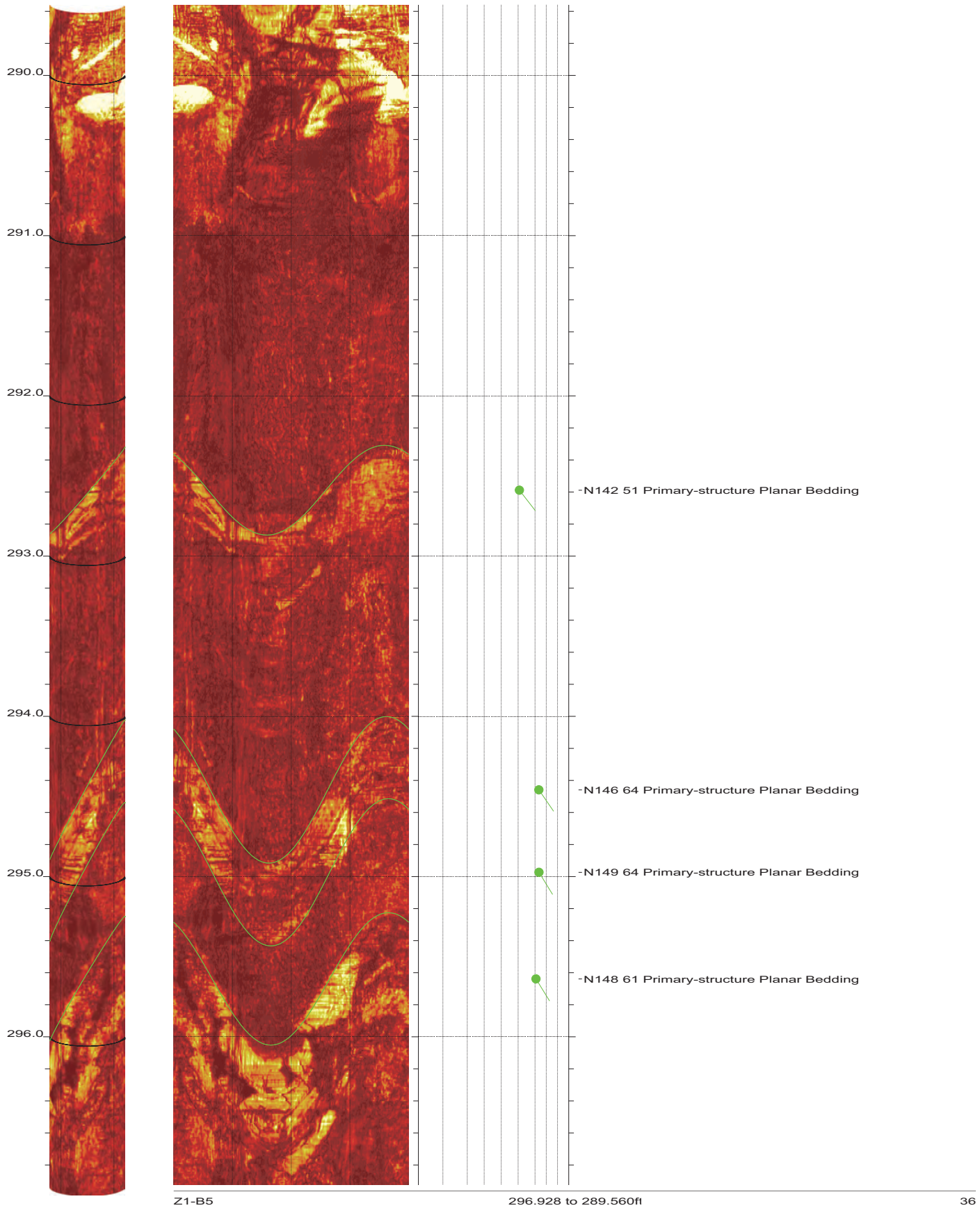


SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 34 of 64

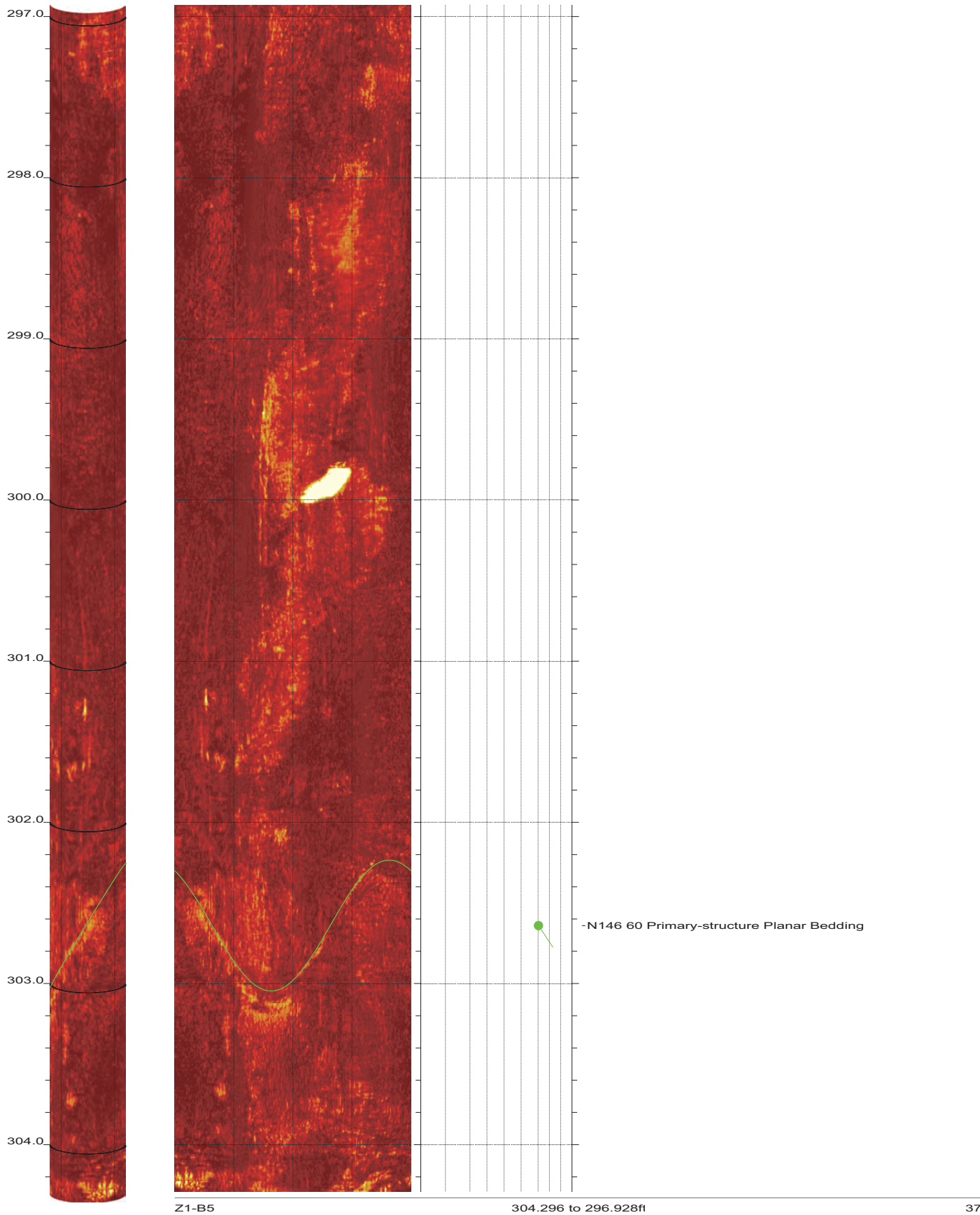




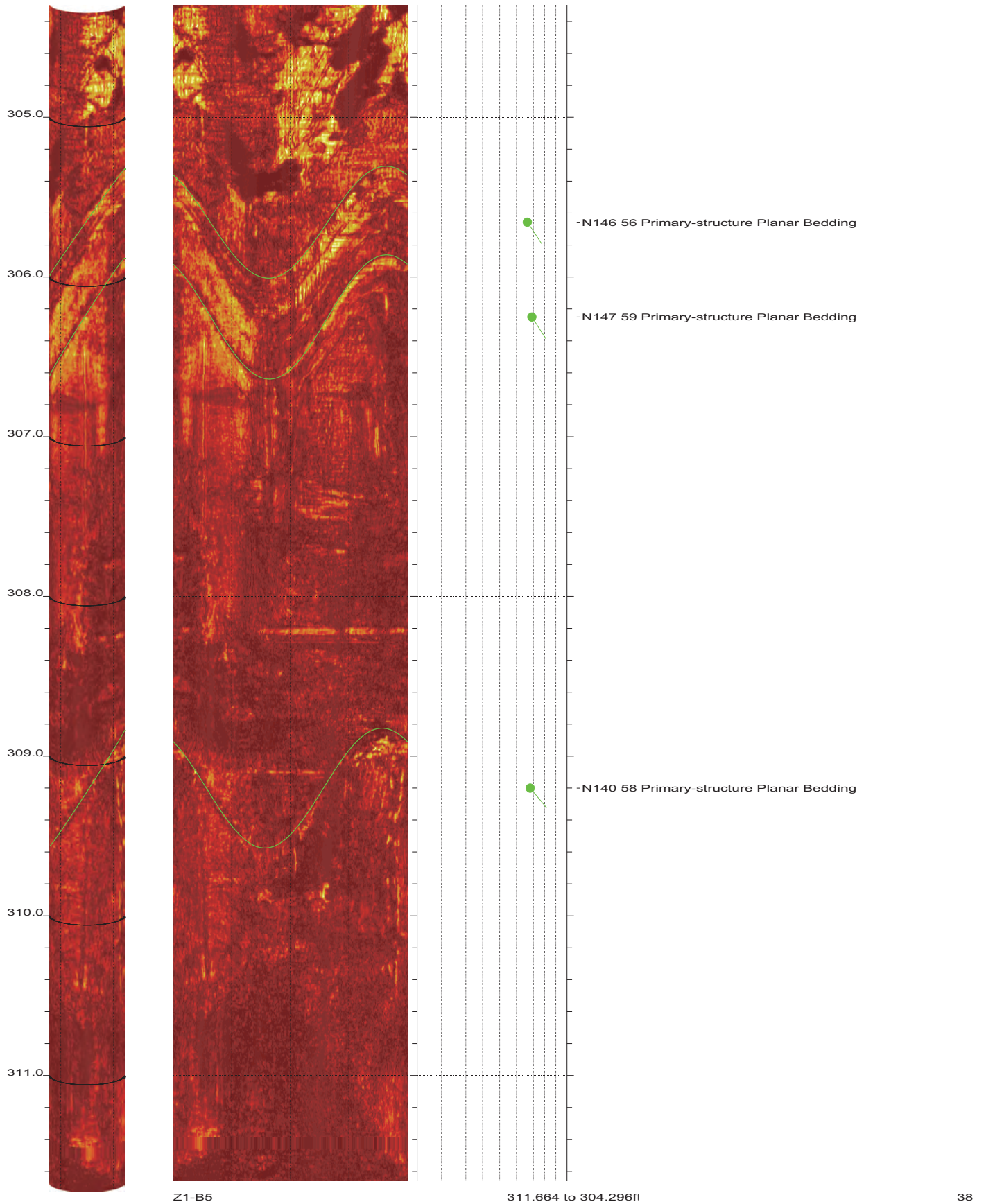
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 35 of 64



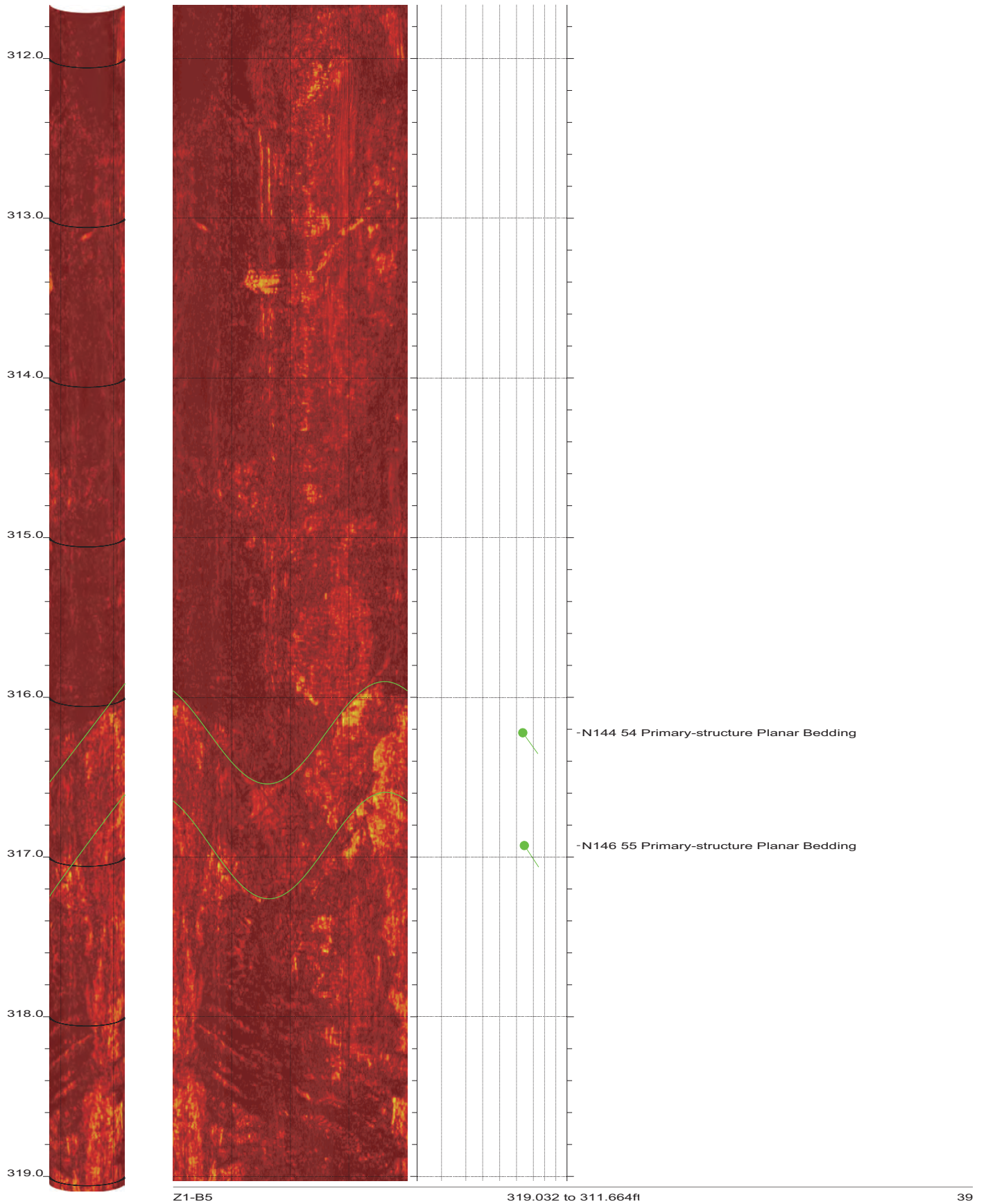
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 36 of 64



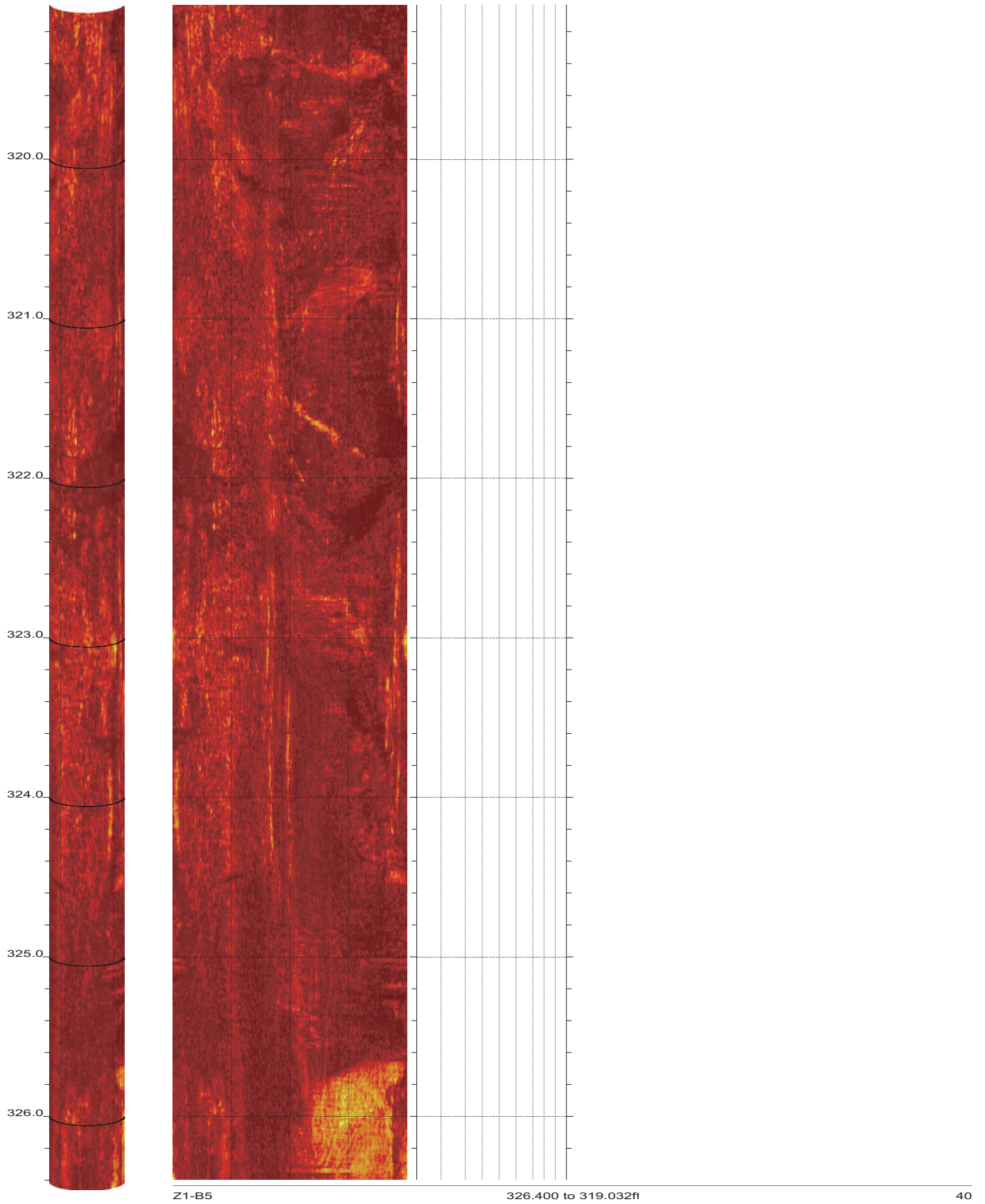
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 37 of 64



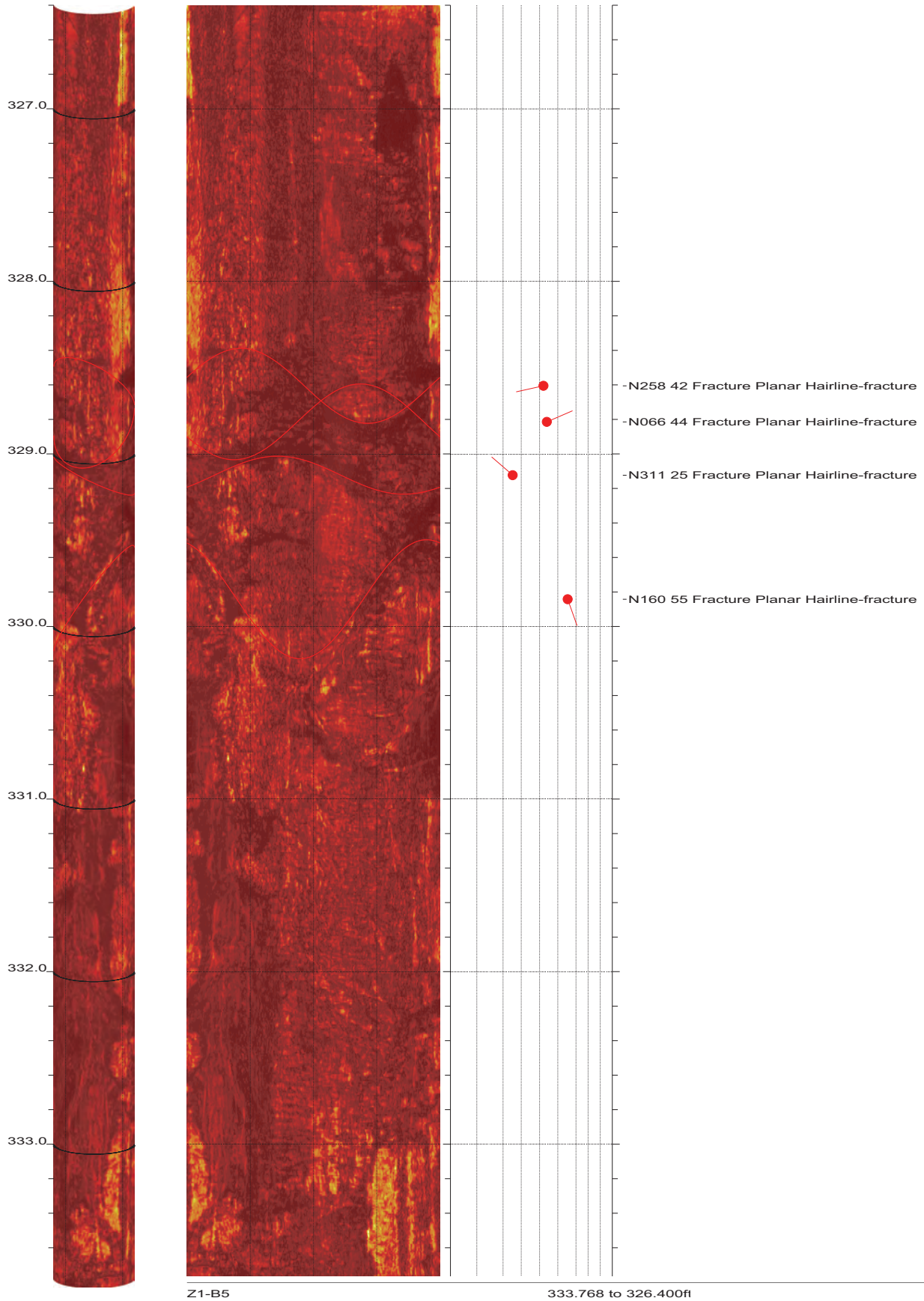
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 38 of 64



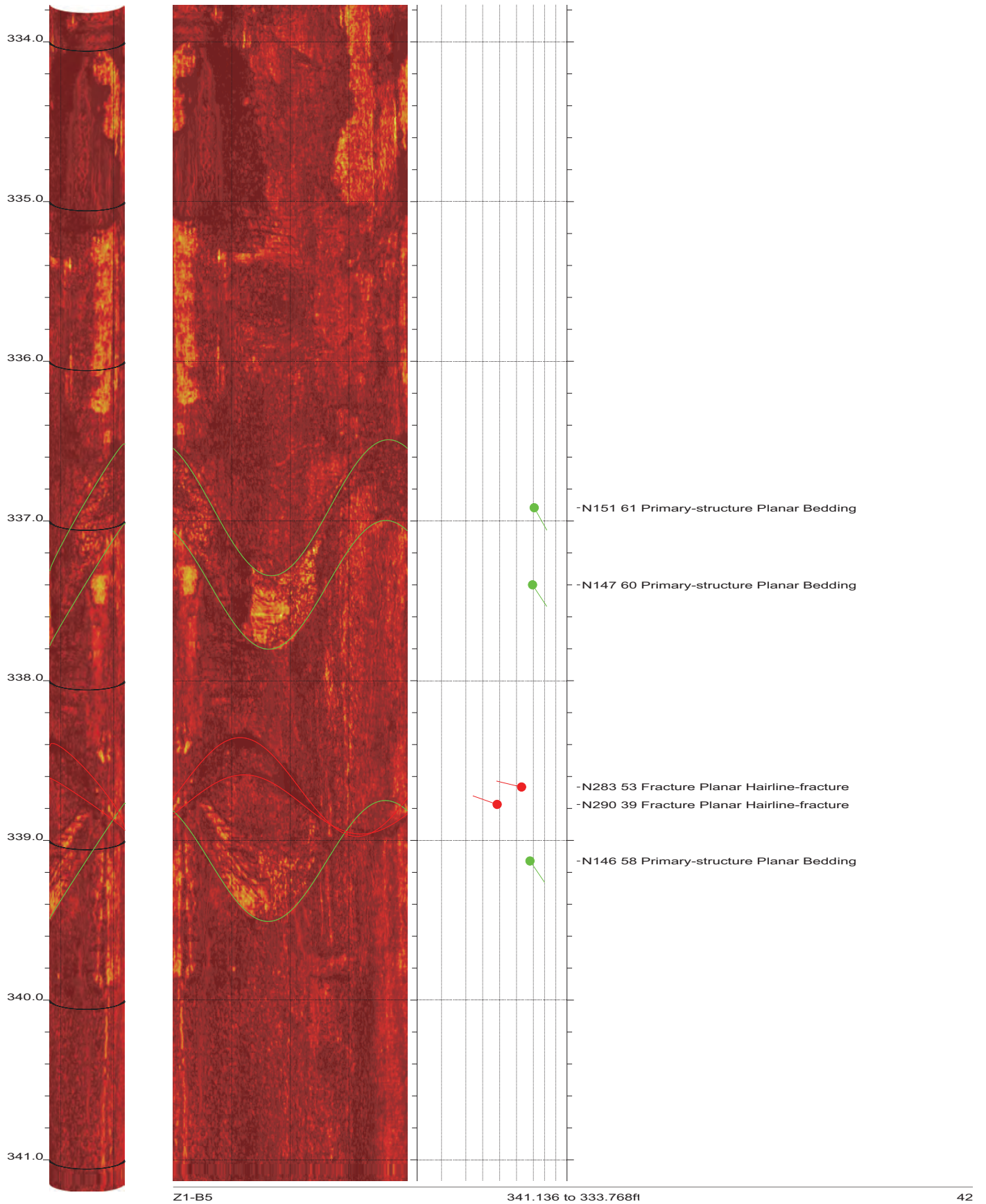
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 39 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 40 of 64

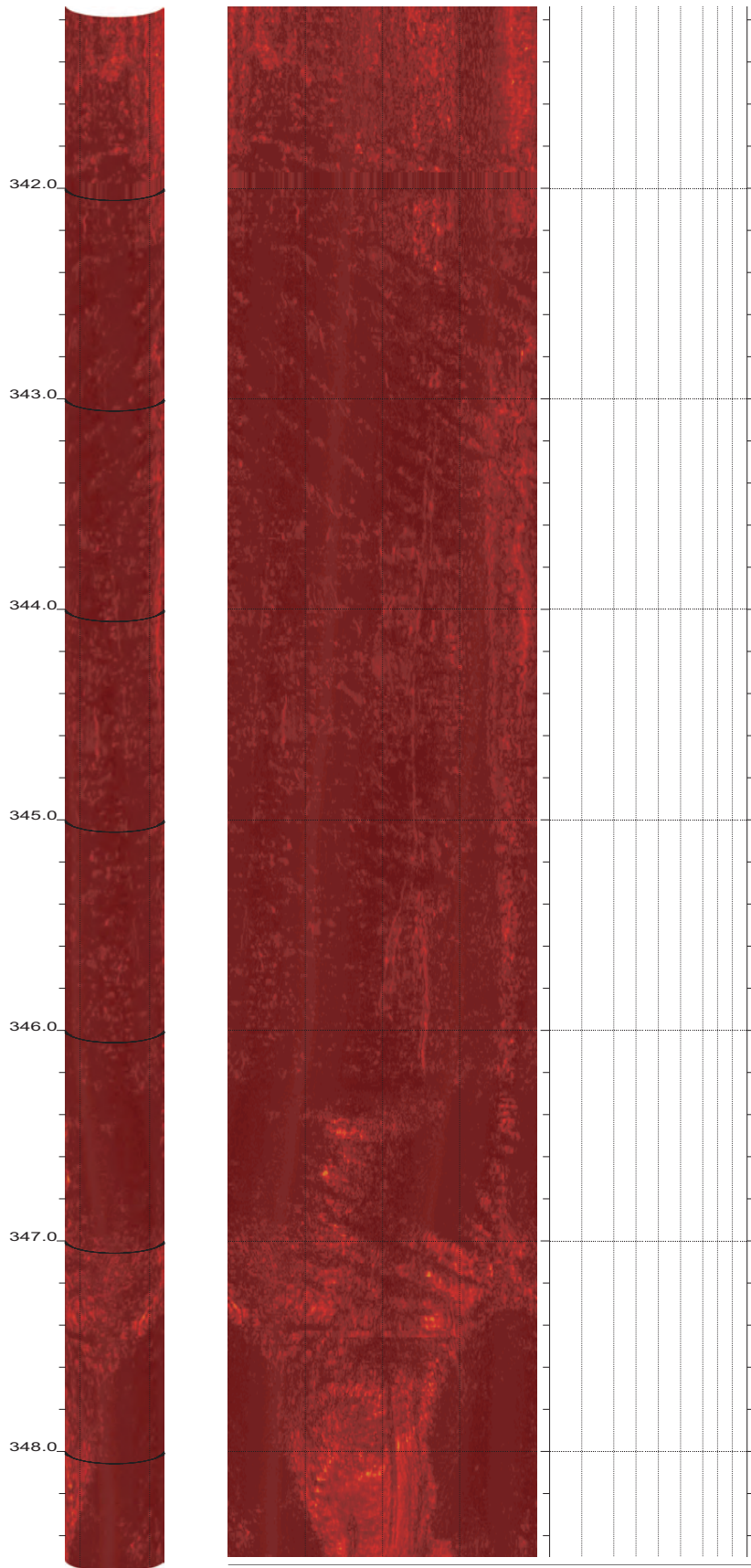


SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 41 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 42 of 64



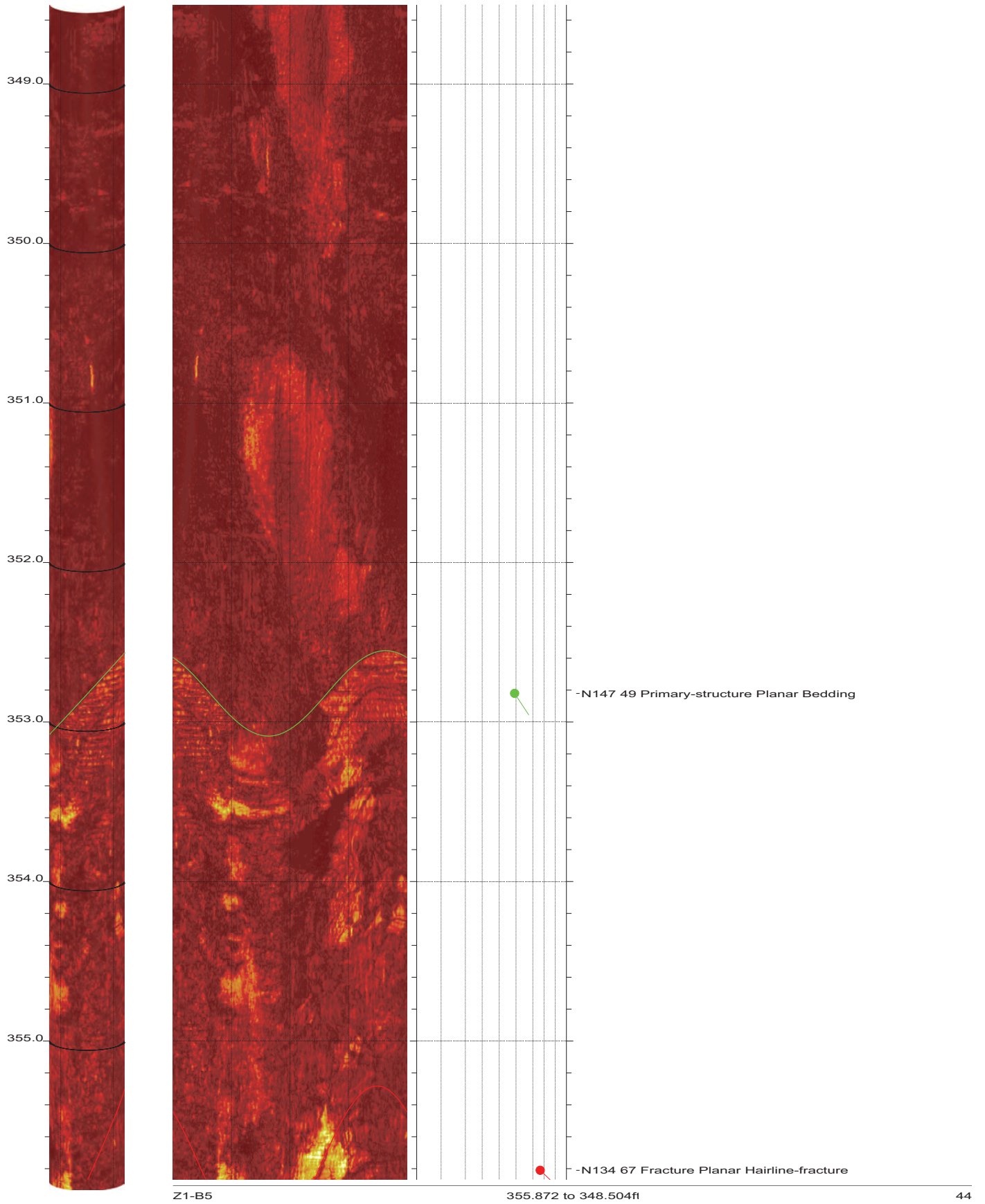


Z1-B5

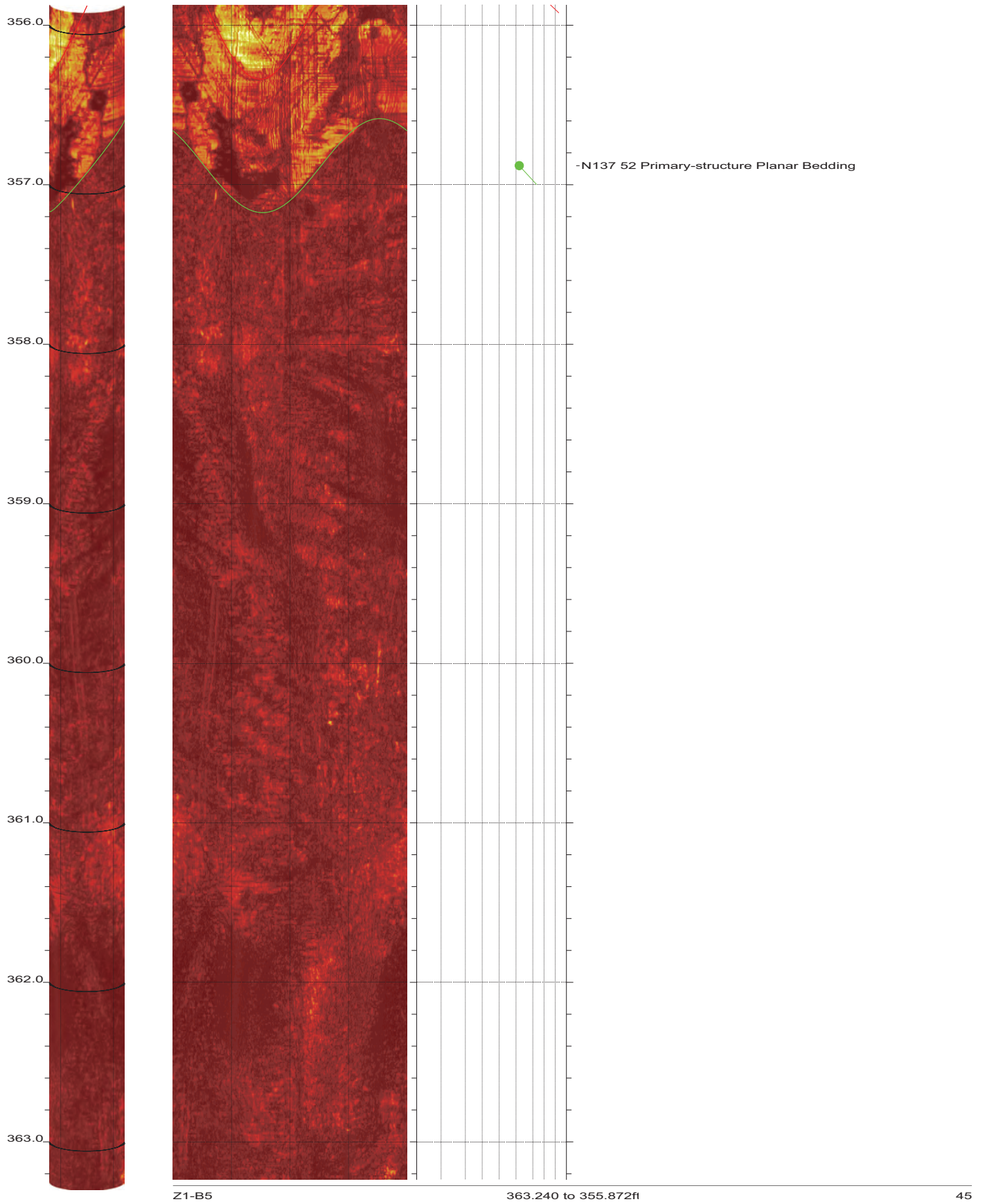
348.504 to 341.136ft

43

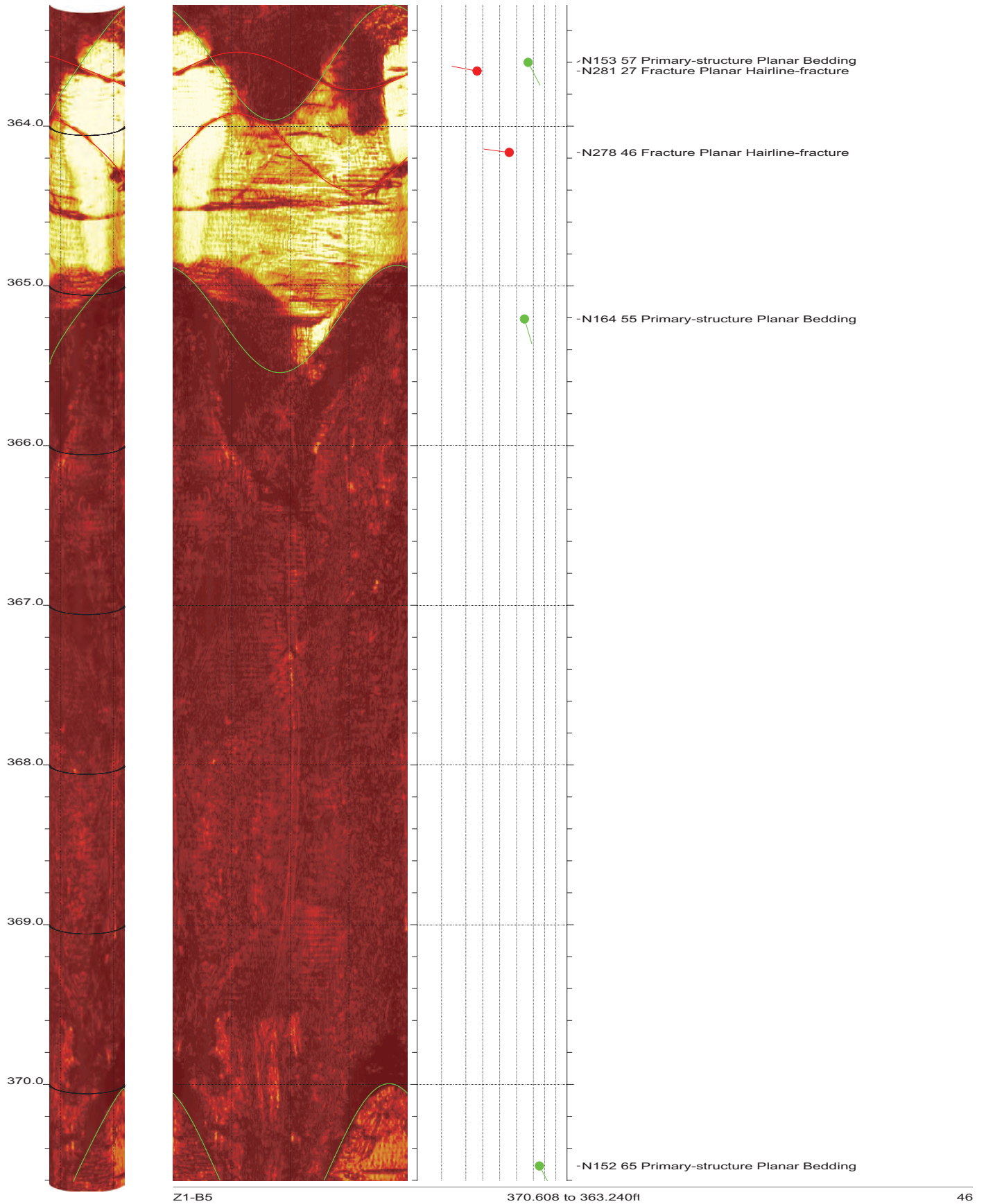
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 43 of 64



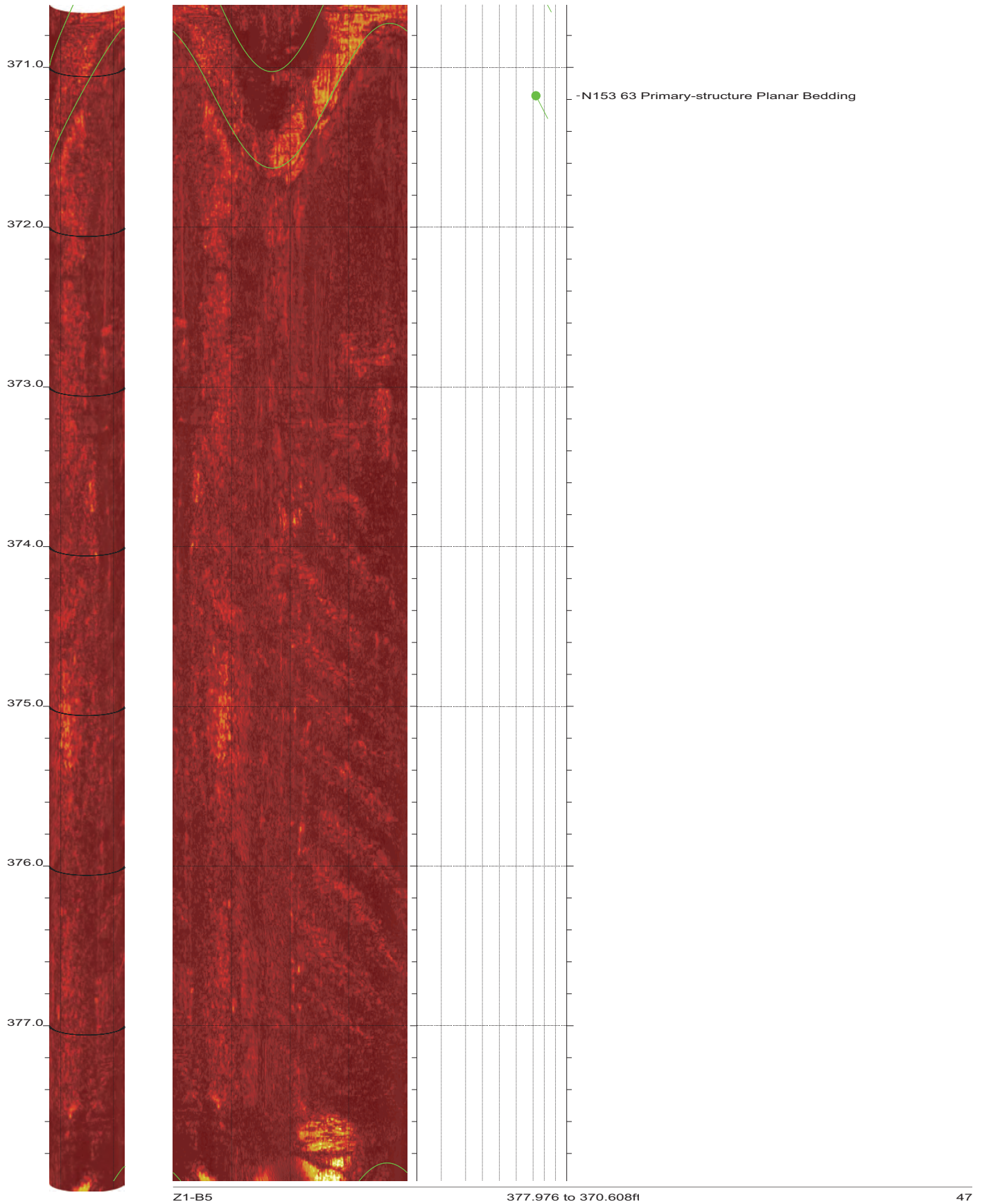
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 44 of 64



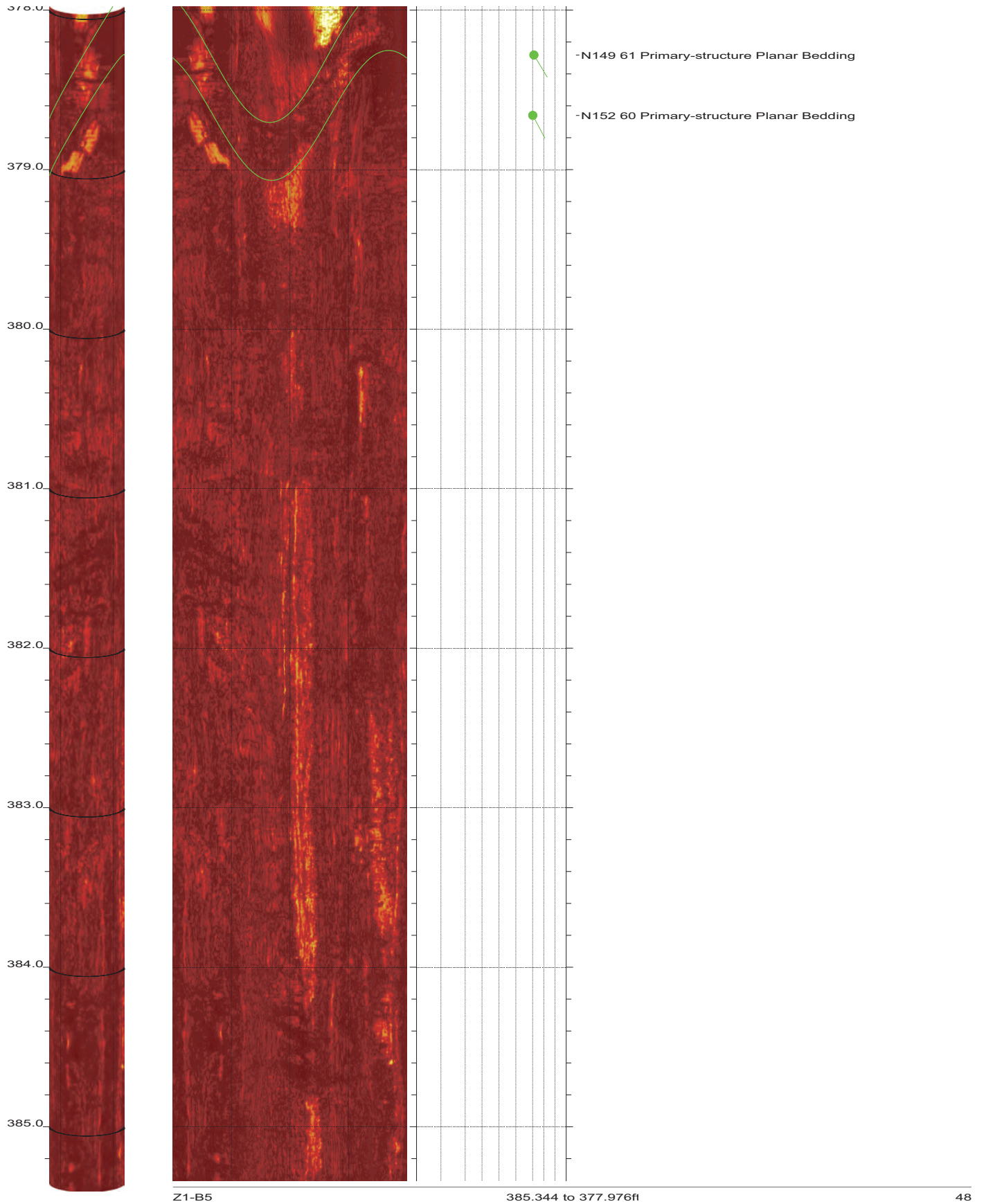
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 45 of 64



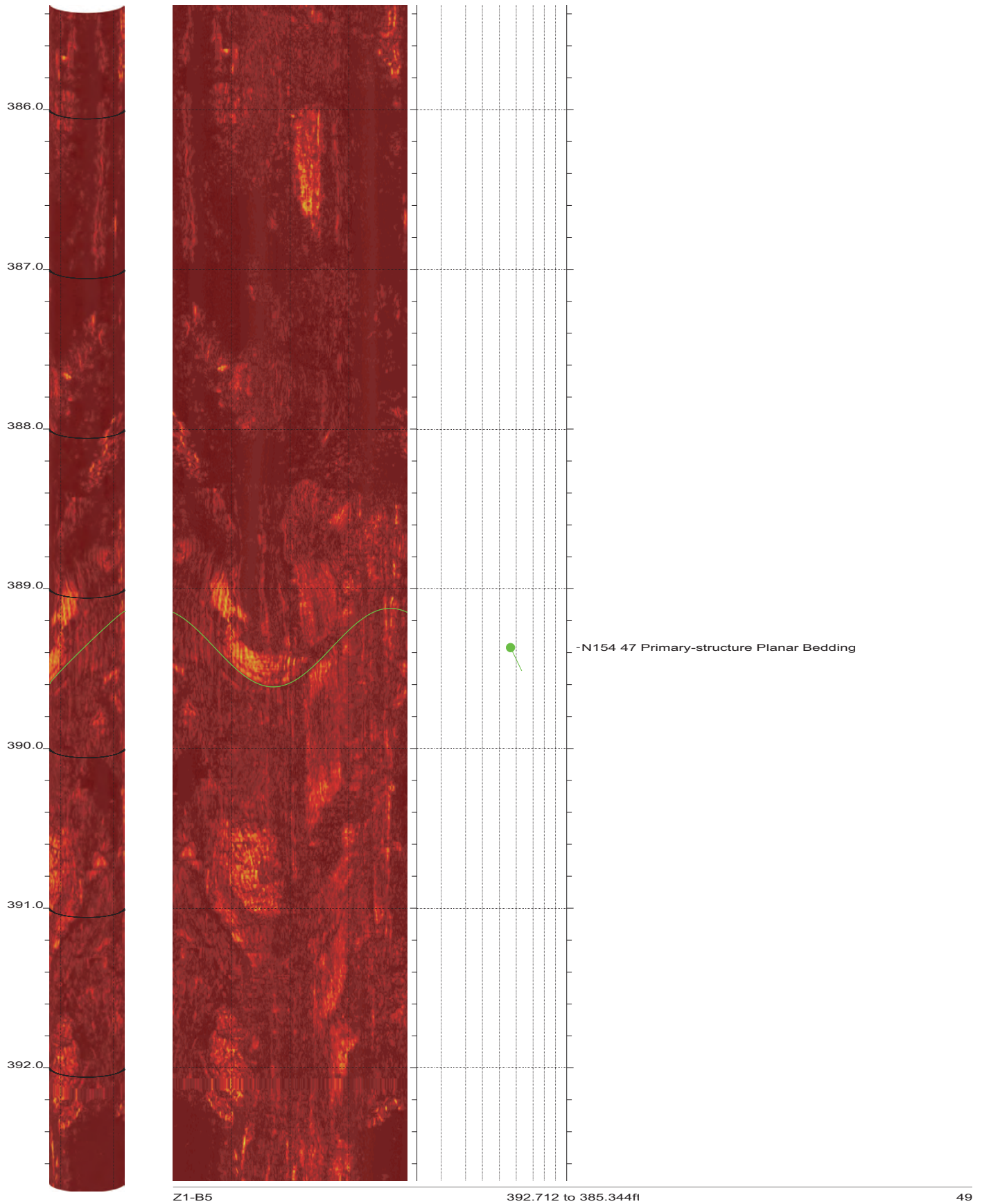
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 46 of 64



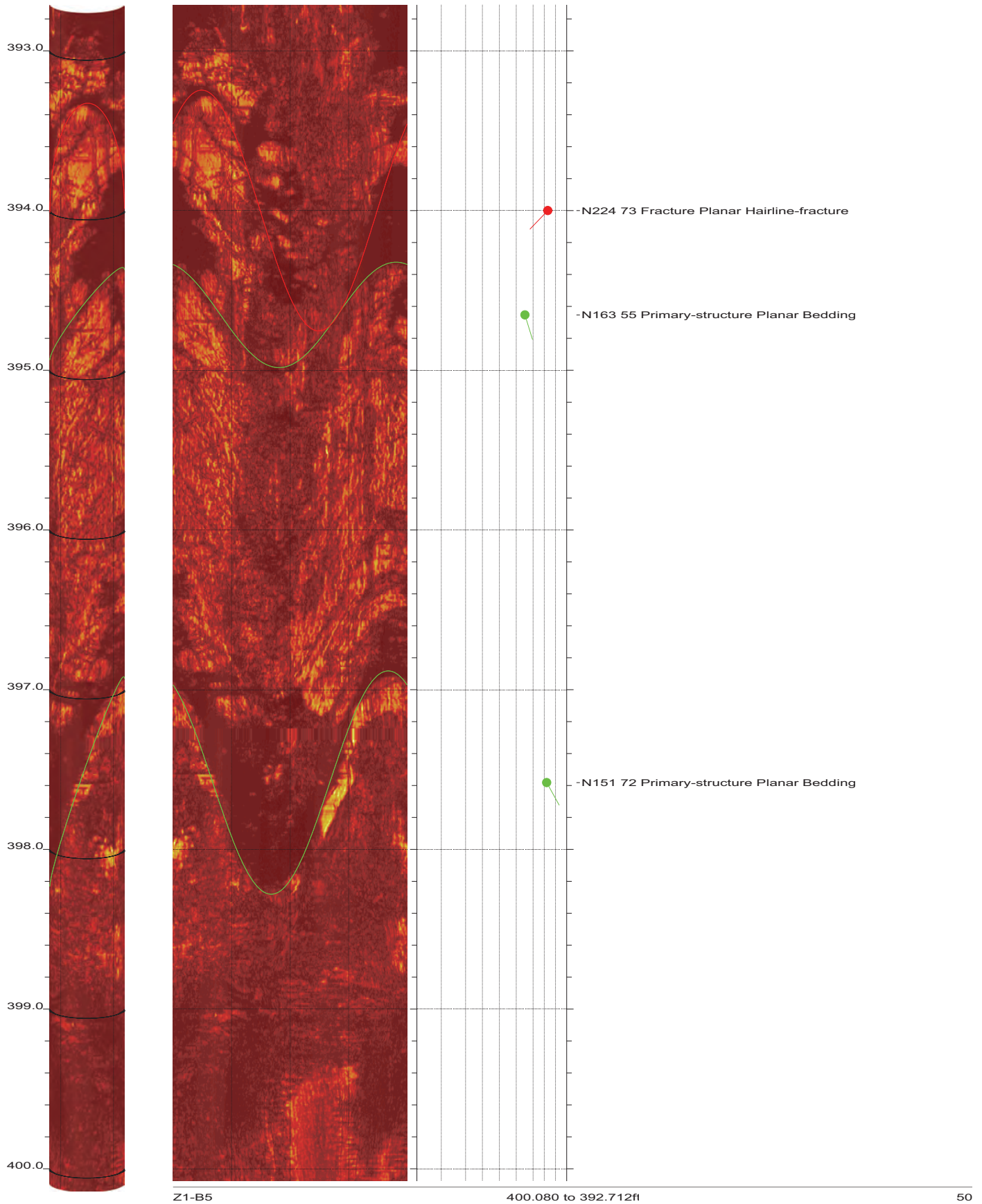
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 47 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 48 of 64

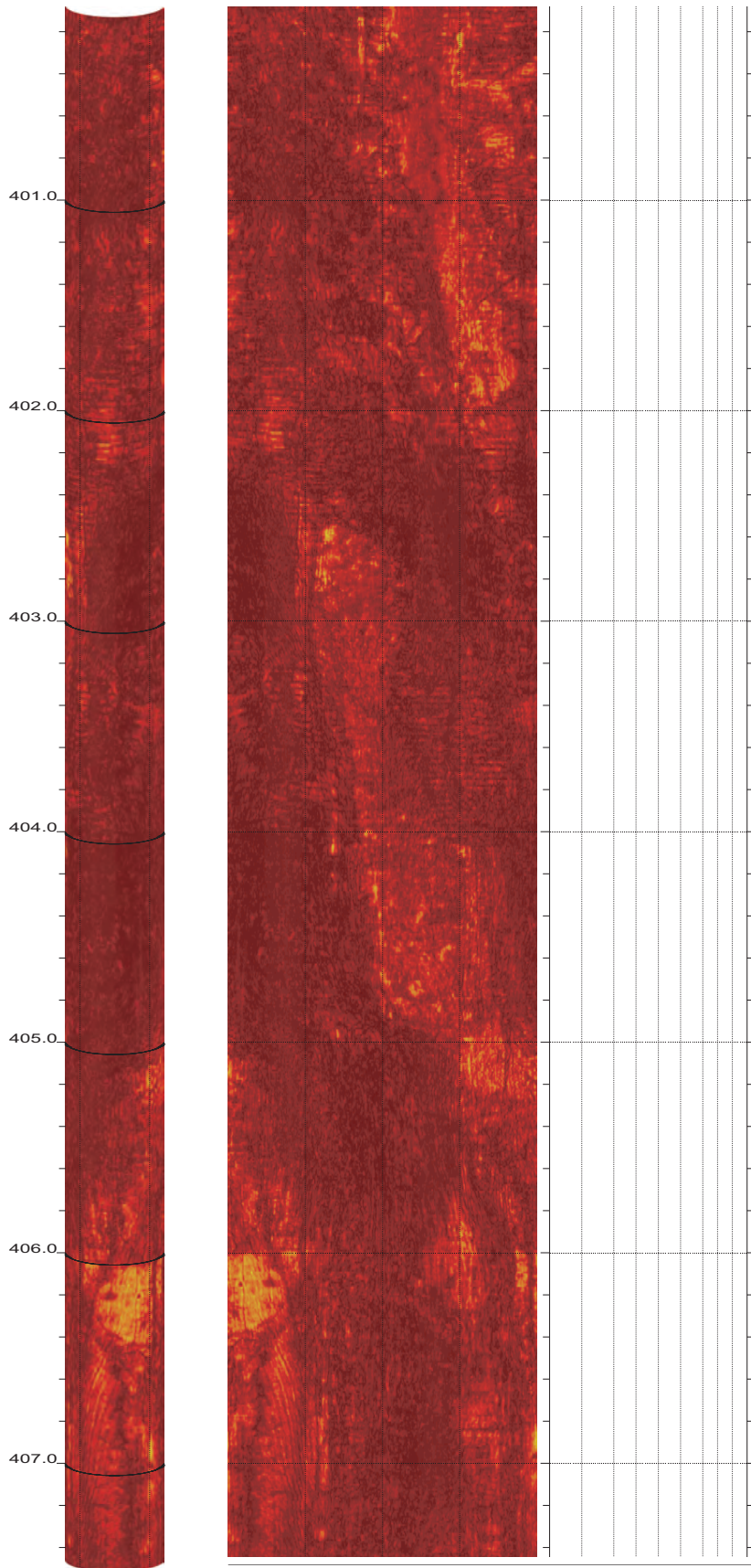


SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 49 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 50 of 64



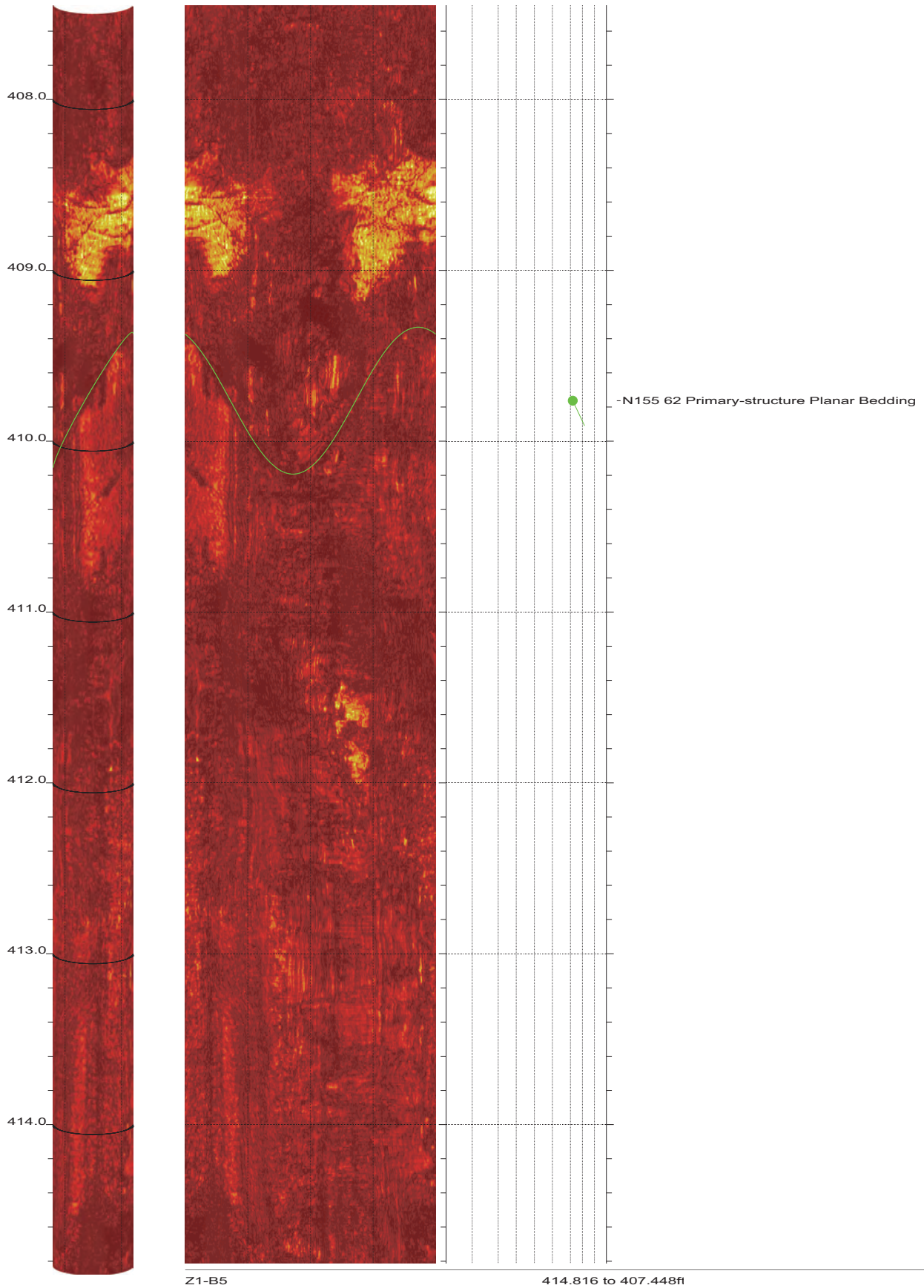


Z1-B5

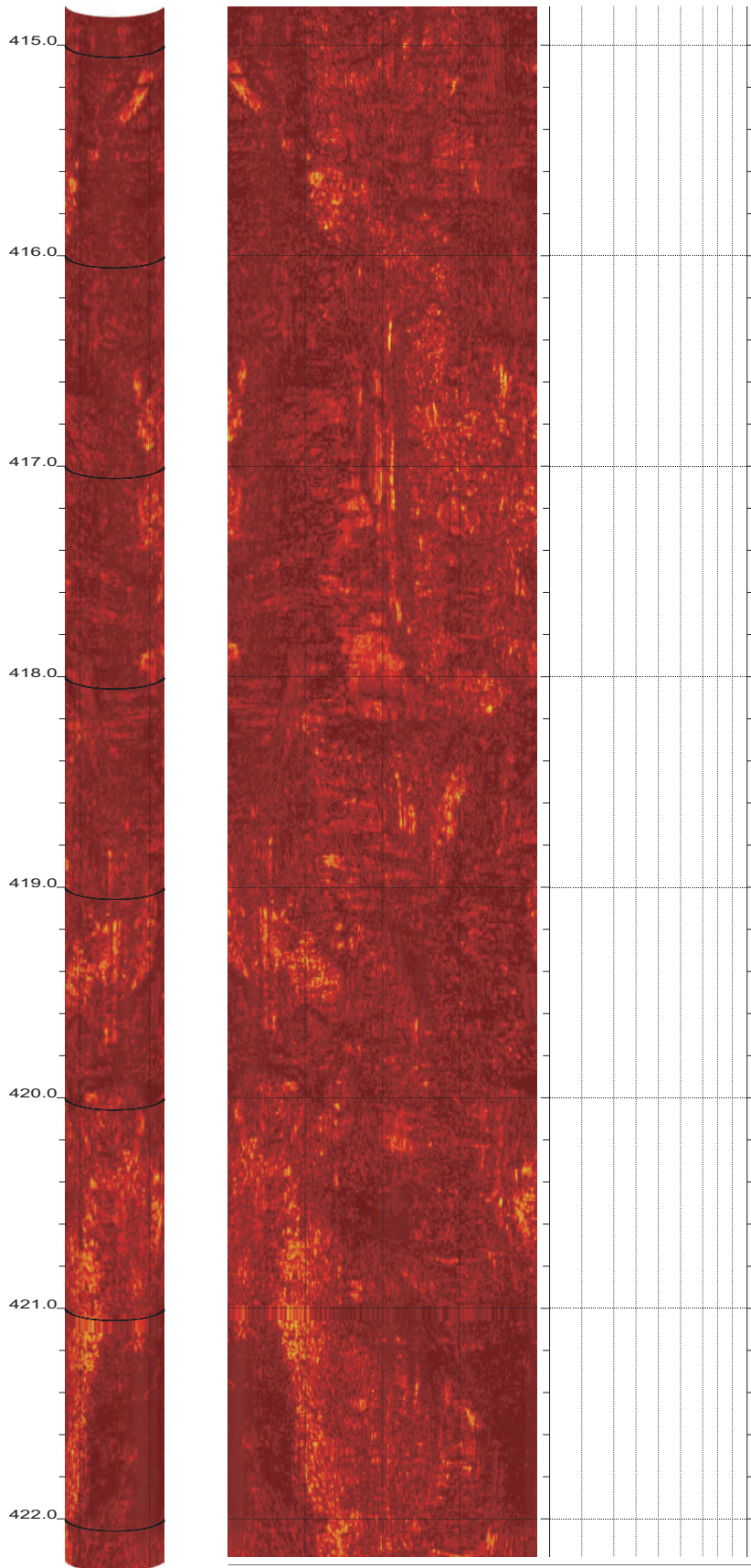
407.448 to 400.080ft

51

SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 51 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 52 of 64

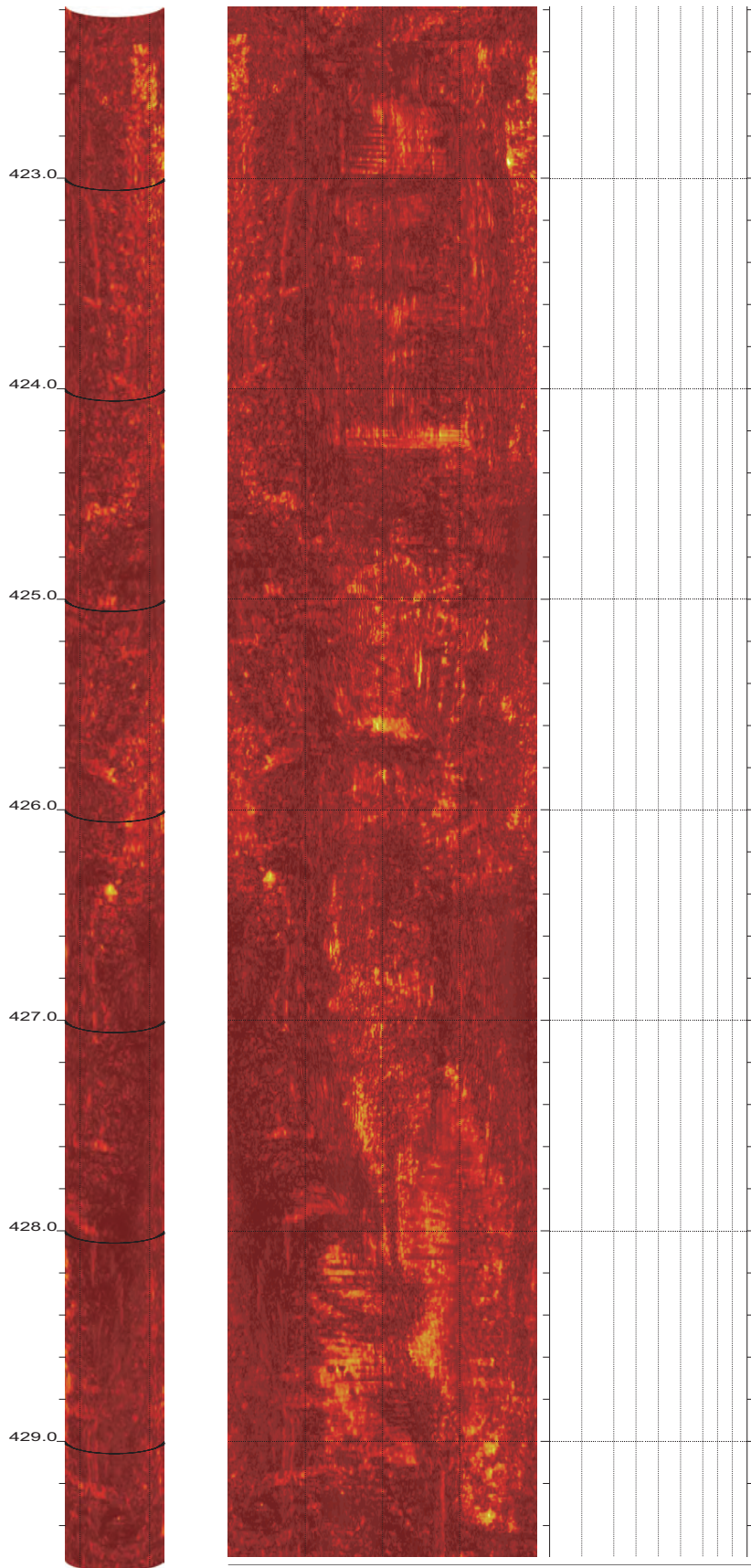


Z1-B5

422.184 to 414.816ft

53

SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 53 of 64

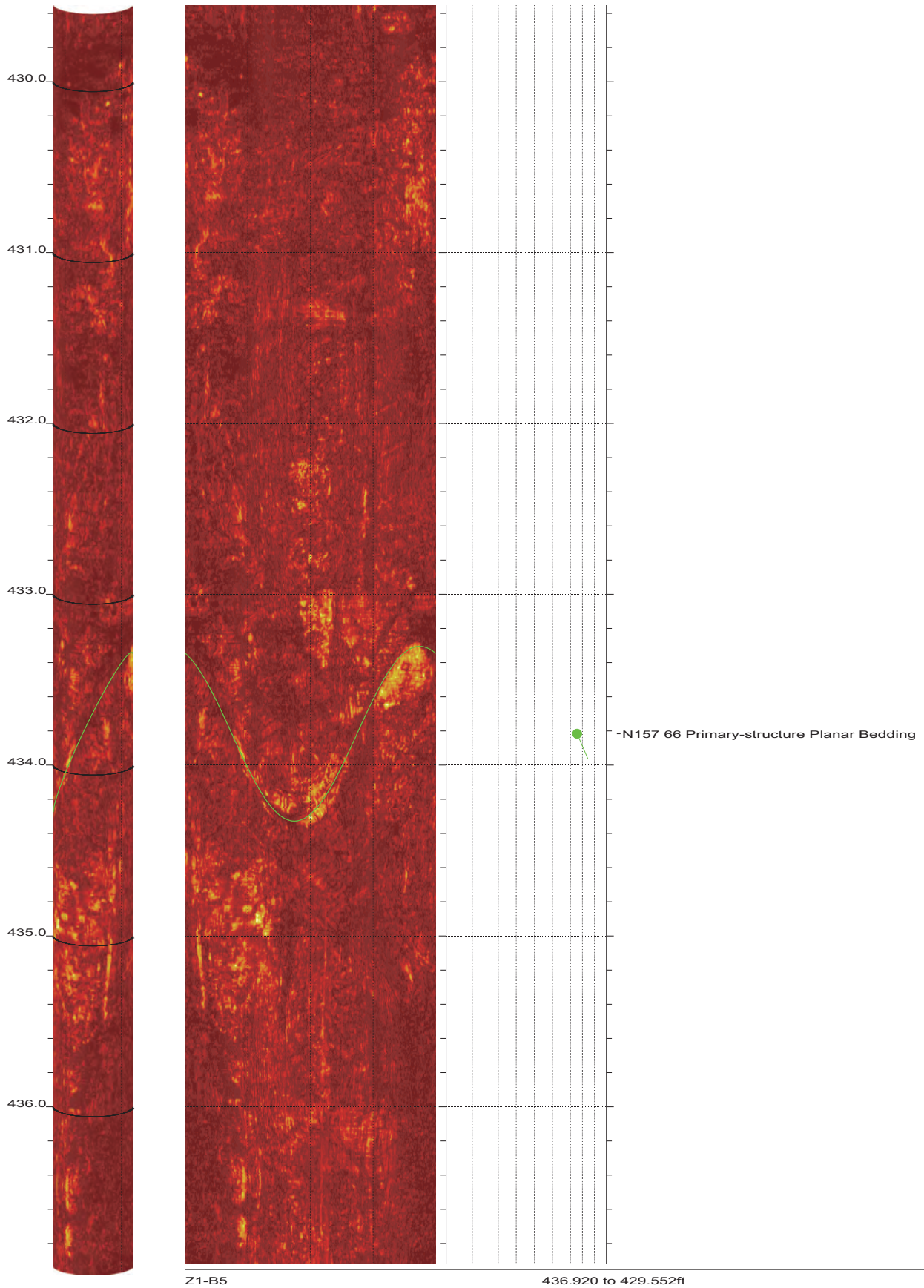


Z1-B5

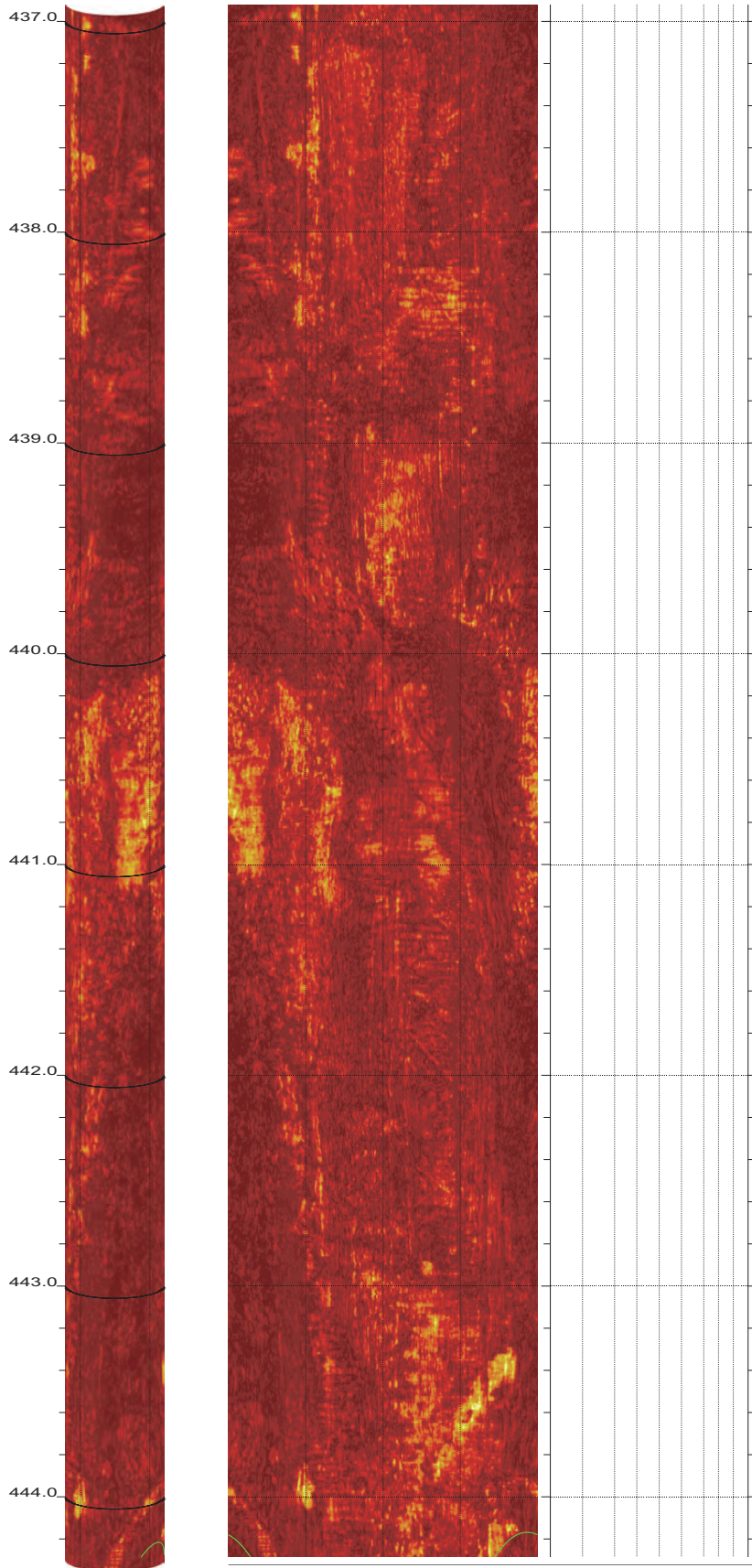
429.552 to 422.184ft

54

SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 54 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 55 of 64

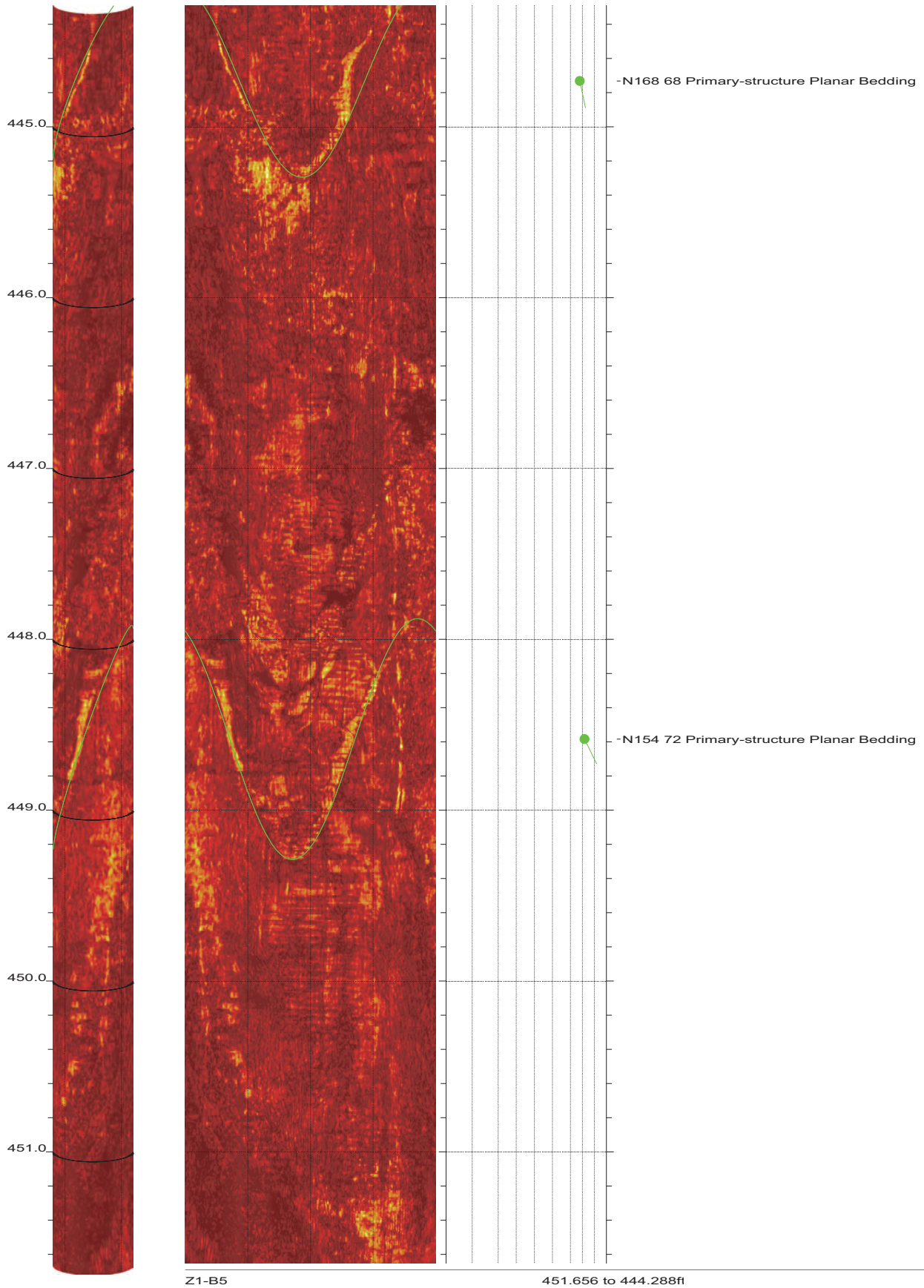


Z1-B5

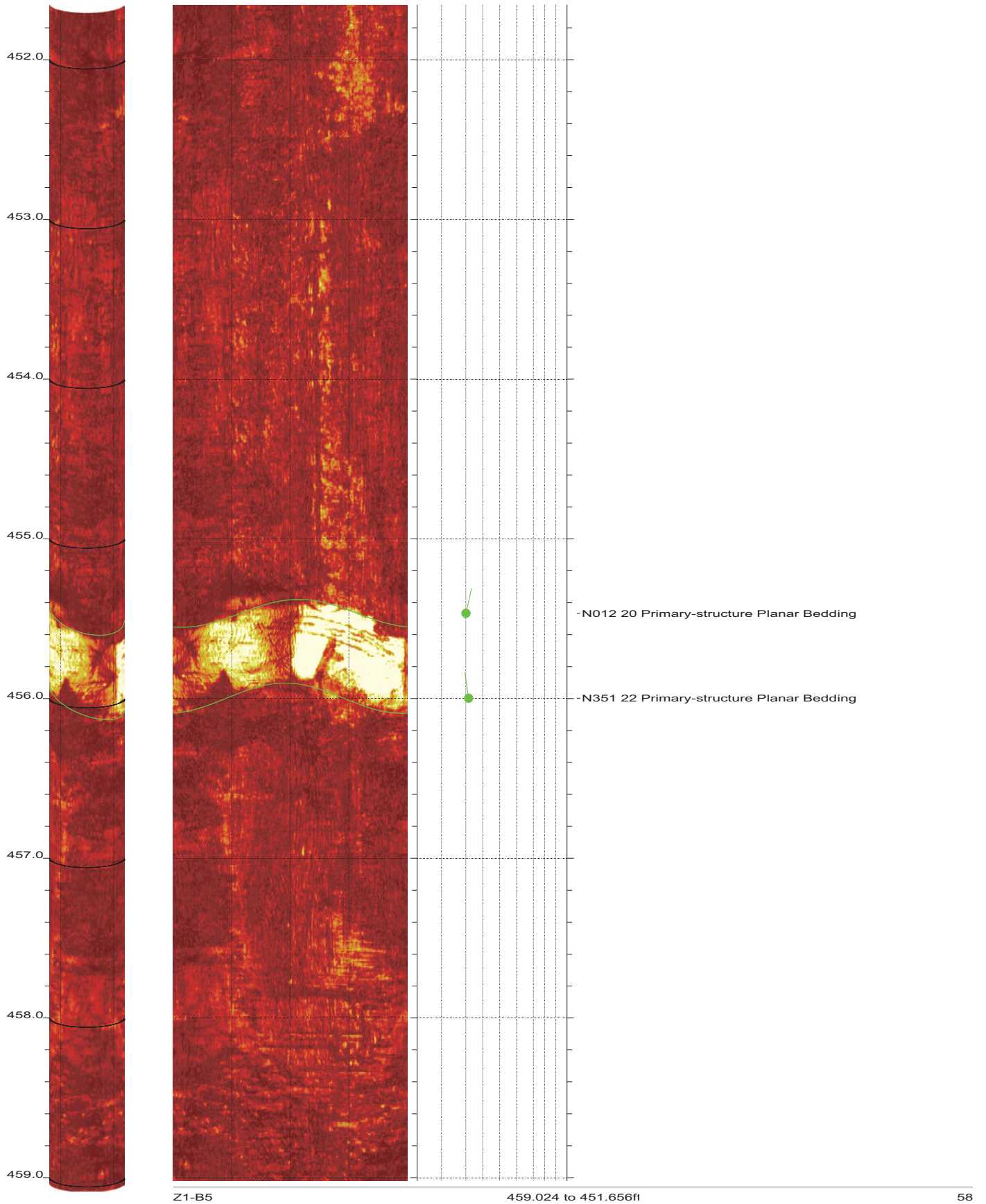
444.288 to 436.920ft

56

SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 56 of 64

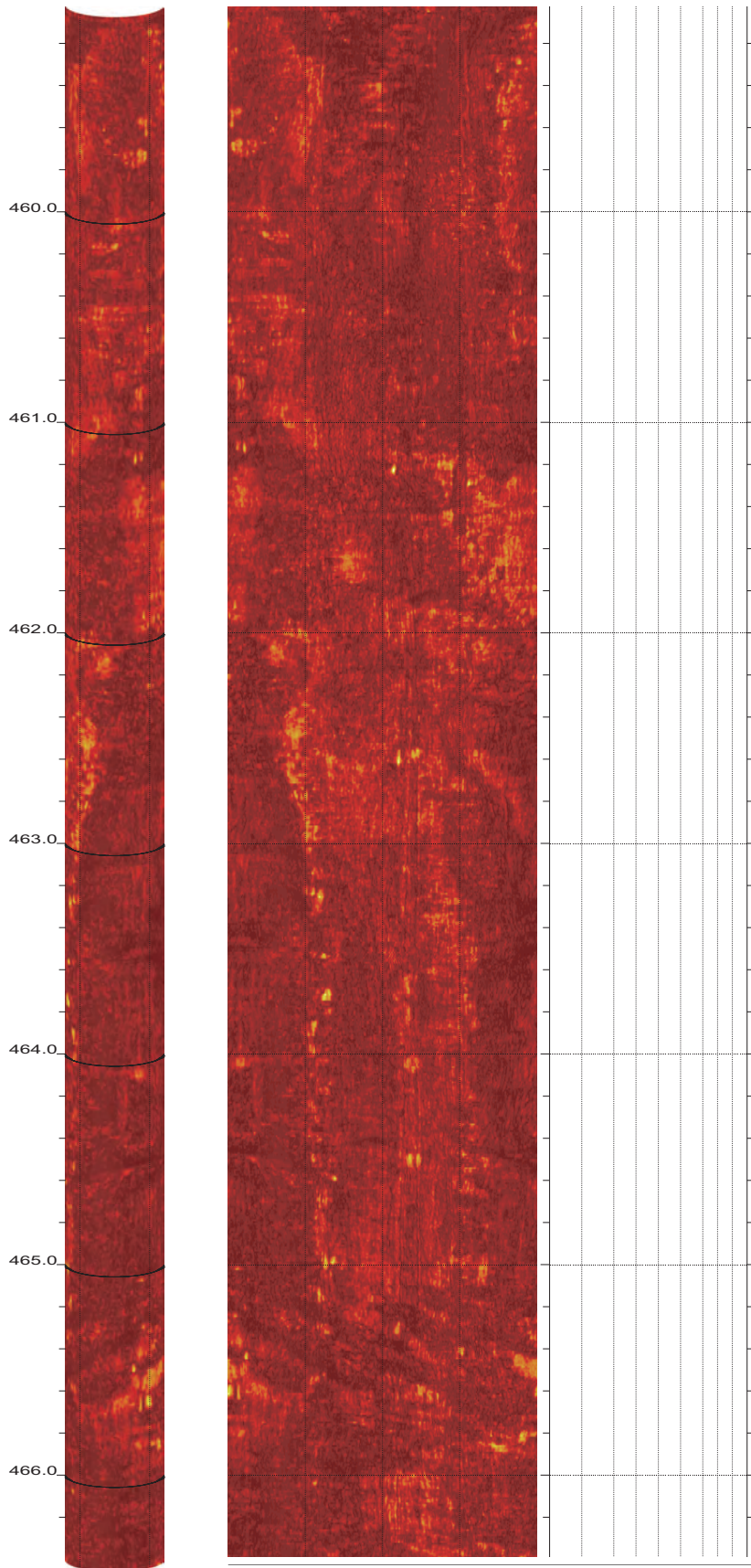


SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 57 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 58 of 64



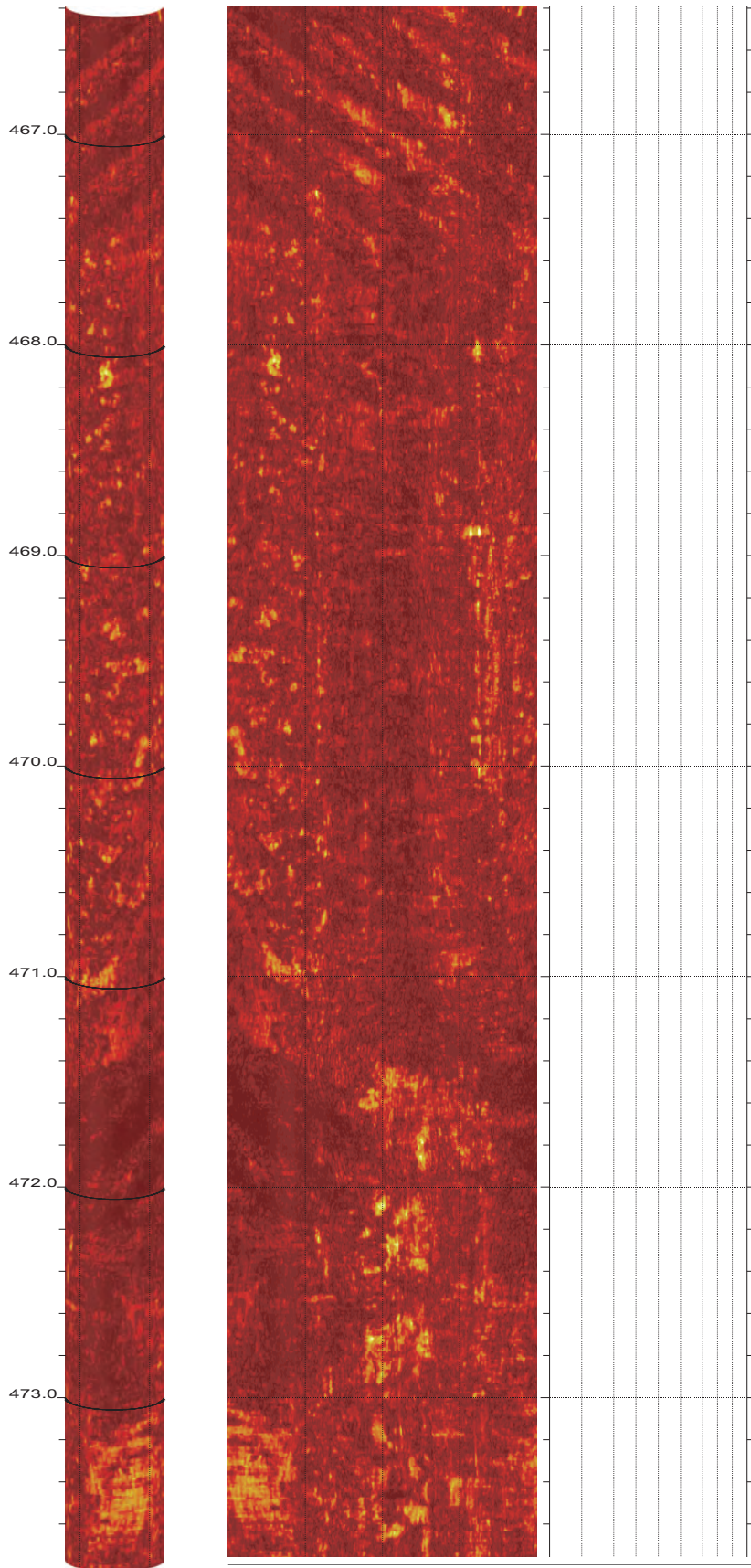


Z1-B5

466.392 to 459.024ft

59

SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 59 of 64

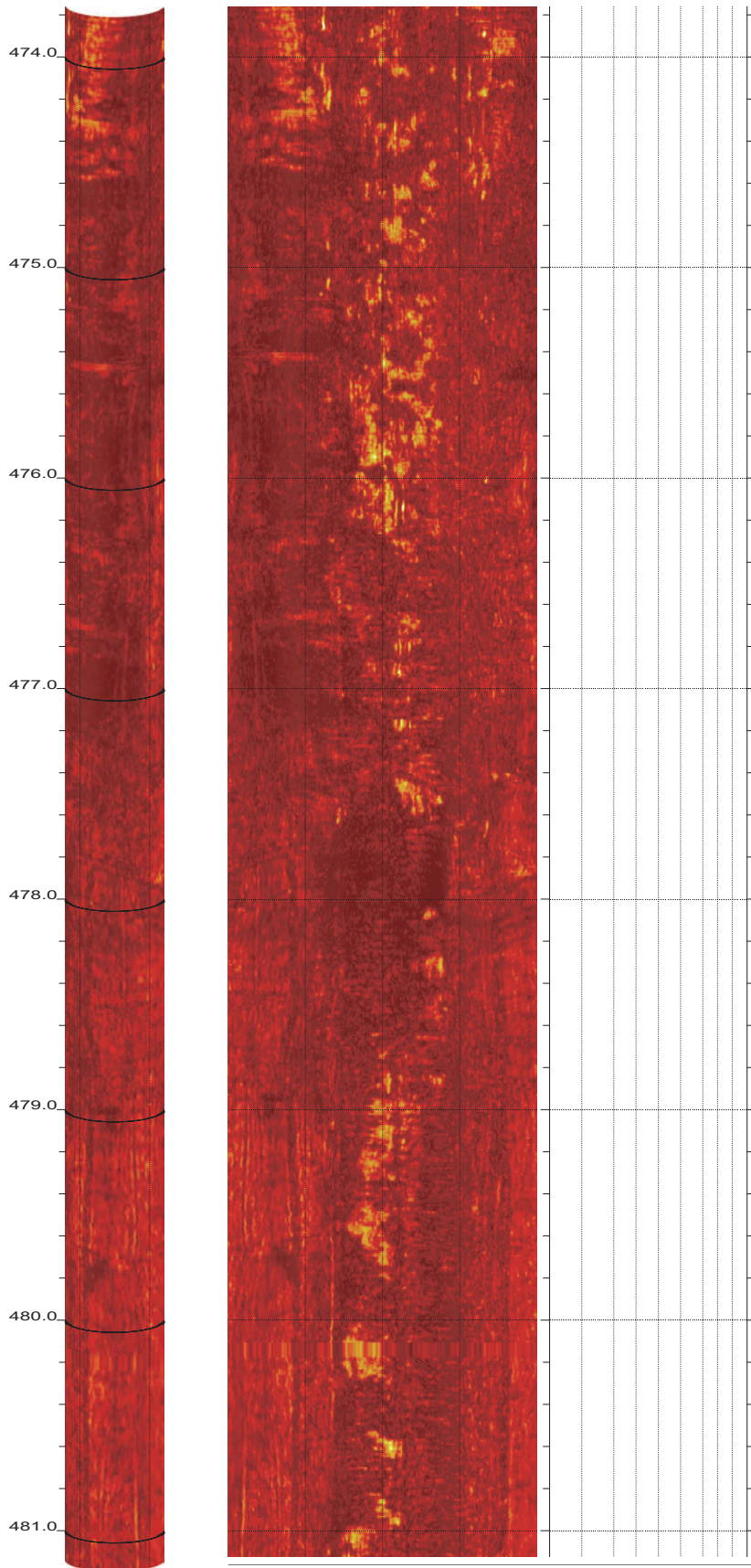


Z1-B5

473.760 to 466.392ft

60

SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 60 of 64

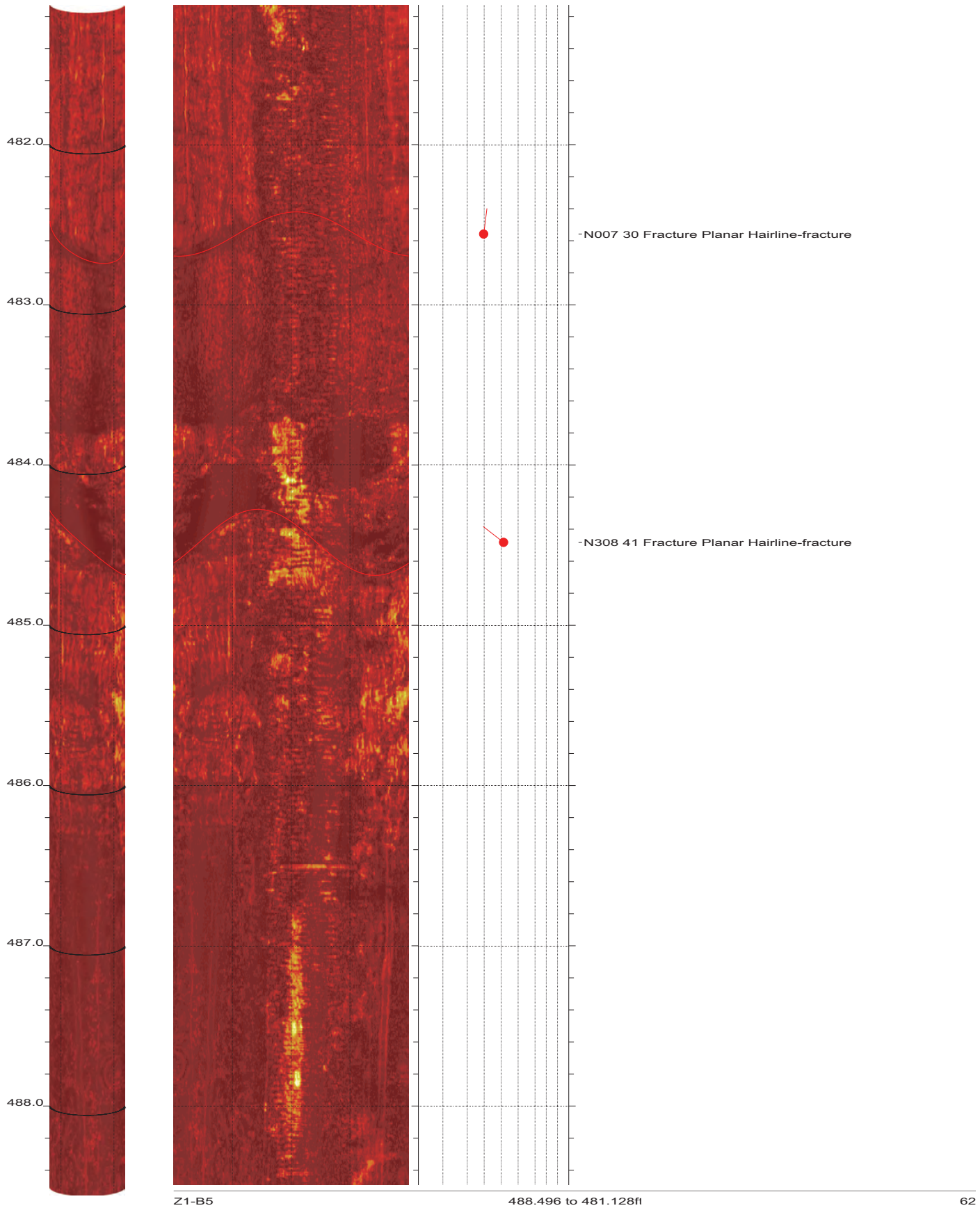


Z1-B5

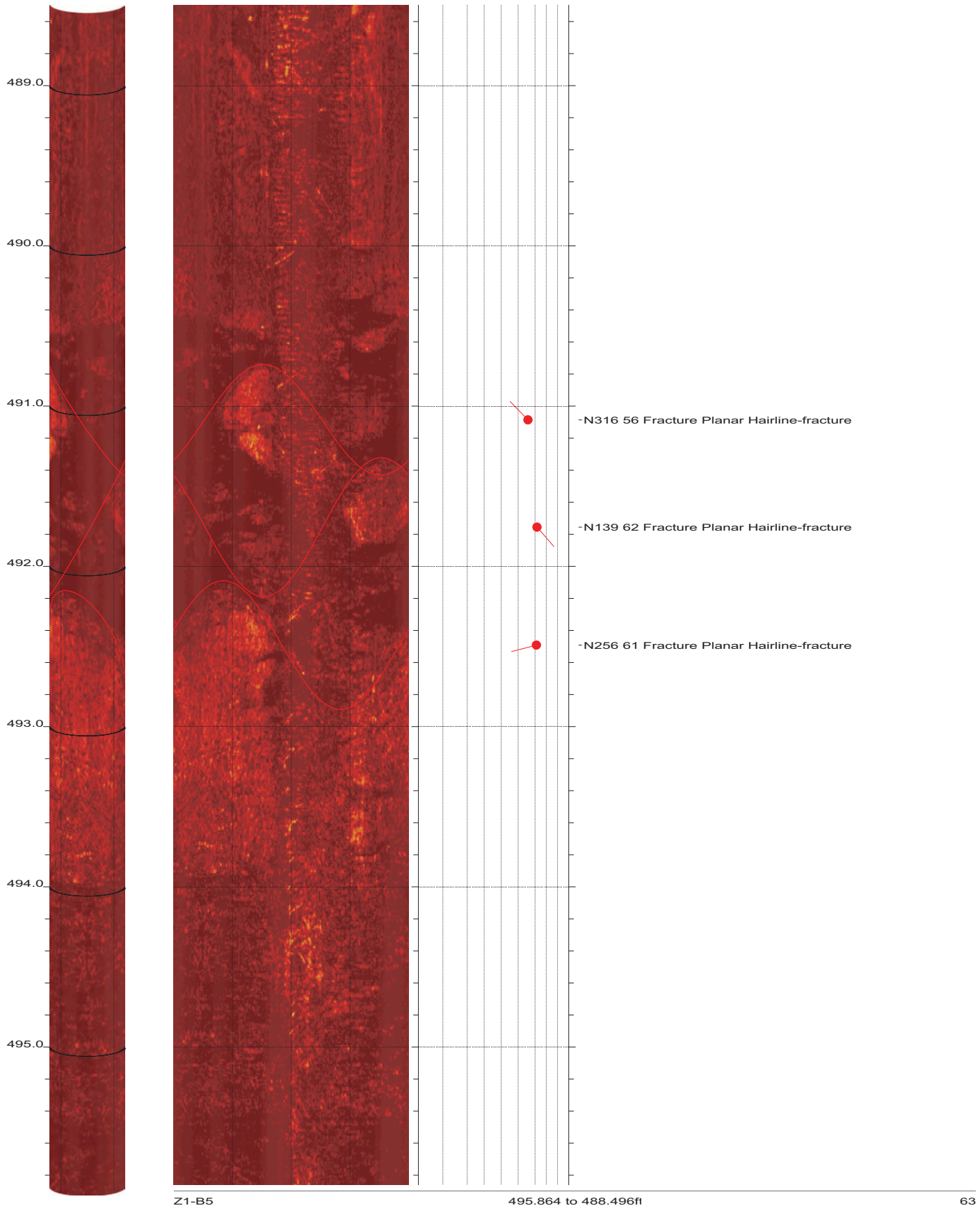
481.128 to 473.760ft

61

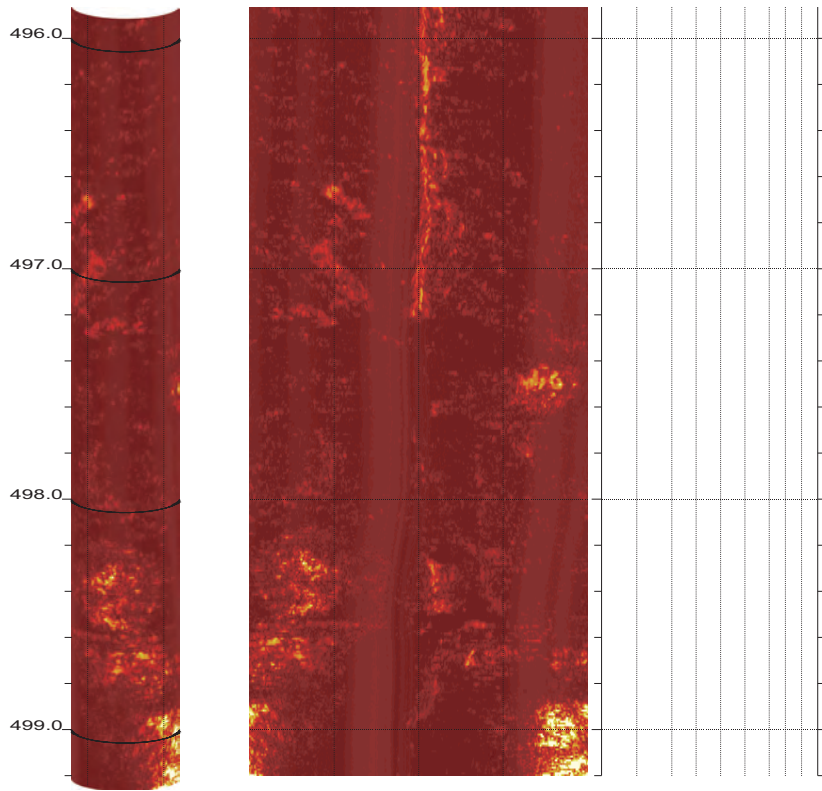
SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 61 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 62 of 64



SR-710 Boring Z1-B5 Acoustic Televiewer Dips rev 1 Sheet 63 of 64





CASCADE DRILLING

Borehole: Z1-B6

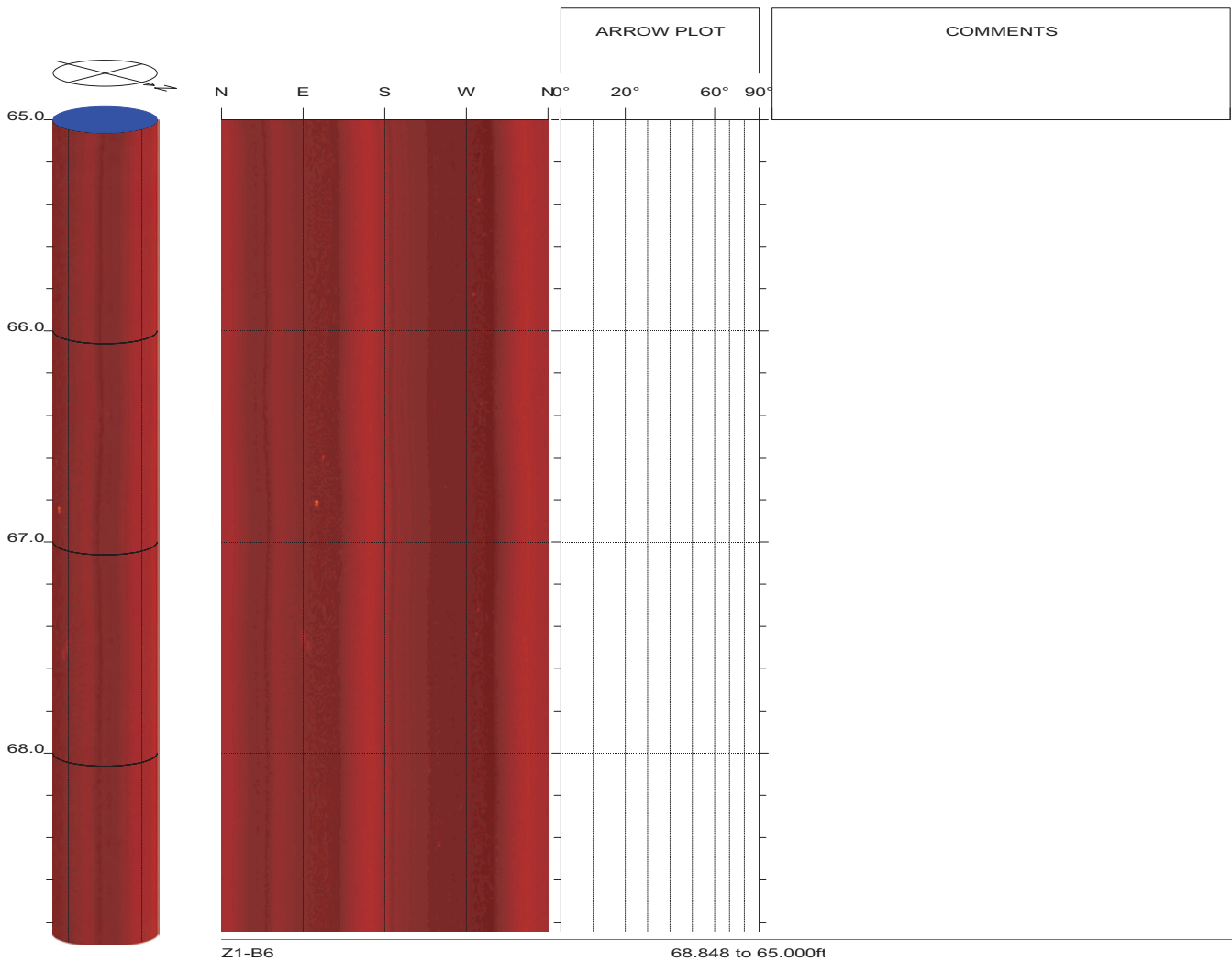
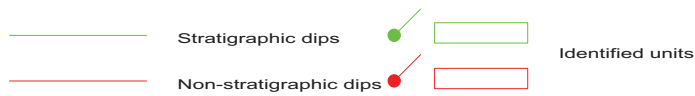
SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

Zone from 399.800 to 65.000ft  
 Format: BHTV-NESWN

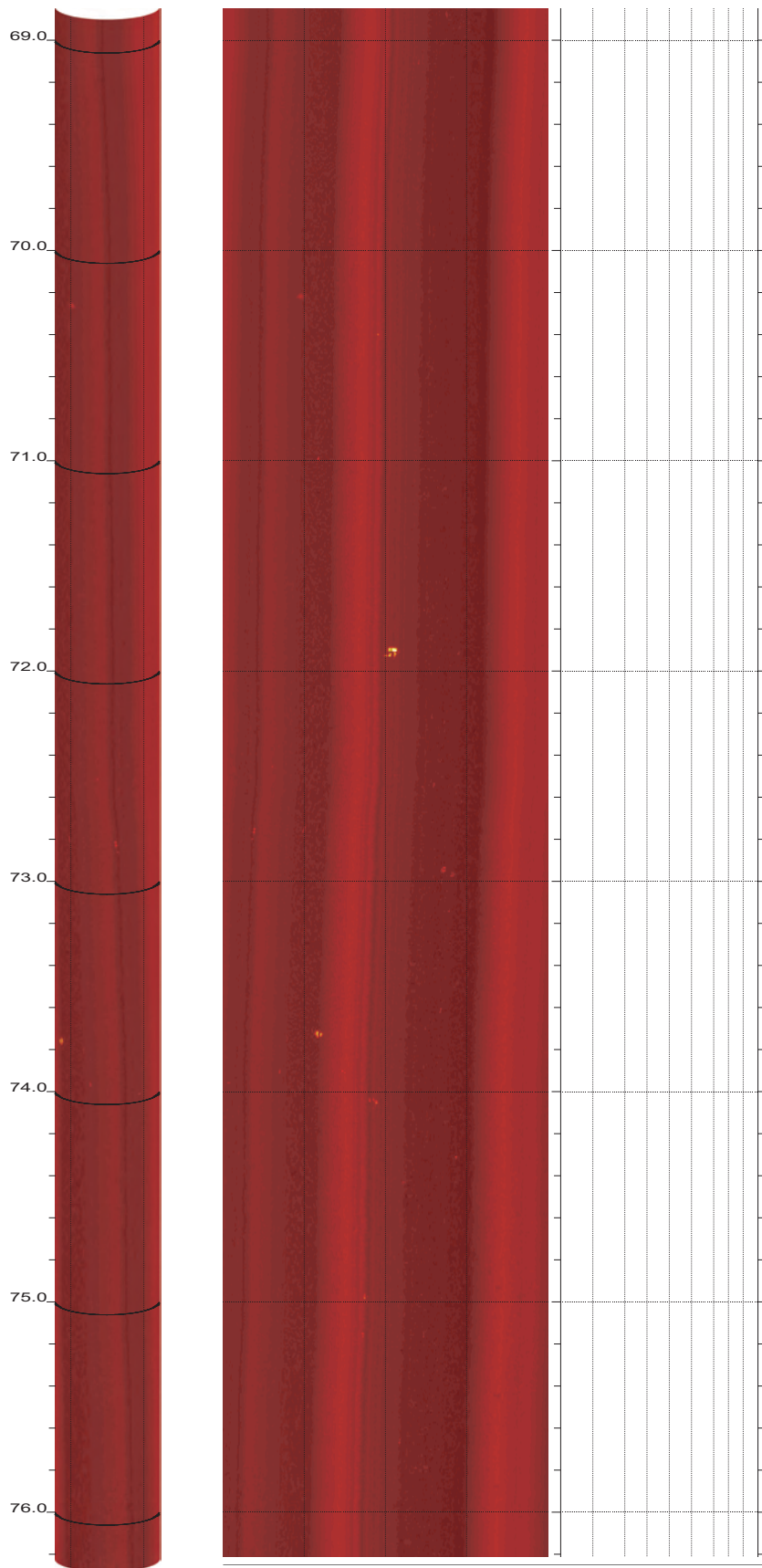
Borehole diam: 5.900inch  
 Vertical = borehole-axis  
 Image: Amplitude



Z1-B6

68.848 to 65.000ft

1



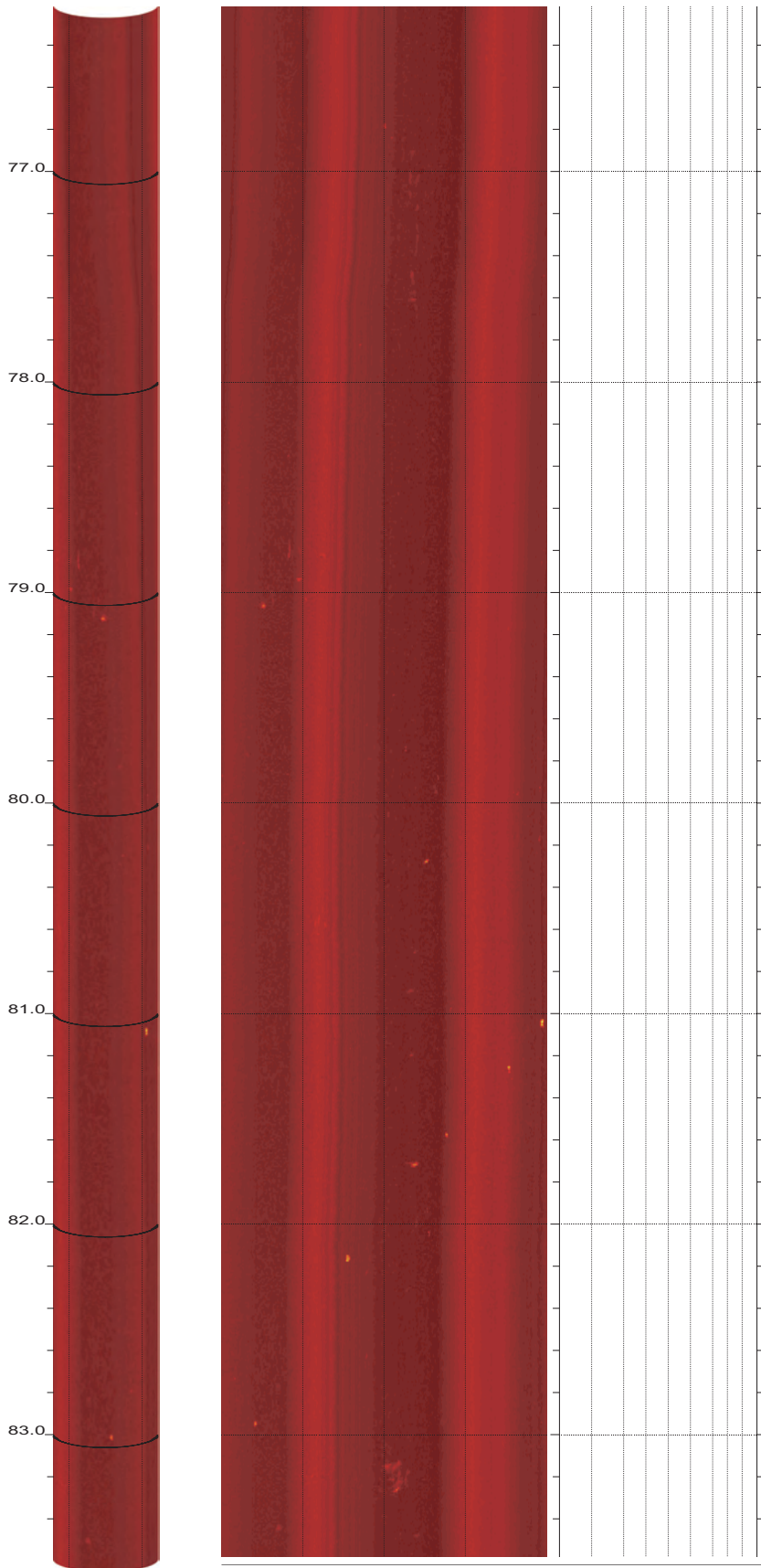
Z1-B6

76.216 to 68.848ft

2

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 2 of 46



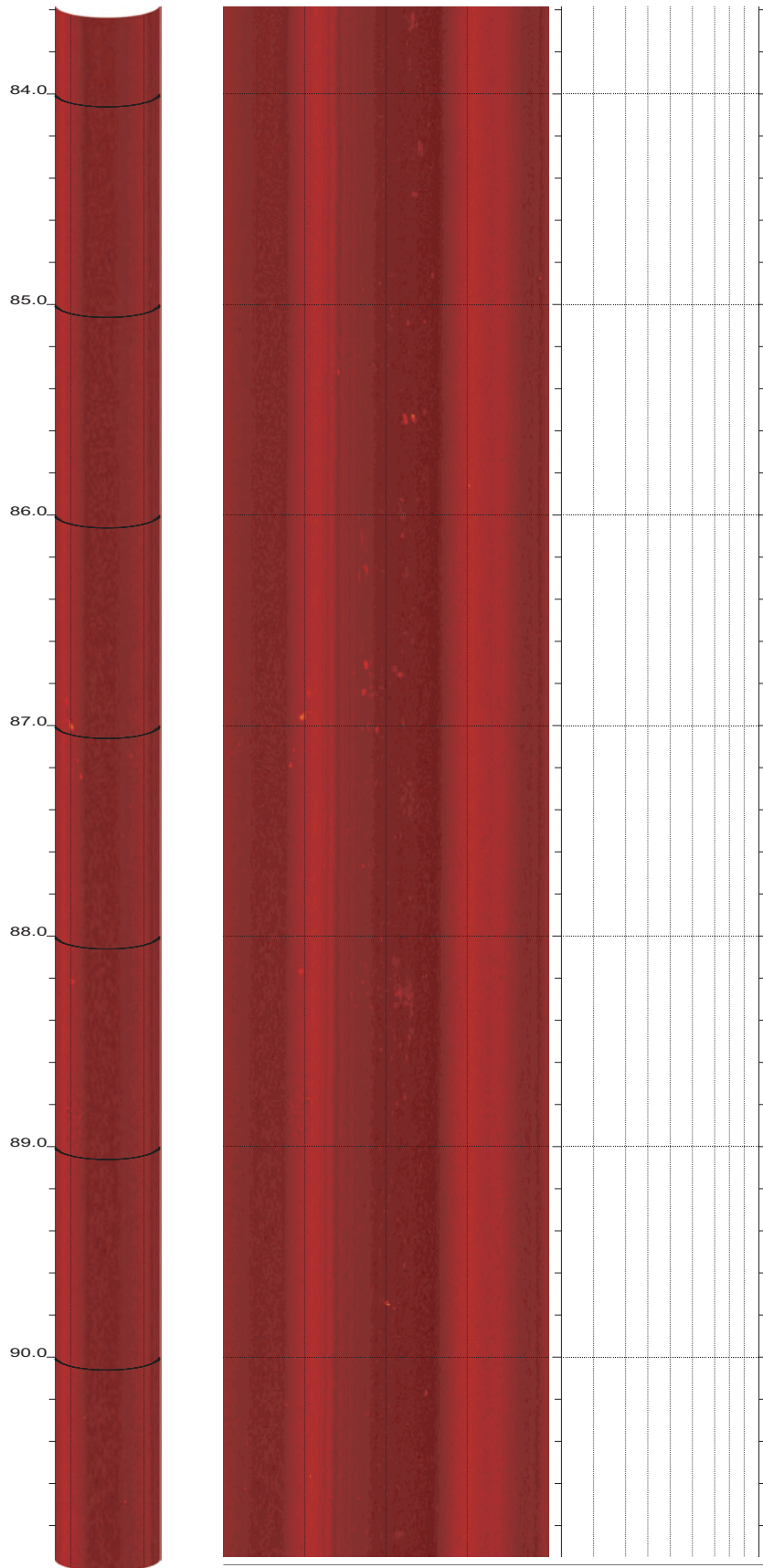


Z1-B6

83.584 to 76.216ft

3

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 3 of 46

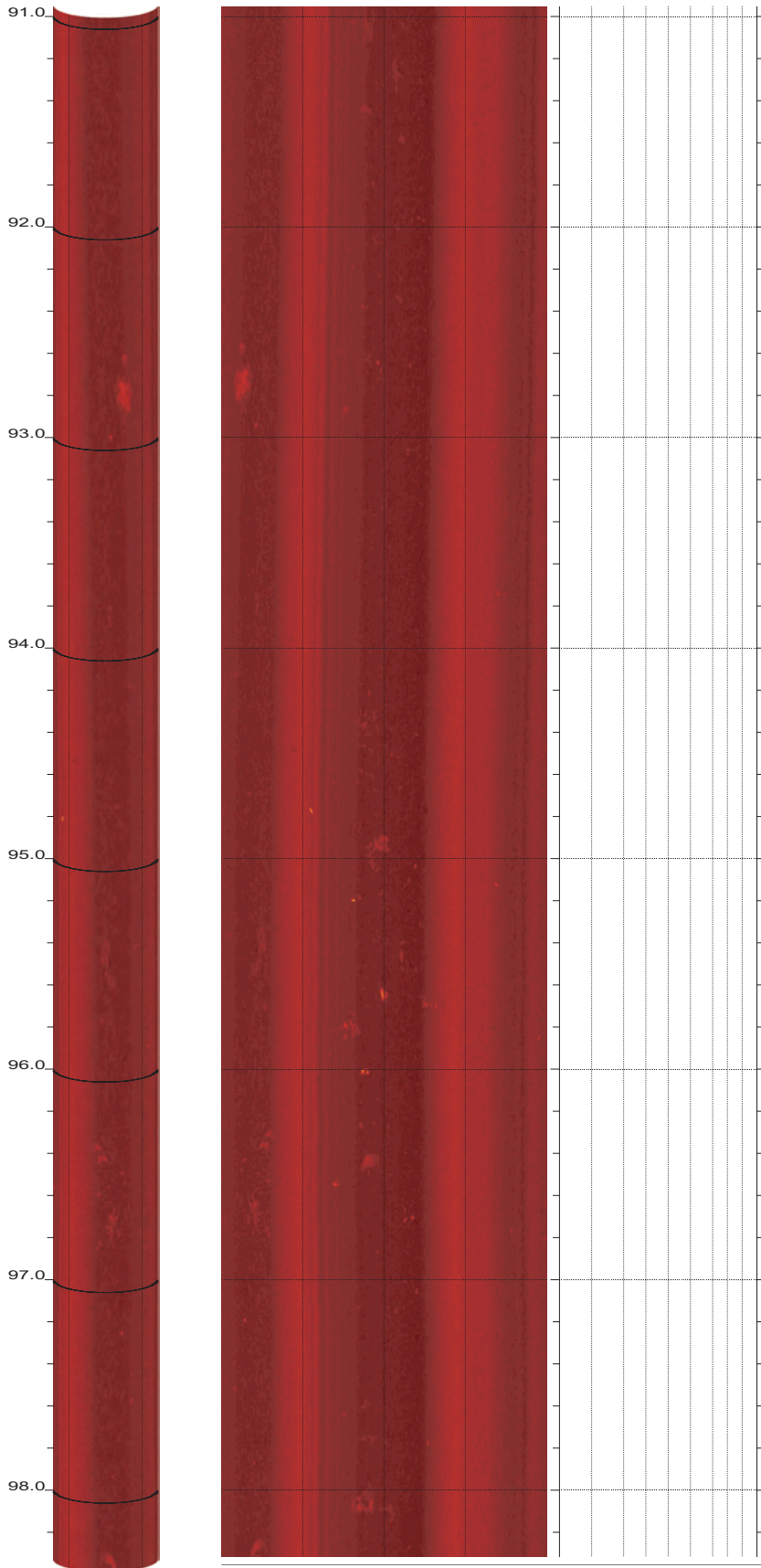


Z1-B6

90.952 to 83.584ft

4

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 4 of 46

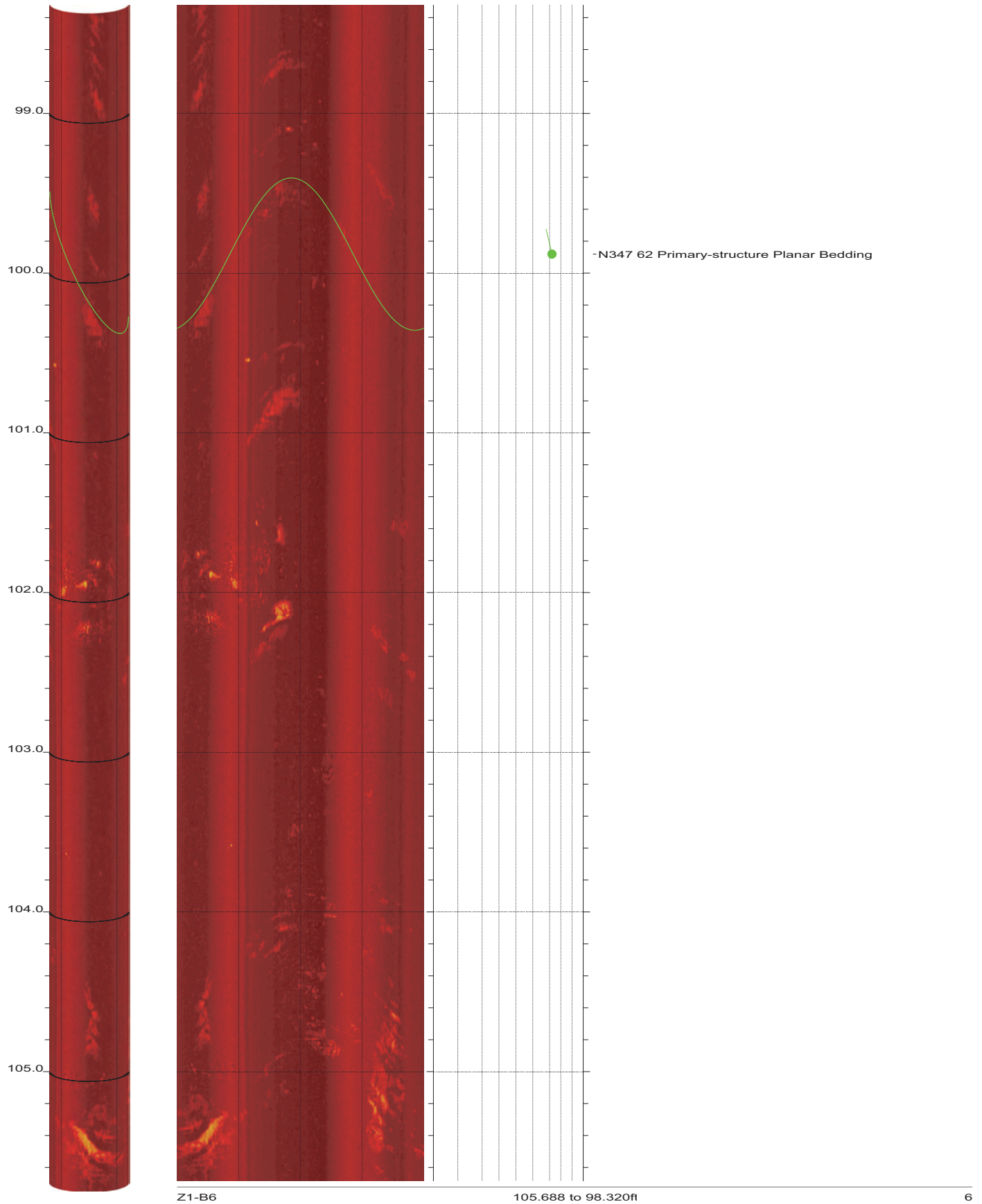


Z1-B6

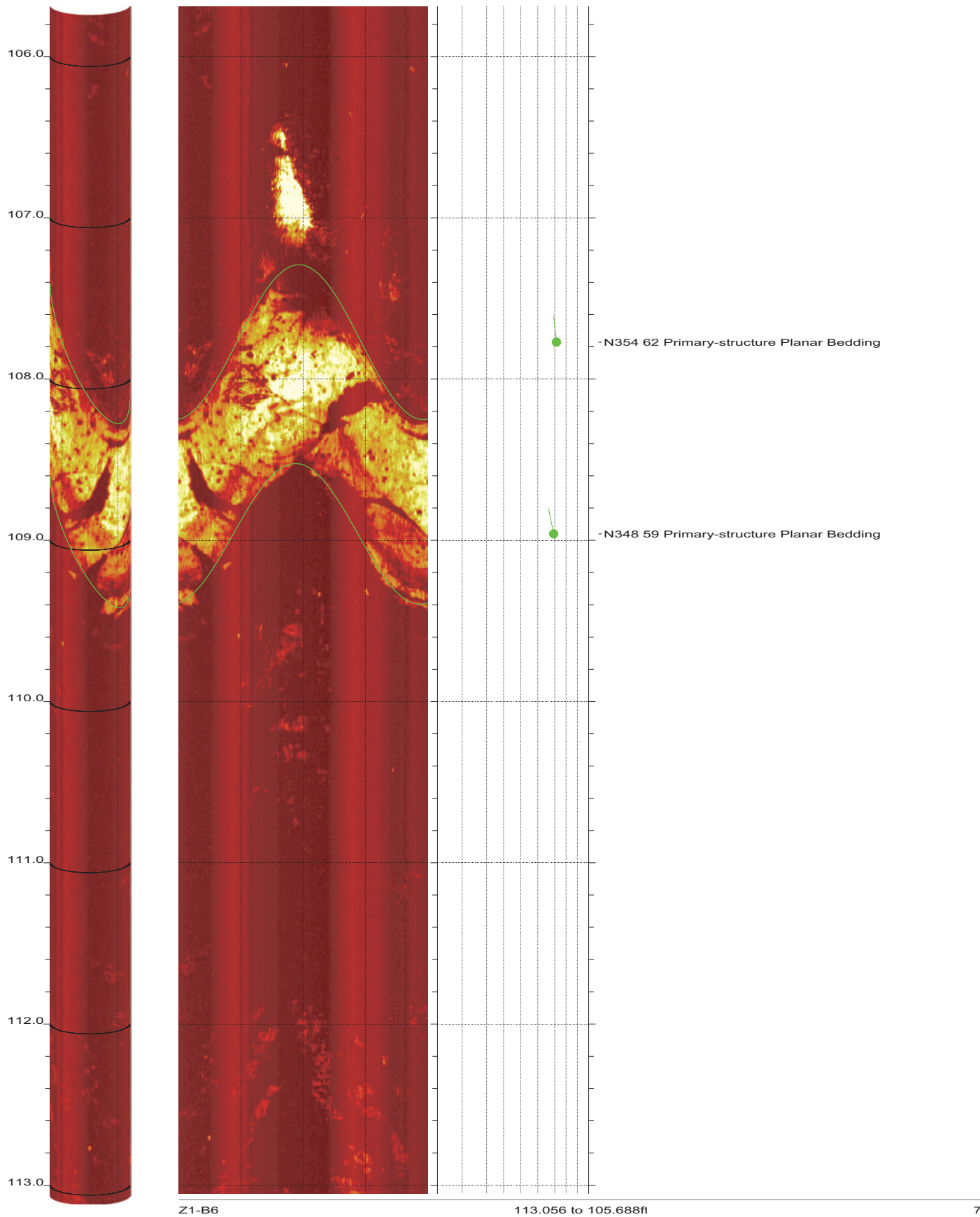
98.320 to 90.952ft

5

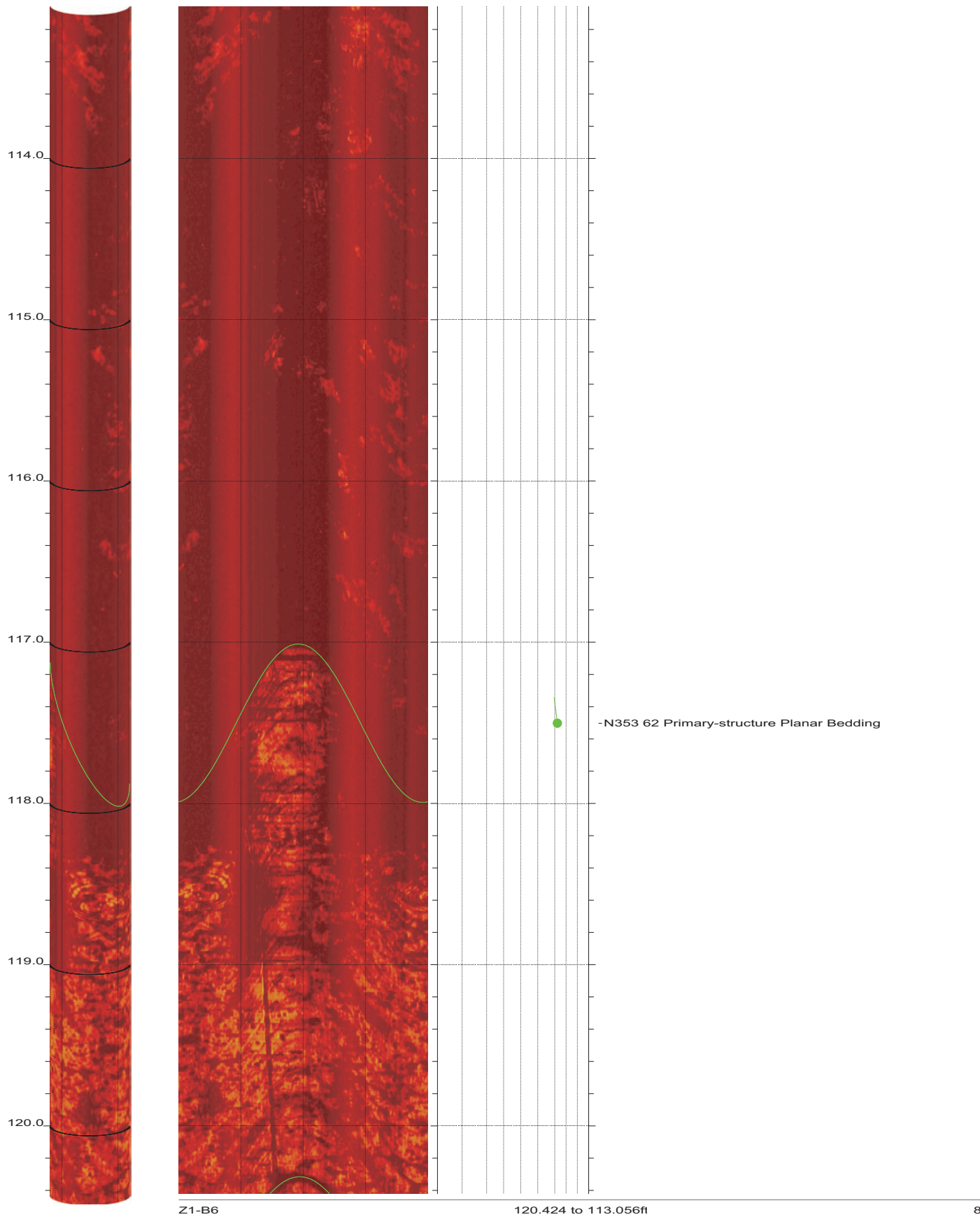
SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 5 of 46



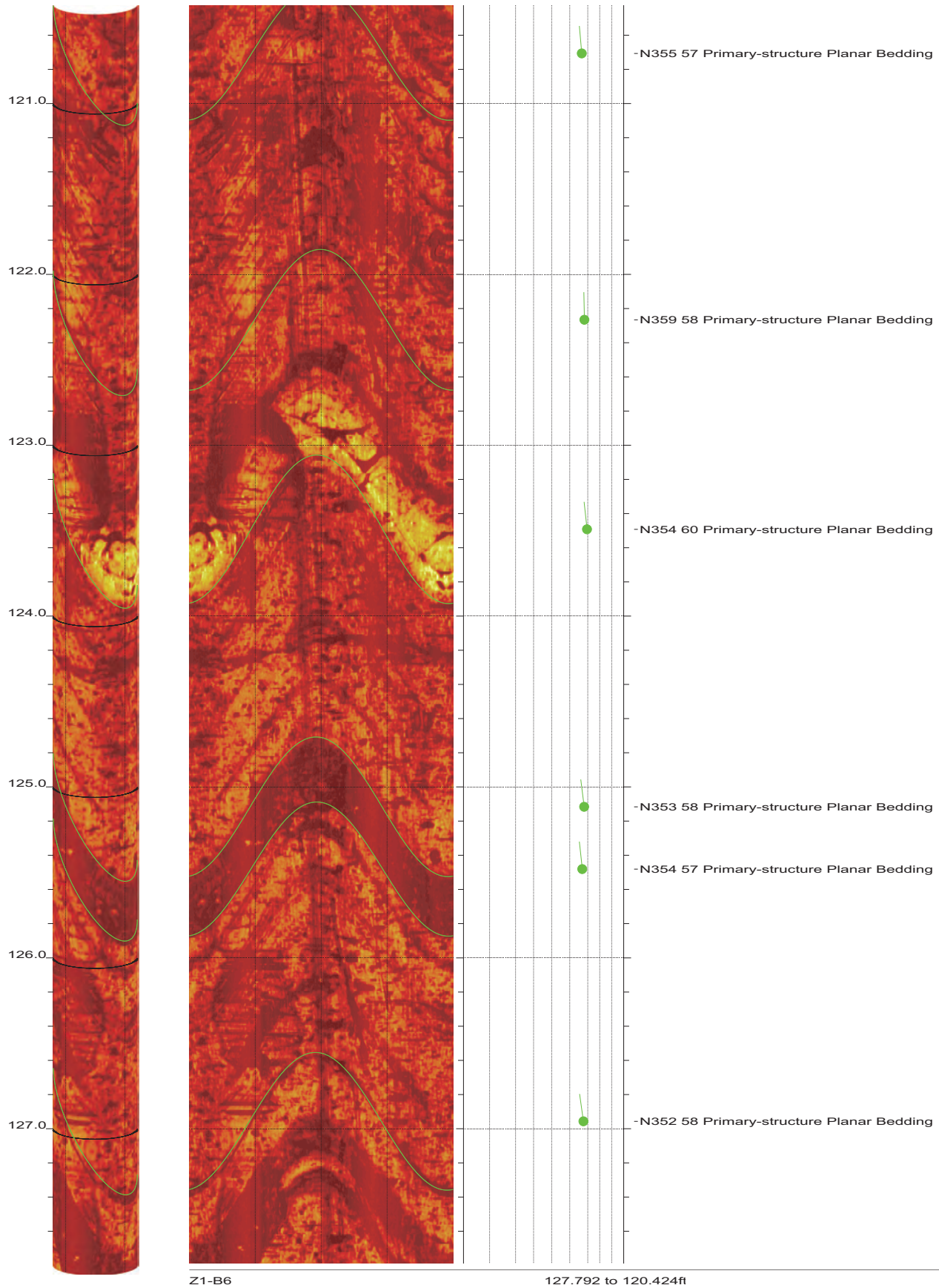
SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 6 of 46

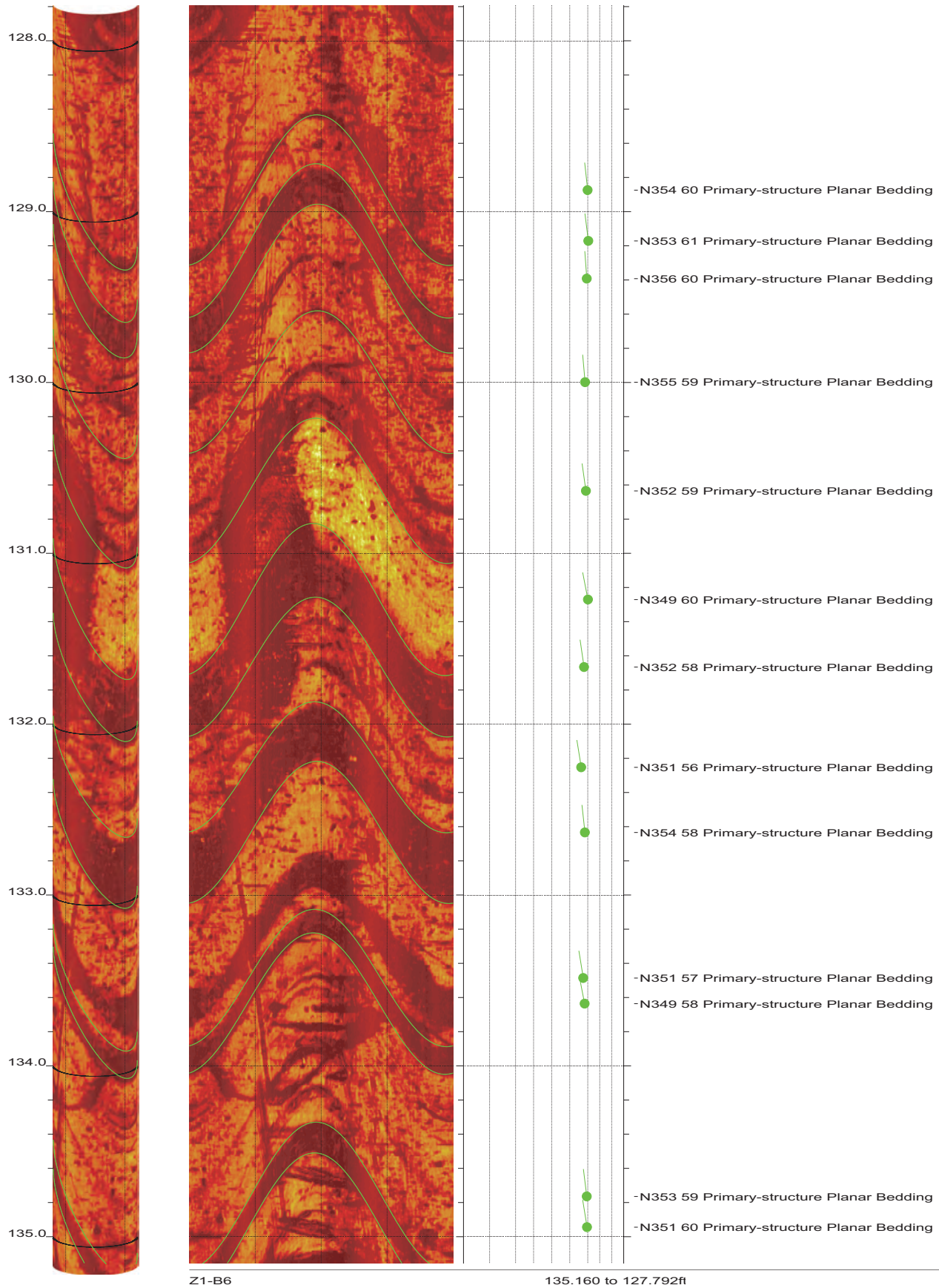


SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 7 of 46



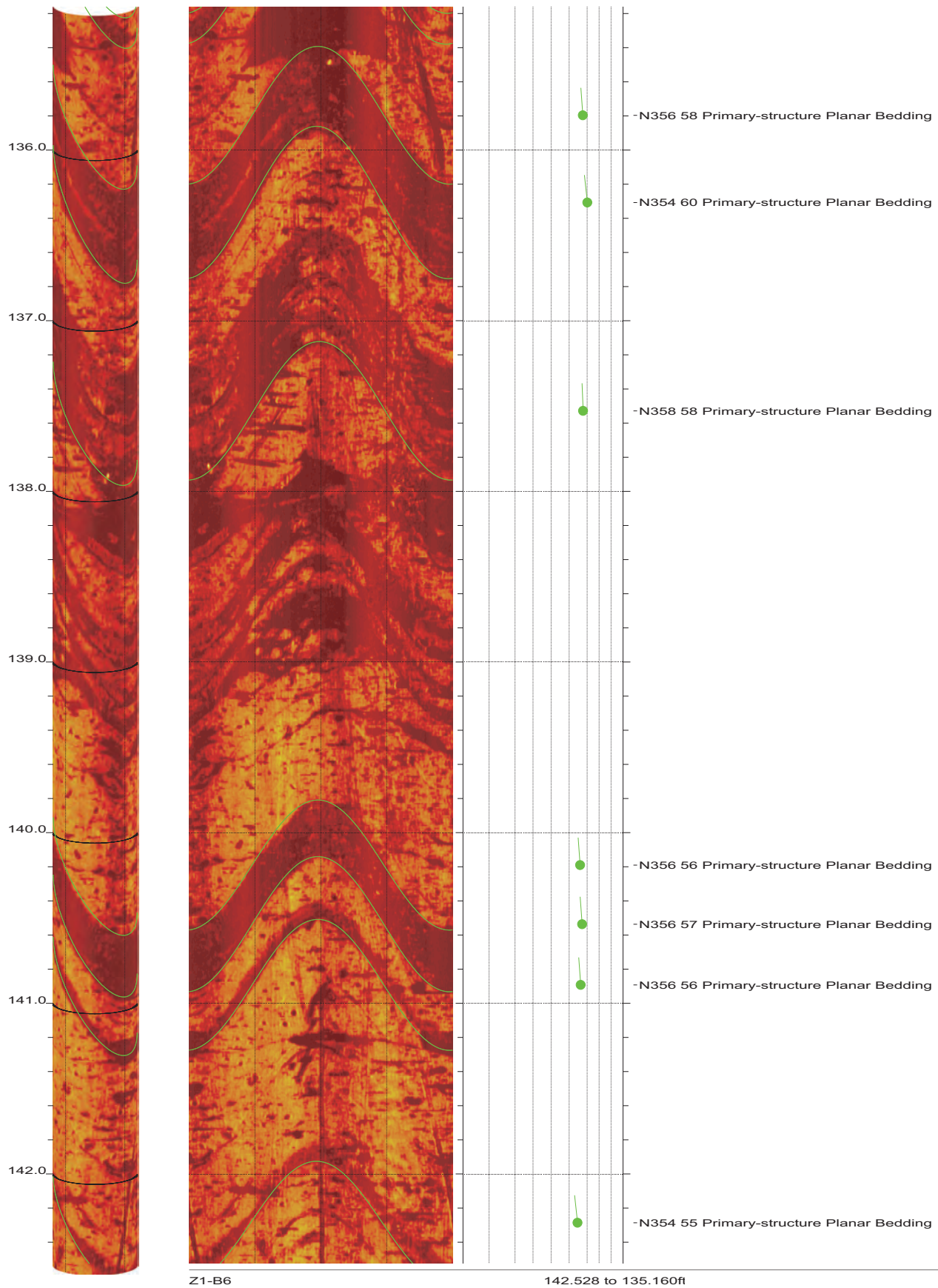
SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 8 of 46

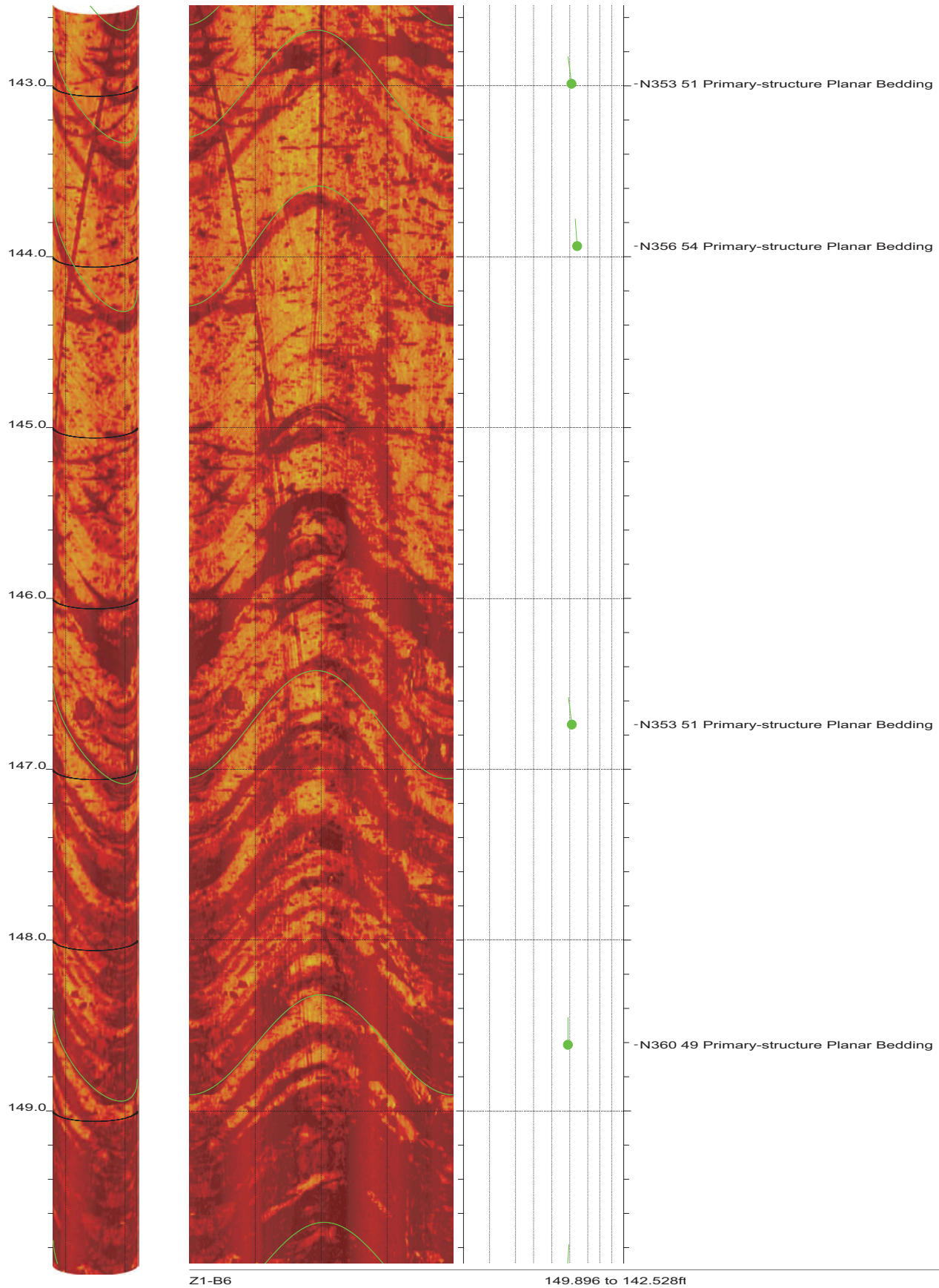




SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 10 of 46





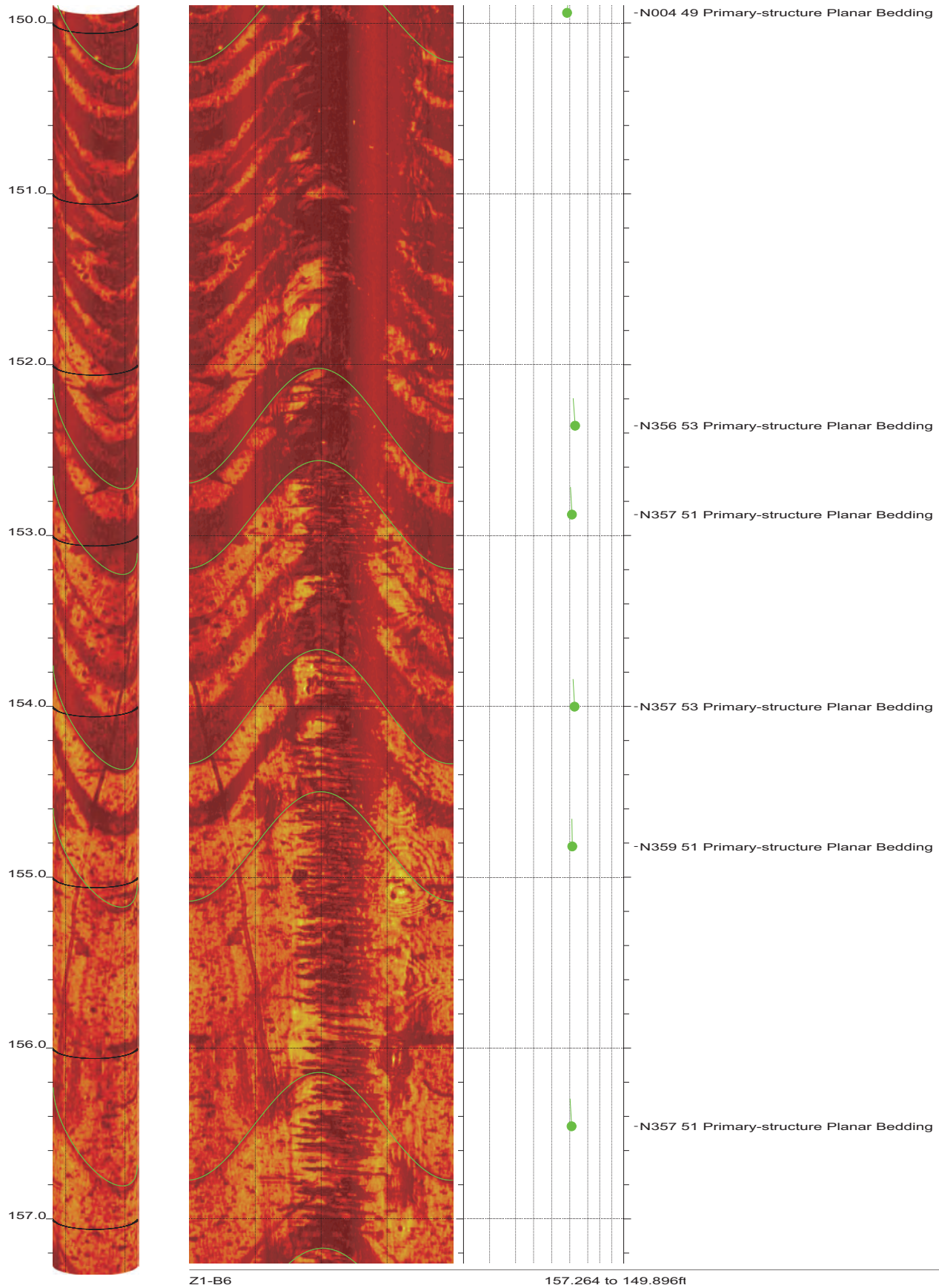


Z1-B6

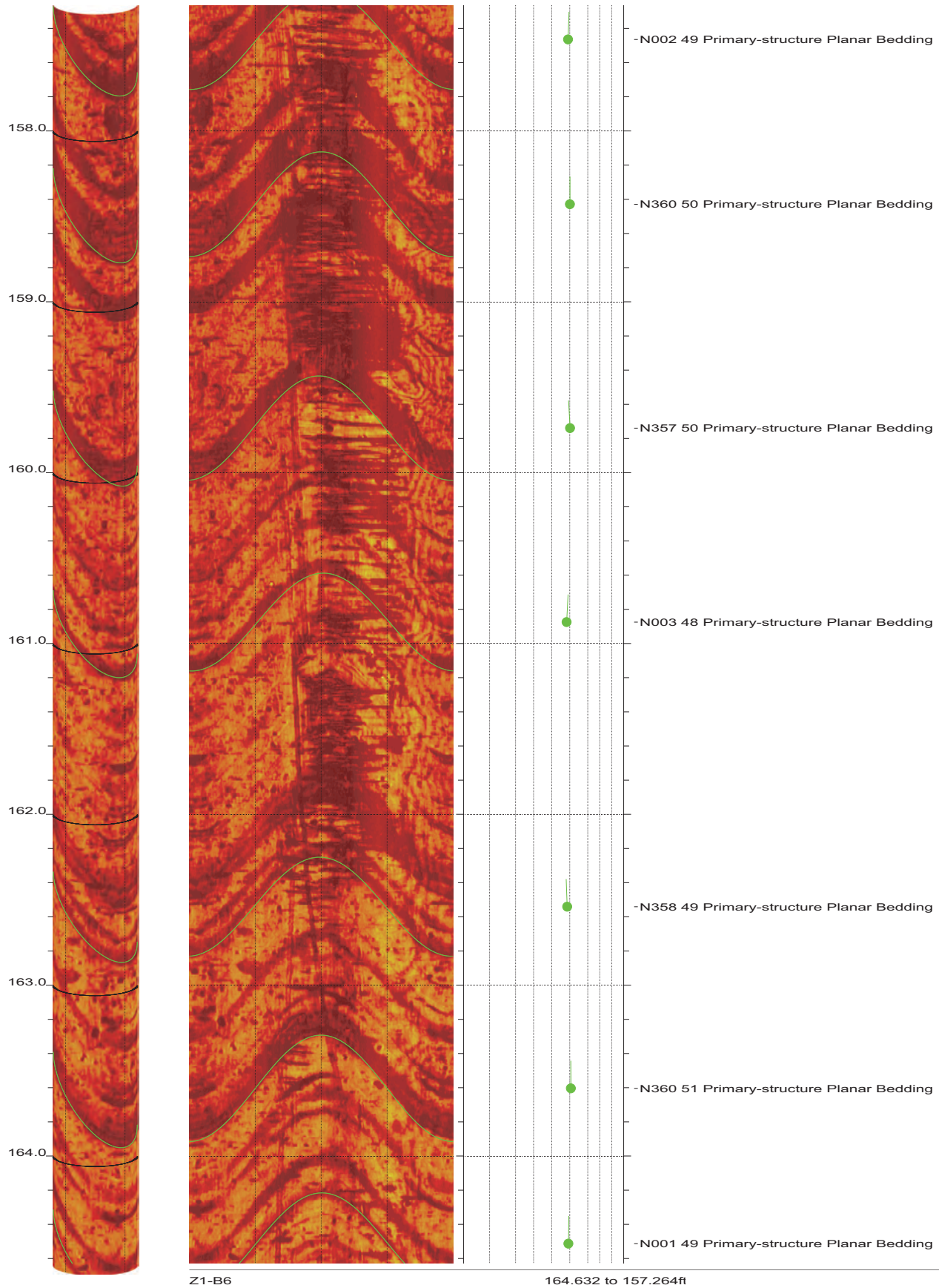
149.896 to 142.528ft

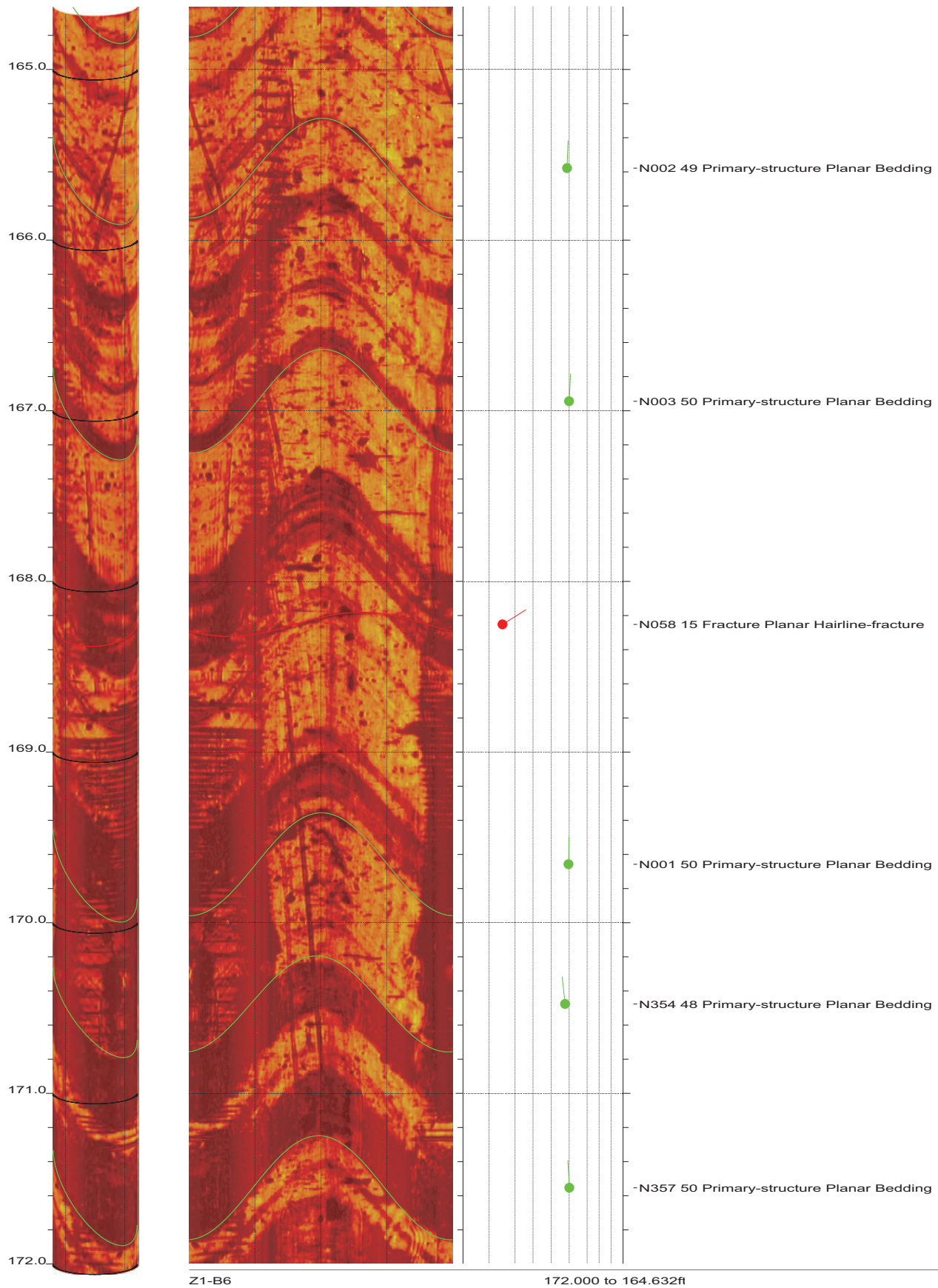
12

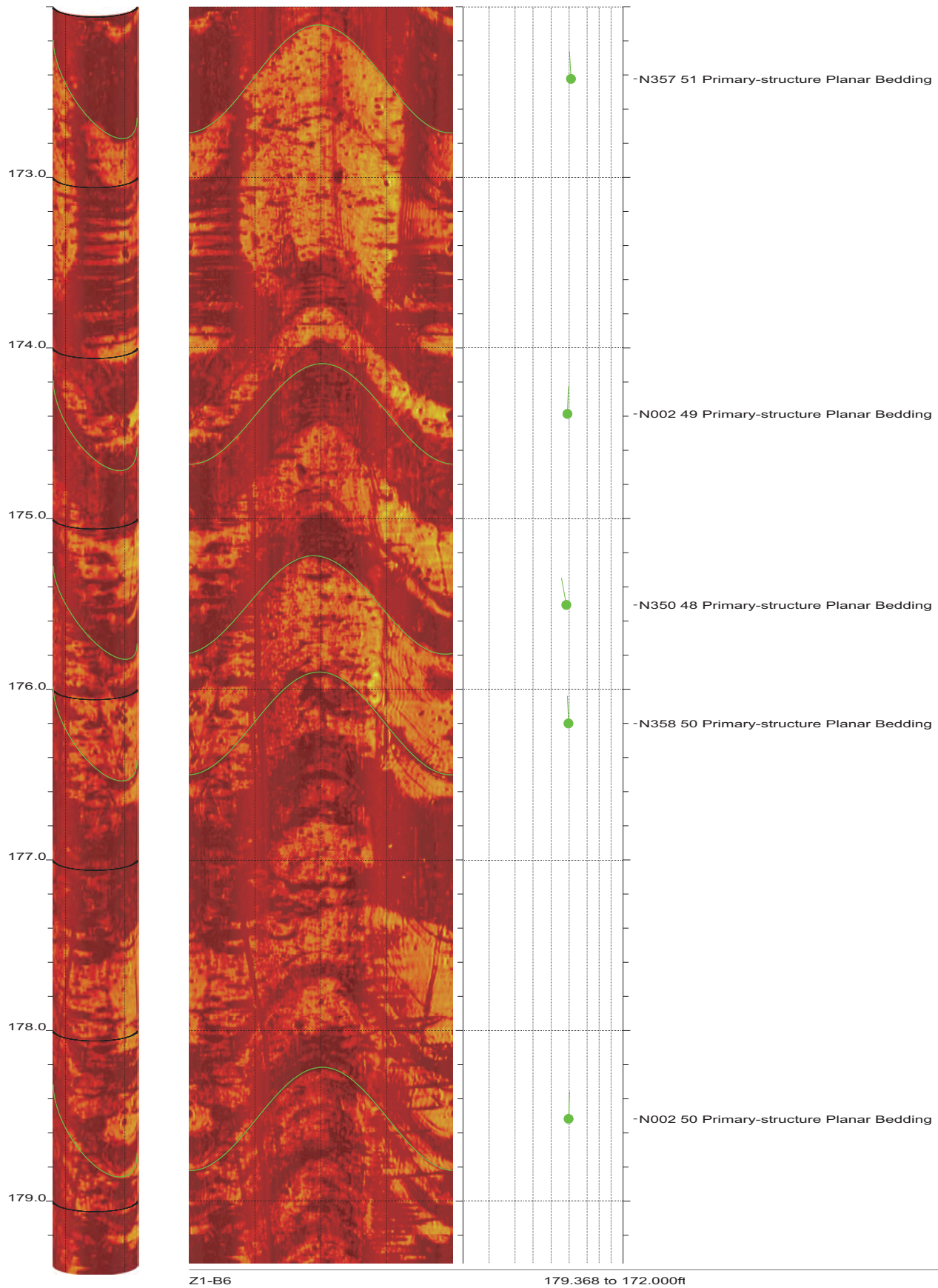
SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 12 of 46



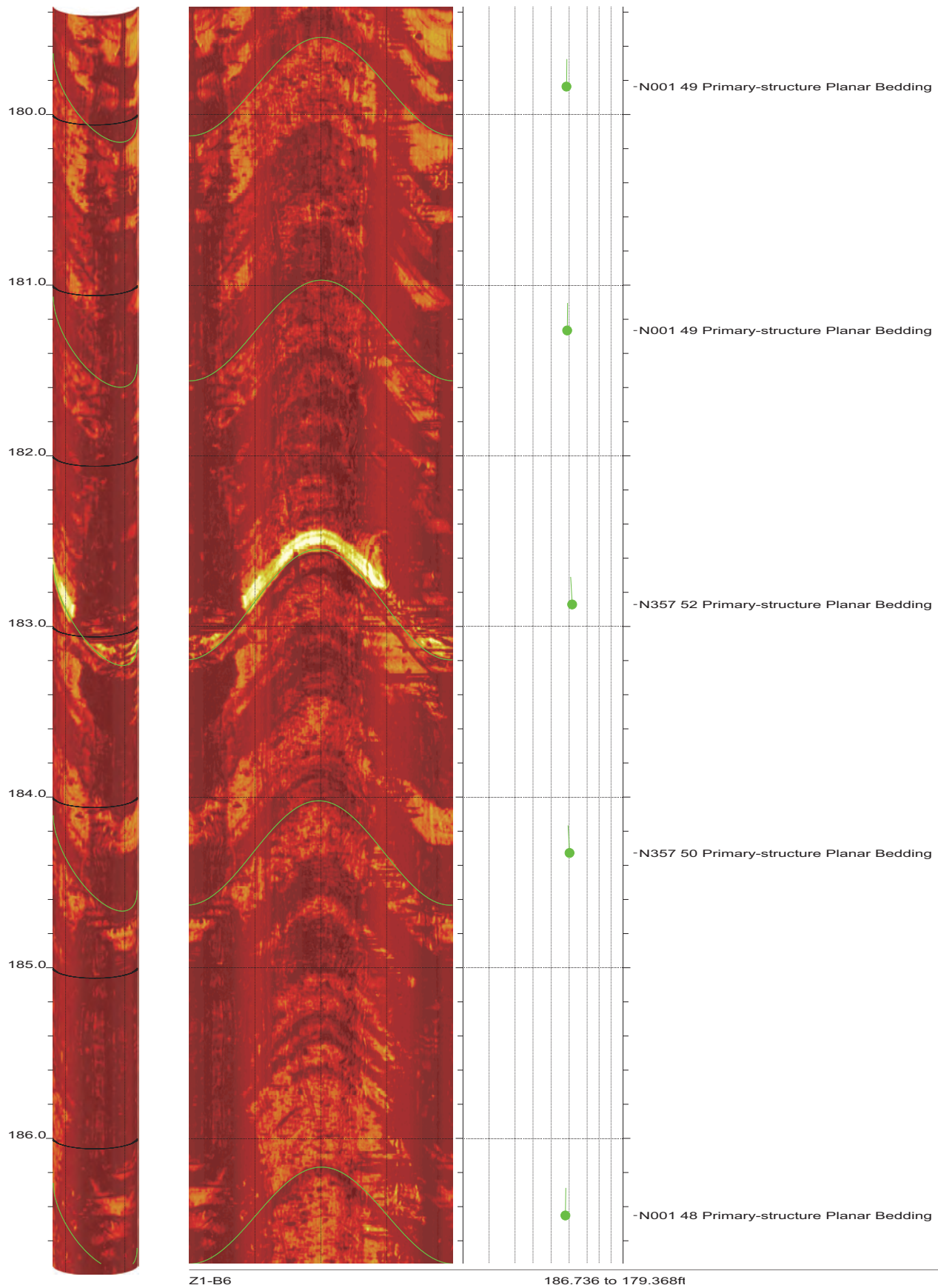
SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 13 of 46

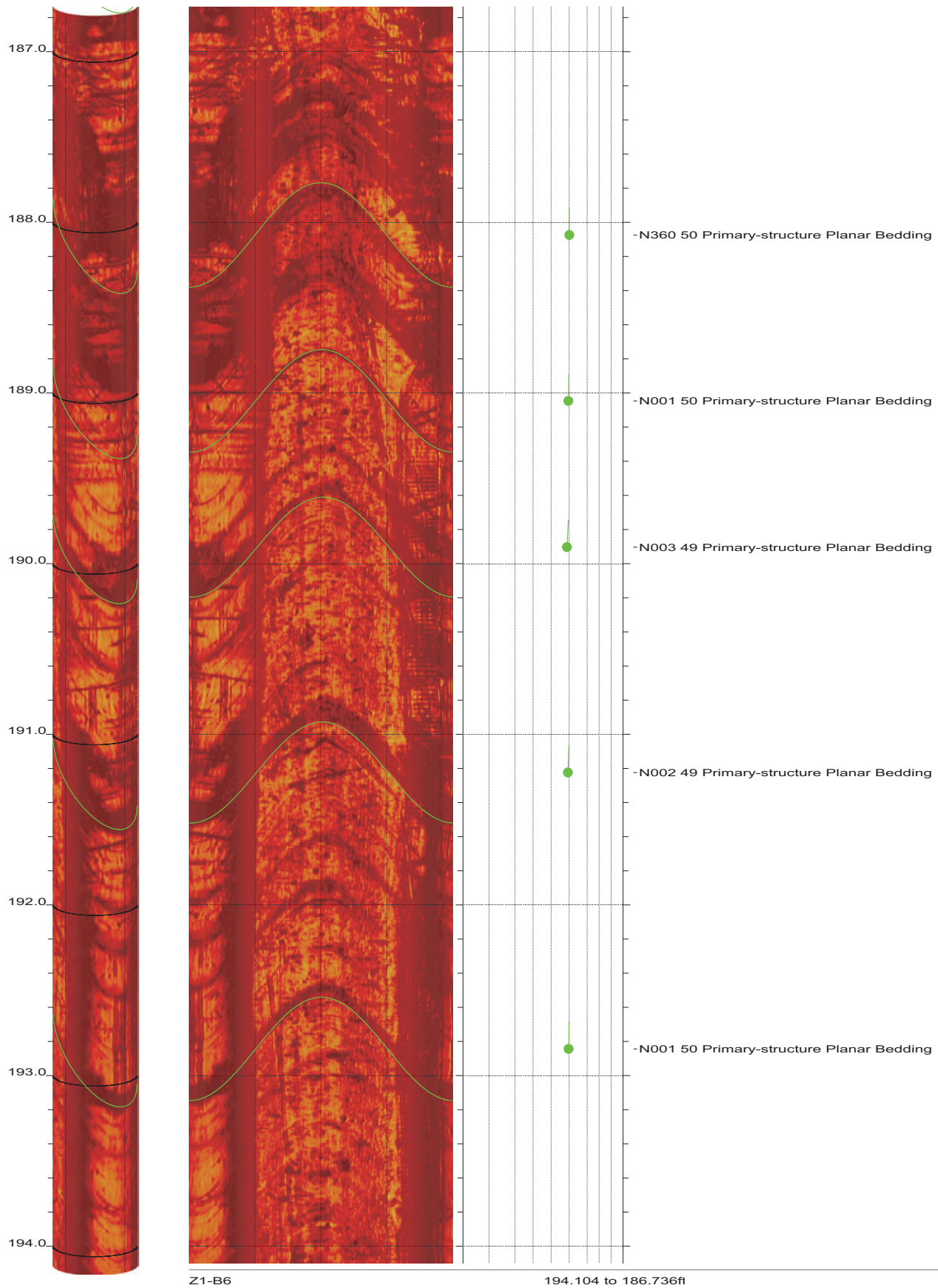






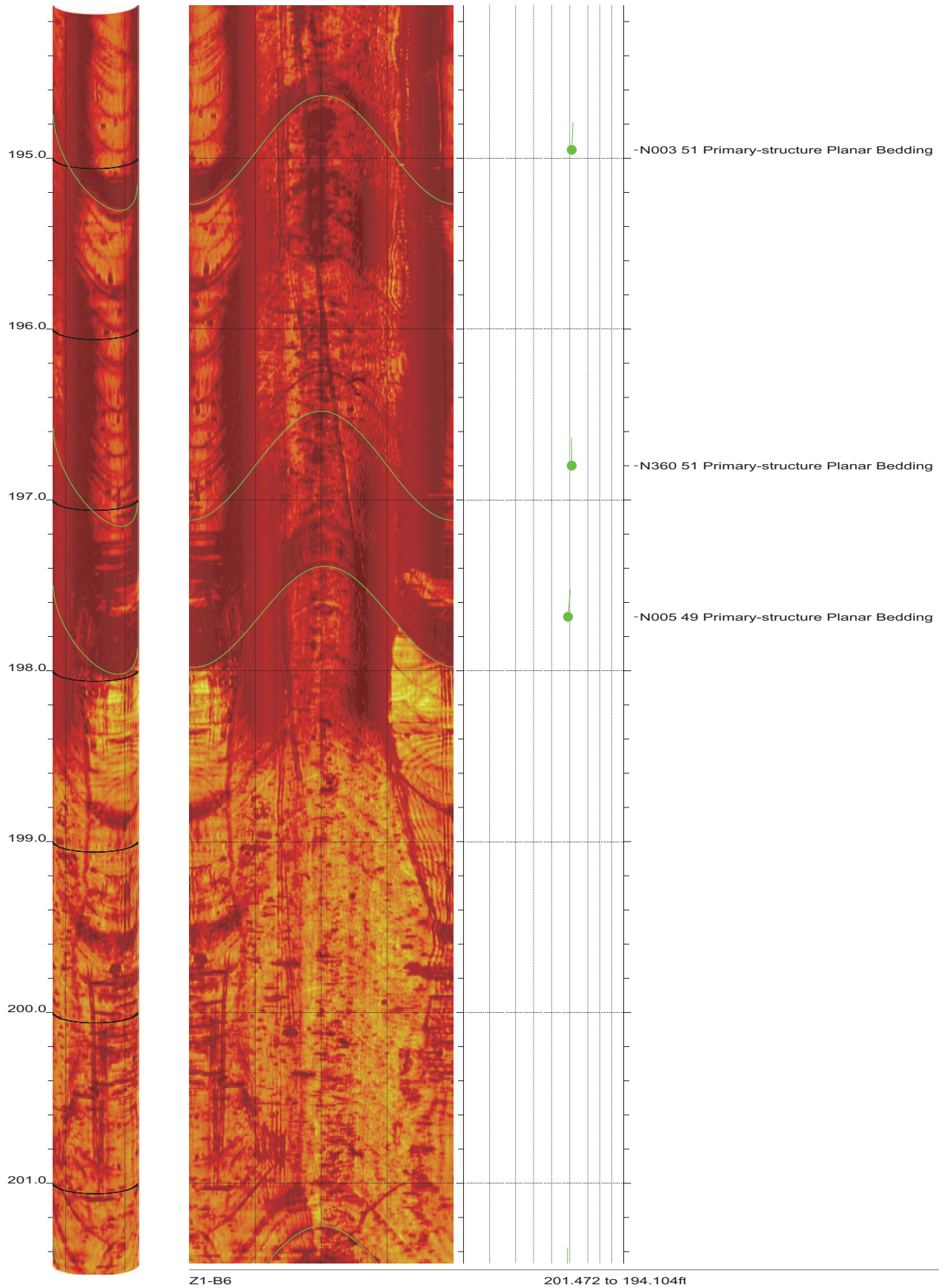
SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 16 of 46





SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 18 of 46



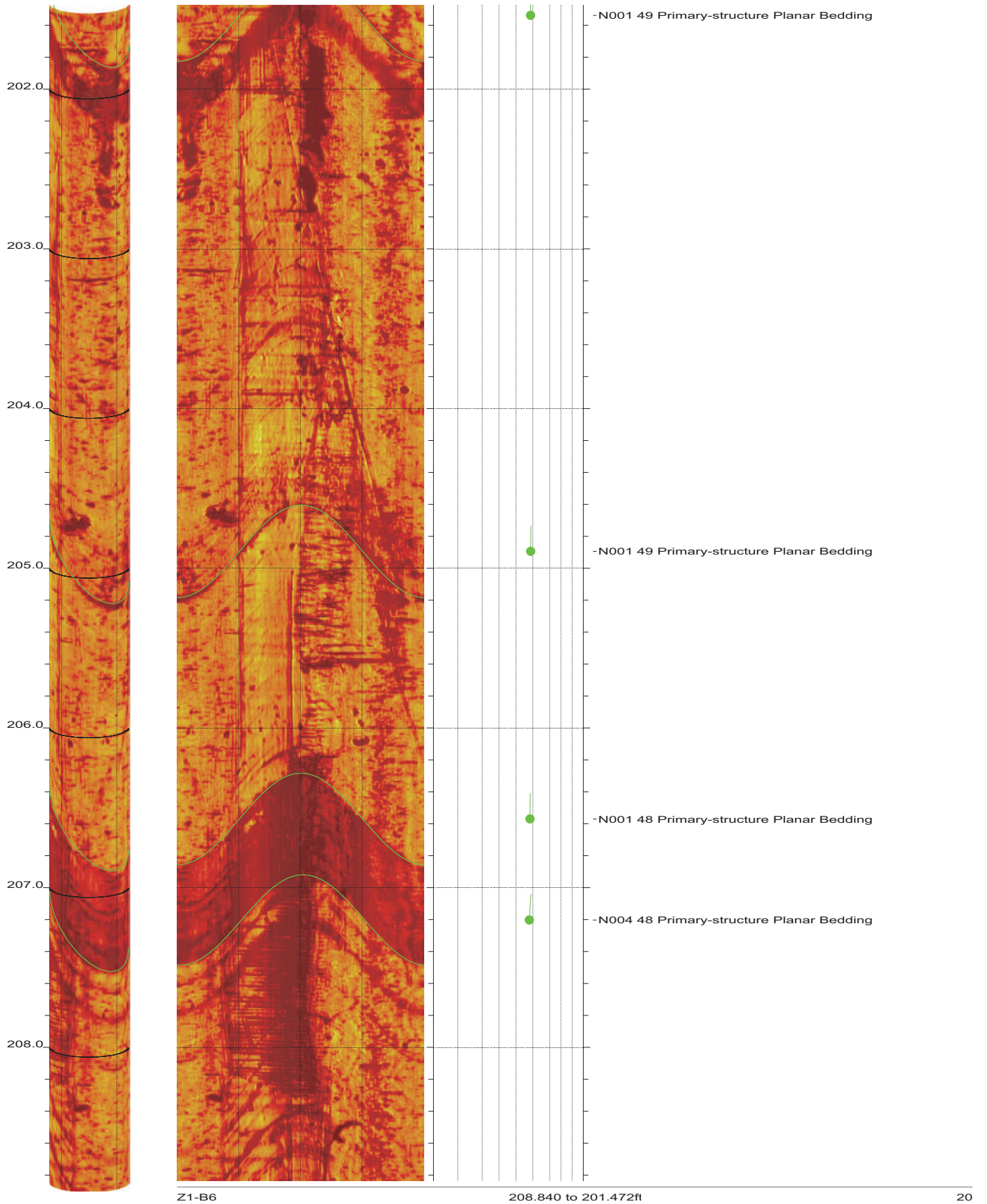


Z1-B6

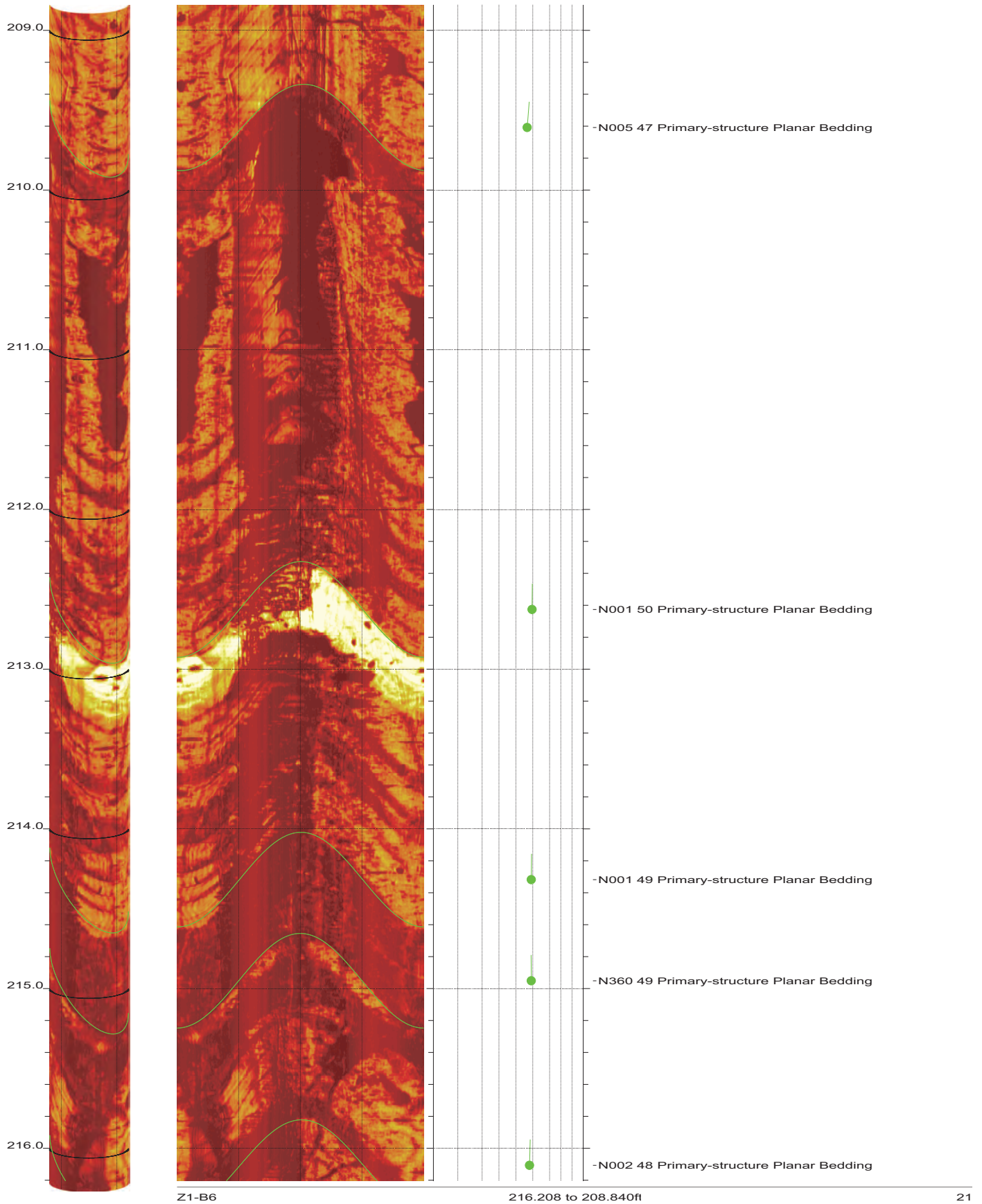
201.472 to 194.104ft

19

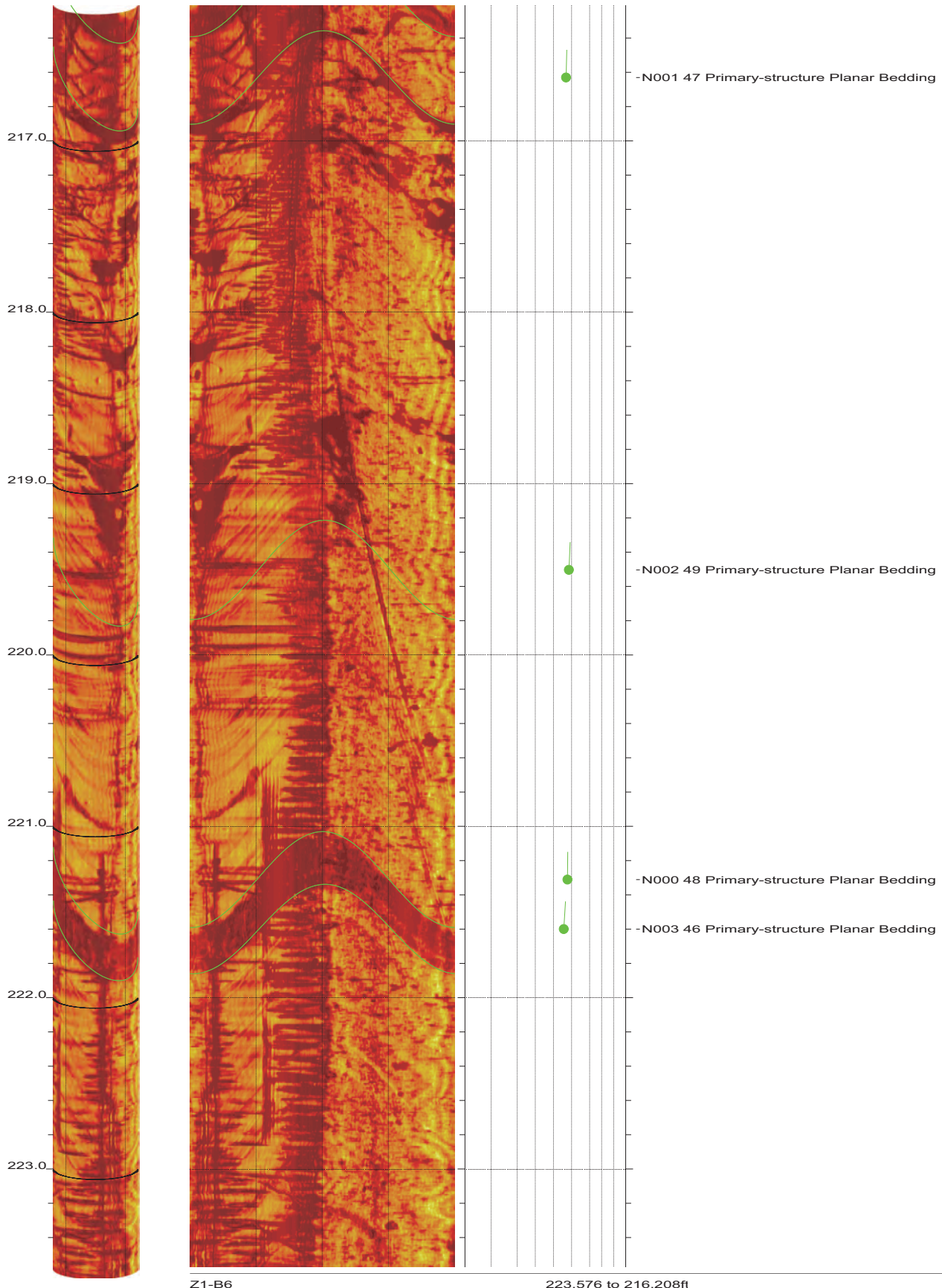
SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 19 of 46

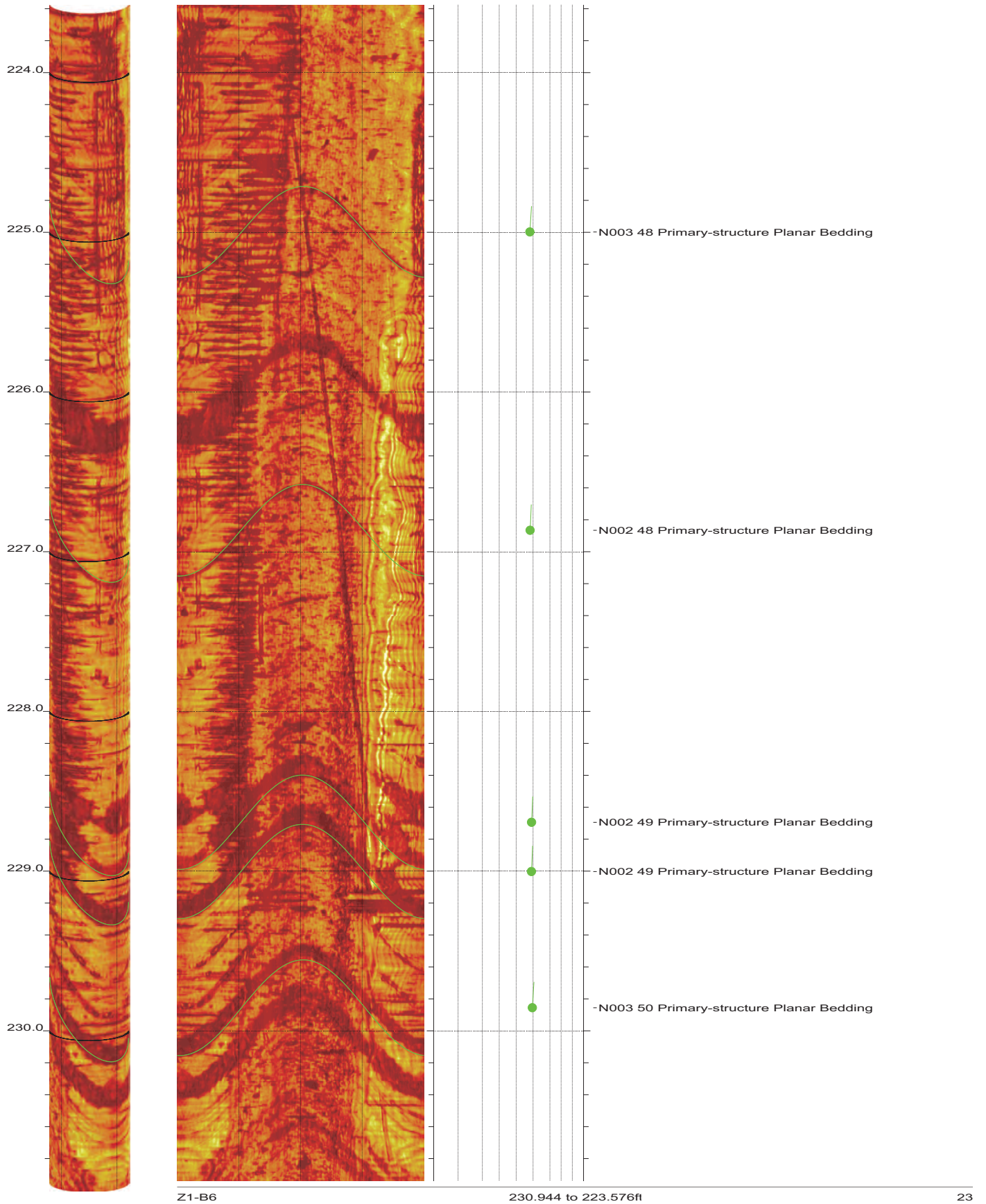


SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 20 of 46

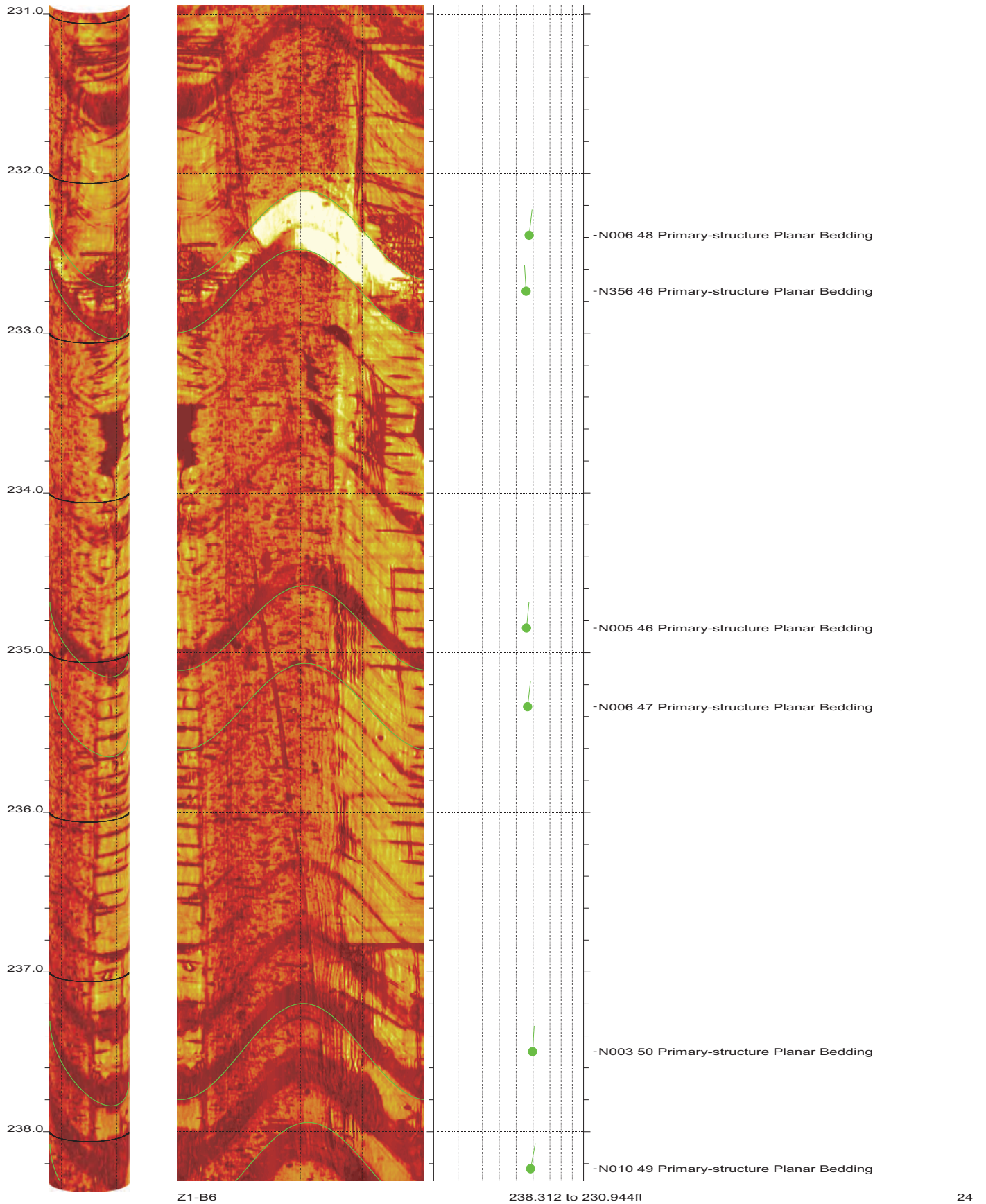


SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 21 of 46

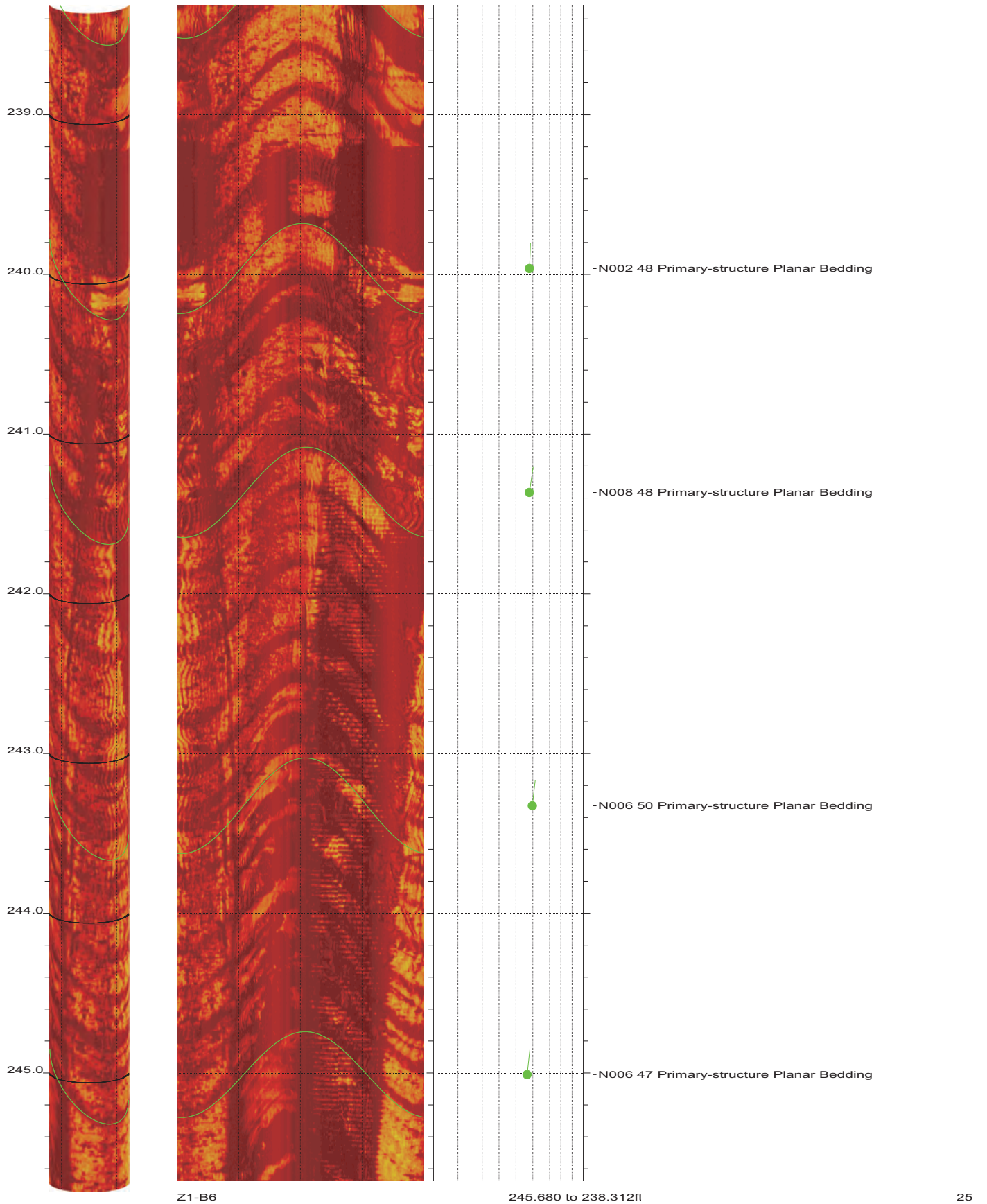




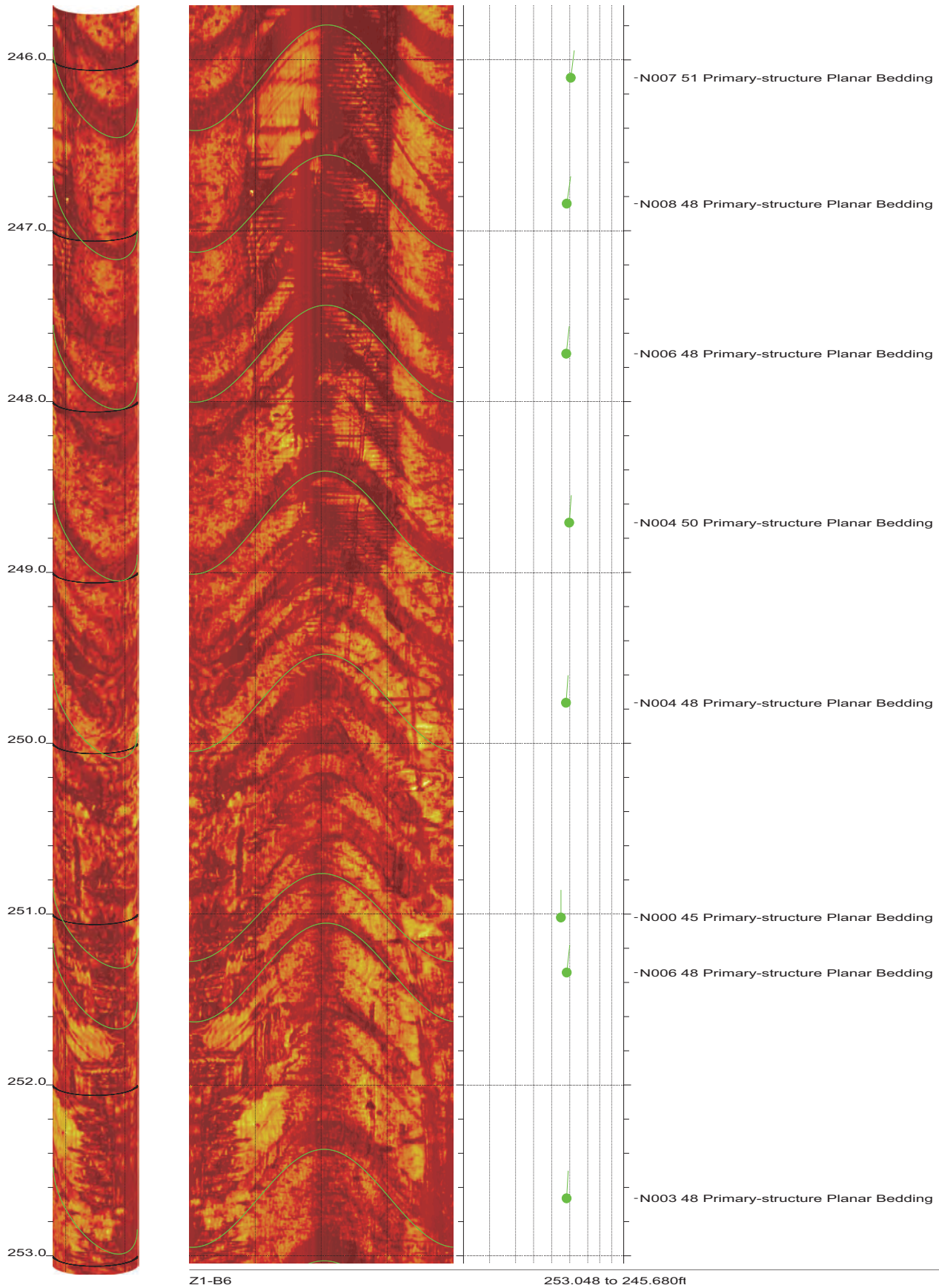
SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 23 of 46



SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 24 of 46



SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 25 of 46



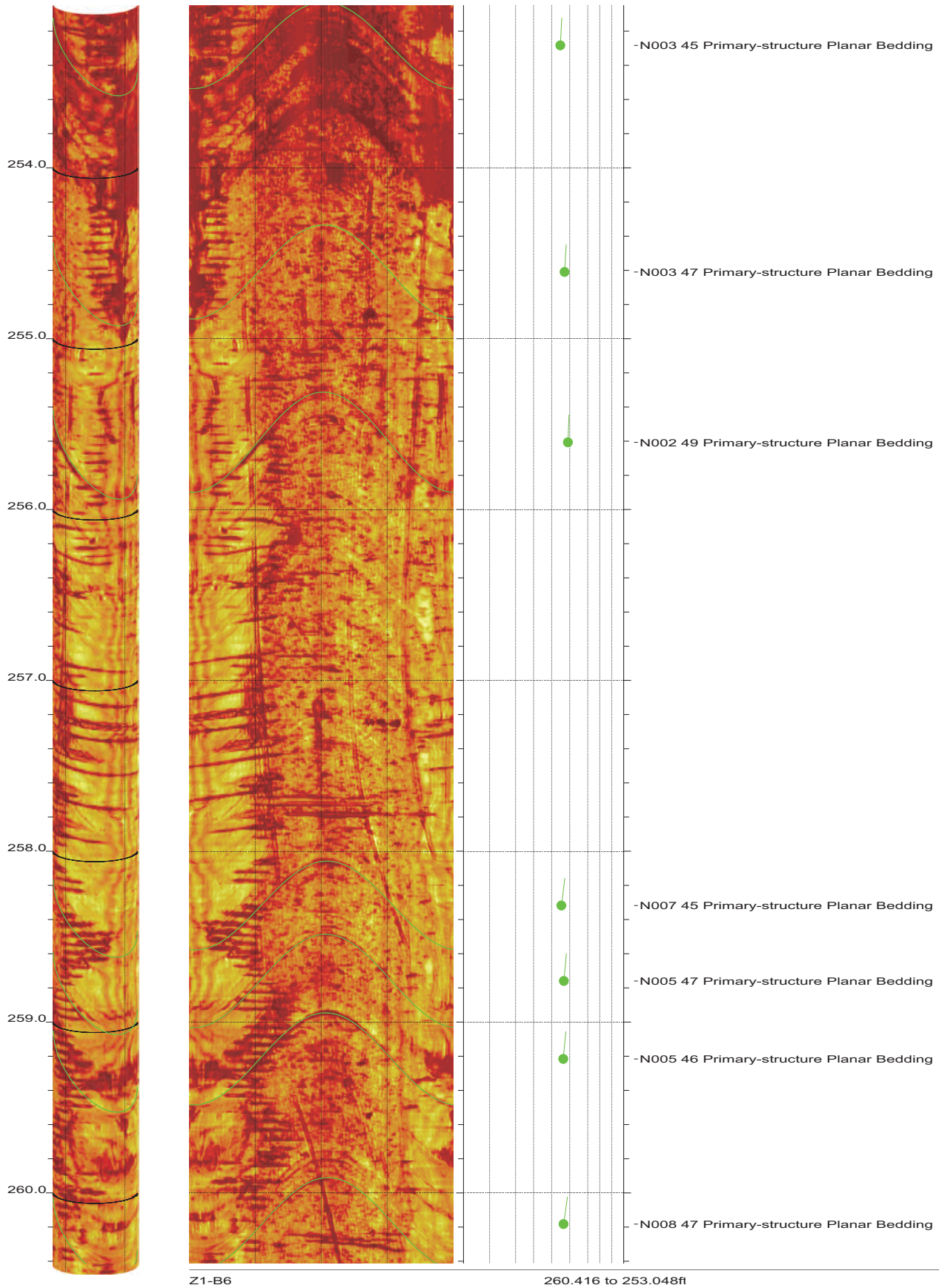
Z1-B6

253.048 to 245.680ft

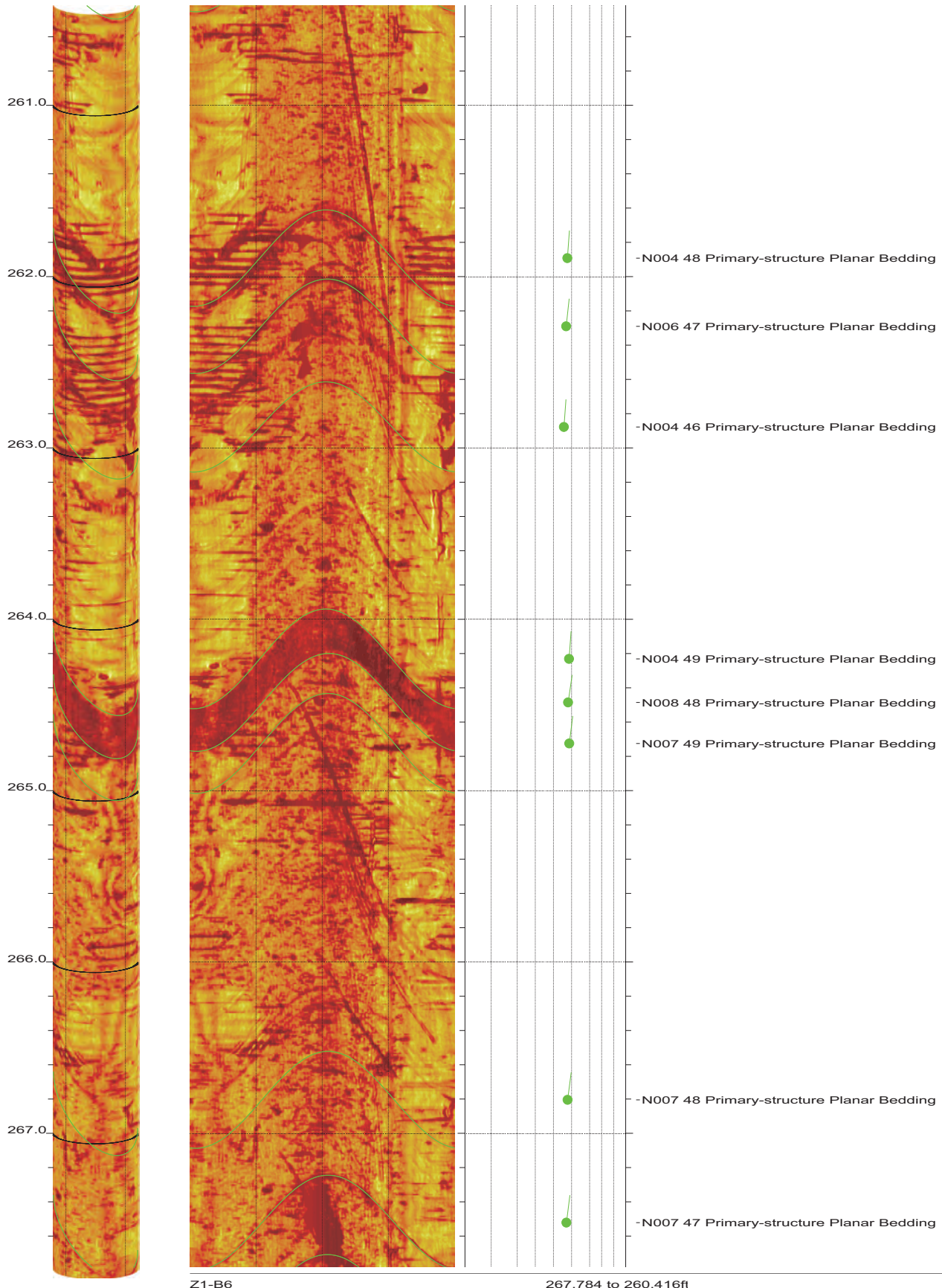
26

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 26 of 46





SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 27 of 46

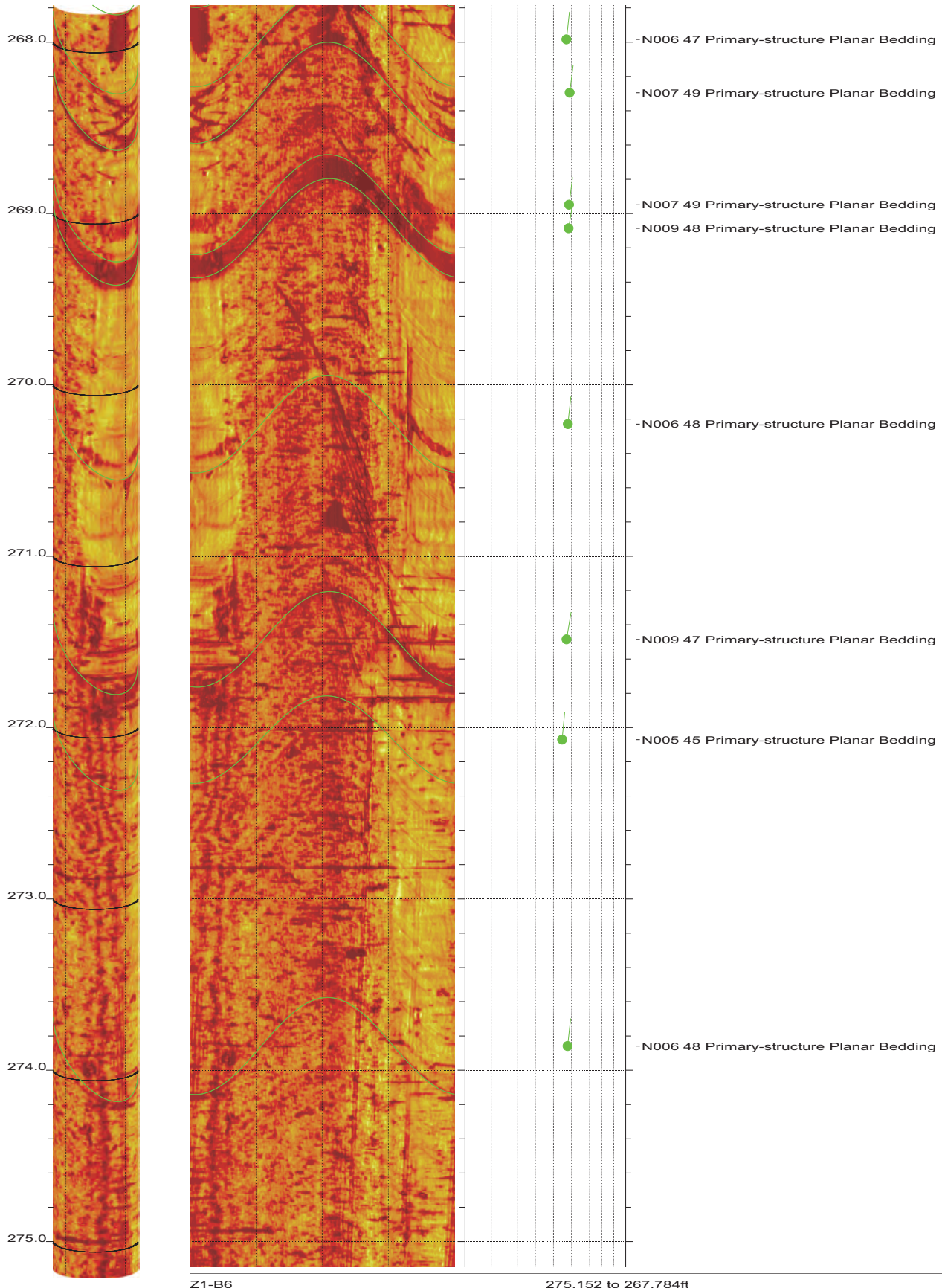


Z1-B6

267.784 to 260.416ft

28

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 28 of 46

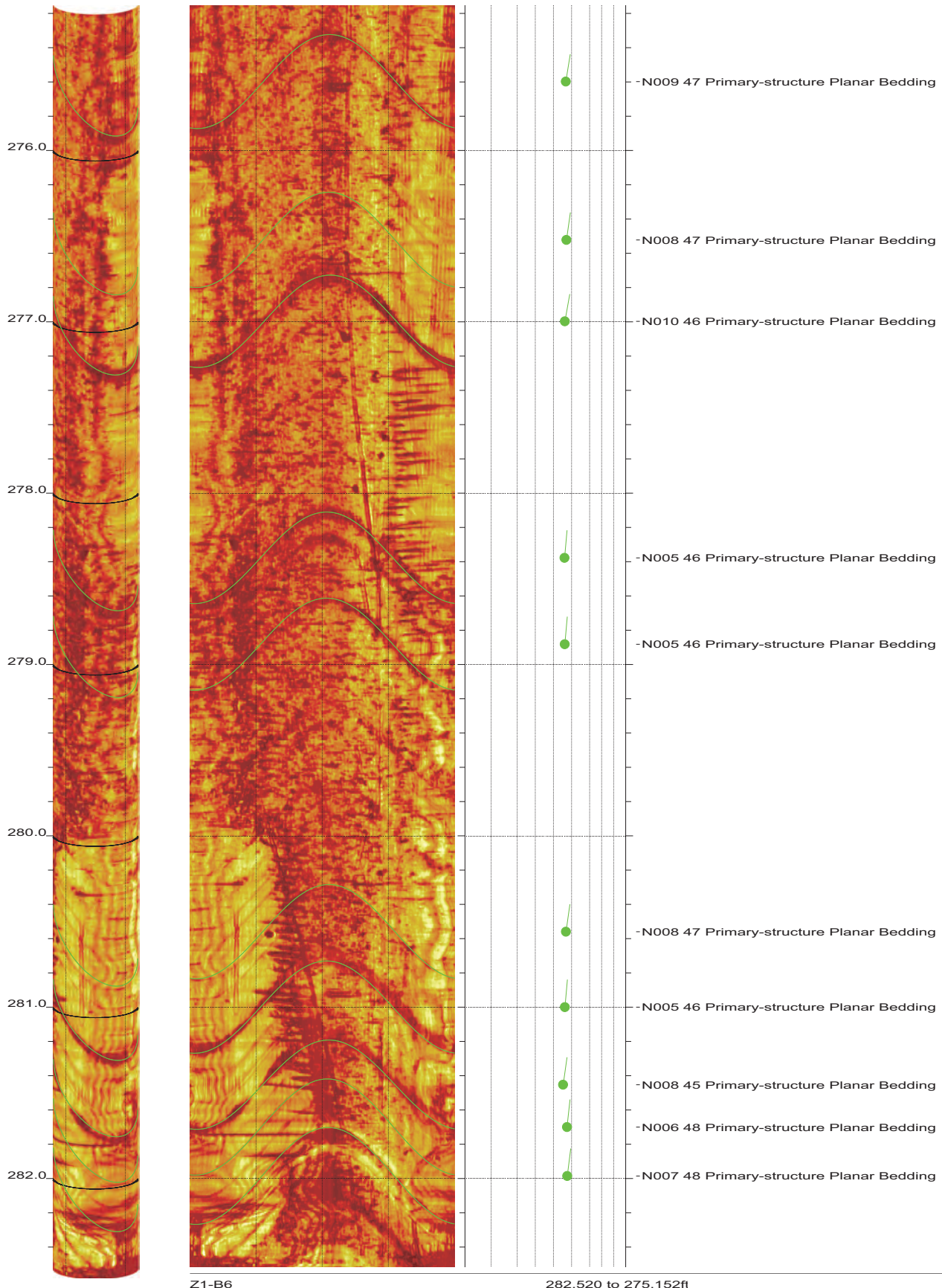


Z1-B6

275.152 to 267.784ft

29

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 29 of 46

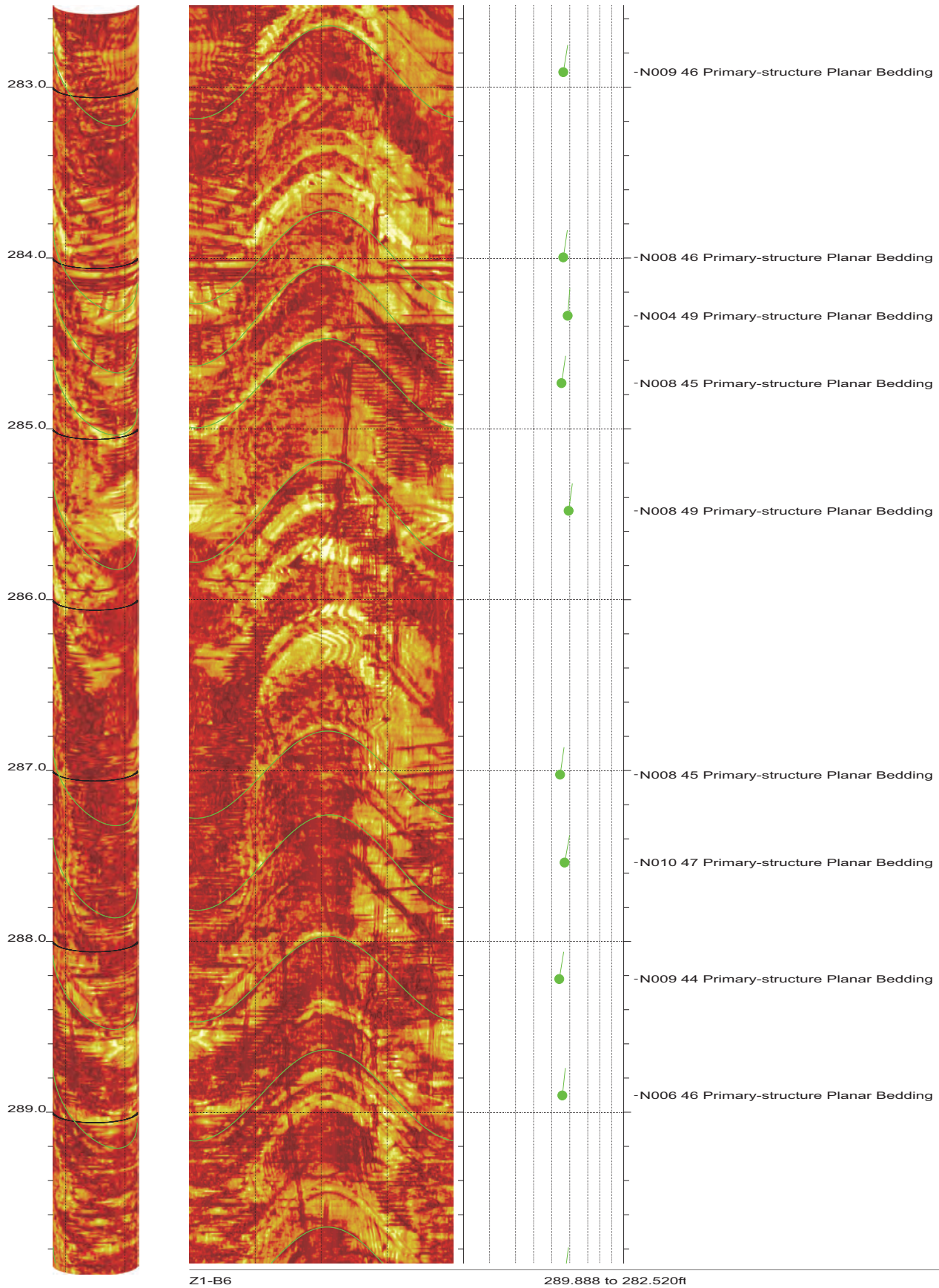


Z1-B6

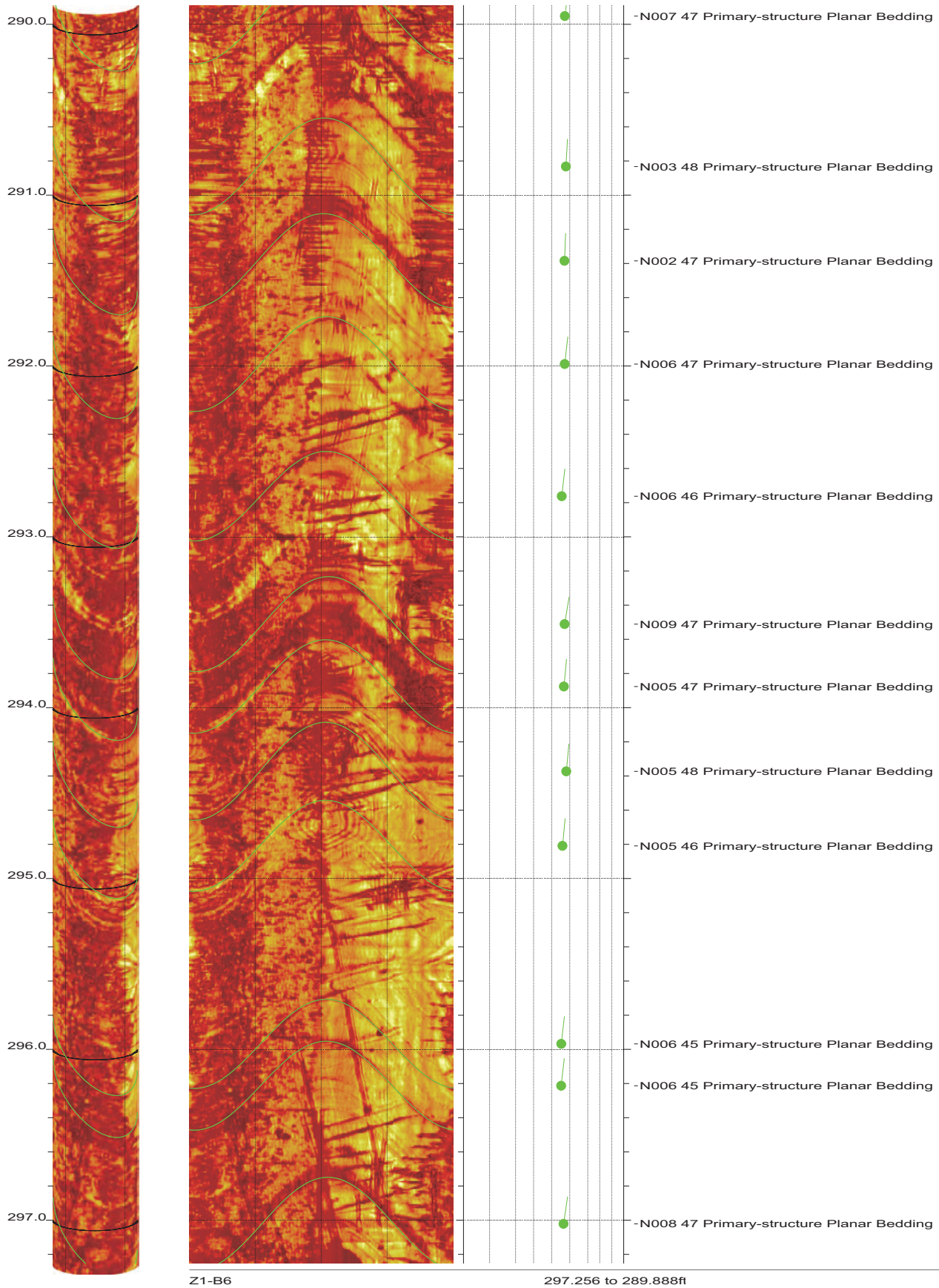
282.520 to 275.152ft

30

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 30 of 46



SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 31 of 46

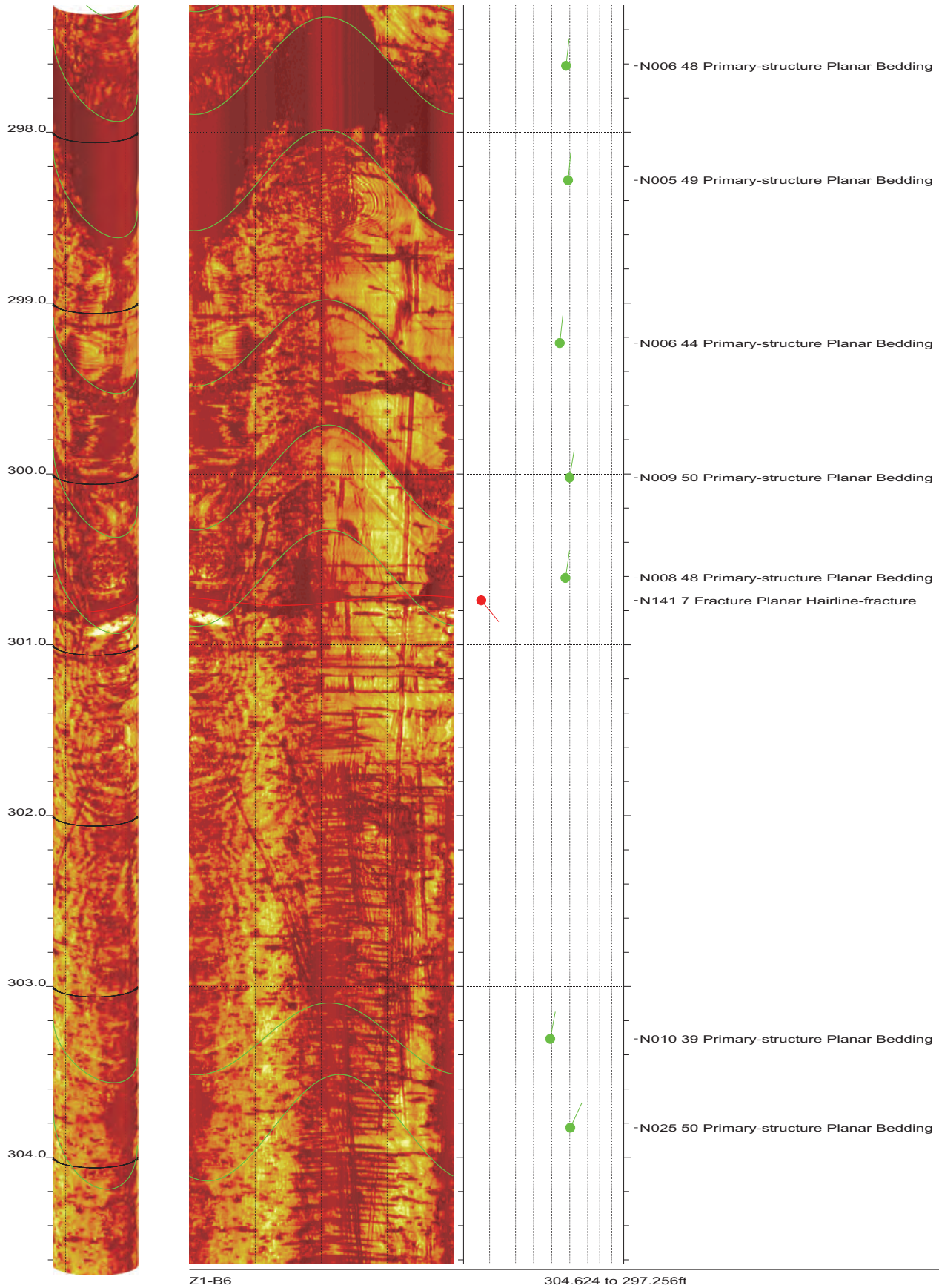


Z1-B6

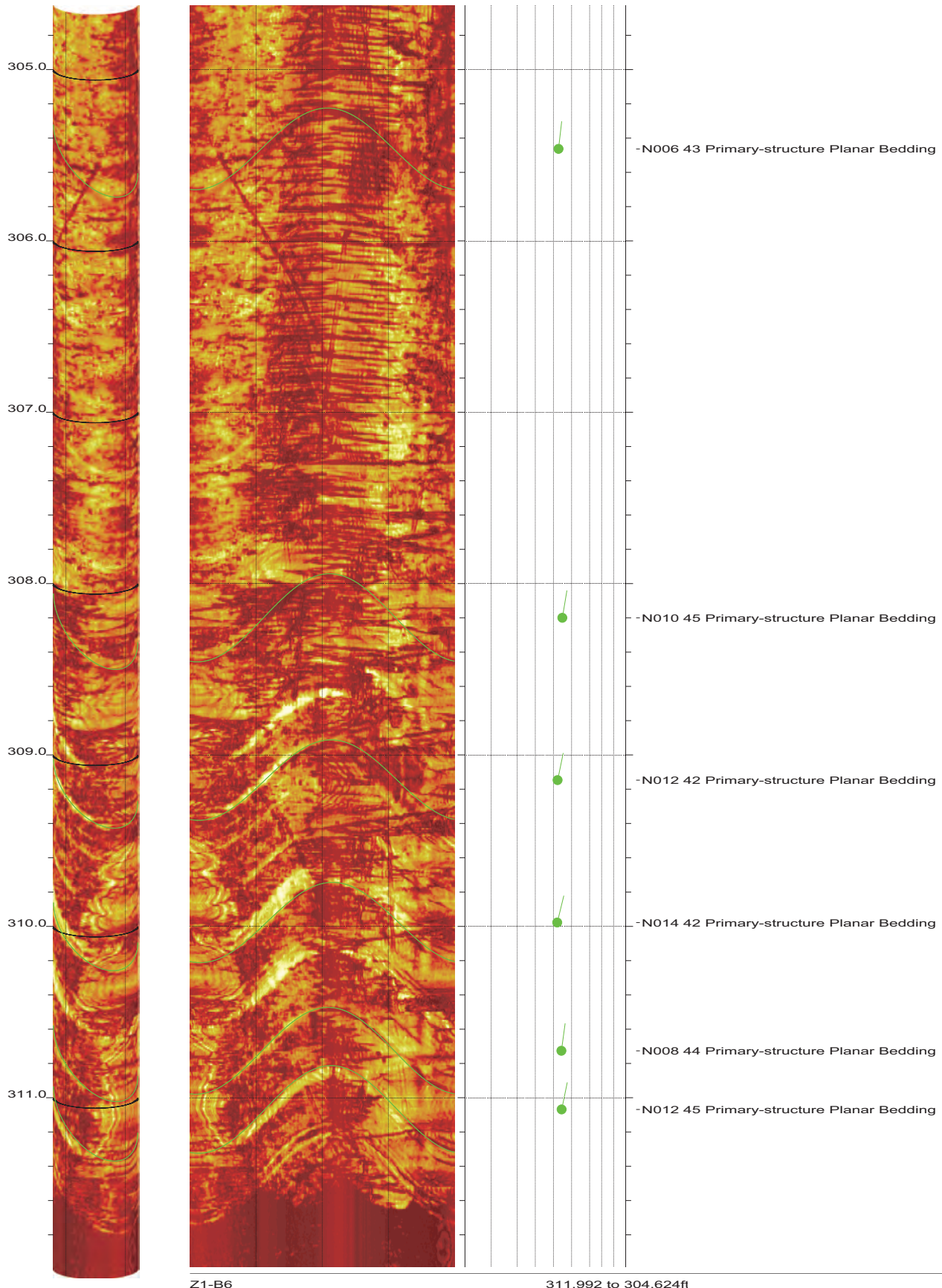
297.256 to 289.888ft

32

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 32 of 46



SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 33 of 46



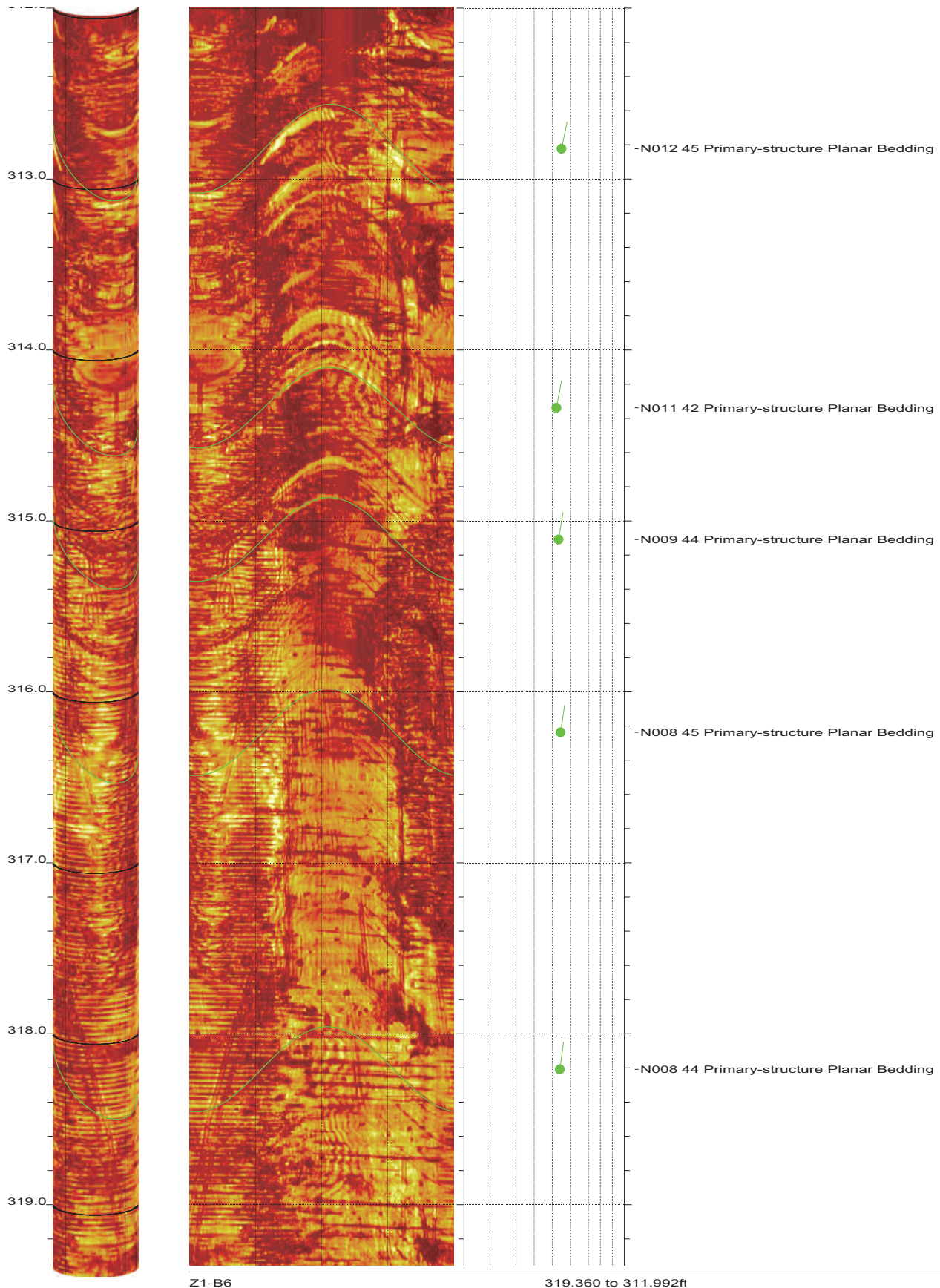
Z1-B6

311.992 to 304.624ft

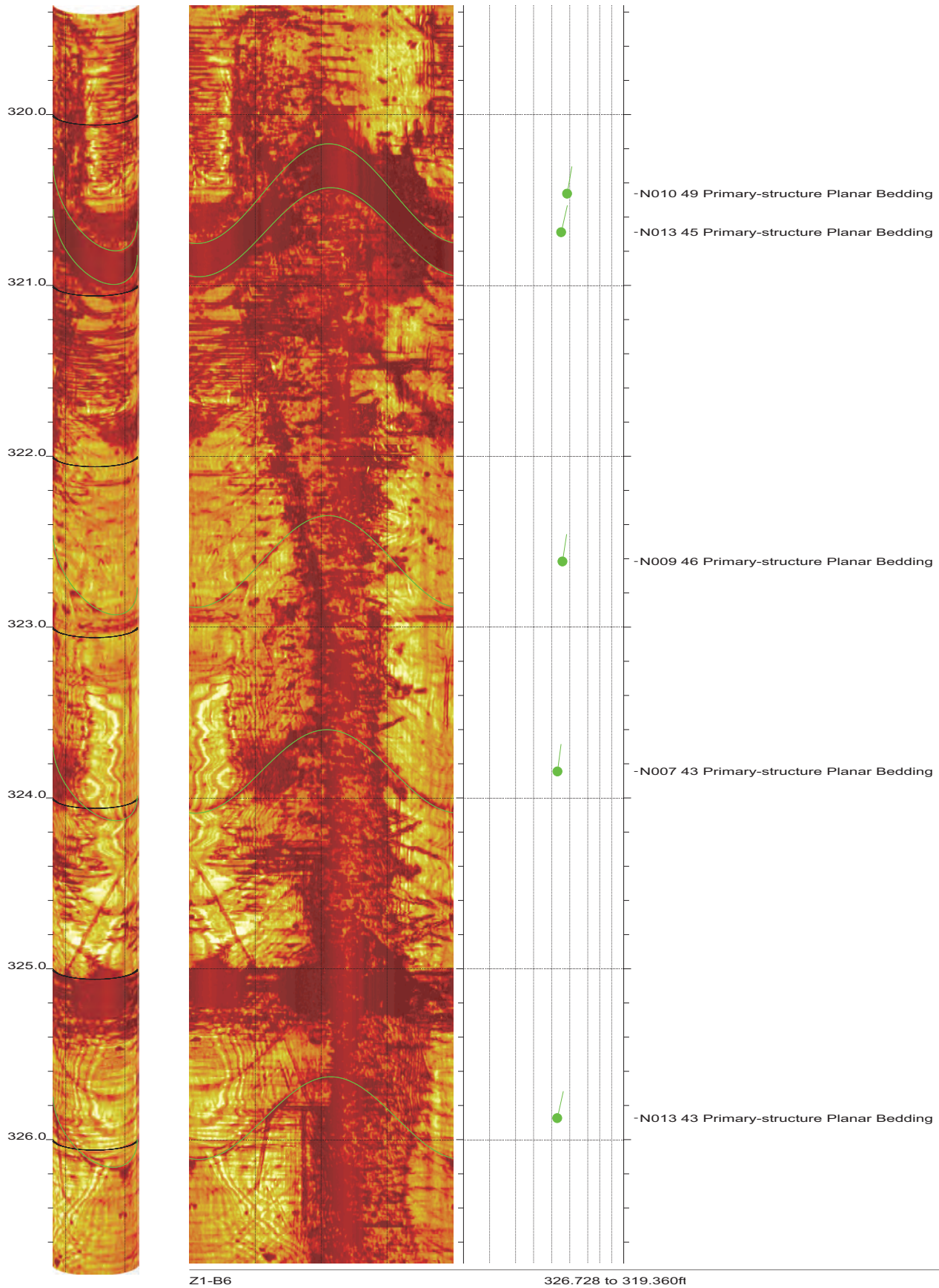
34

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 34 of 46

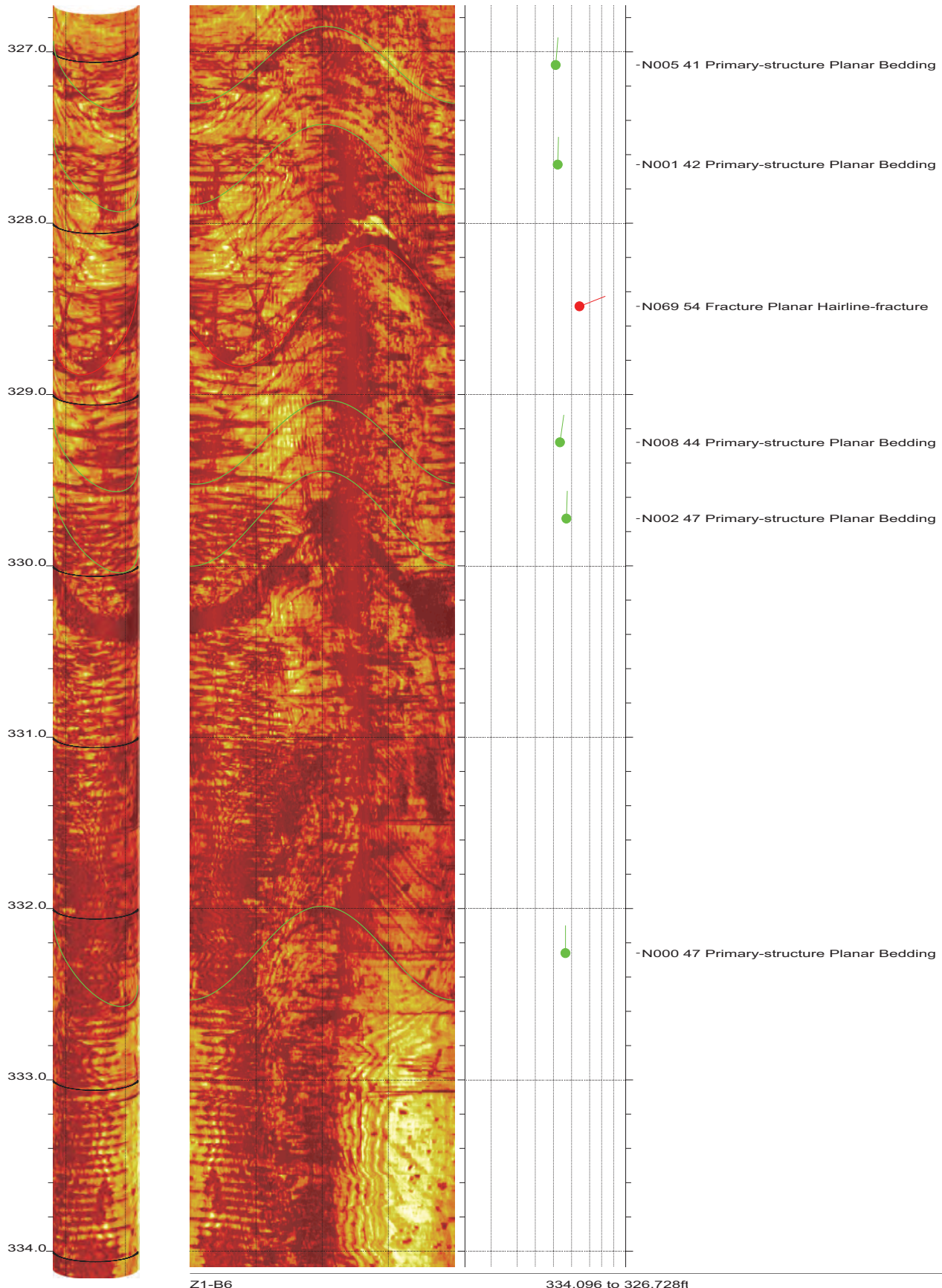




SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 35 of 46



SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 36 of 46

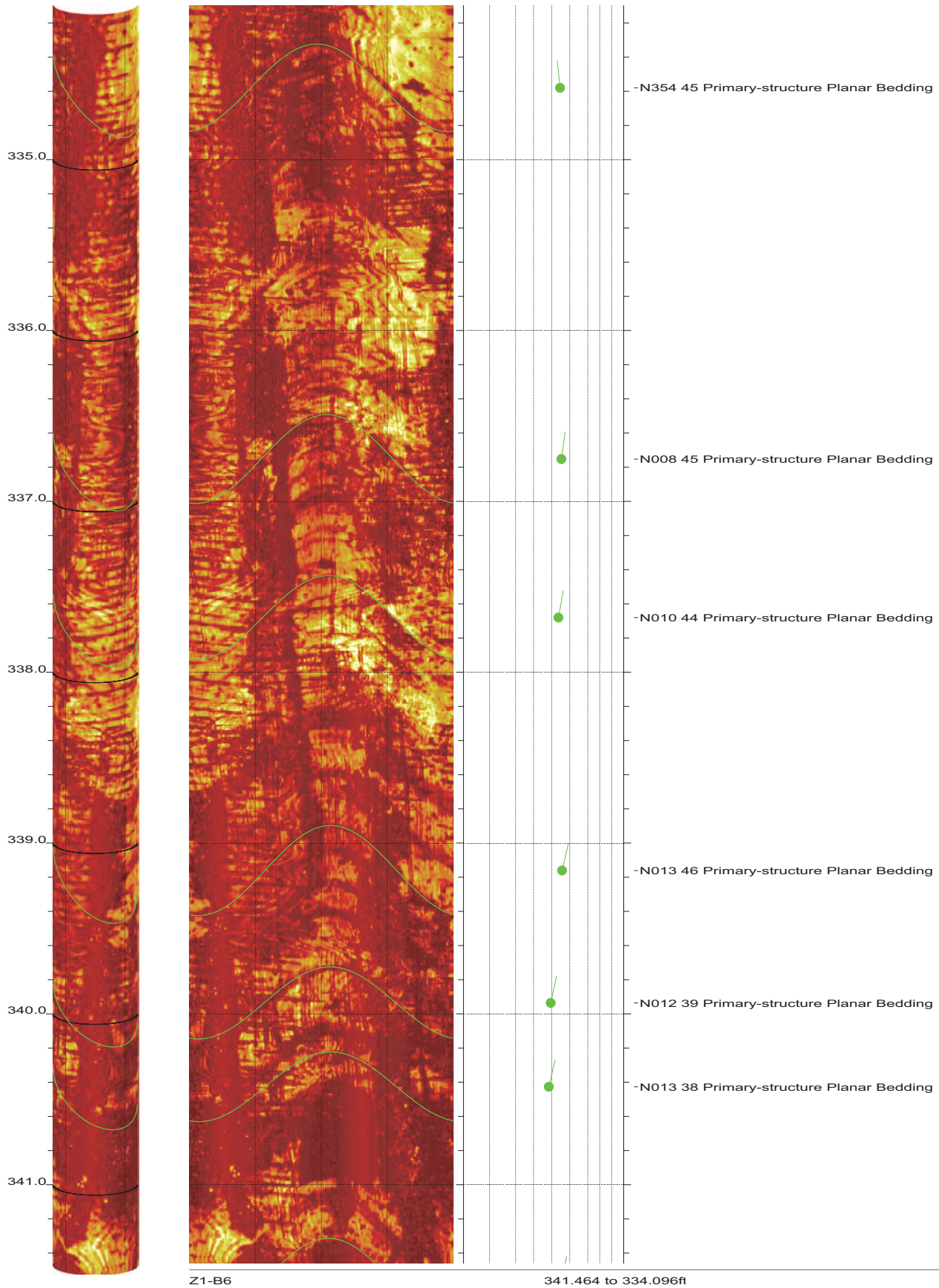


Z1-B6

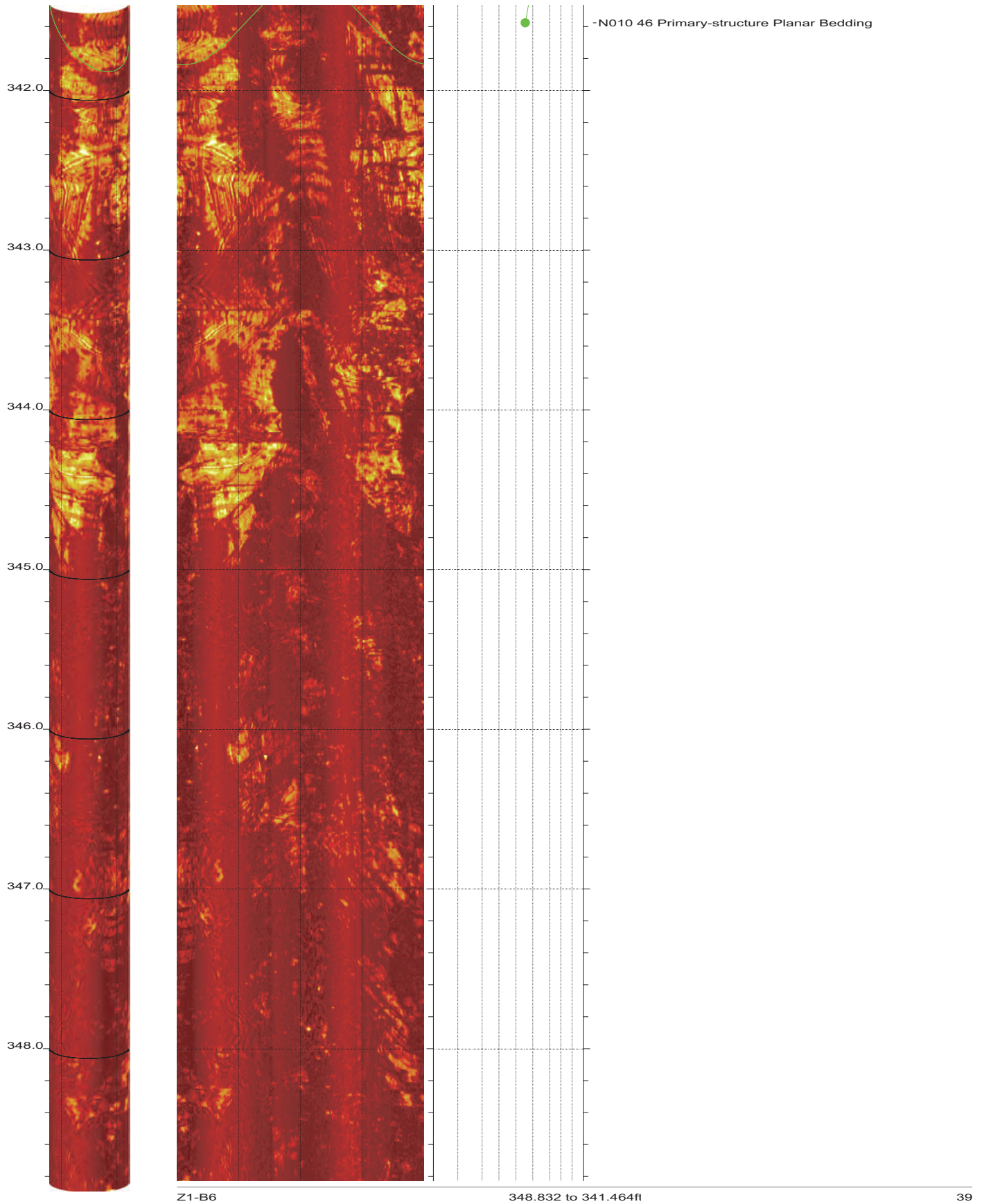
334.096 to 326.728ft

37

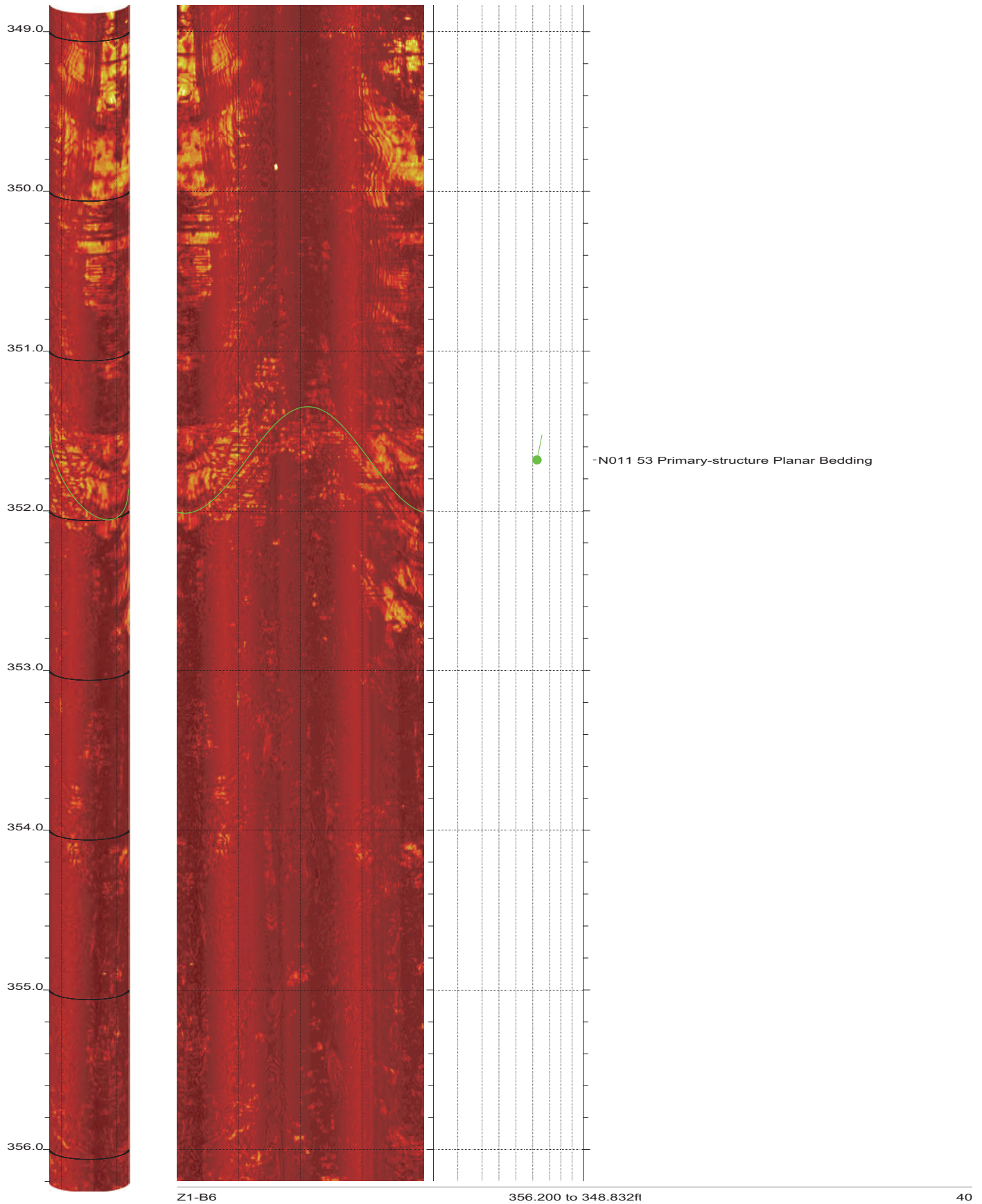
SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 37 of 46



SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 38 of 46



SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 39 of 46

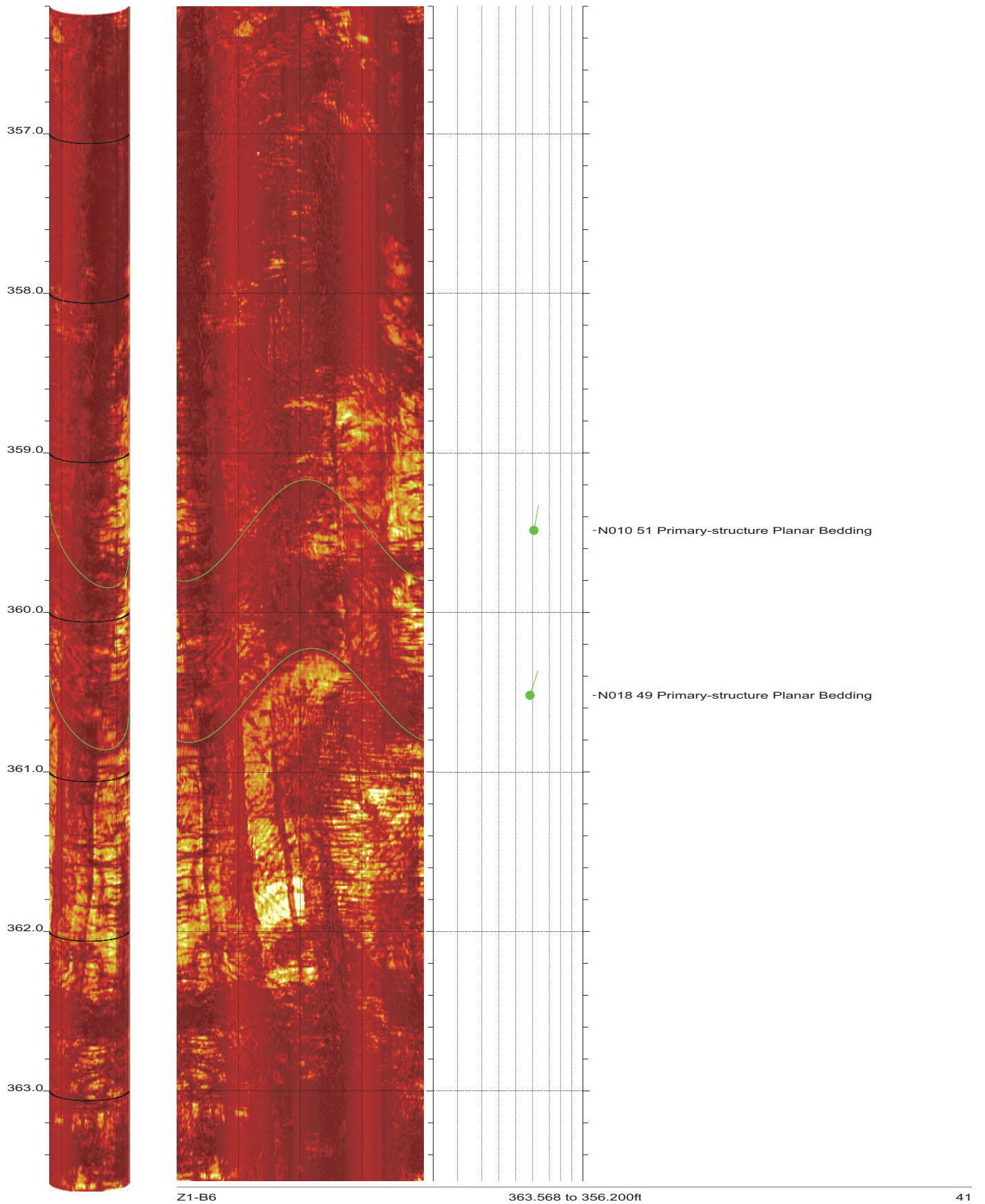


Z1-B6

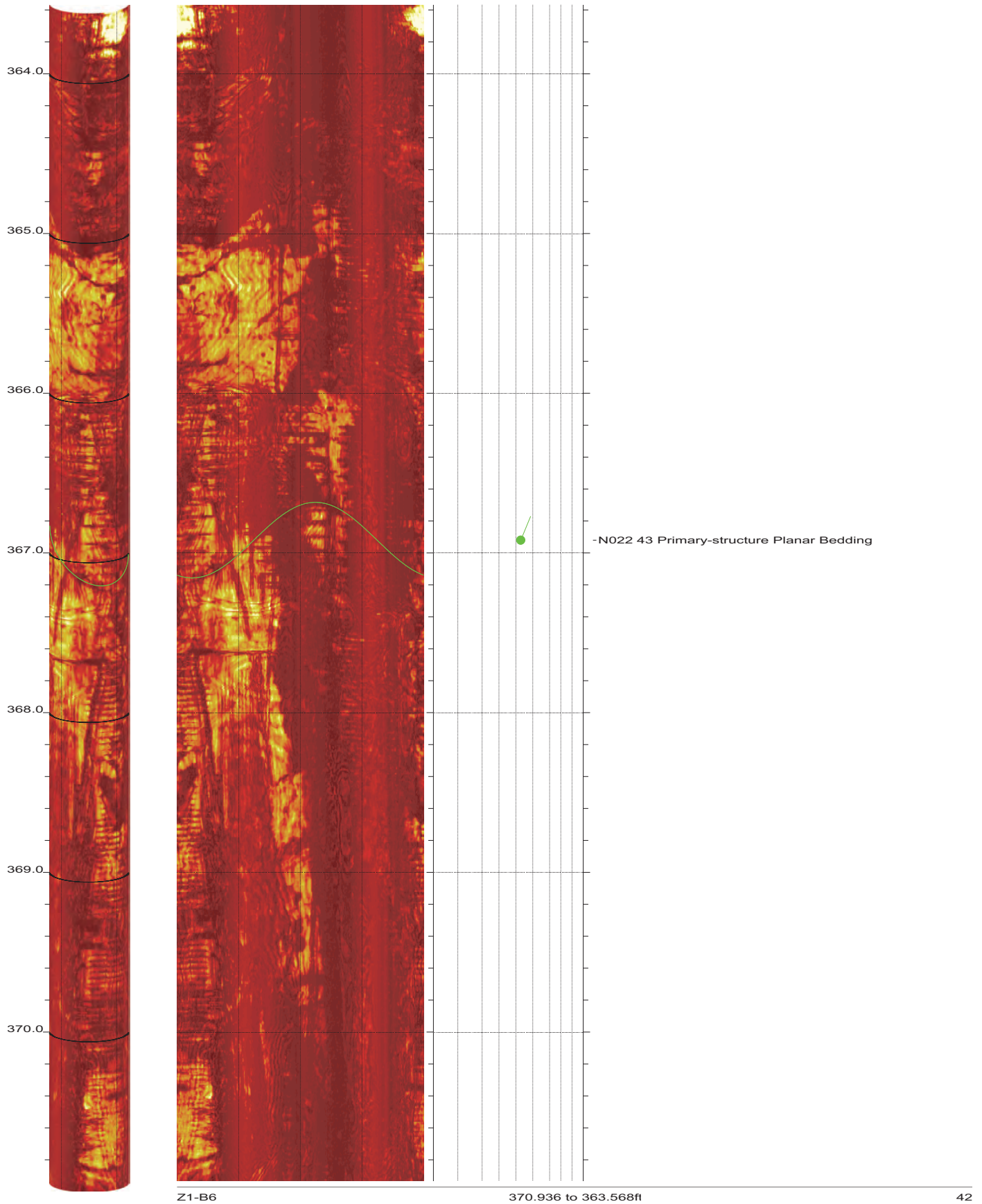
356.200 to 348.832ft

40

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 40 of 46



SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 41 of 46



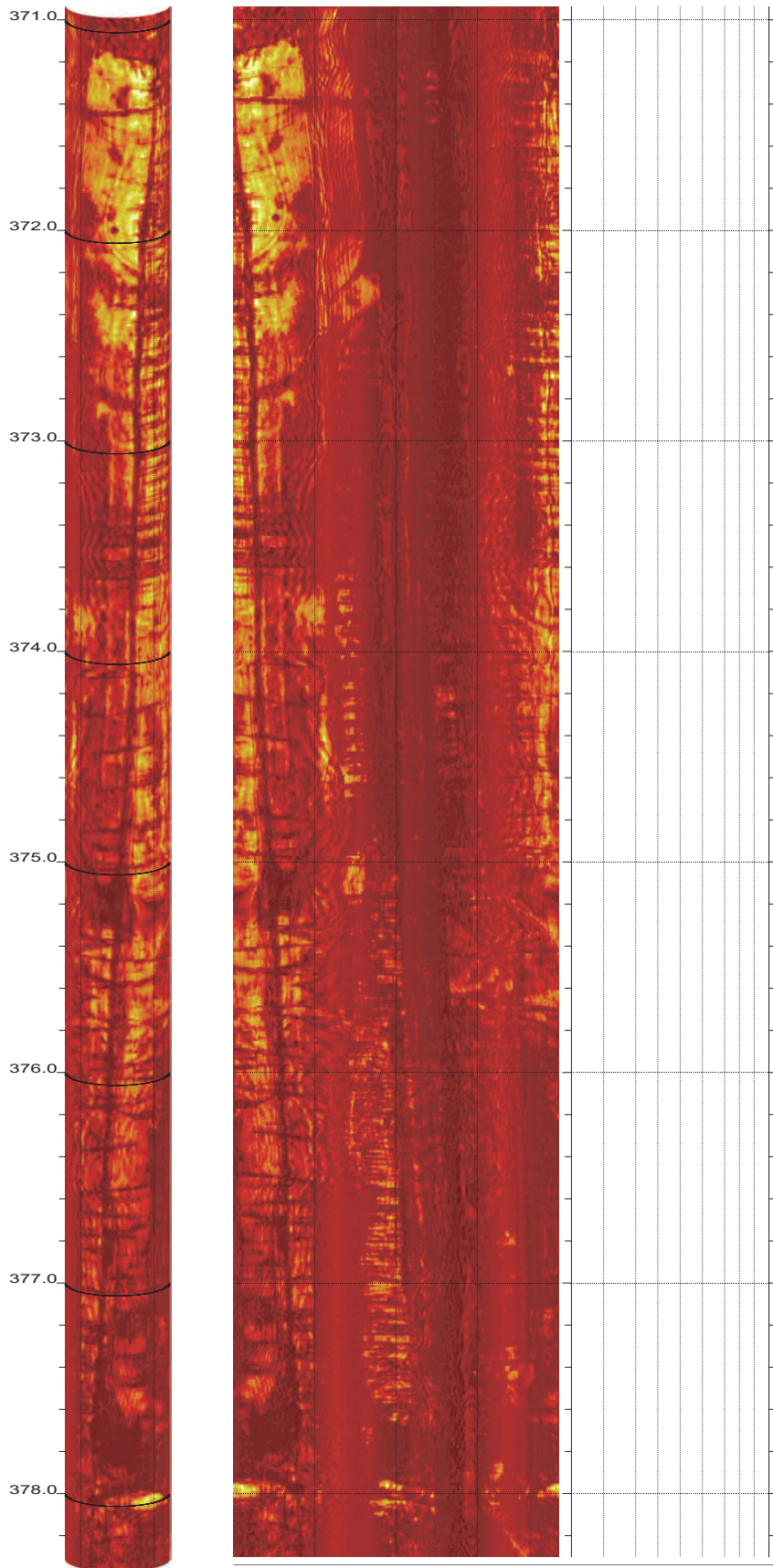
Z1-B6

370.936 to 363.568ft

42

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 42 of 46



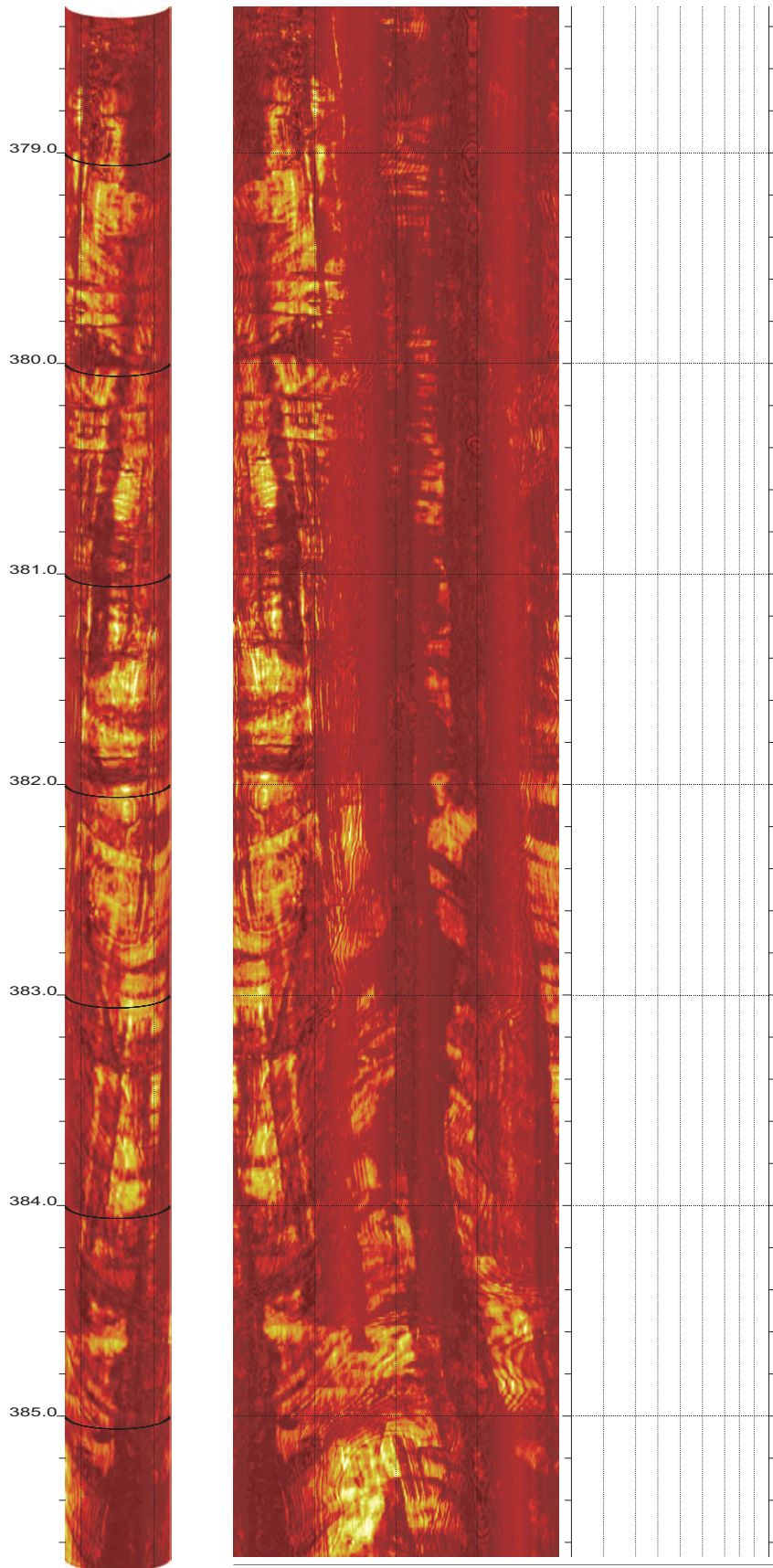


Z1-B6

378.304 to 370.936ft

43

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 43 of 46

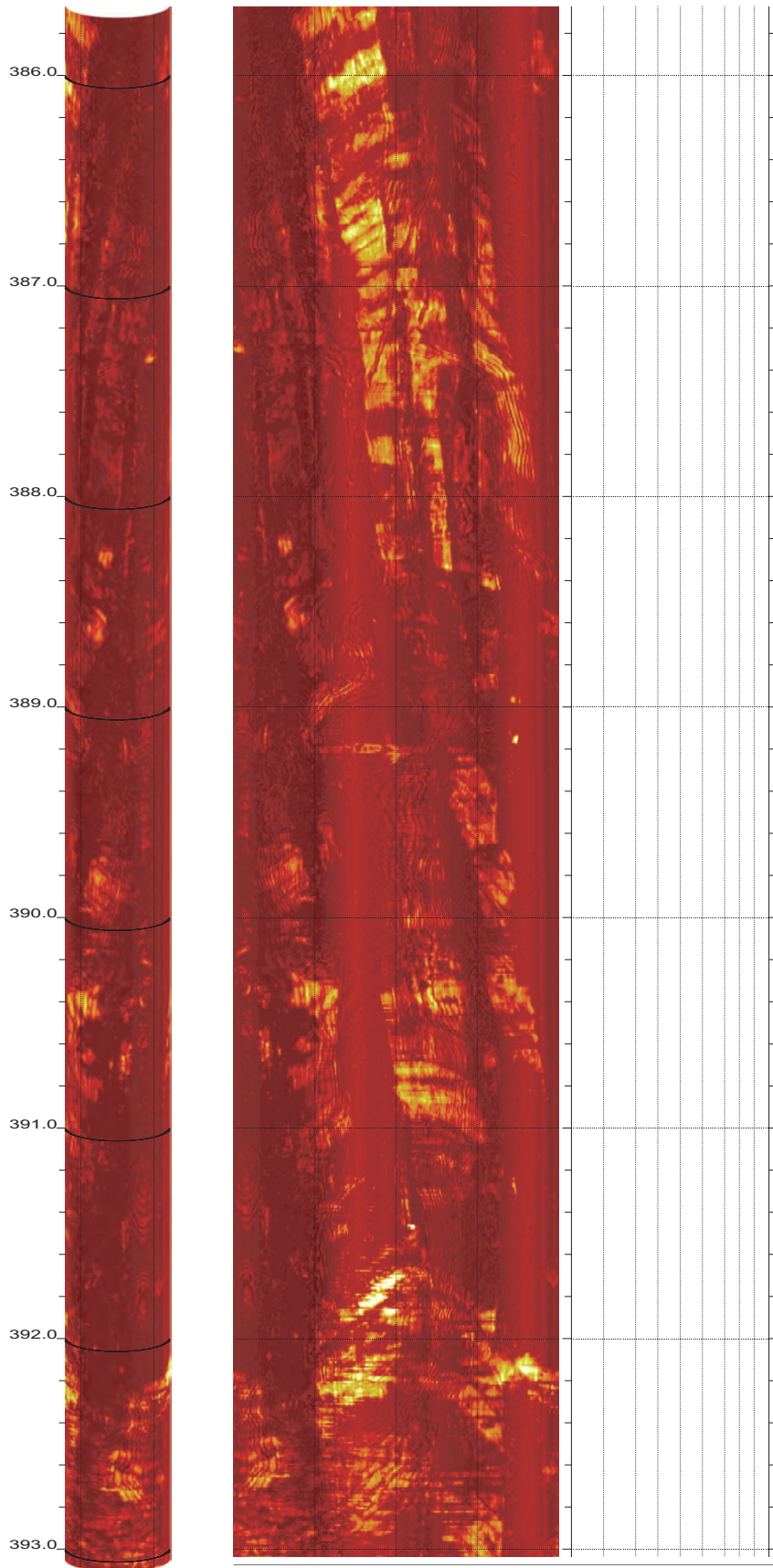


Z1-B6

385.672 to 378.304ft

44

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 44 of 46

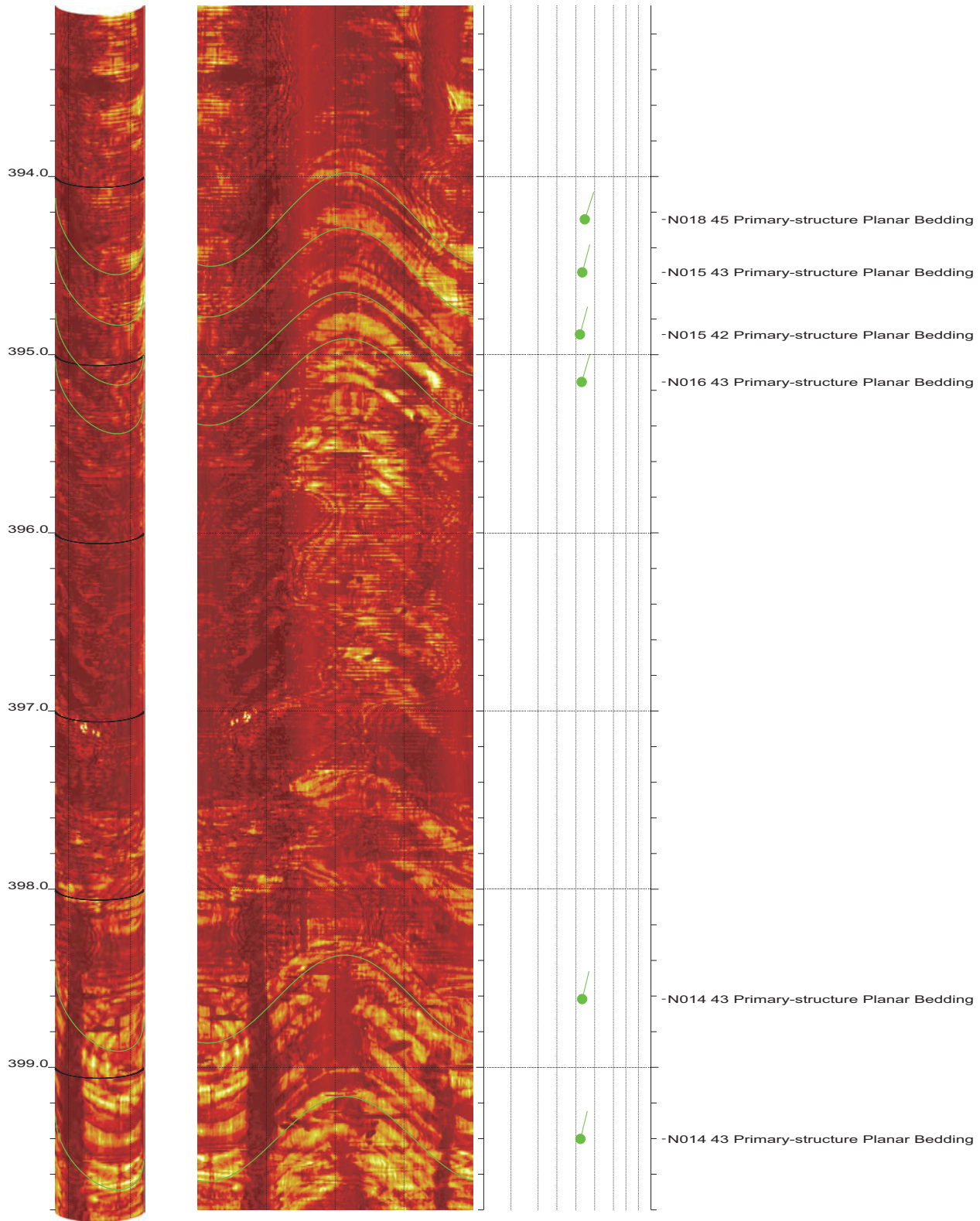


Z1-B6

393.040 to 385.672ft

45

SR-710 Boring Z1-B6 Acoustic Televiewer Dips rev 1 Sheet 45 of 46





CASCADE DRILLING

Borehole: Z1-B7

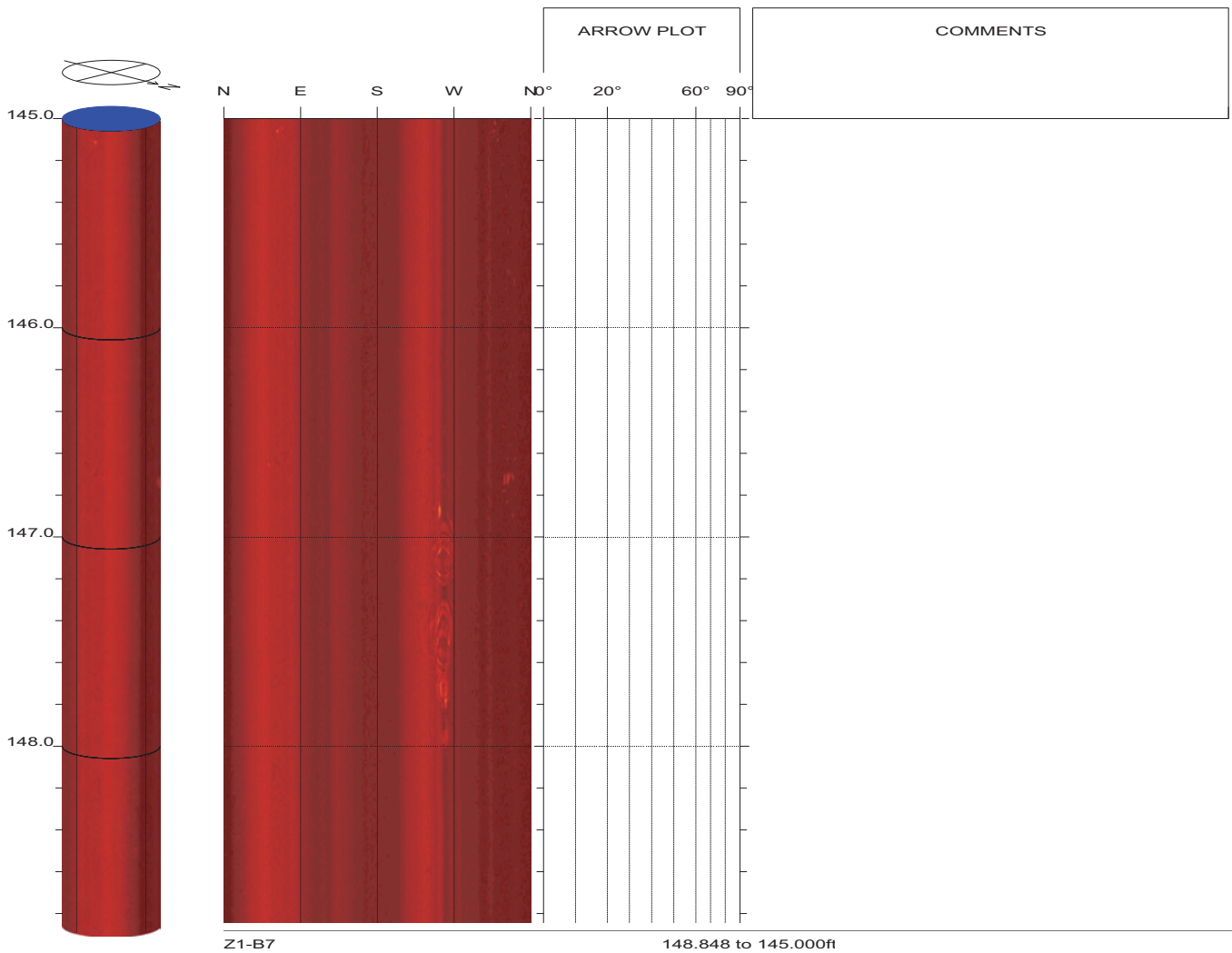
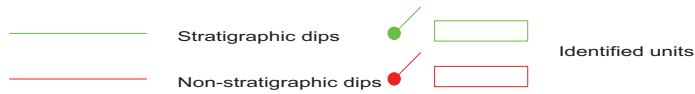
SR-710 TUNNEL INVESTIGATION

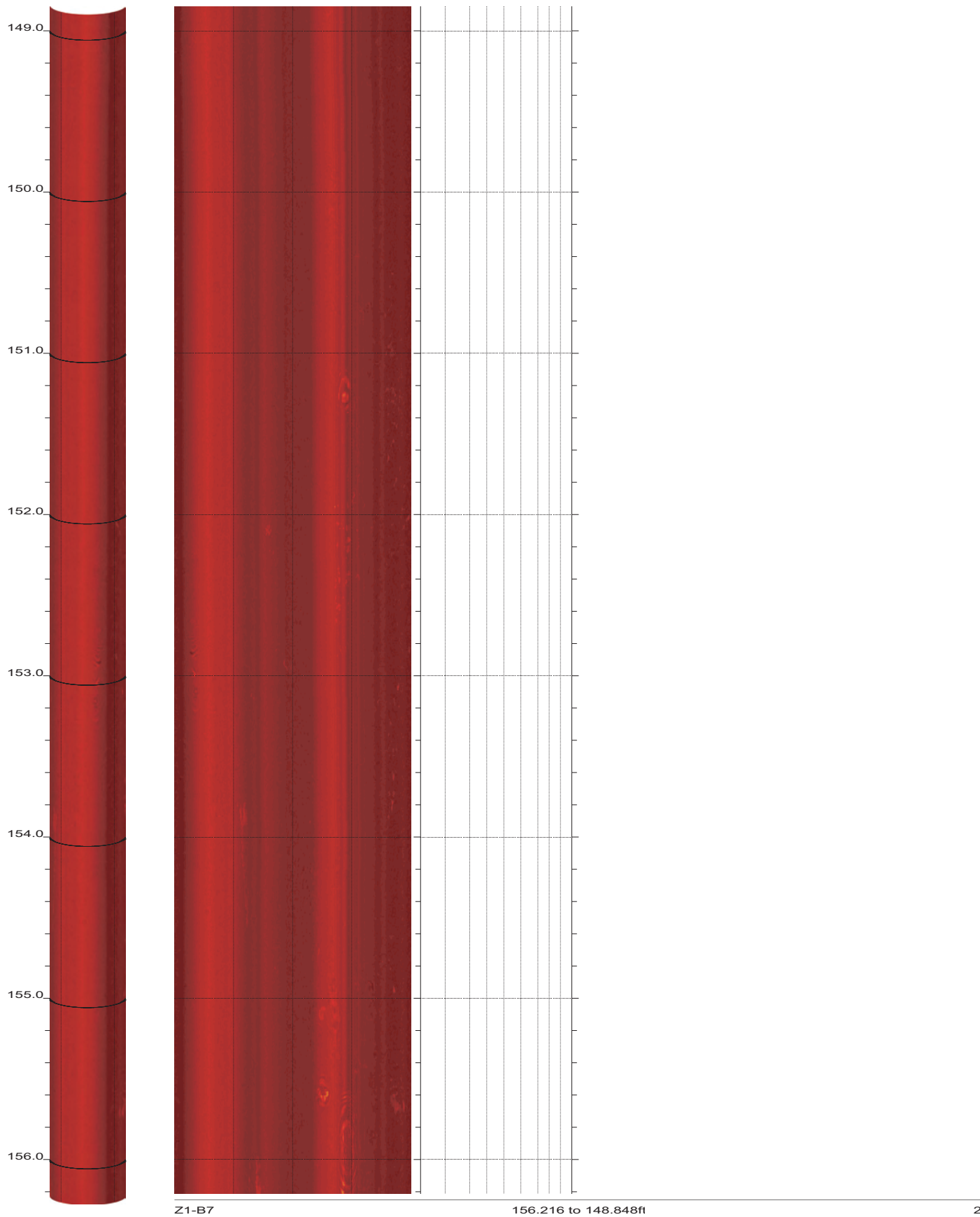
top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

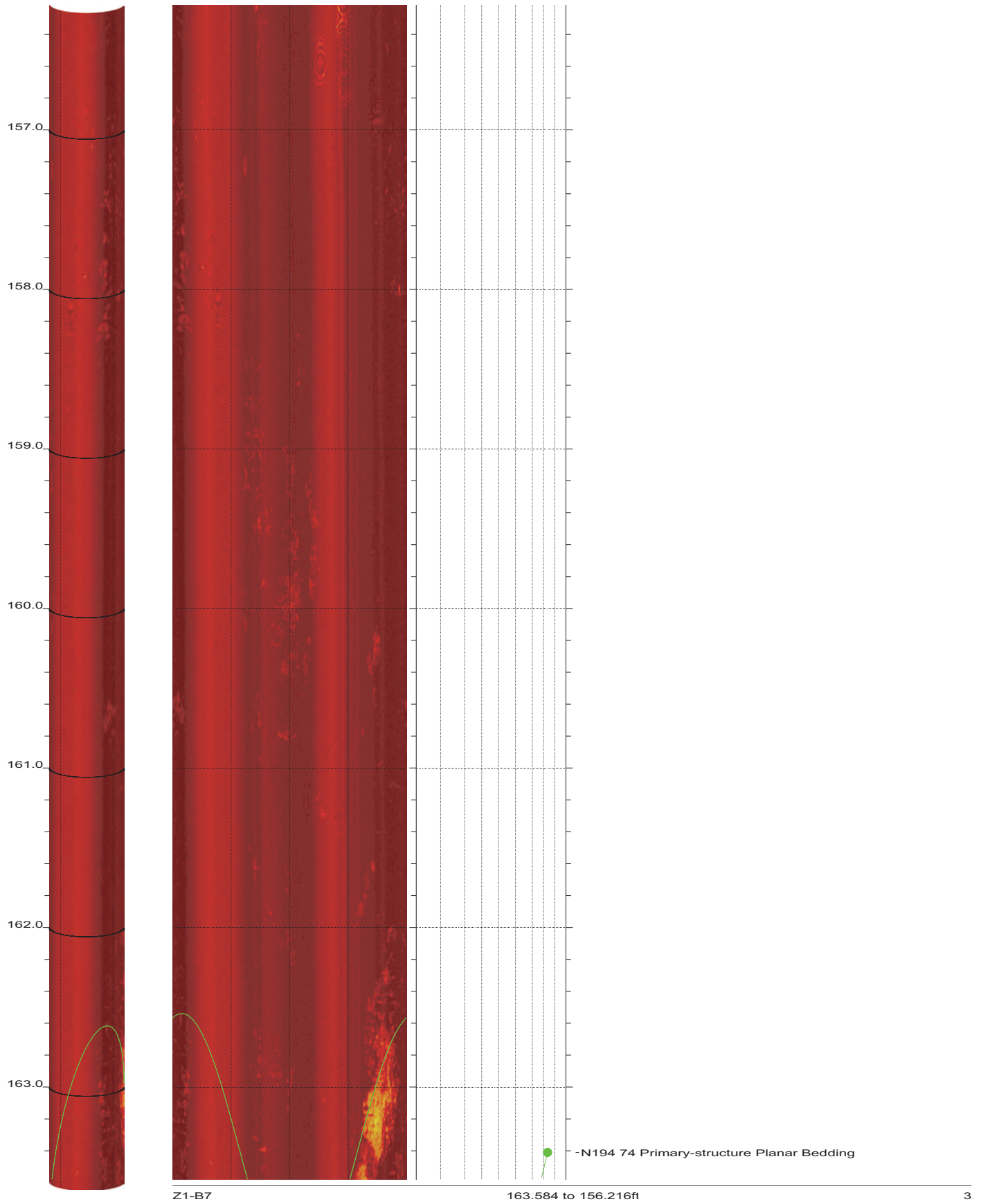
Zone from 298.800 to 145.000ft  
 Format: BHTV-NESWN

Borehole diam: 5.600inch  
 Vertical = borehole-axis  
 Image: Amplitude

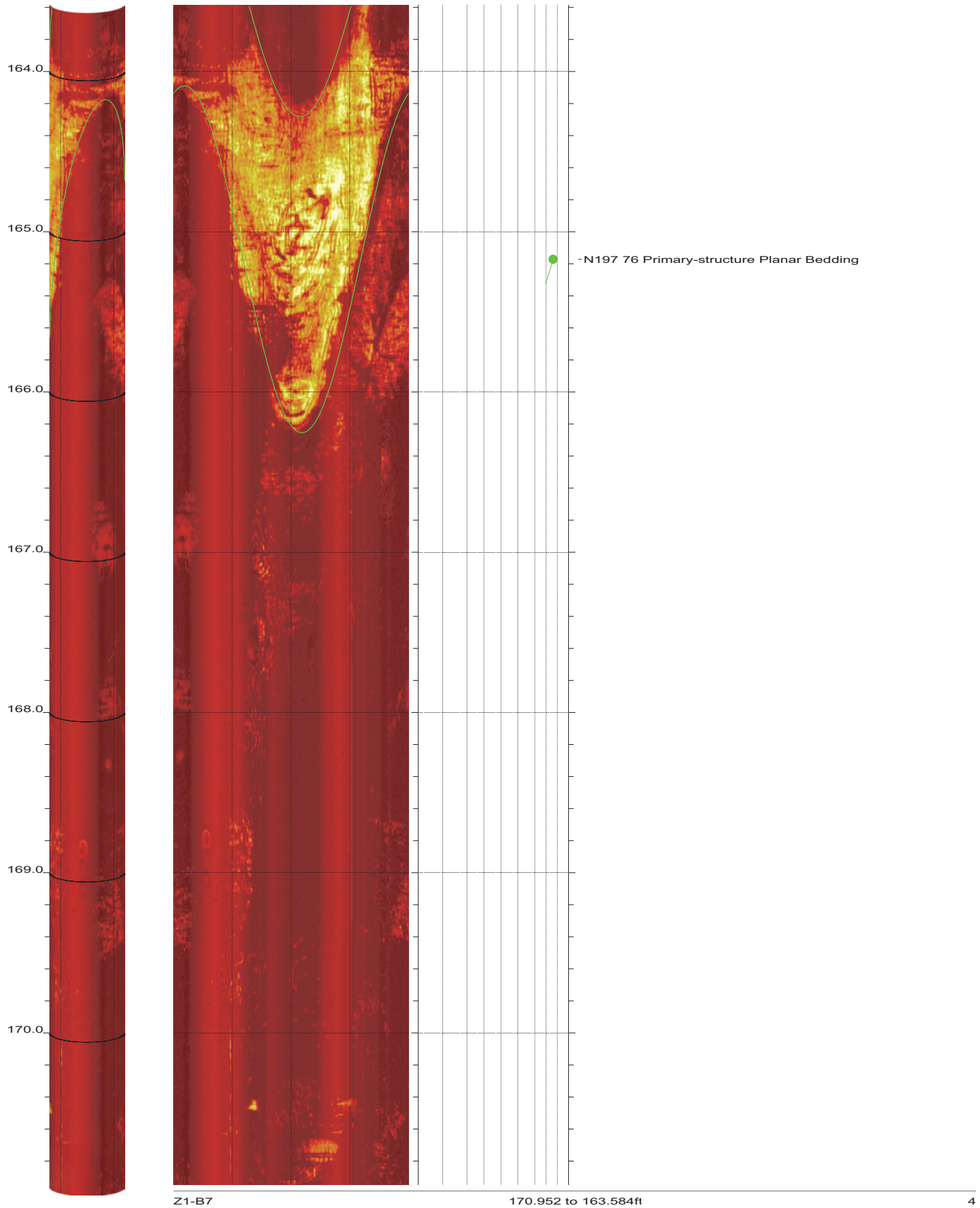




SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 2 of 22

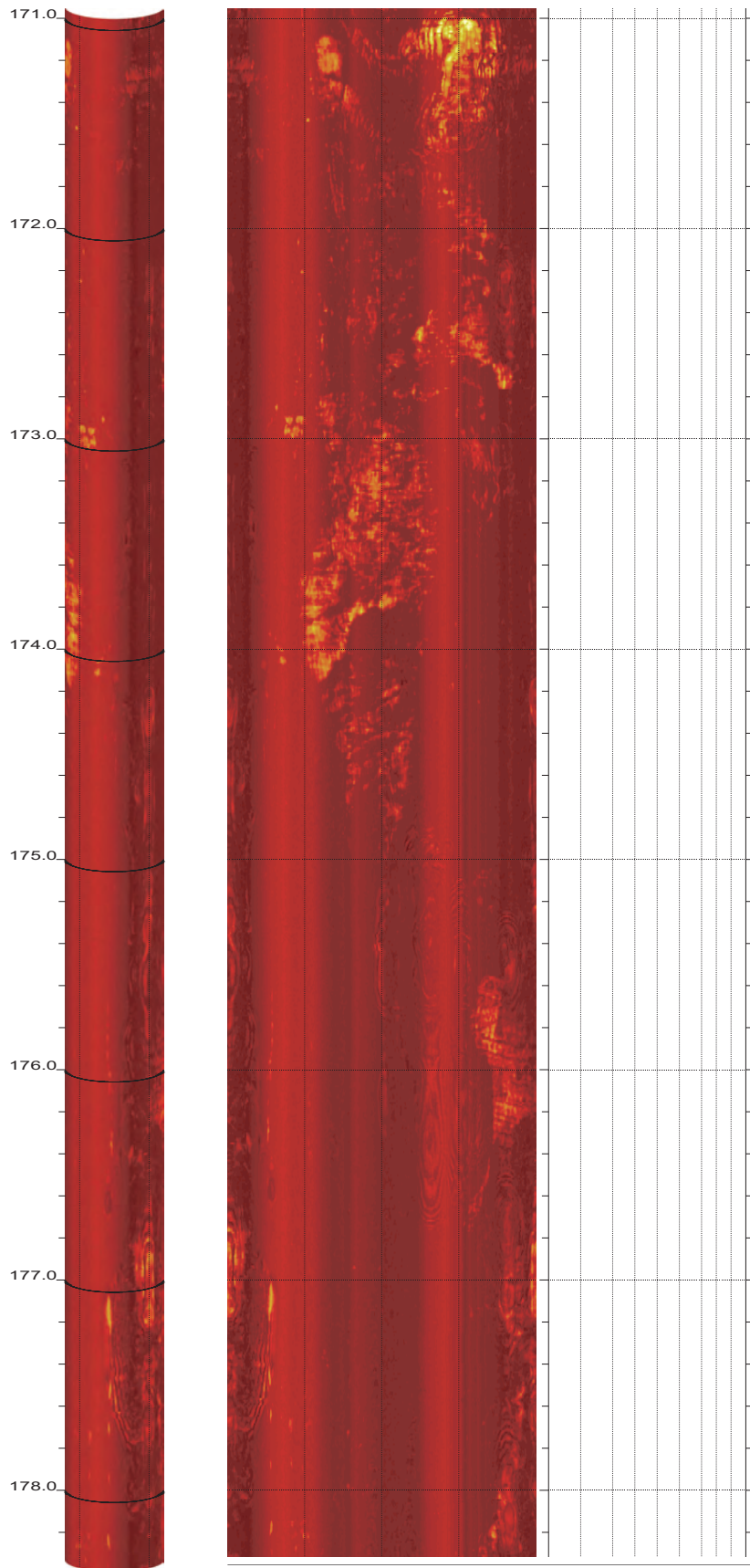


SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 3 of 22



SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 4 of 22



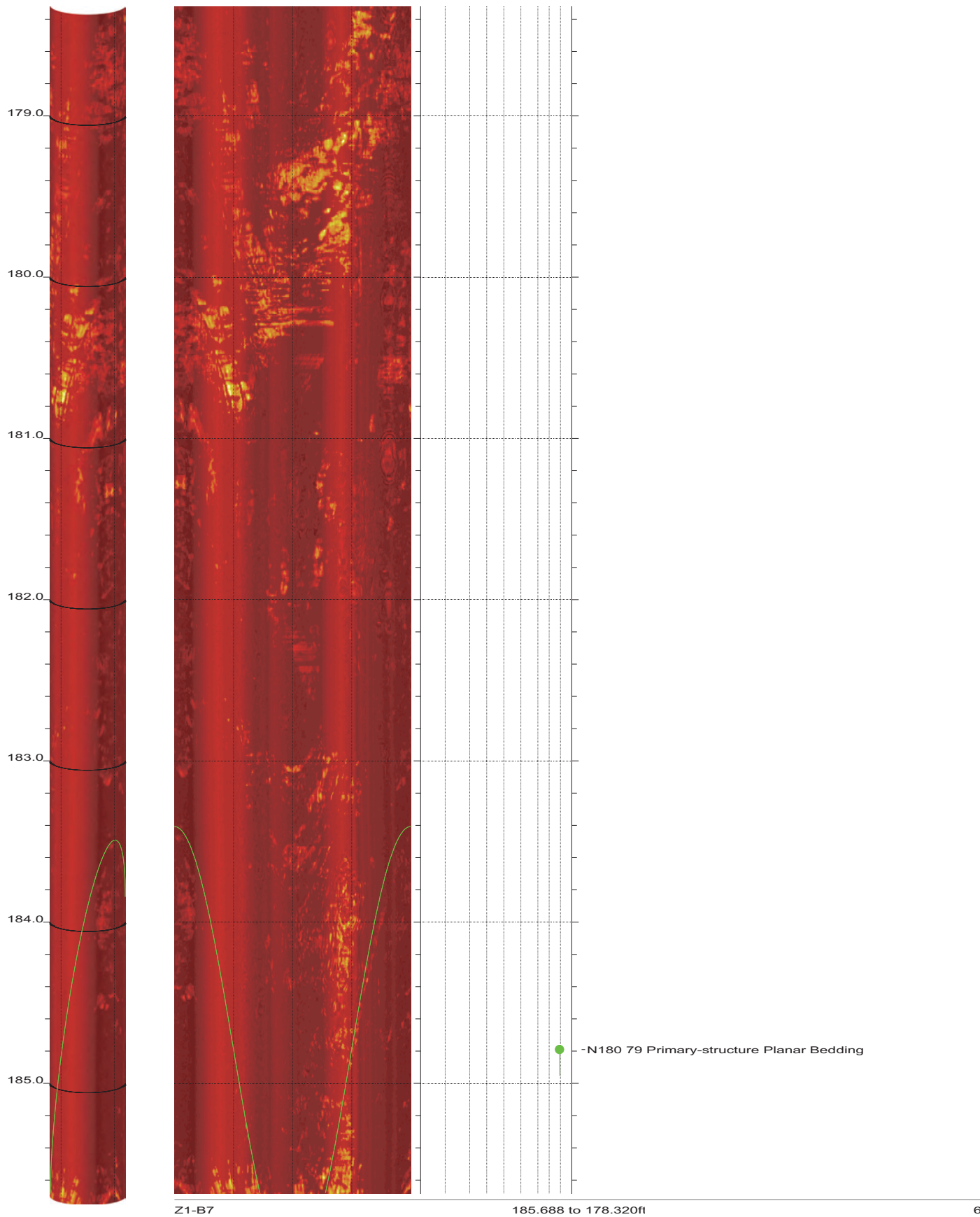


Z1-B7

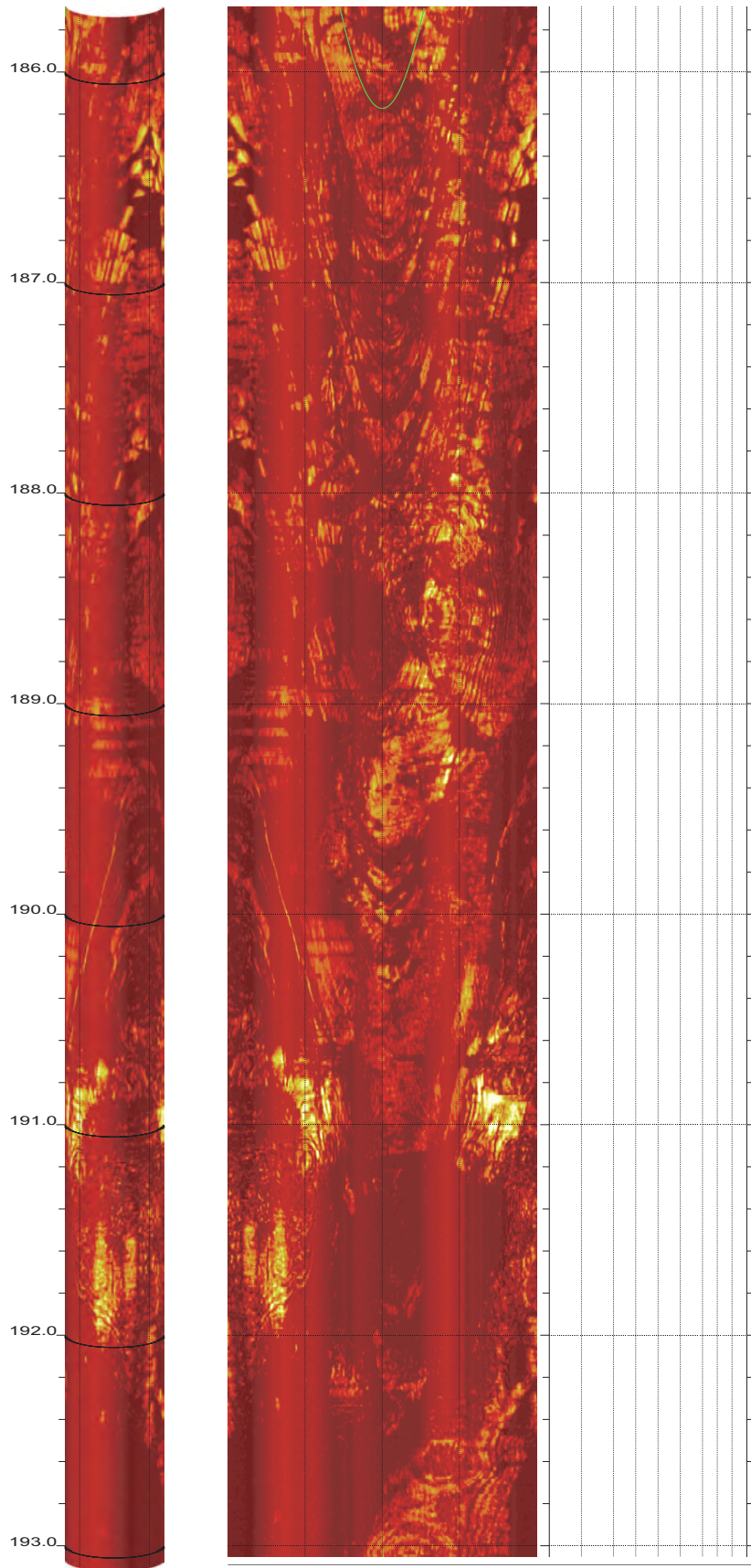
178.320 to 170.952ft

5

SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 5 of 22



SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 6 of 22

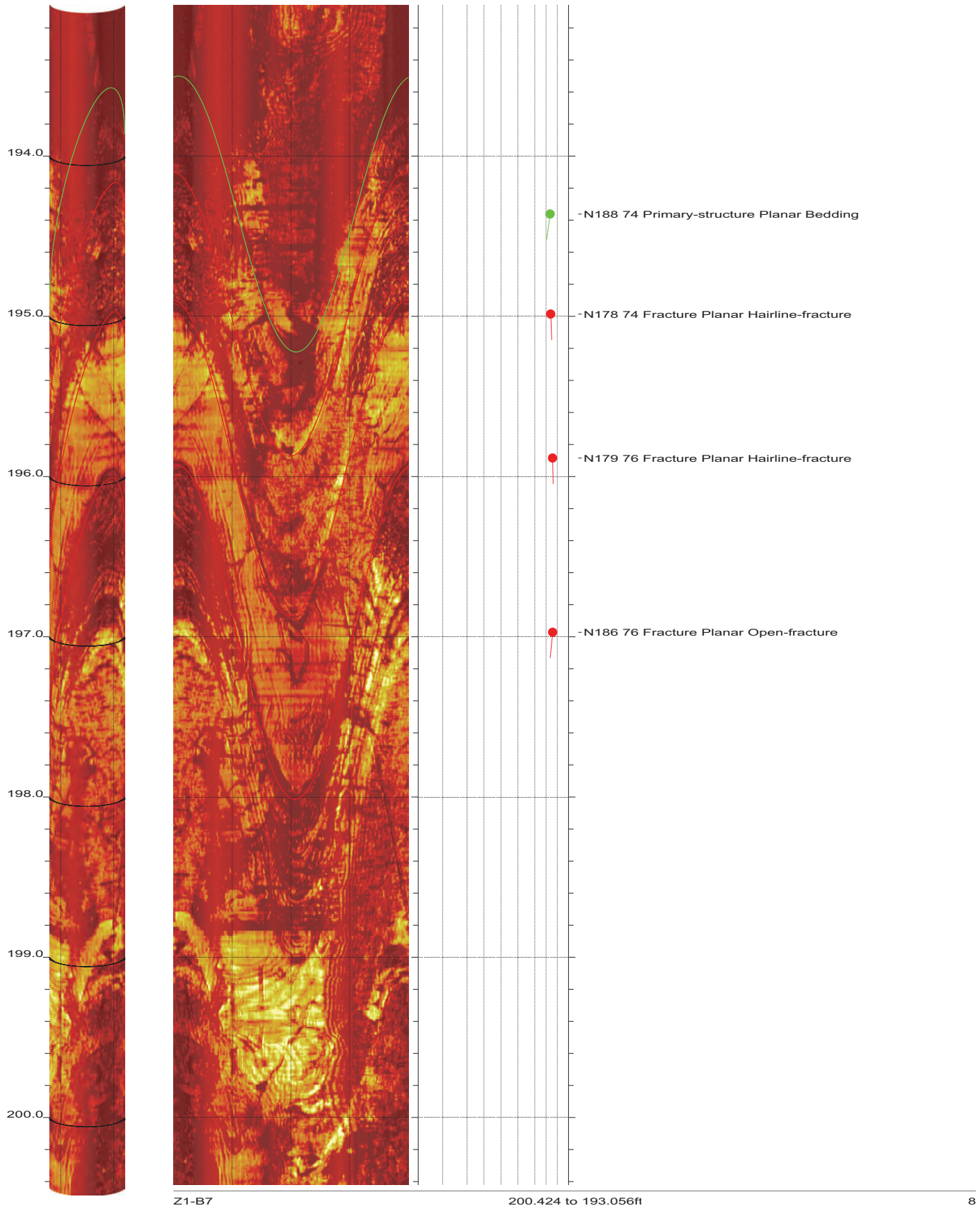


Z1-B7

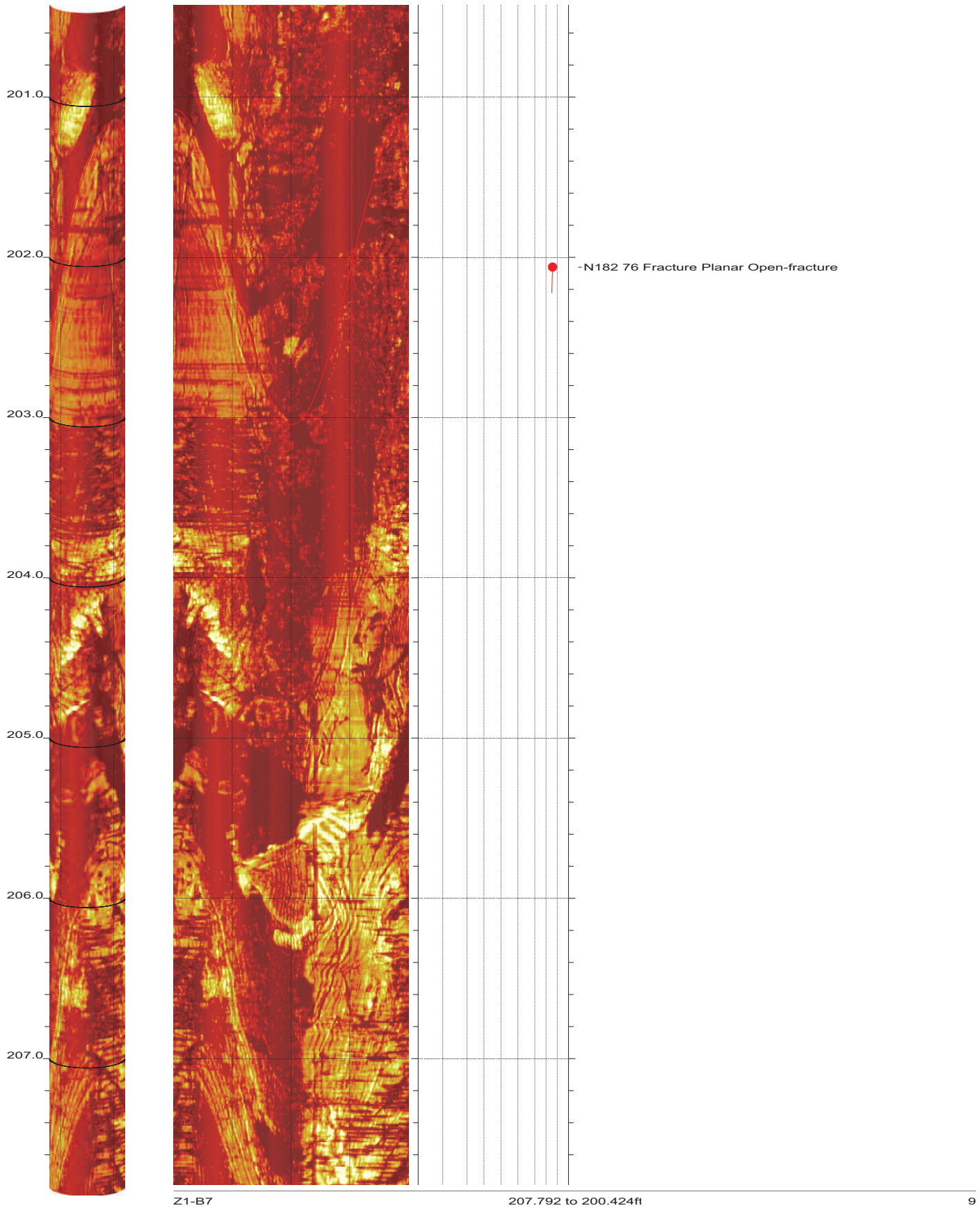
193.056 to 185.688ft

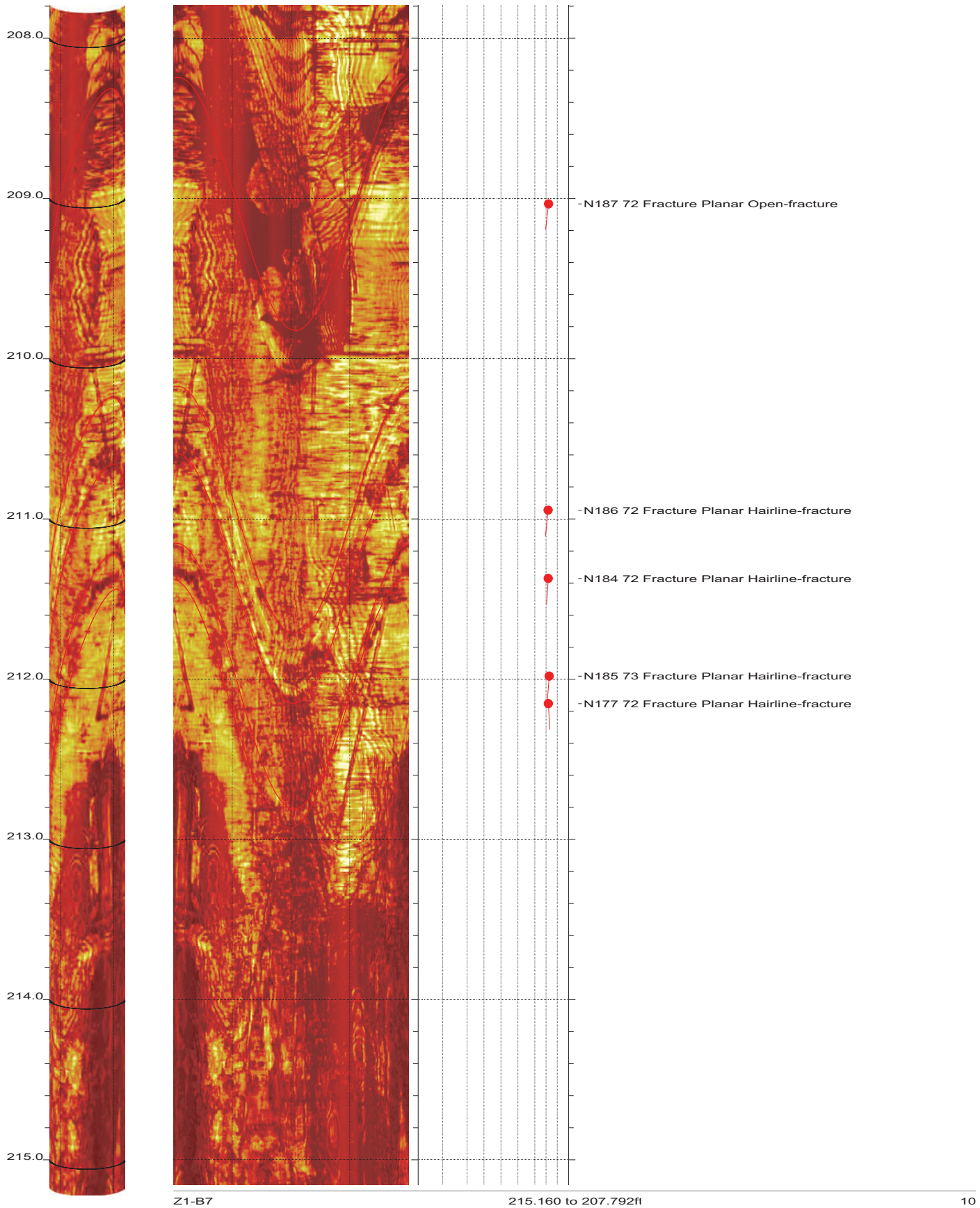
7

SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 7 of 22

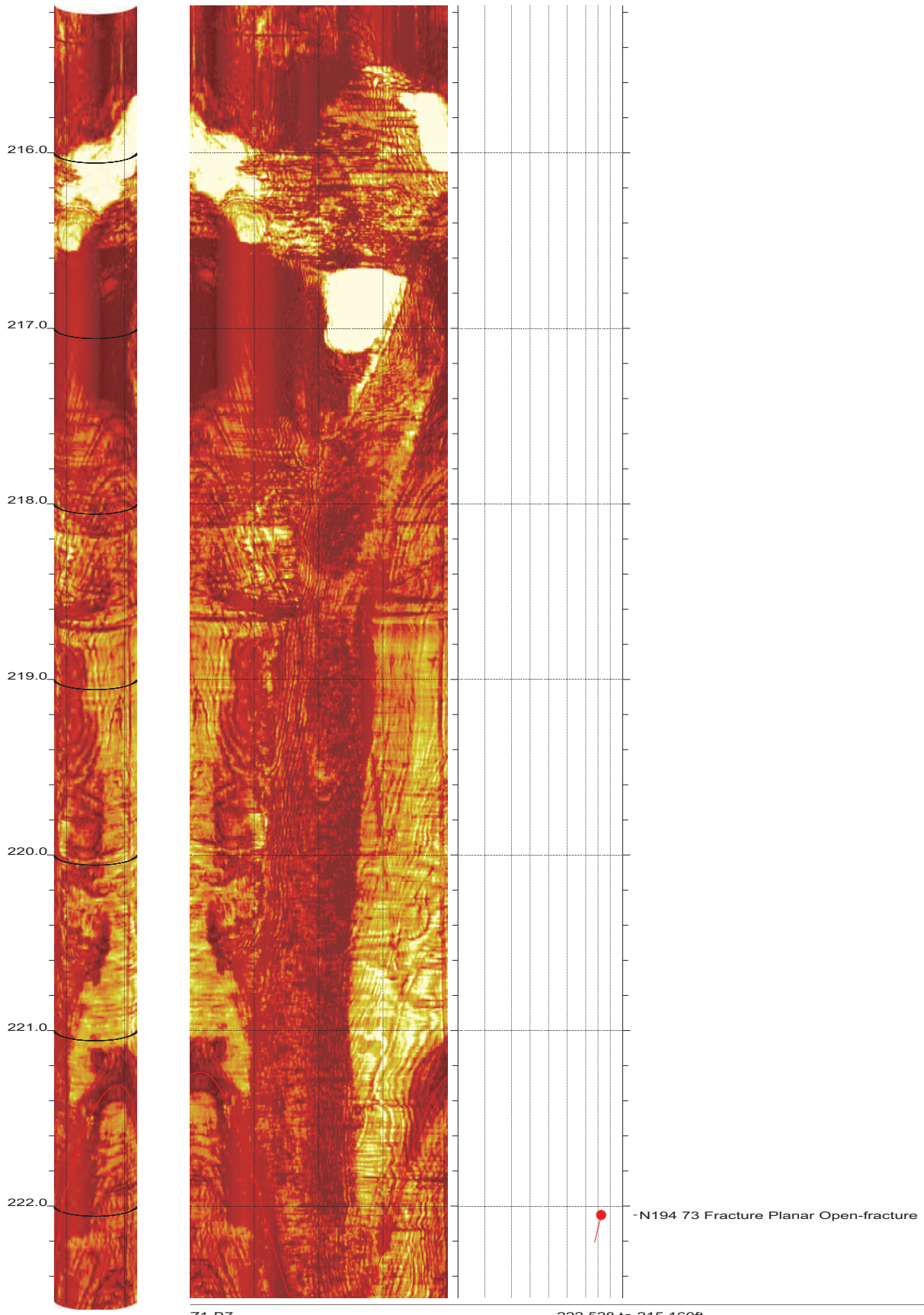


SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 8 of 22





SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 10 of 22

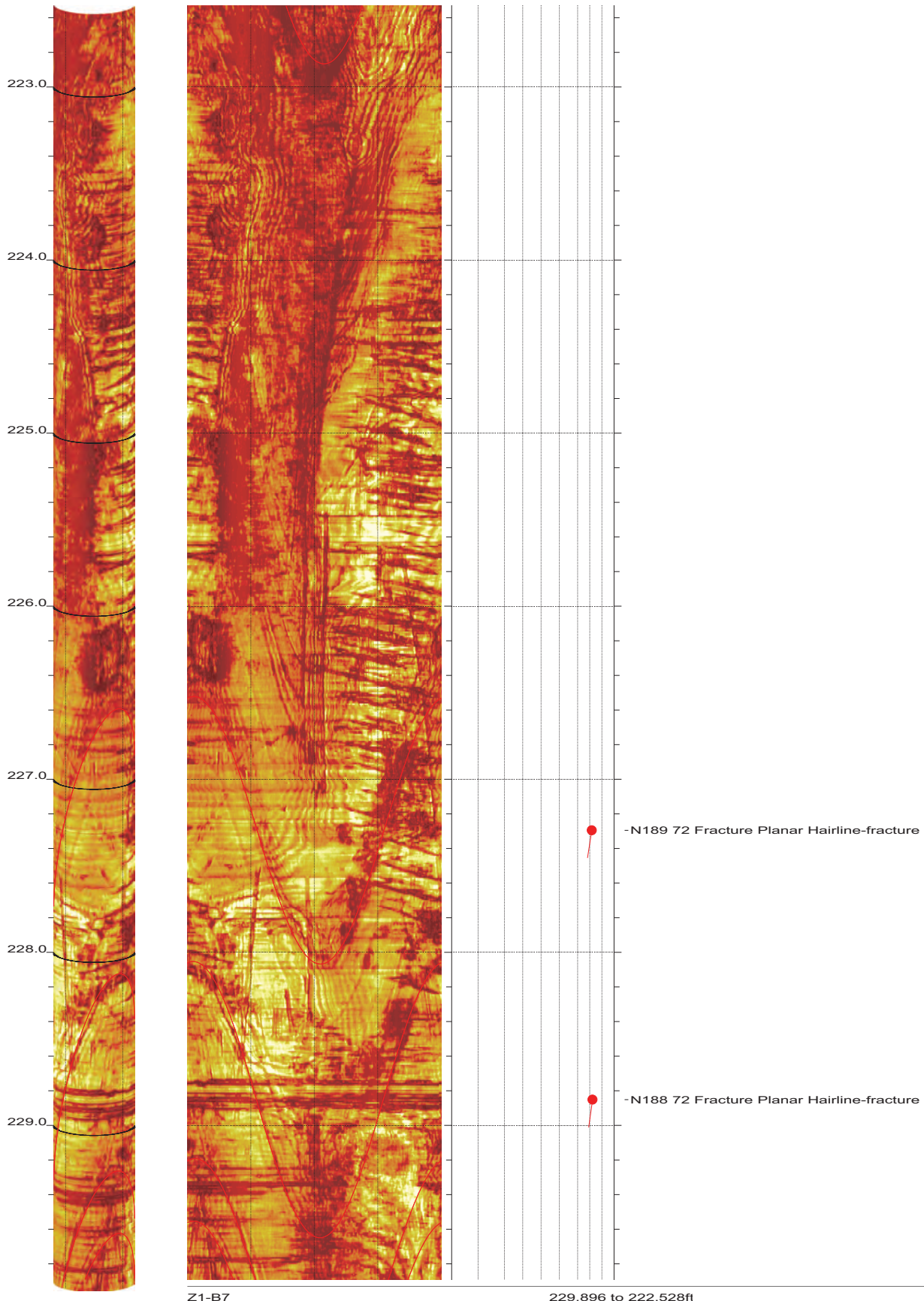


Z1-B7

222.528 to 215.160ft

11

SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 11 of 22



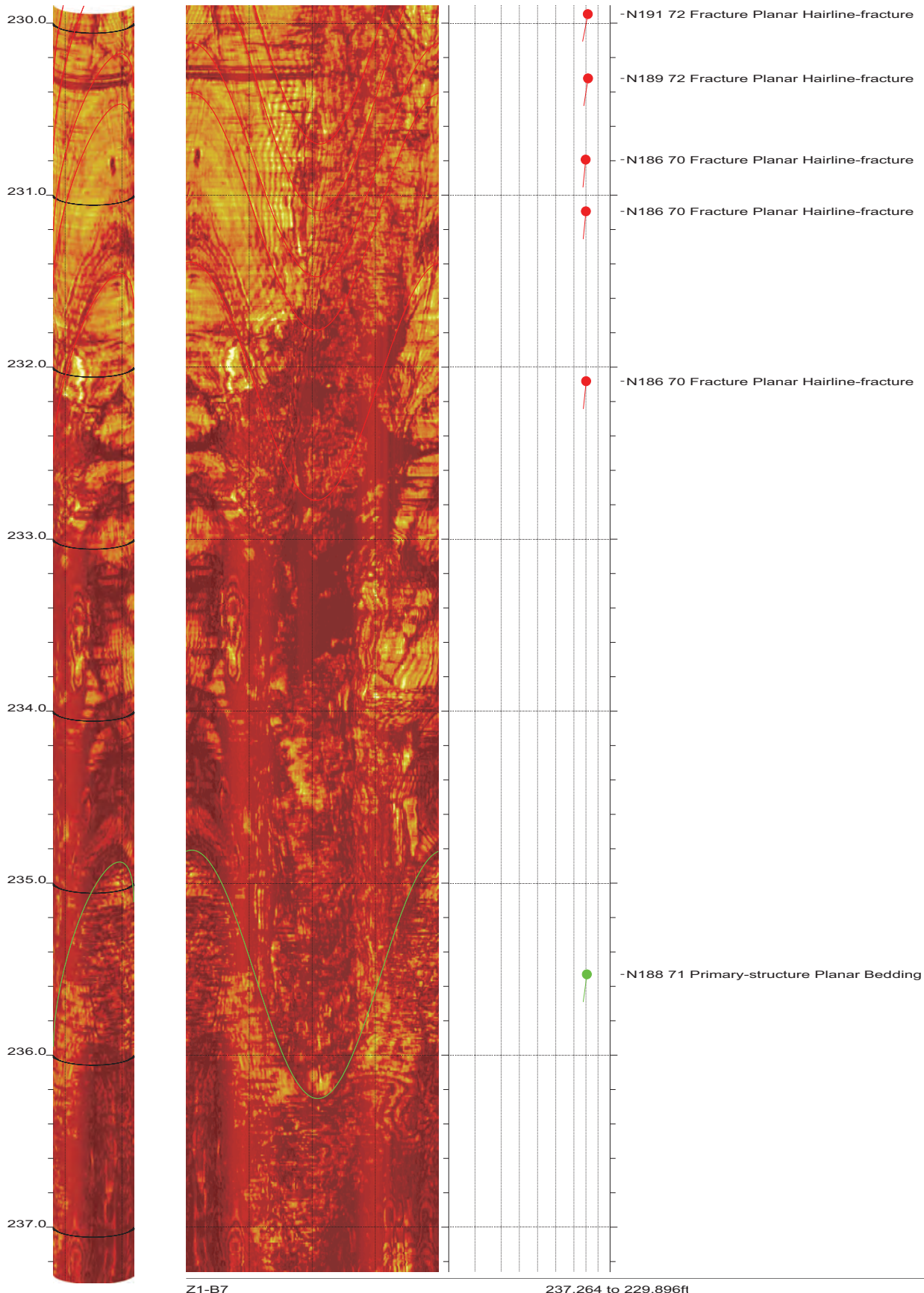
Z1-B7

229.896 to 222.528ft

12

SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 12 of 22



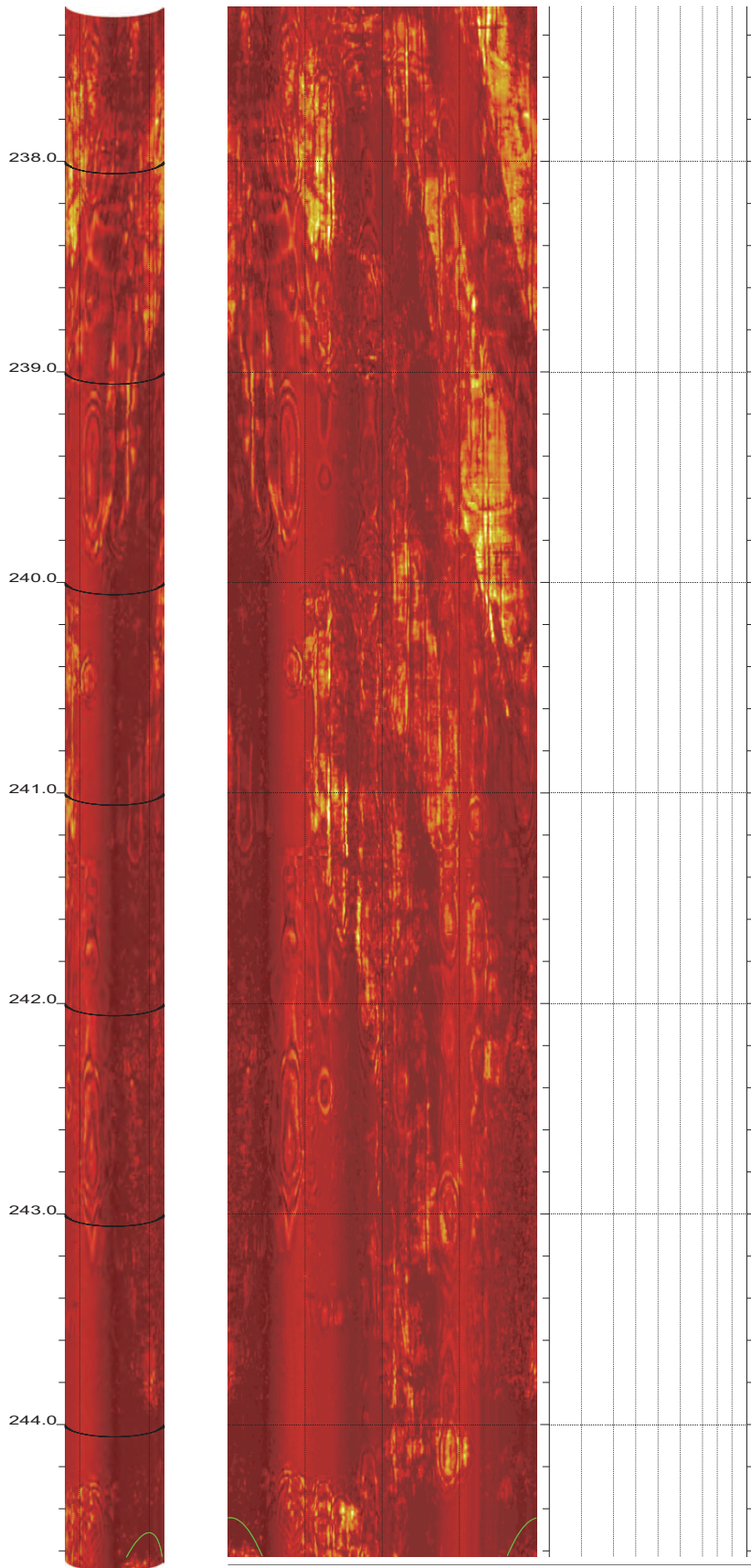


Z1-B7

237.264 to 229.896ft

13

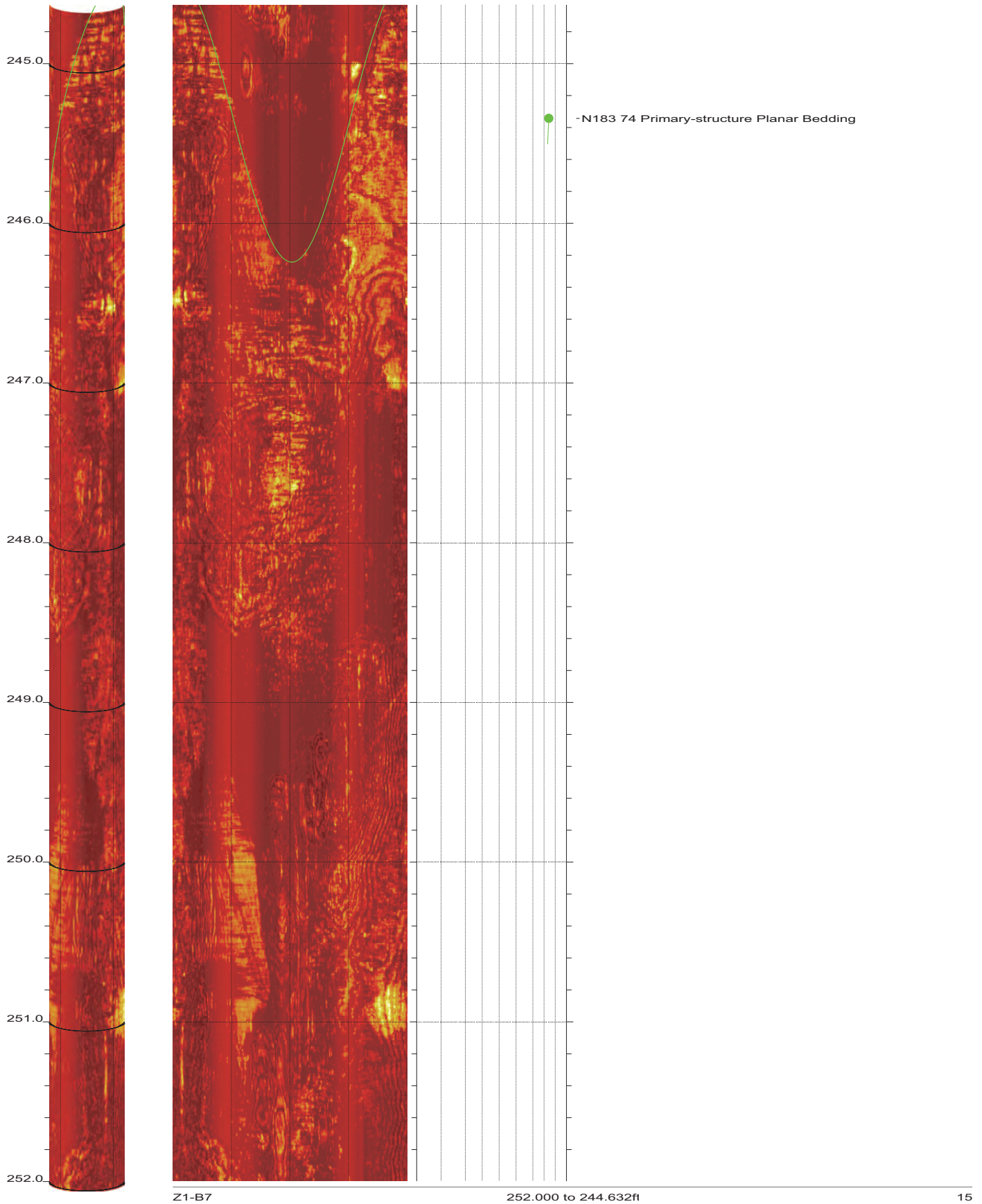
SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 13 of 22



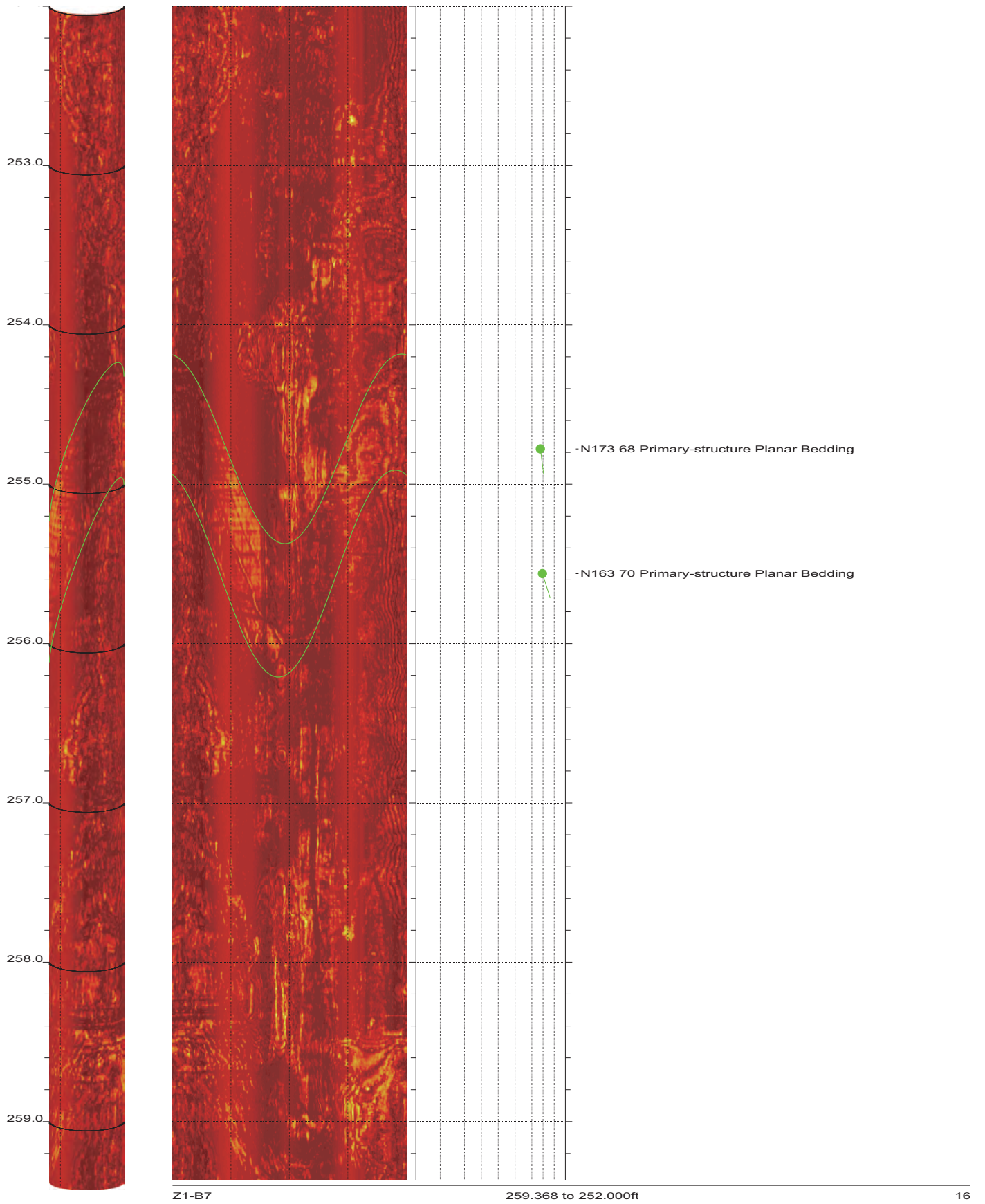
Z1-B7

244.632 to 237.264ft

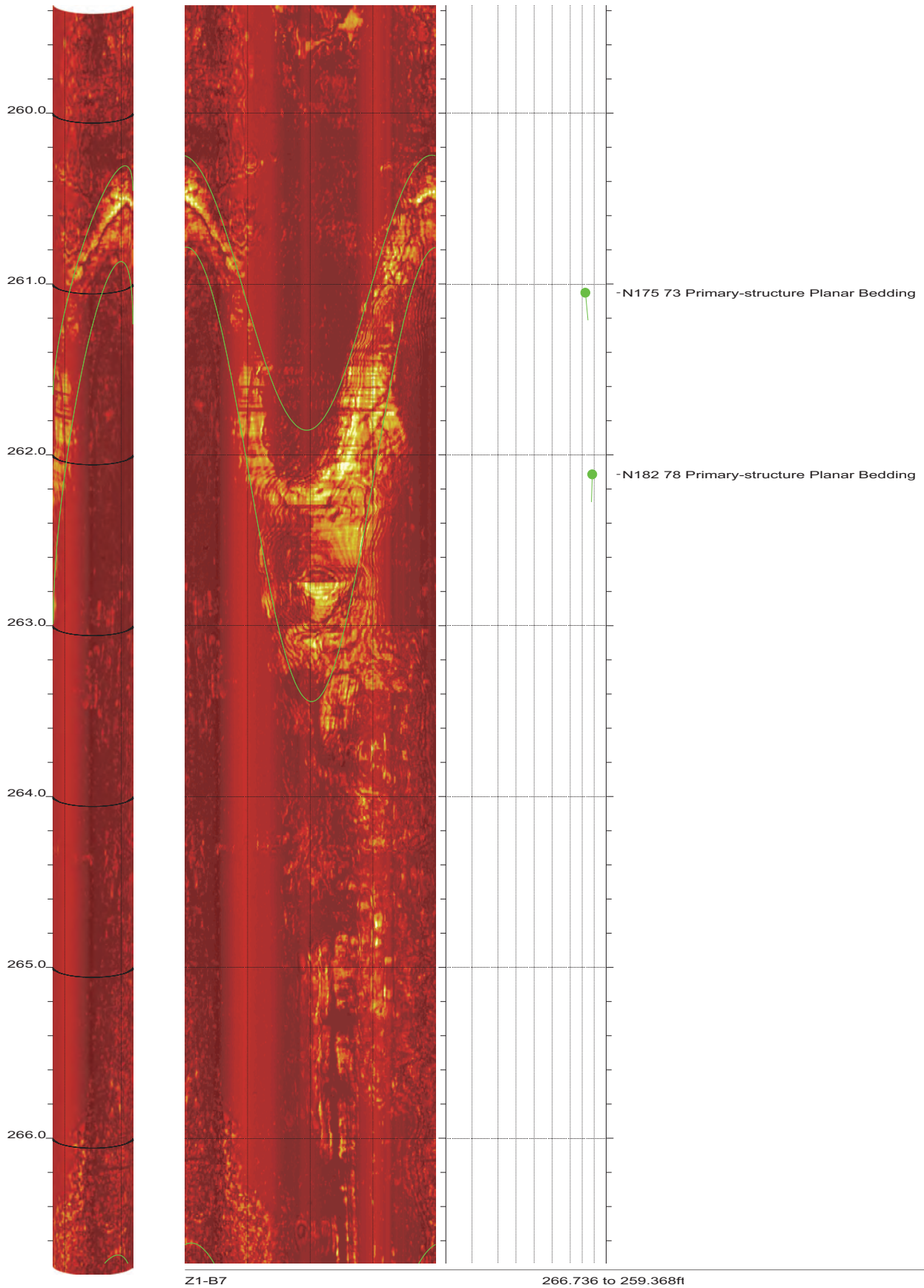
14

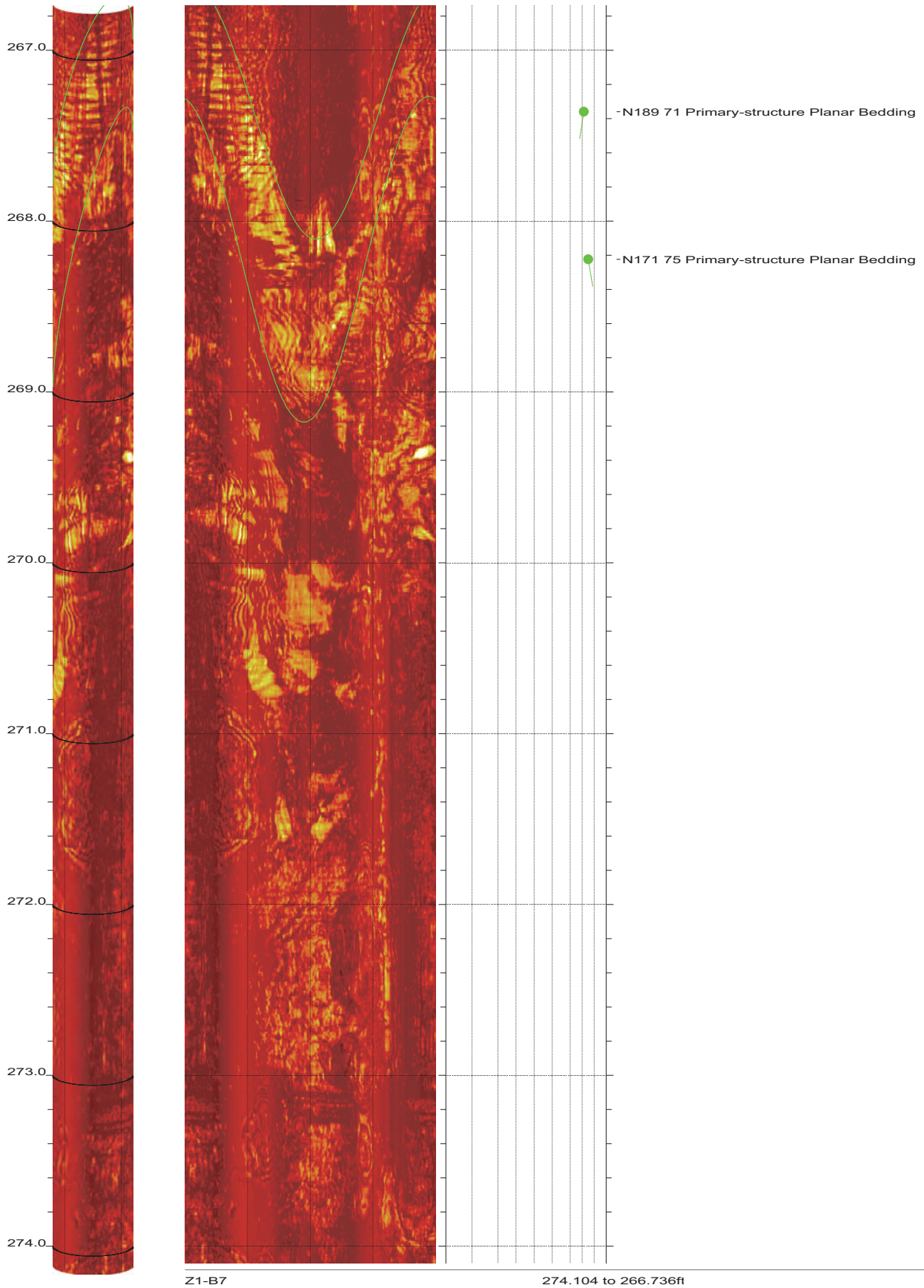


SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 15 of 22

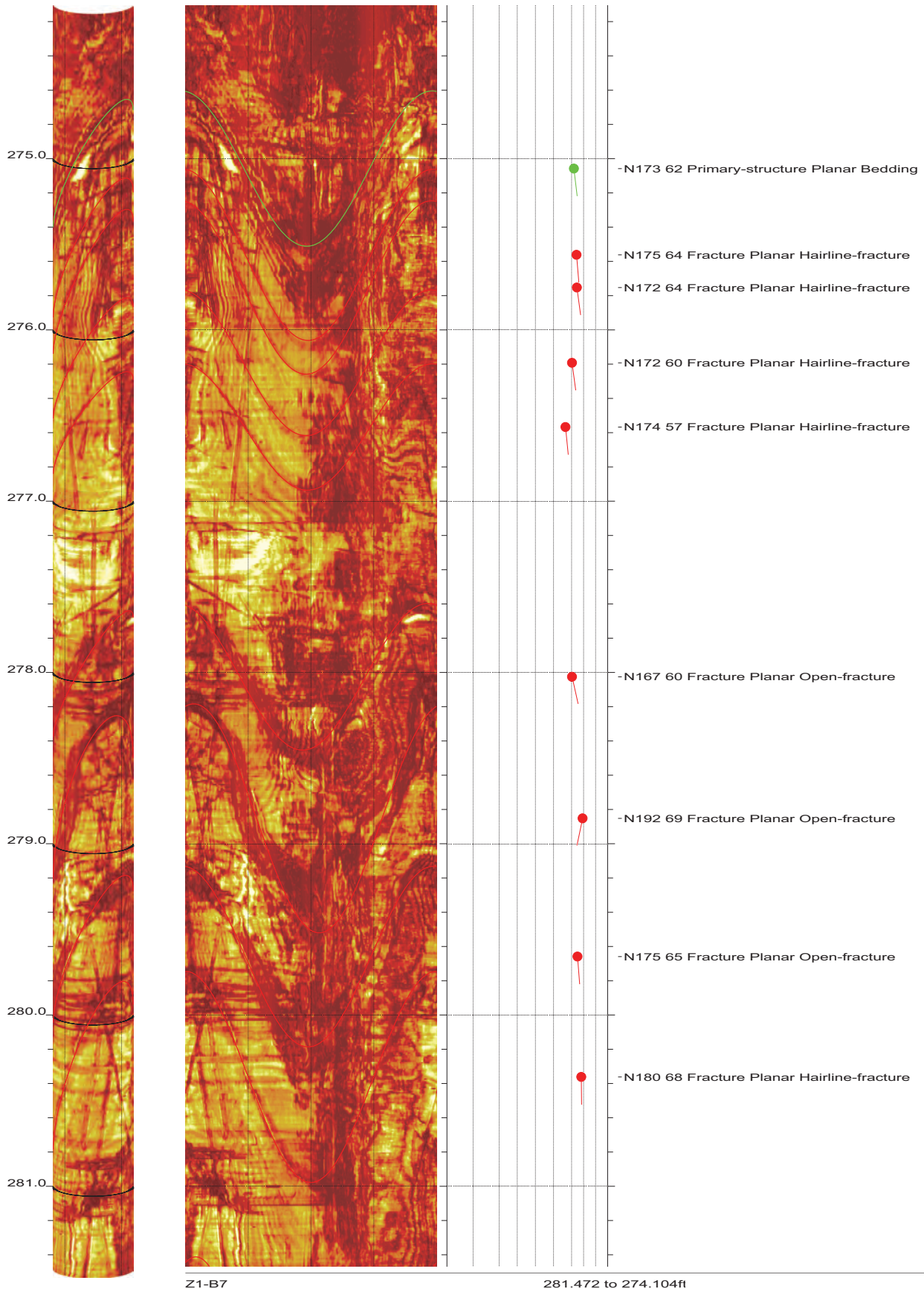


SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 16 of 22

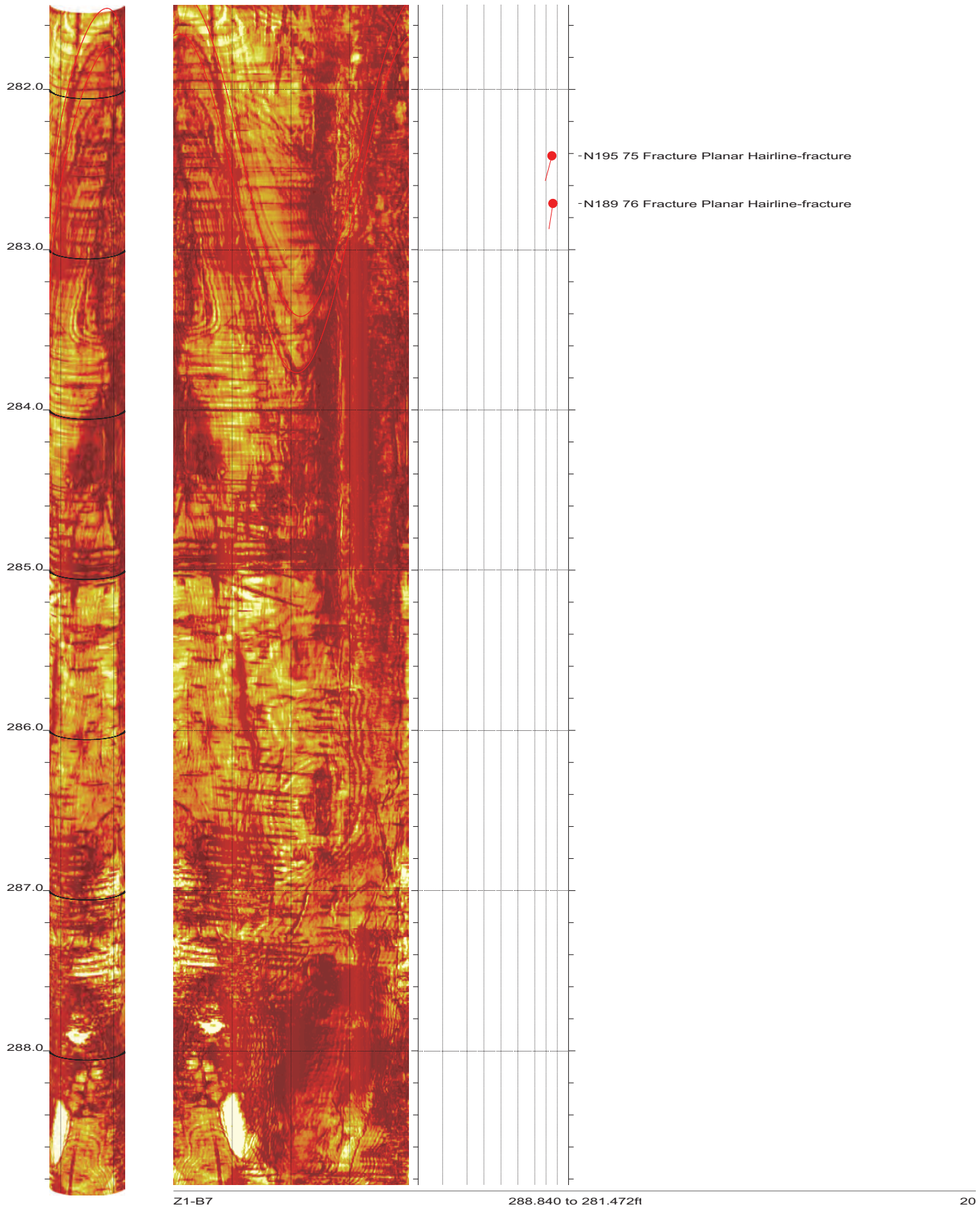




SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 18 of 22

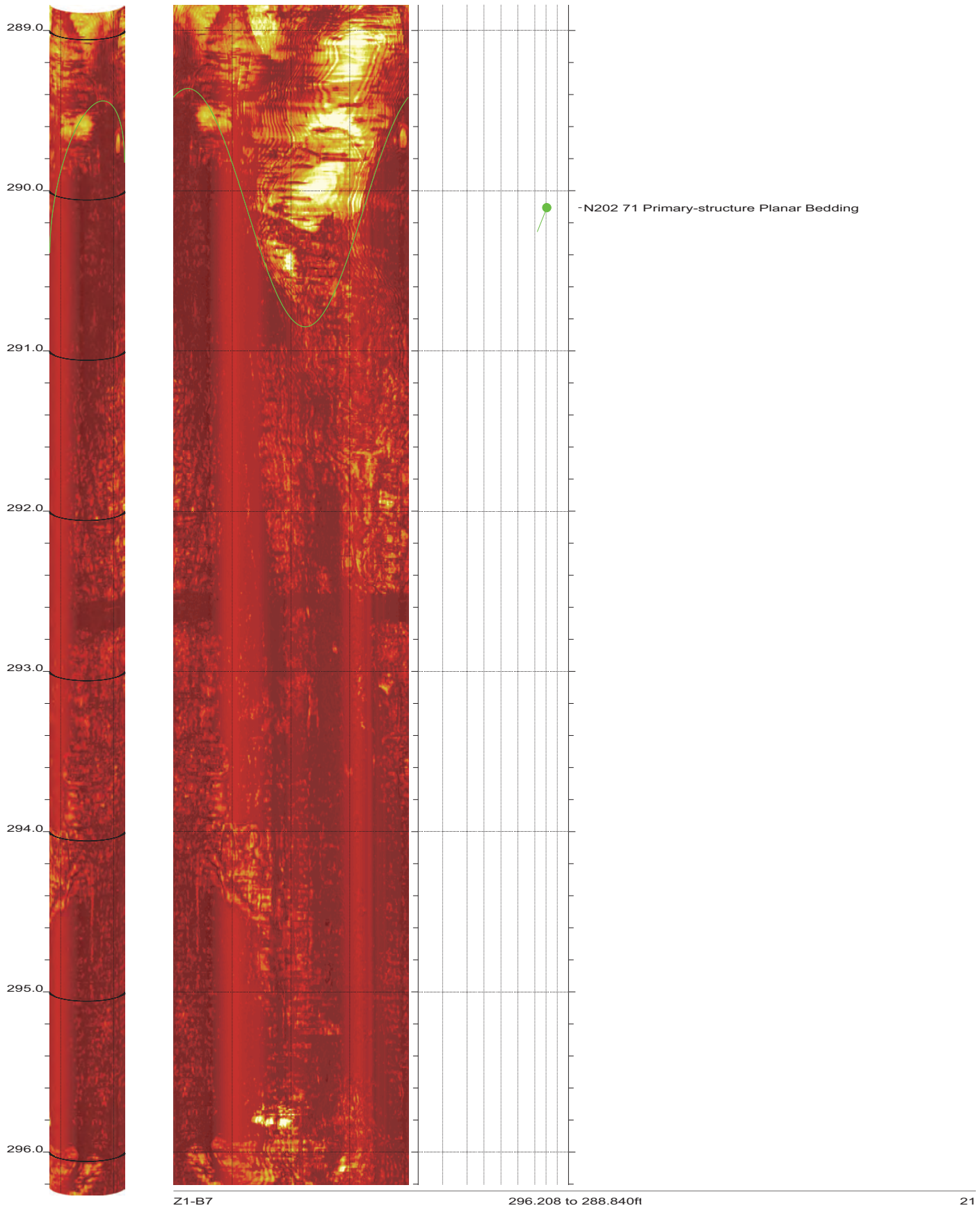


SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 19 of 22

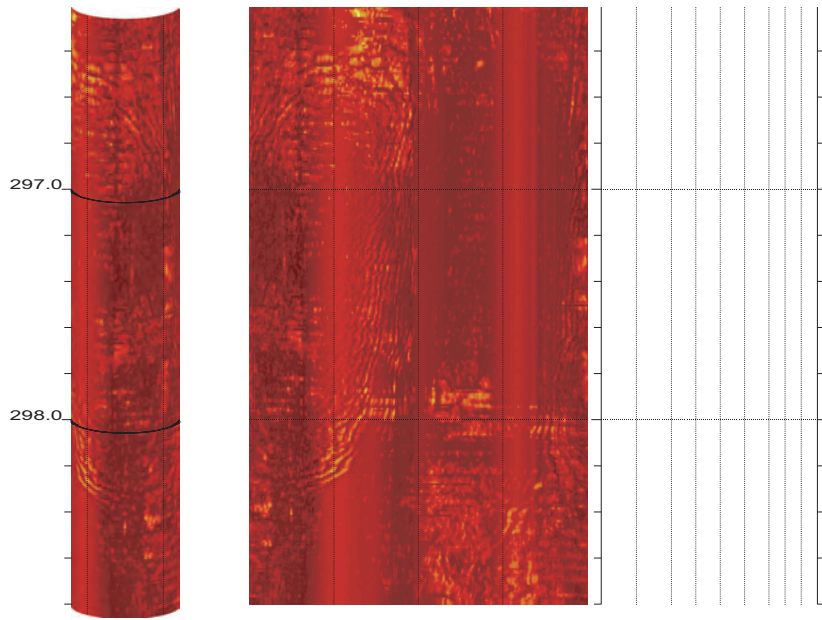


SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 20 of 22





SR-710 Boring Z1-B7 Acoustic Televiewer Dips rev 1 Sheet 21 of 22





CASCADE DRILLING

Borehole: Z2-B1

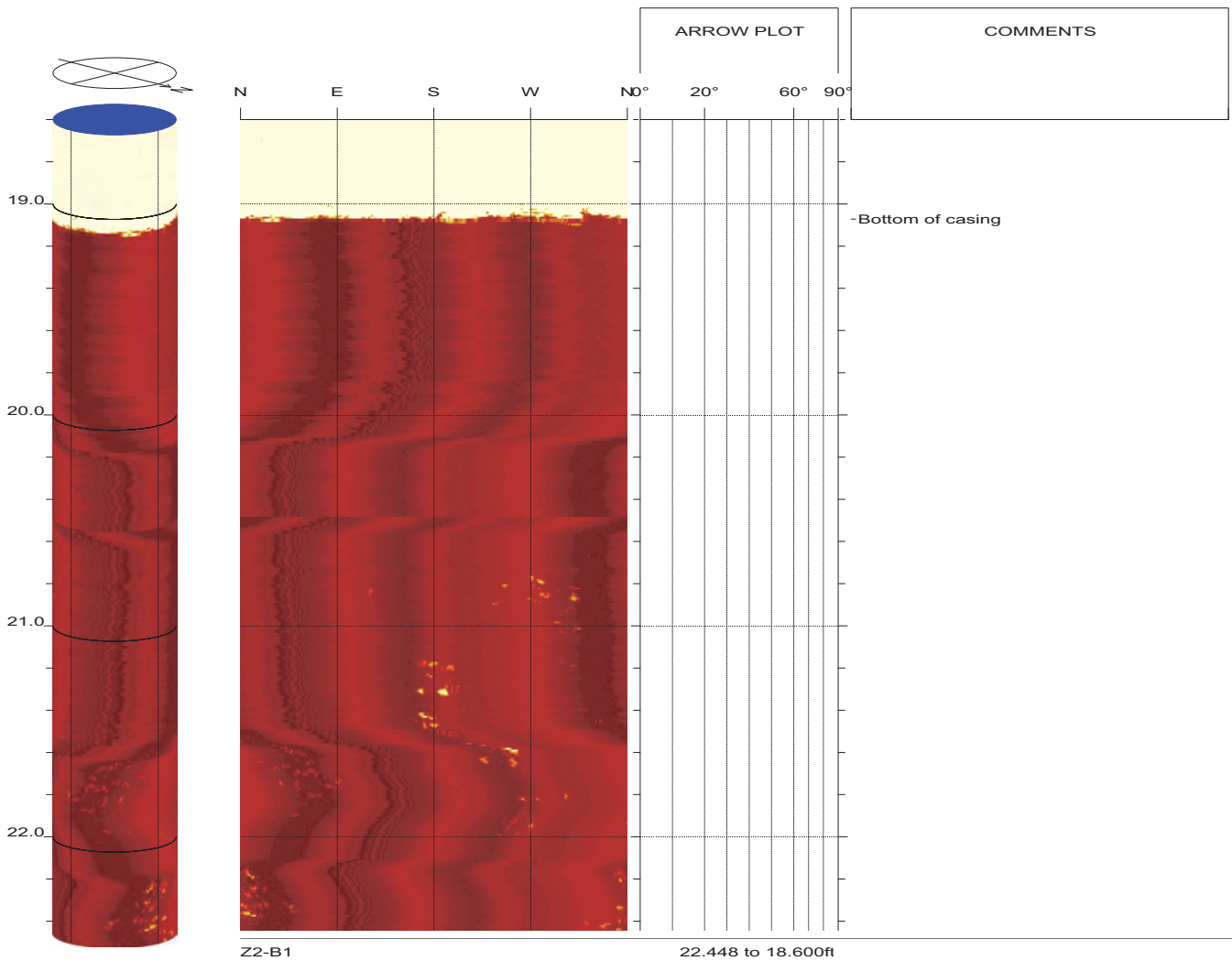
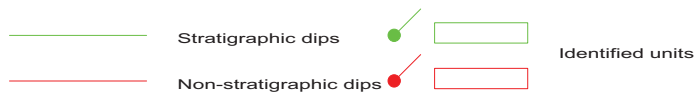
SR-710 TUNNEL INVESTIGATION

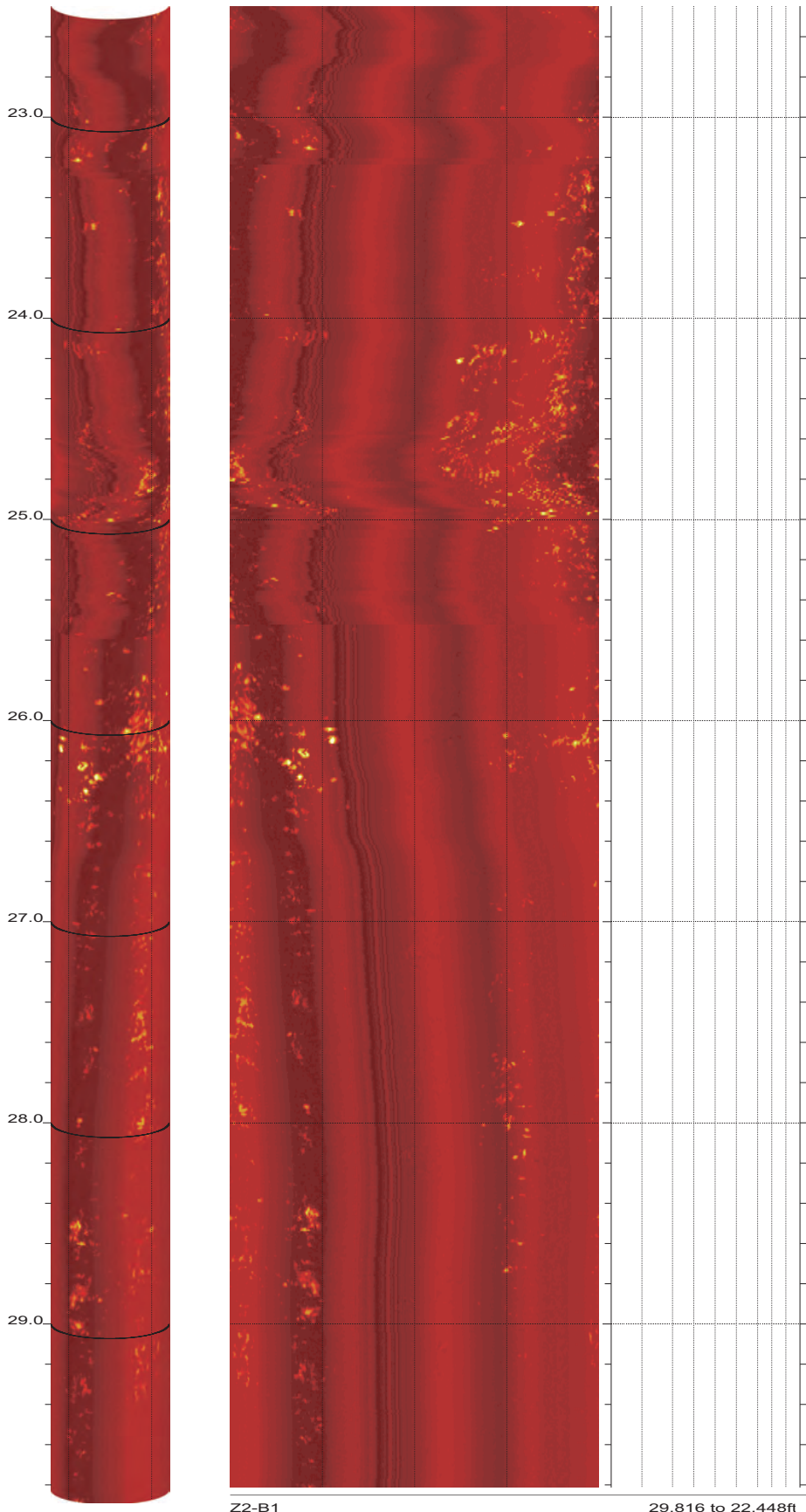
top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

Zone from 148.800 to 18.600ft  
 Format: BHTV-NESWN

Borehole diam: 7.000inch  
 Vertical = borehole-axis  
 Image: Amplitude



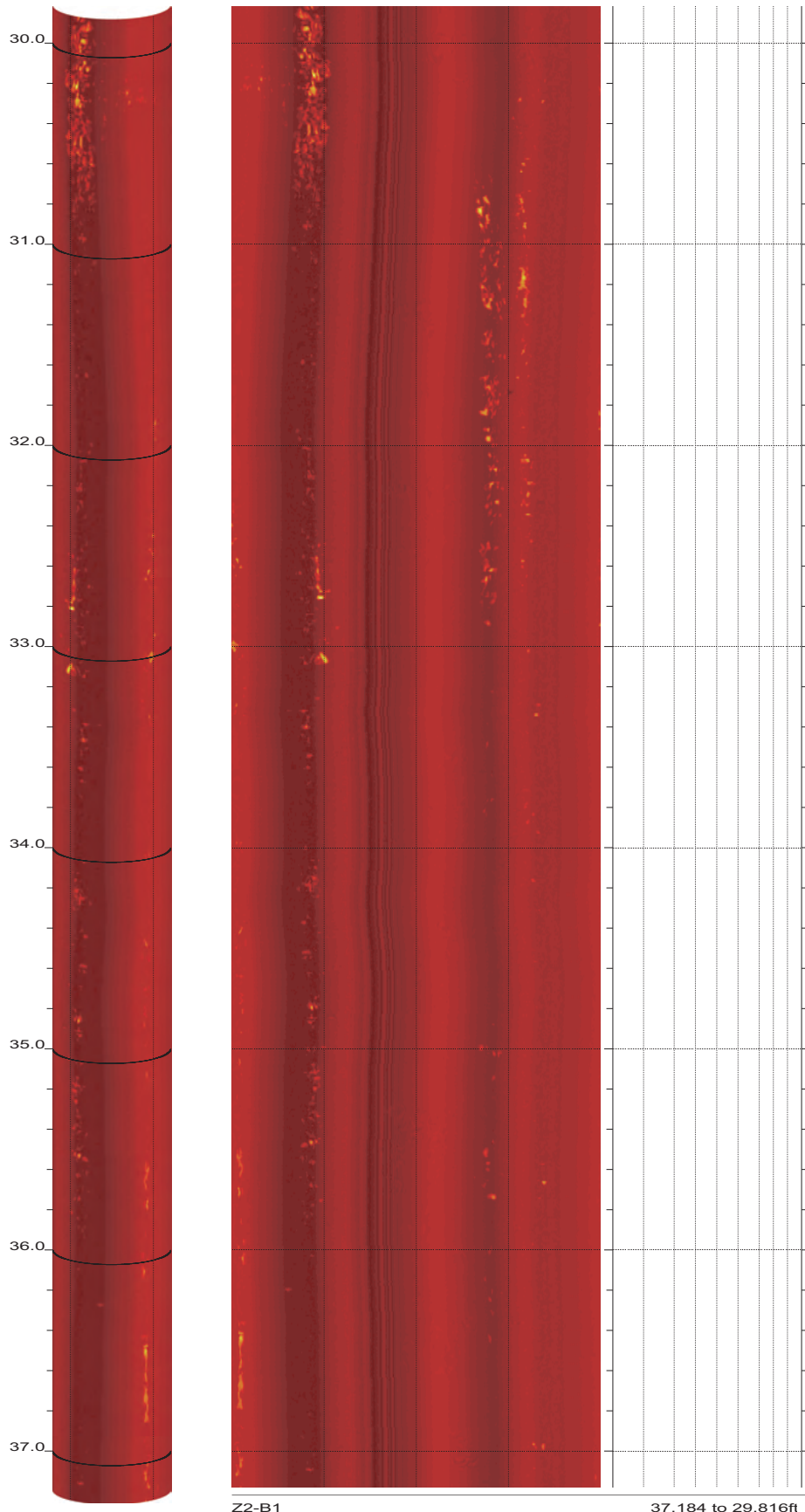


Z2-B1

29.816 to 22.448ft

2

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 2 of 19

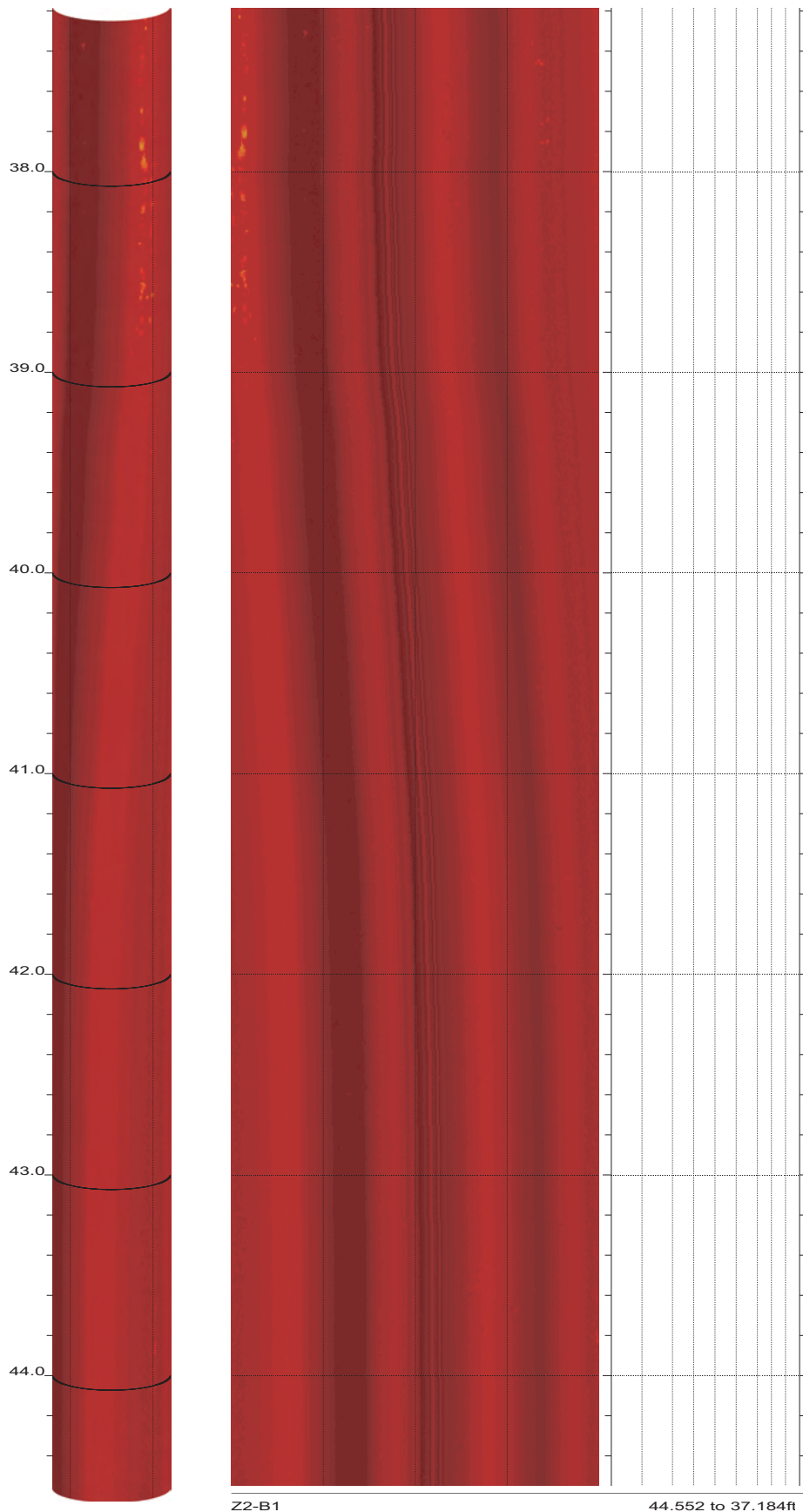


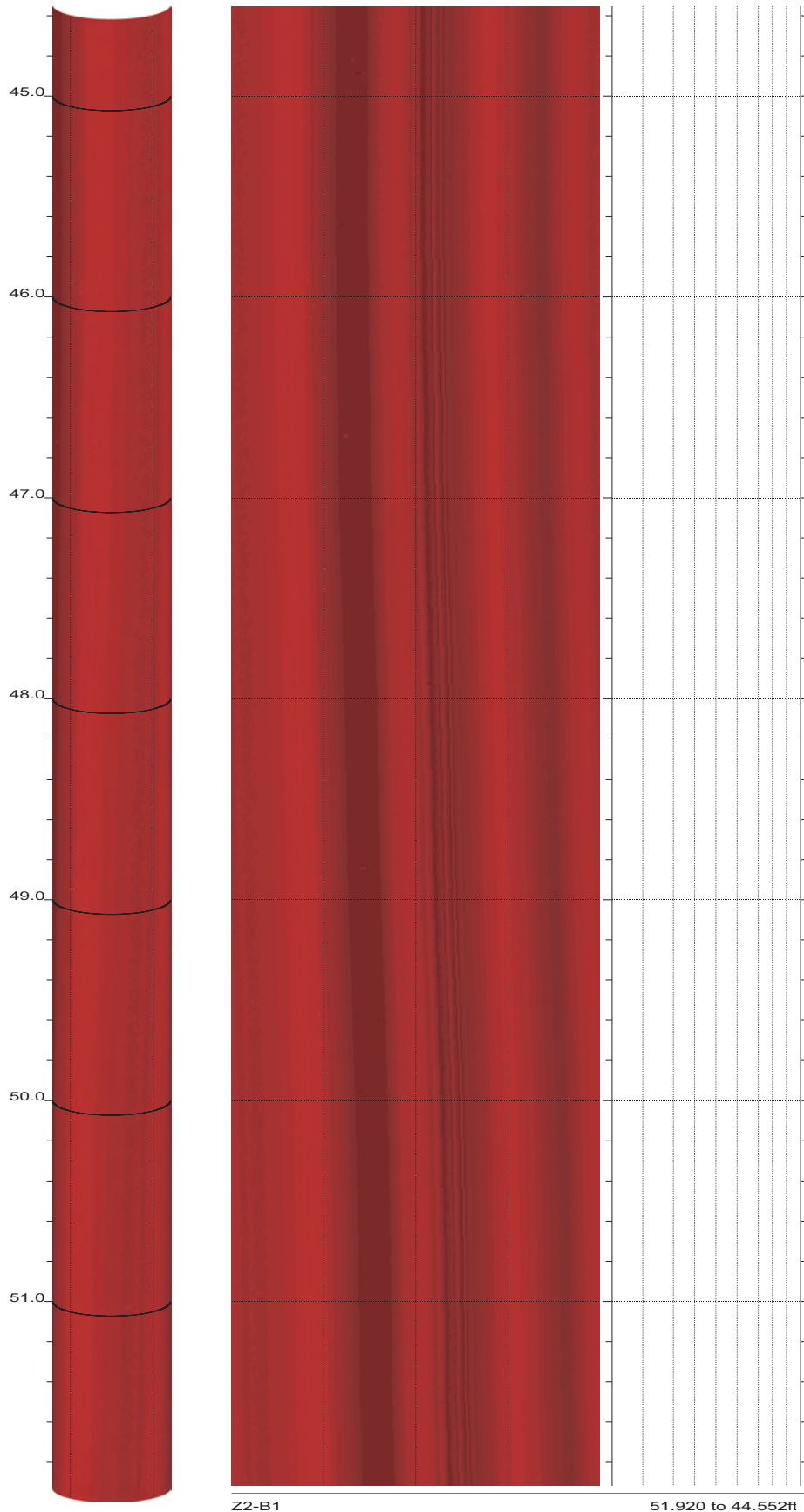
Z2-B1

37.184 to 29.816ft

3

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 3 of 19



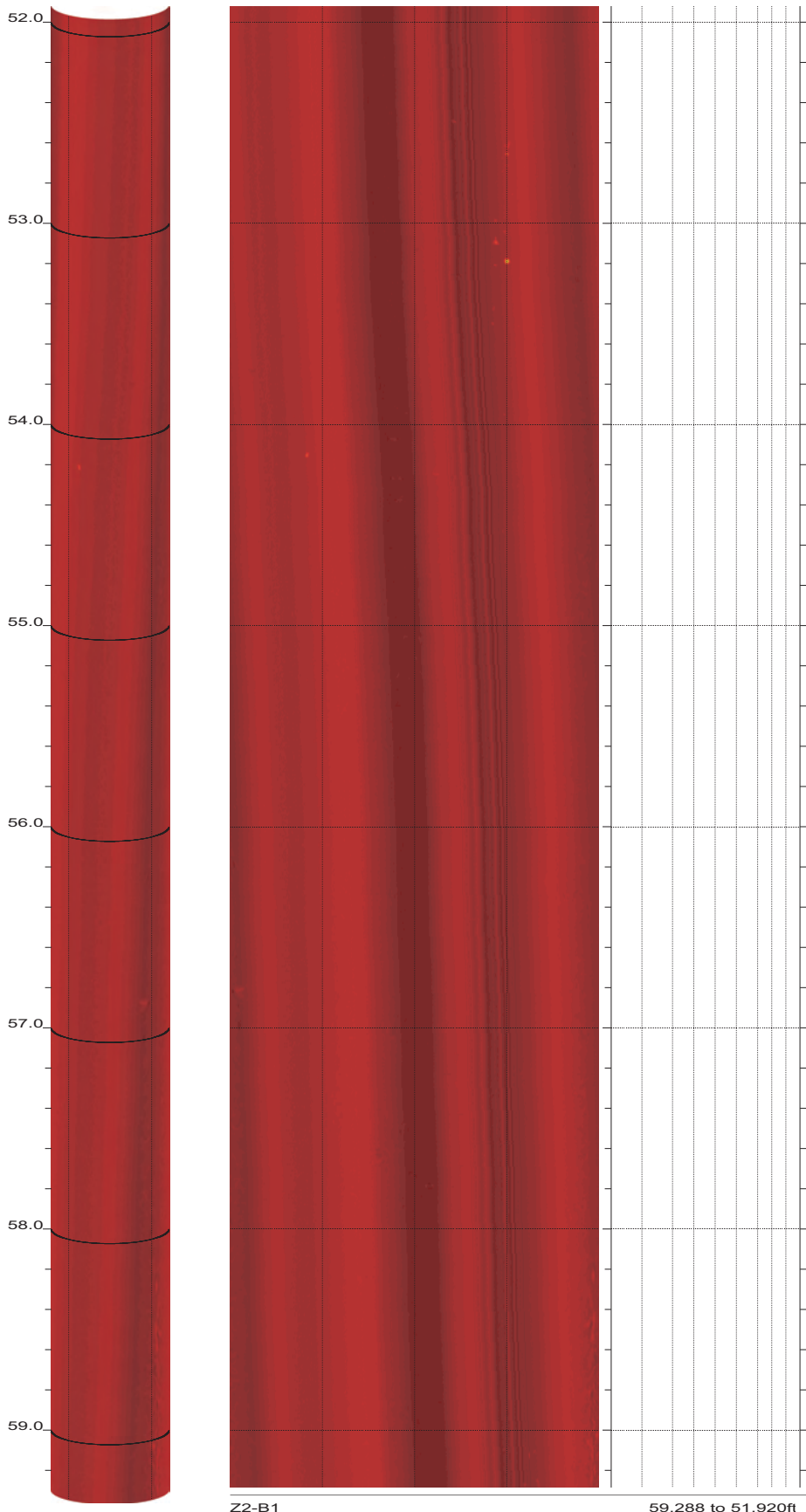


Z2-B1

51.920 to 44.552ft

5

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 5 of 19



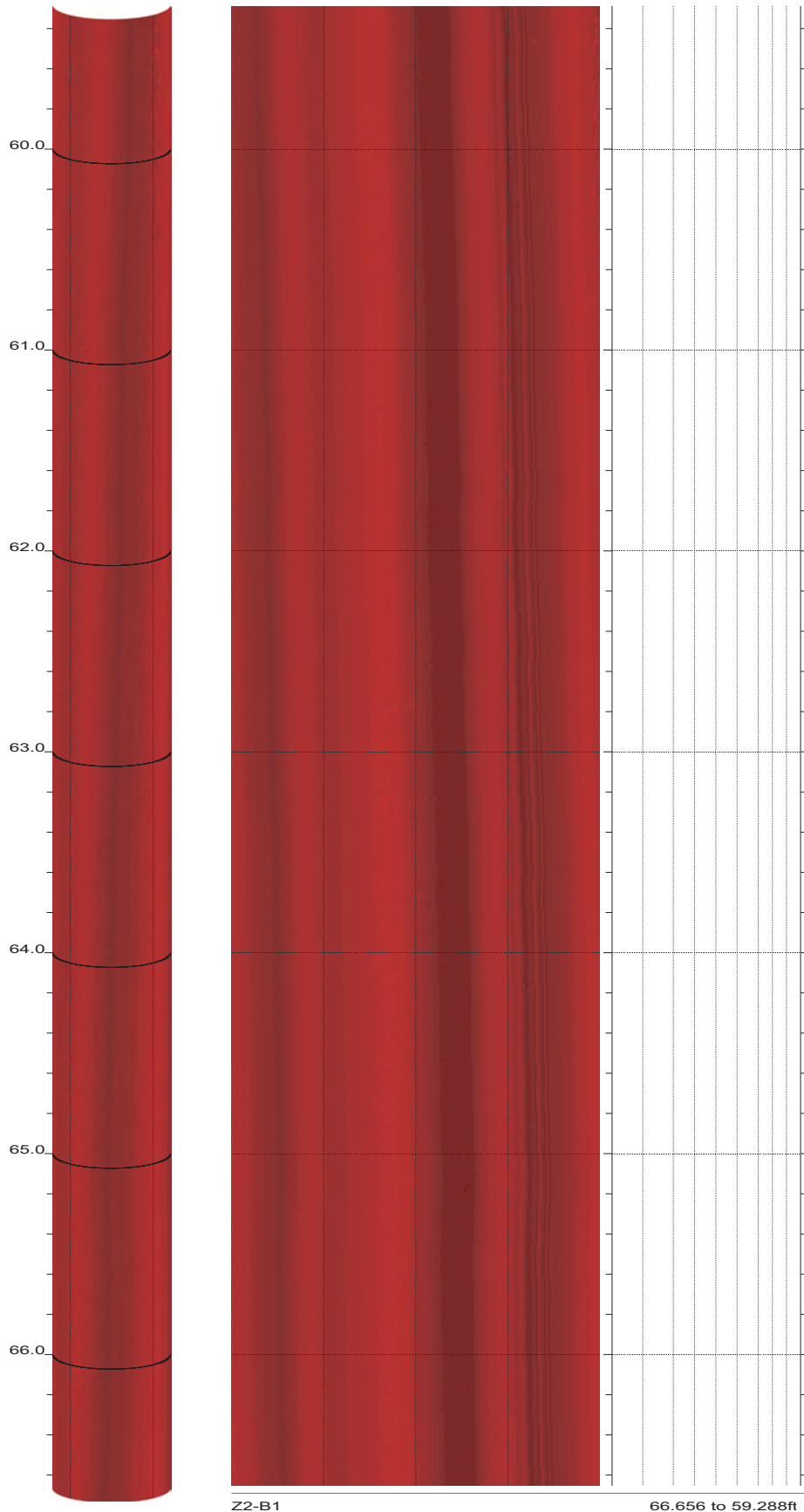
Z2-B1

59.288 to 51.920ft

6

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 6 of 19



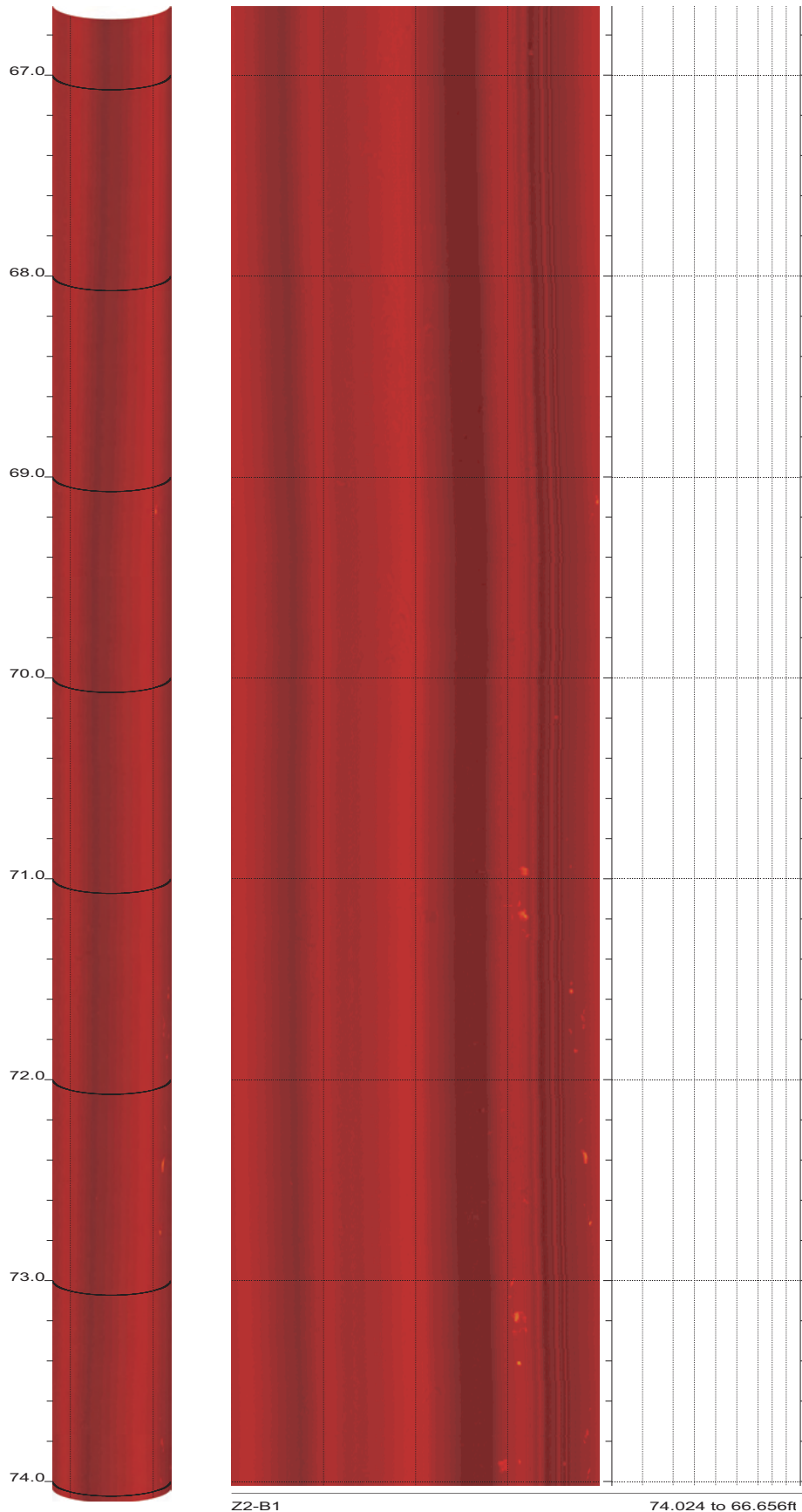


Z2-B1

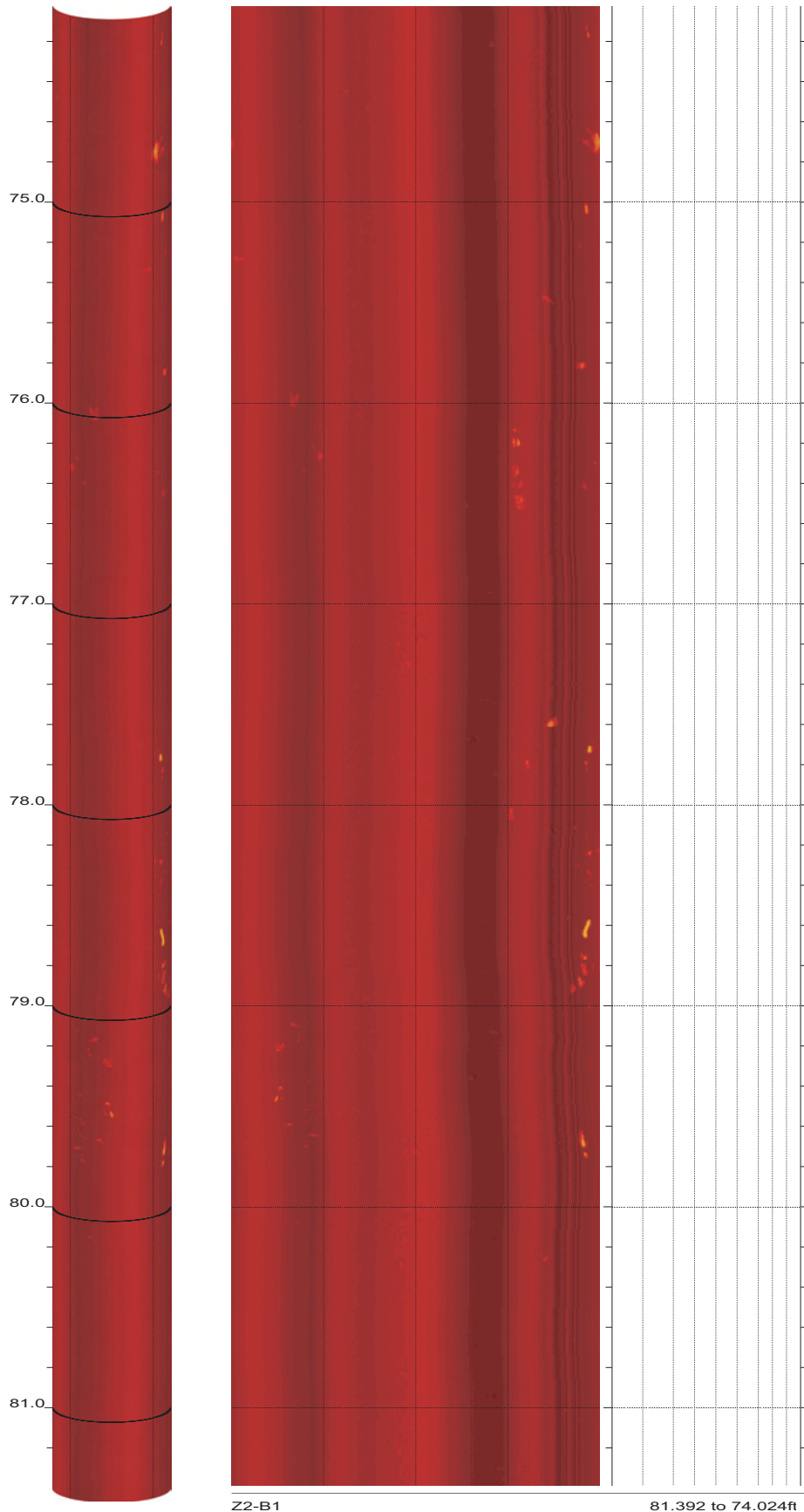
66.656 to 59.288ft

7

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 7 of 19



SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 8 of 19

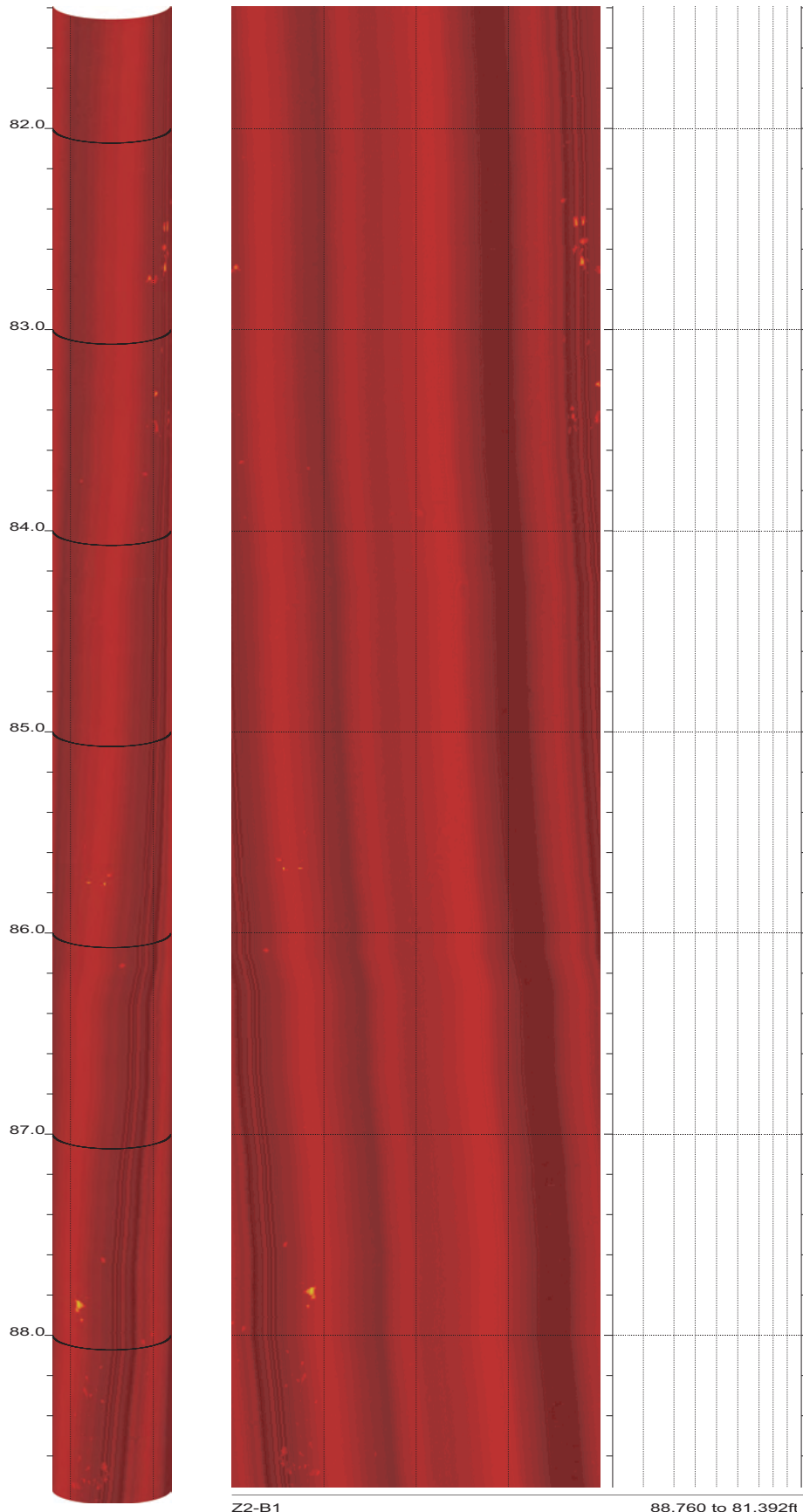


Z2-B1

81.392 to 74.024ft

9

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 9 of 19

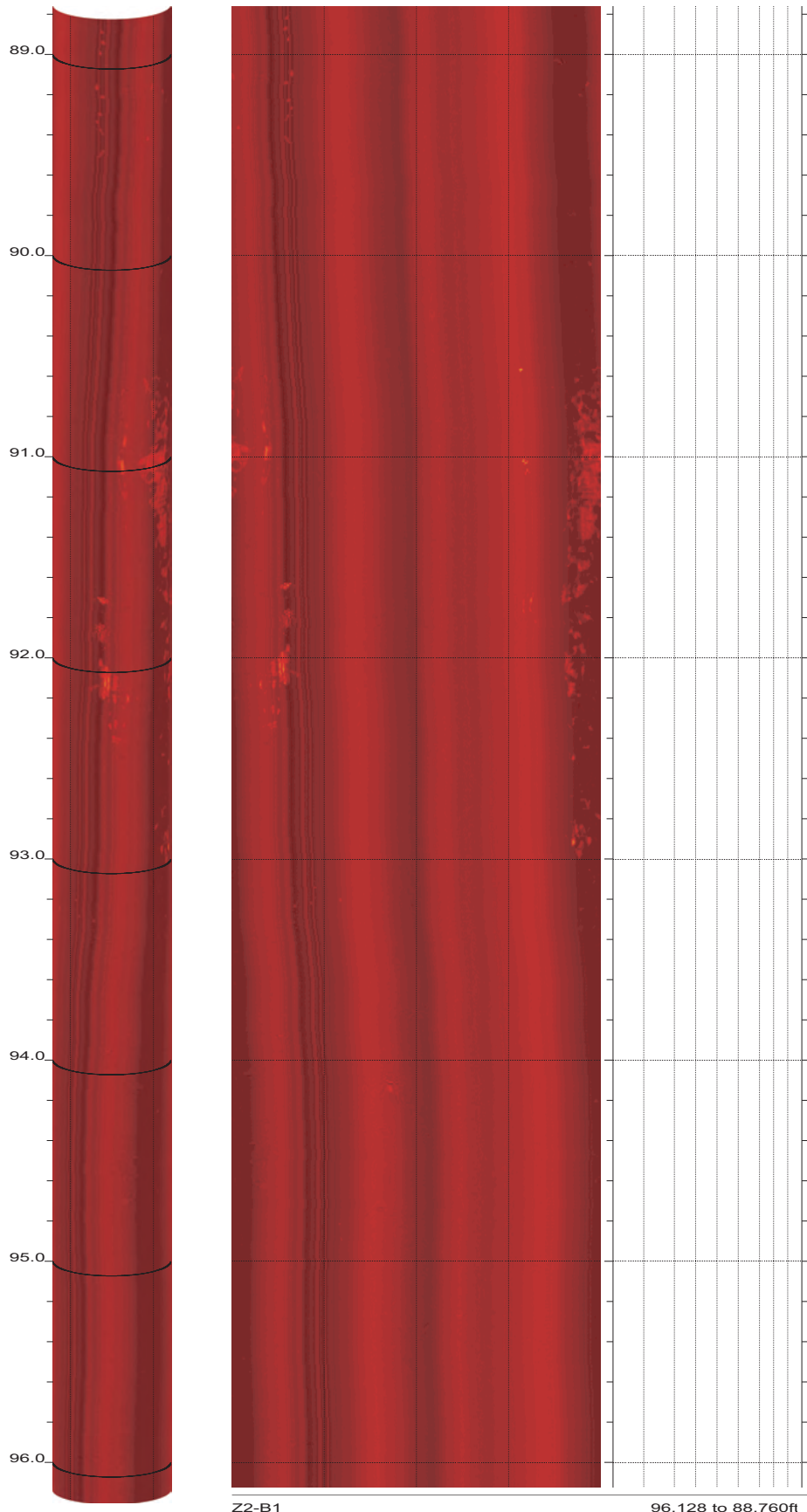


Z2-B1

88.760 to 81.392ft

10

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 10 of 19

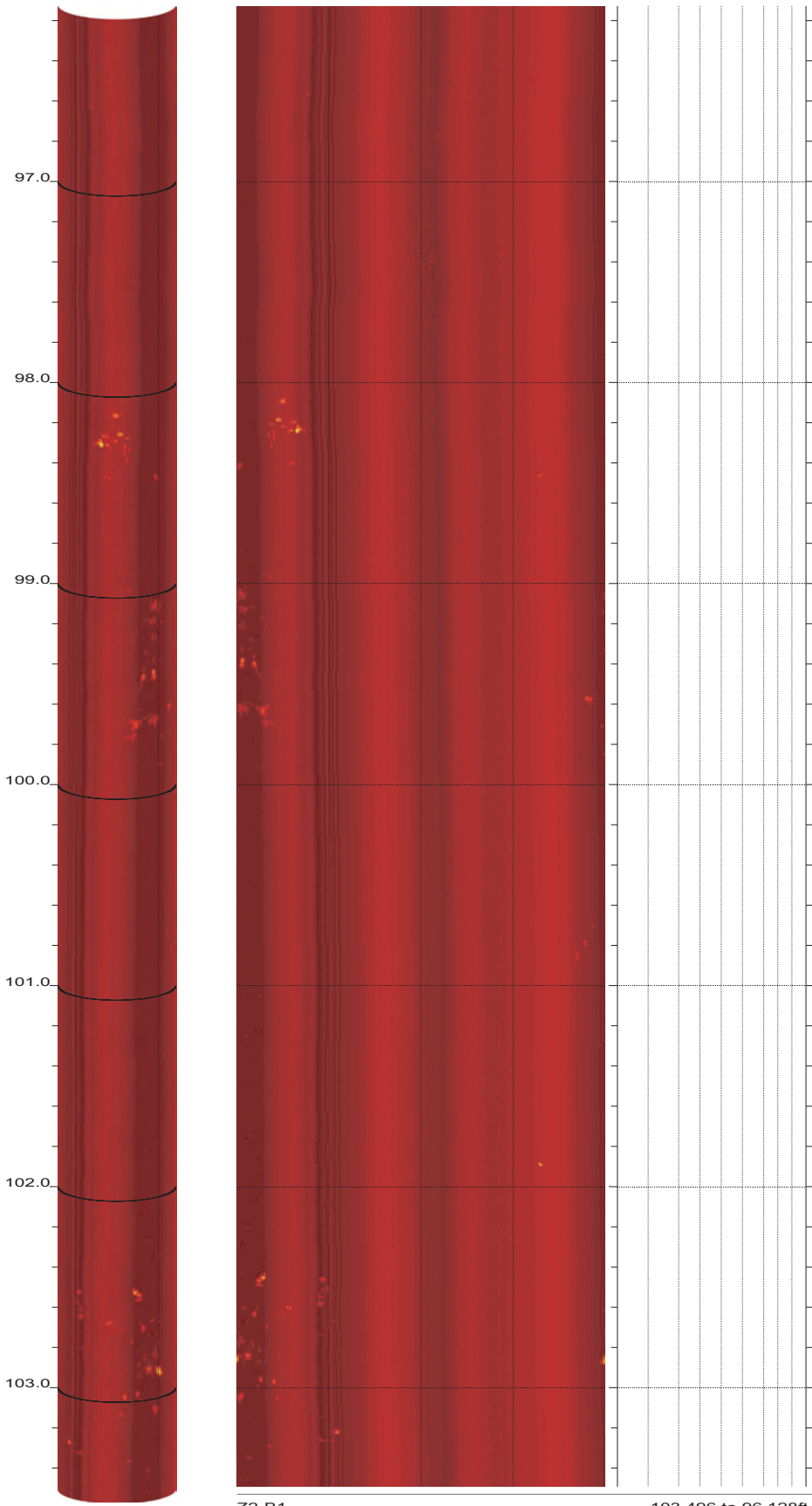


Z2-B1

96.128 to 88.760ft

11

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 11 of 19

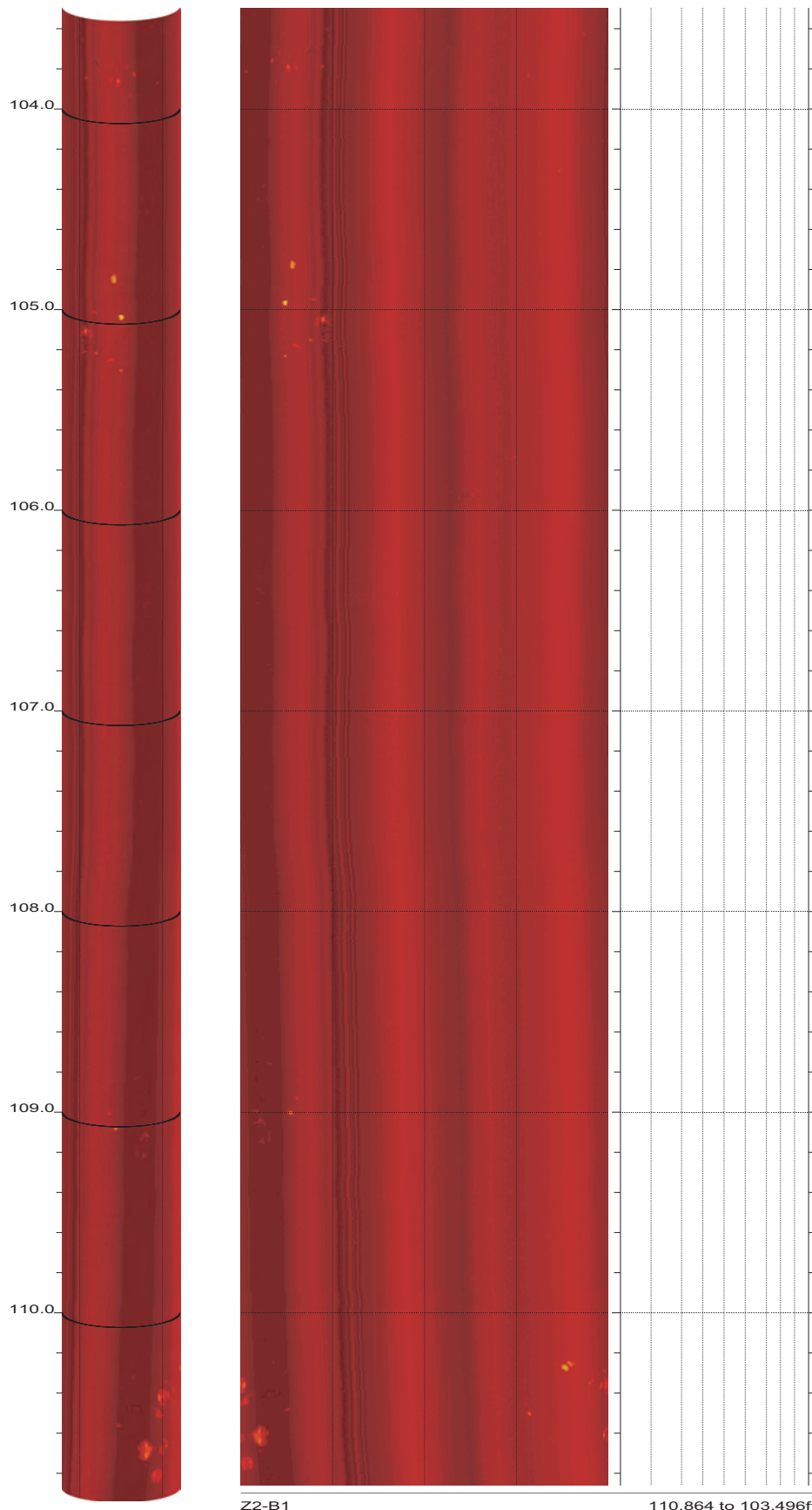


Z2-B1

103.496 to 96.128ft

12

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 12 of 19

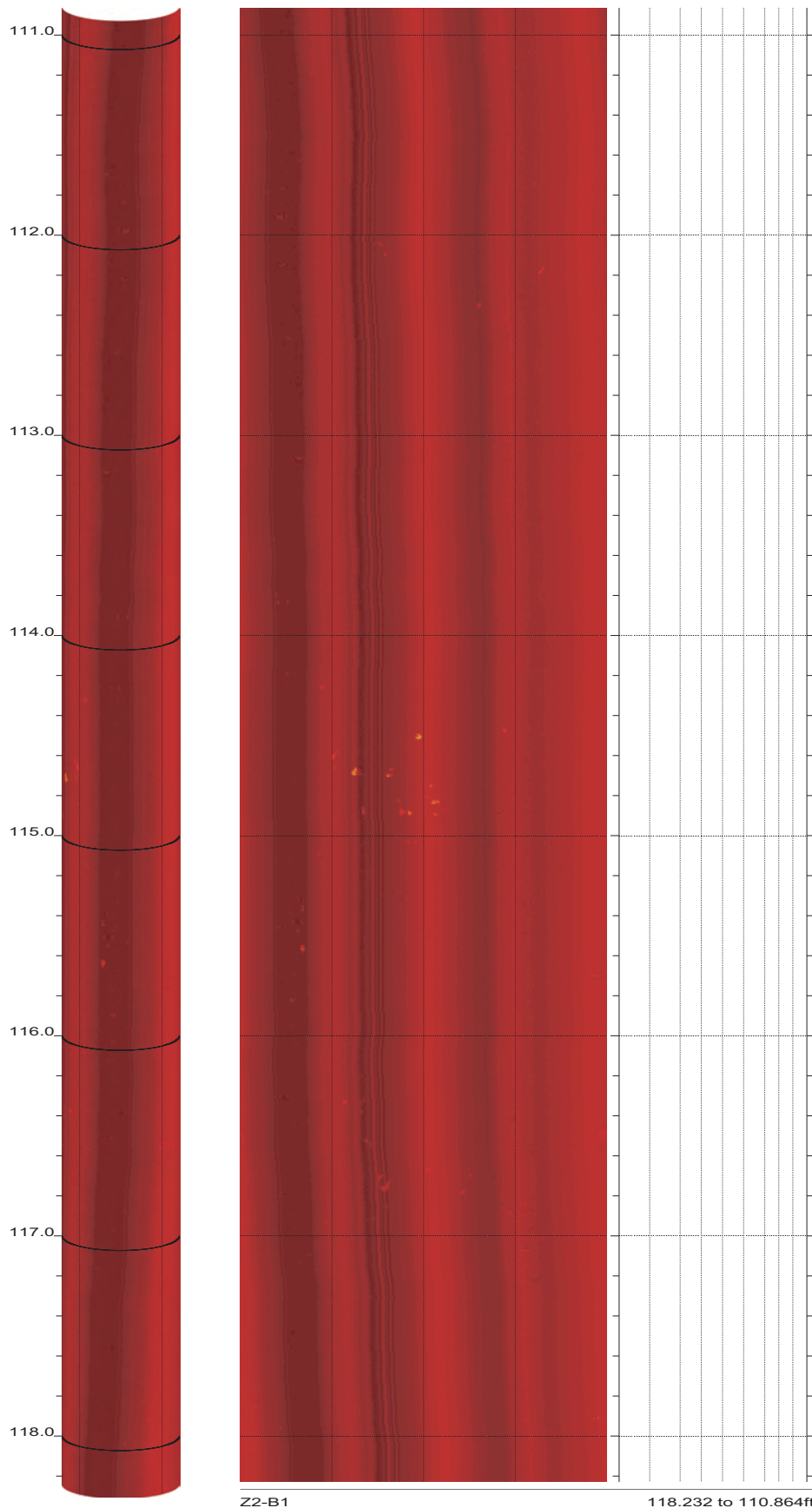


Z2-B1

110.864 to 103.496ft

13

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 13 of 19



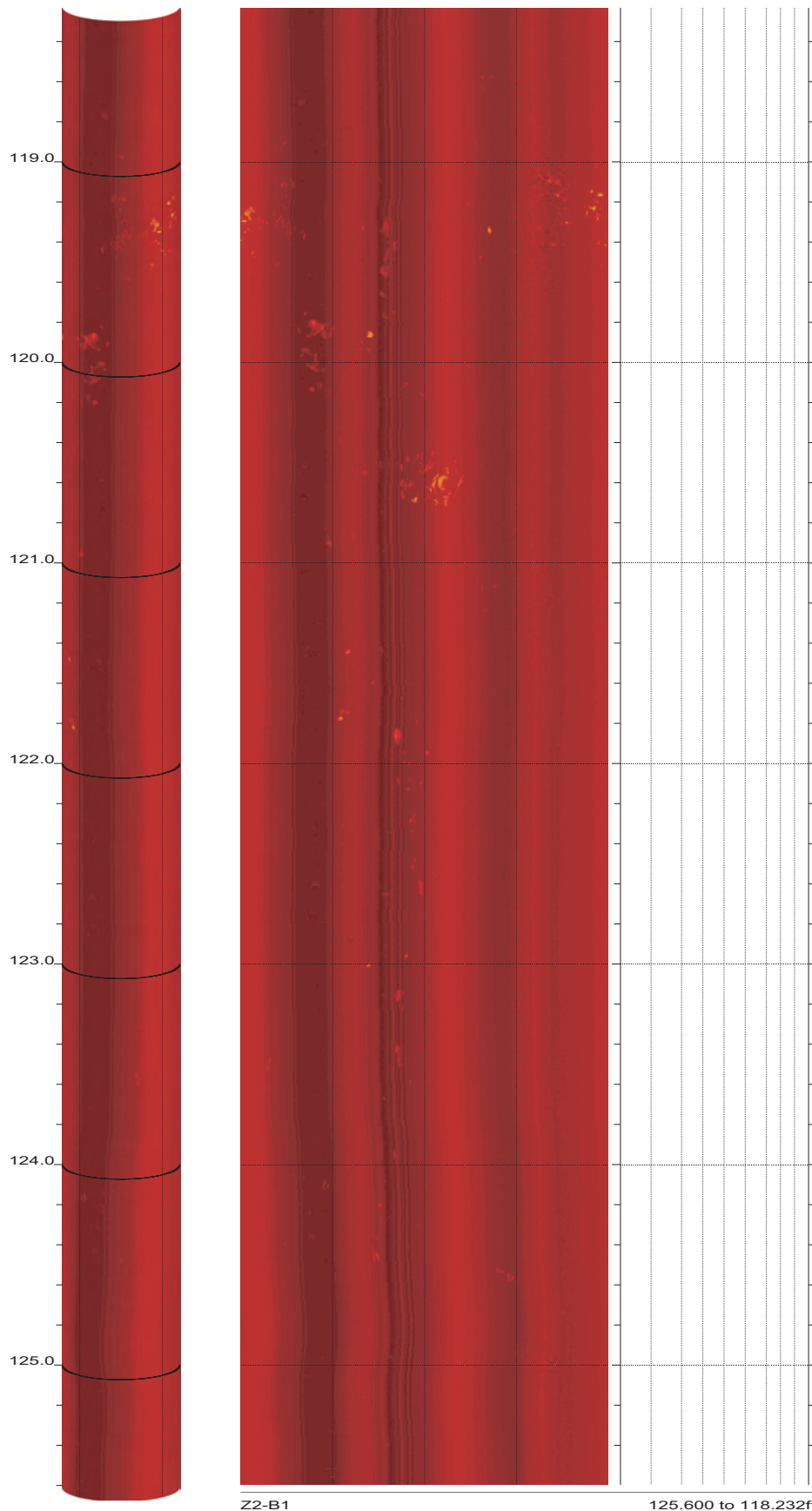
Z2-B1

118.232 to 110.864ft

14

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 14 of 19



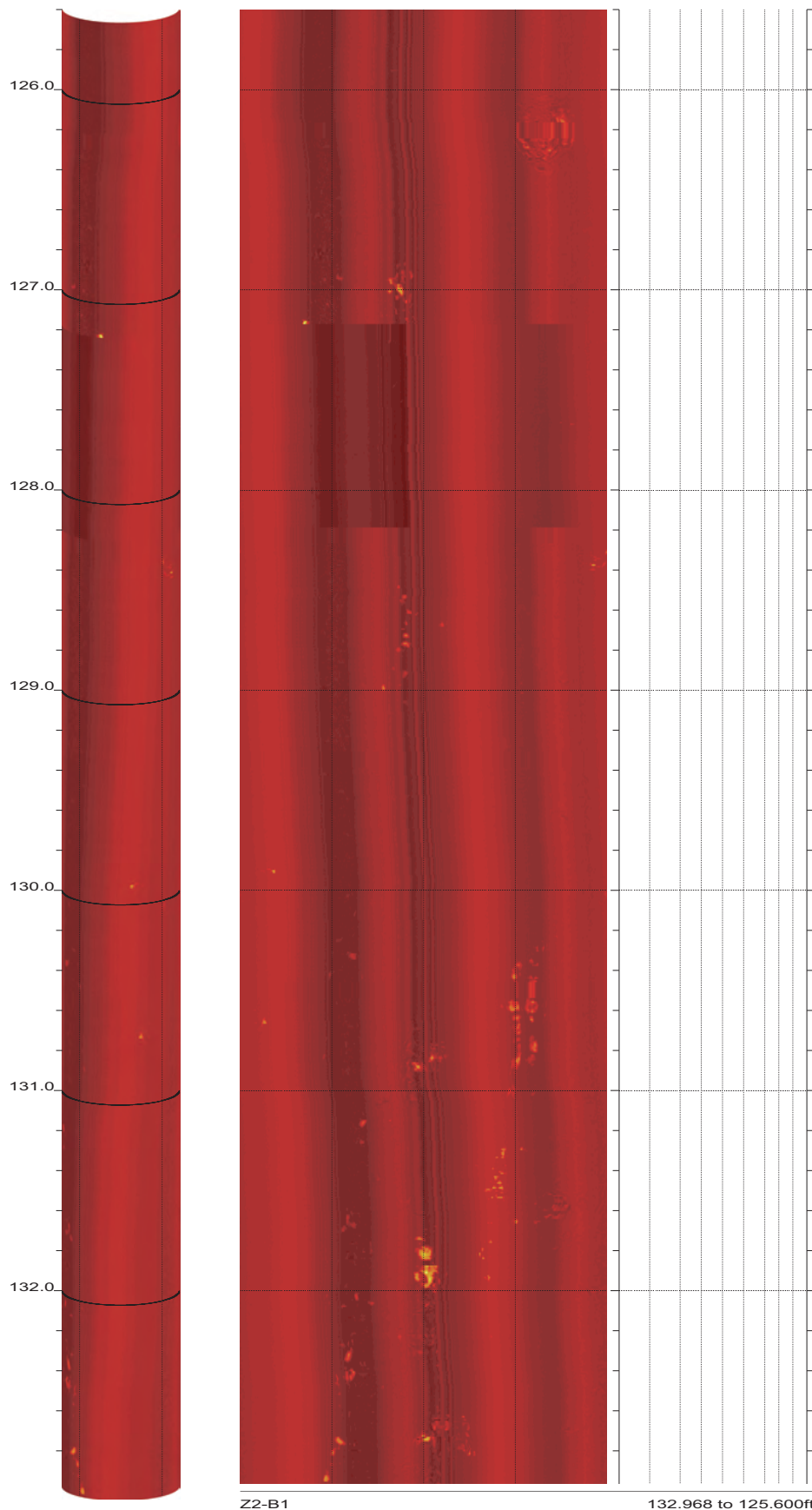


Z2-B1

125.600 to 118.232ft

15

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 15 of 19

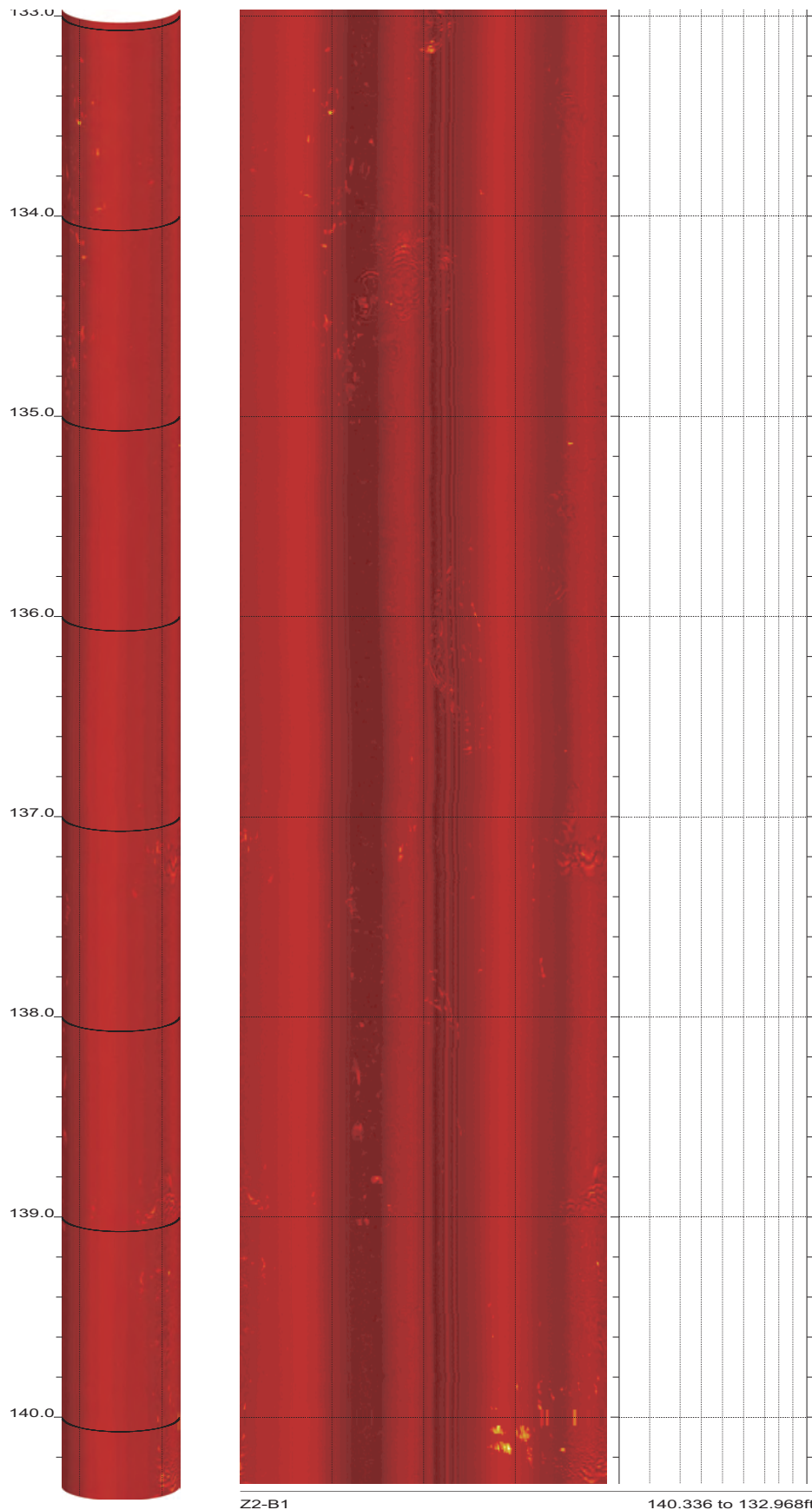


Z2-B1

132.968 to 125.600ft

16

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 16 of 19

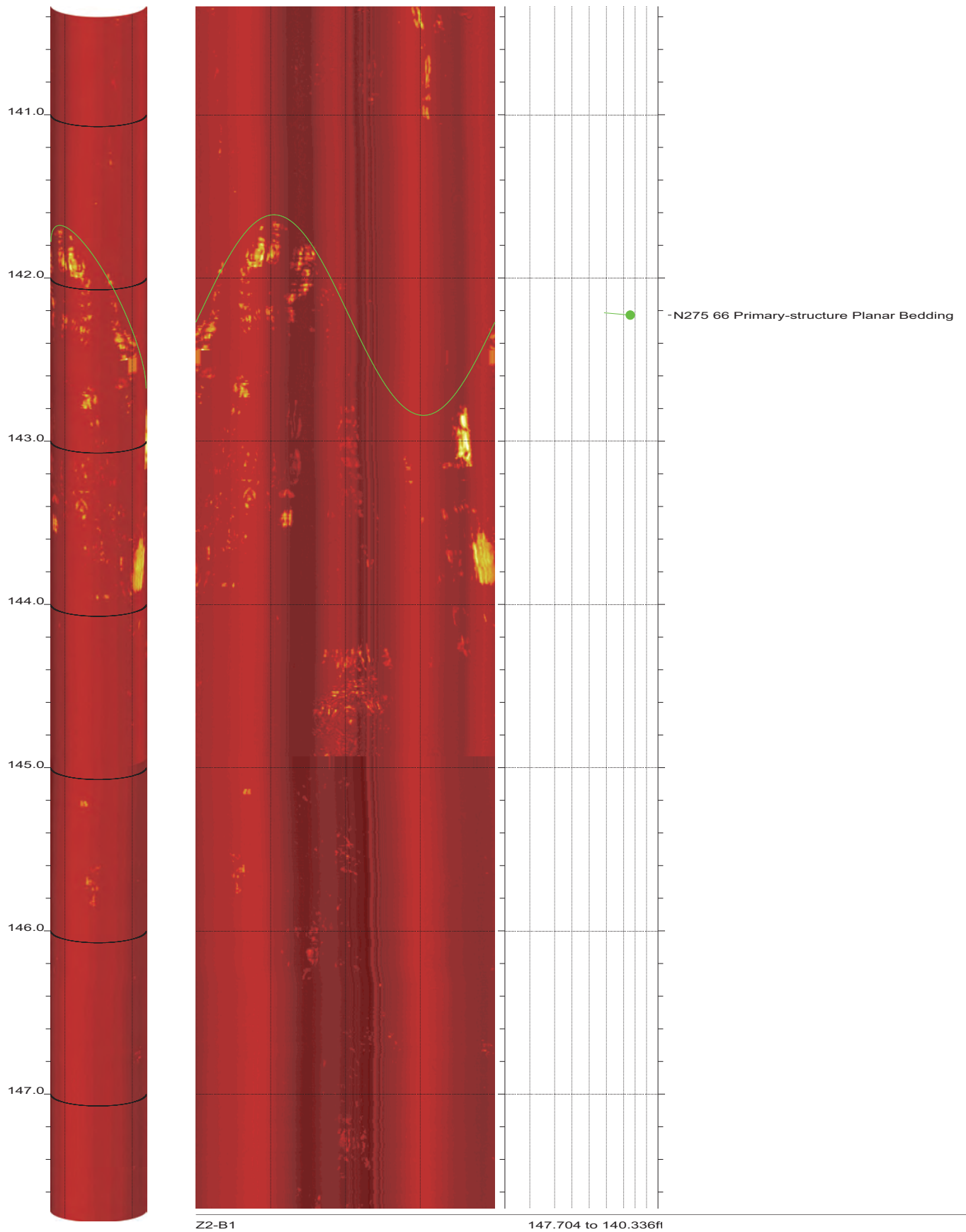


Z2-B1

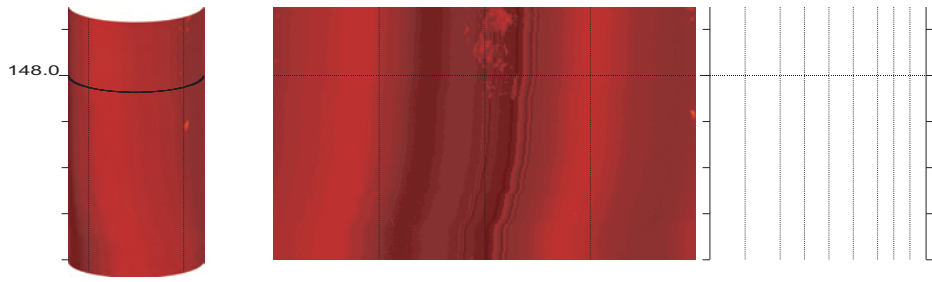
140.336 to 132.968ft

17

SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 17 of 19



SR-710 Boring Z2-B1 Acoustic Televiewer Dips rev 1 Sheet 18 of 19





CASCADE DRILLING

Borehole: Z2-B4

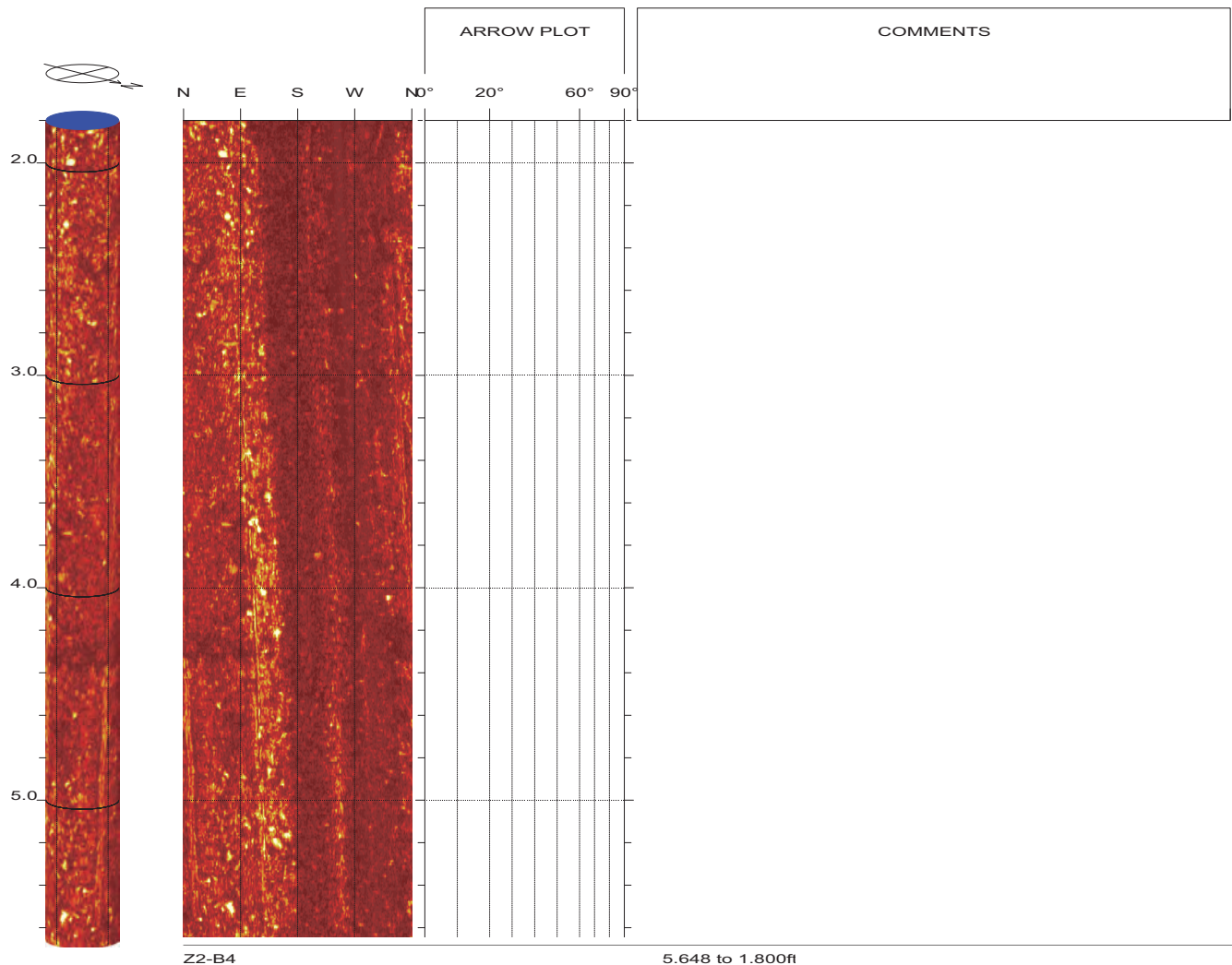
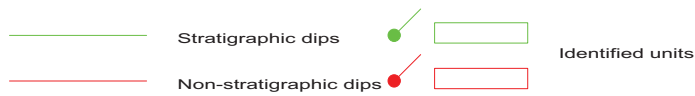
SR-710 TUNNEL INVESTIGATION

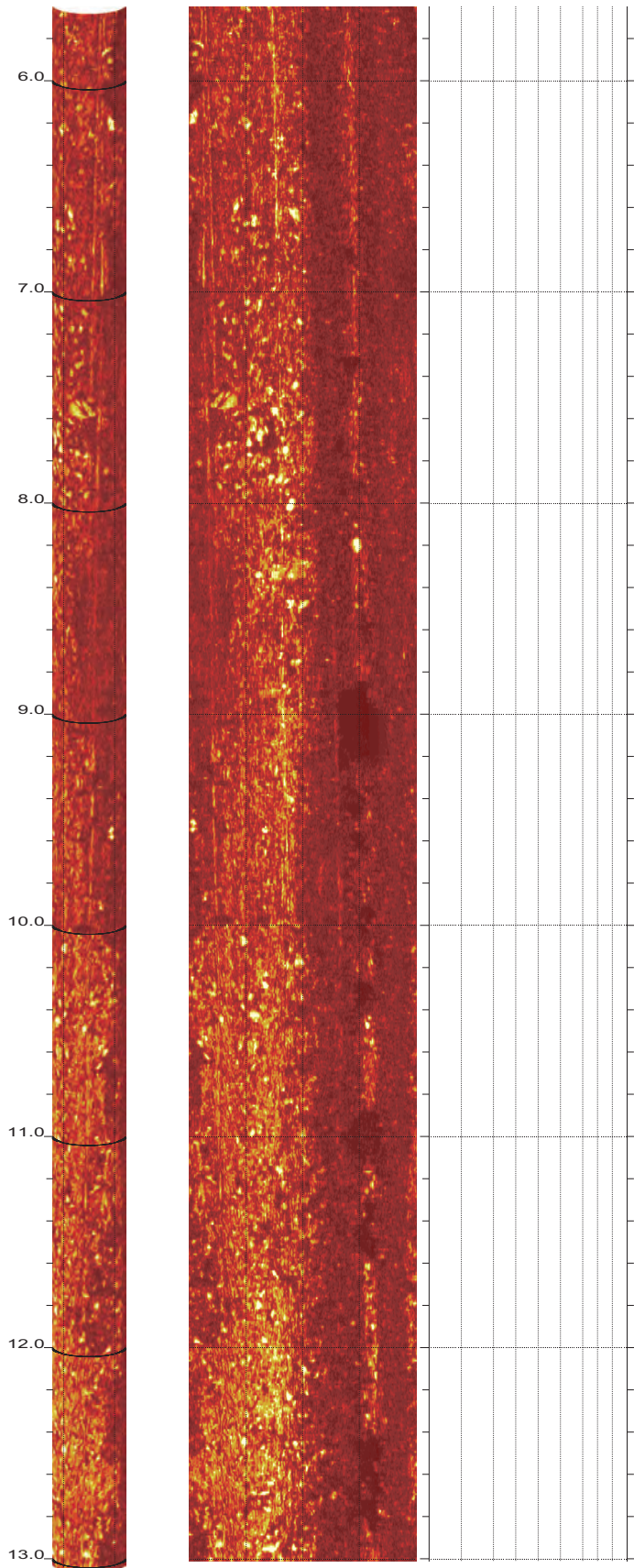
top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

Zone from 374.600 to 1.800ft  
 Format: BHTV-NESWN

Borehole diam: 4.100inch  
 Vertical = borehole-axis  
 Image: Amplitude

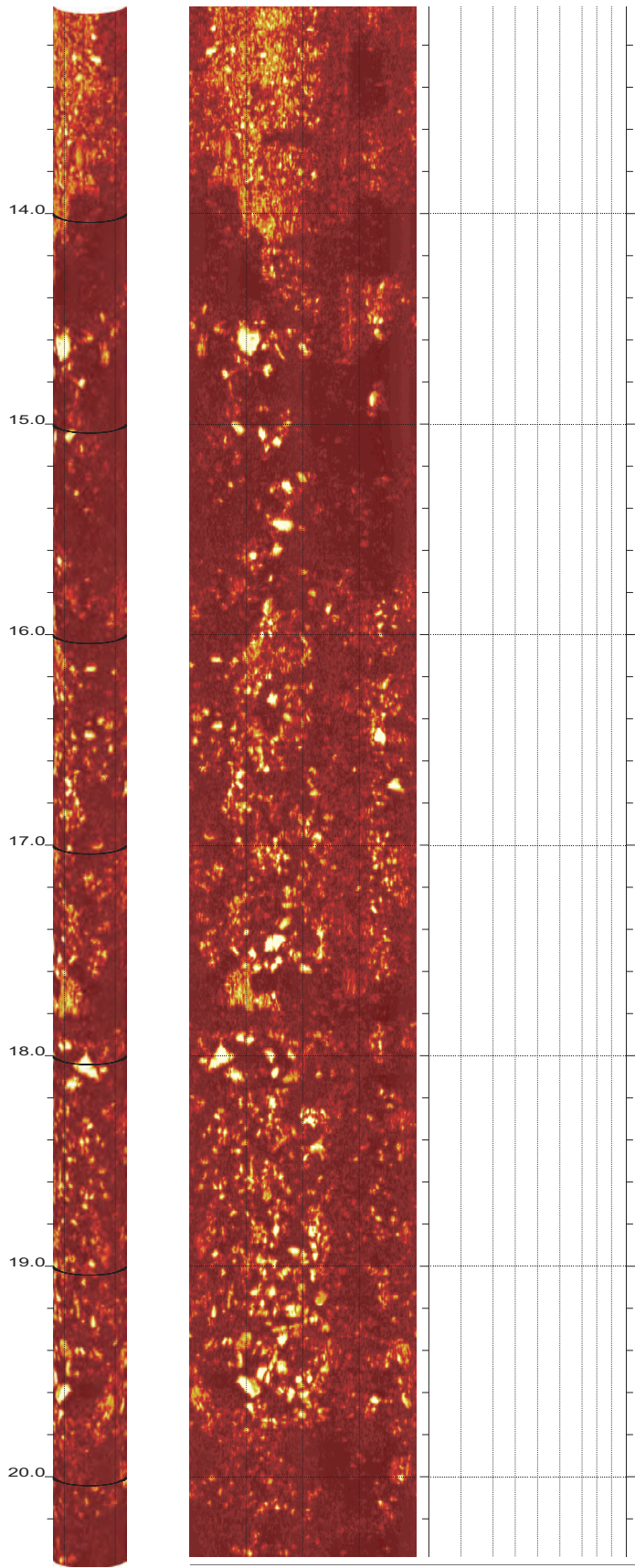




Z2-B4

13.016 to 5.648ft

2

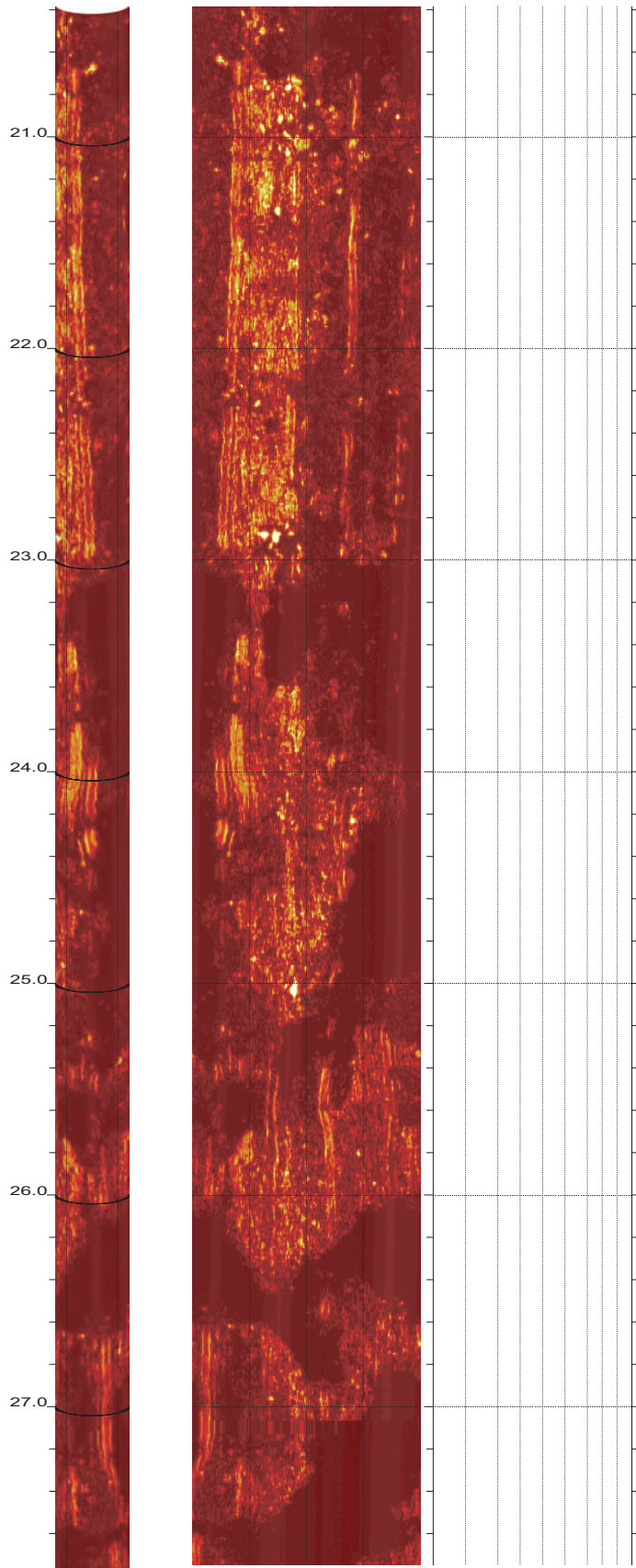


Z2-B4

20.384 to 13.016ft

3

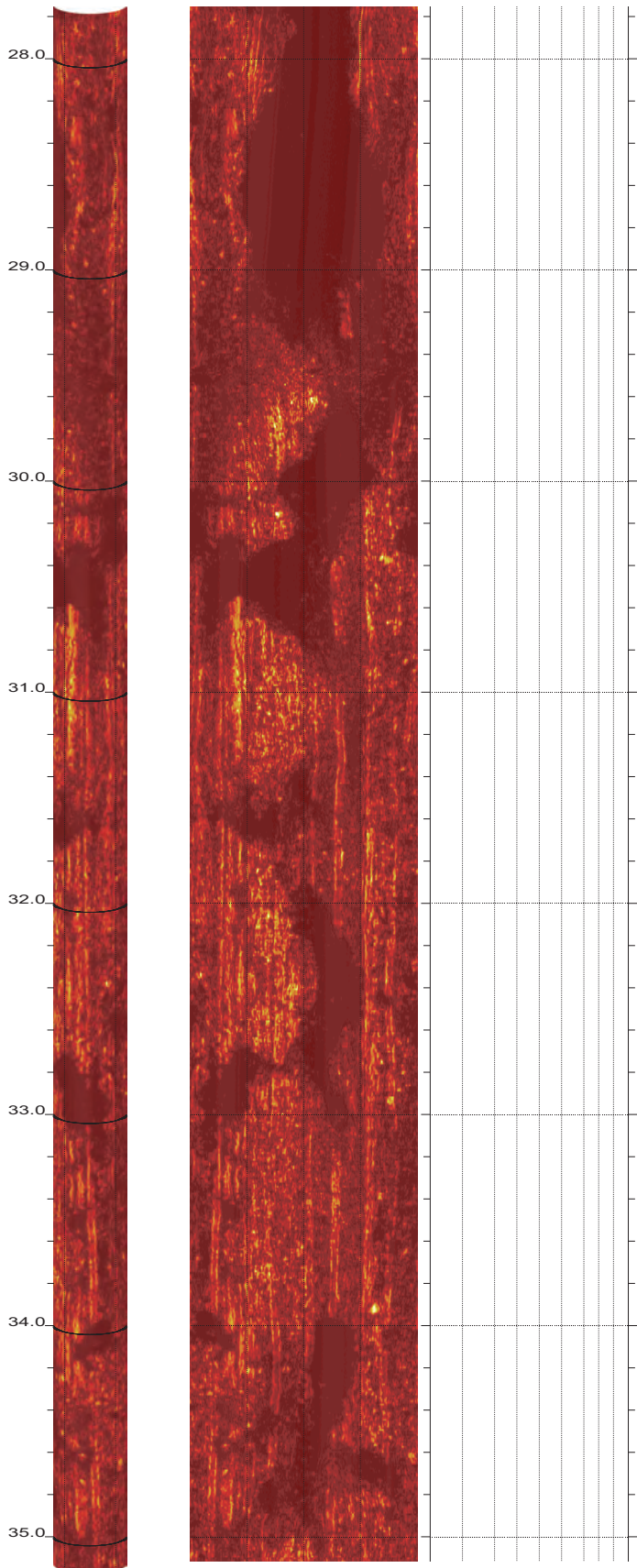




Z2-B4

27.752 to 20.384ft

4

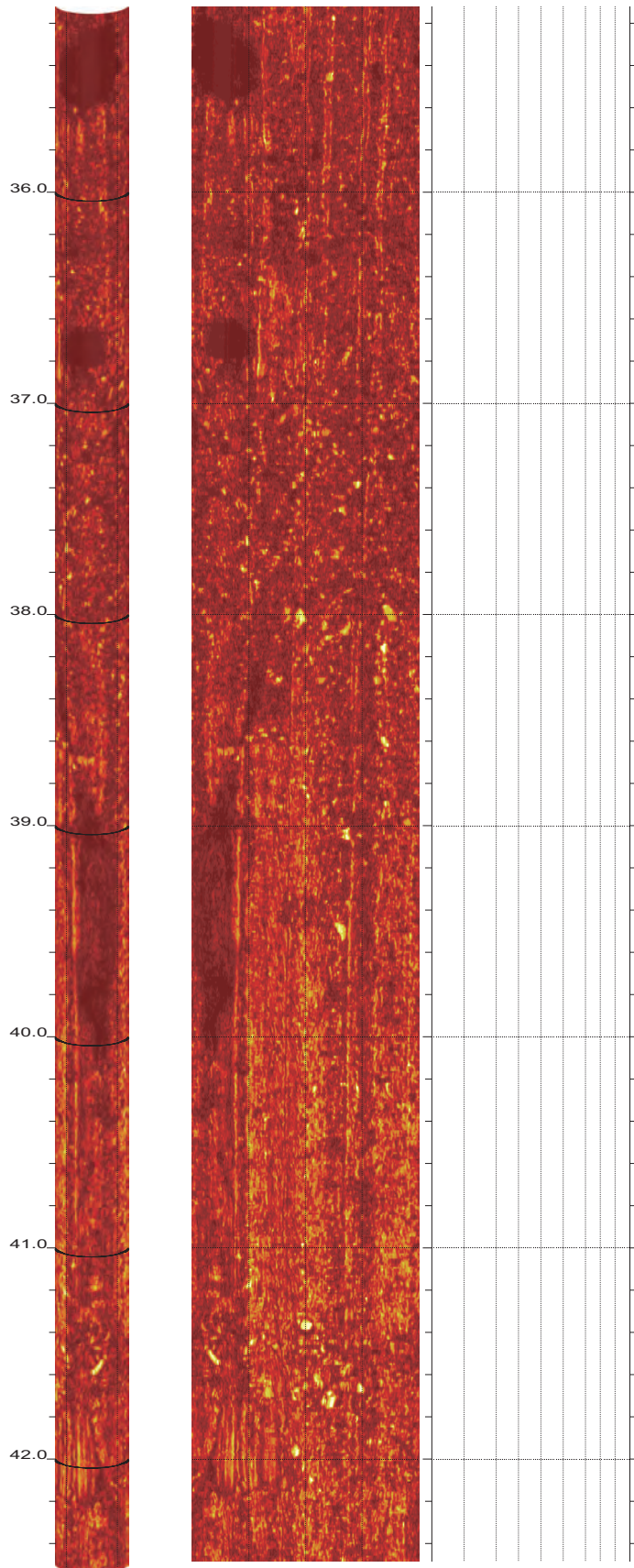


Z2-B4

35.120 to 27.752ft

5

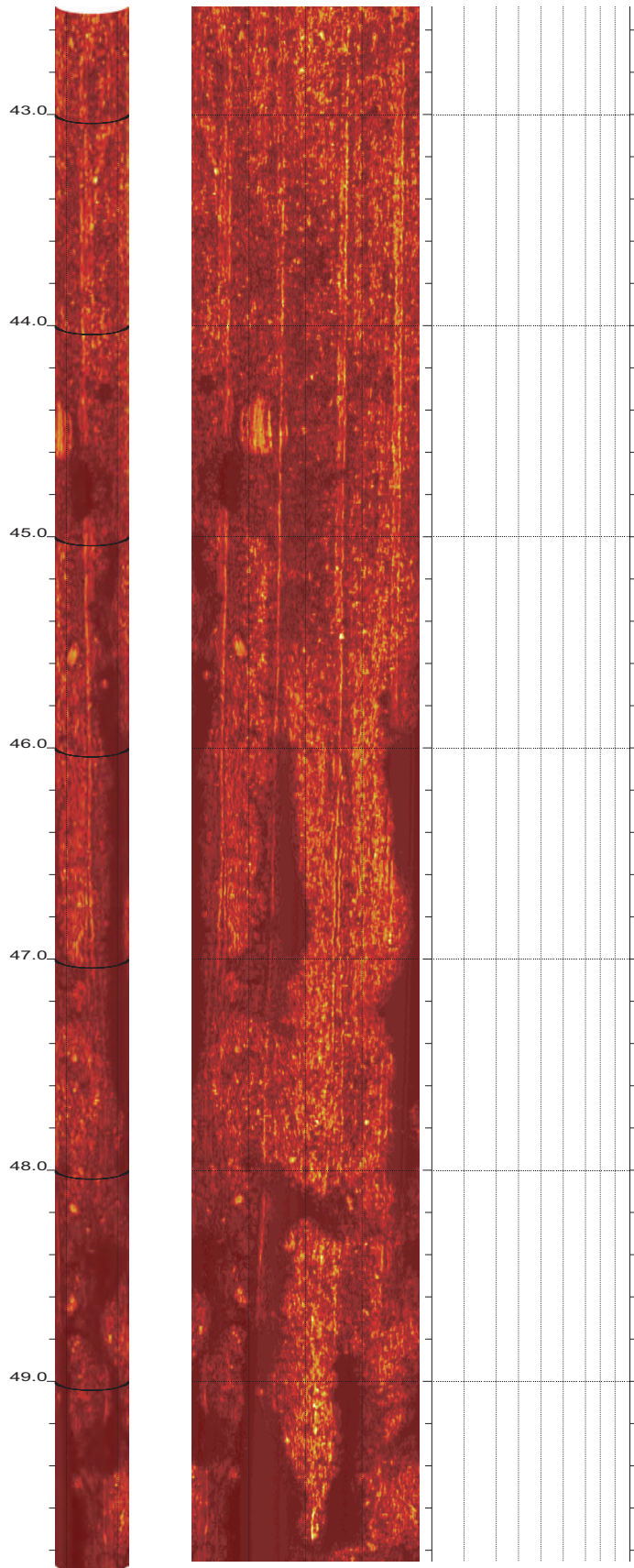
SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 5 of 52



Z2-B4

42.488 to 35.120ft

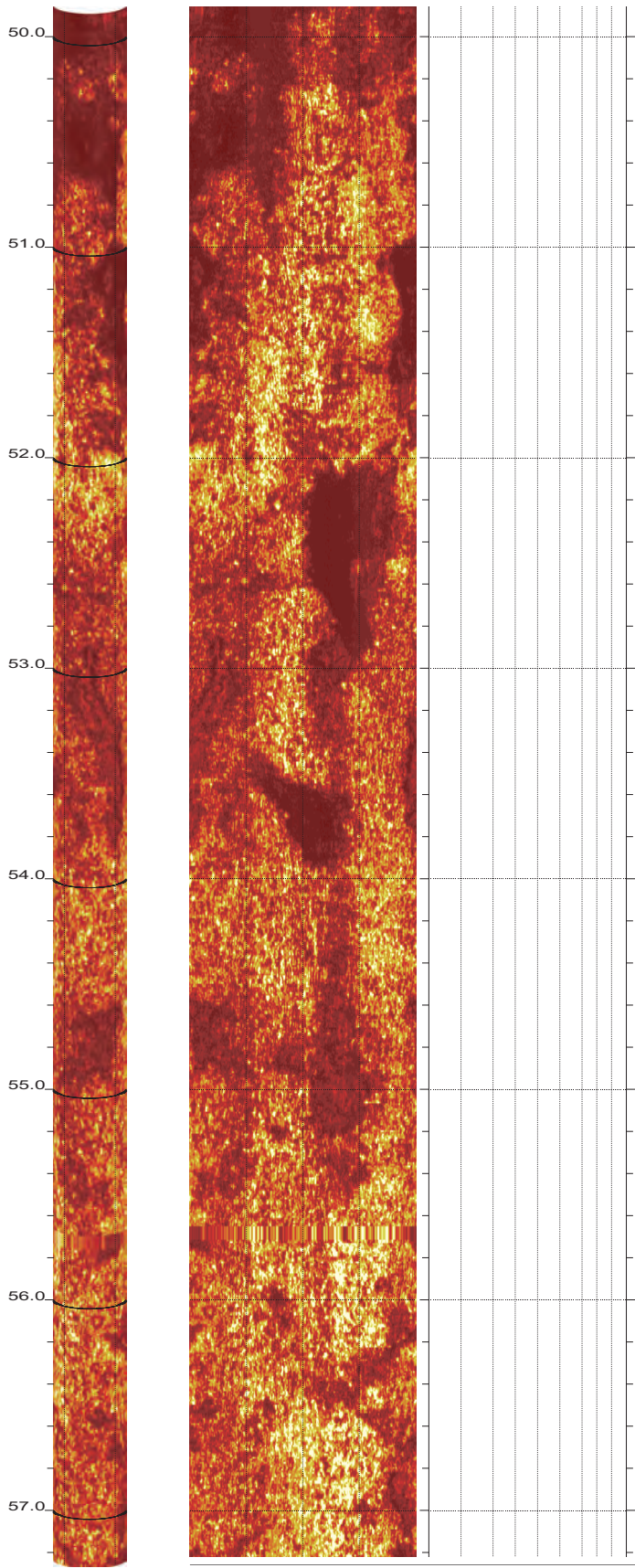
6



Z2-B4

49.856 to 42.488ft

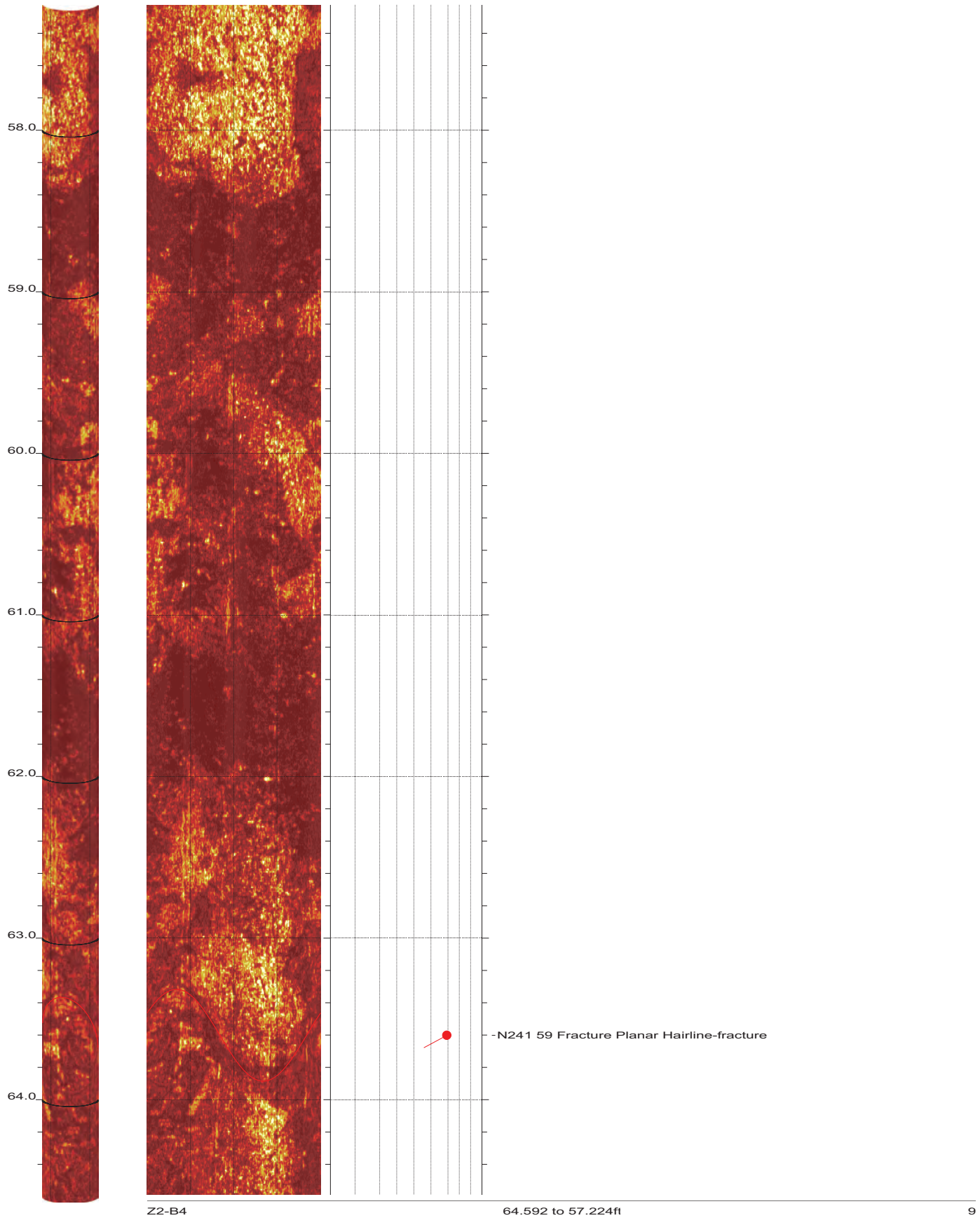
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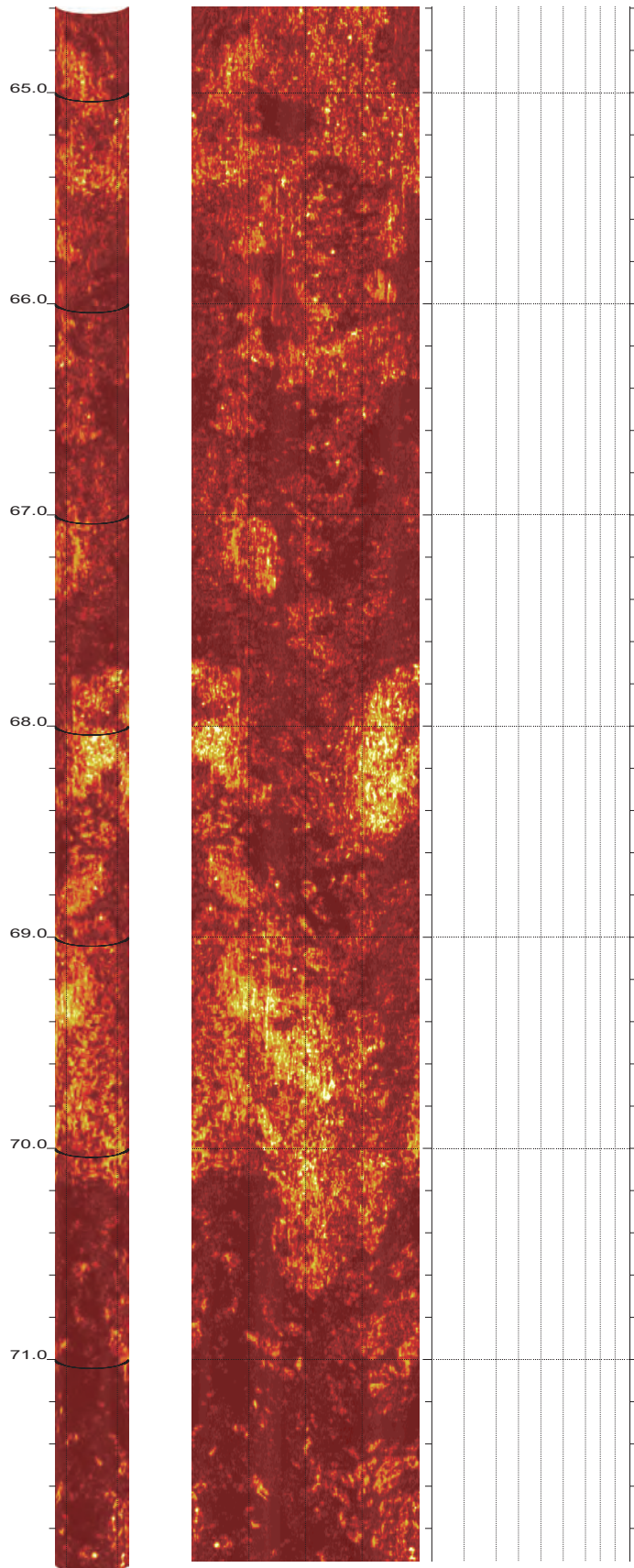


Z2-B4

57.224 to 49.856ft

8

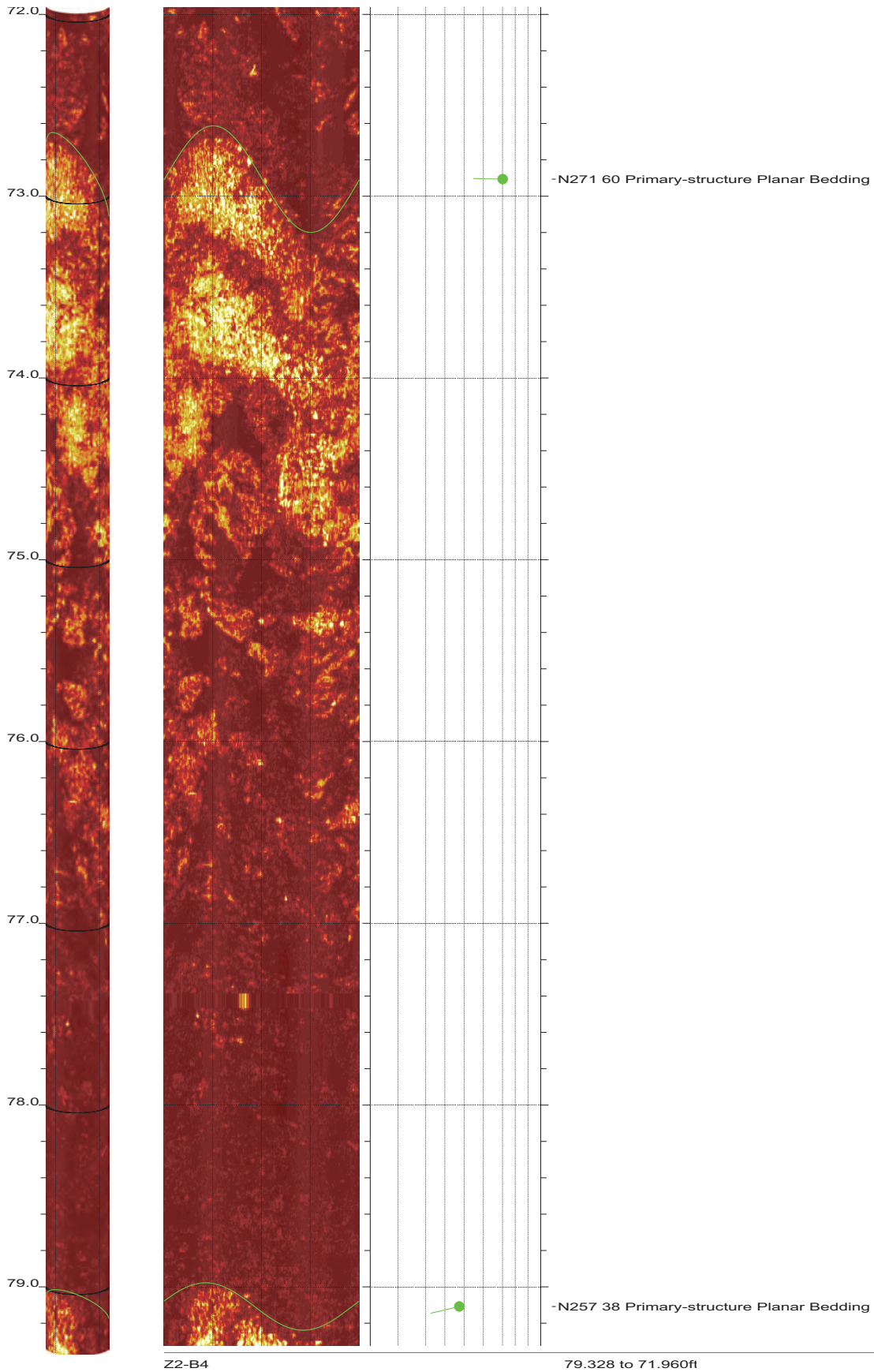




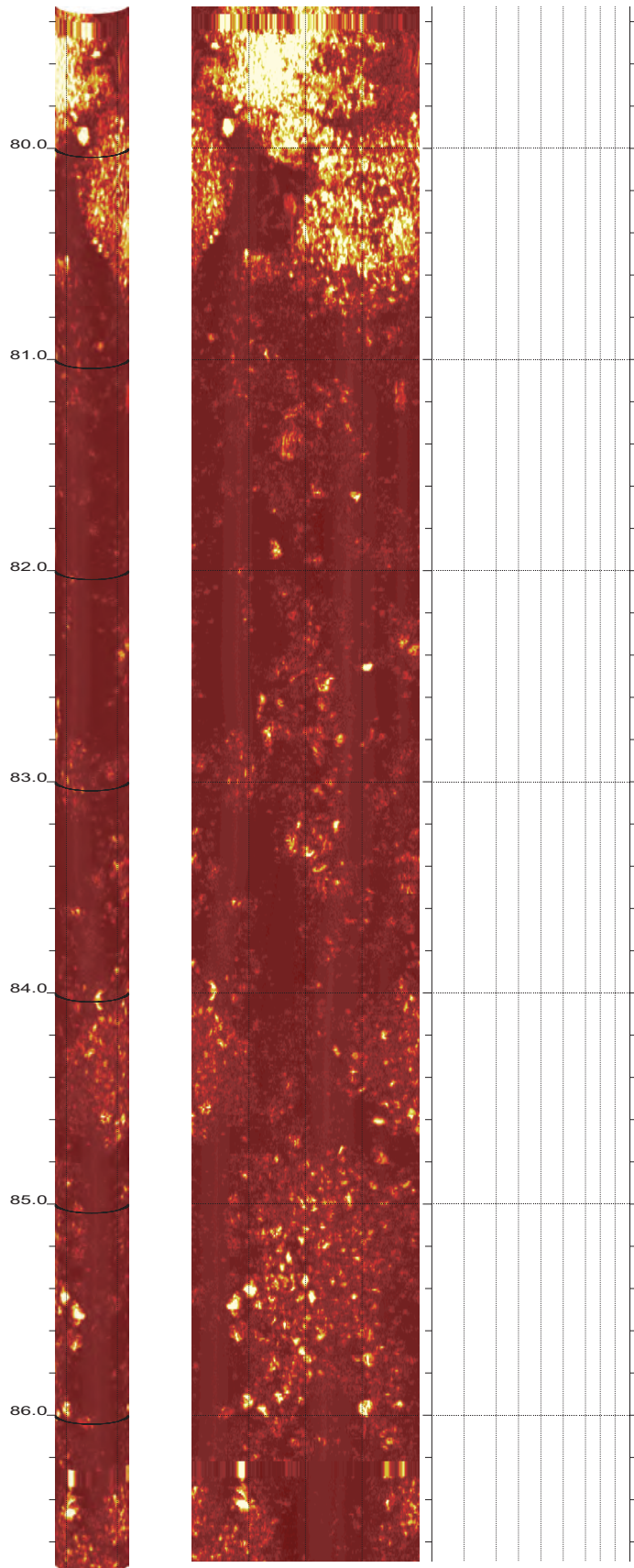
Z2-B4

71.960 to 64.592ft

10



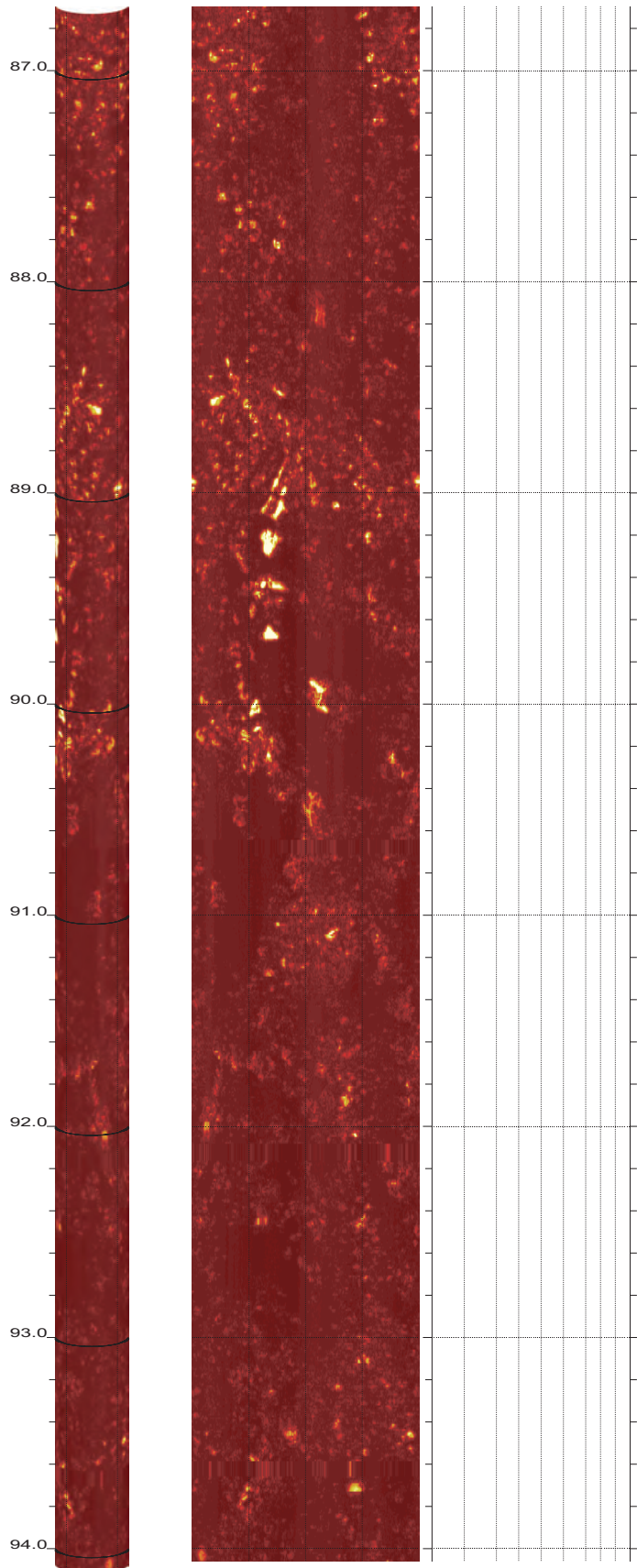




Z2-B4

86.696 to 79.328ft

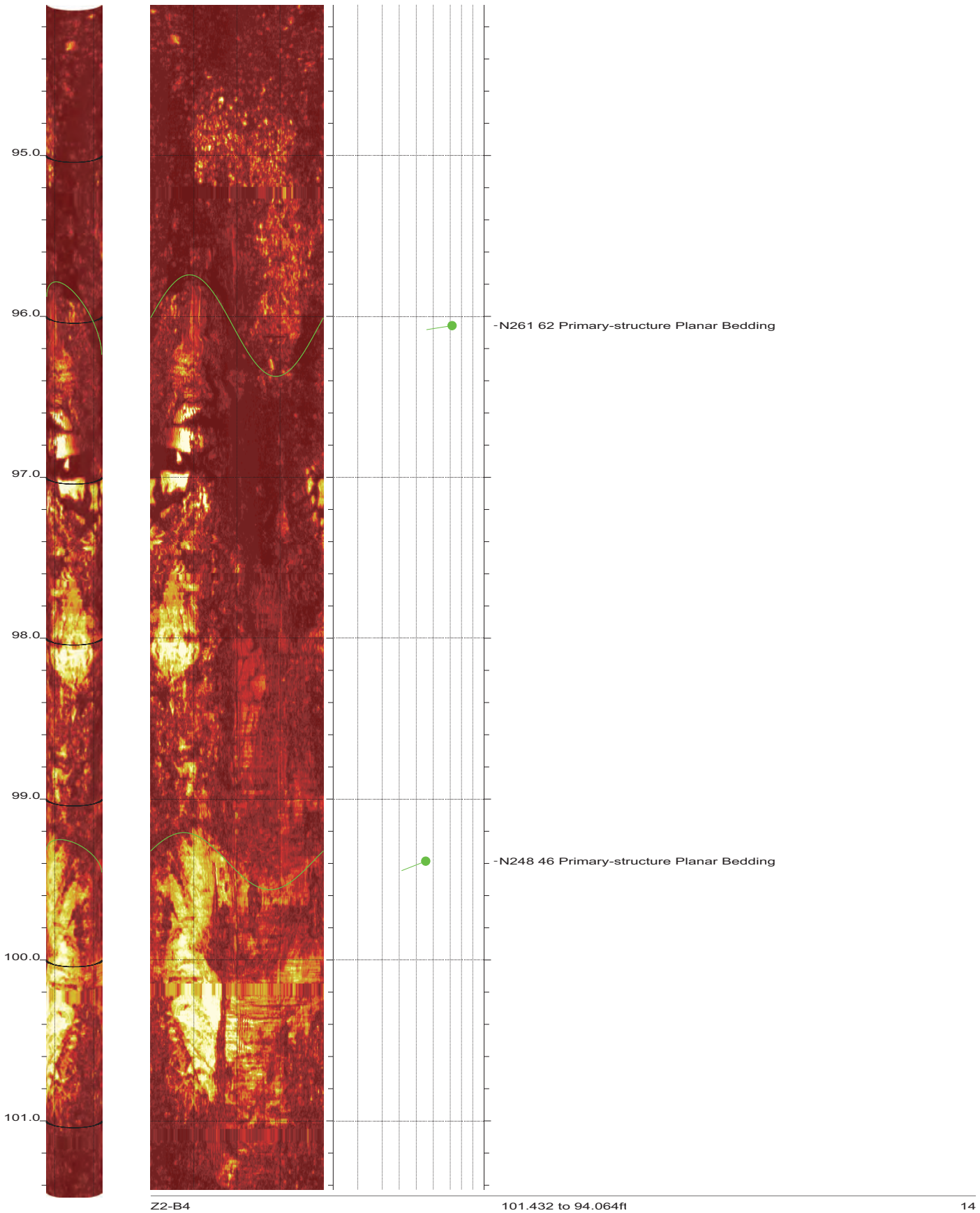
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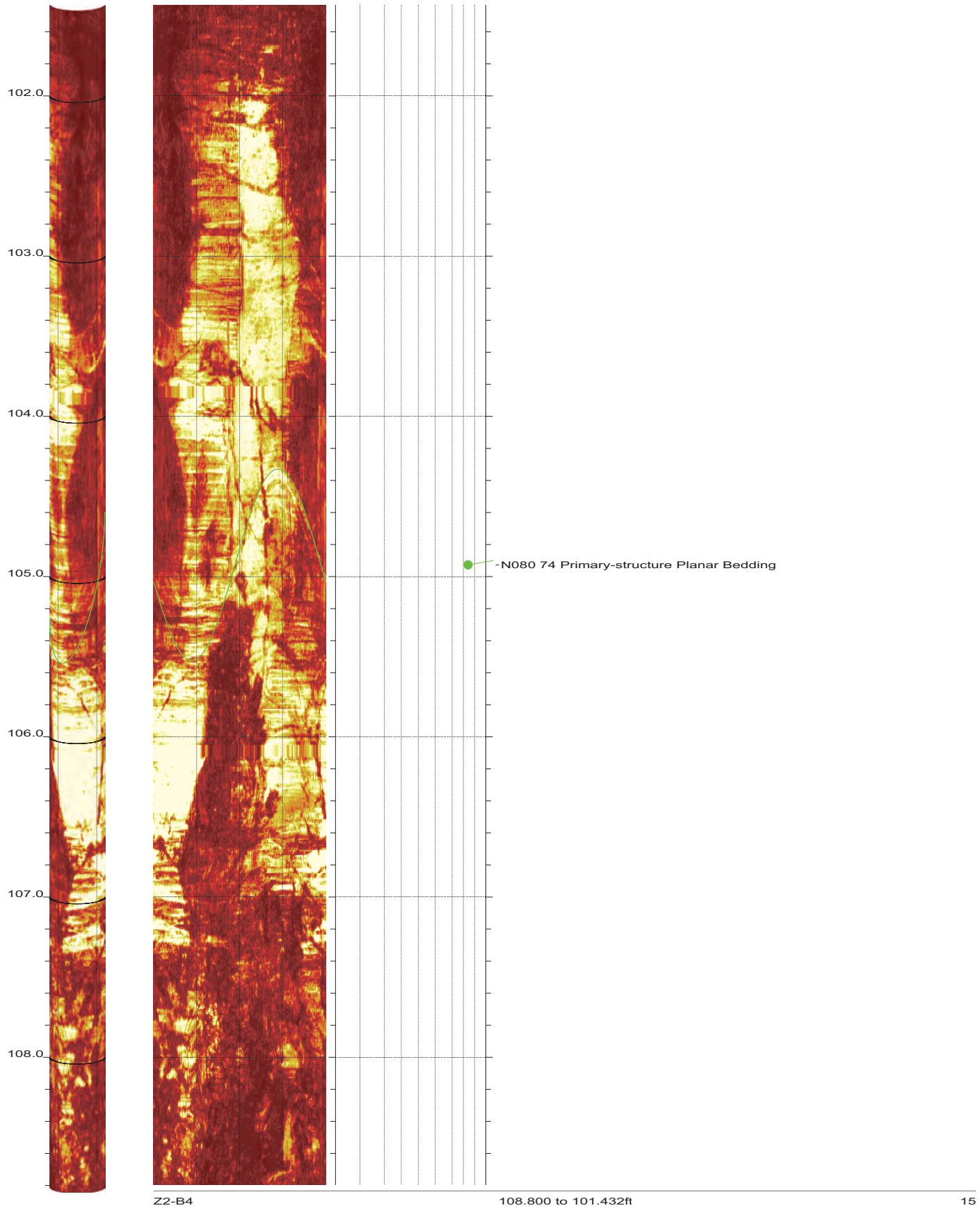
Z2-B4

94.064 to 86.696ft

13



SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 14 of 52

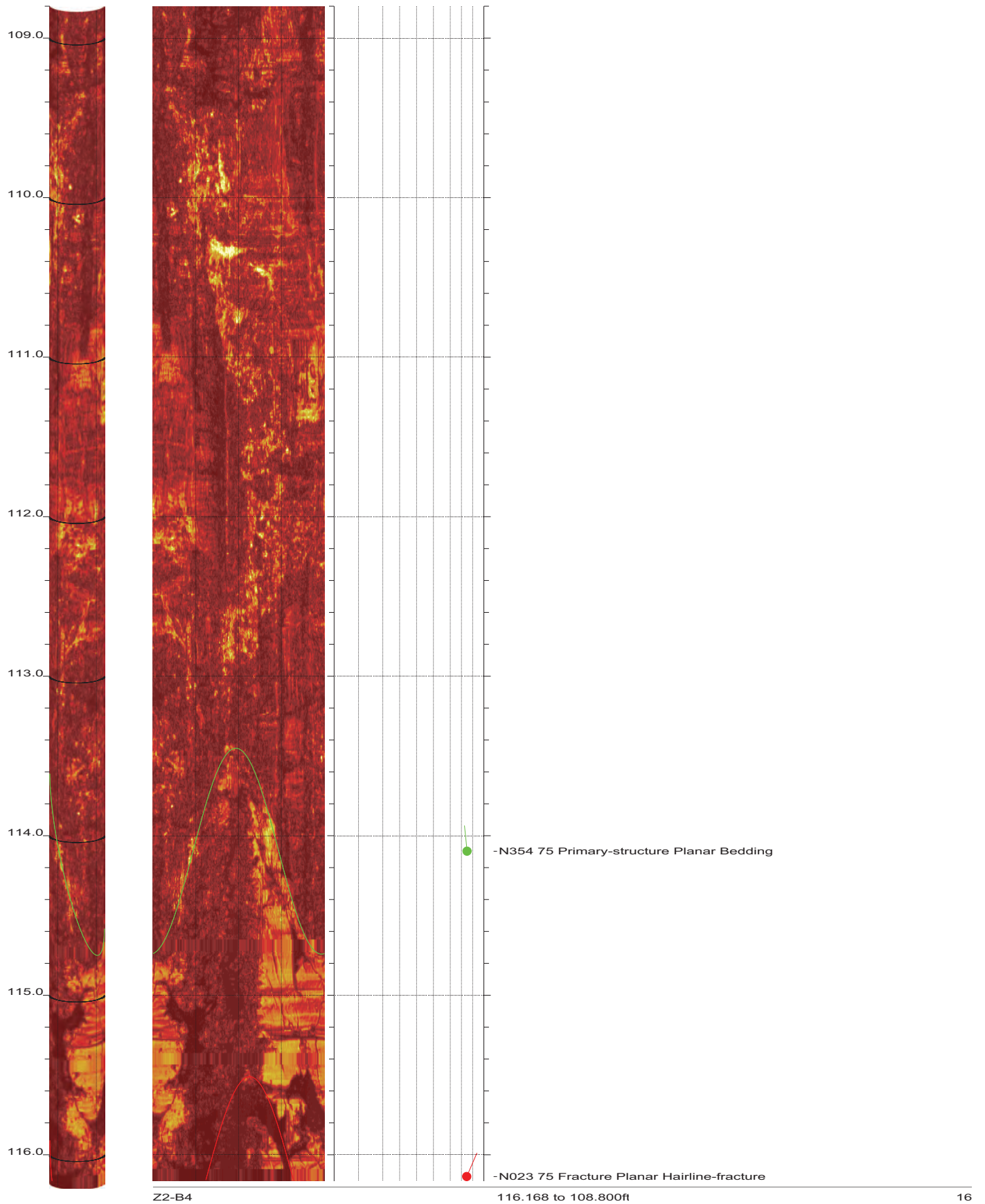


Z2-B4

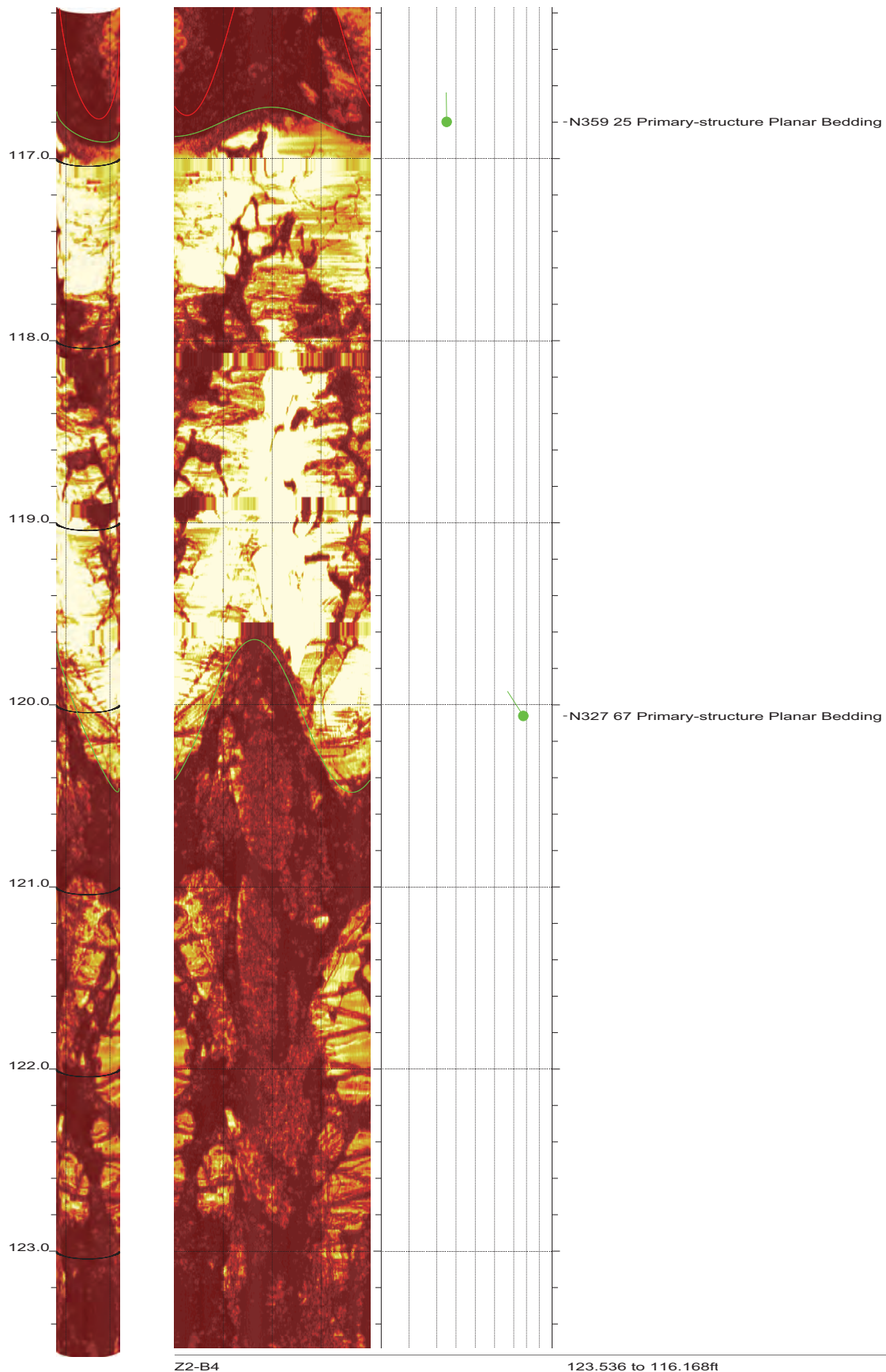
108.800 to 101.432ft

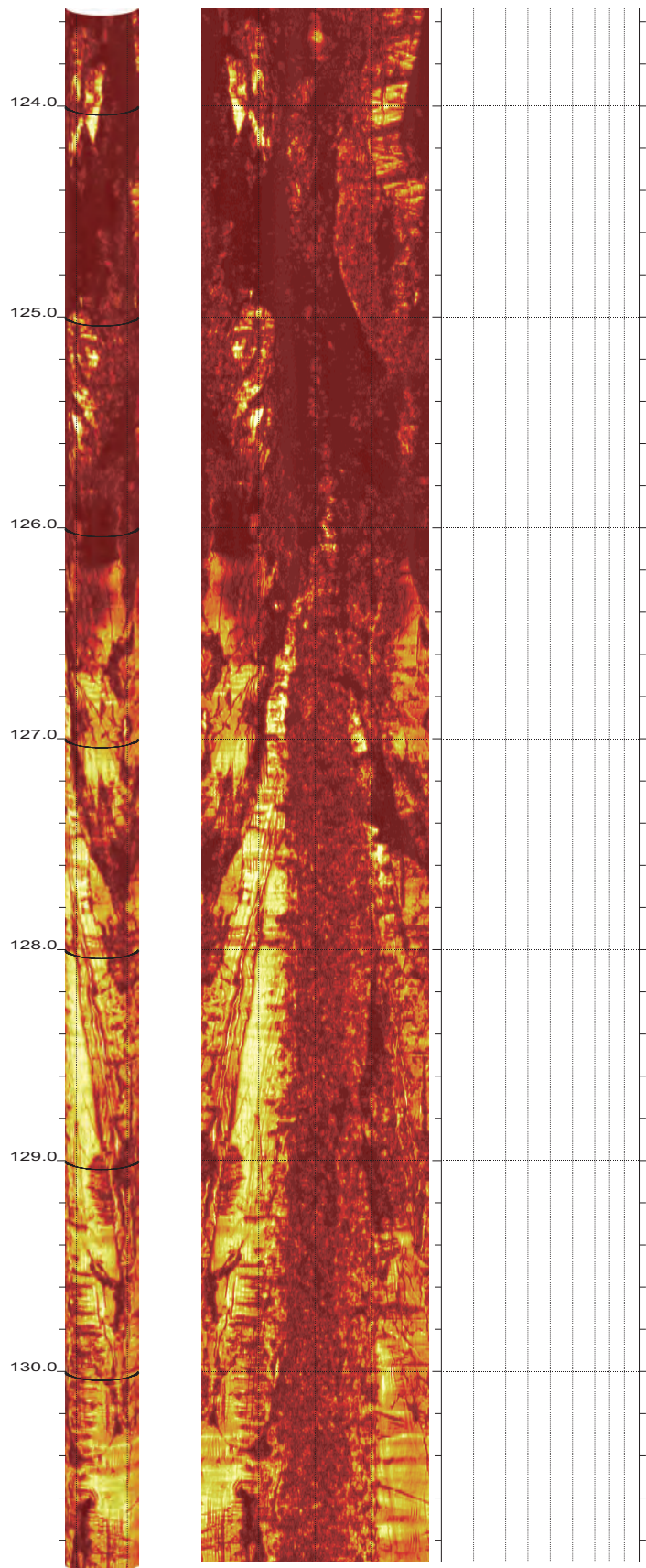
15

SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 15 of 52



SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 16 of 52



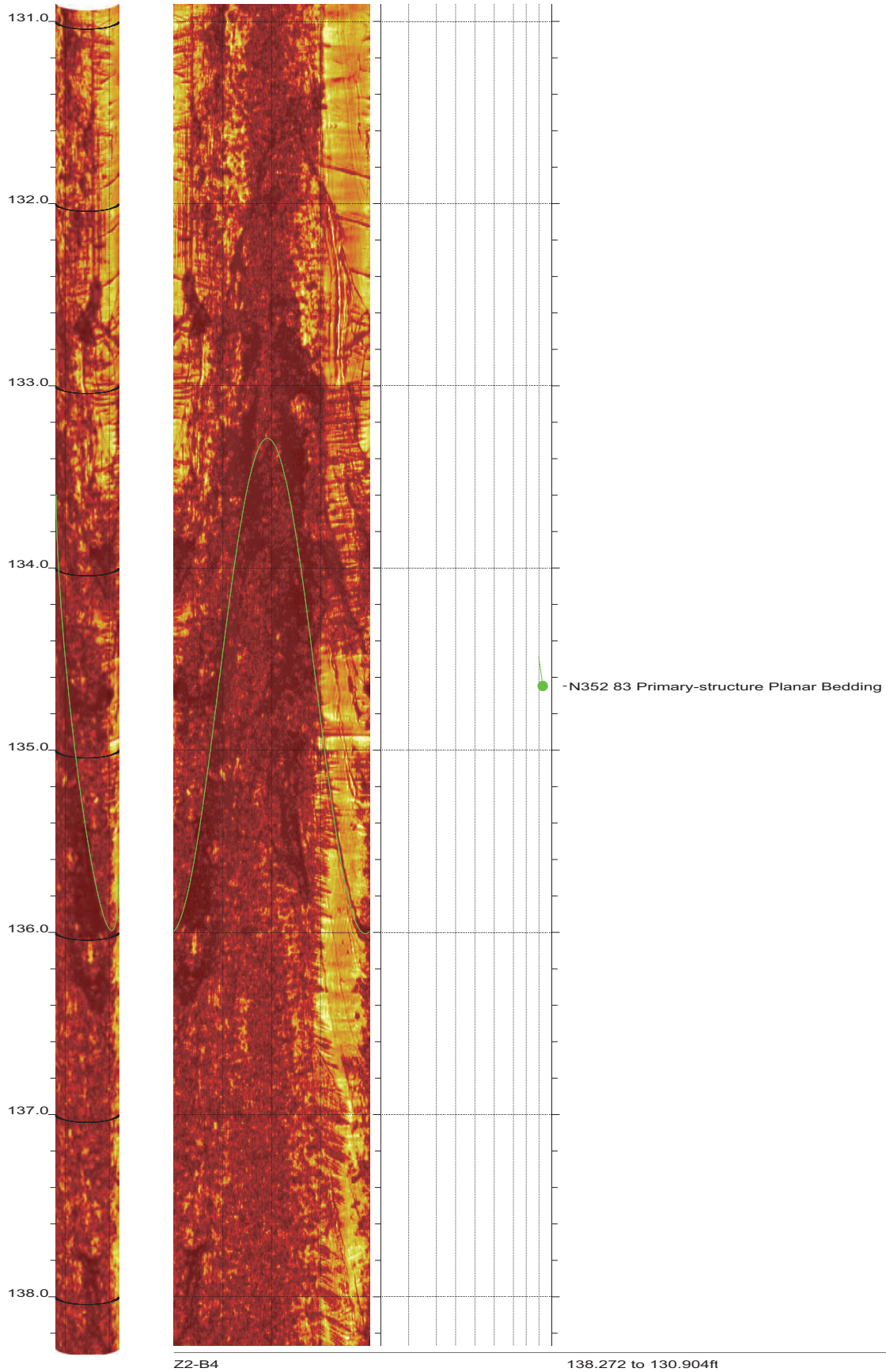


Z2-B4

130.904 to 123.536ft

18

SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 18 of 52

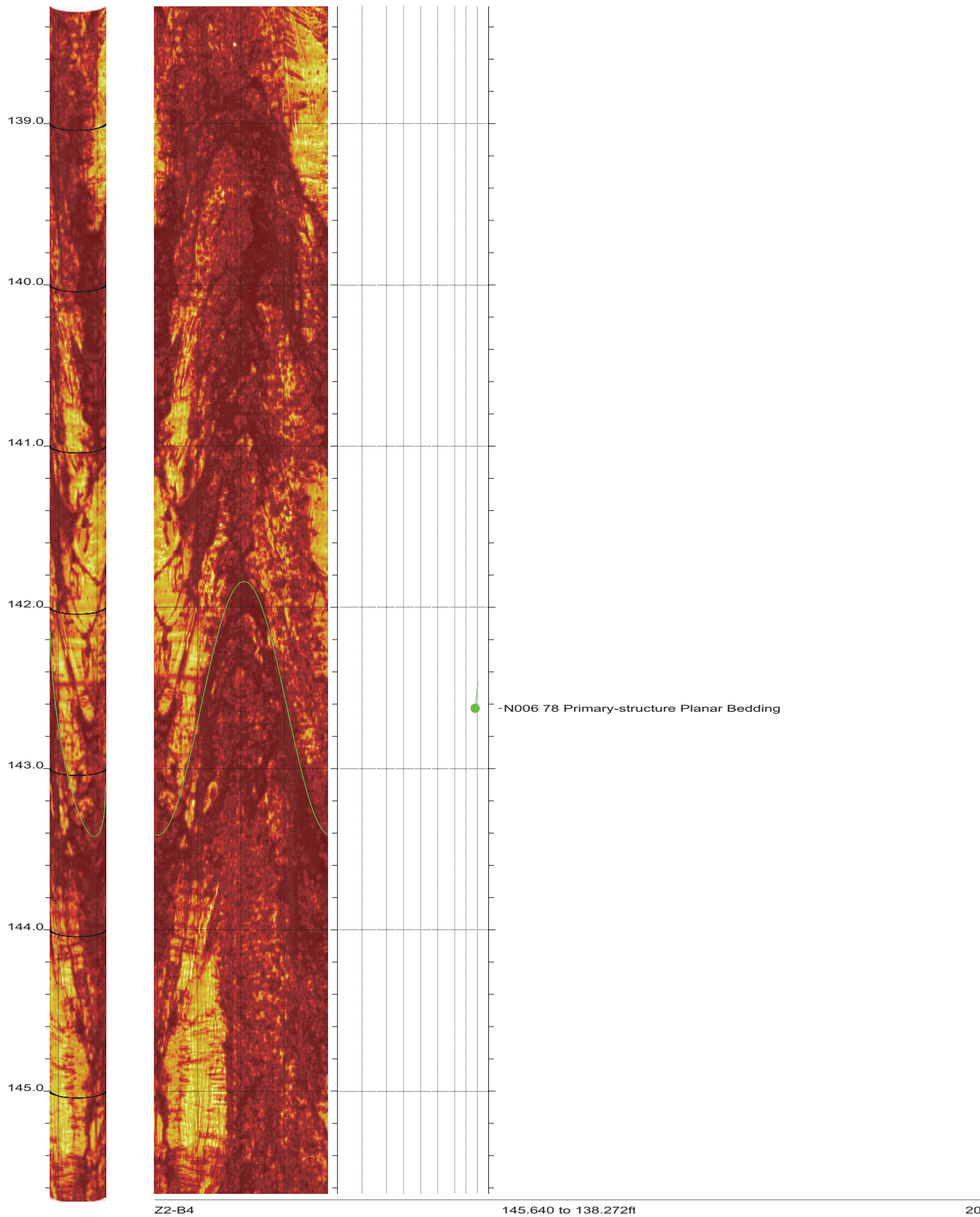


Z2-B4

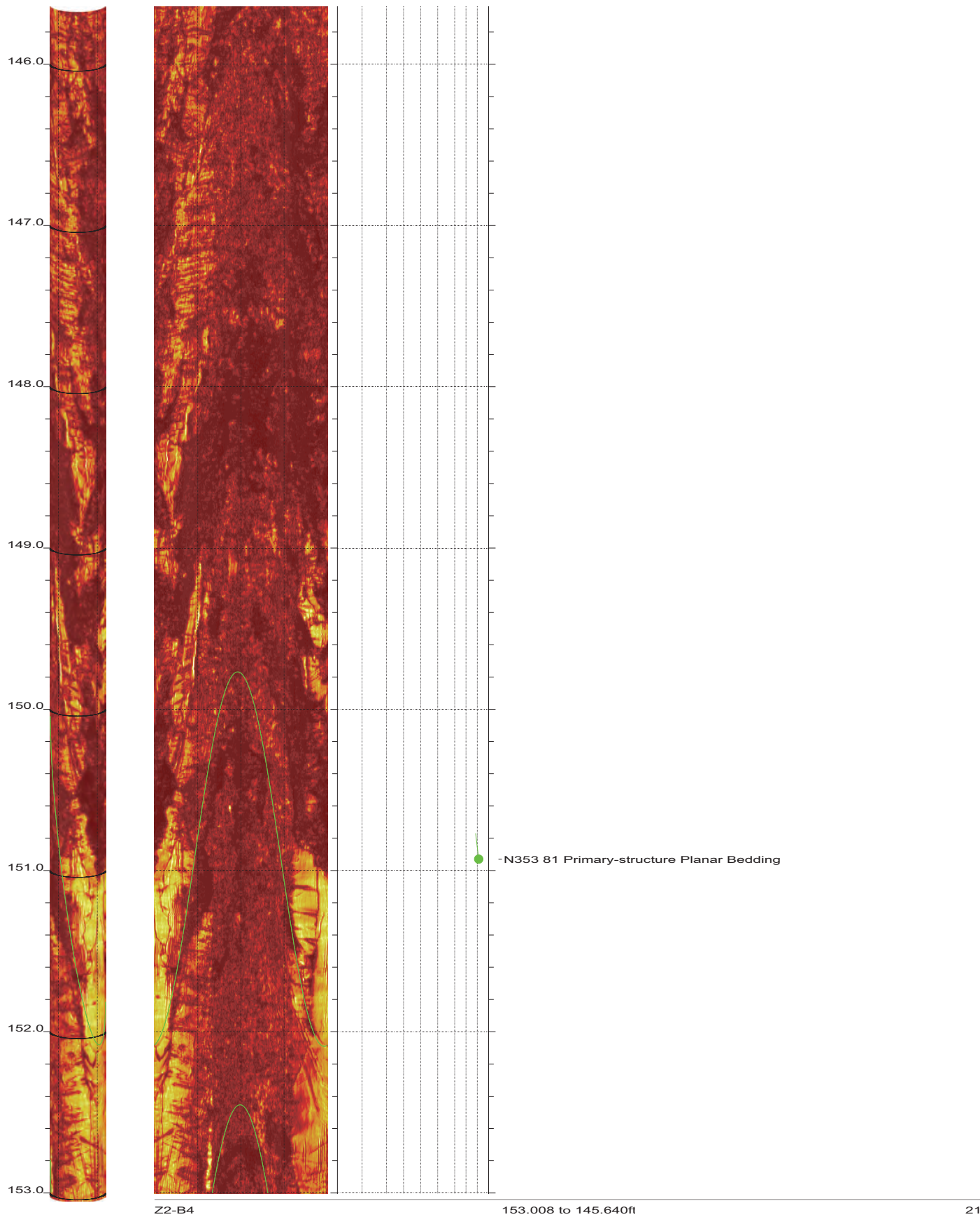
138.272 to 130.904ft

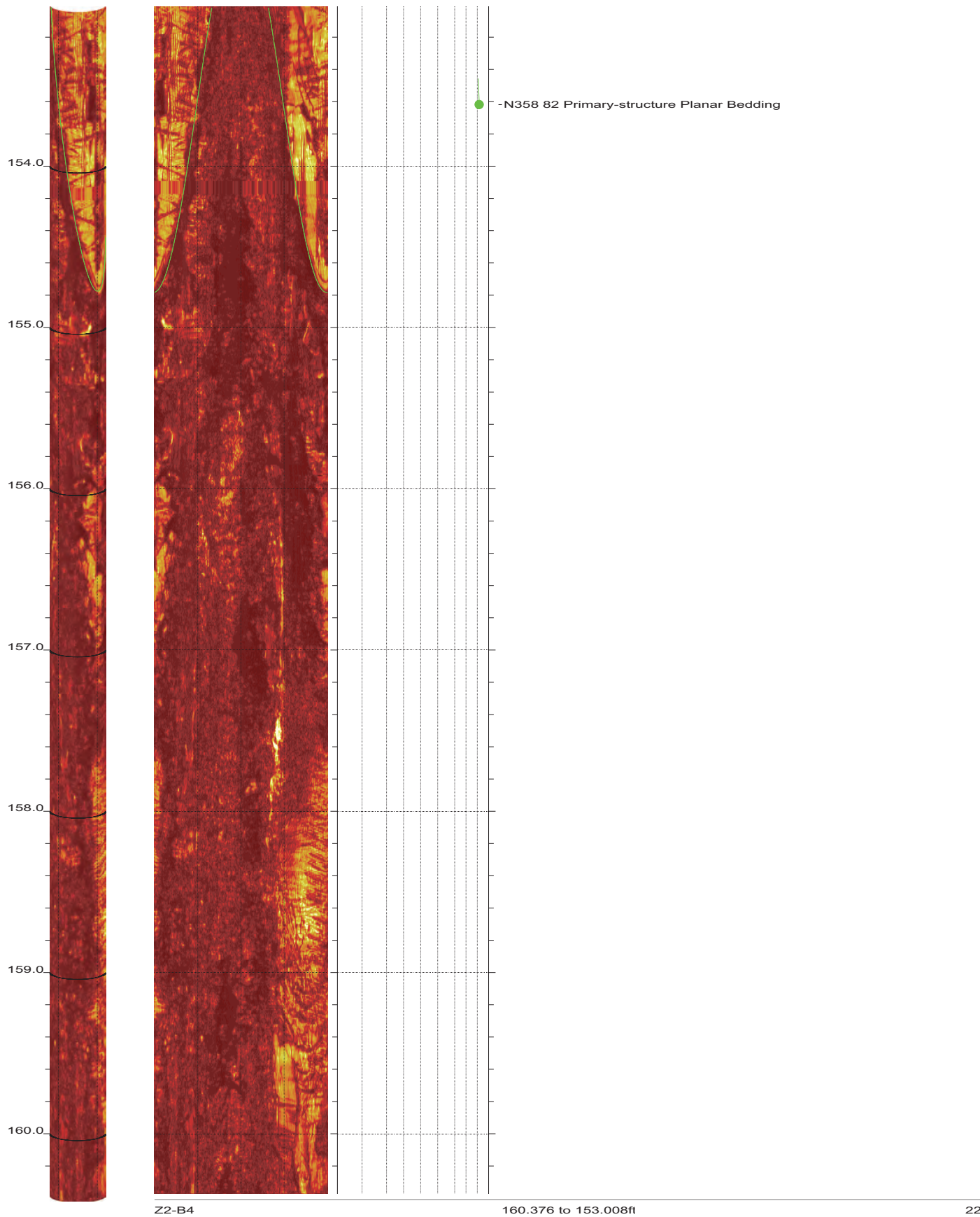
19



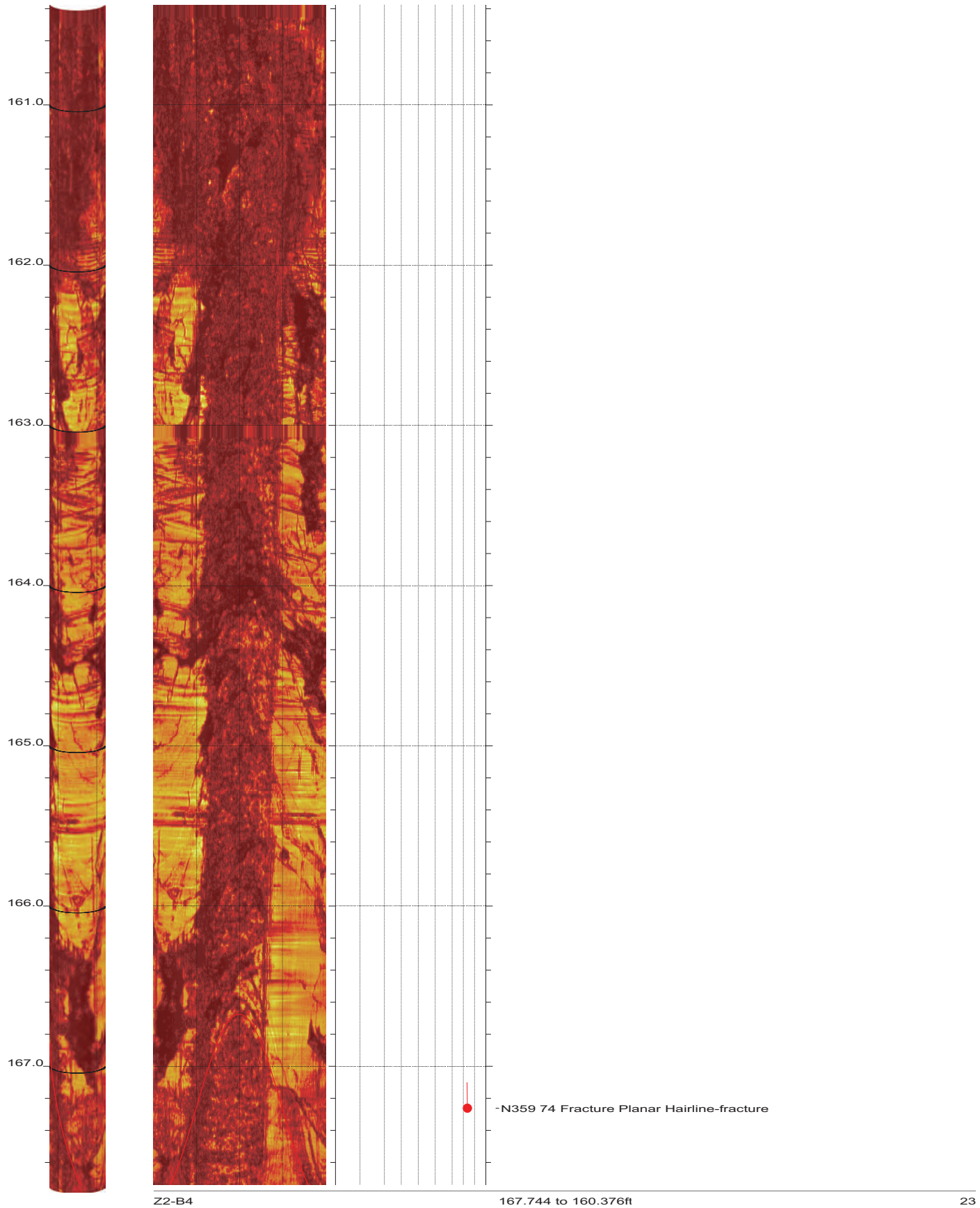


SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 20 of 52

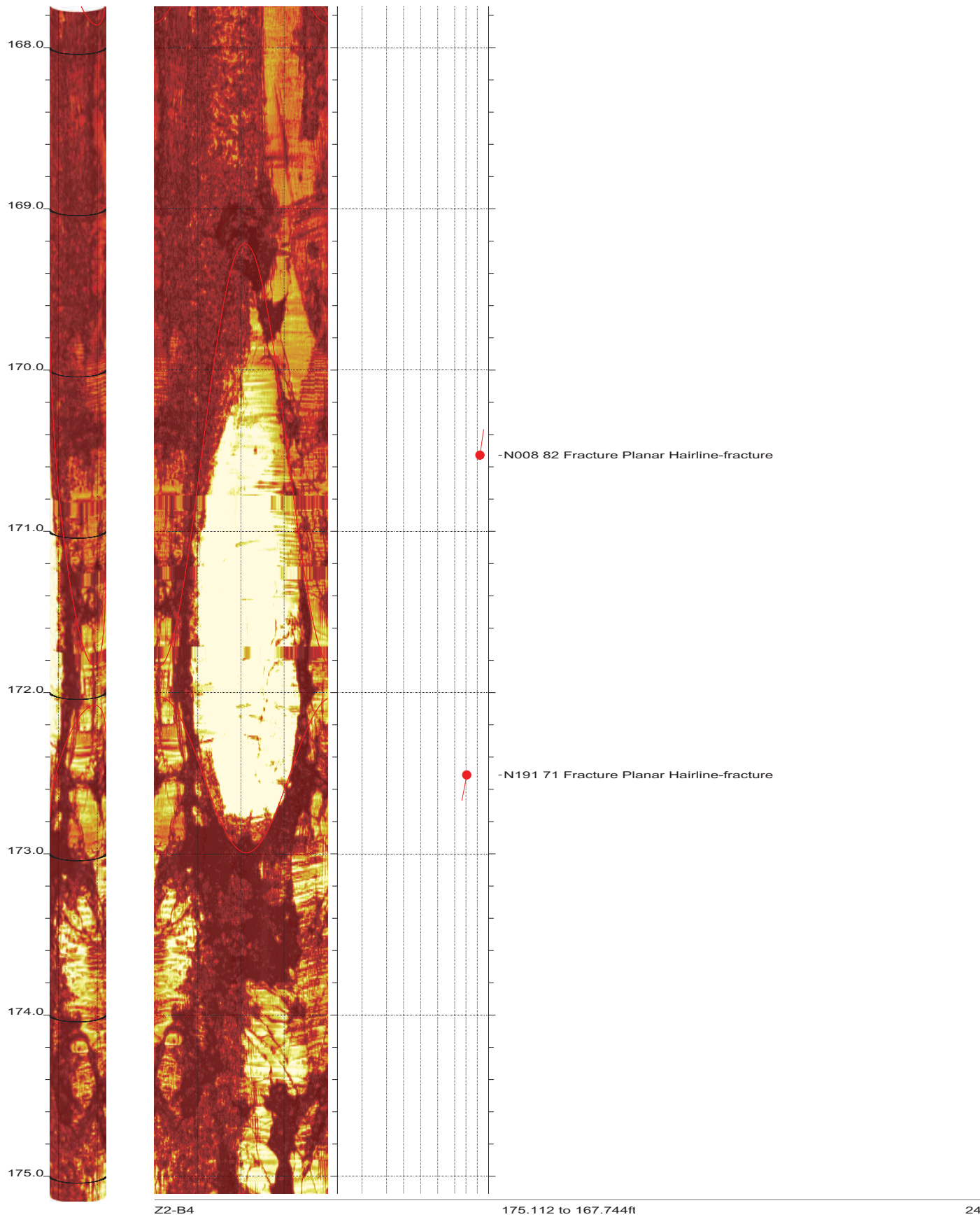




SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 22 of 52



SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 23 of 52

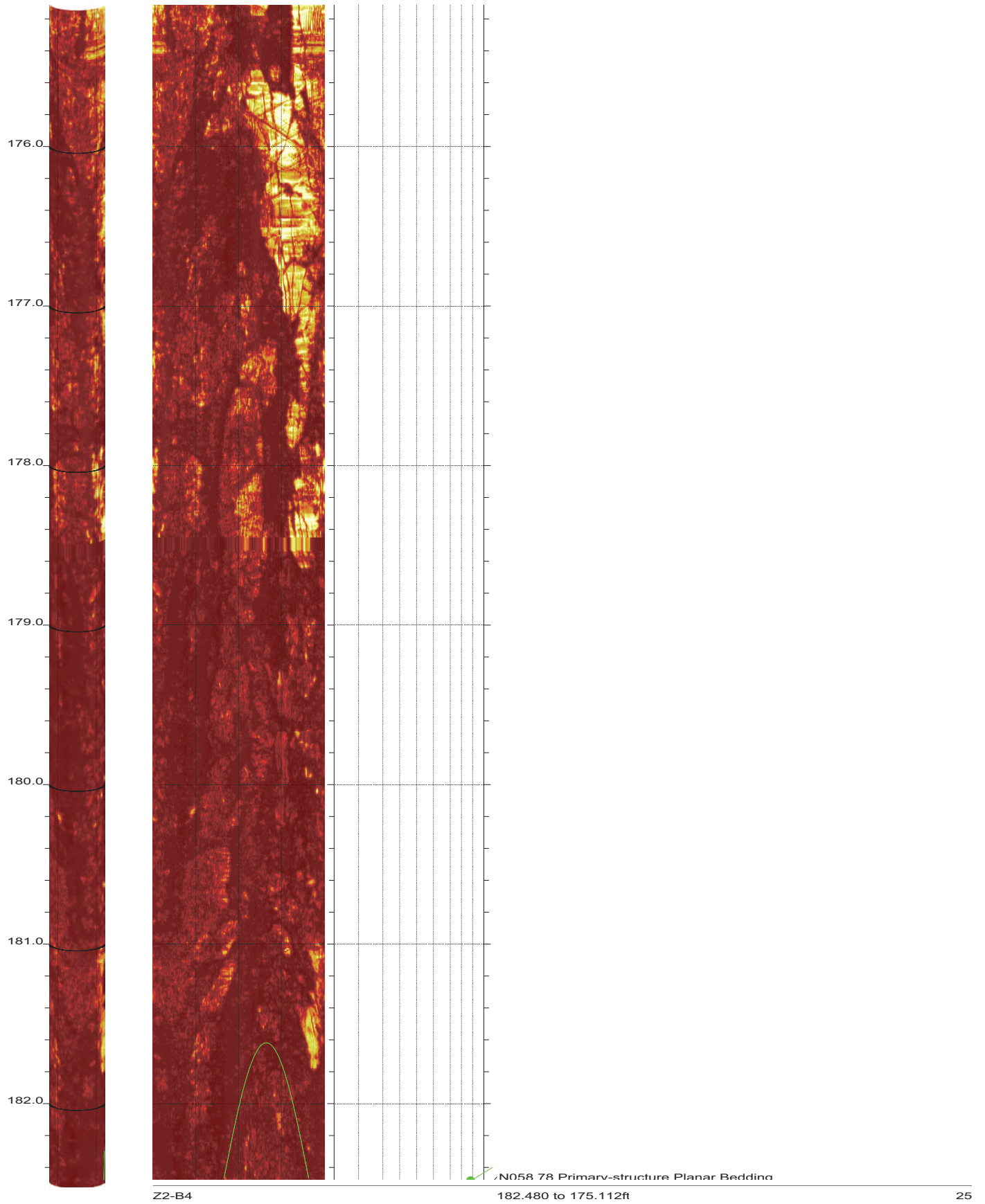


Z2-B4

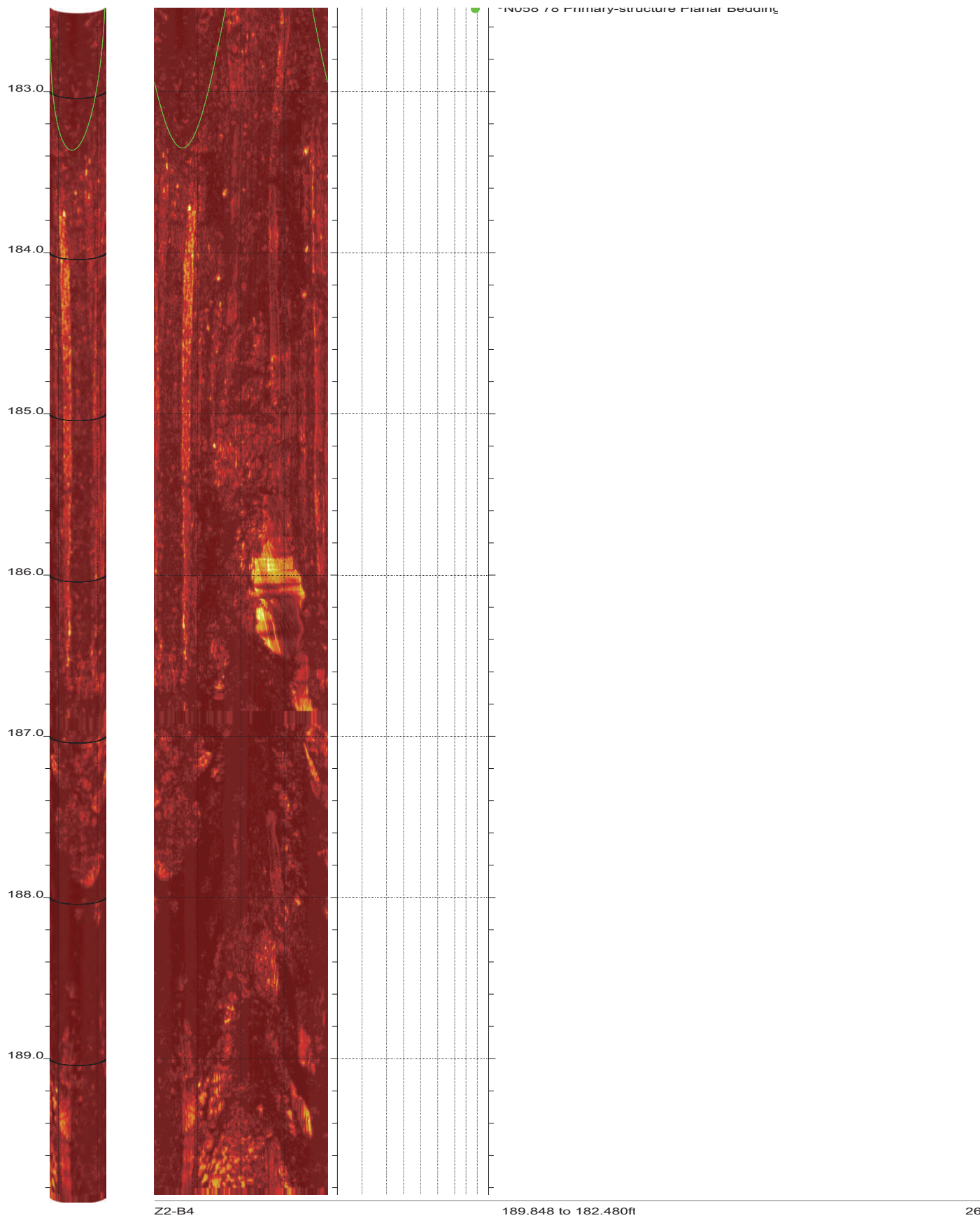
175.112 to 167.744ft

24

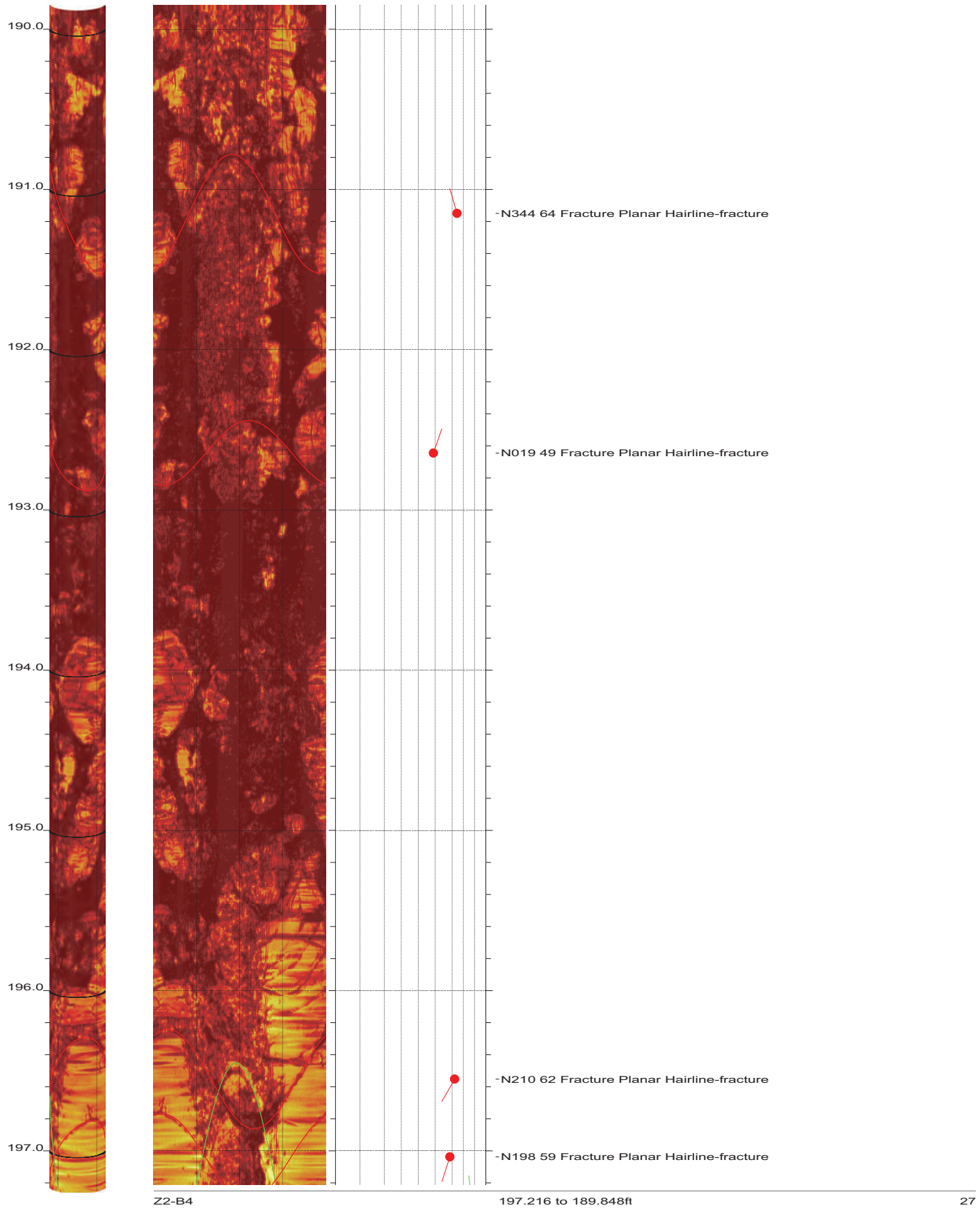
SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 24 of 52



SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 25 of 52

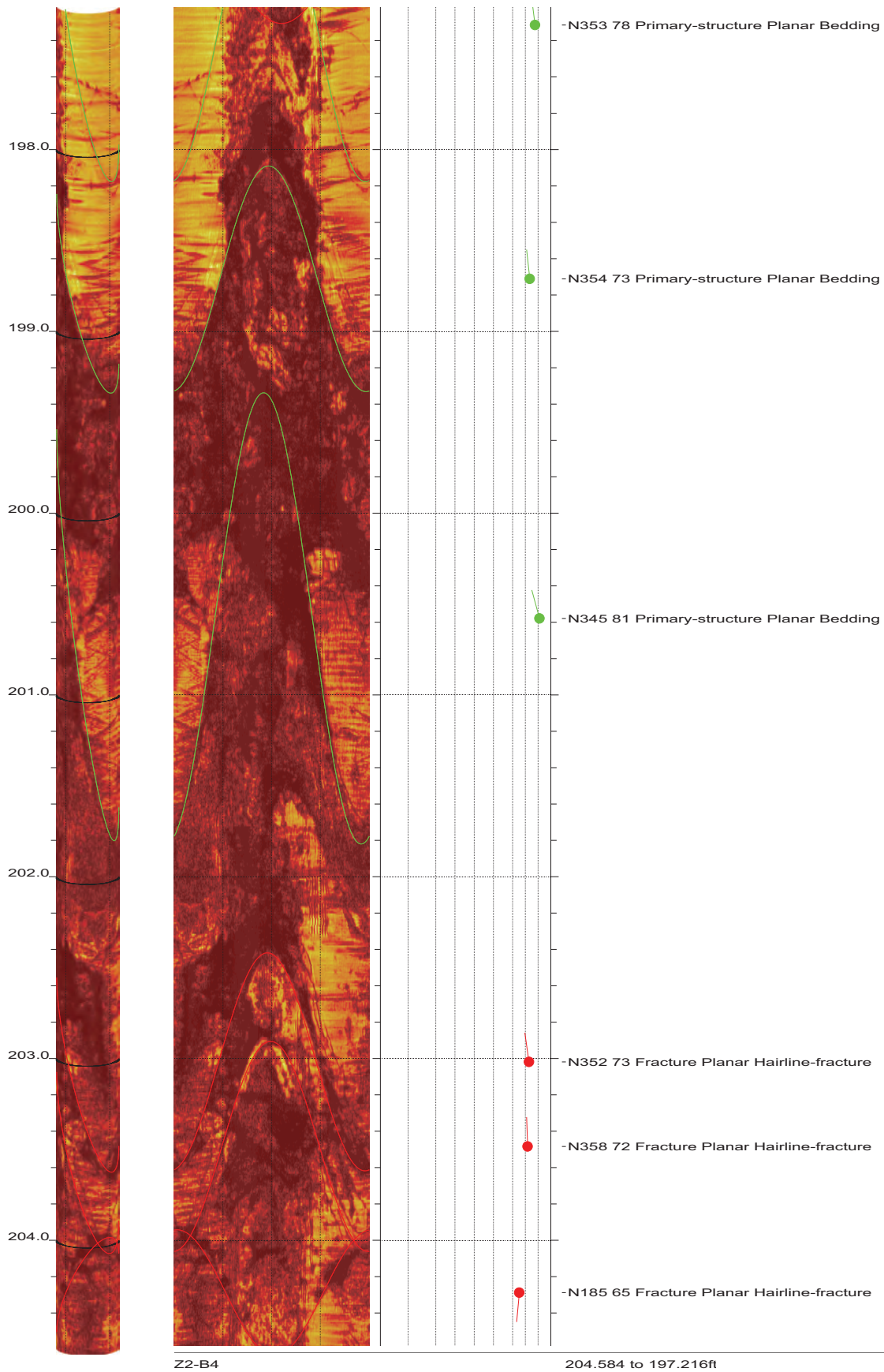


SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 26 of 52

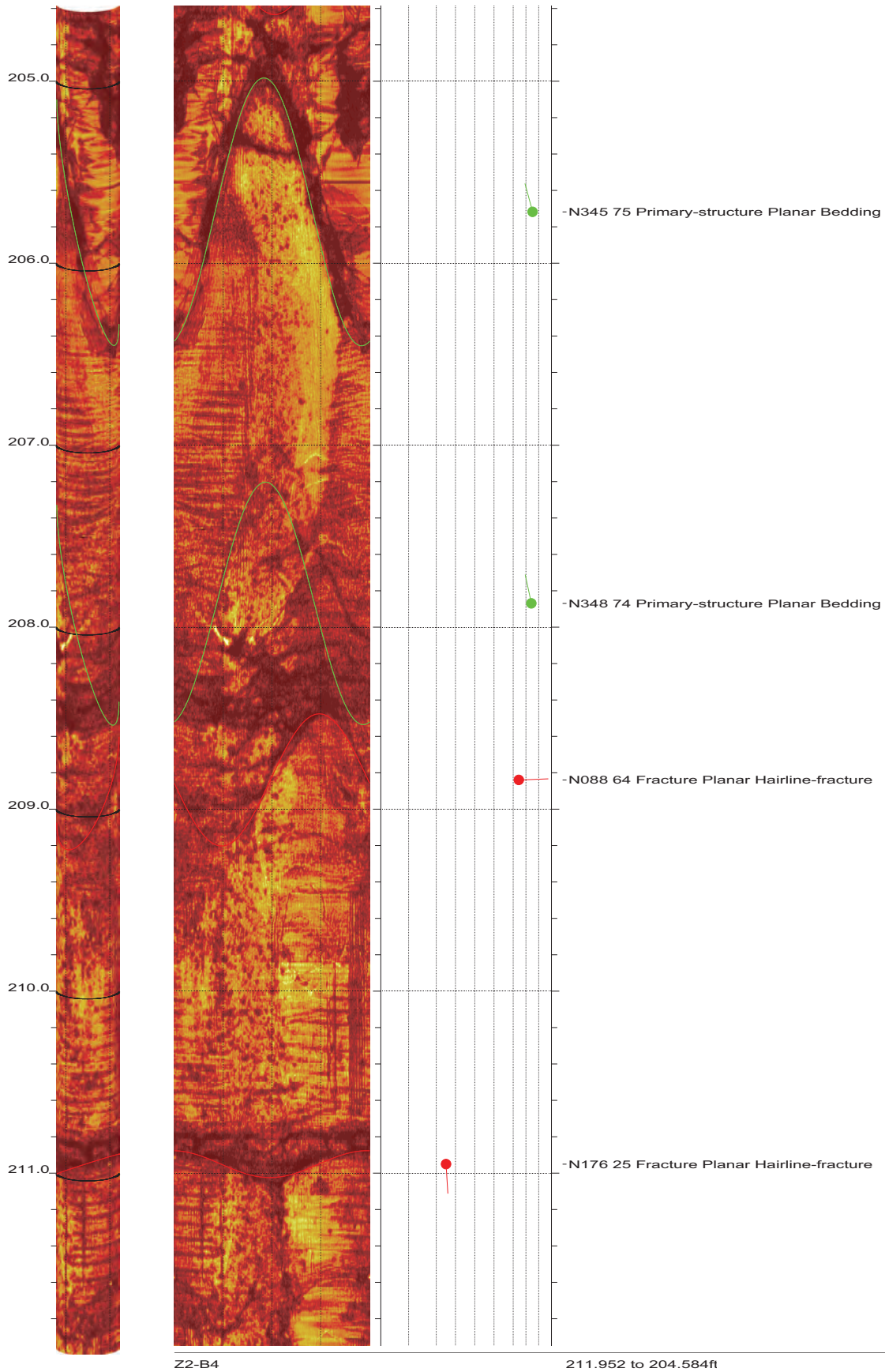


SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 27 of 52

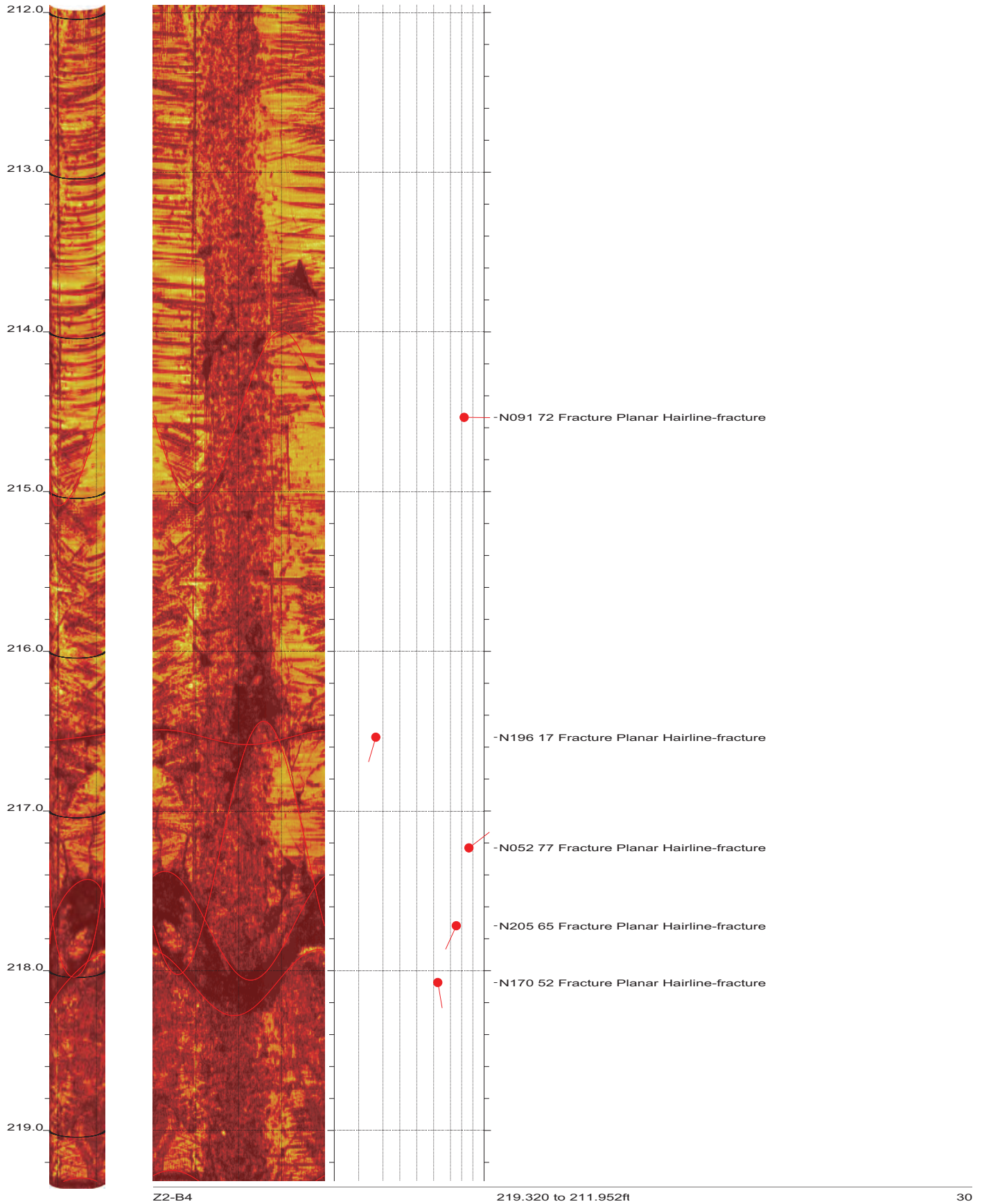




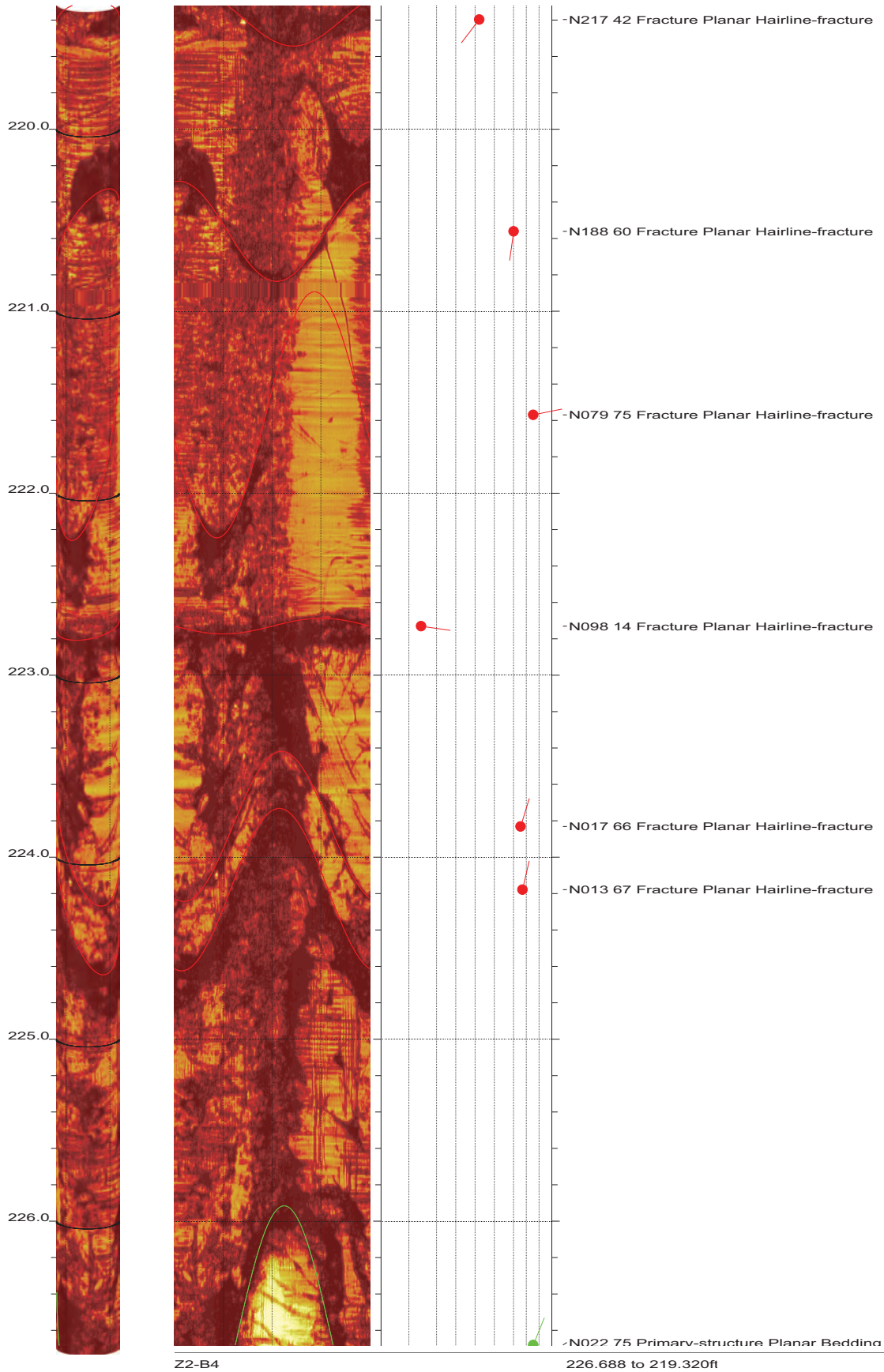
SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 28 of 52



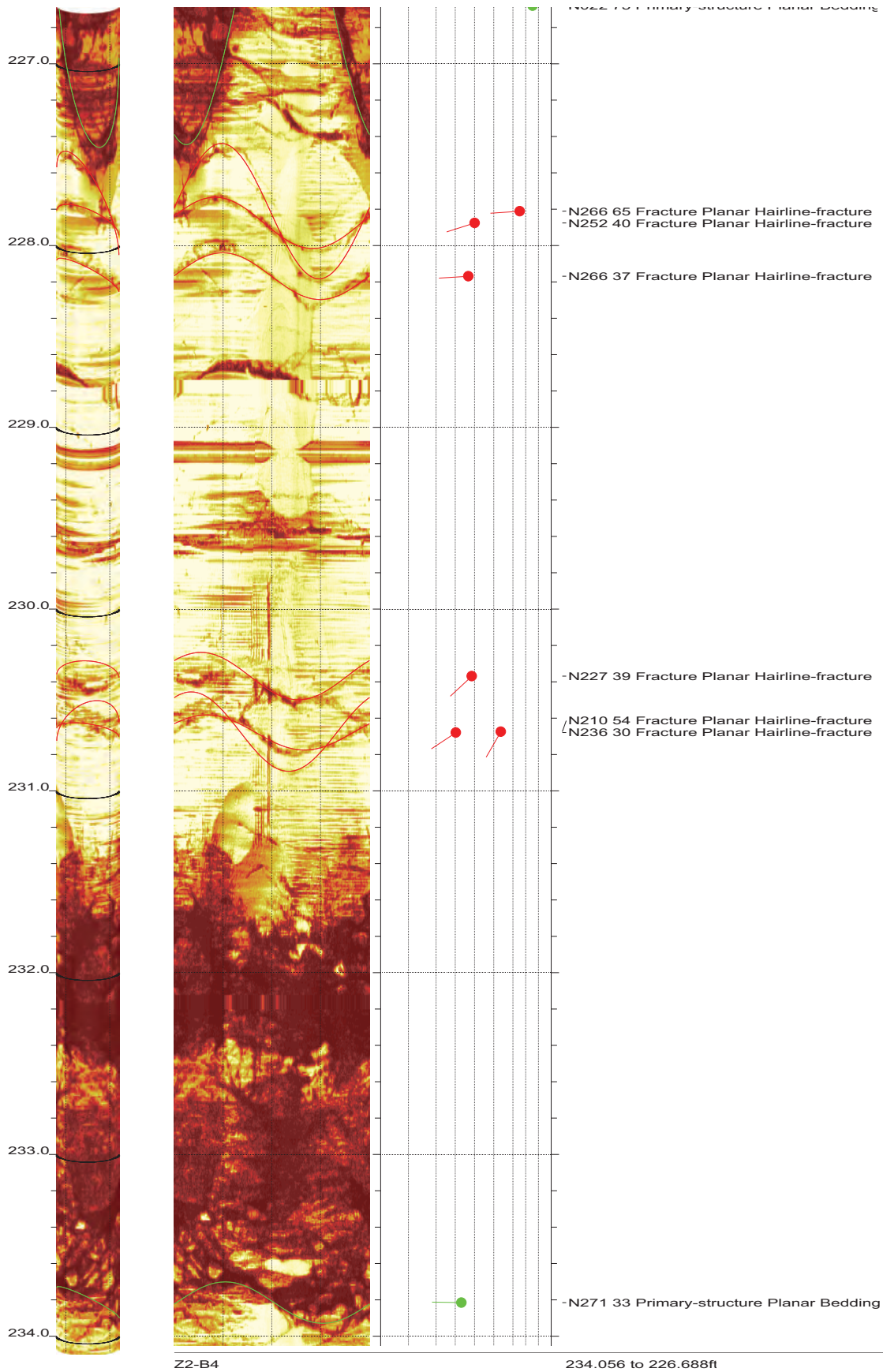
SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 29 of 52



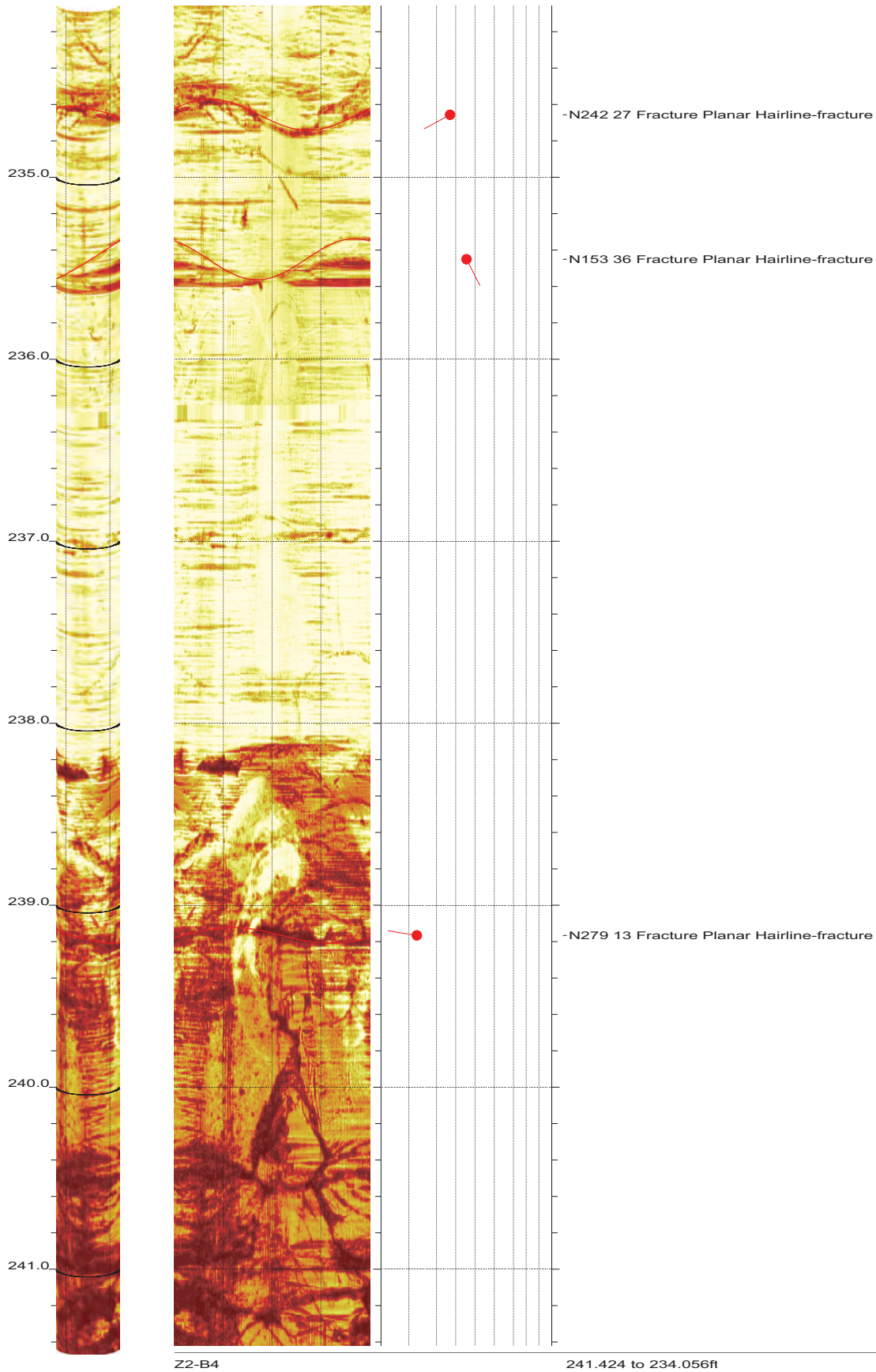
SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 30 of 52

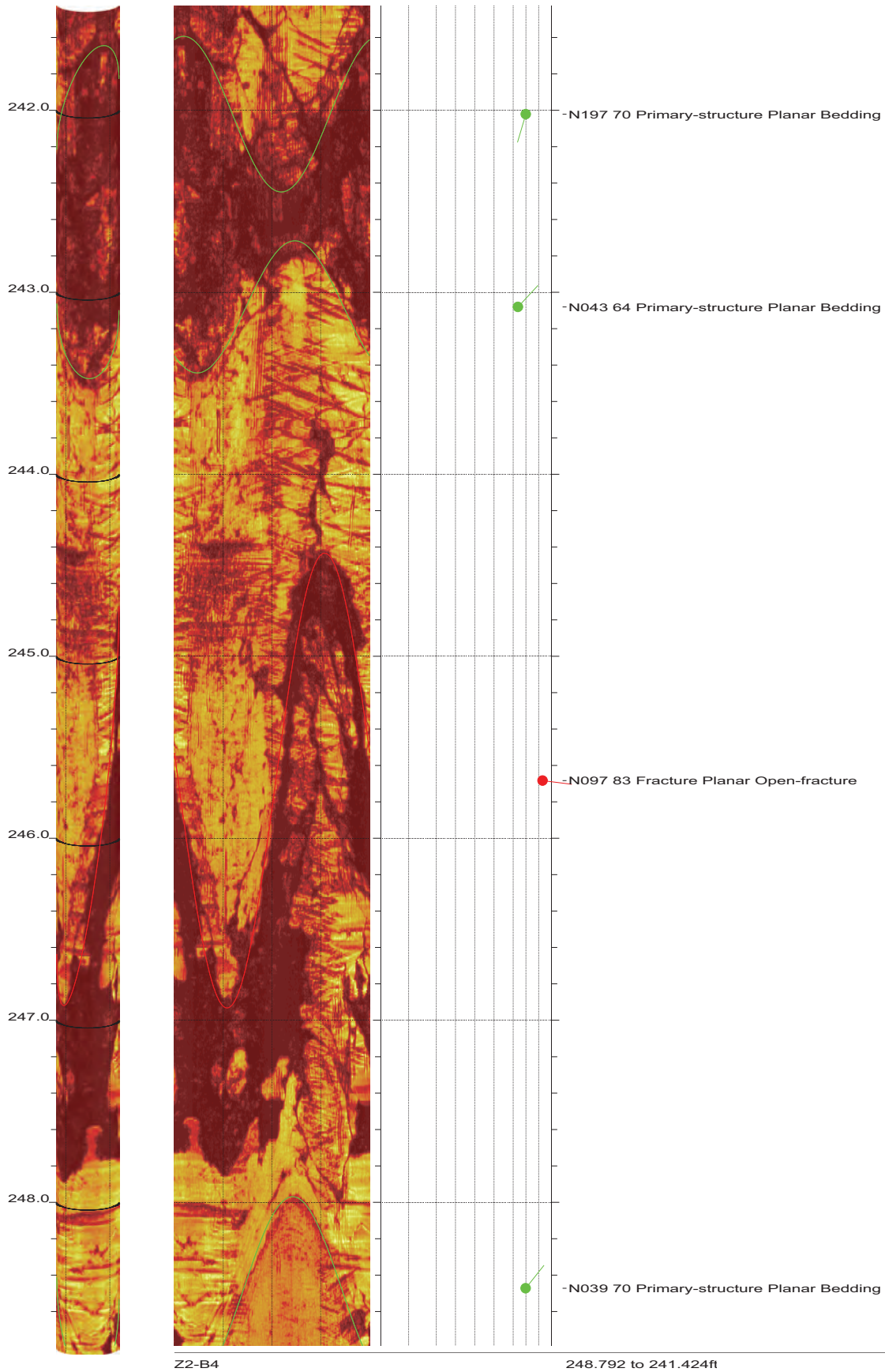


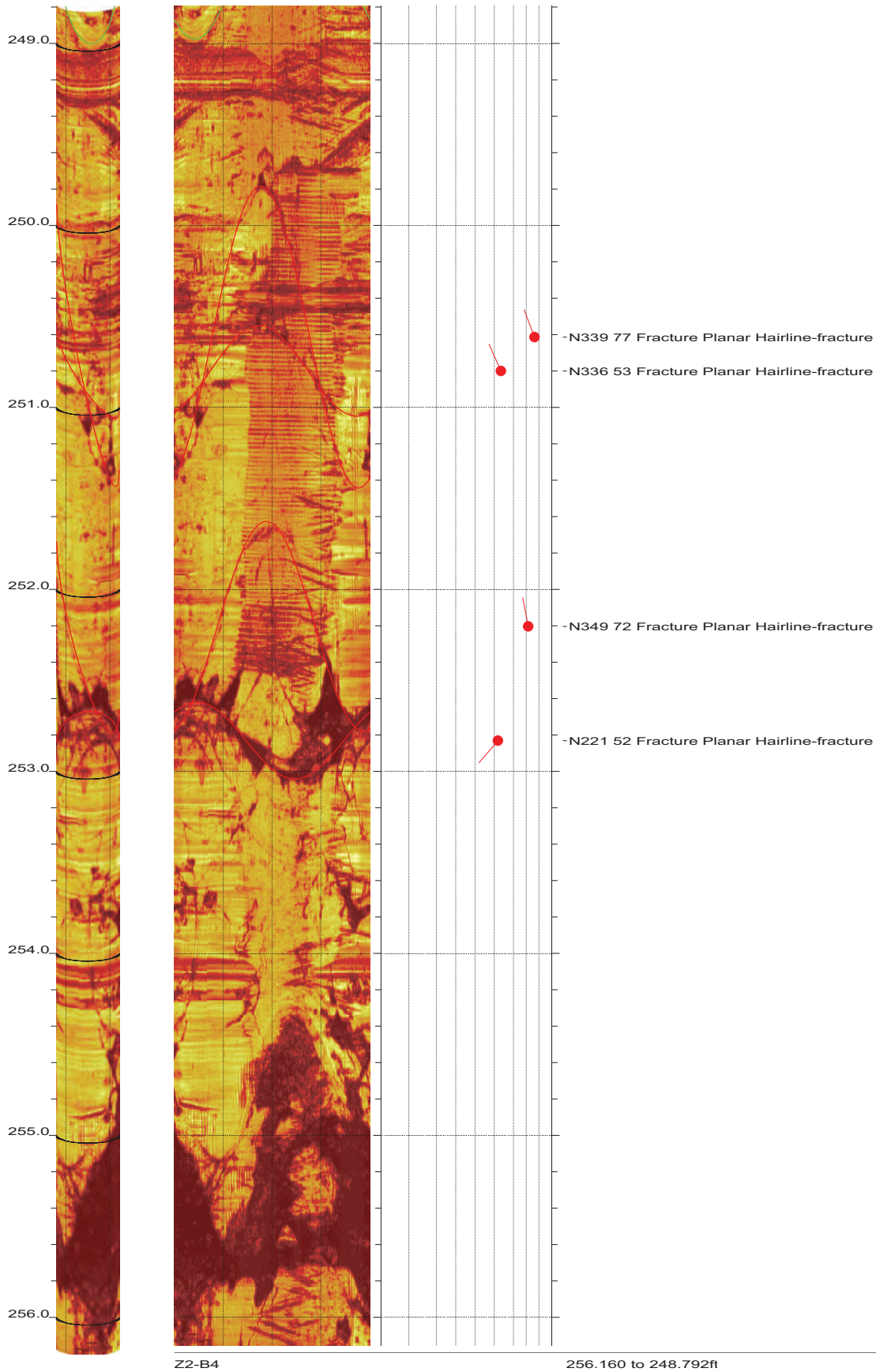
SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 31 of 52



SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 32 of 52

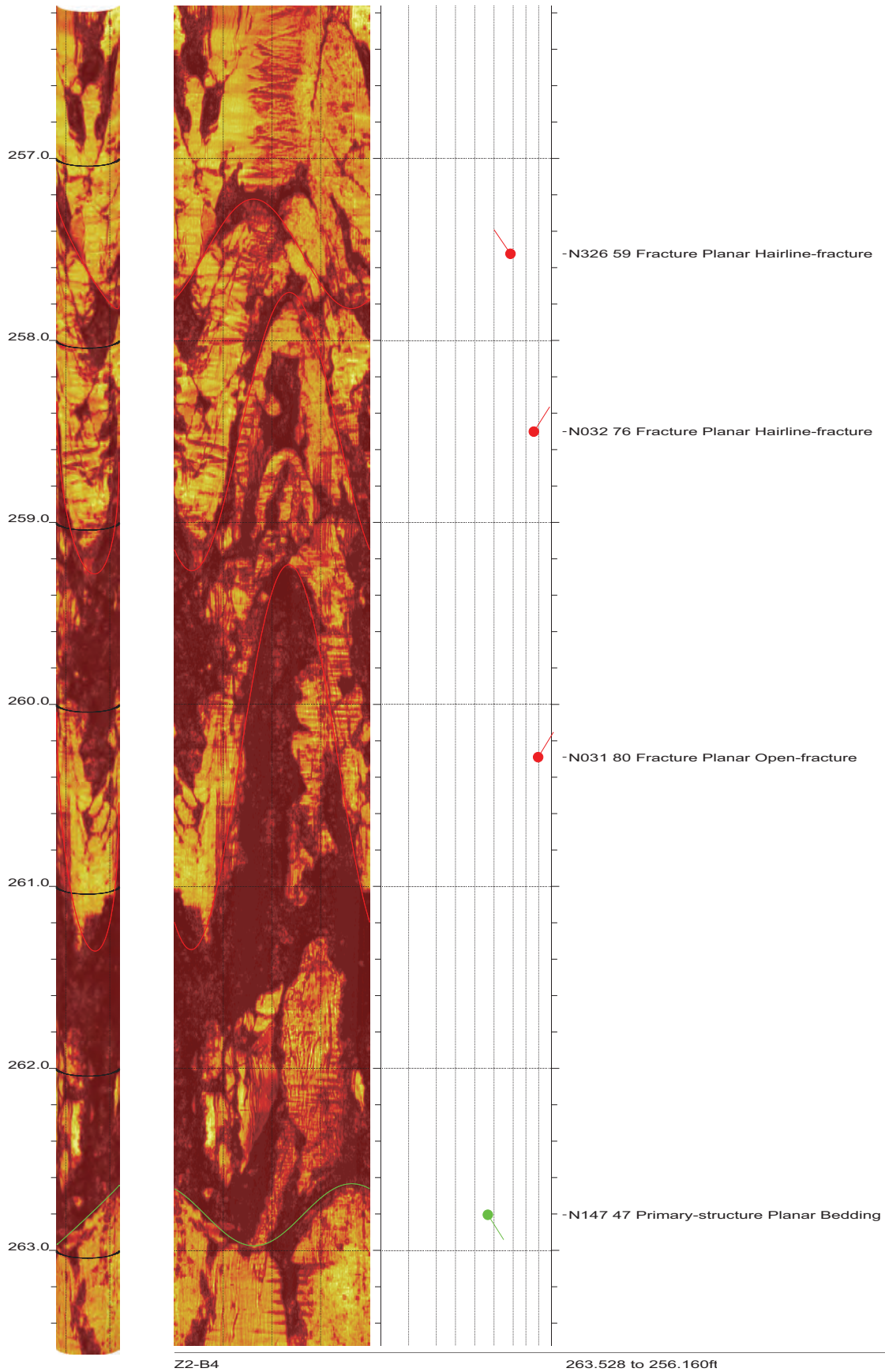


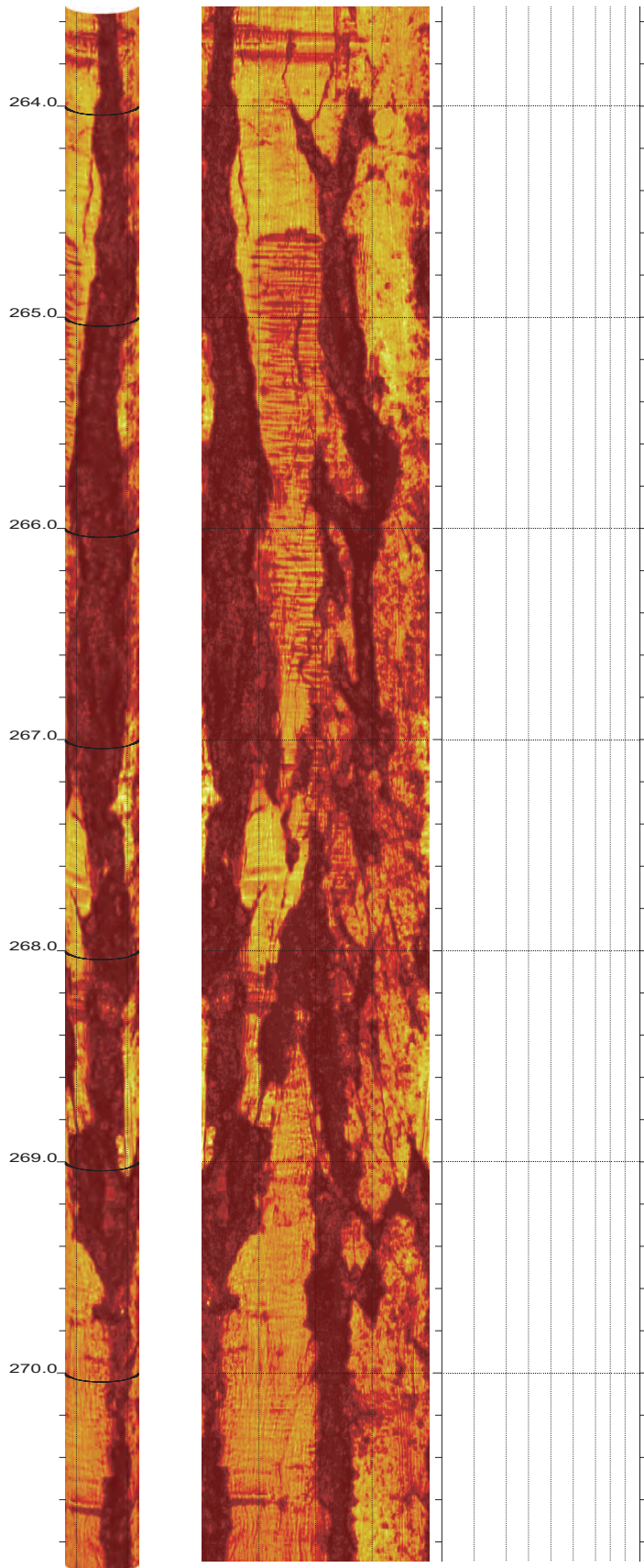




SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 35 of 52





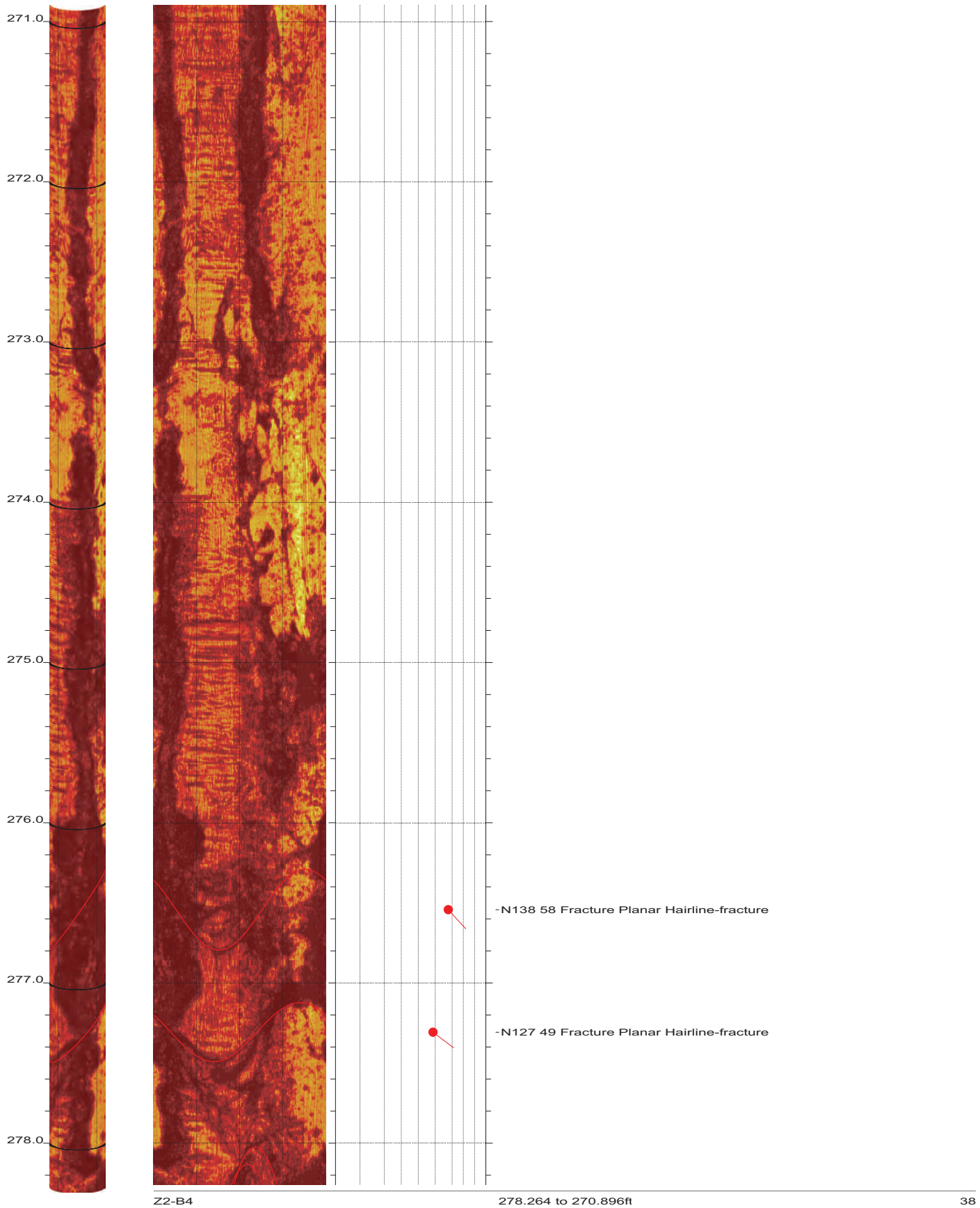


Z2-B4

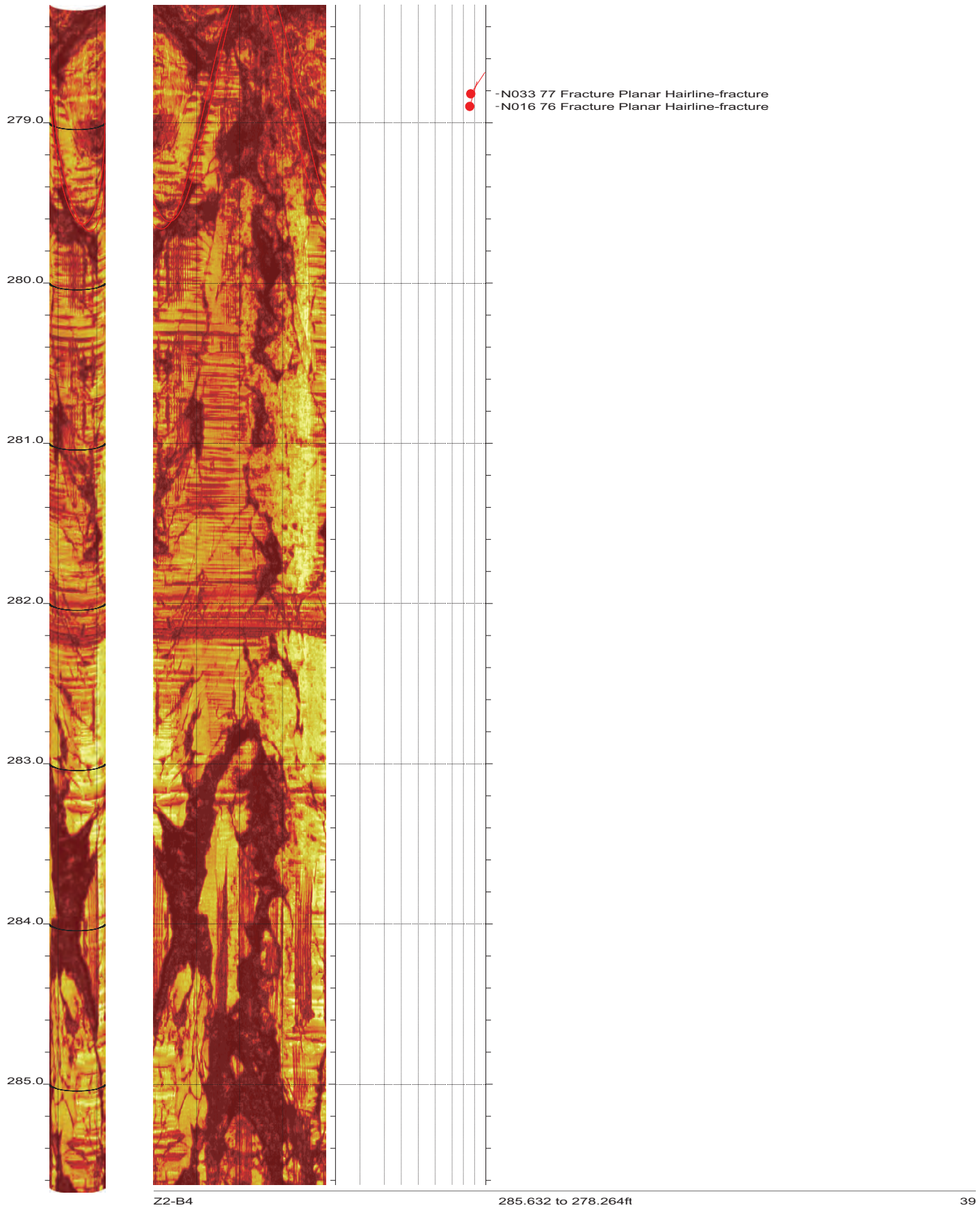
270.896 to 263.528ft

37

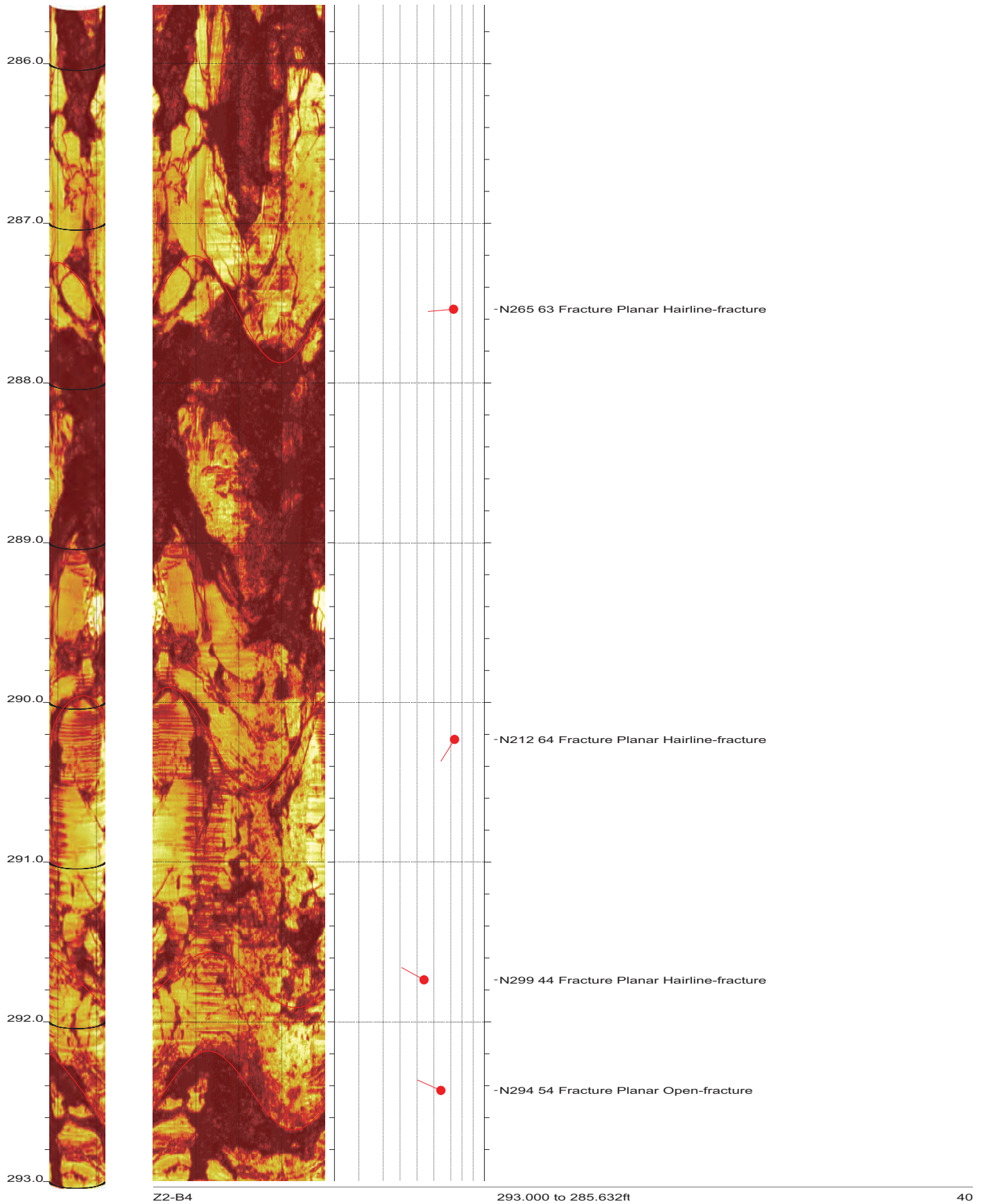
SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 37 of 52



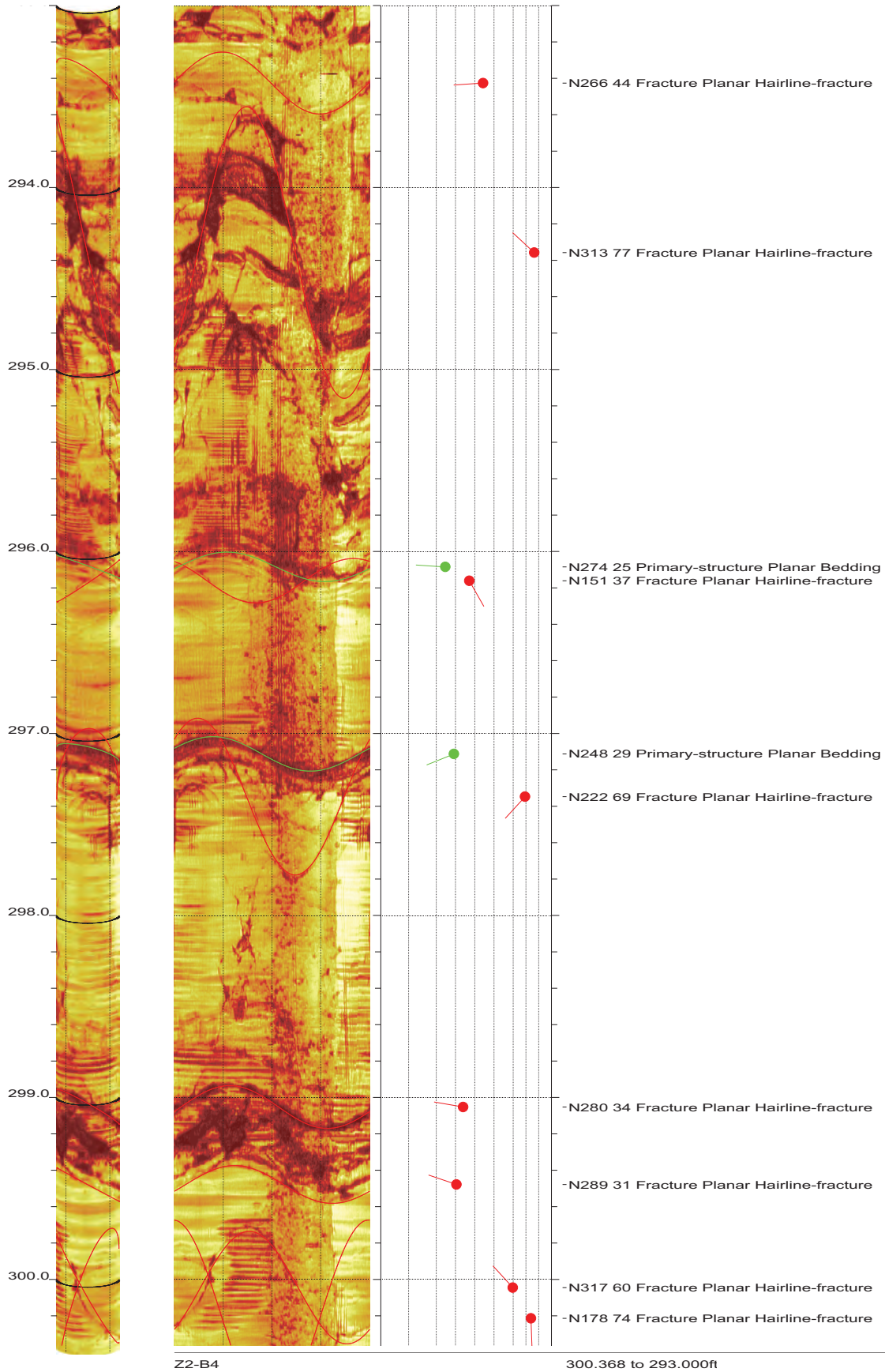
SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 38 of 52



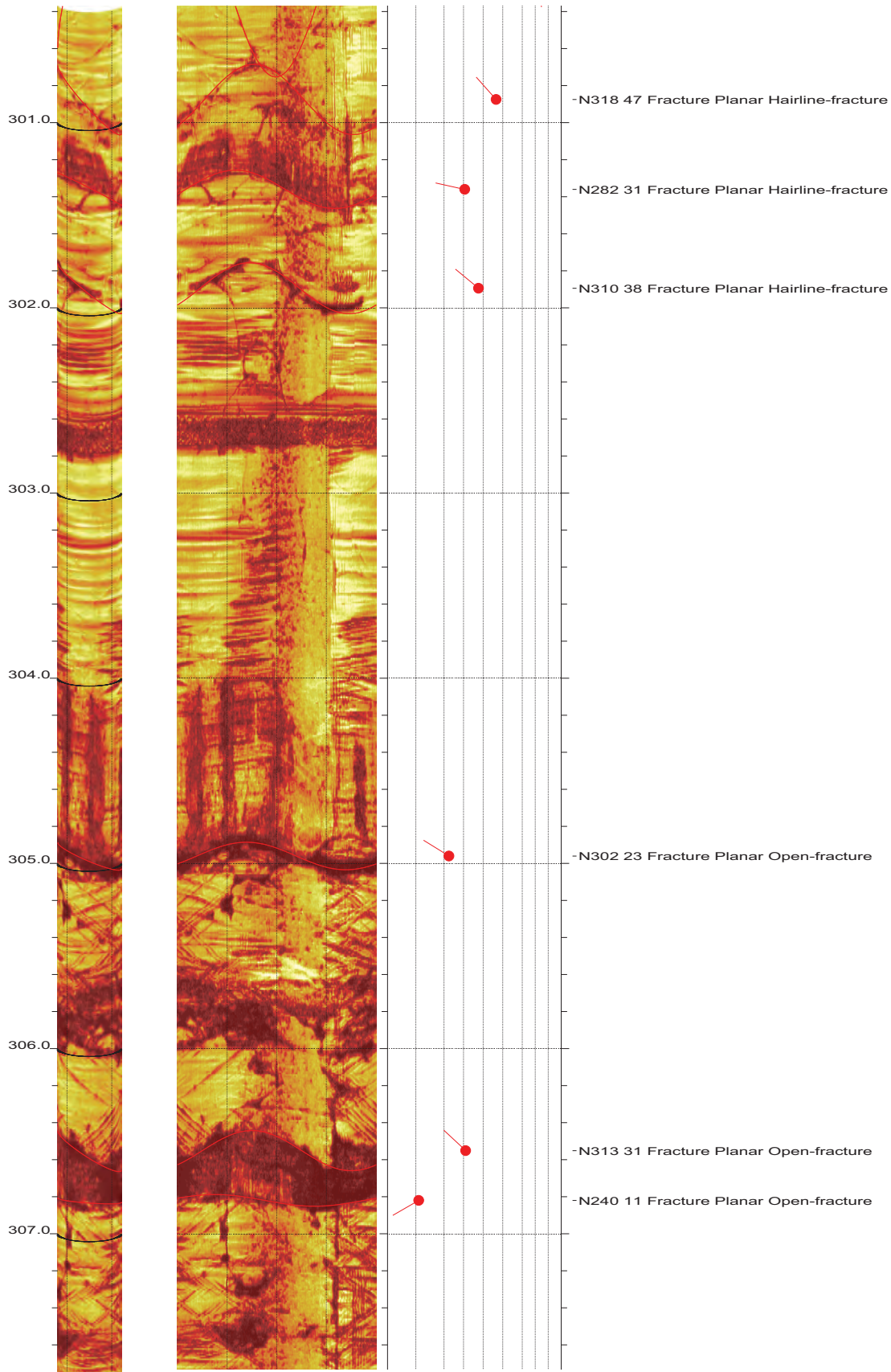
SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 39 of 52



SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 40 of 52



SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 41 of 52

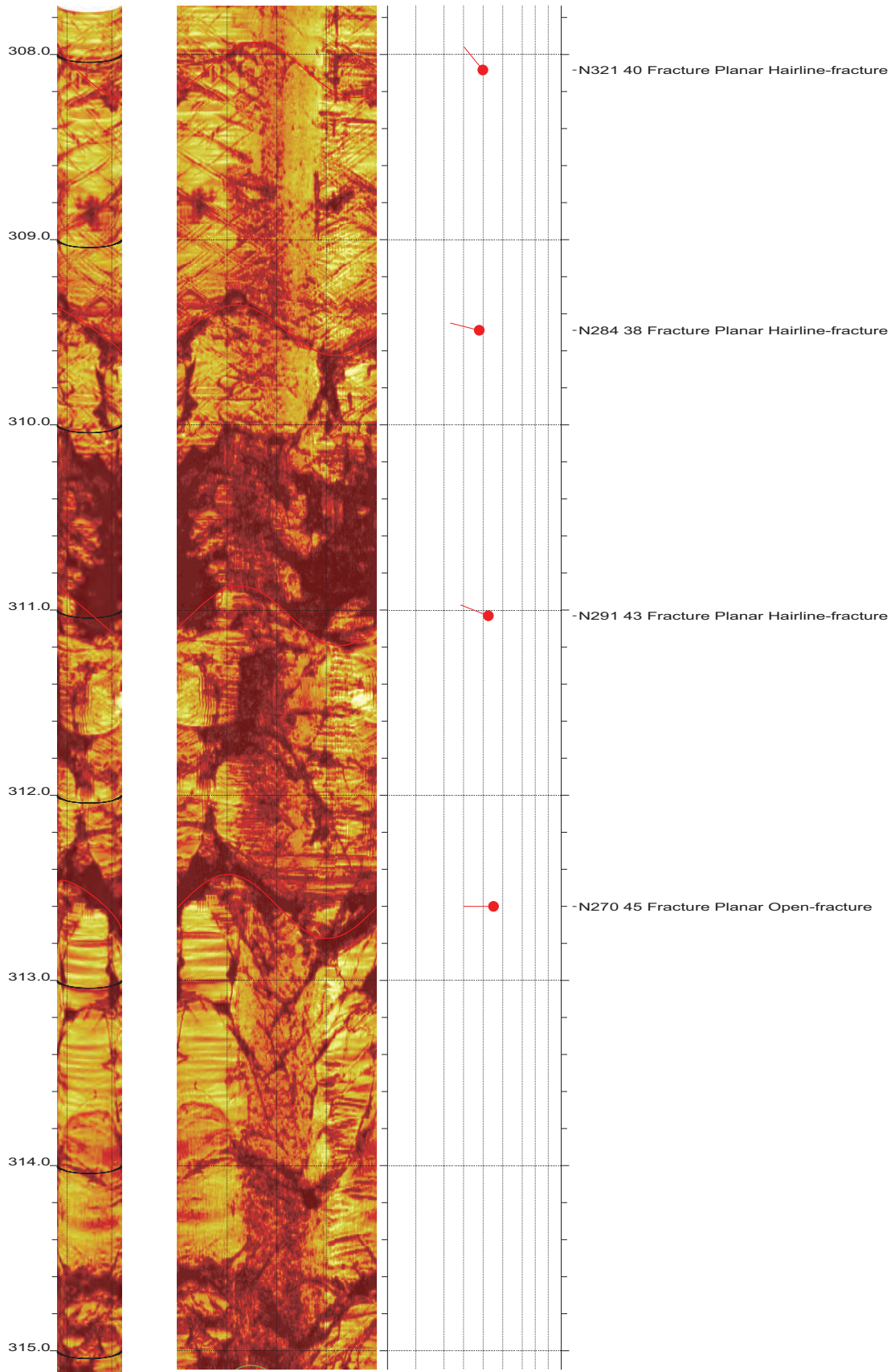


Z2-B4

307.736 to 300.368ft

42

SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 42 of 52

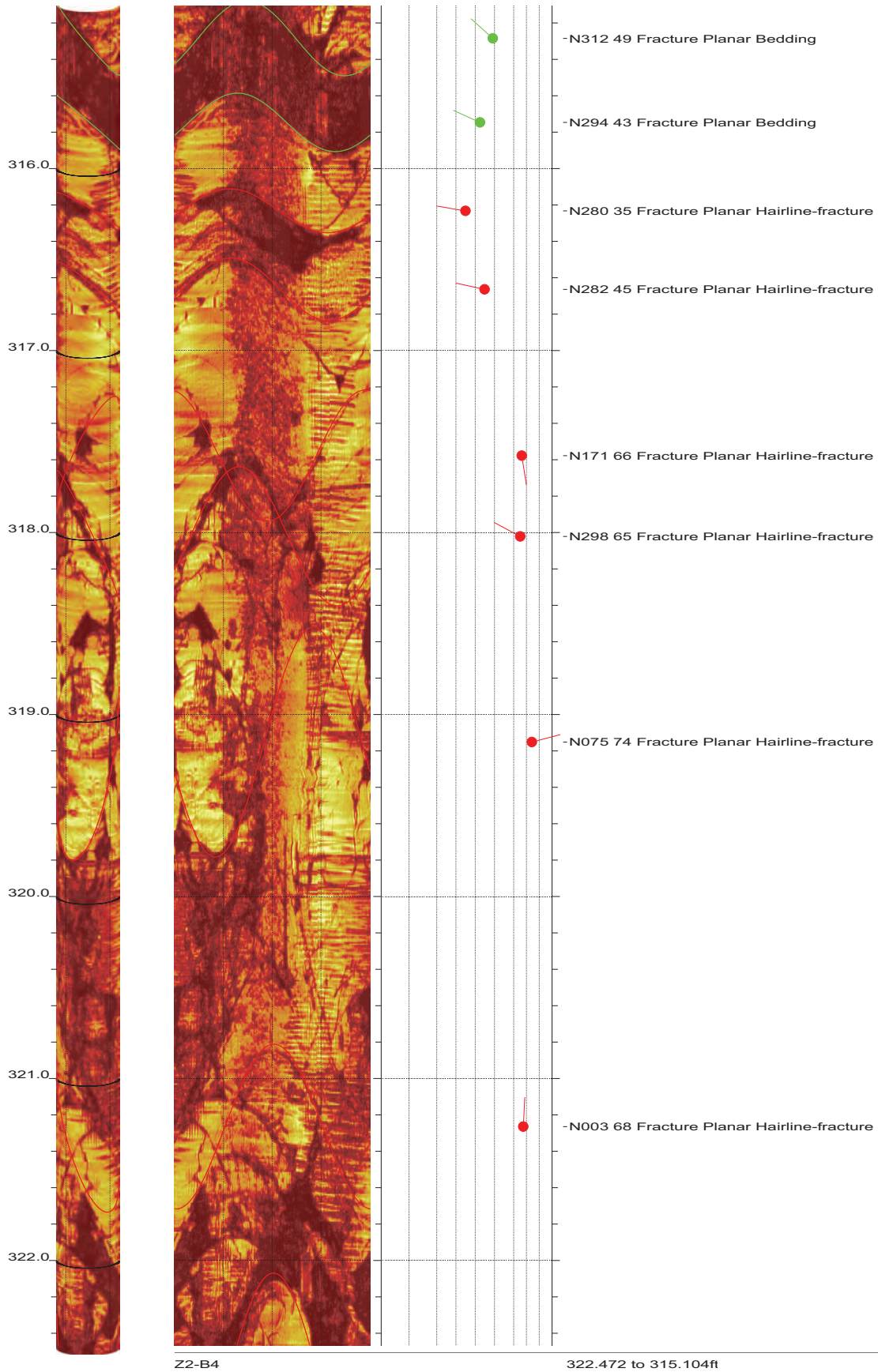


Z2-B4

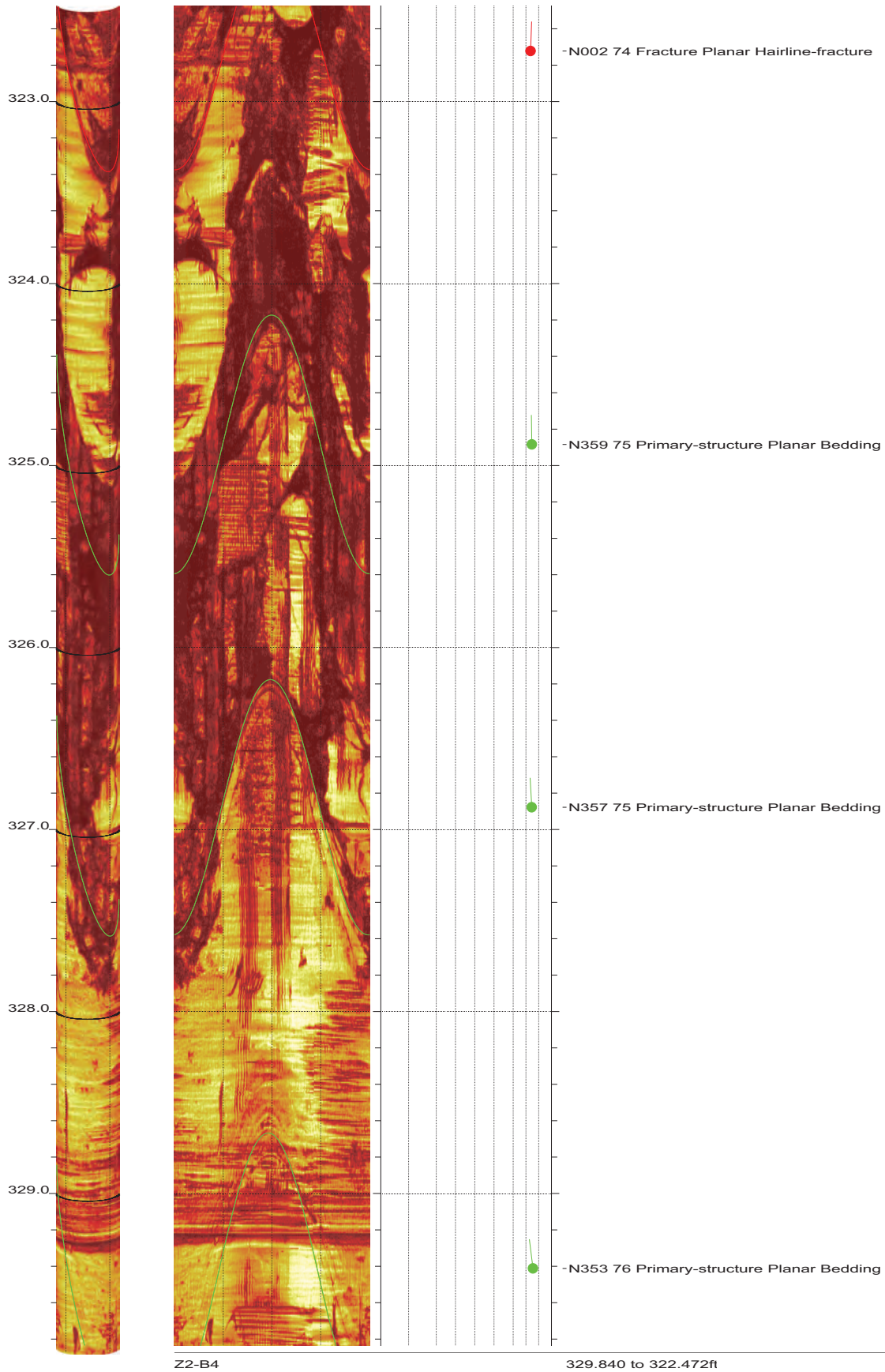
315.104 to 307.736ft

43





SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 44 of 52

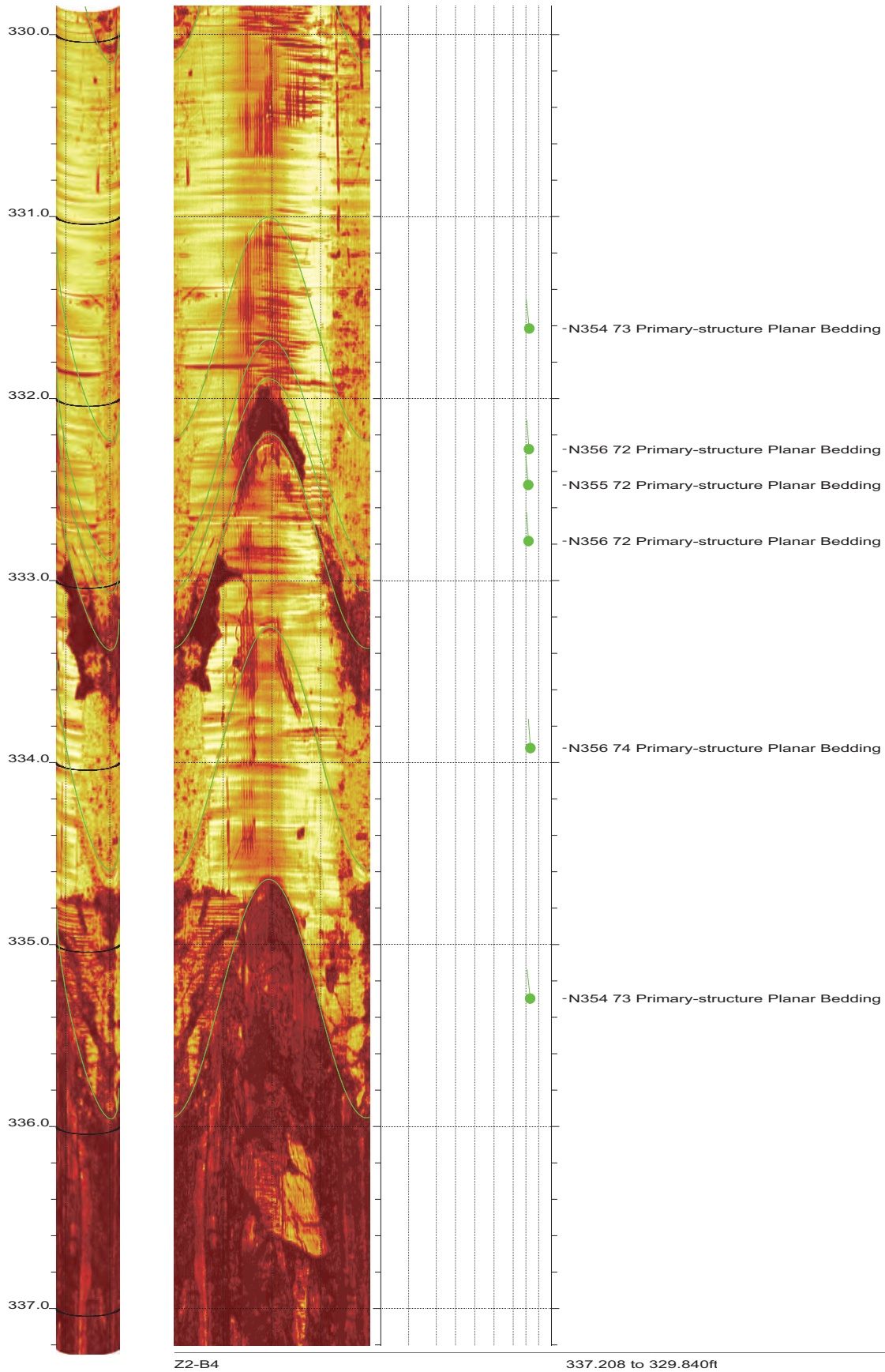


Z2-B4

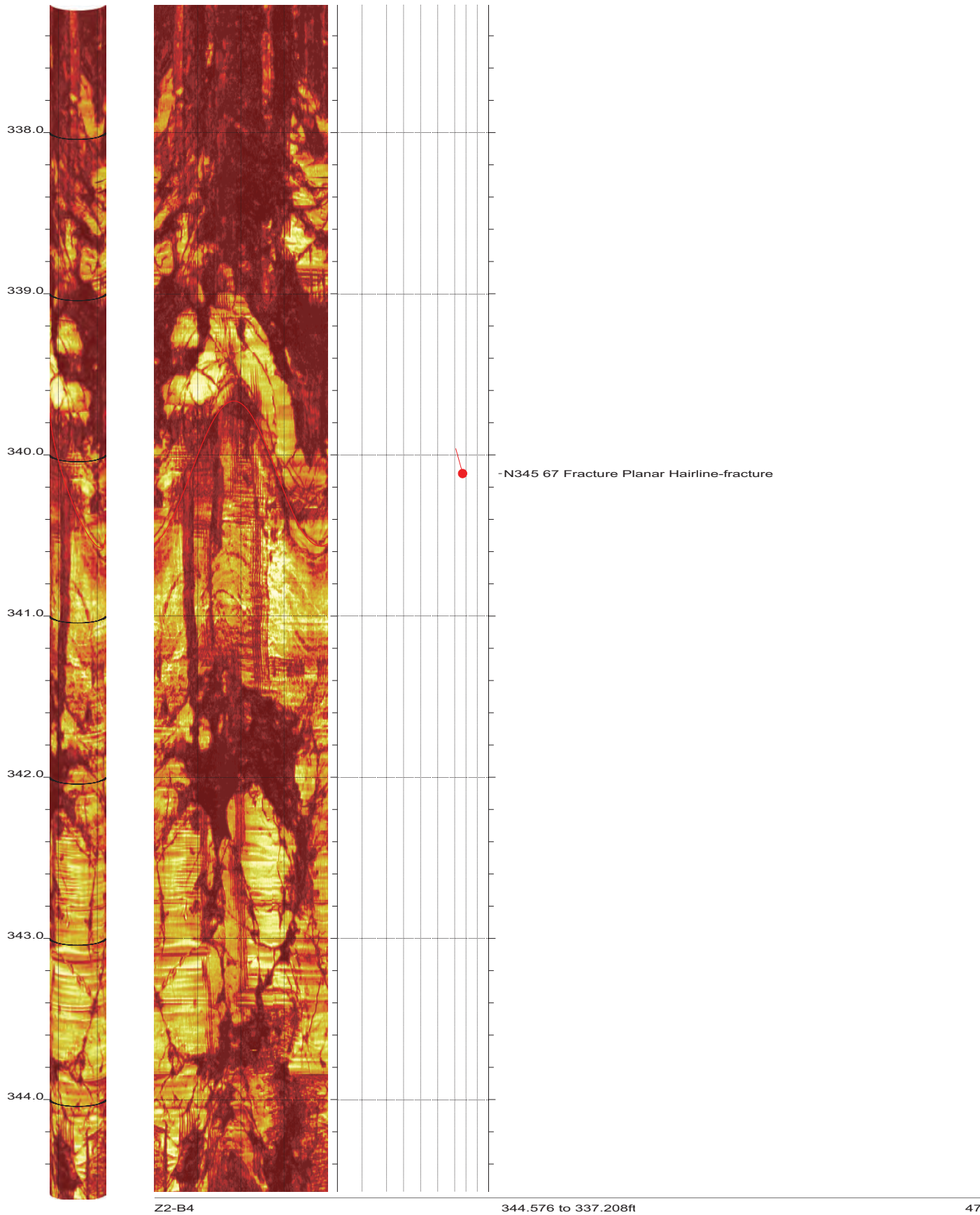
329.840 to 322.472ft

45

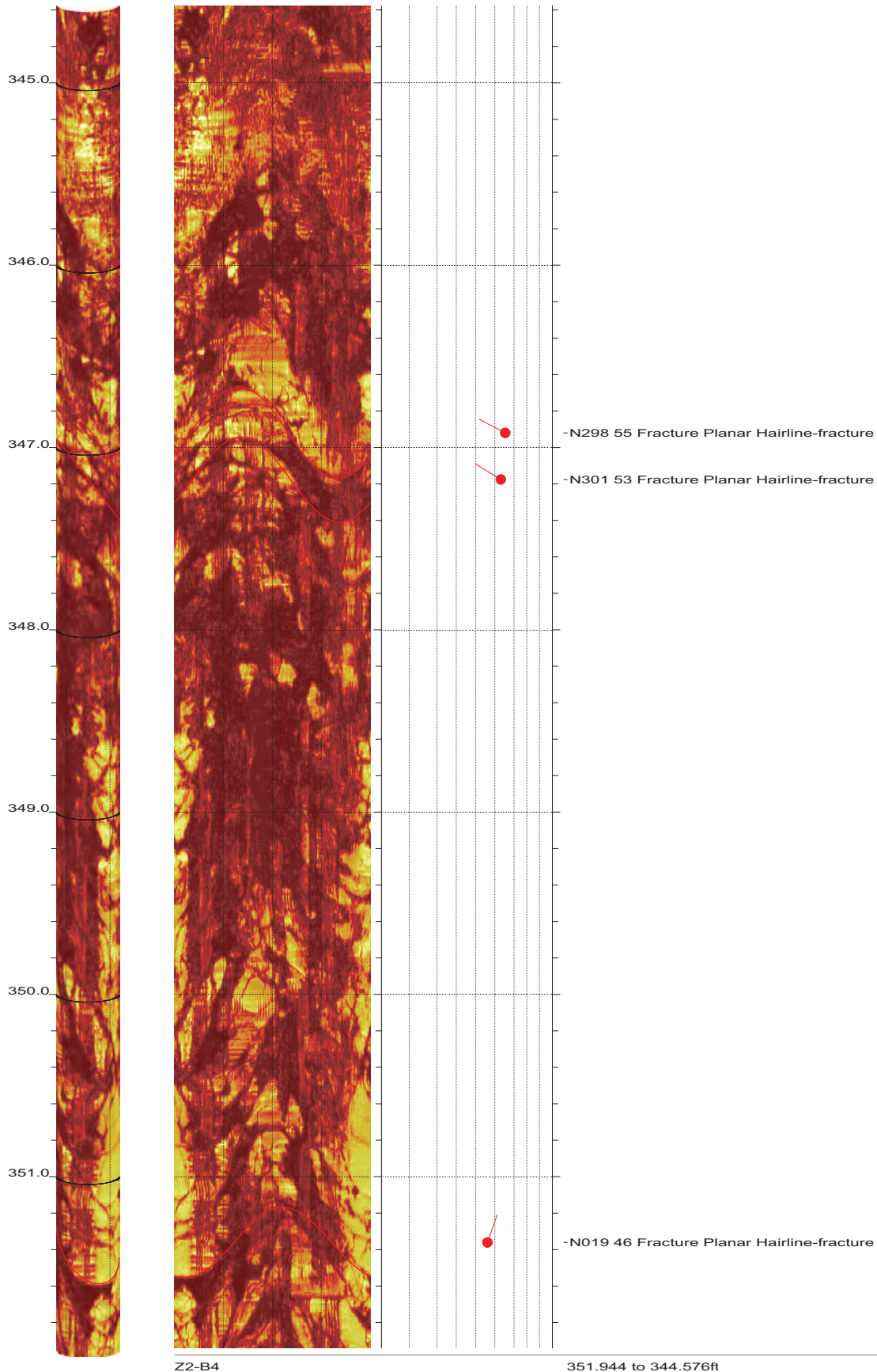
SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 45 of 52

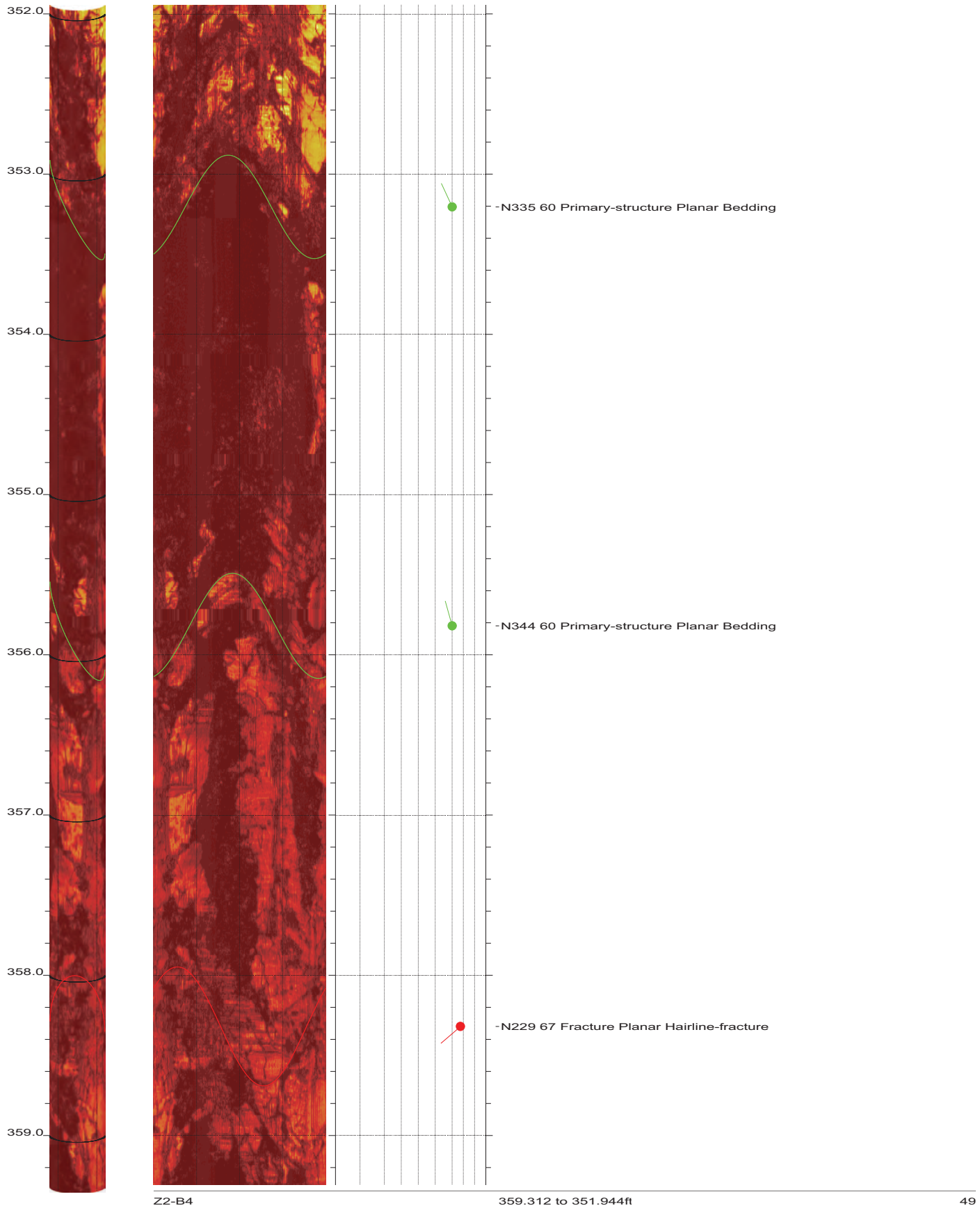


SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 46 of 52

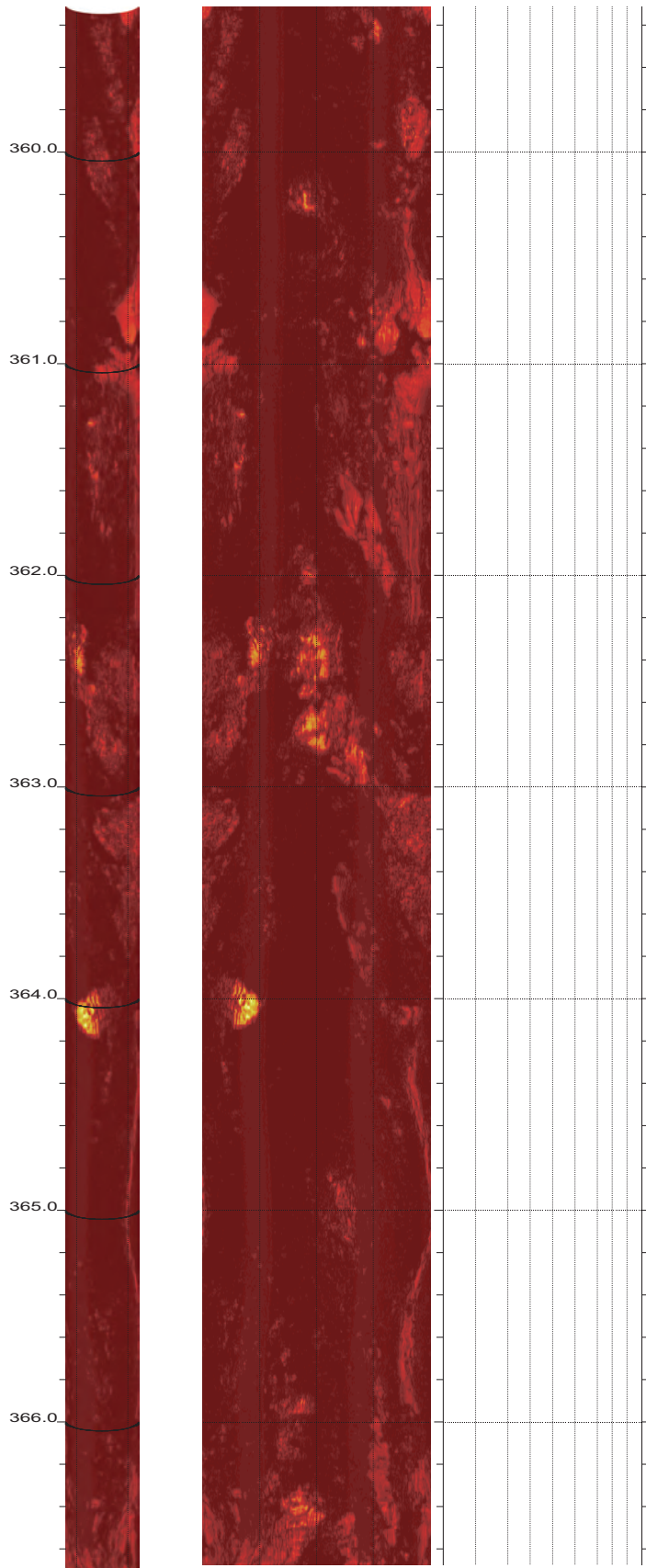


SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 47 of 52





SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 49 of 52

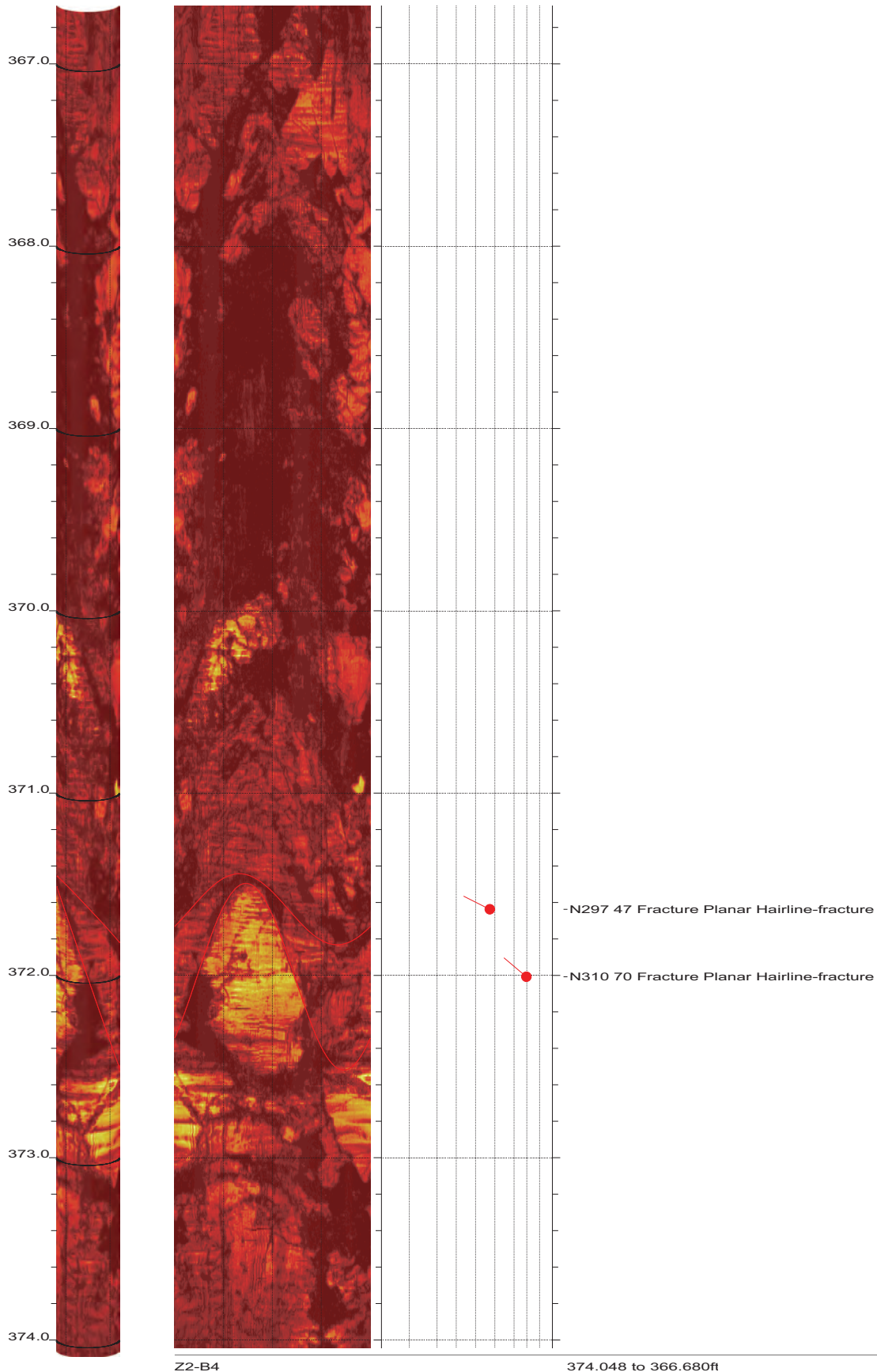


Z2-B4

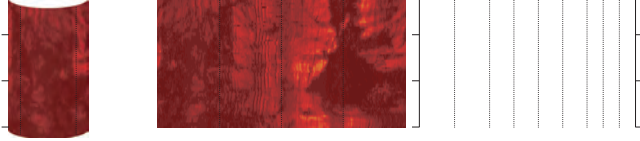
366.680 to 359.312ft

50

SR-710 Boring Z2-B4 Acoustic Televiewer Dips rev 1 Sheet 50 of 52









CASCADE DRILLING

Borehole: Z3-B1

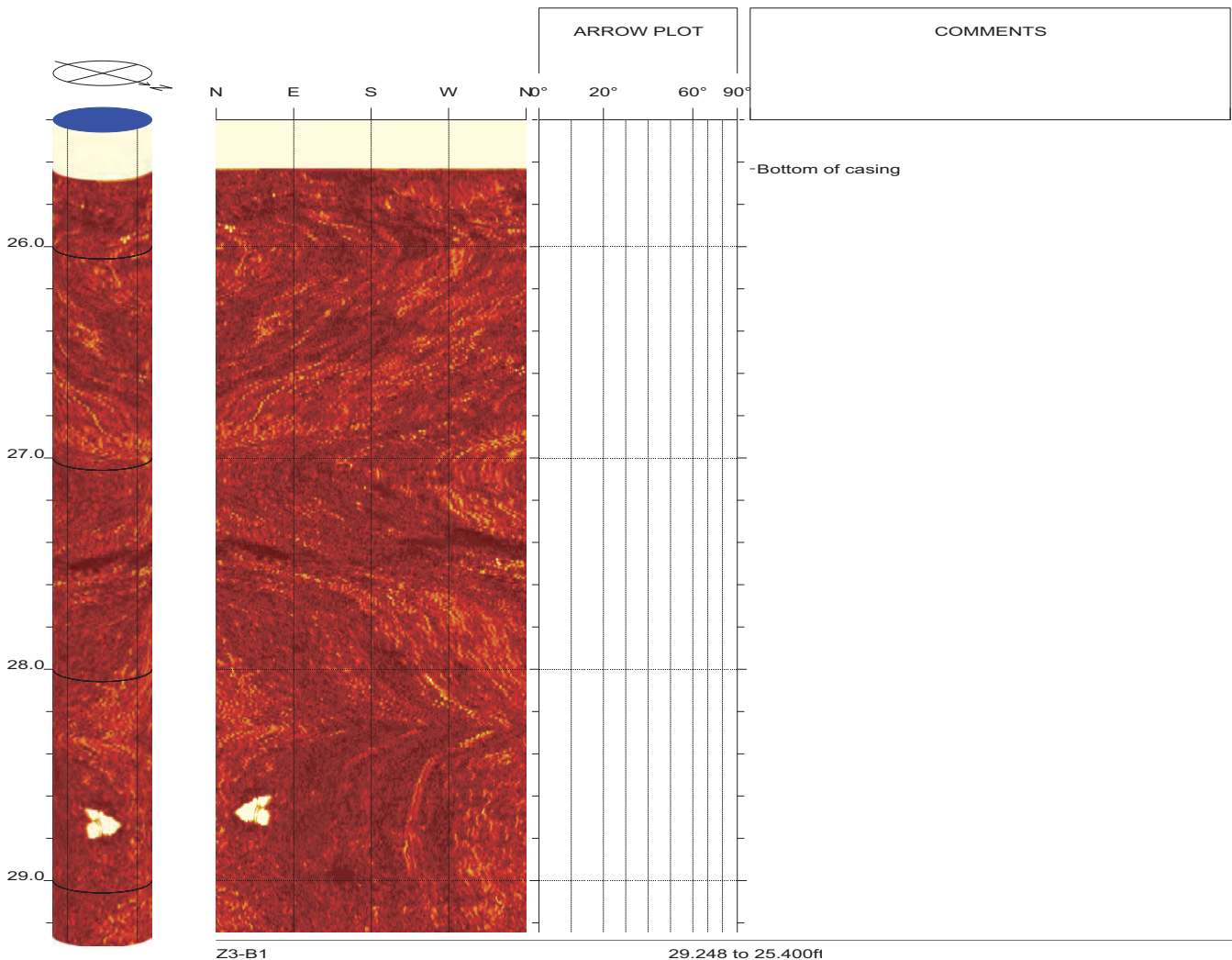
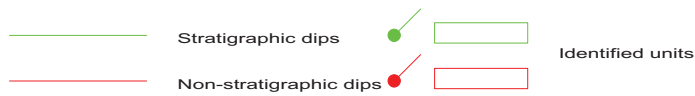
SR-710 TUNNEL INVESTIGATION

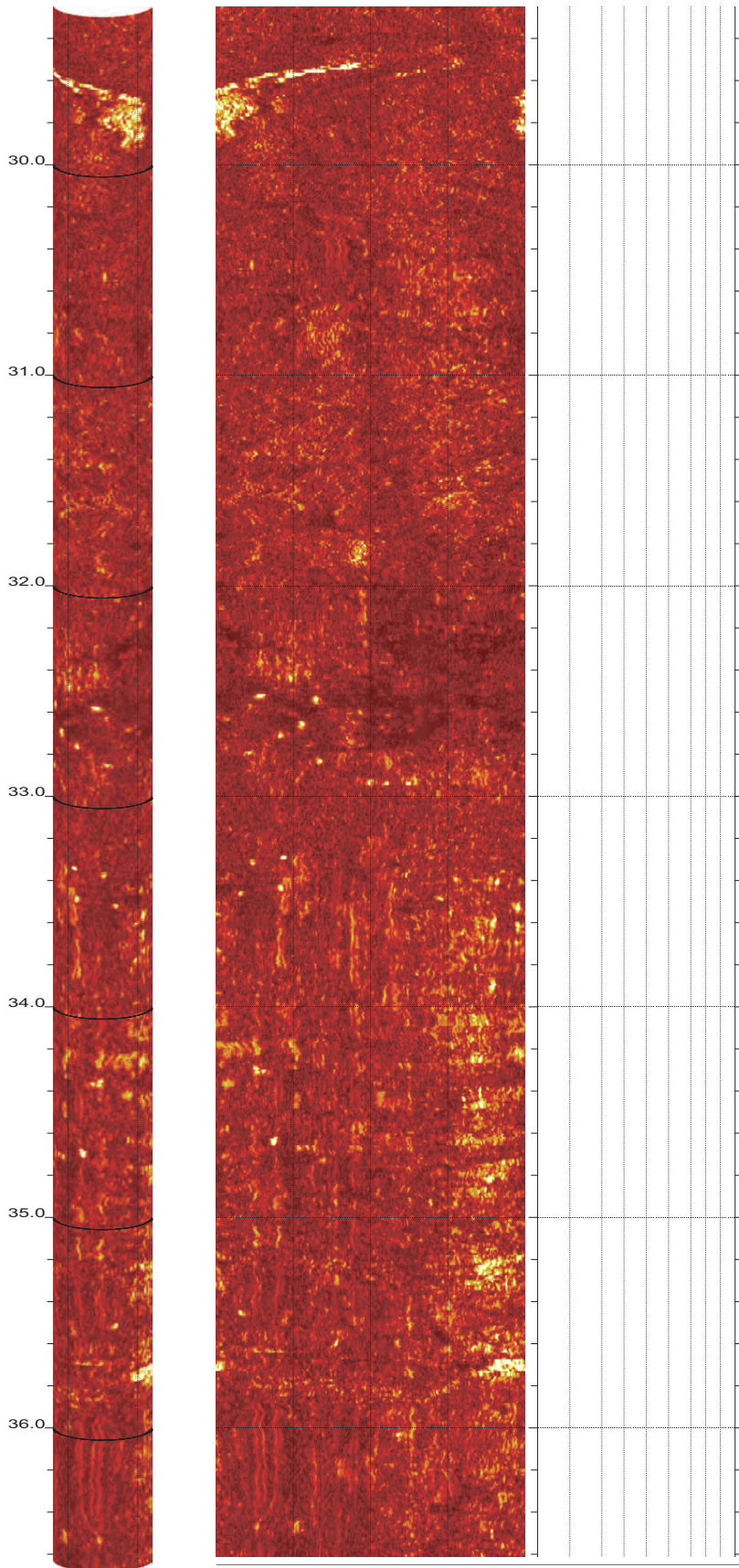
top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

Zone from 300.200 to 25.400ft  
 Format: BHTV-NESWN

Borehole diam: 5.600inch  
 Vertical = borehole-axis  
 Image: Amplitude



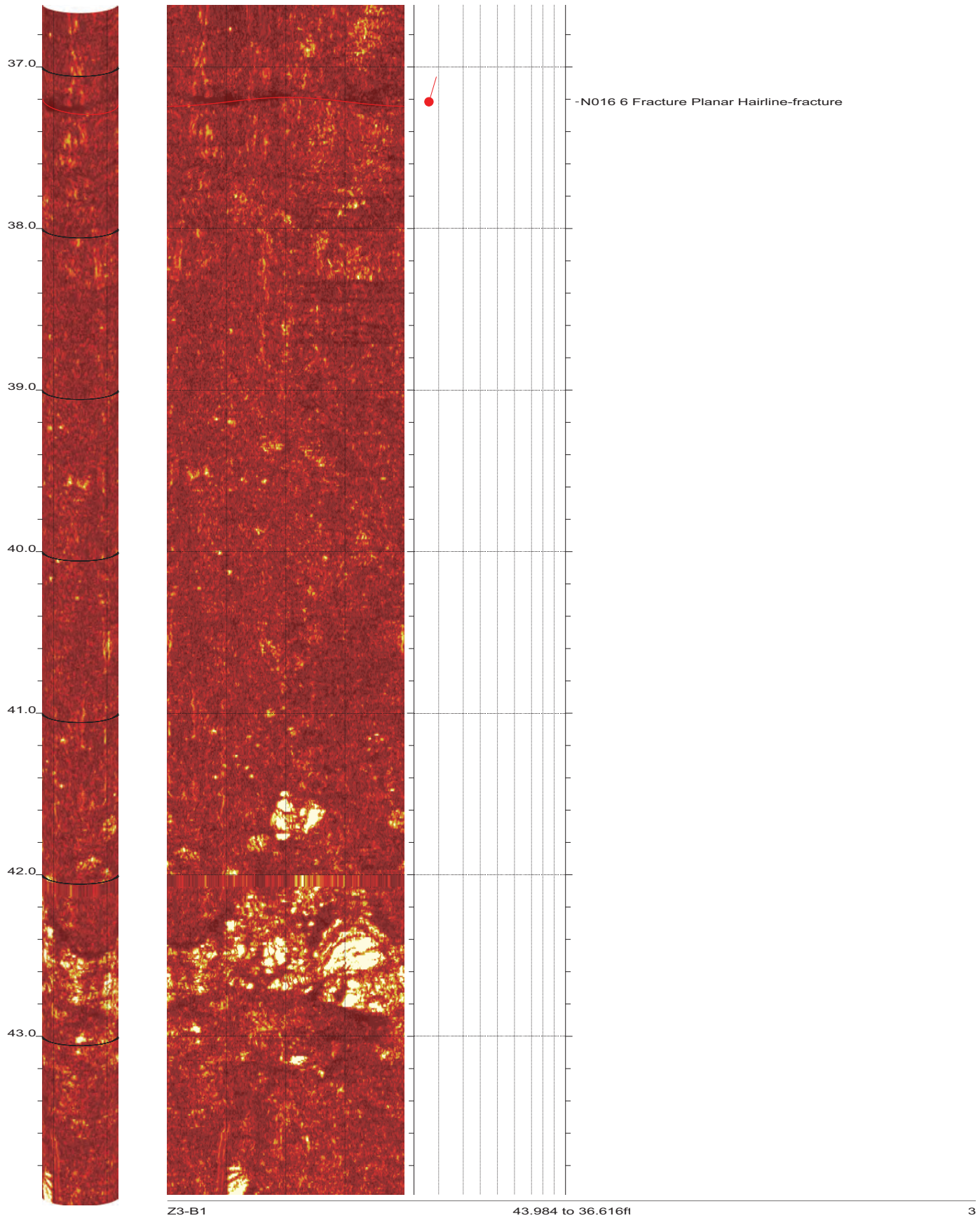


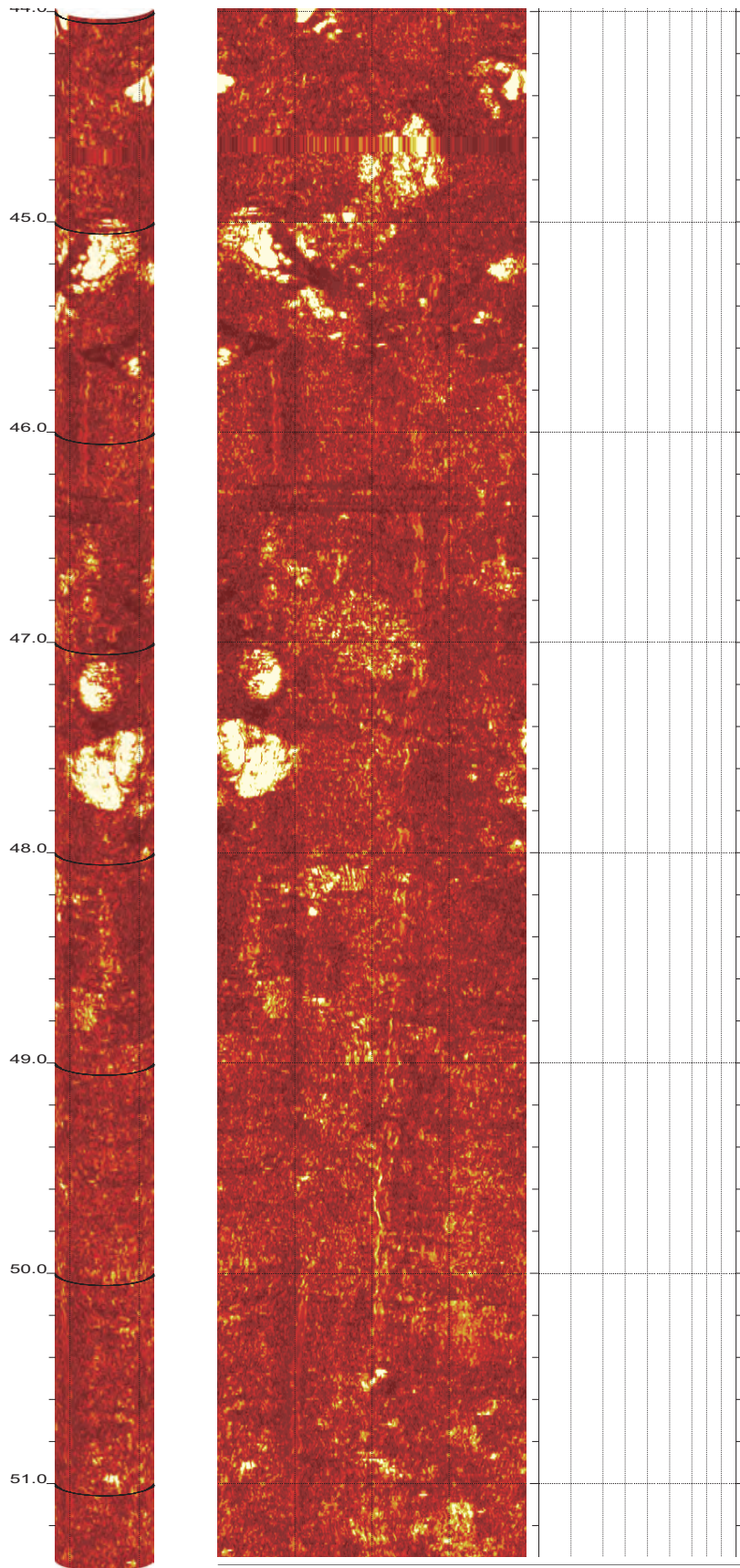
Z3-B1

36.616 to 29.248ft

2

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 2 of 38



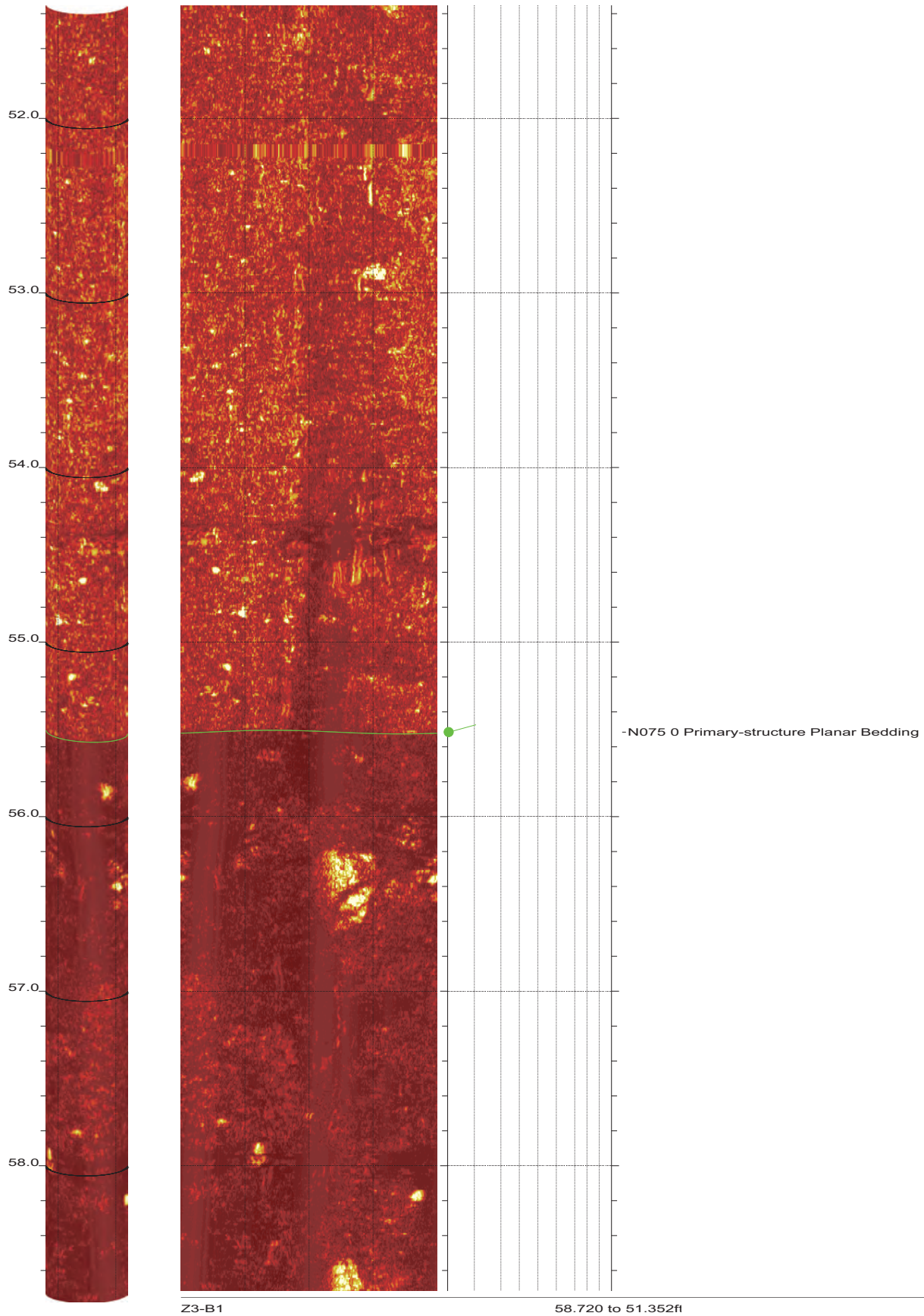


Z3-B1

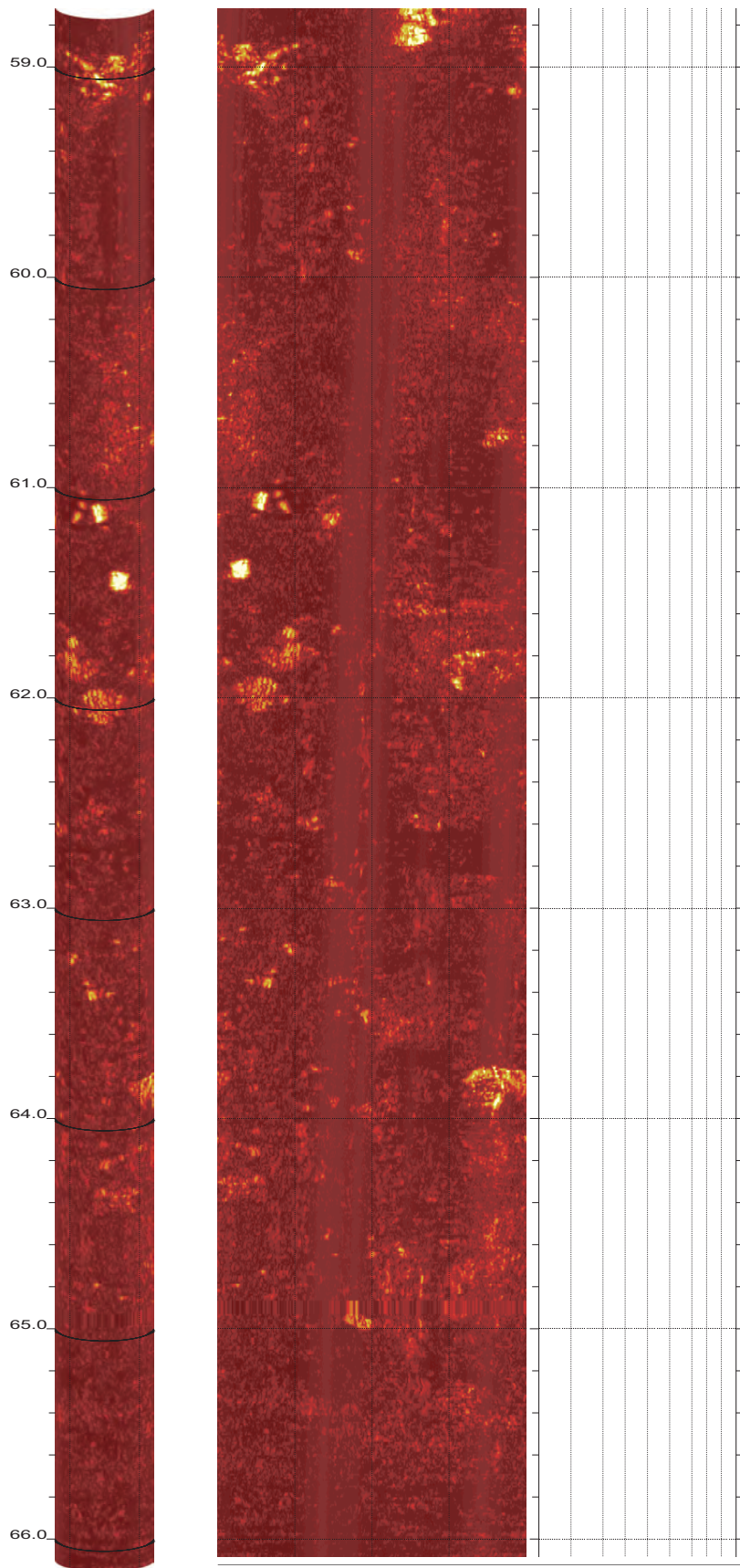
51.352 to 43.984ft

4

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 4 of 38



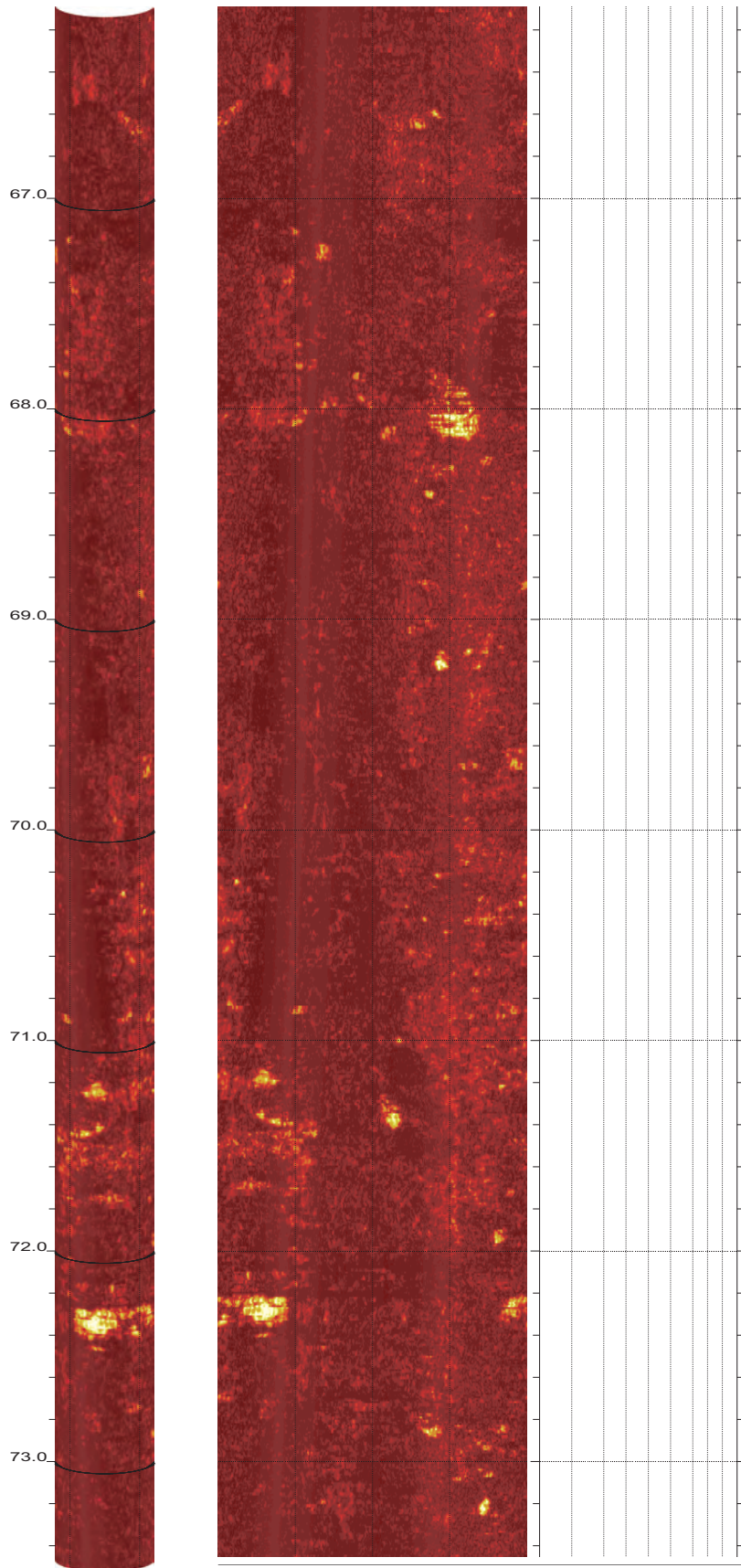
SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 5 of 38



Z3-B1

66.088 to 58.720ft

6

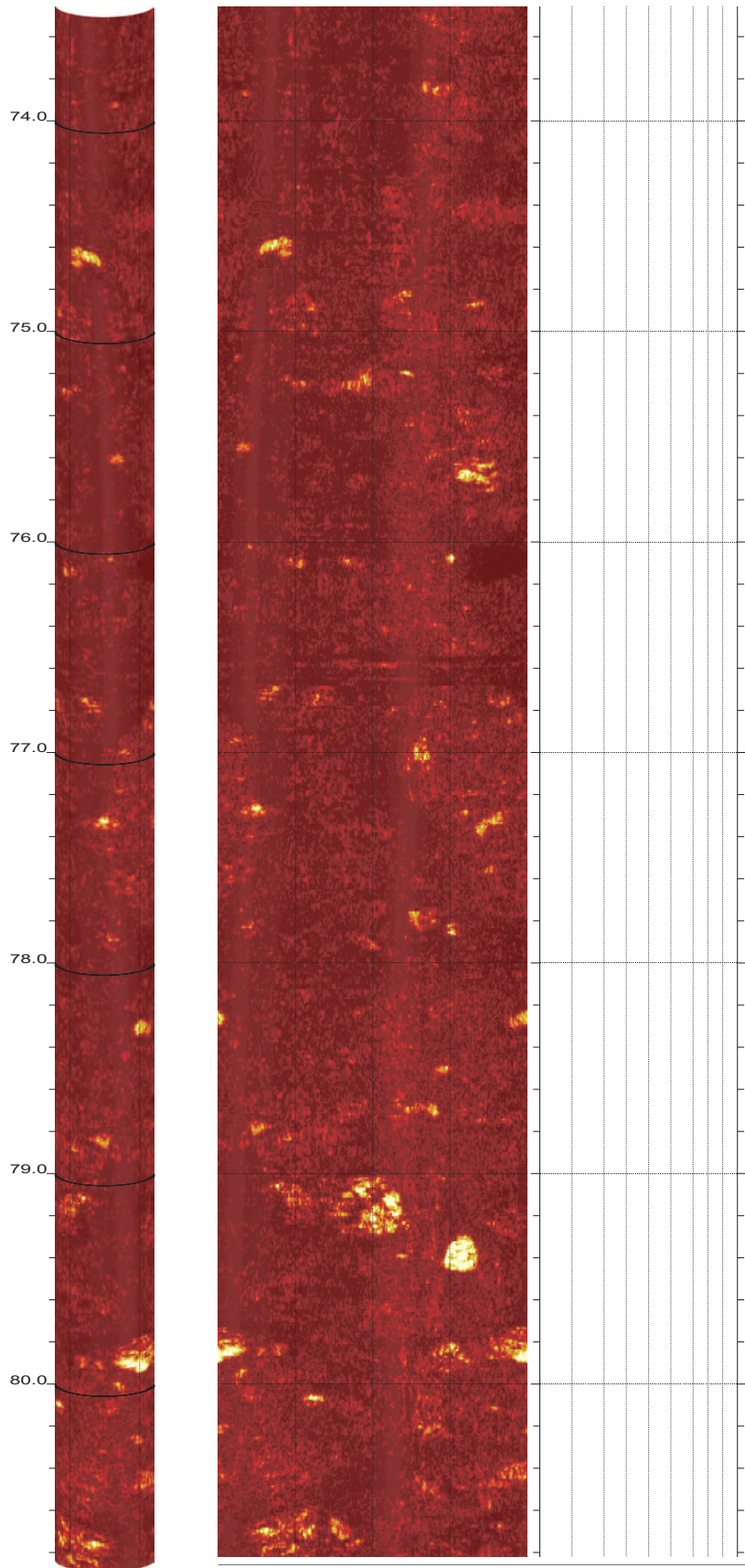


Z3-B1

73.456 to 66.088ft

7

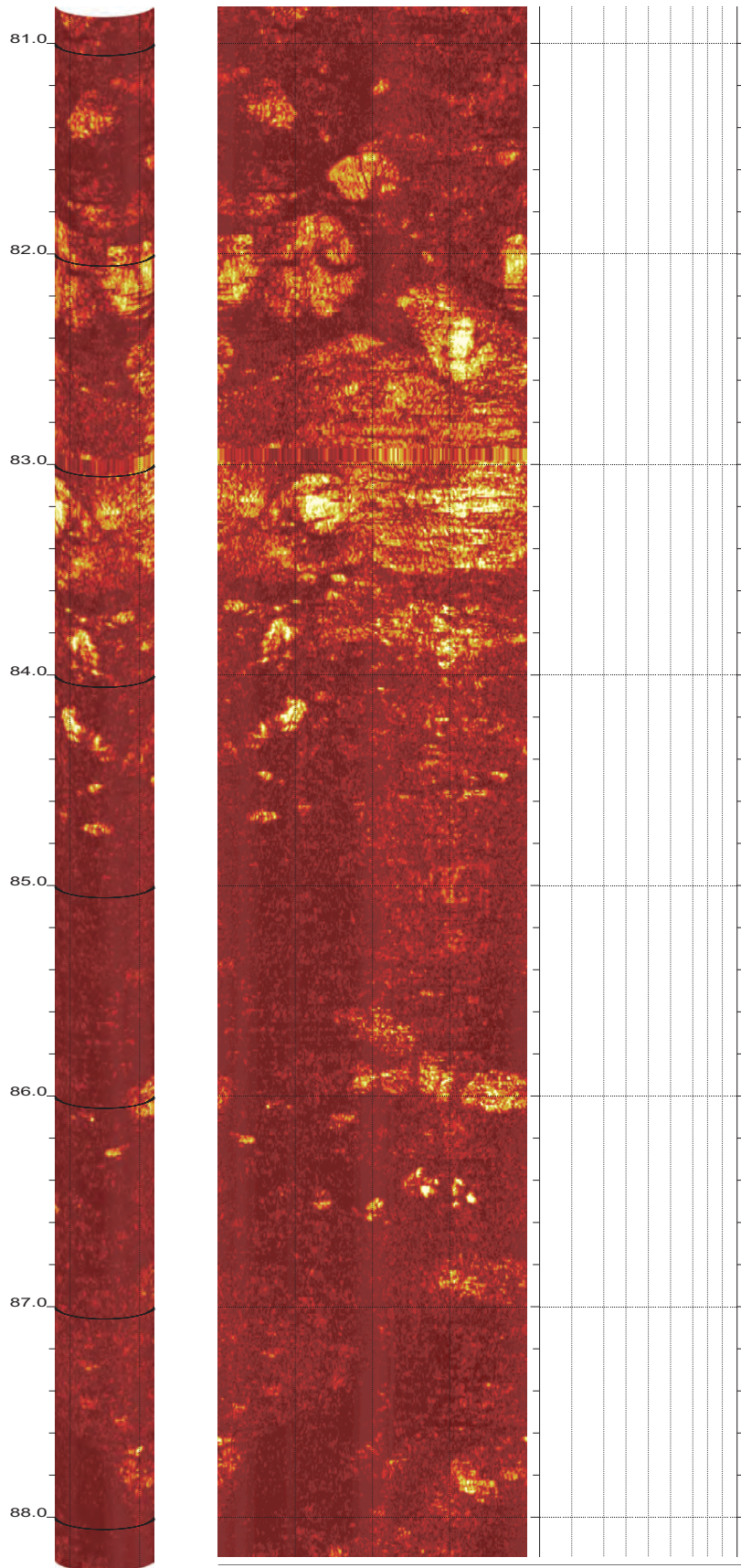




Z3-B1

80.824 to 73.456ft

8

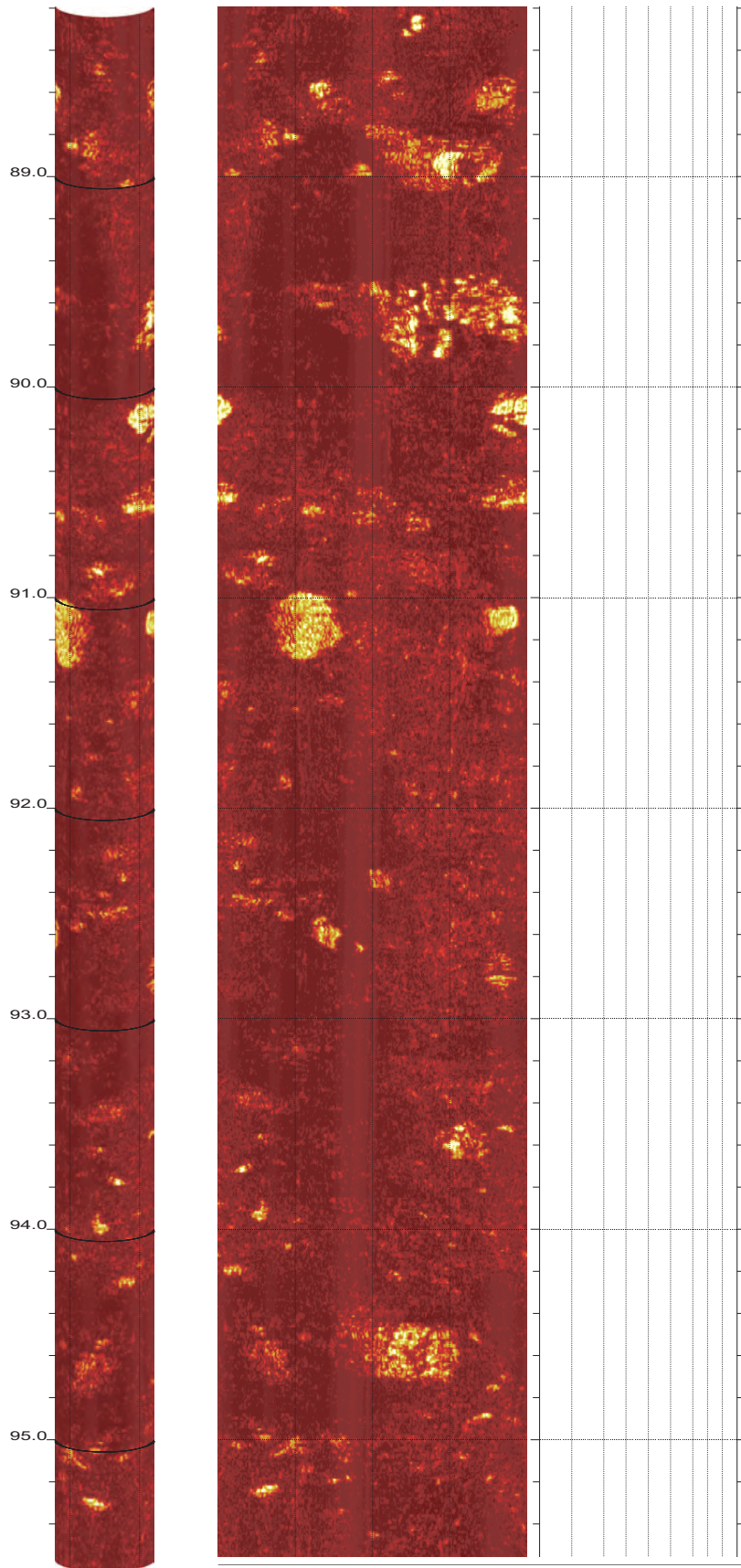


Z3-B1

88.192 to 80.824ft

9

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 9 of 38

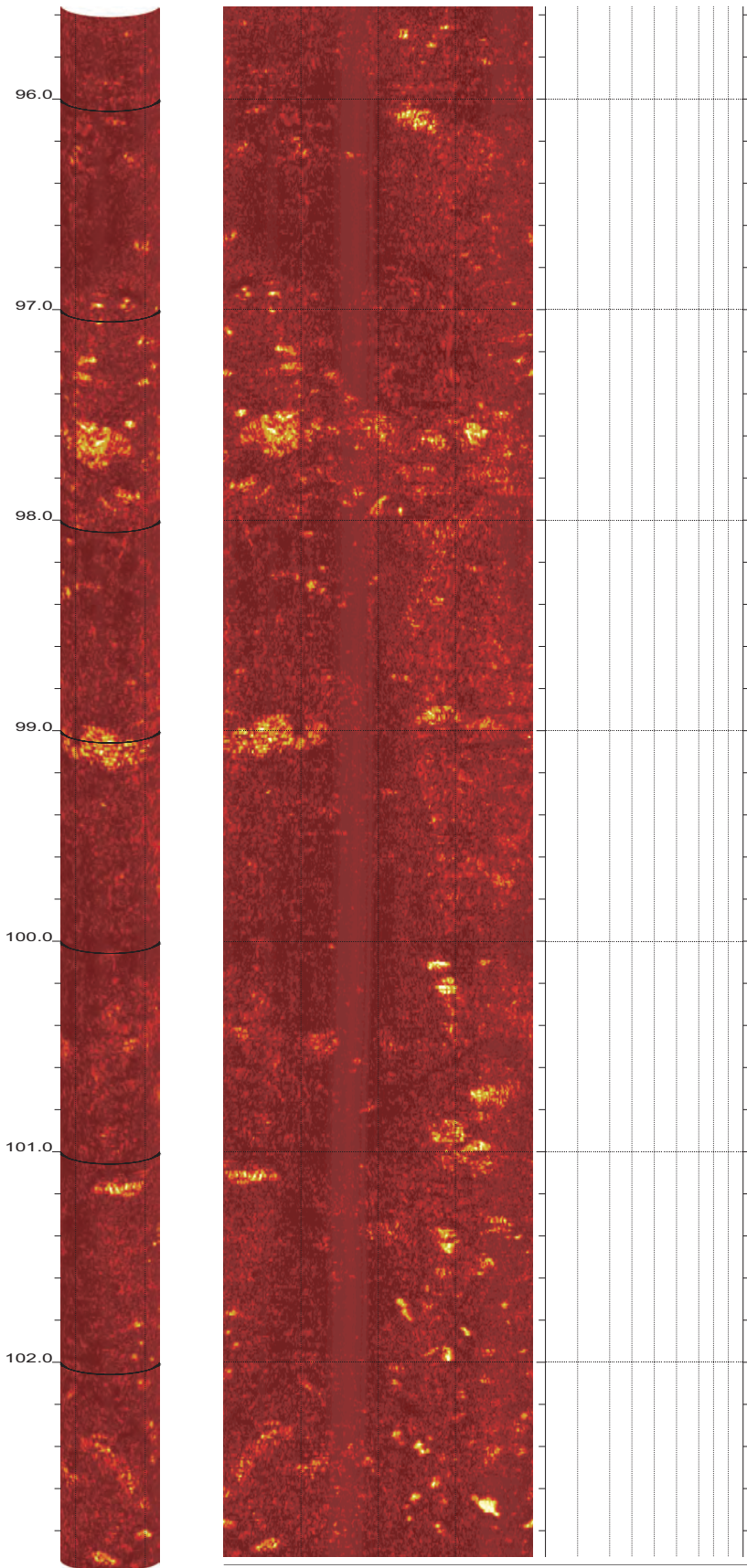


Z3-B1

95.560 to 88.192ft

10

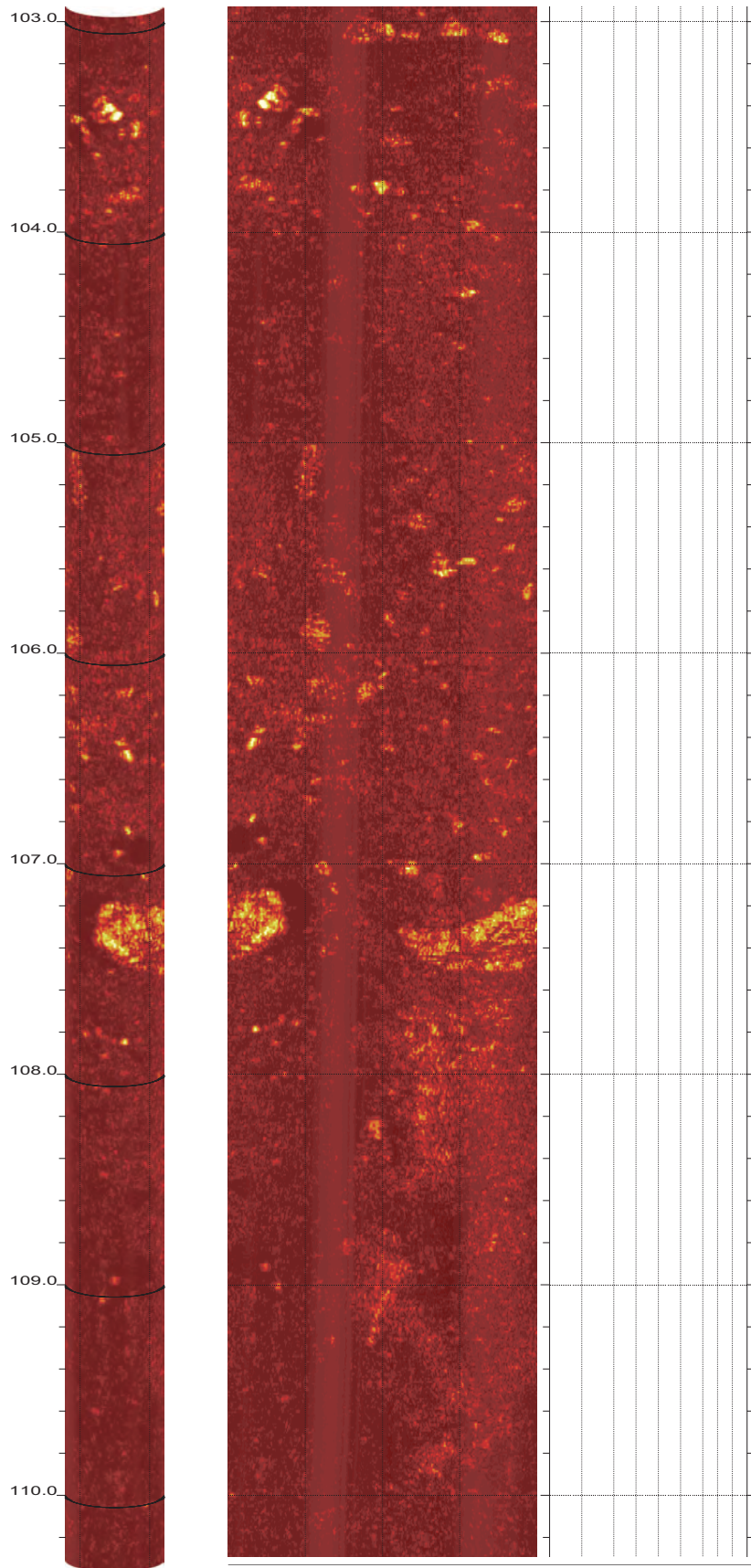
SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 10 of 38



Z3-B1

102.928 to 95.560ft

11

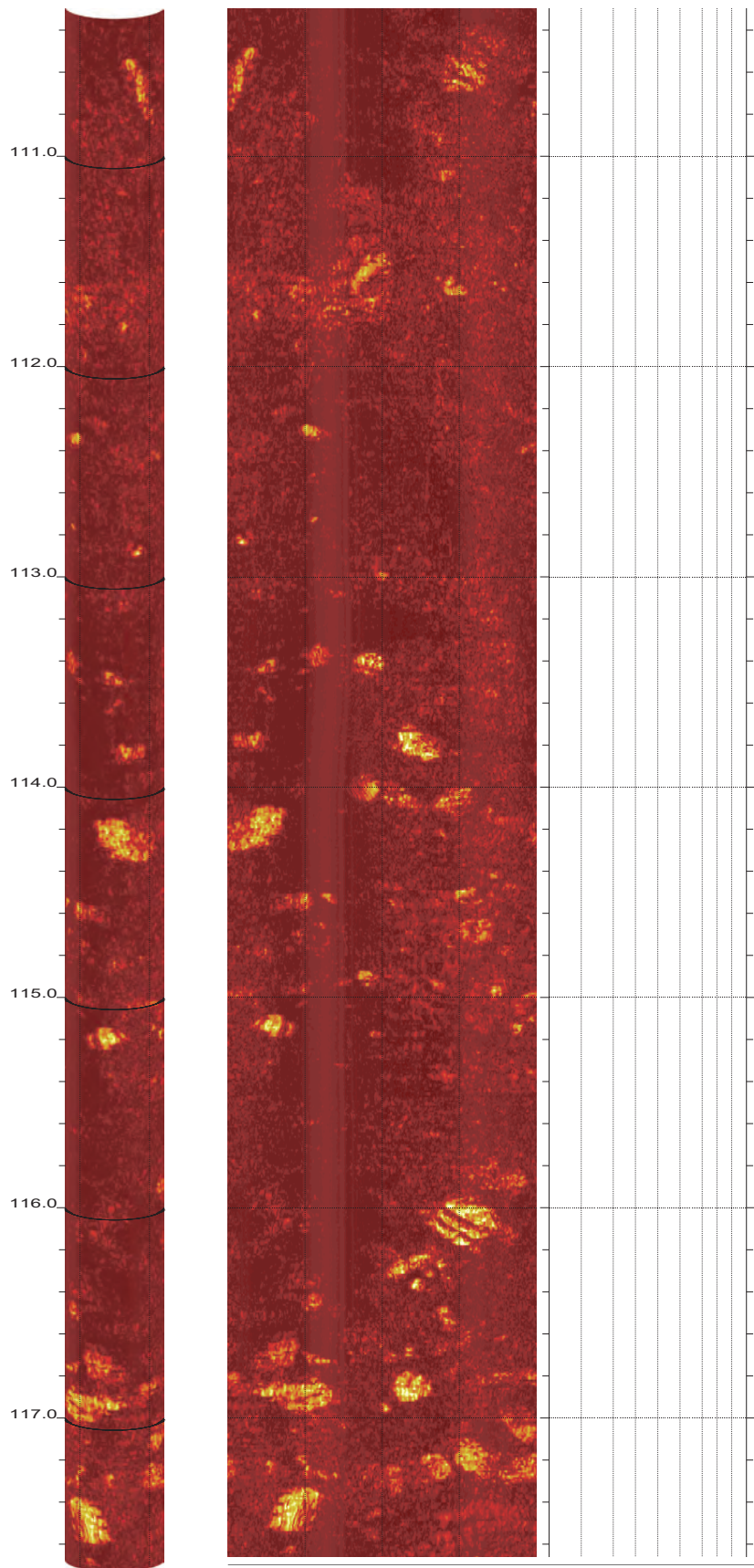


Z3-B1

110.296 to 102.928ft

12

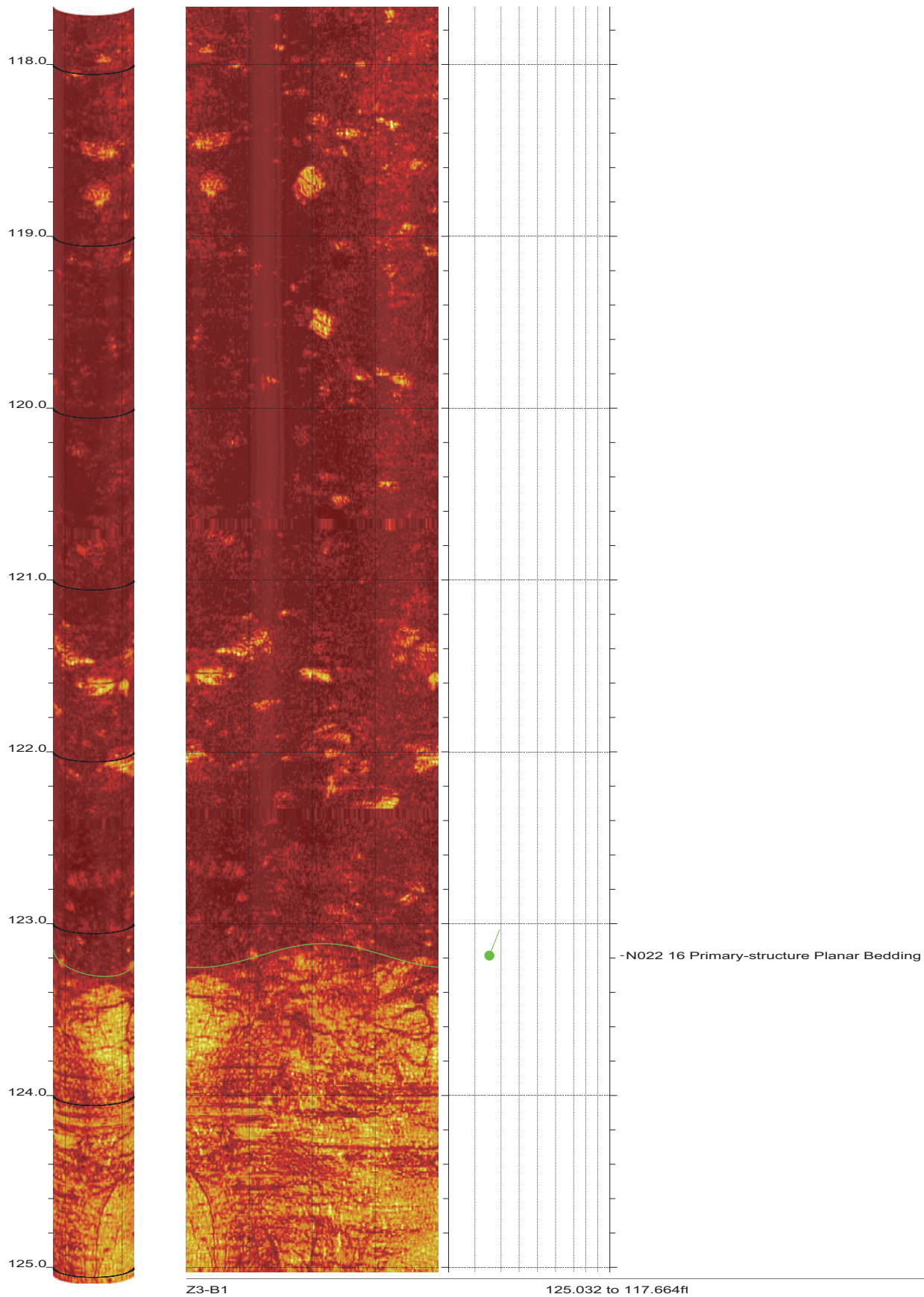
SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 12 of 38

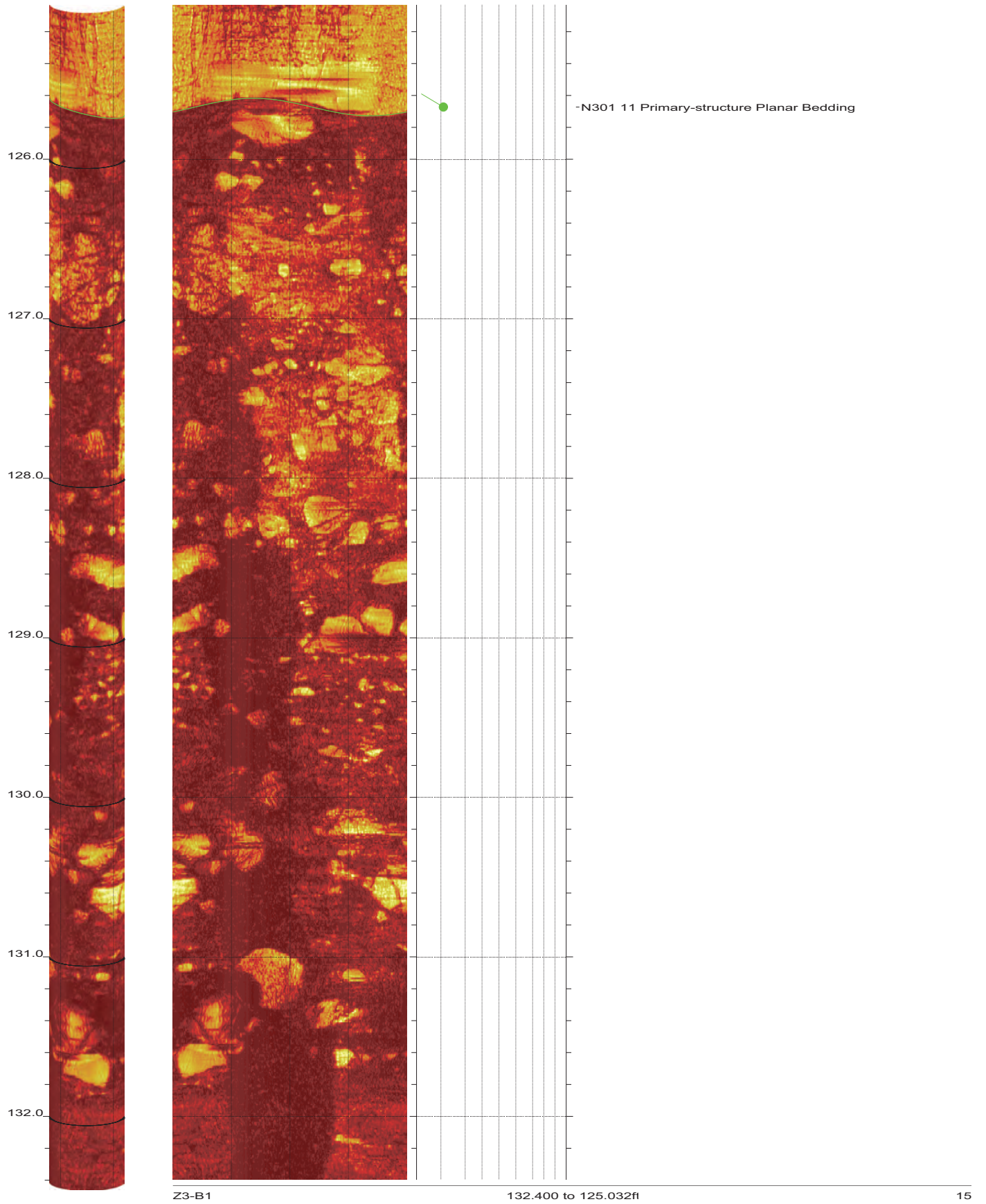


Z3-B1

117.664 to 110.296ft

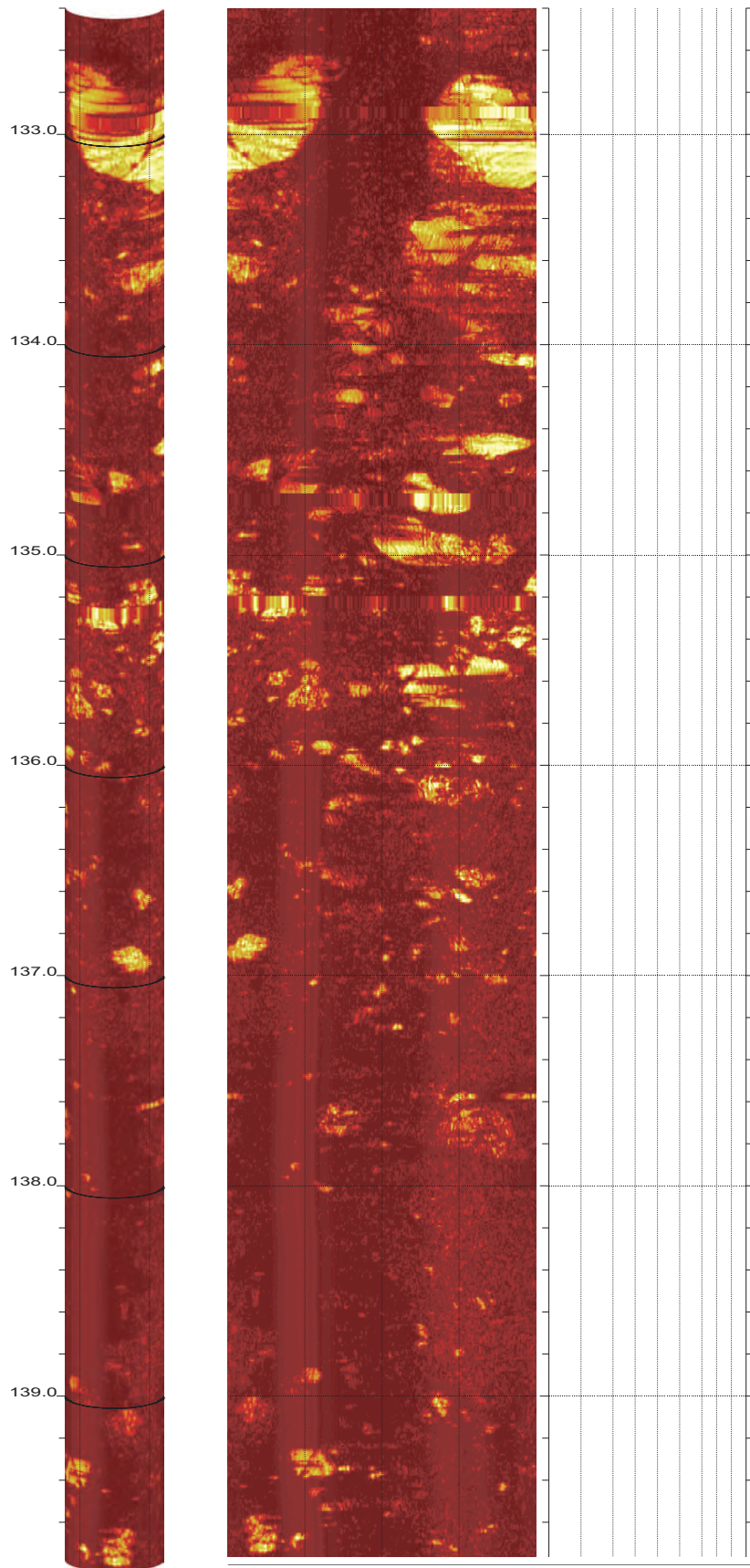
13





SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 15 of 38



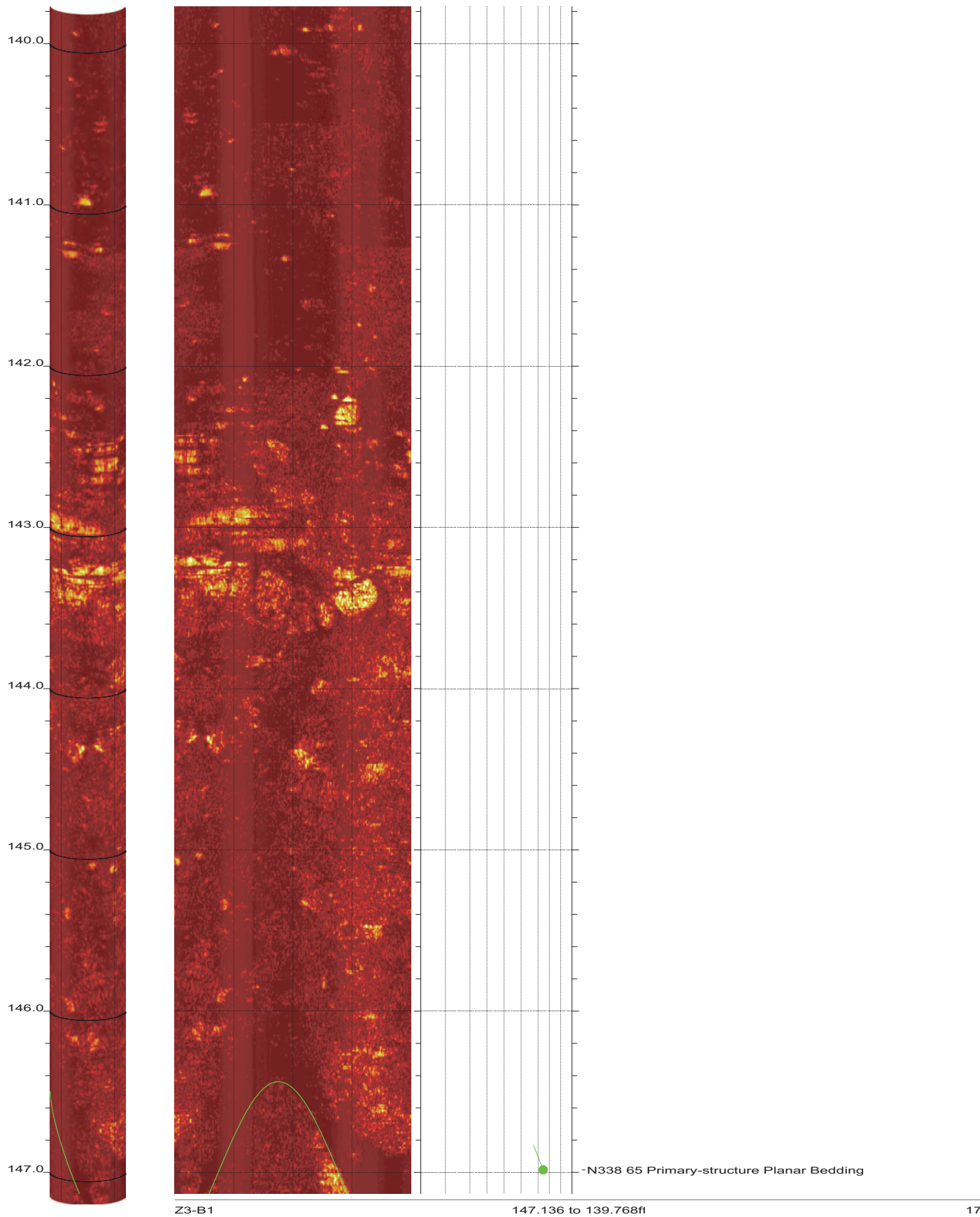


Z3-B1

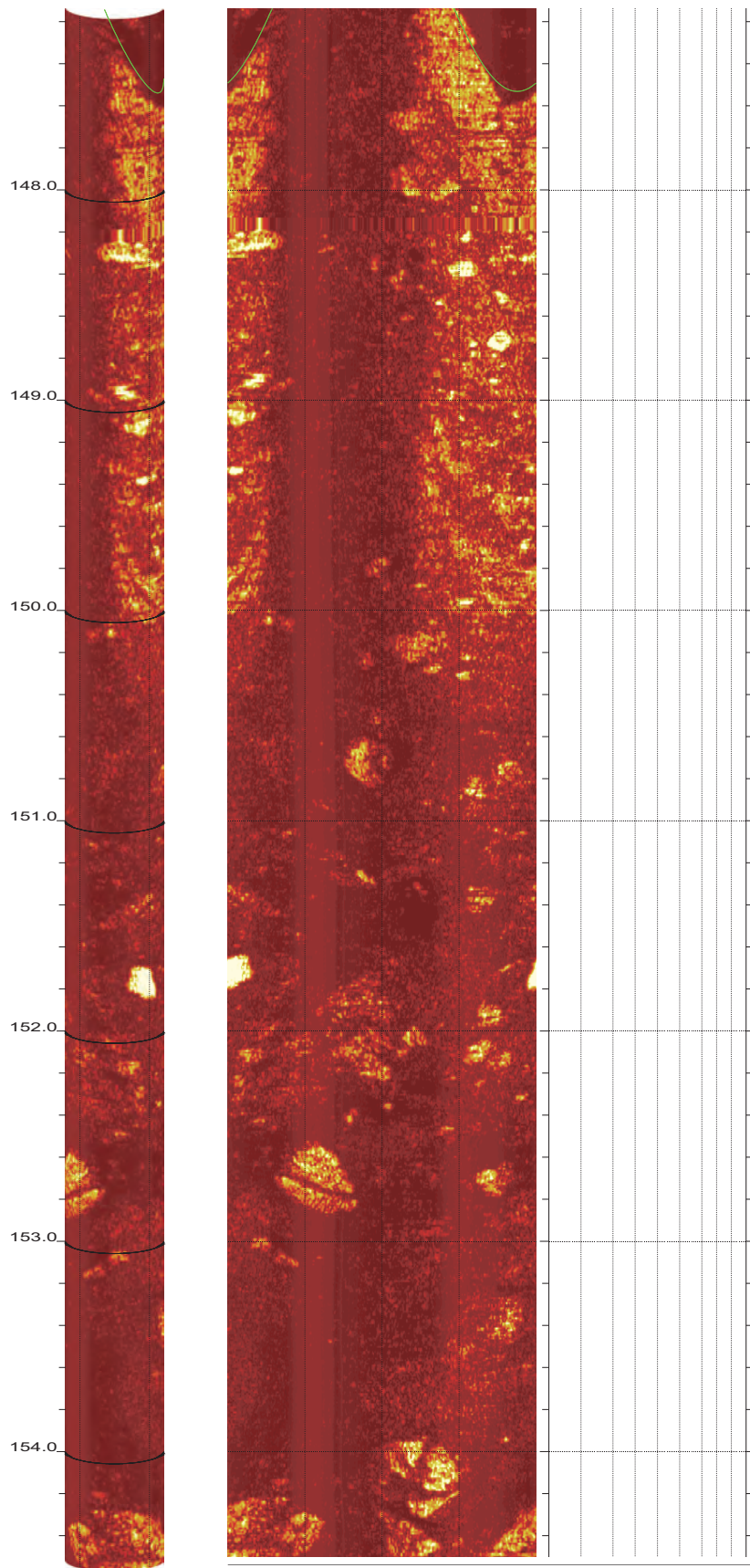
139.768 to 132.400ft

16

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 16 of 38



SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 17 of 38

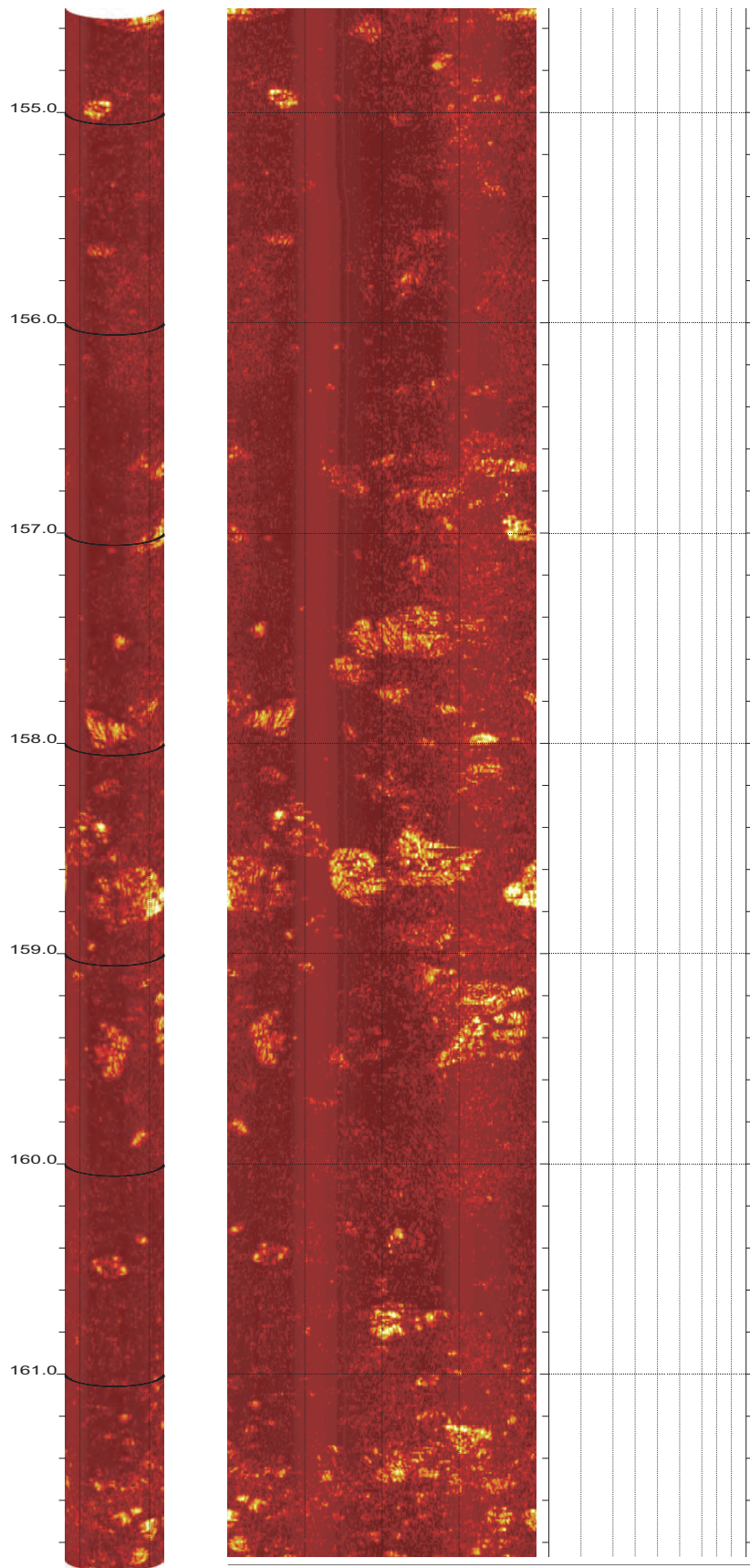


Z3-B1

154.504 to 147.136ft

18

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 18 of 38

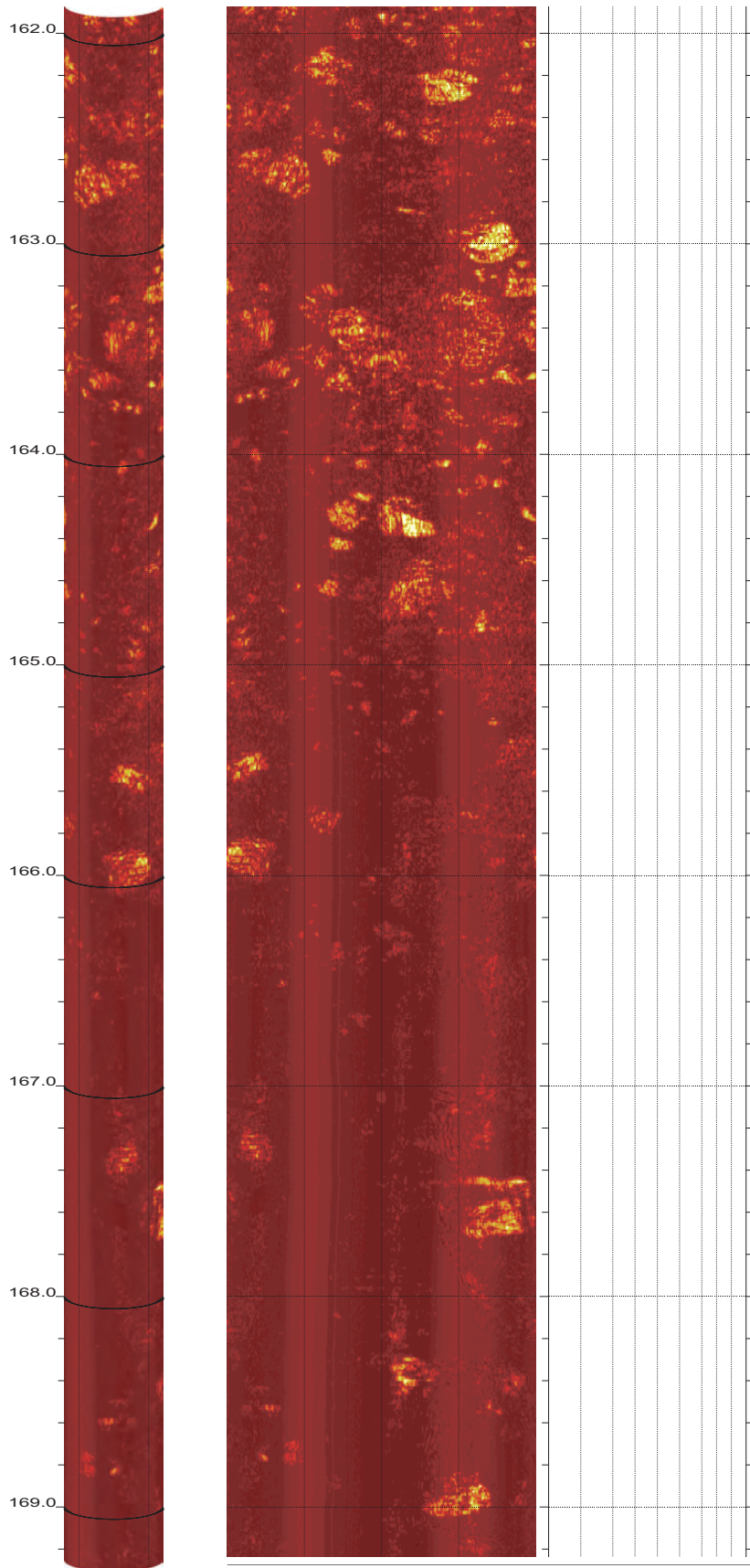


Z3-B1

161.872 to 154.504ft

19

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 19 of 38

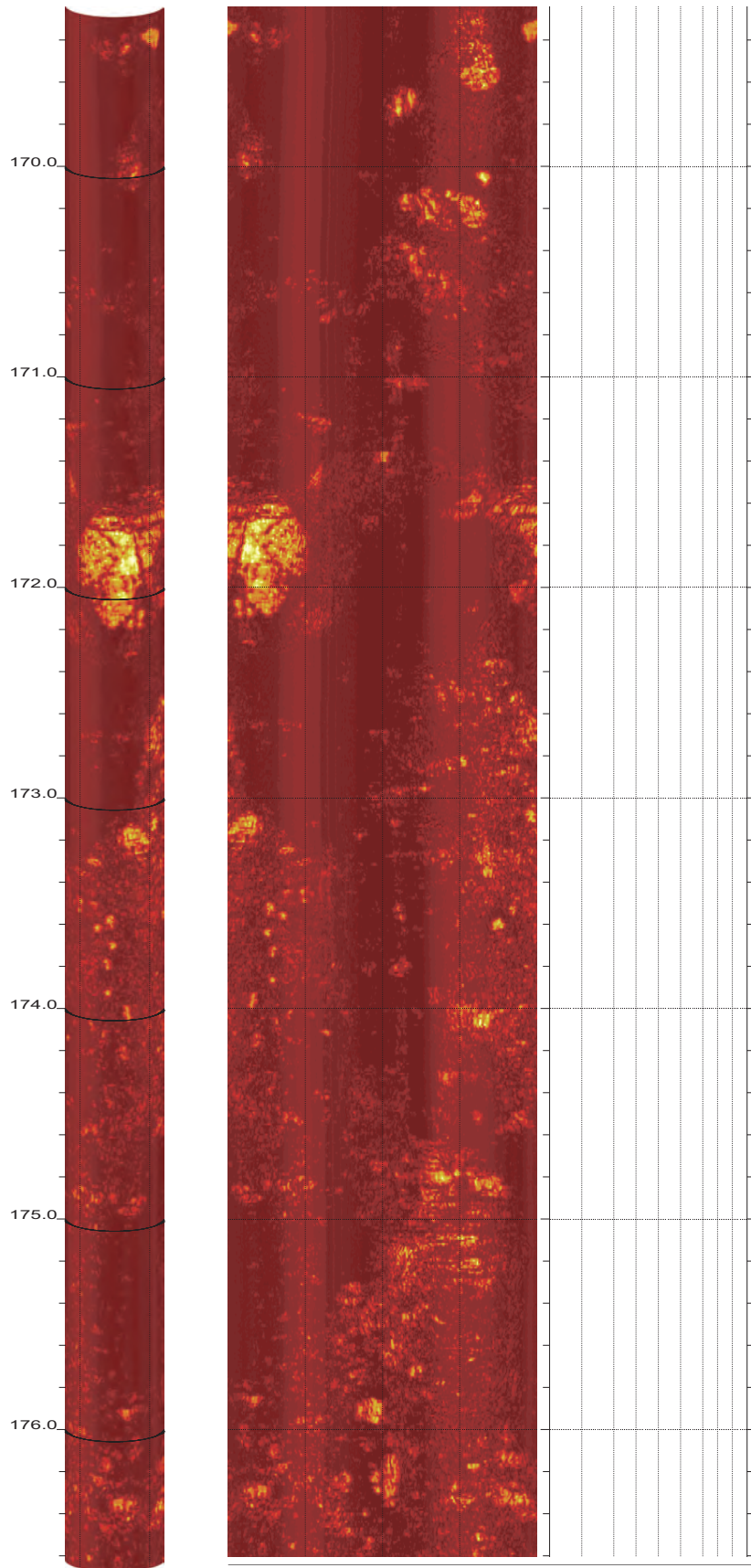


Z3-B1

169.240 to 161.872ft

20

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 20 of 38

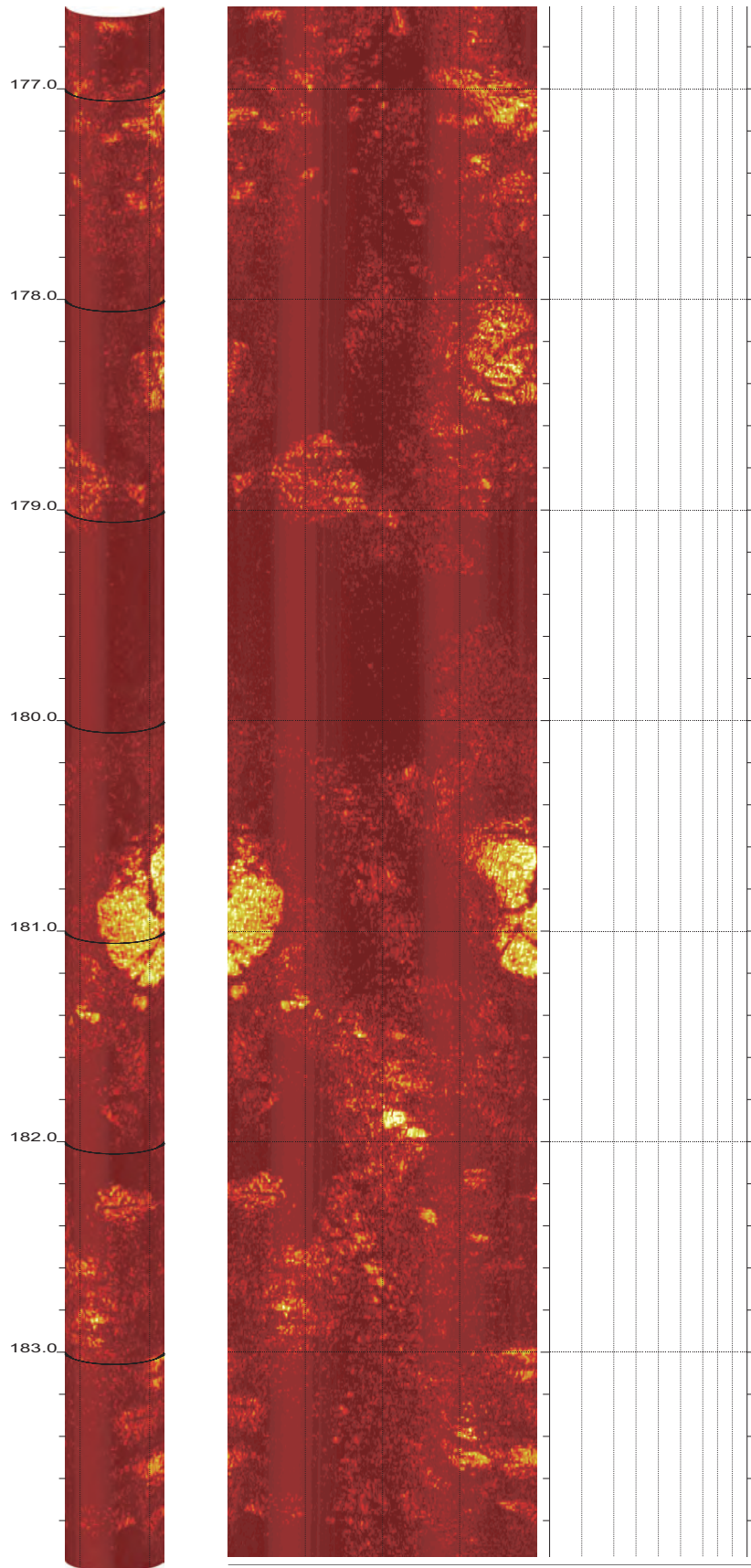


Z3-B1

176.608 to 169.240ft

21

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 21 of 38

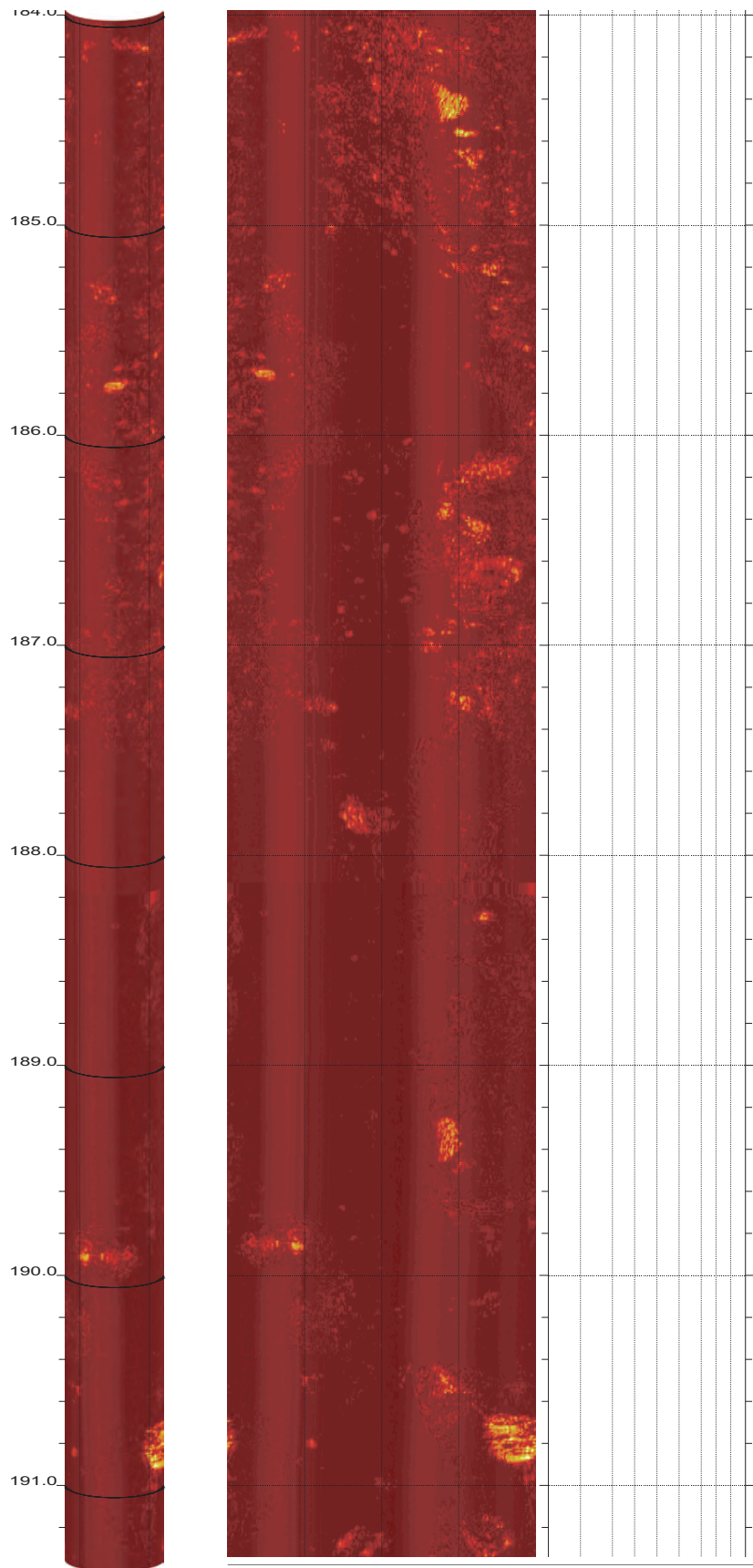


Z3-B1

183.976 to 176.608ft

22

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 22 of 38



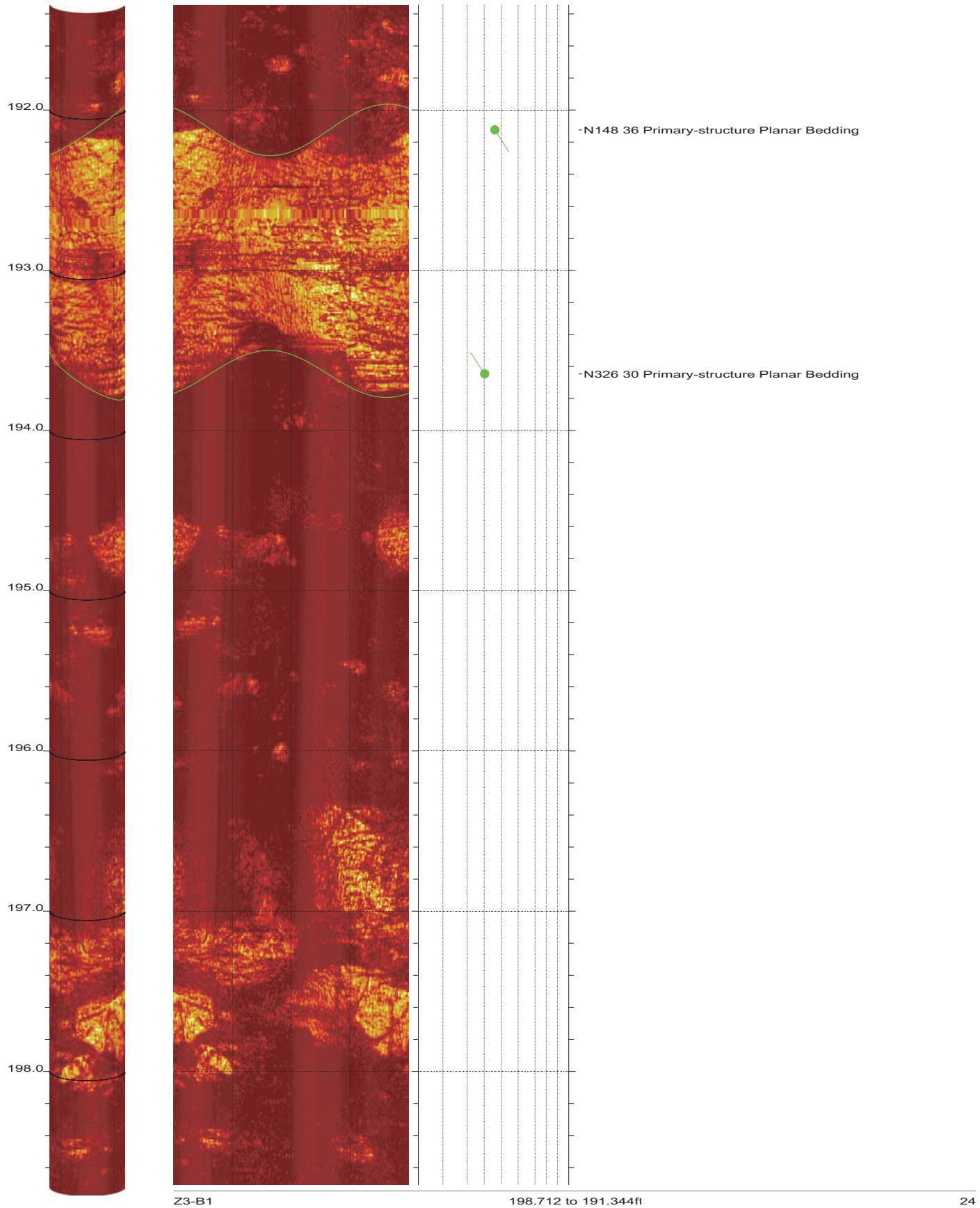
Z3-B1

191.344 to 183.976ft

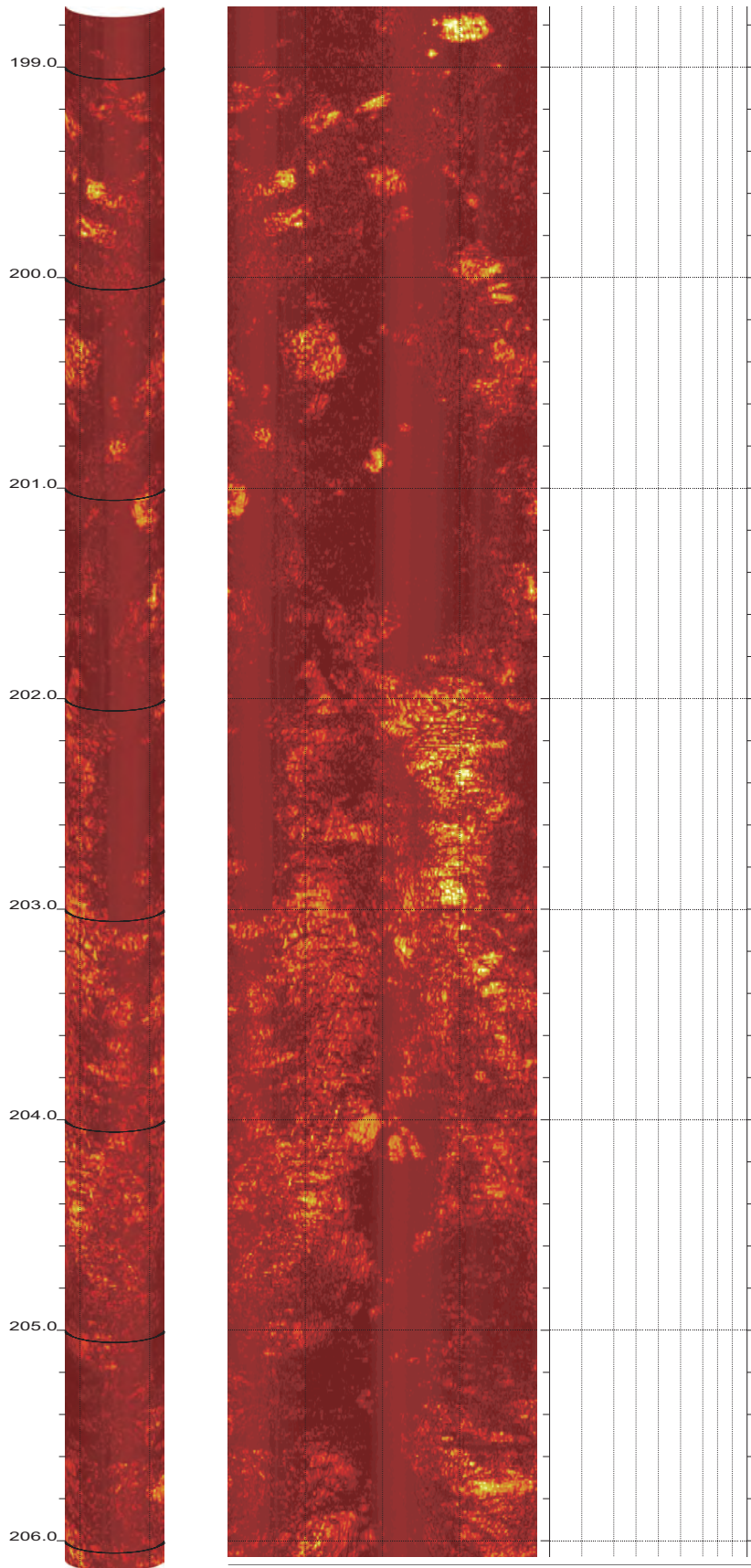
23

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 23 of 38





SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 24 of 38

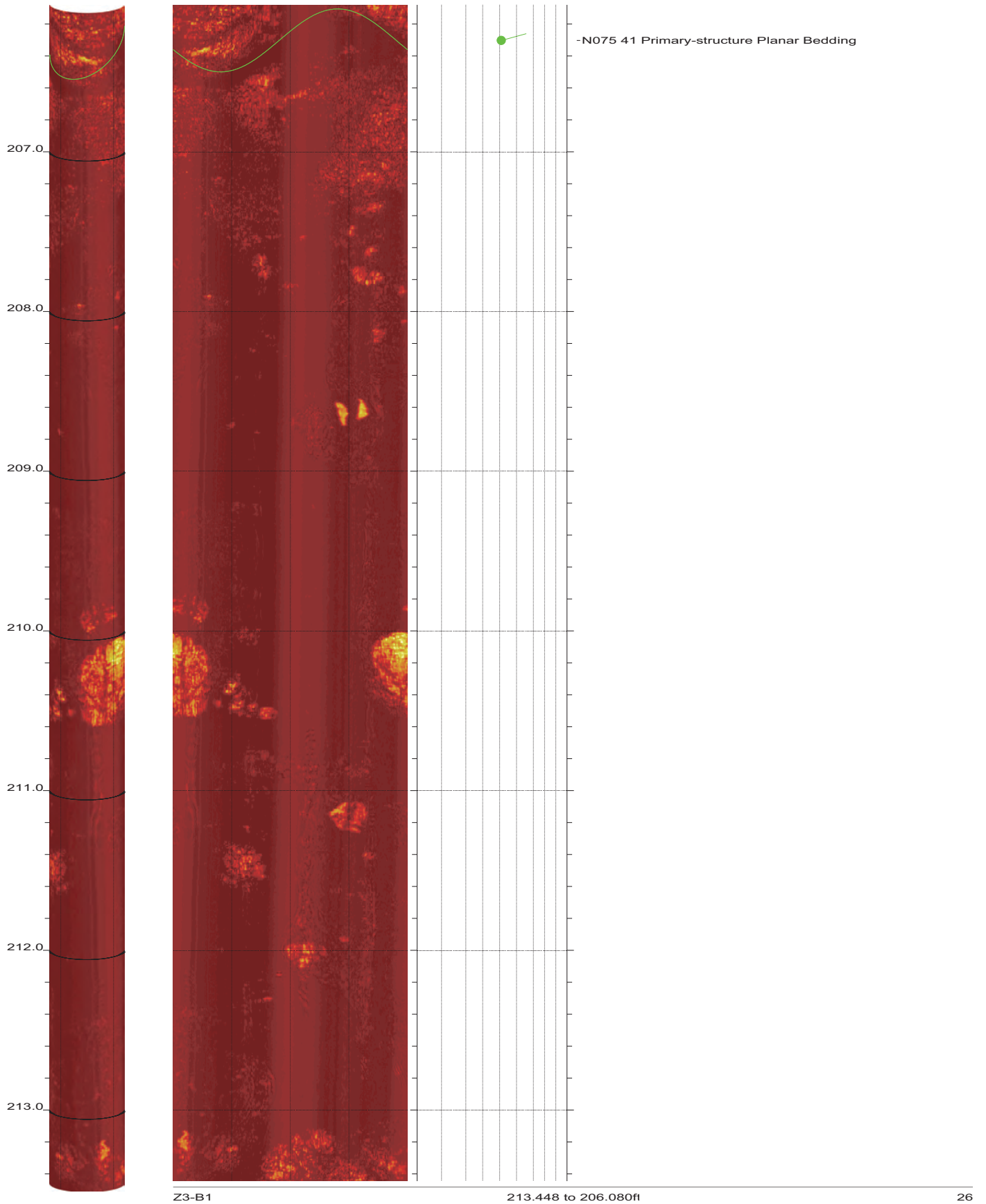


Z3-B1

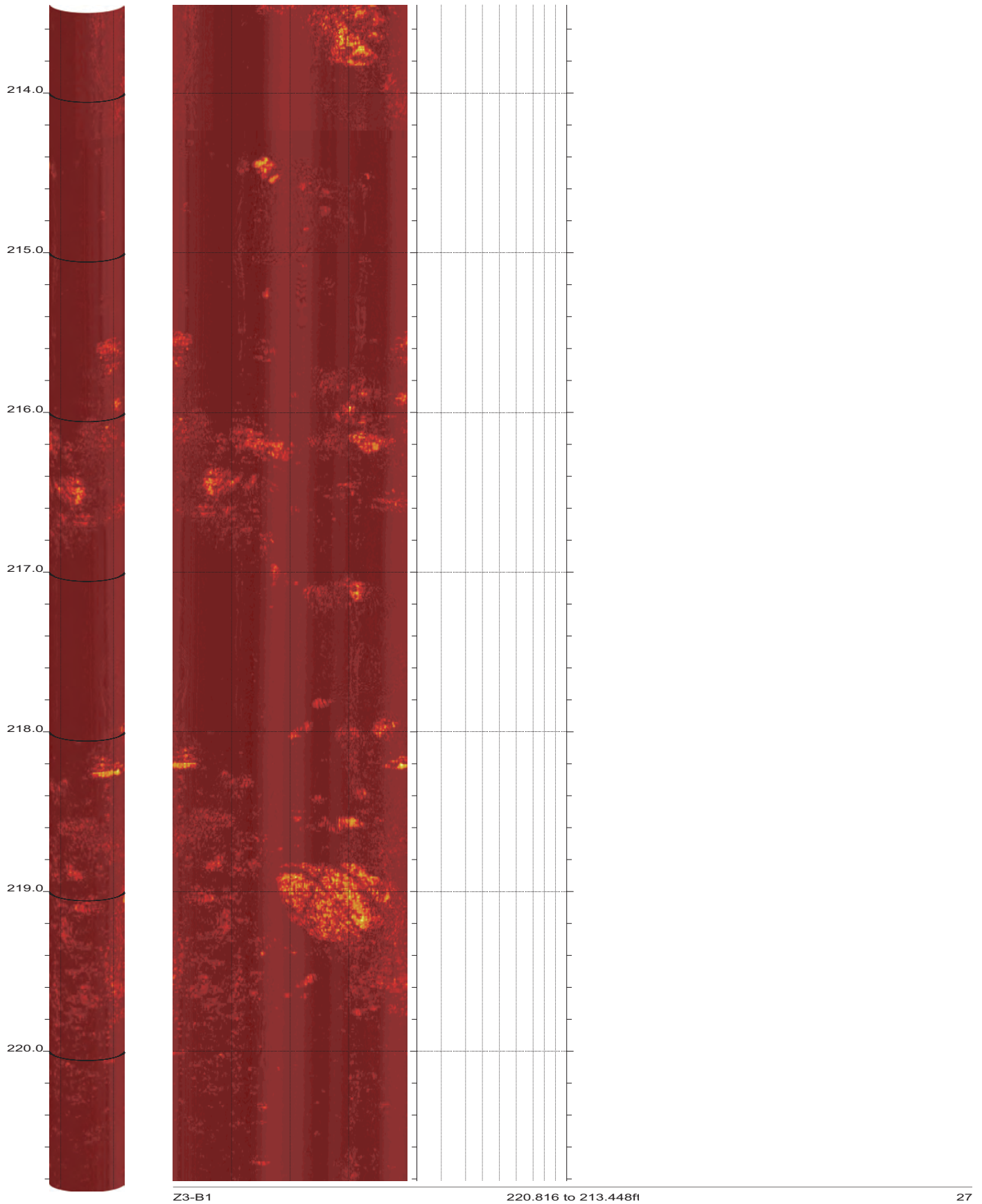
206.080 to 198.712ft

25

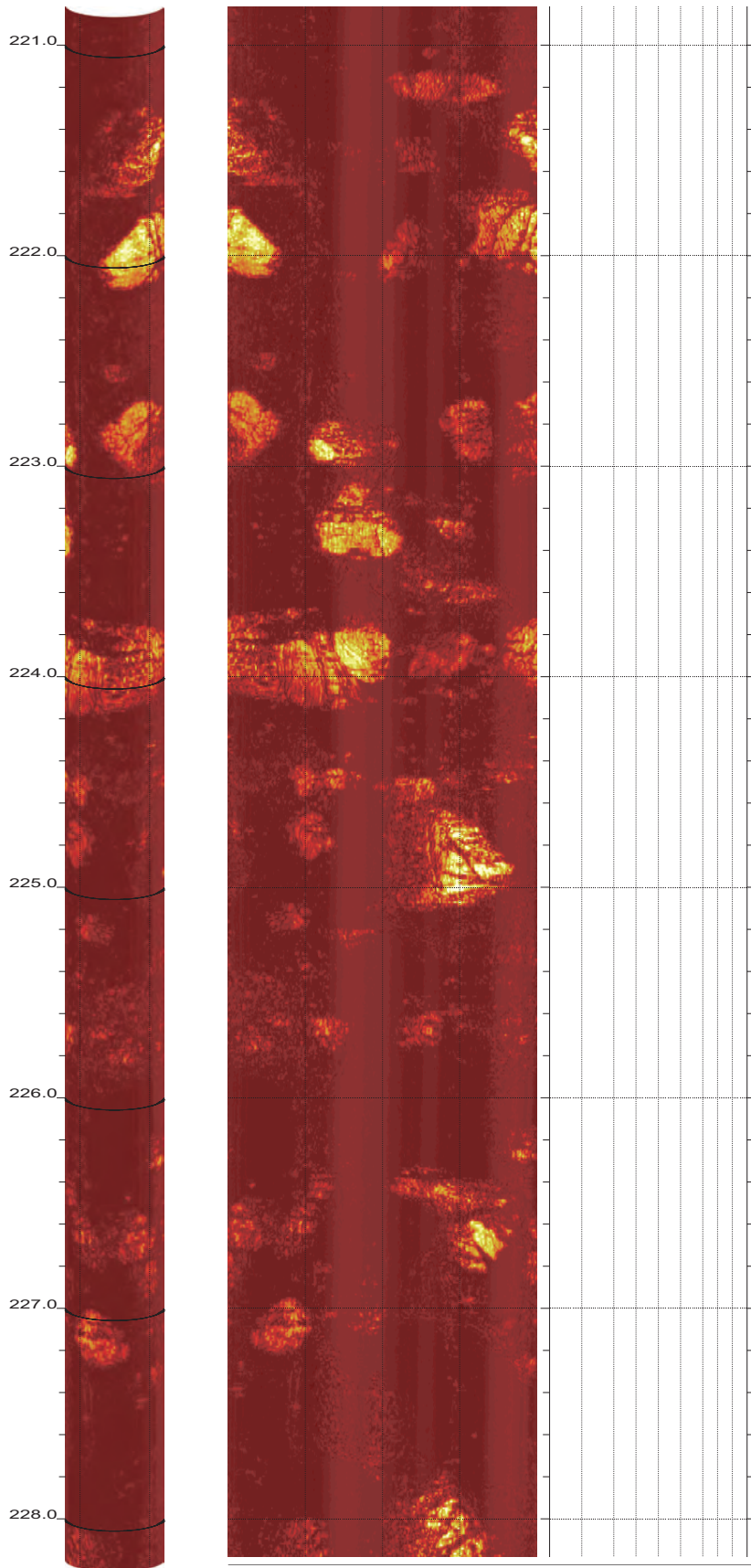
SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 25 of 38



SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 26 of 38



SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 27 of 38

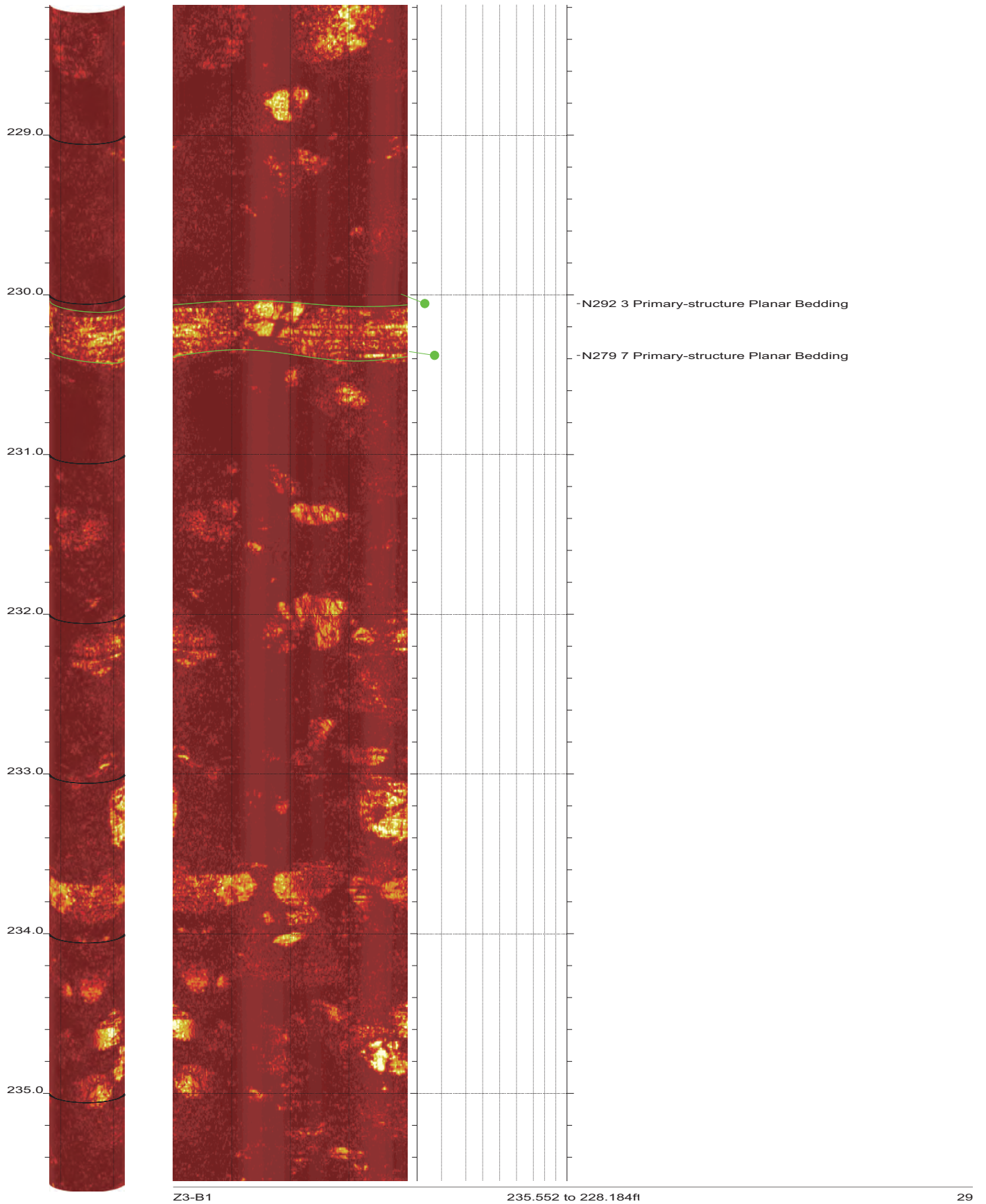


Z3-B1

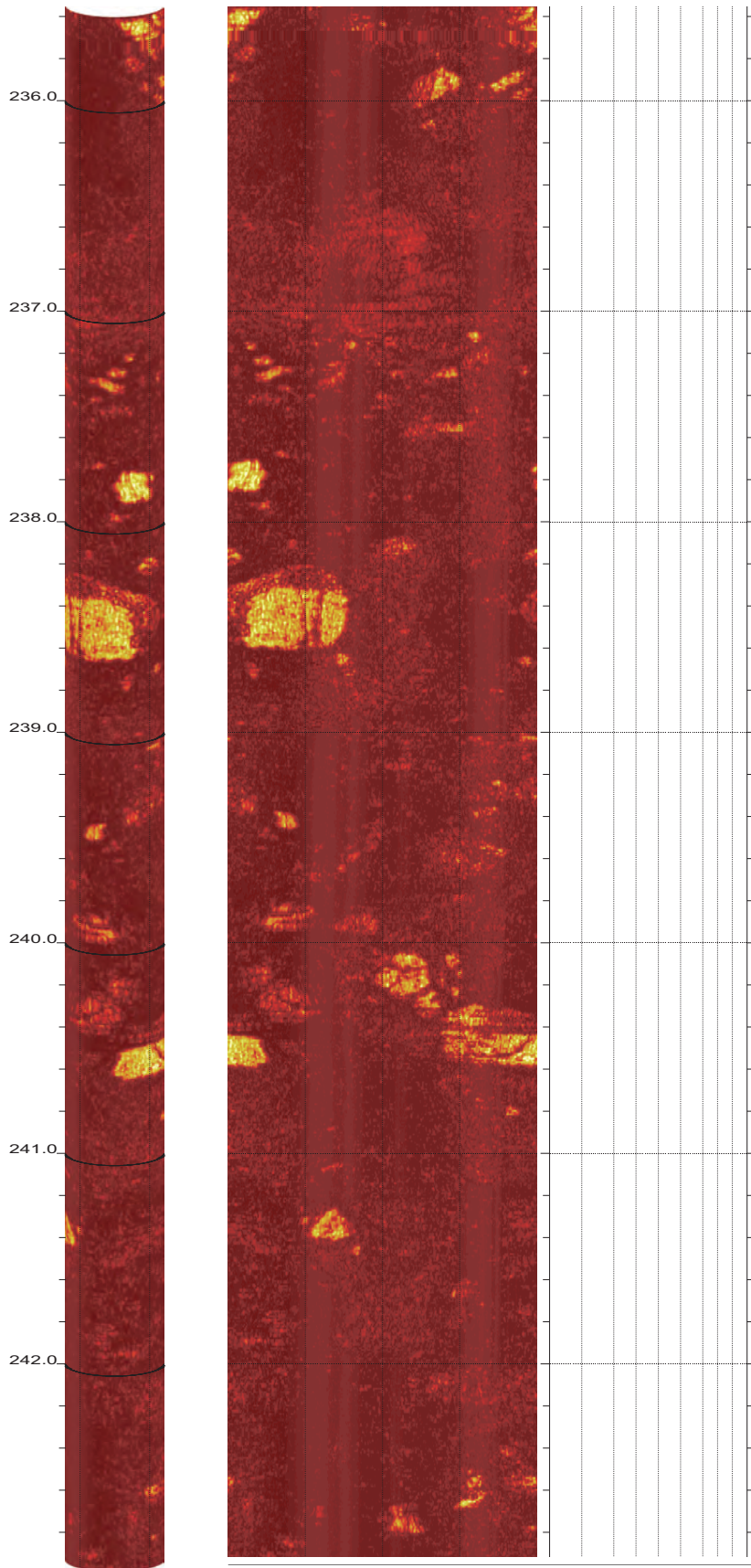
228.184 to 220.816ft

28

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 28 of 38



SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 29 of 38

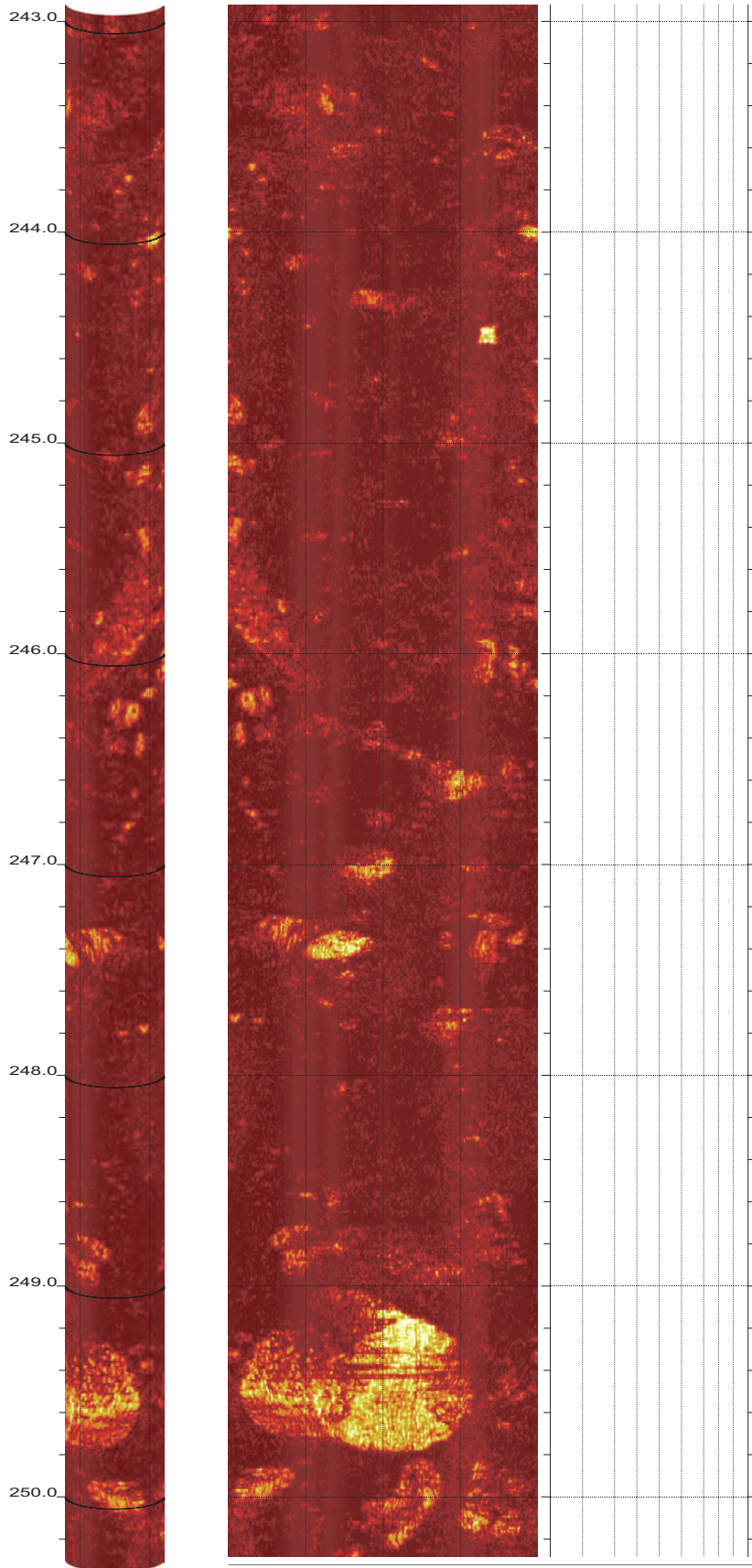


Z3-B1

242.920 to 235.552ft

30

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 30 of 38

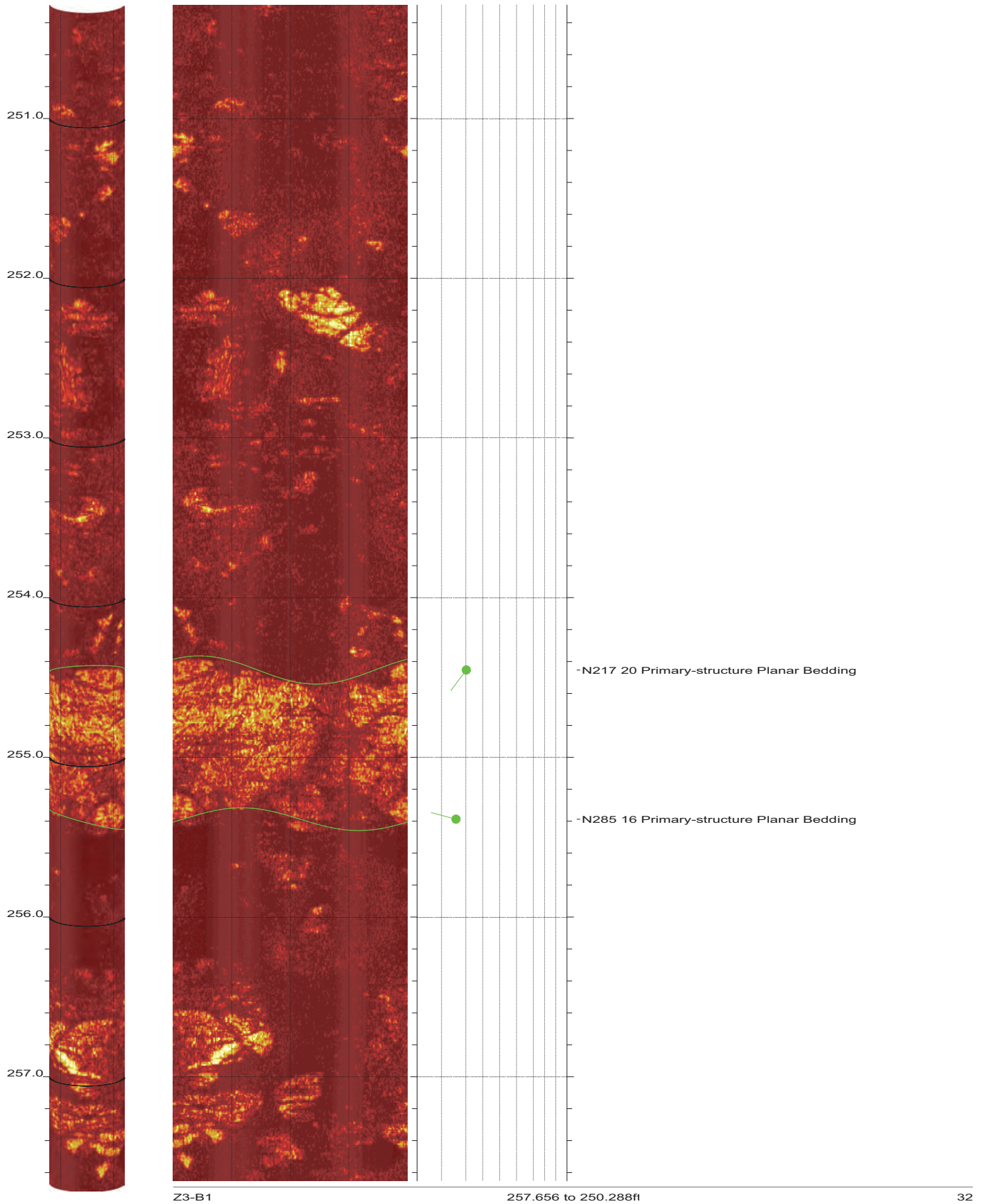


Z3-B1

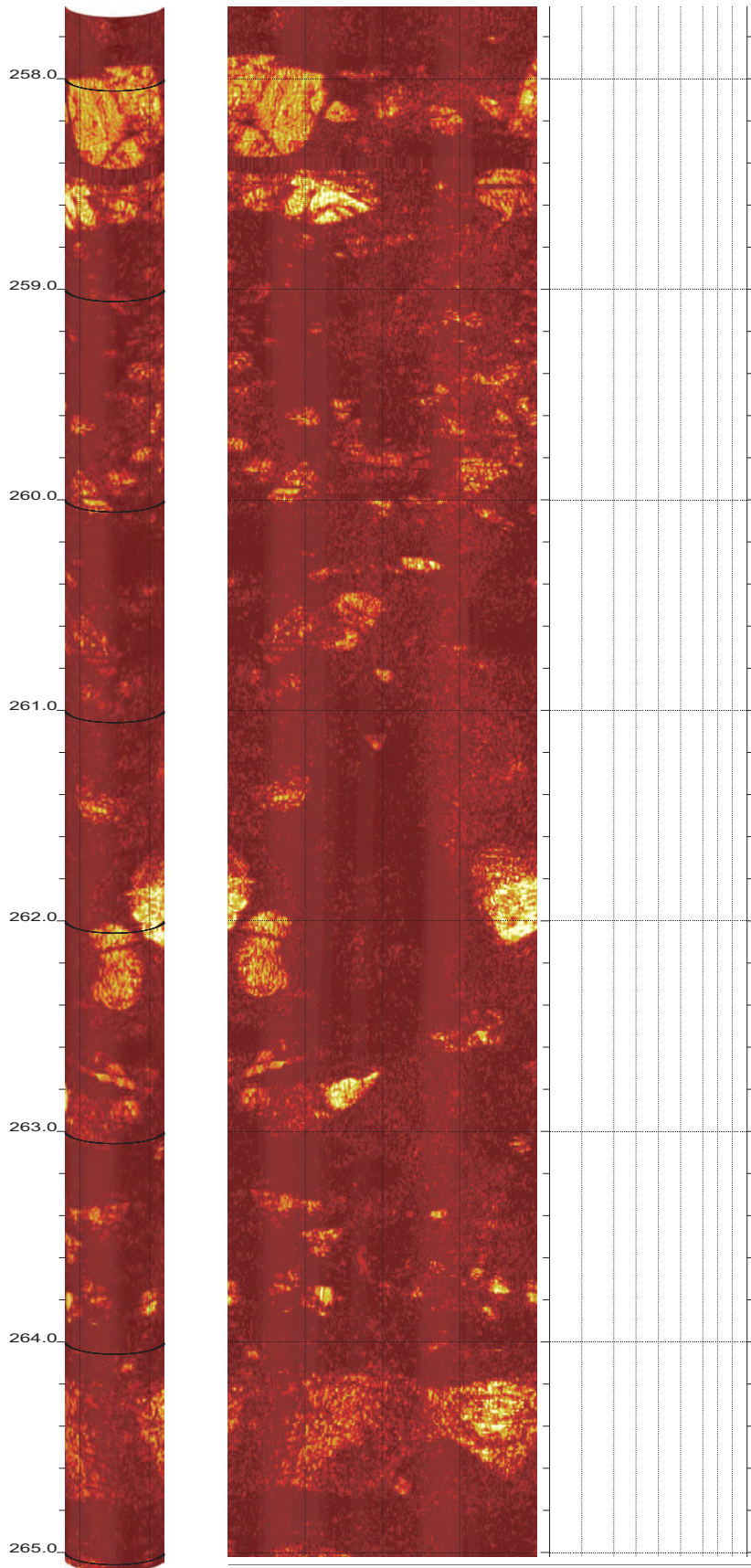
250.288 to 242.920ft

31





SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 32 of 38

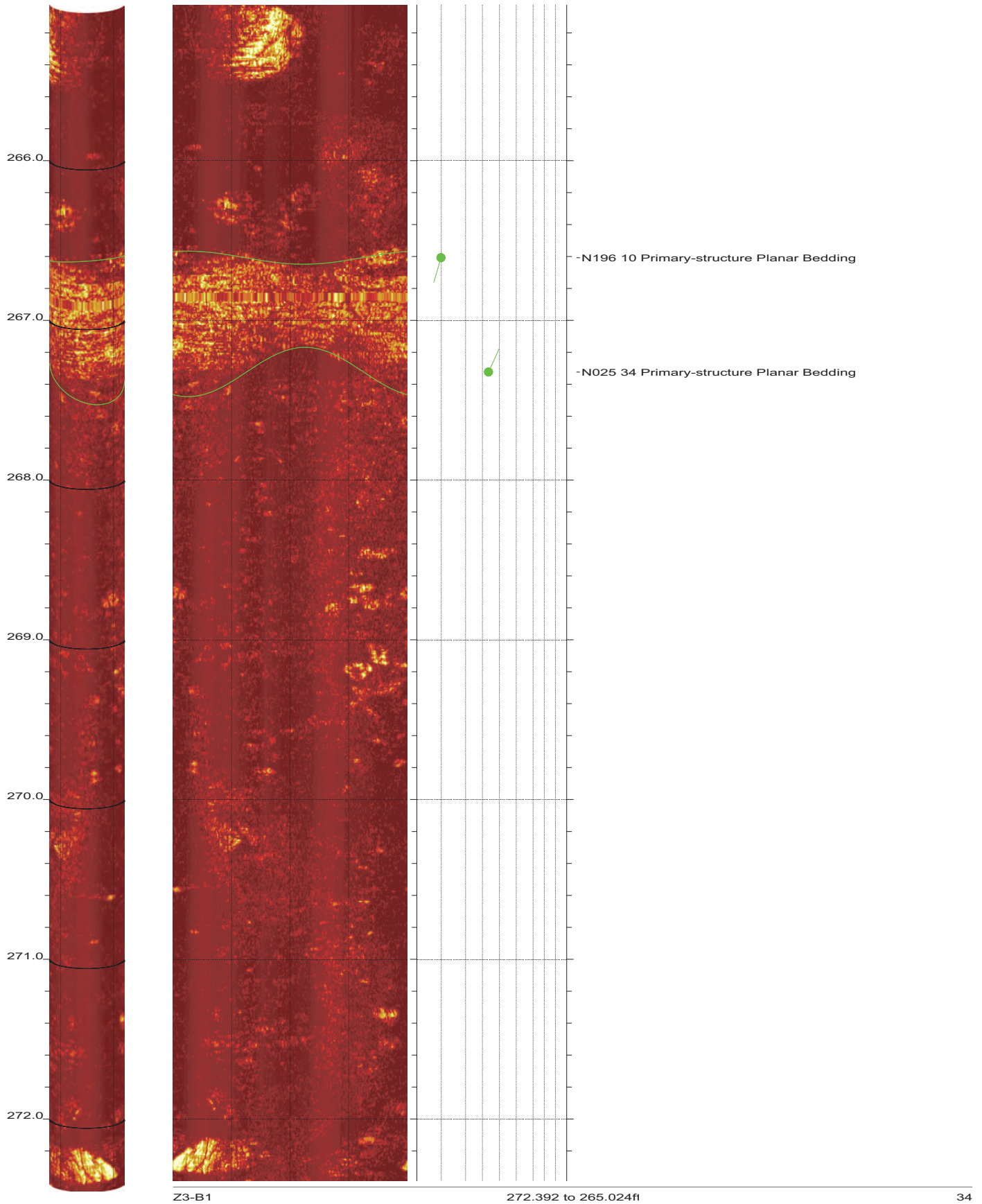


Z3-B1

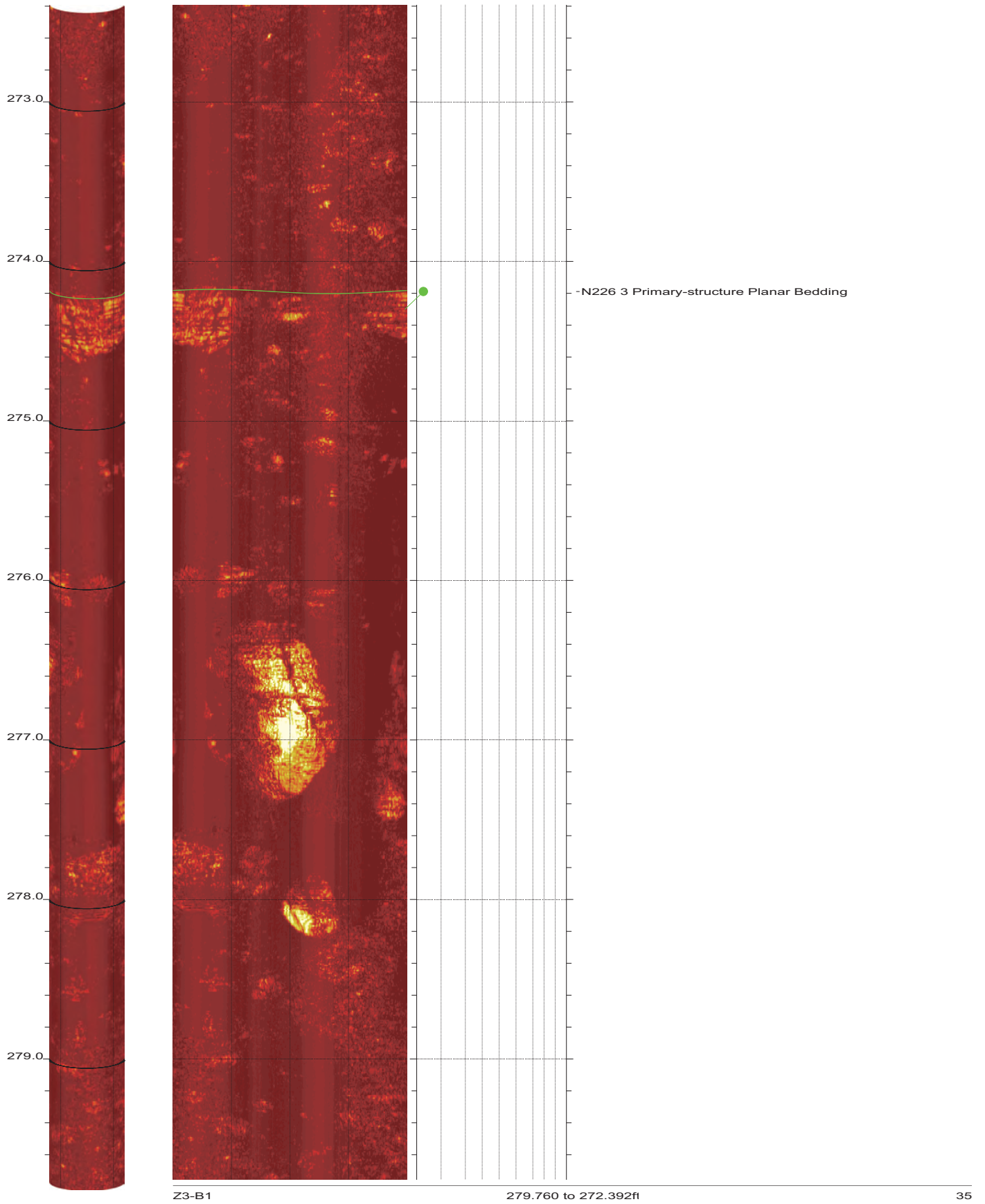
265.024 to 257.656ft

33

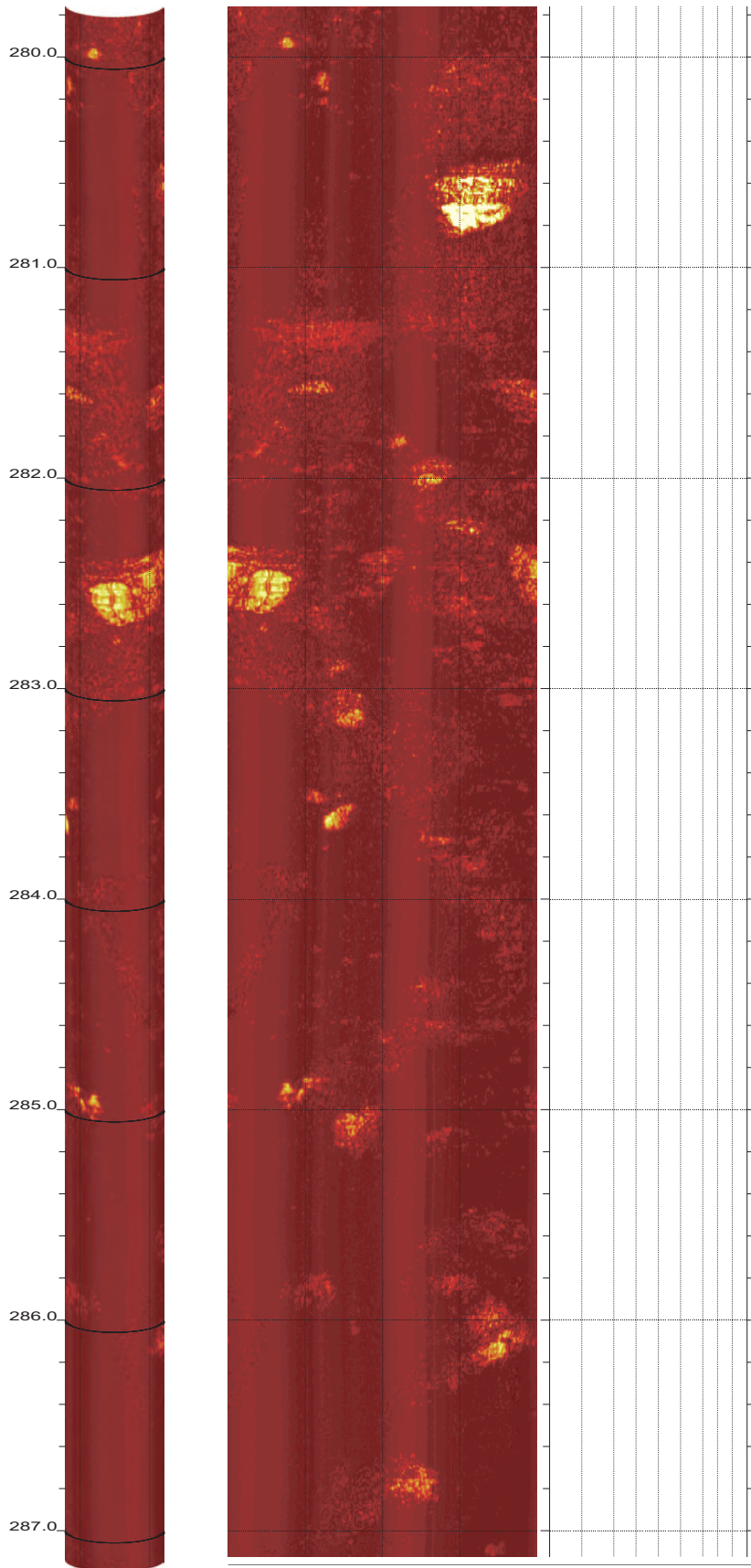
SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 33 of 38



SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 34 of 38



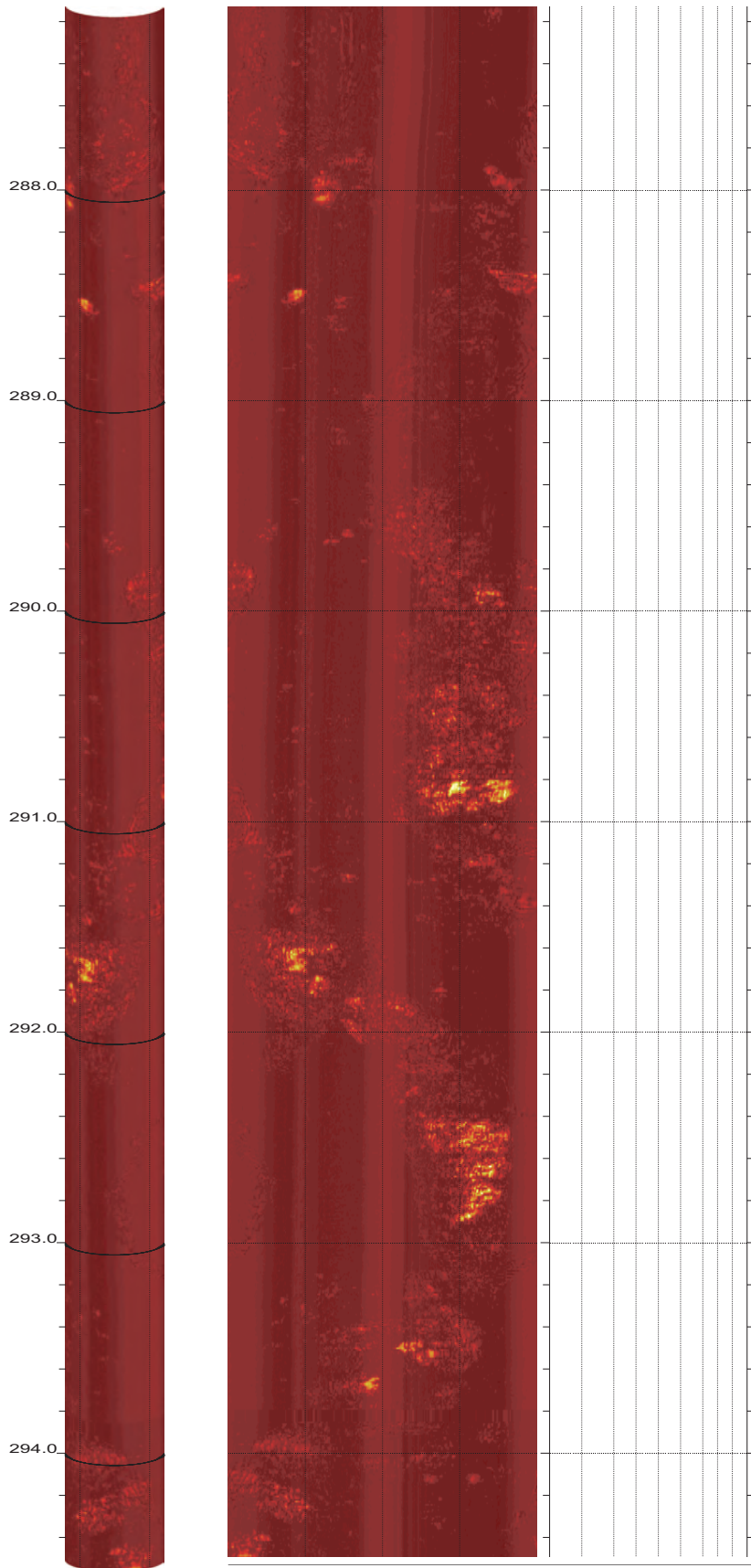
SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 35 of 38



Z3-B1

287.128 to 279.760ft

36

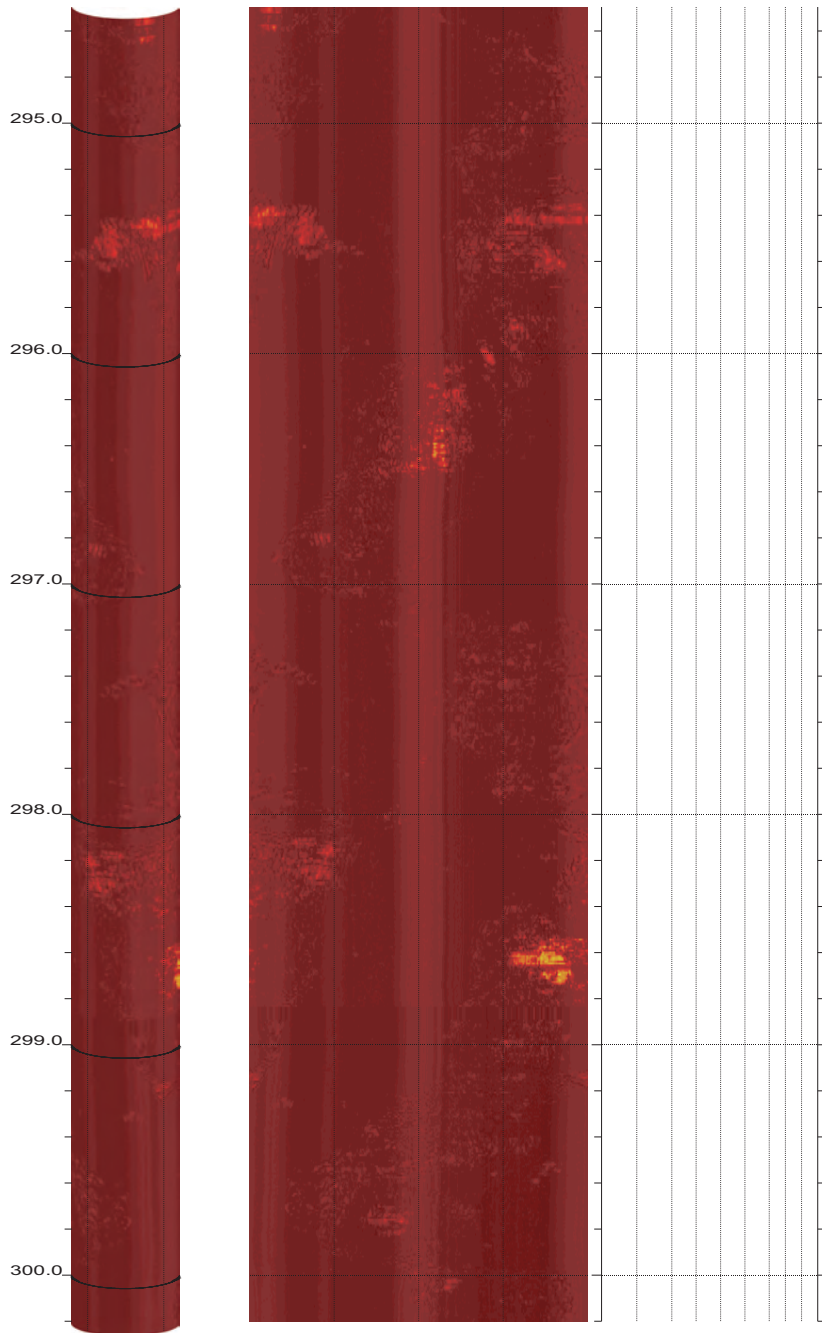


Z3-B1

294.496 to 287.128ft

37

SR-710 Boring Z3-B1 Acoustic Televiewer Dips rev 1 Sheet 37 of 38





BHTV DATA PROCESSING  
 RGLDIP vsn 6.2  
 INTERPRETED BHTV DIPS LOG

CASCADE DRILLING

Borehole: Z3-B3

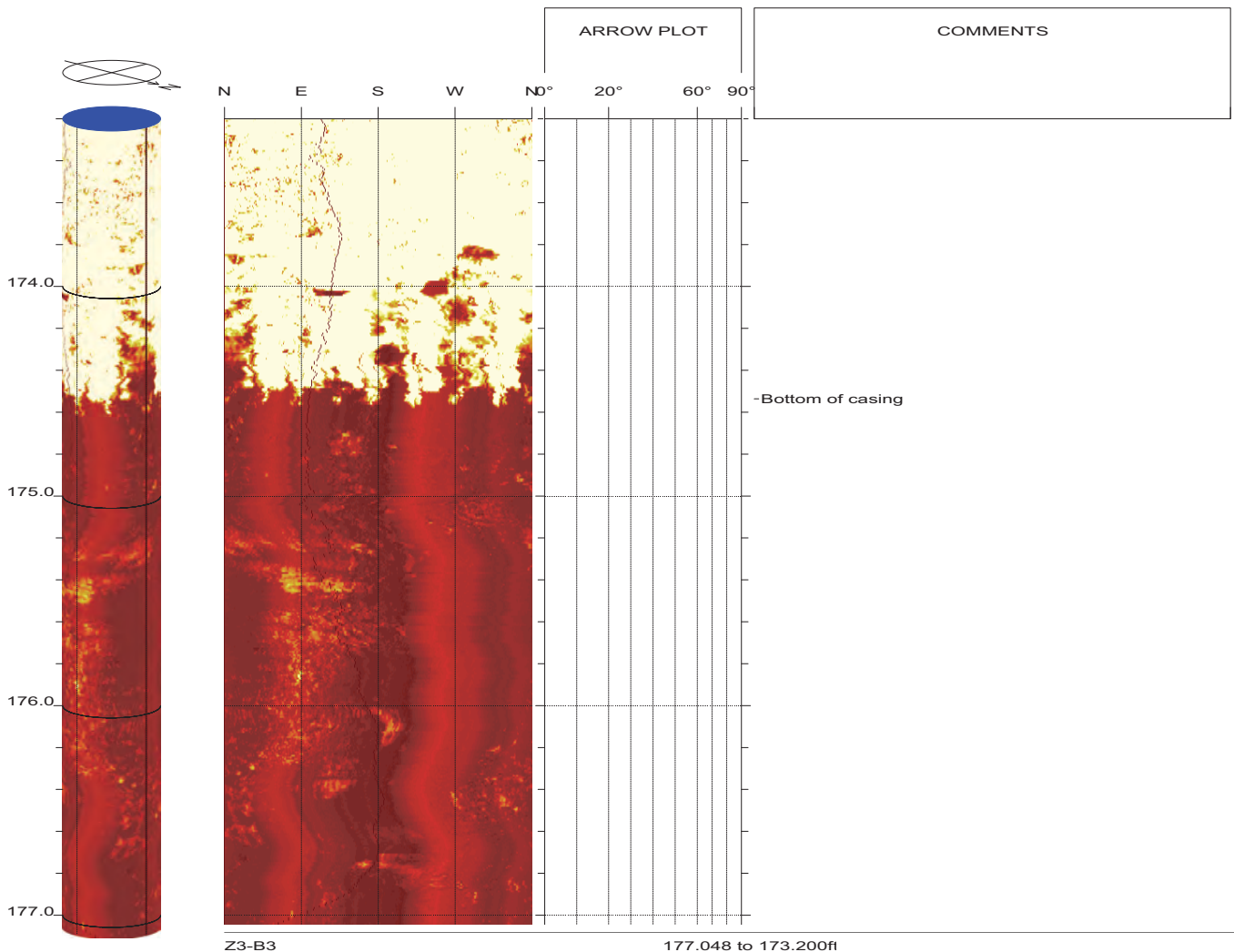
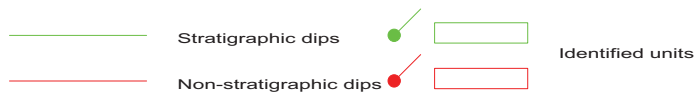
SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

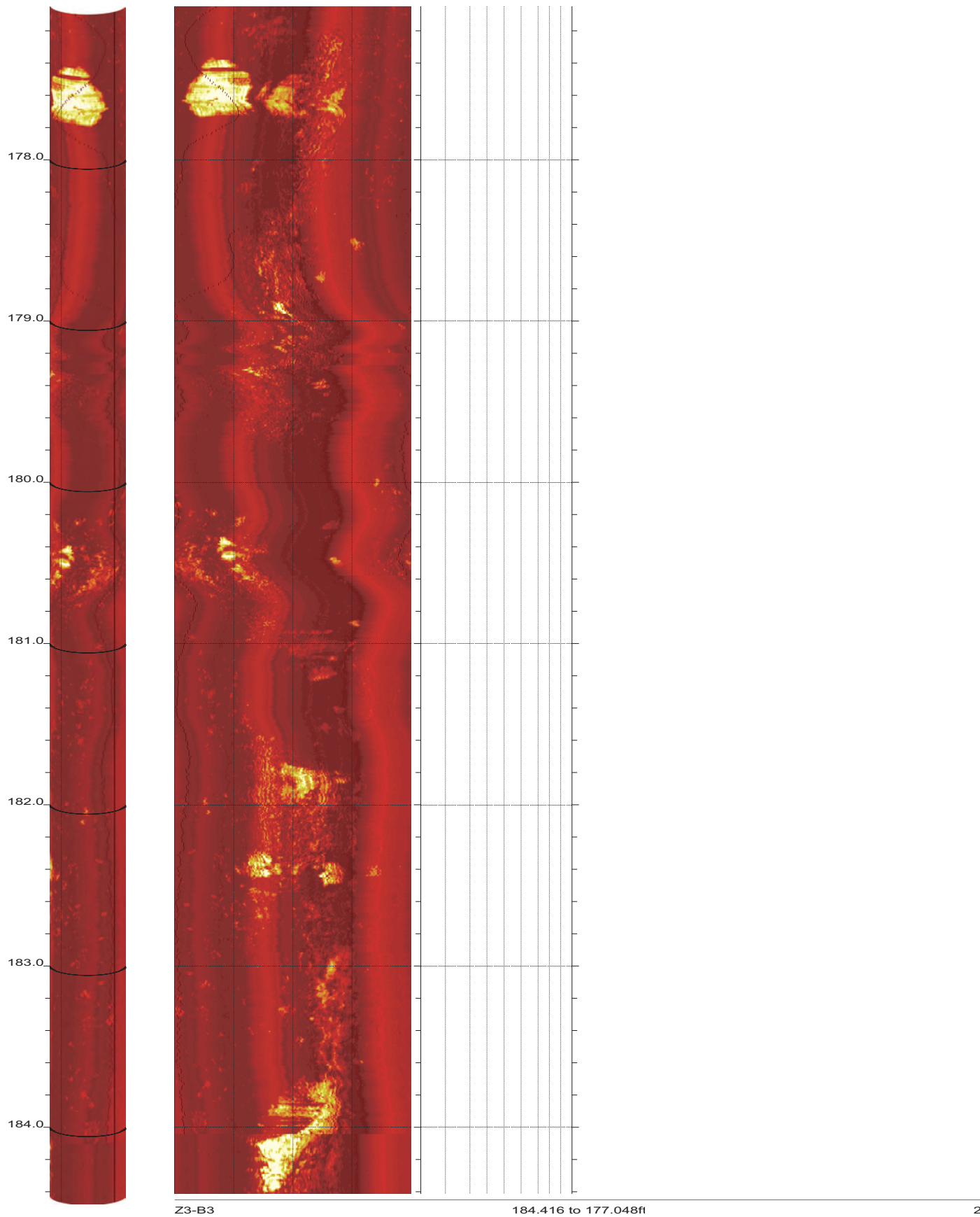
North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

Zone from 273.984 to 173.200ft  
 Format: BHTV-NESWN

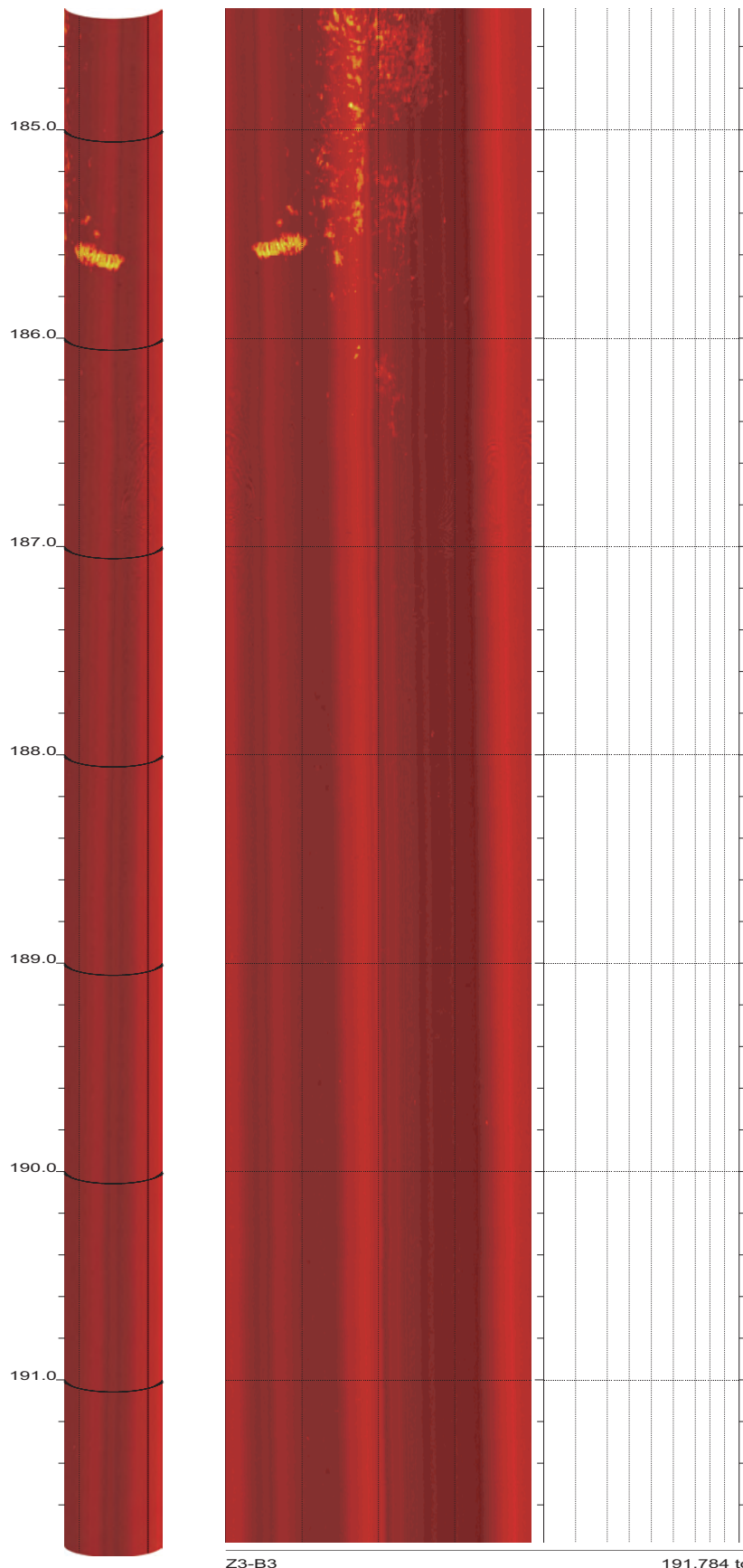
Borehole diam: 5.600inch  
 Vertical = borehole-axis  
 Image: Amplitude







SR-710 Boring Z3-B3 Acoustic Televiewer Dips rev 1 Sheet 2 of 15

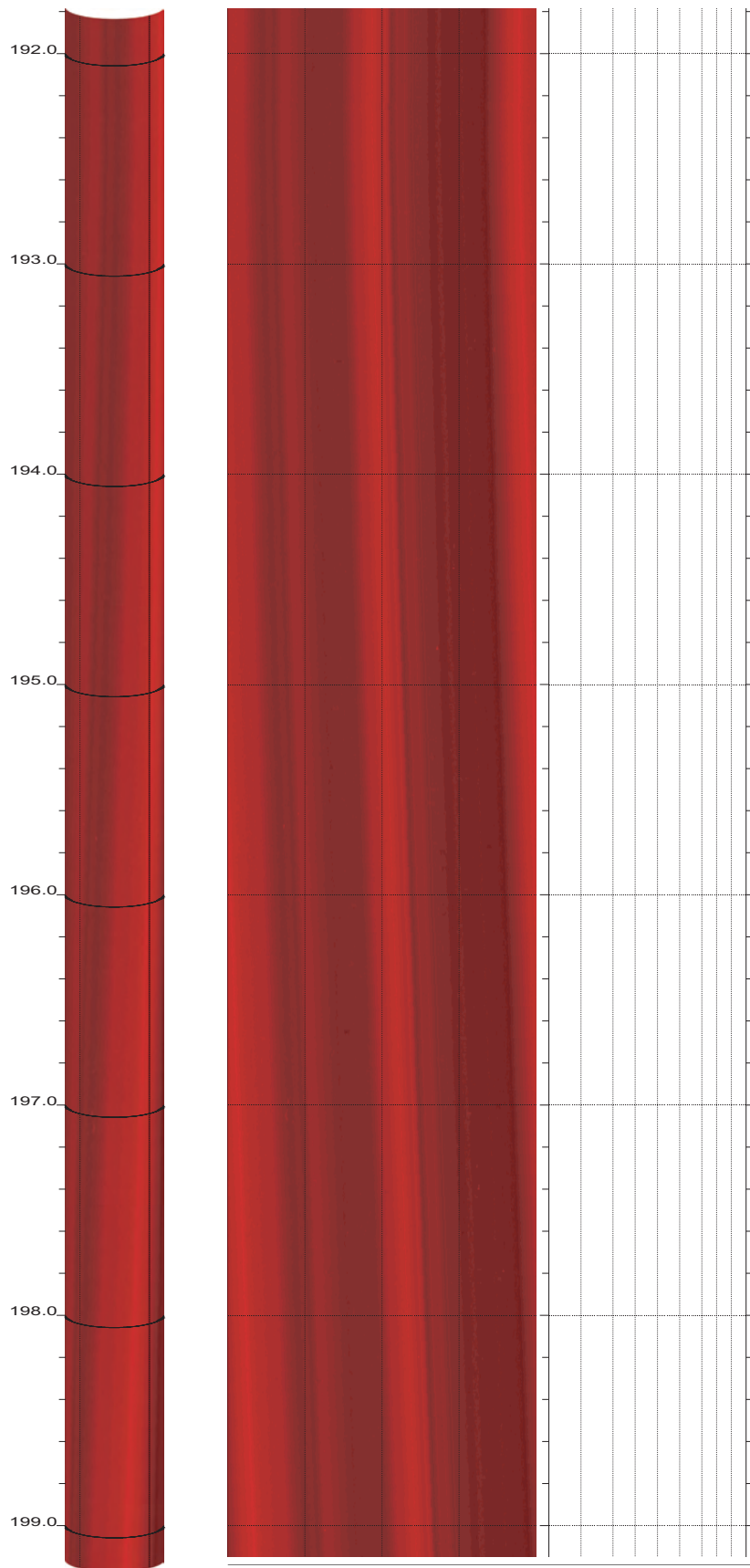


Z3-B3

191.784 to 184.416ft

3

SR-710 Boring Z3-B3 Acoustic Televiewer Dips rev 1 Sheet 3 of 15

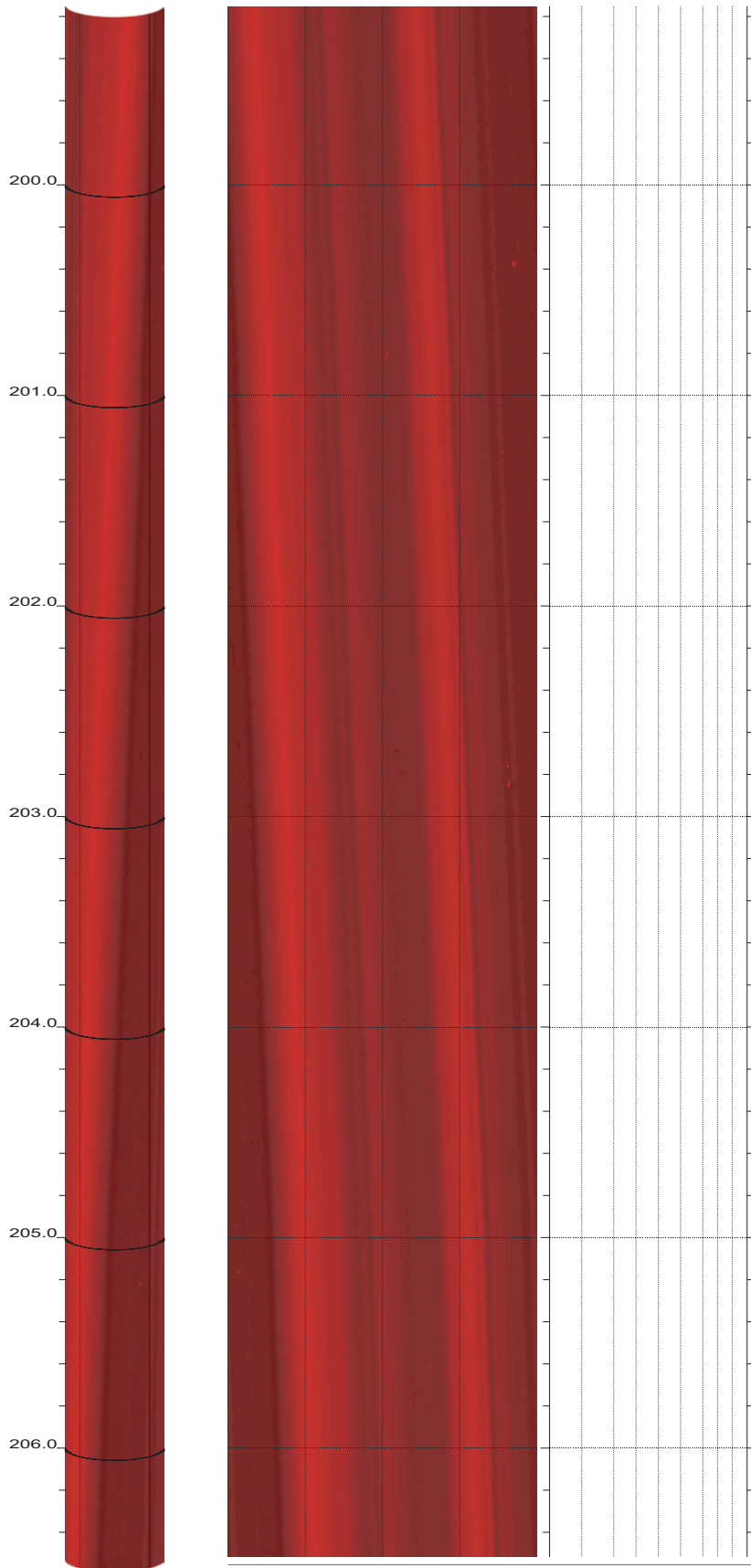


Z3-B3

199.152 to 191.784ft

4

SR-710 Boring Z3-B3 Acoustic Televiewer Dips rev 1 Sheet 4 of 15

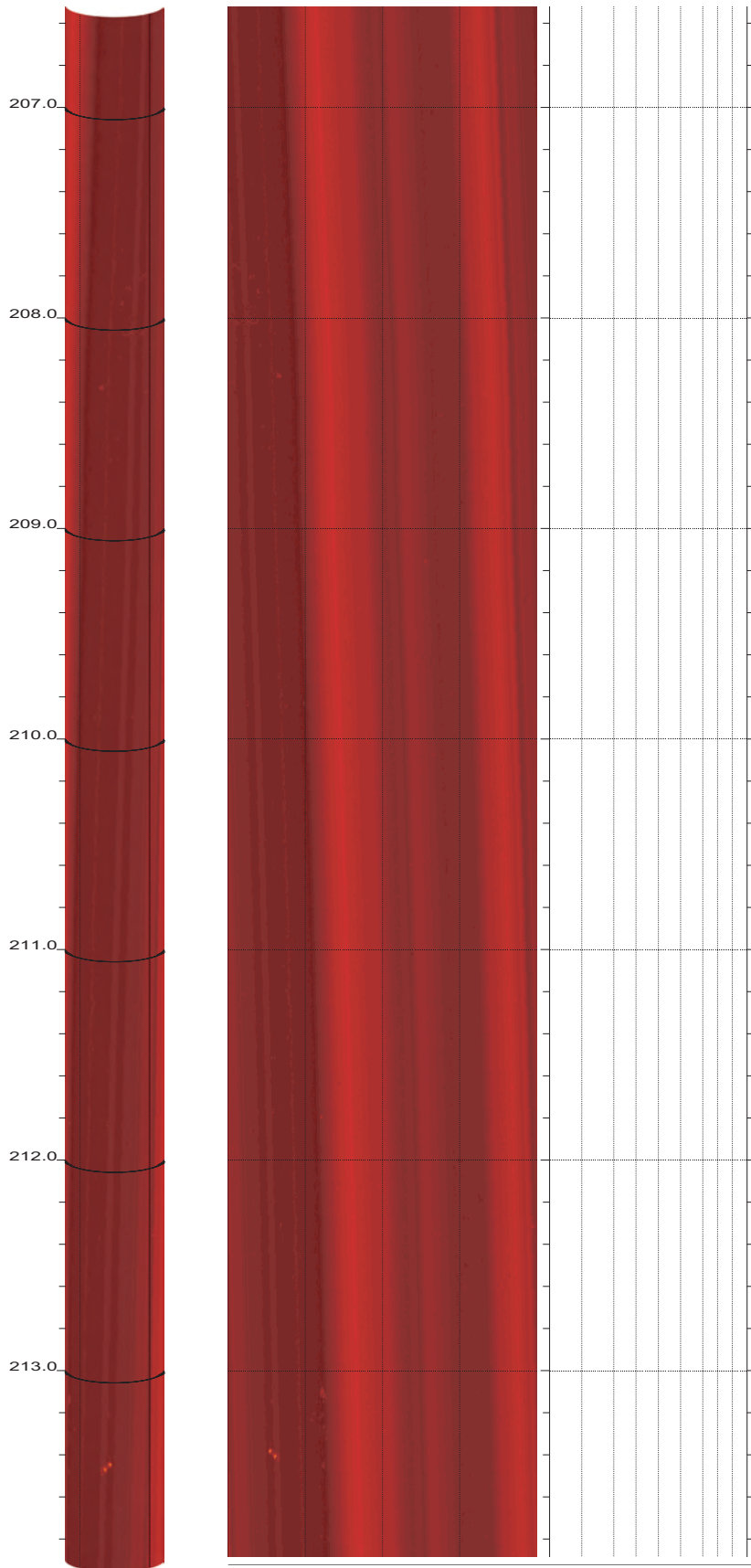


Z3-B3

206.520 to 199.152ft

5

SR-710 Boring Z3-B3 Acoustic Televiewer Dips rev 1 Sheet 5 of 15

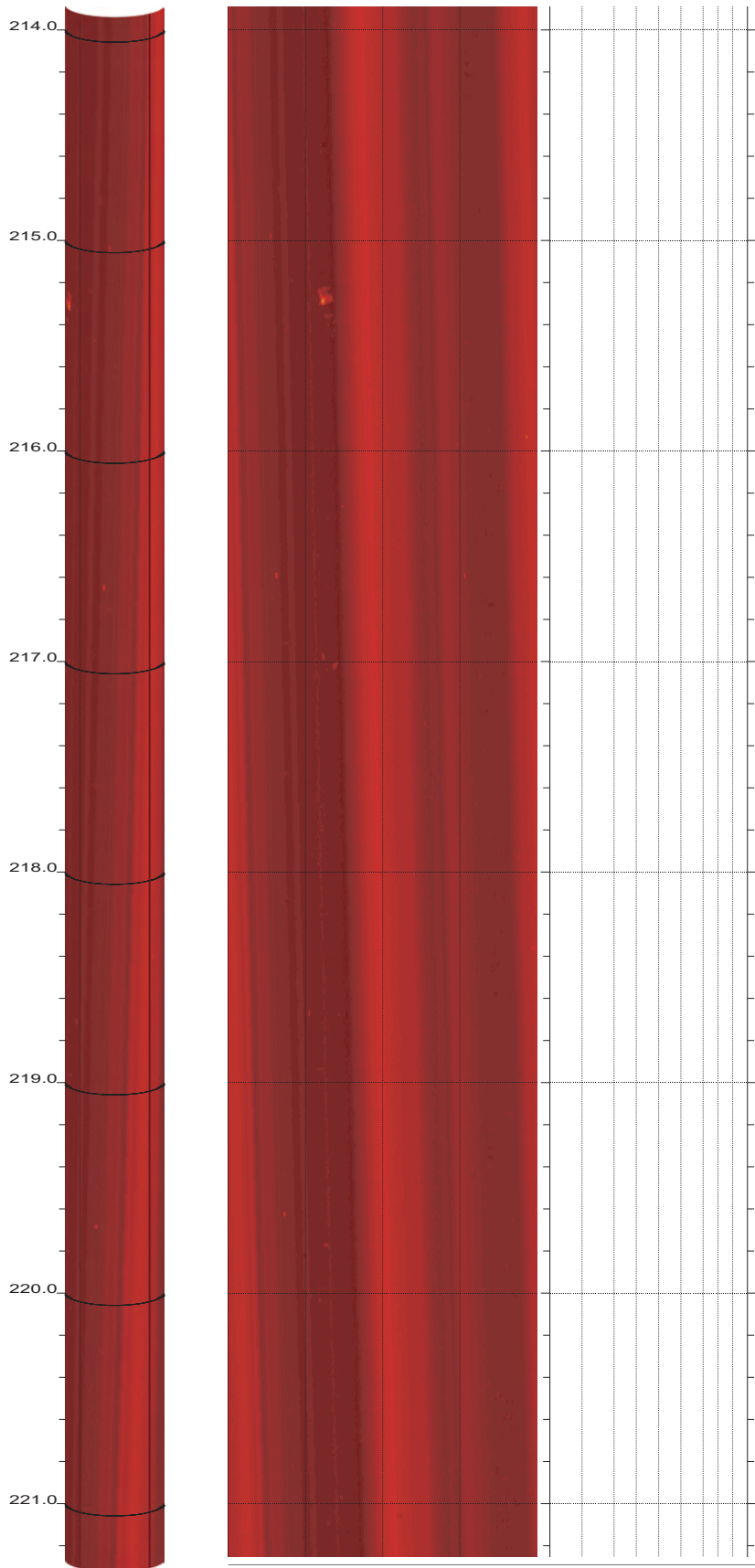


Z3-B3

213.888 to 206.520ft

6

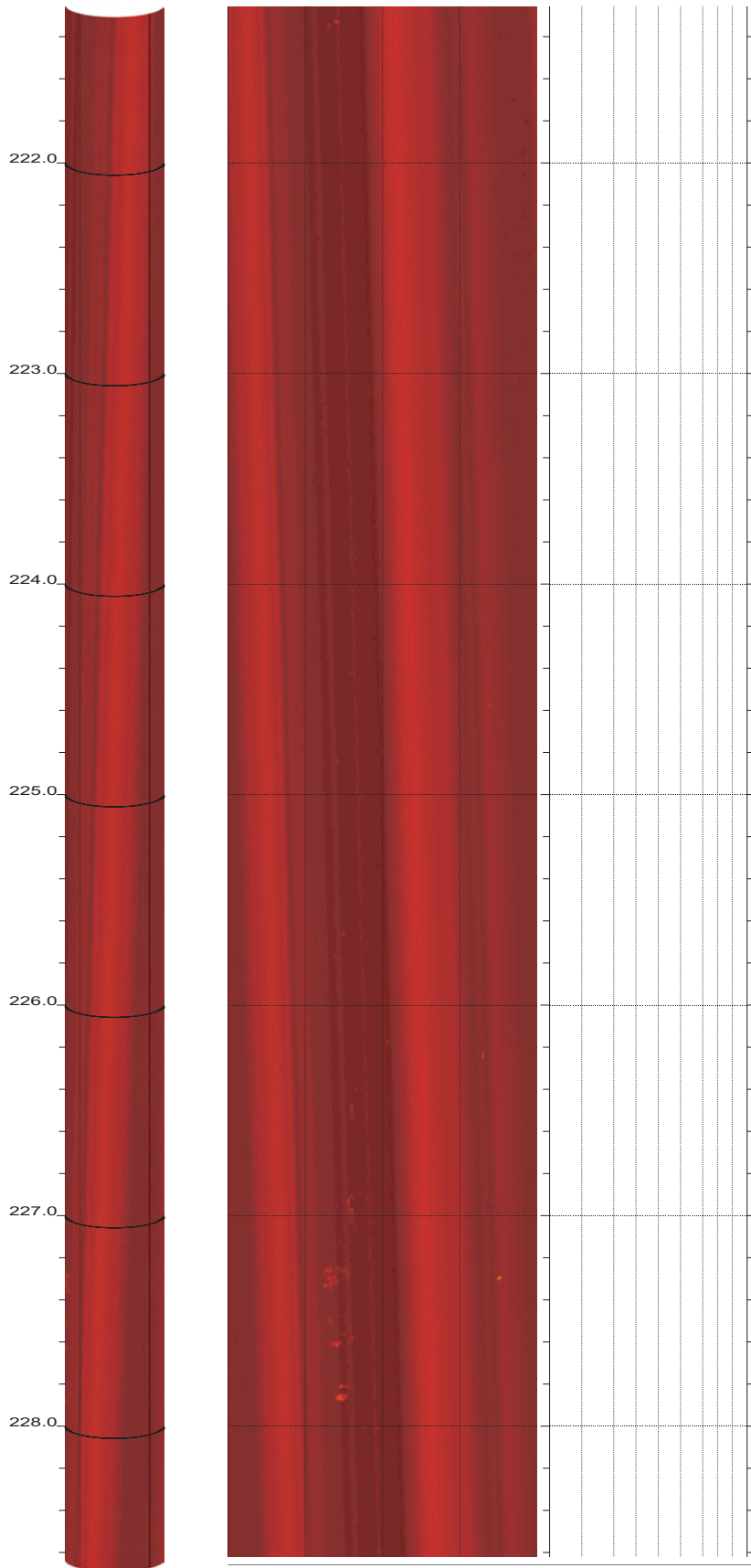
SR-710 Boring Z3-B3 Acoustic Televiewer Dips rev 1 Sheet 6 of 15



Z3-B3

221.256 to 213.888ft

7

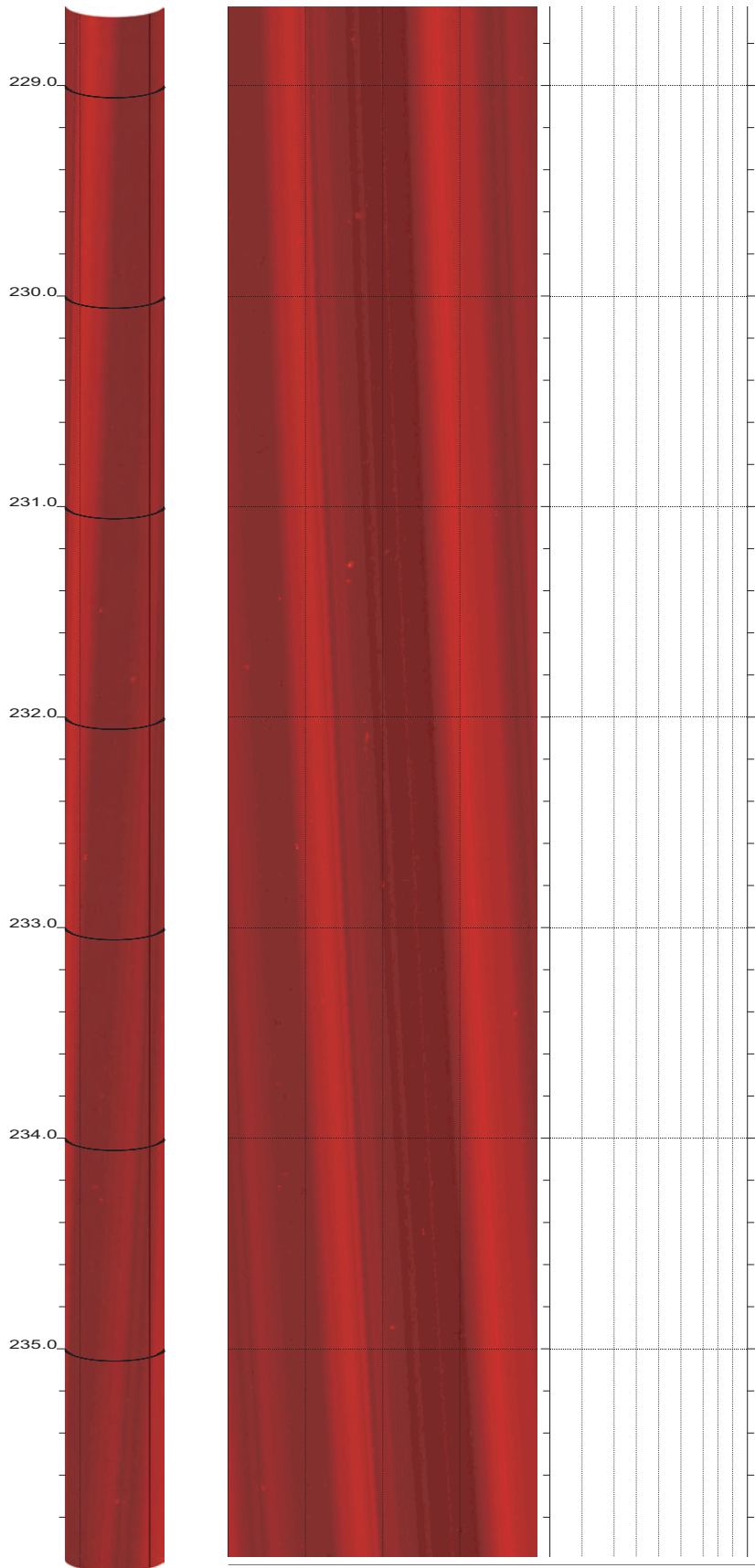


Z3-B3

228.624 to 221.256ft

8

SR-710 Boring Z3-B3 Acoustic Televiewer Dips rev 1 Sheet 8 of 15



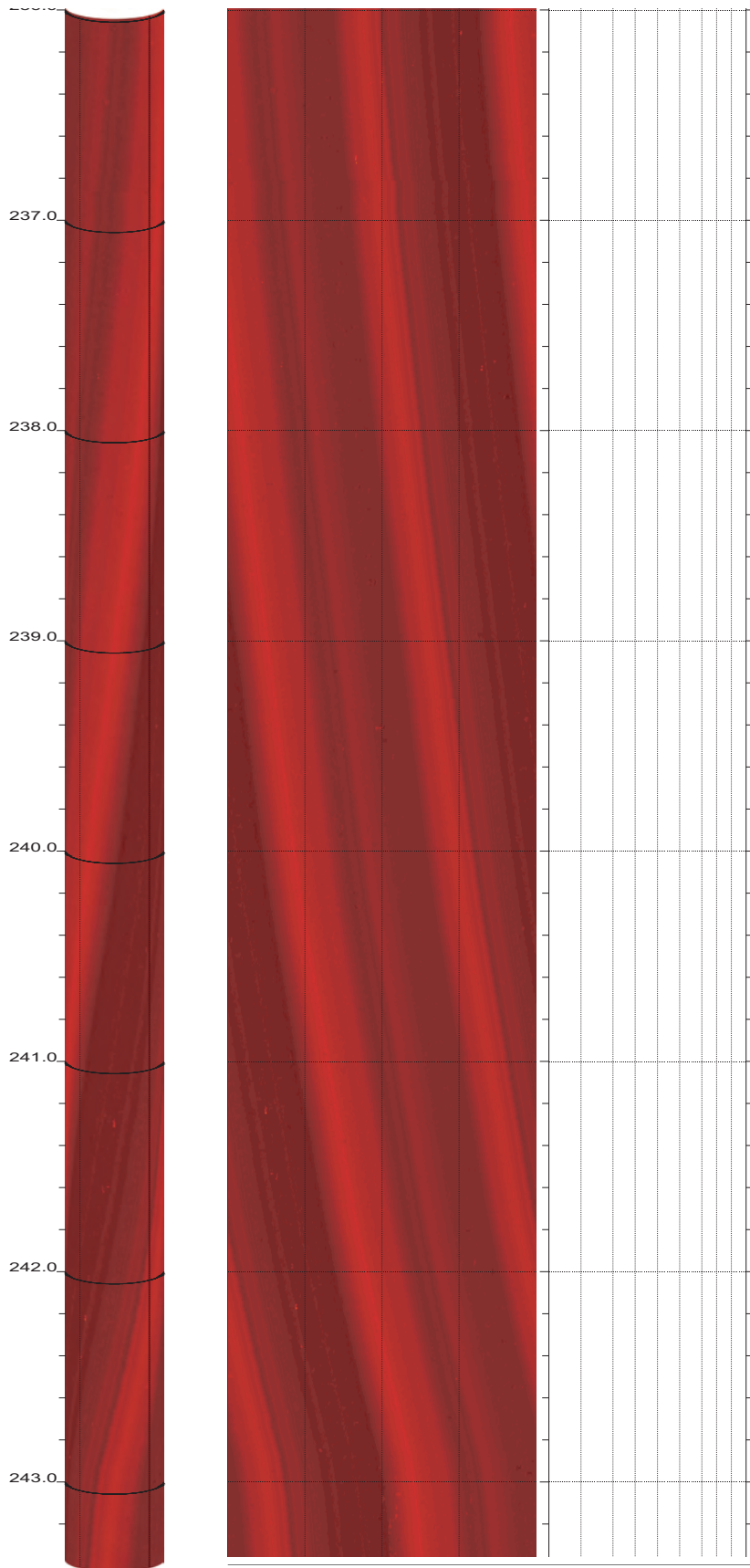
Z3-B3

235.992 to 228.624ft

9

SR-710 Boring Z3-B3 Acoustic Televiewer Dips rev 1 Sheet 9 of 15



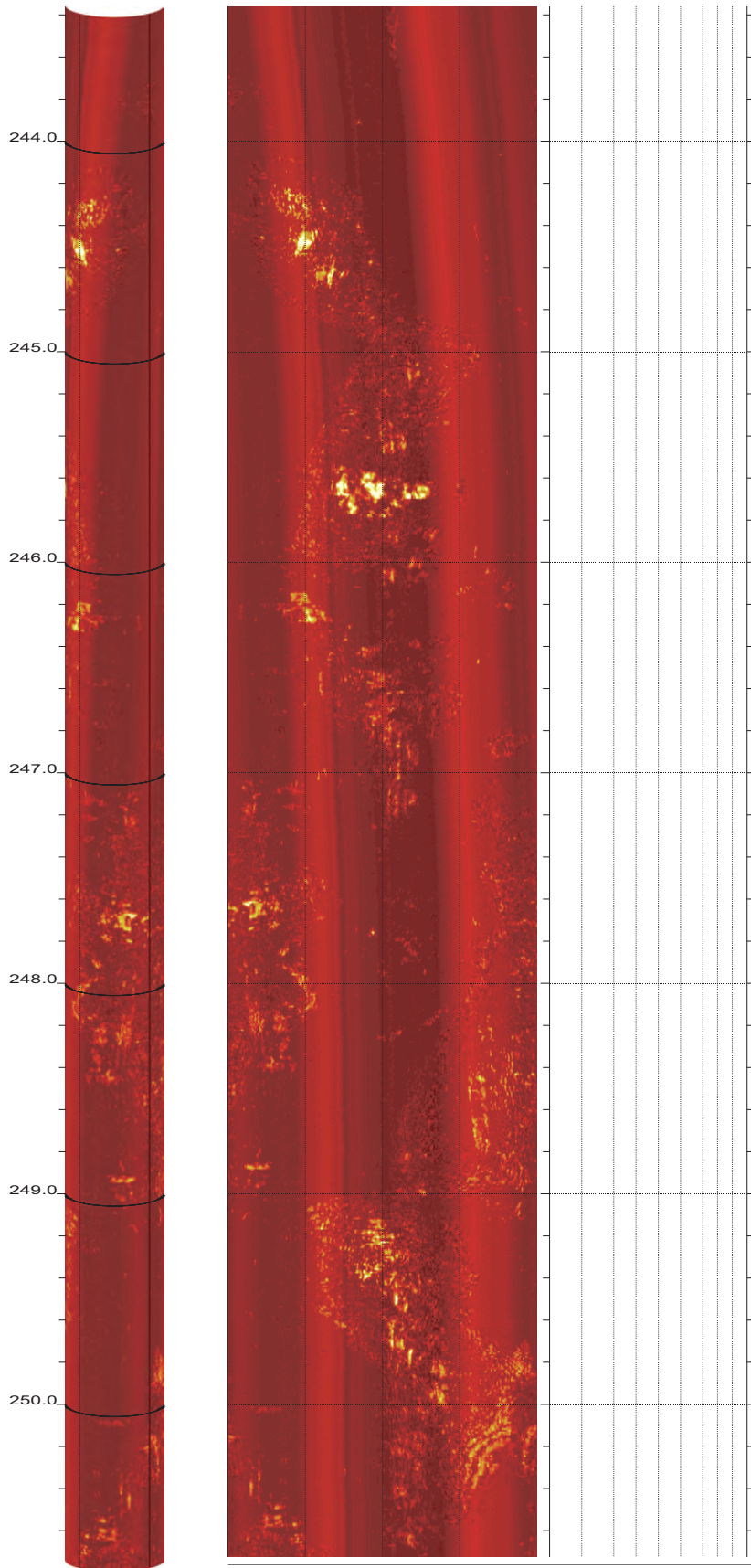


Z3-B3

243.360 to 235.992ft

10

SR-710 Boring Z3-B3 Acoustic Televiewer Dips rev 1 Sheet 10 of 15

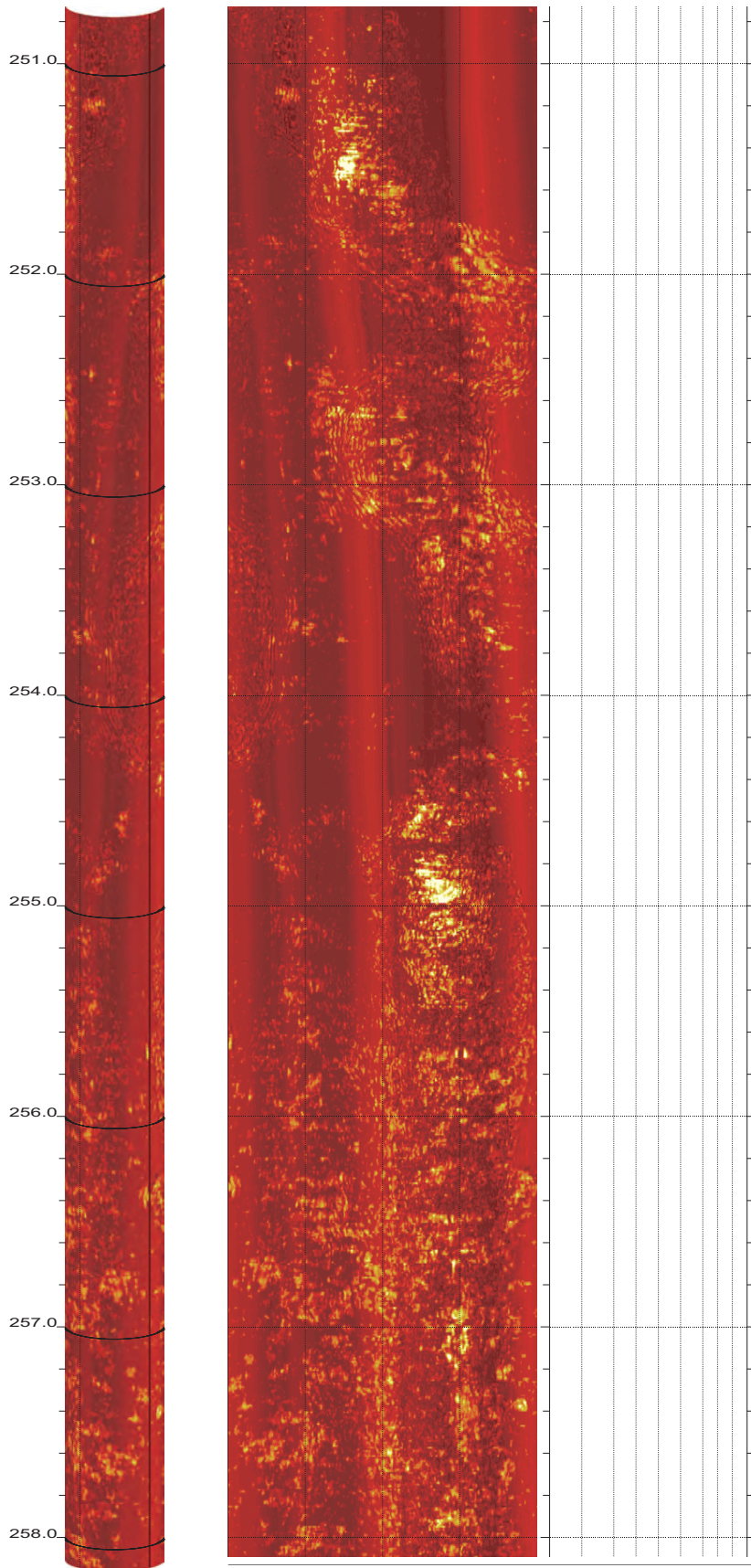


Z3-B3

250.728 to 243.360ft

11

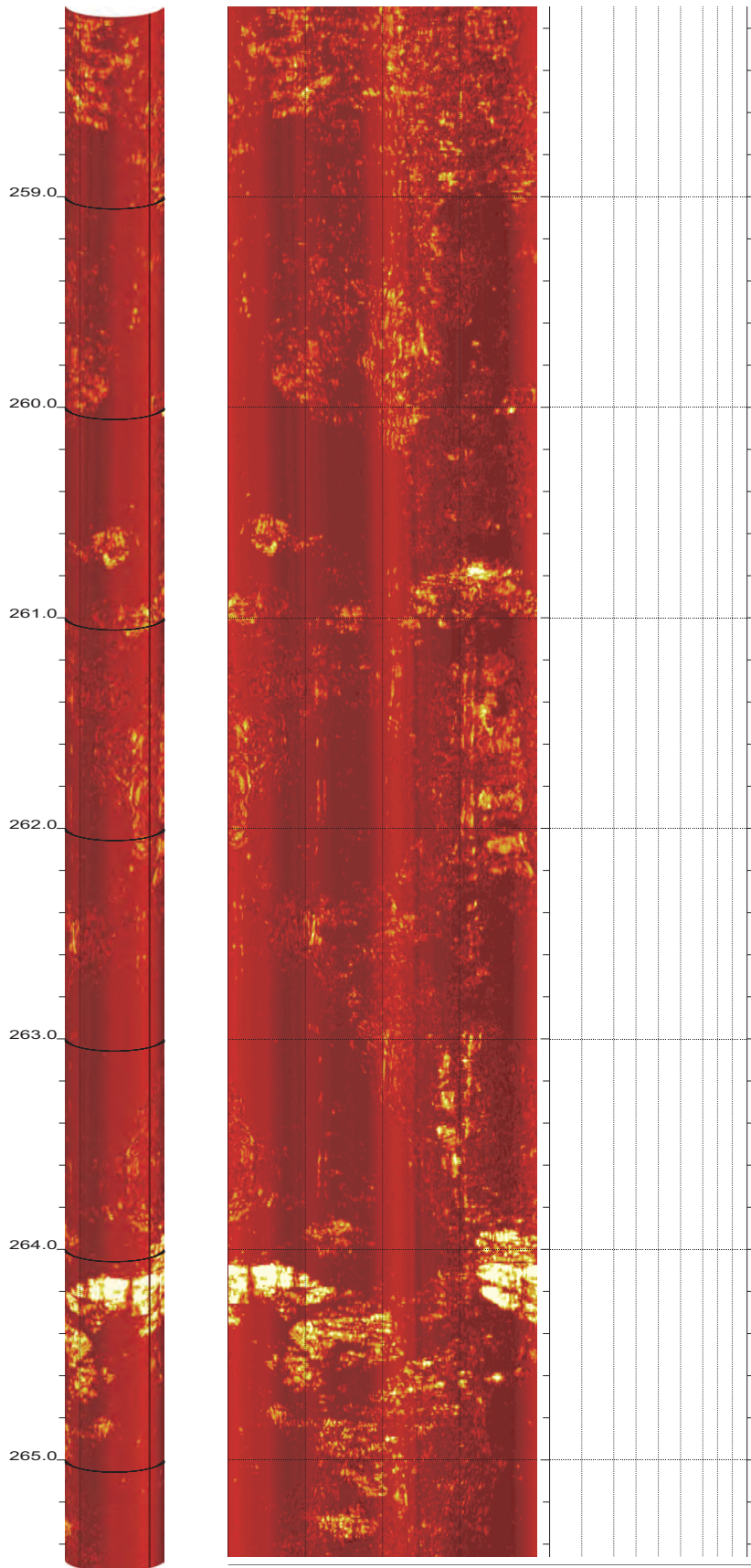
SR-710 Boring Z3-B3 Acoustic Televiewer Dips rev 1 Sheet 11 of 15



Z3-B3

258.096 to 250.728ft

12

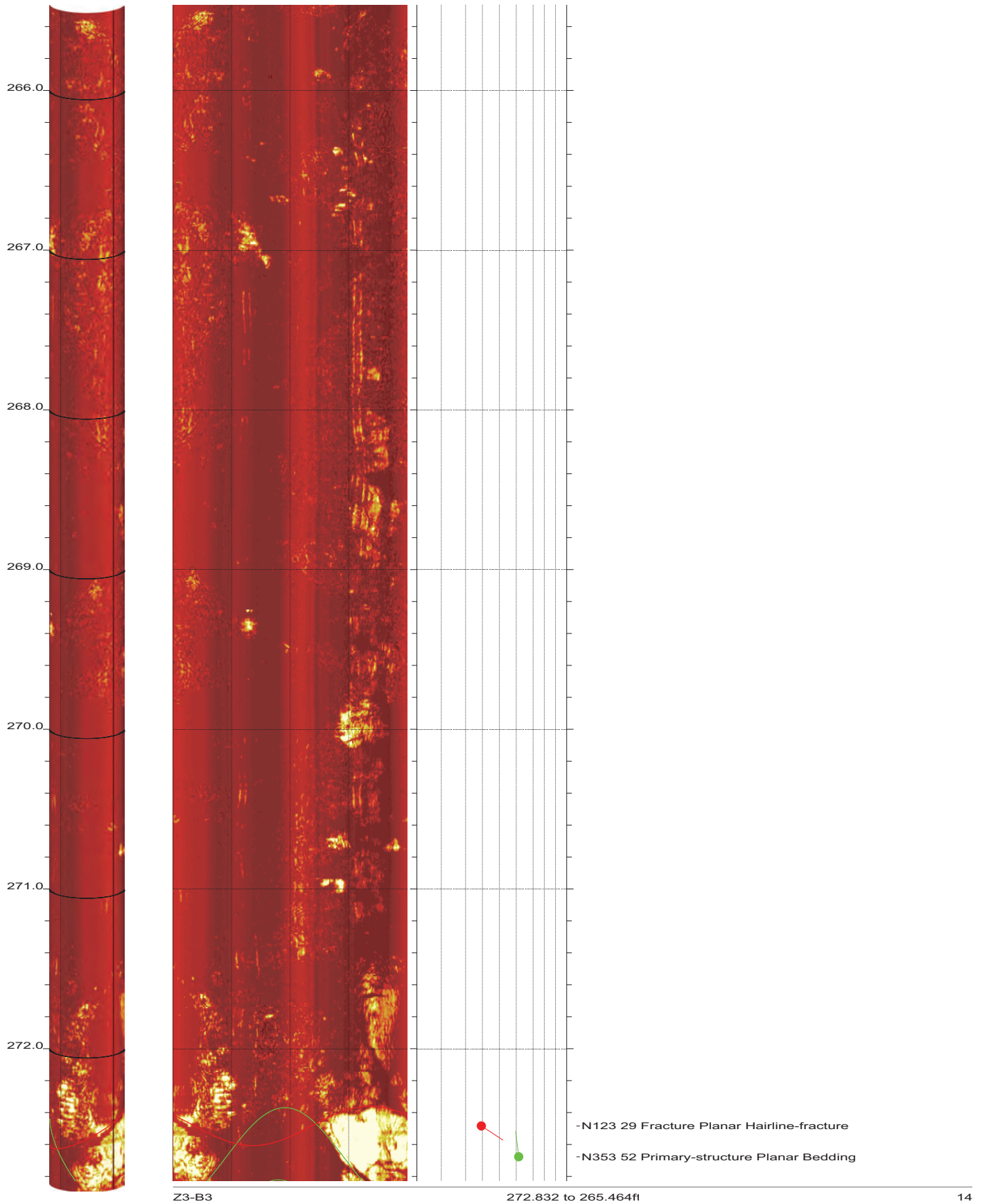


Z3-B3

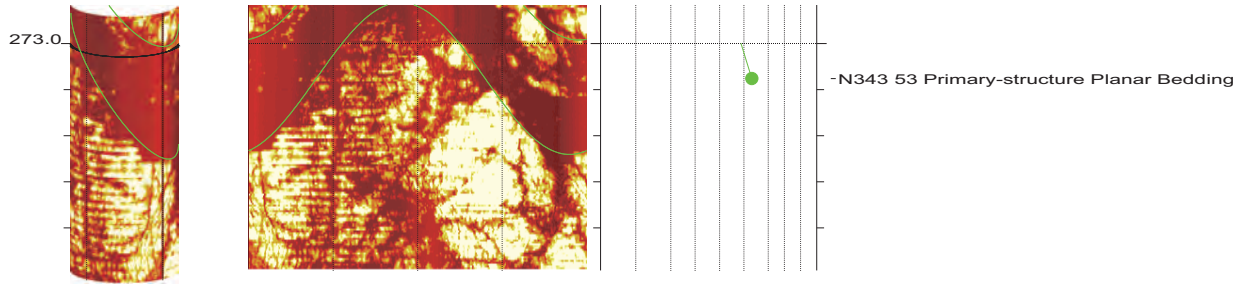
265.464 to 258.096ft

13

SR-710 Boring Z3-B3 Acoustic Televiewer Dips rev 1 Sheet 13 of 15



SR-710 Boring Z3-B3 Acoustic Televiewer Dips rev 1 Sheet 14 of 15





CASCADE DRILLING

Borehole: Z3-B4

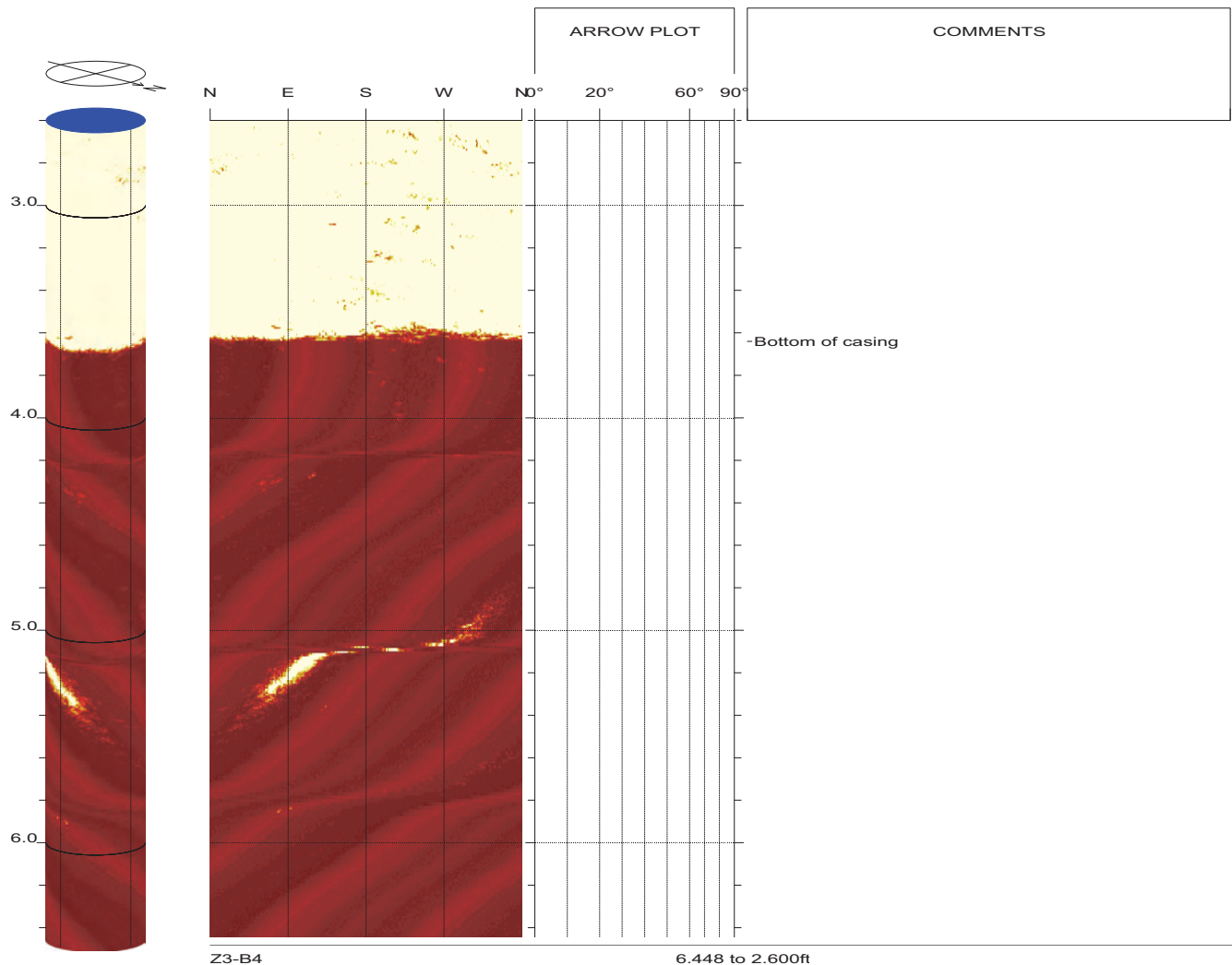
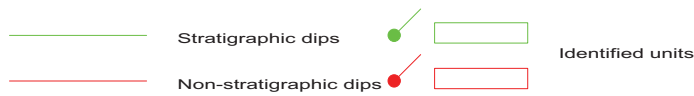
SR-710 TUNNEL INVESTIGATION

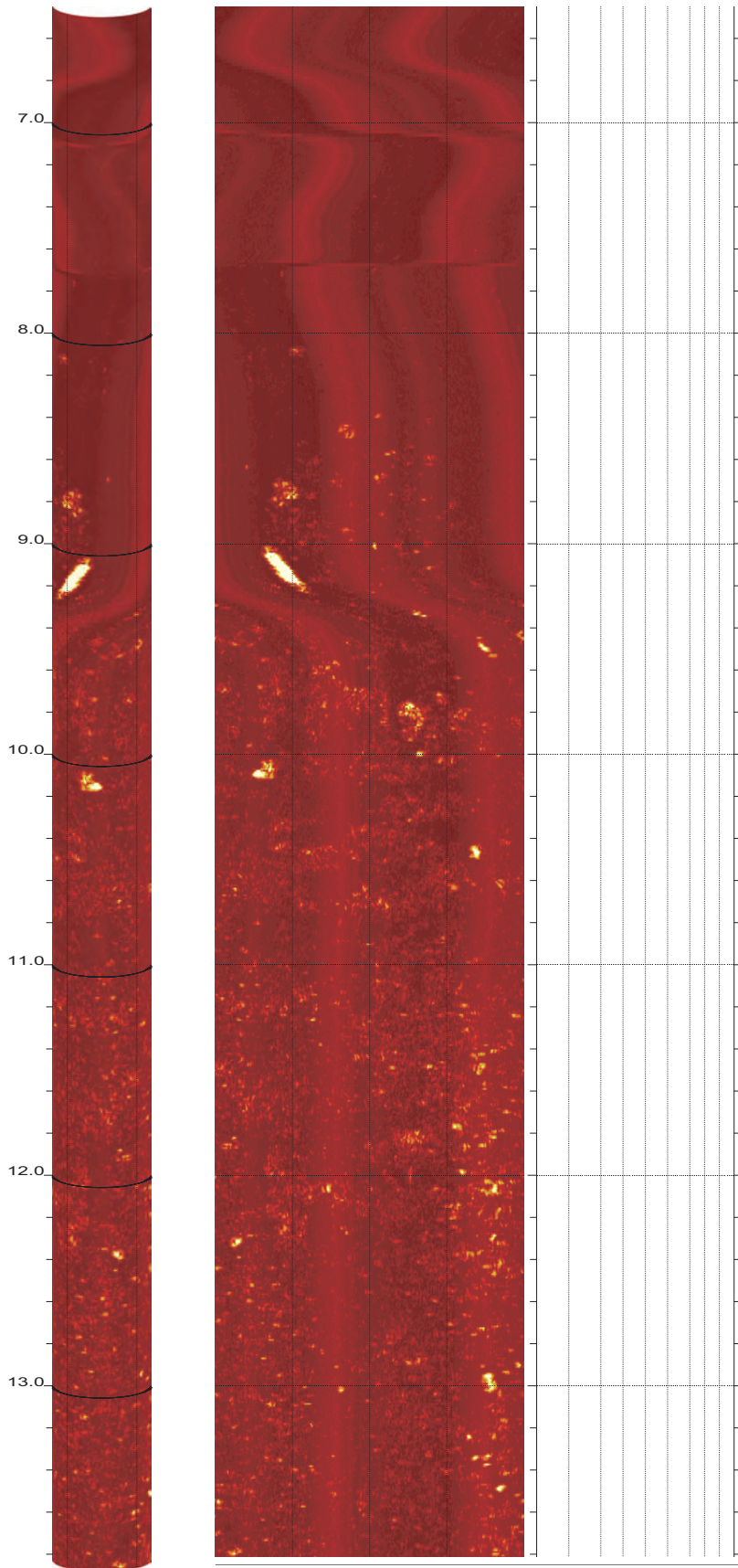
top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

Zone from 275.000 to 2.600ft  
 Format: BHTV-NESWN

Borehole diam: 5.600inch  
 Vertical = borehole-axis  
 Image: Amplitude





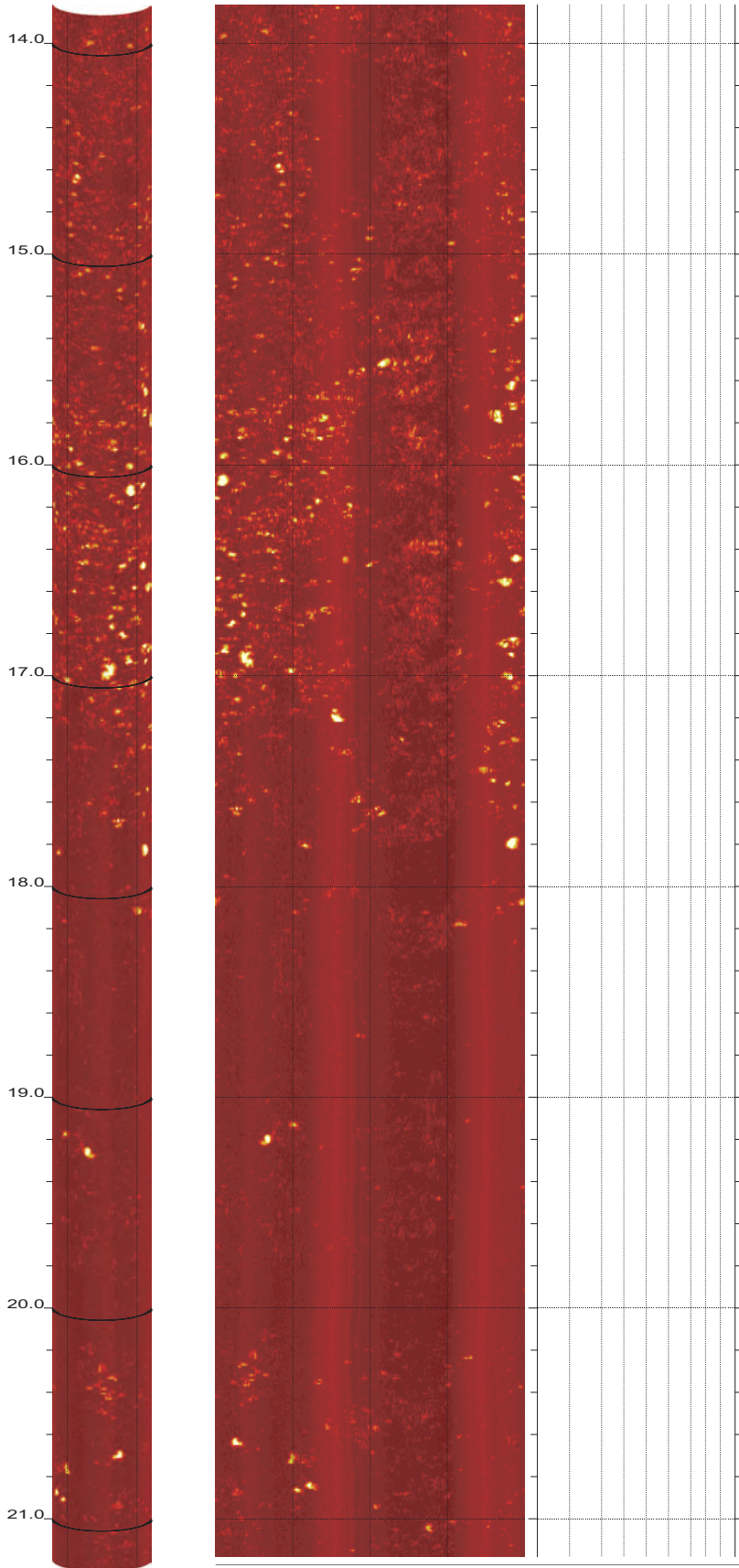
Z3-B4

13.816 to 6.448ft

2

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 2 of 38



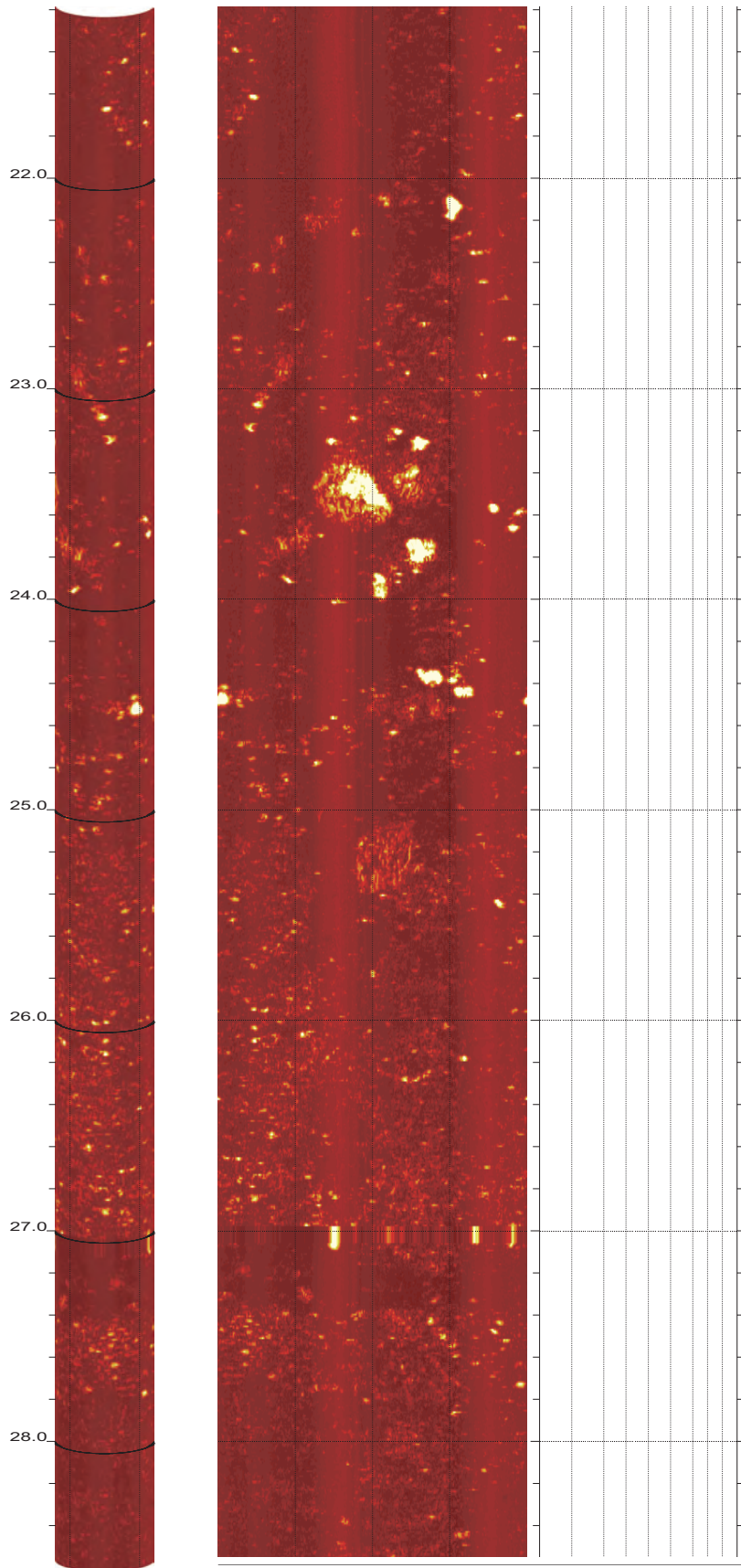


Z3-B4

21.184 to 13.816ft

3

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 3 of 38

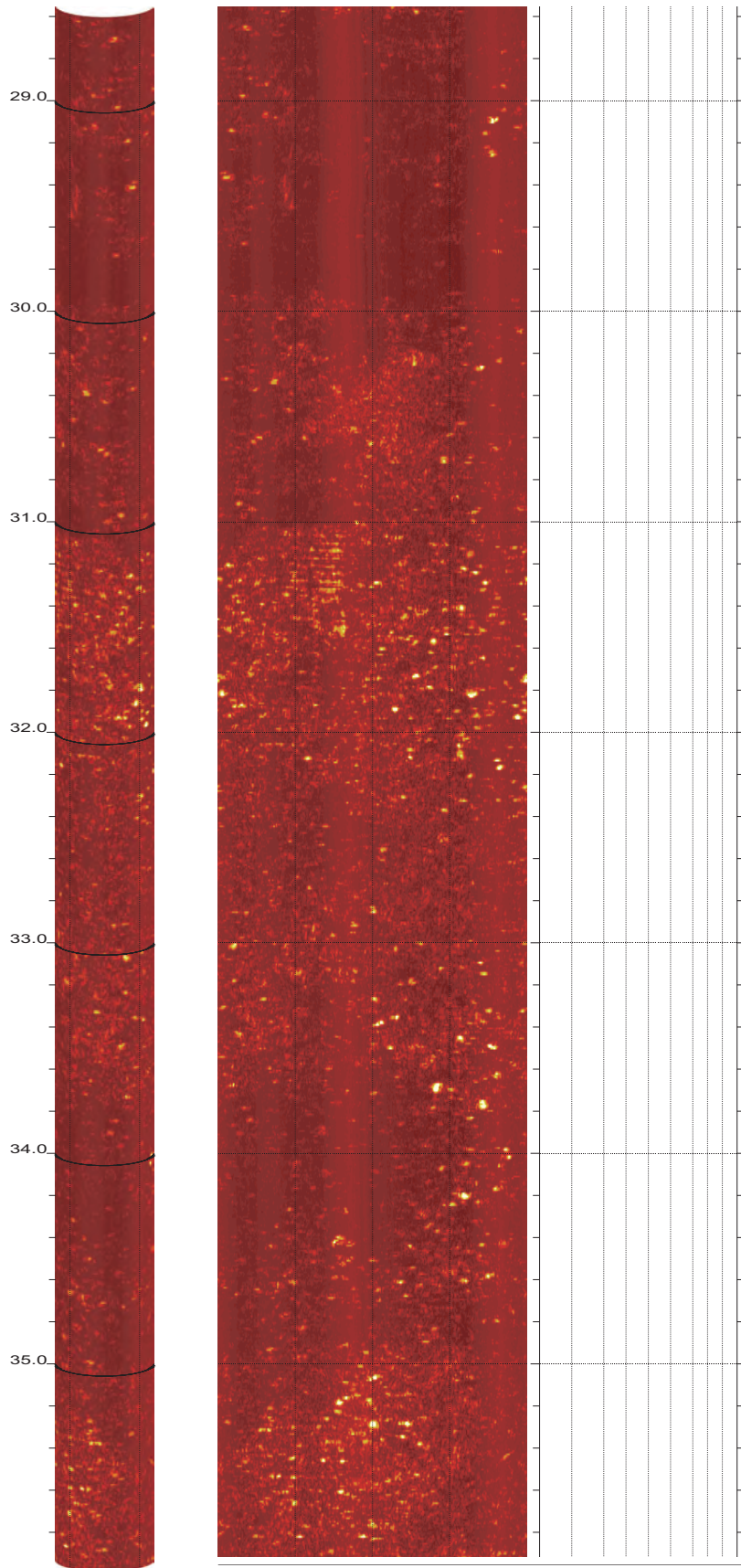


Z3-B4

28.552 to 21.184ft

4

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 4 of 38

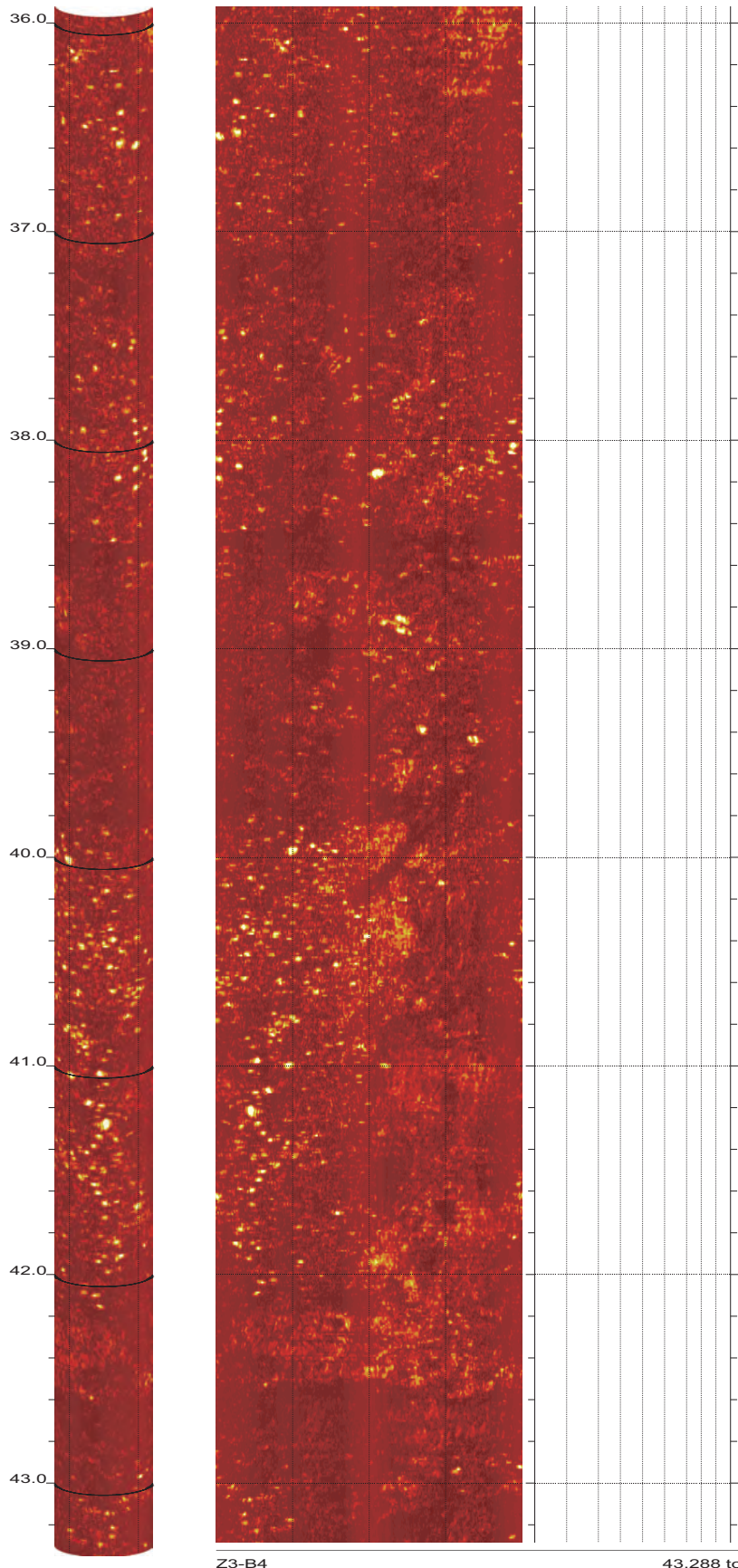


Z3-B4

35.920 to 28.552ft

5

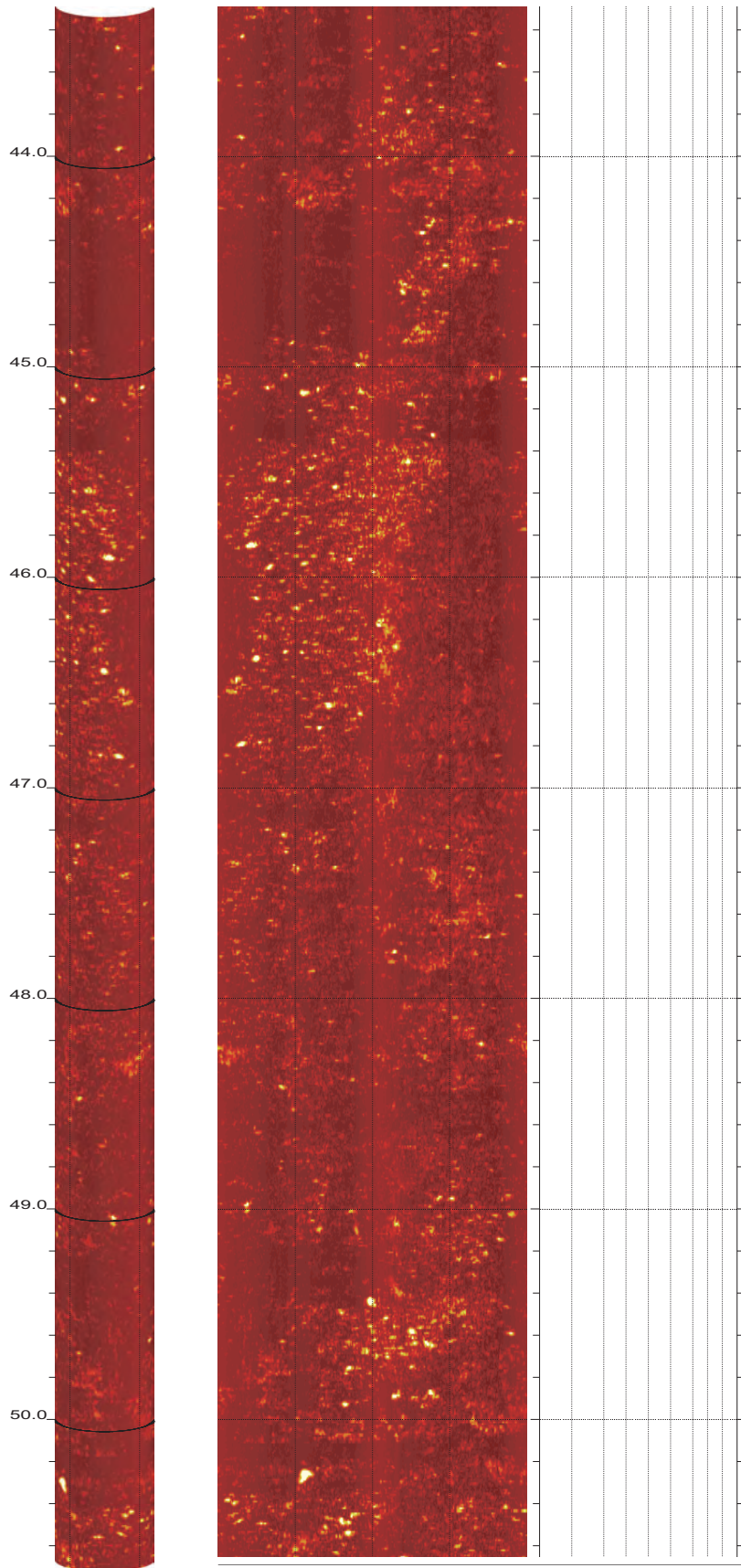
SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 5 of 38



Z3-B4

43.288 to 35.920ft

6

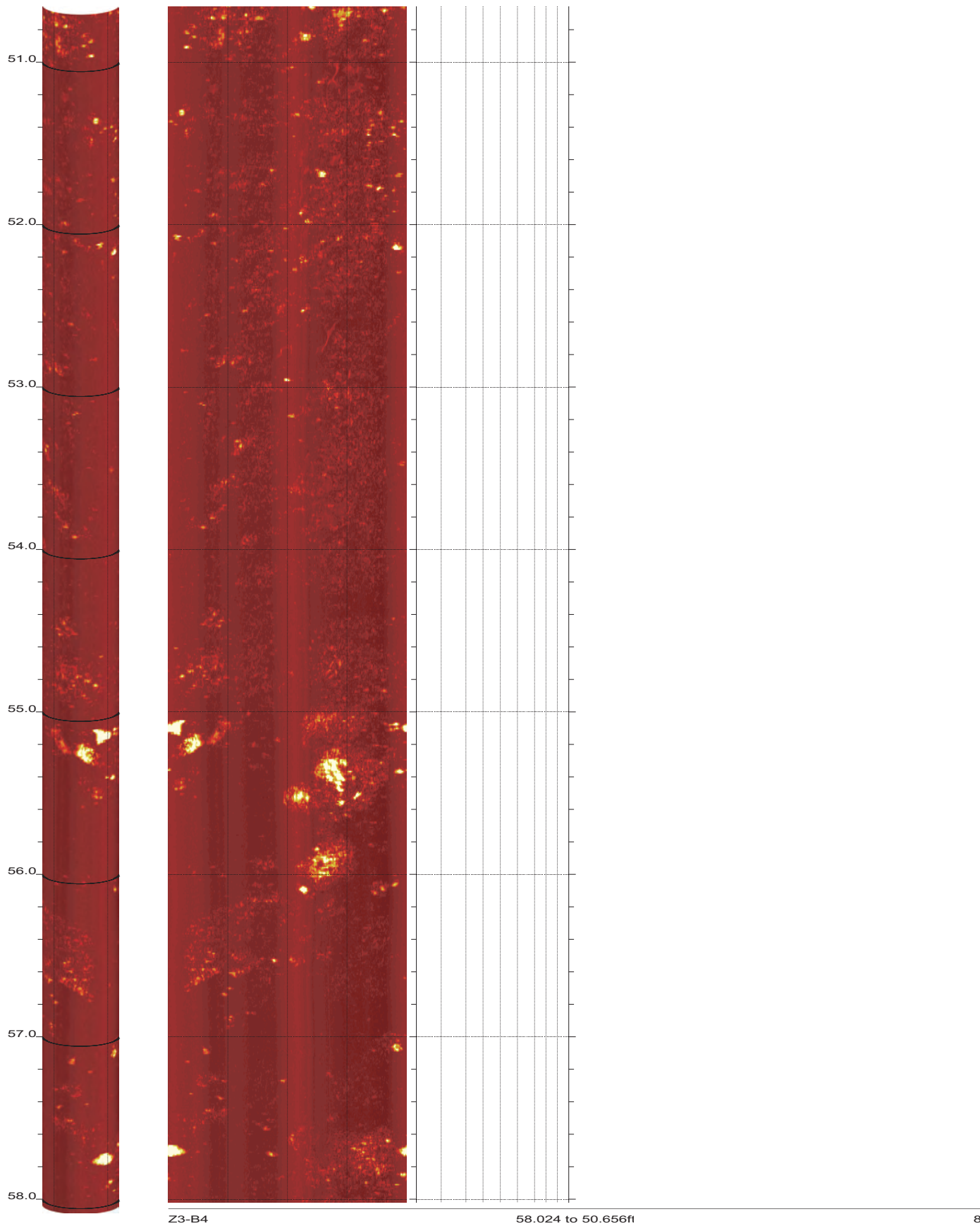


Z3-B4

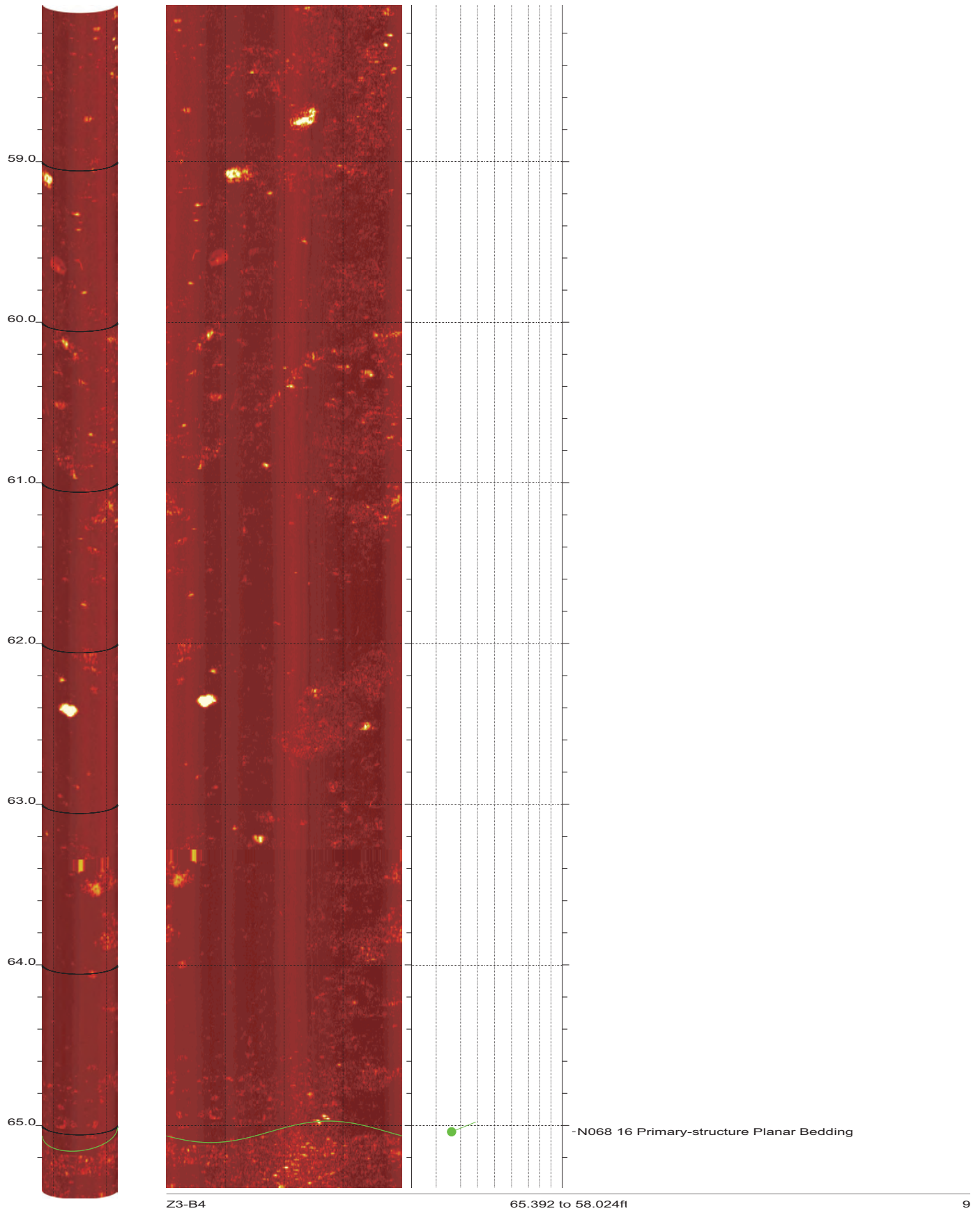
50.656 to 43.288ft

7

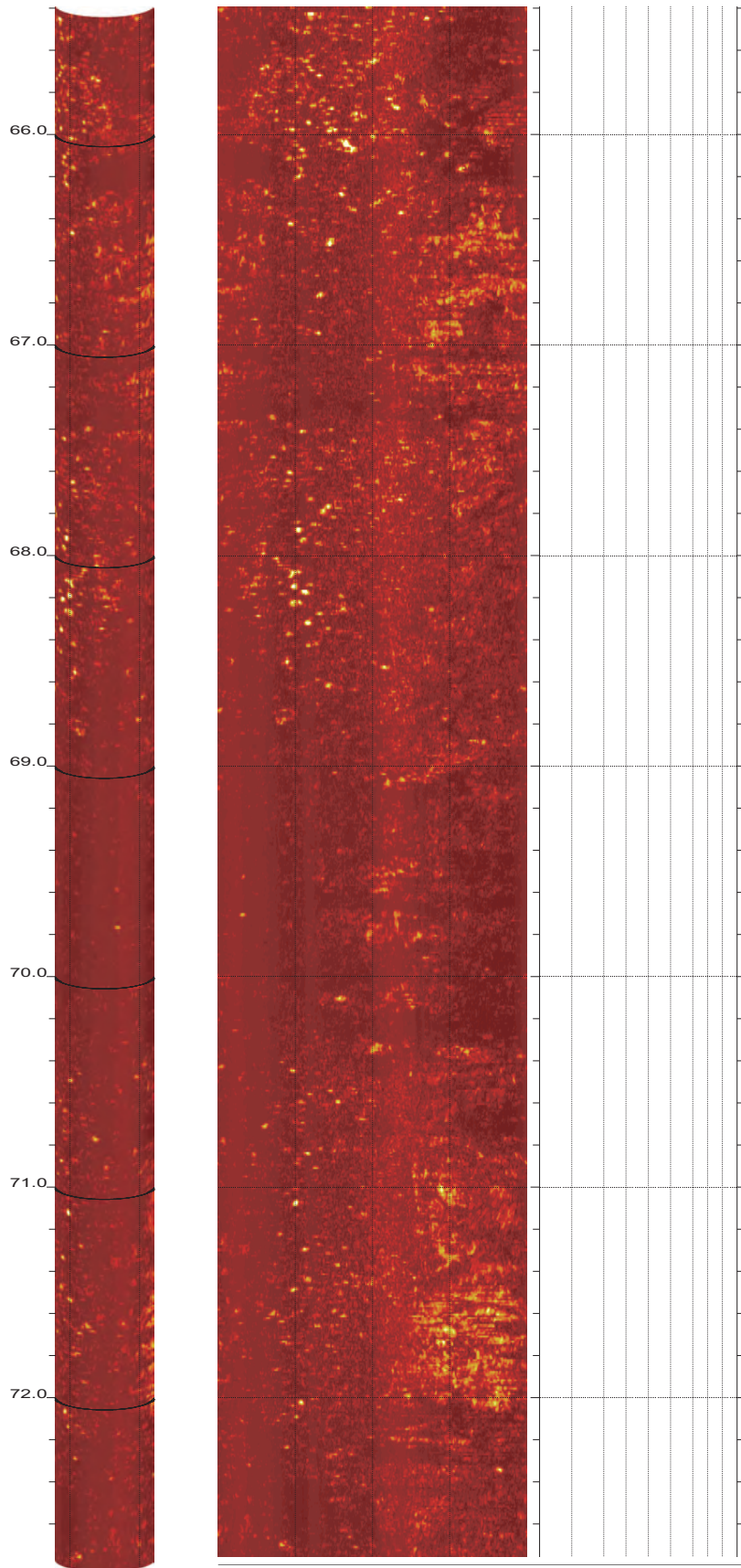
SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 7 of 38



SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 8 of 38



SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 9 of 38



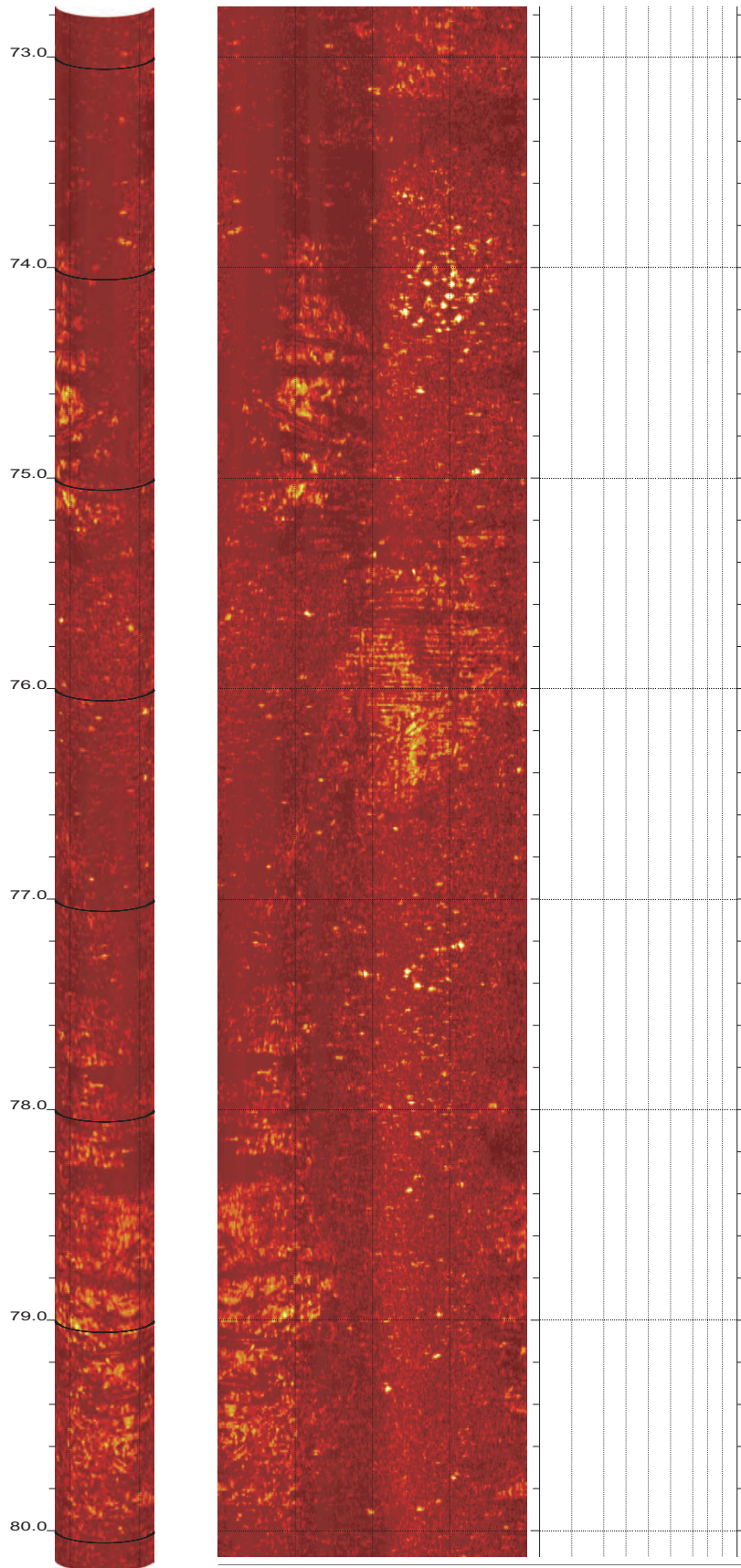
Z3-B4

72.760 to 65.392ft

10

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 10 of 38

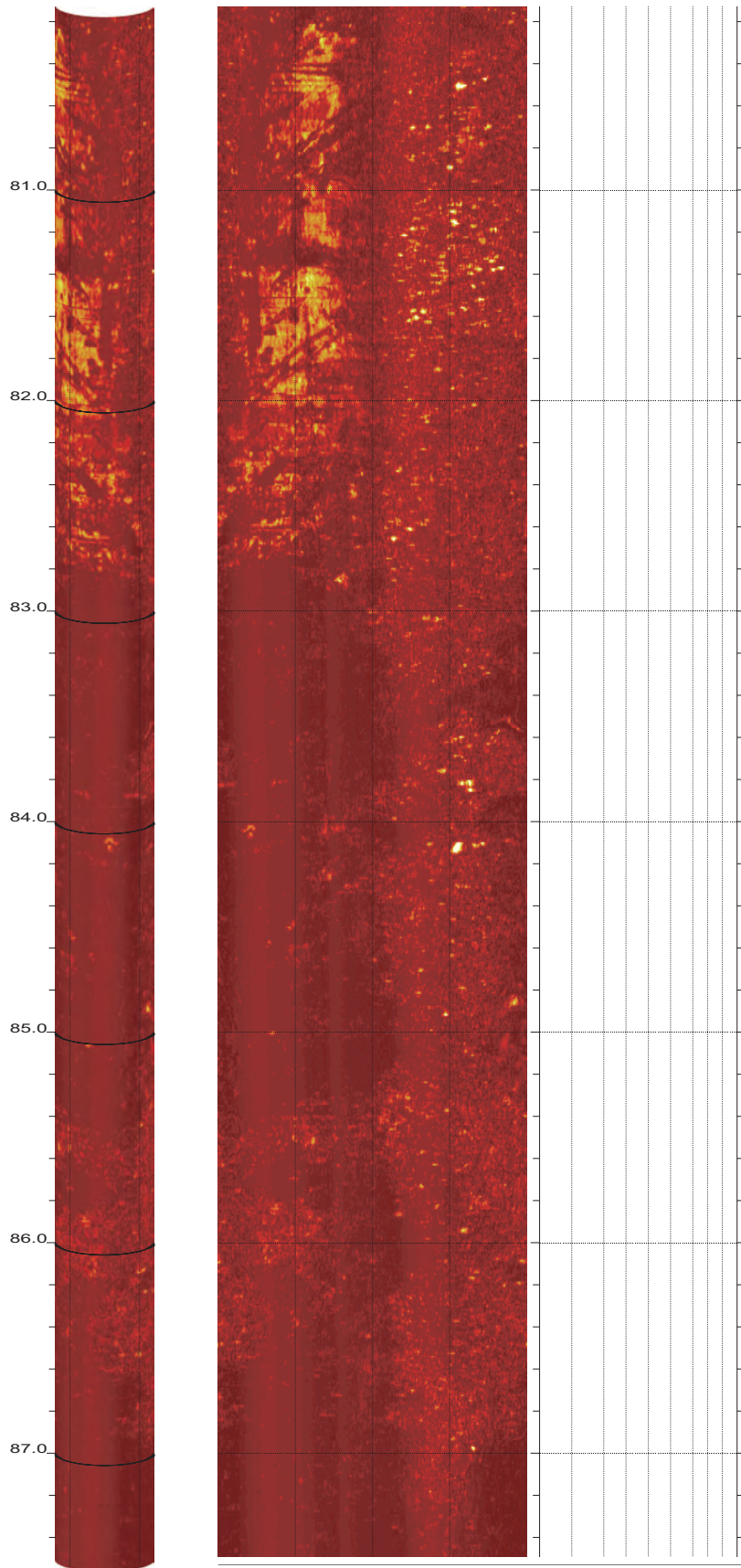




Z3-B4

80.128 to 72.760ft

11

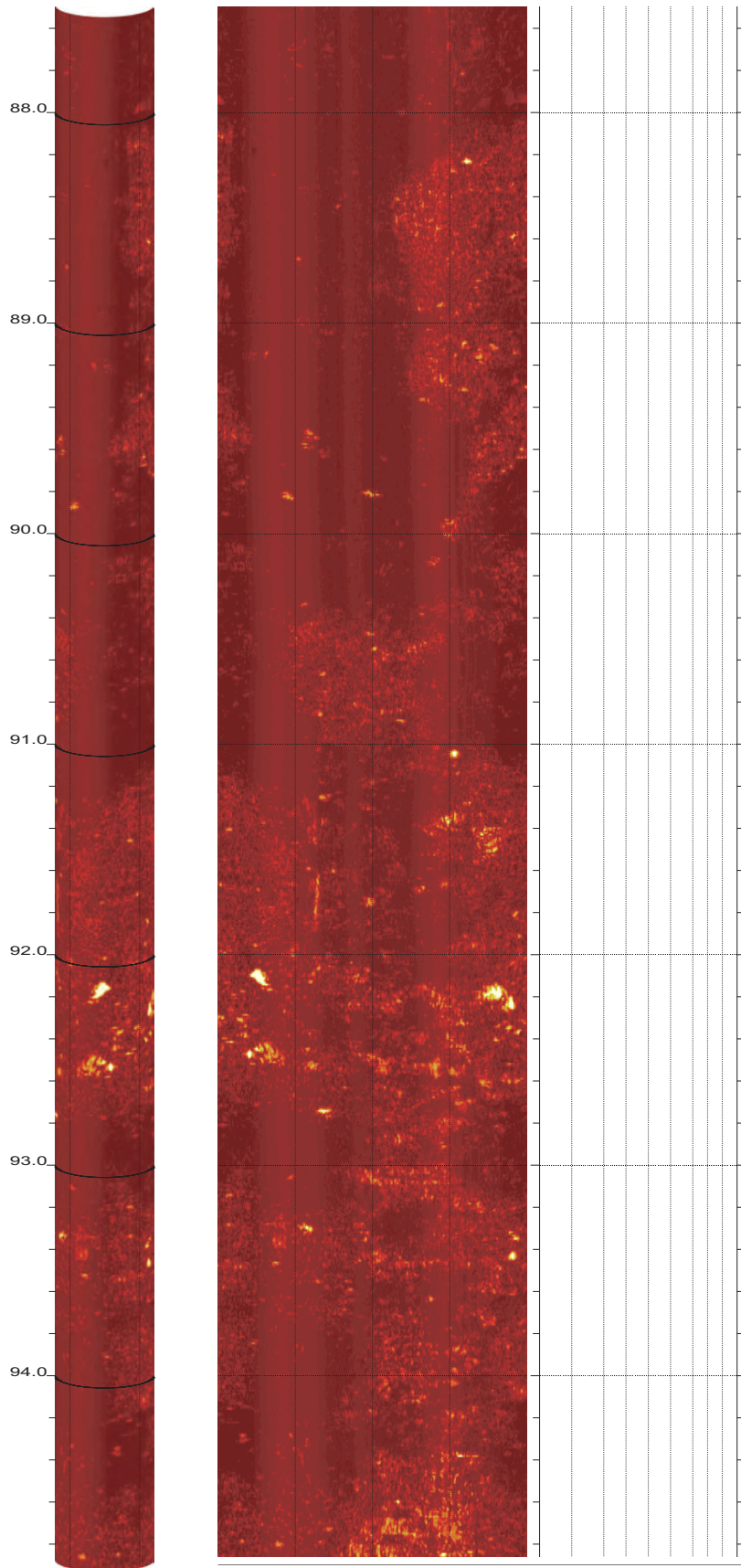


Z3-B4

87.496 to 80.128ft

12

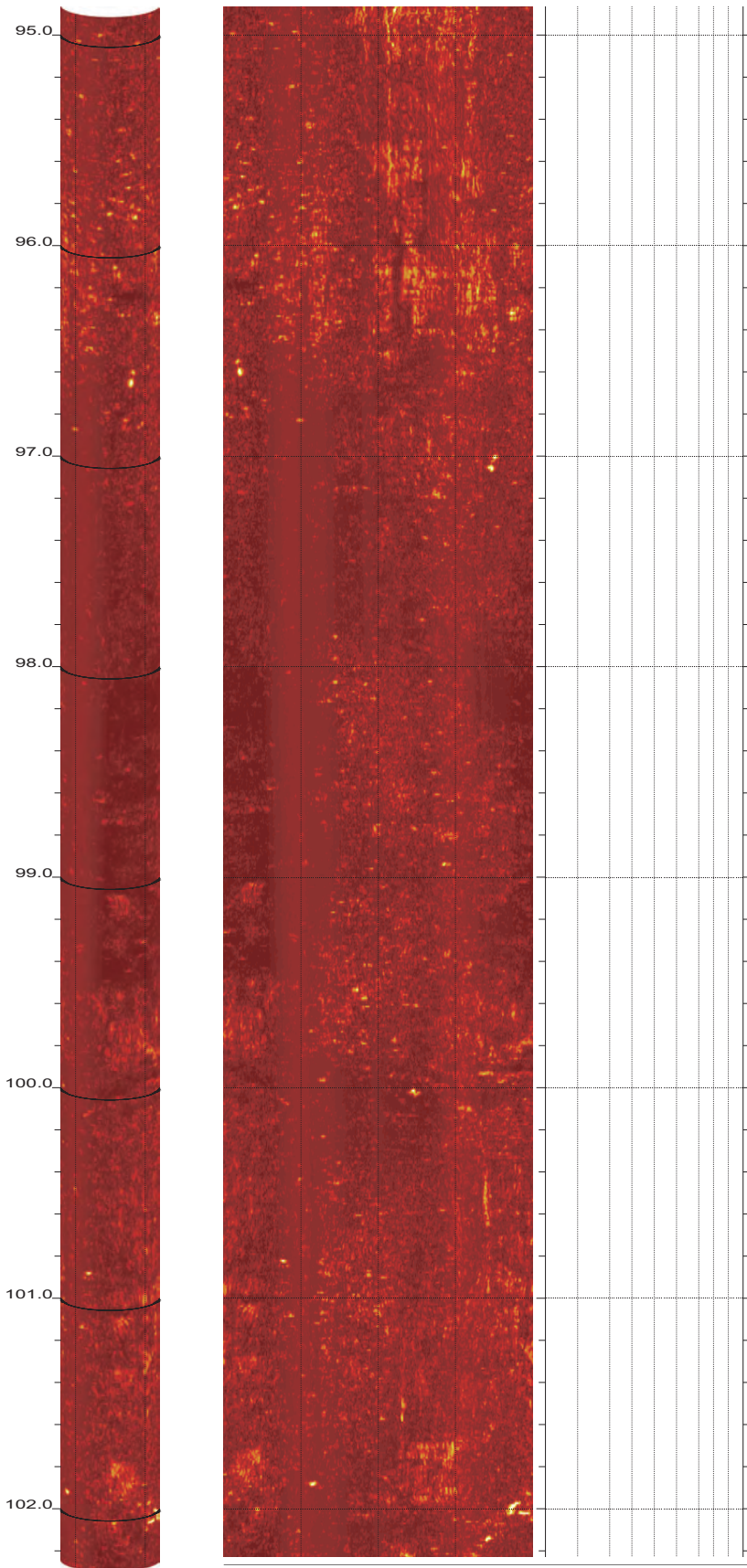
SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 12 of 38



Z3-B4

94.864 to 87.496ft

13

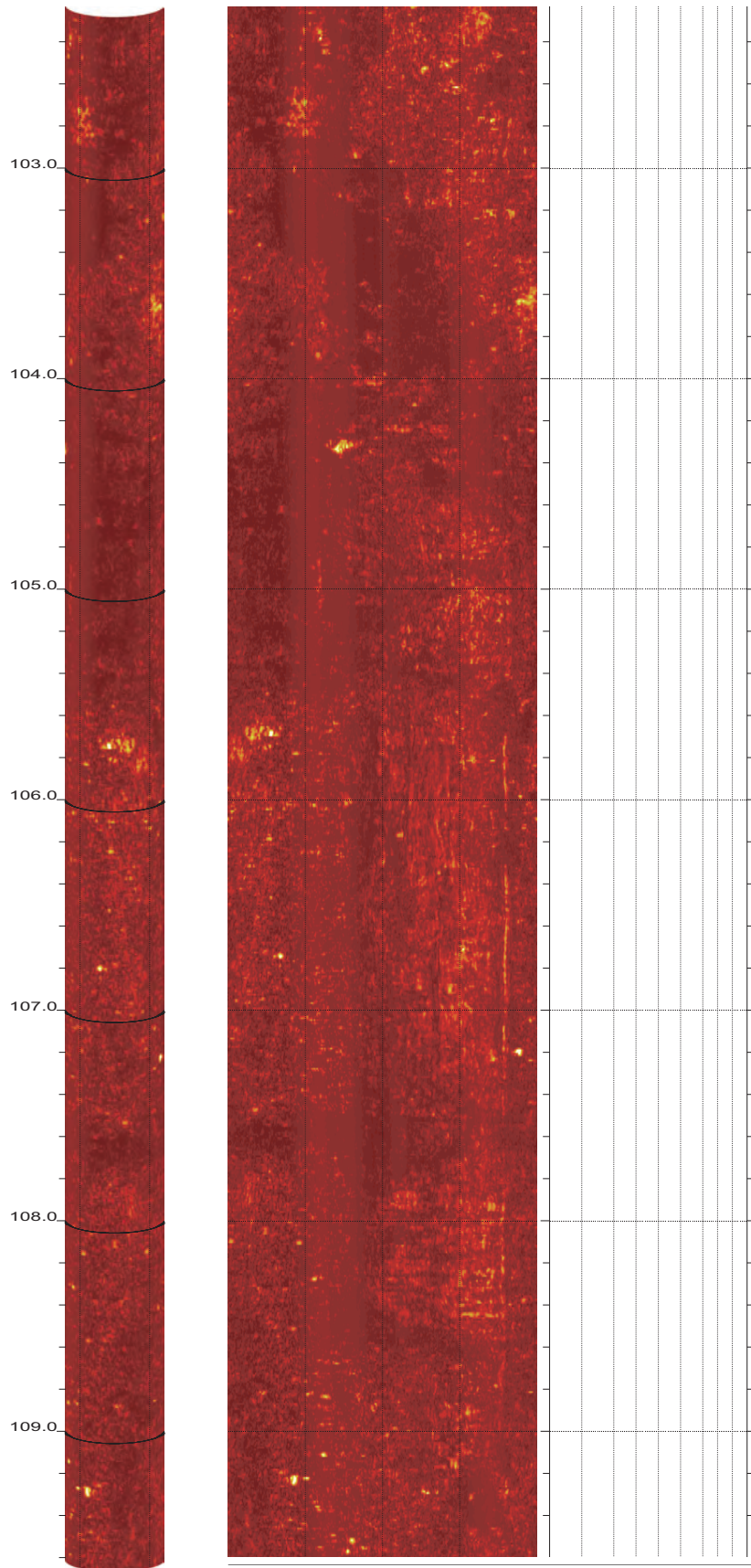


Z3-B4

102.232 to 94.864ft

14

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 14 of 38

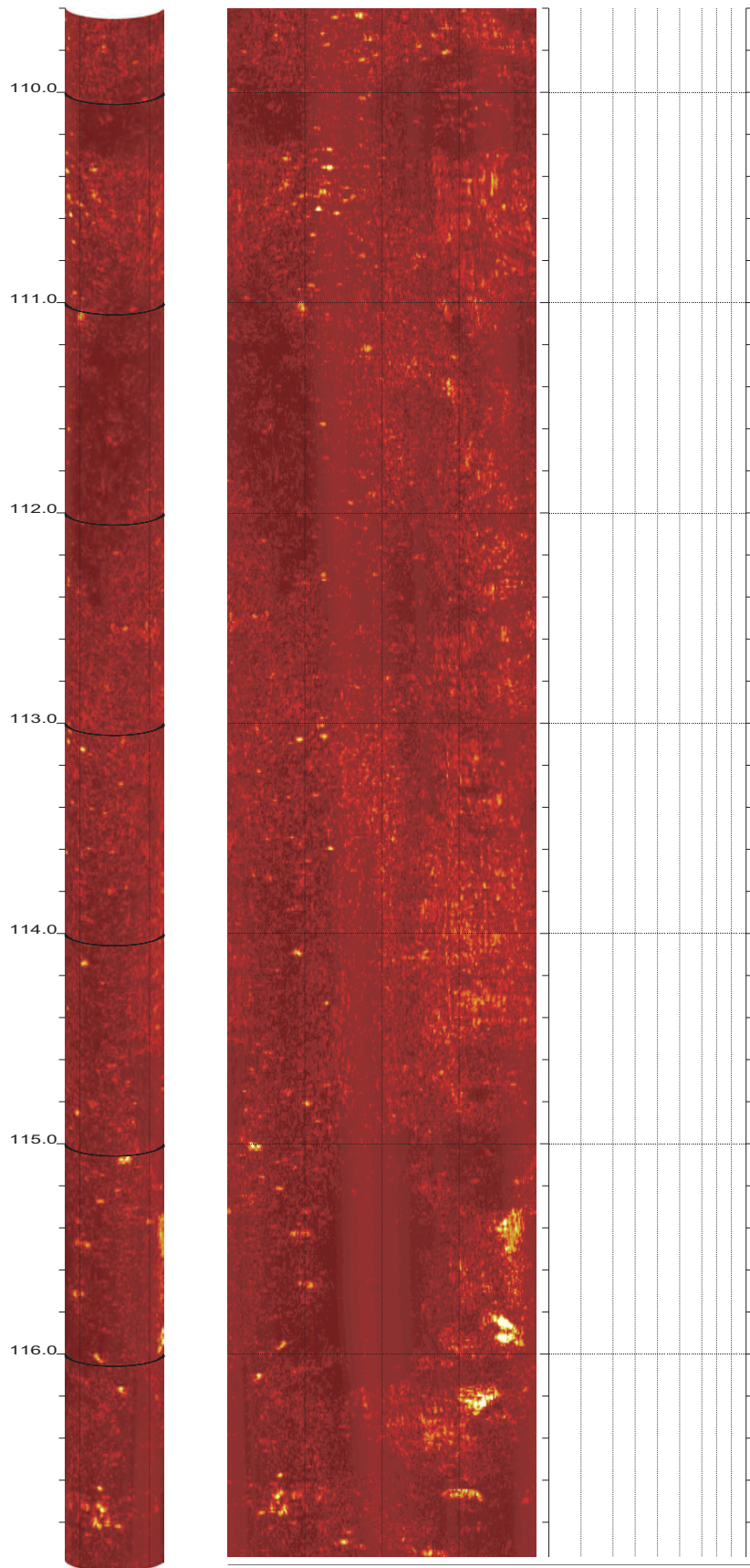


Z3-B4

109.600 to 102.232ft

15

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 15 of 38

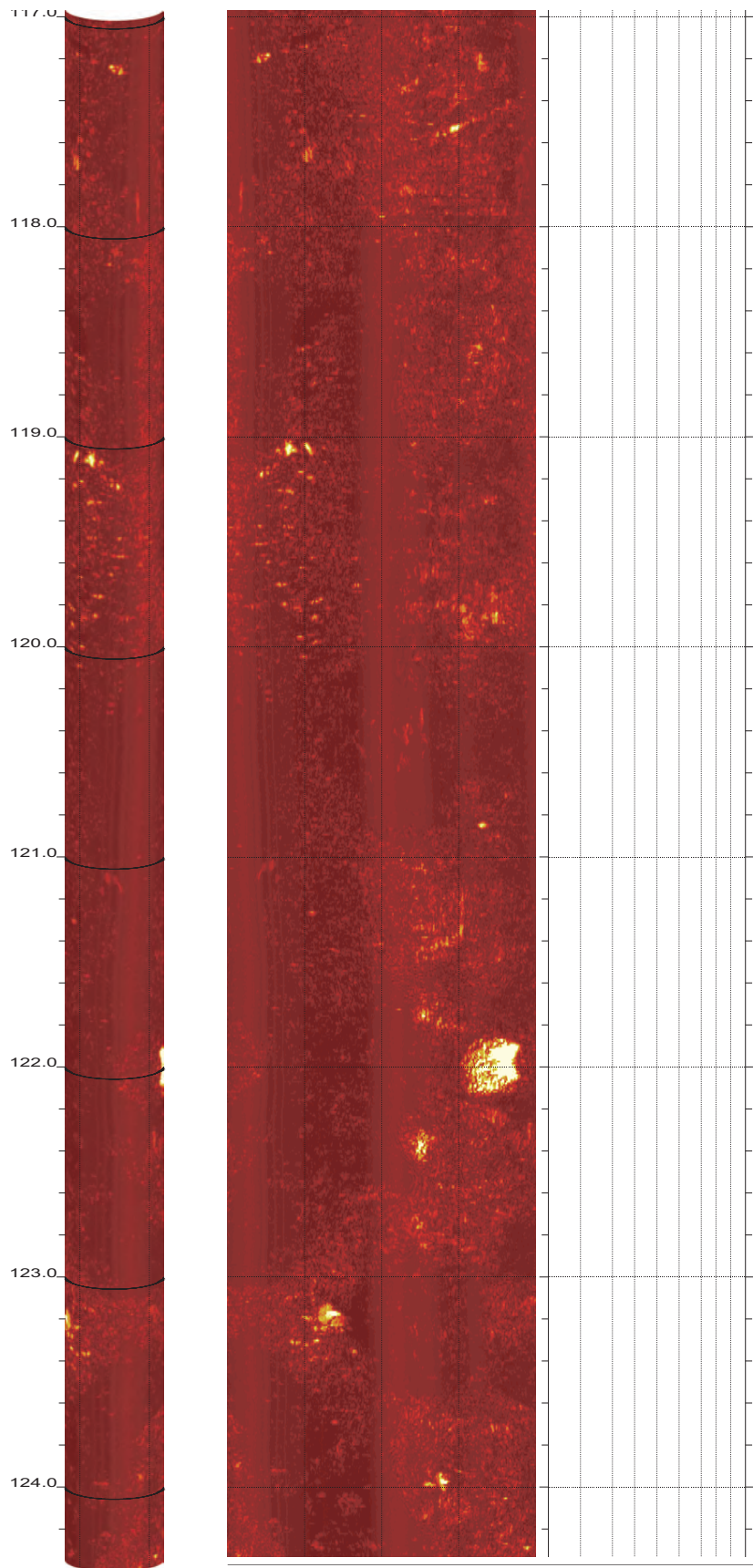


Z3-B4

116.968 to 109.600ft

16

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 16 of 38

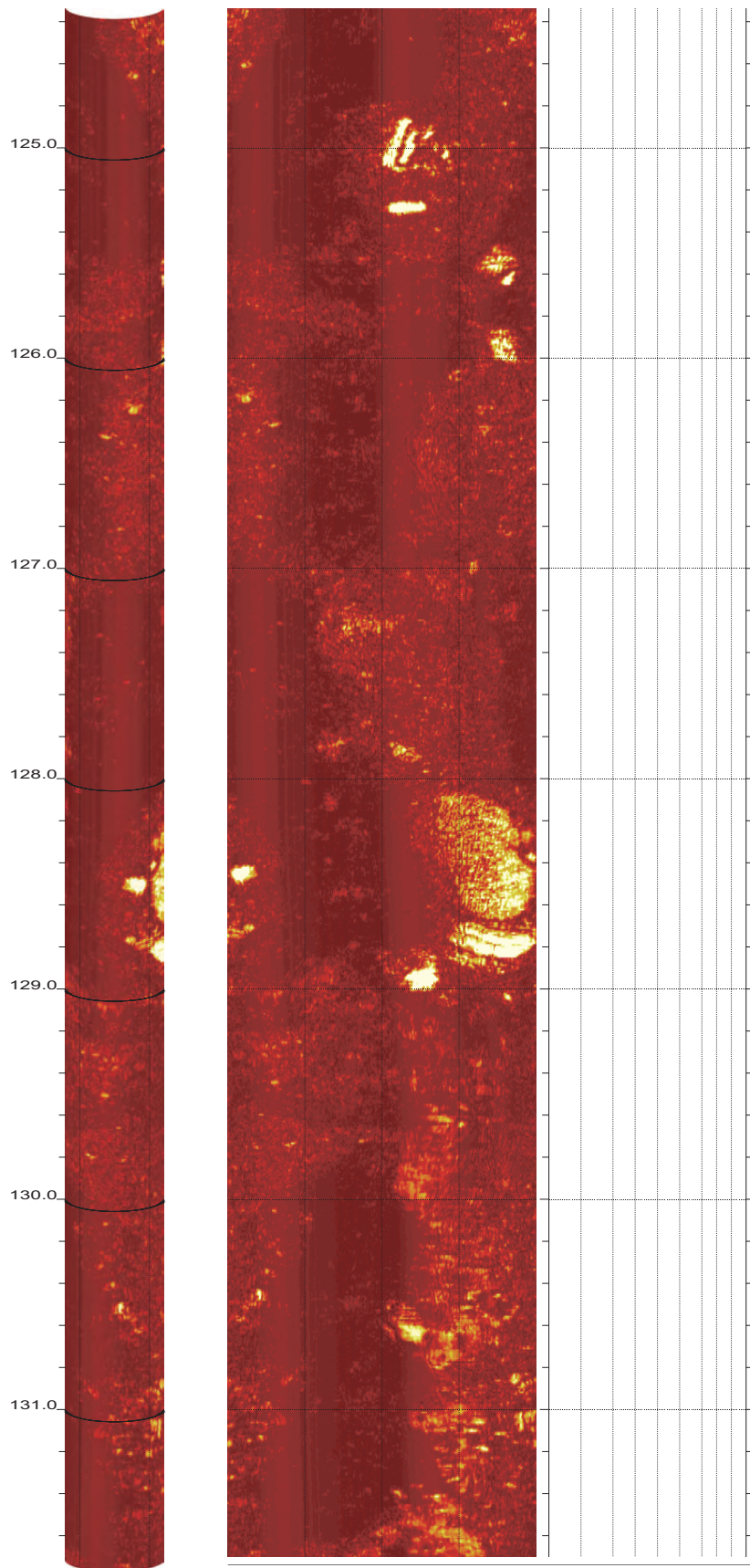


Z3-B4

124.336 to 116.968ft

17

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 17 of 38

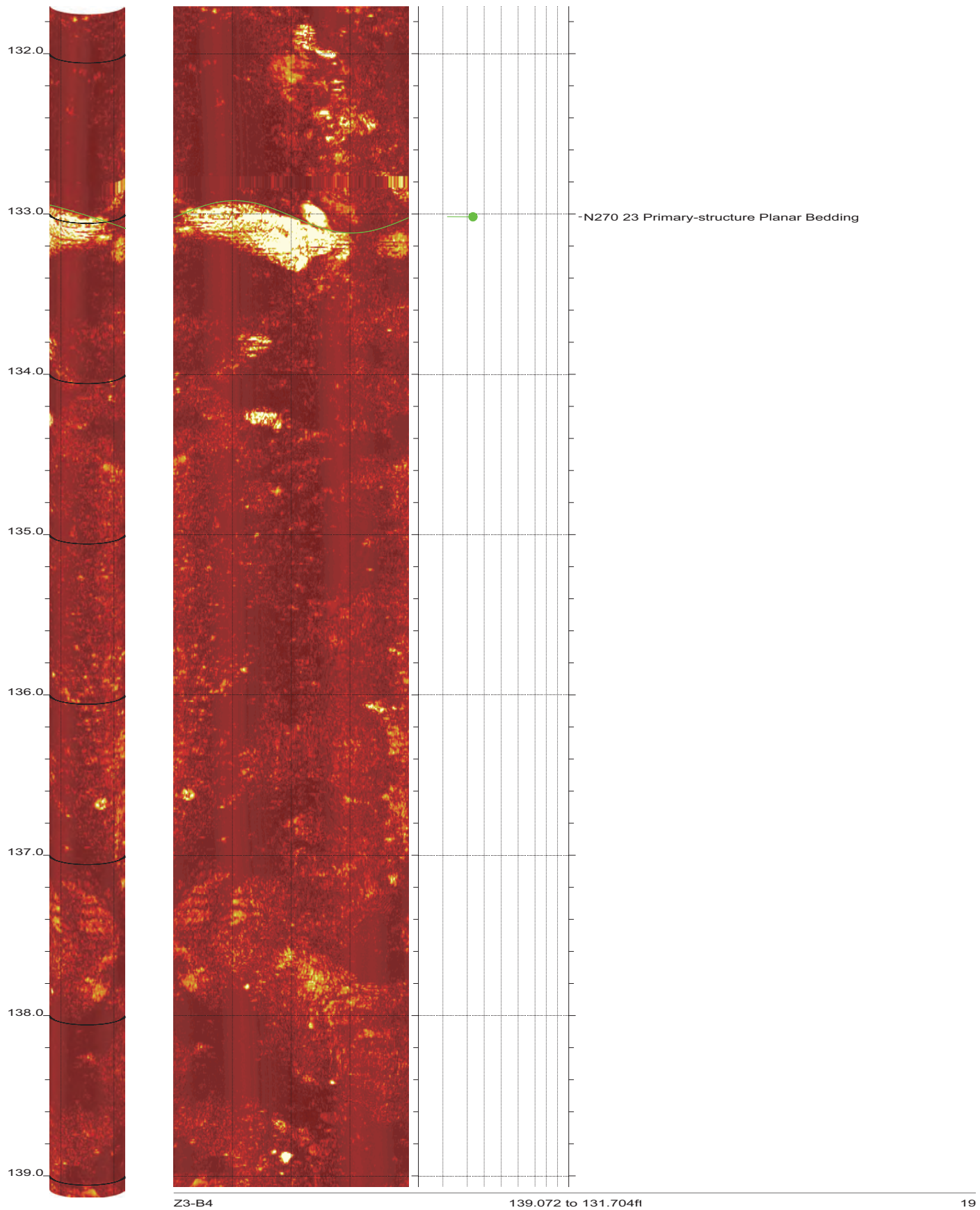


Z3-B4

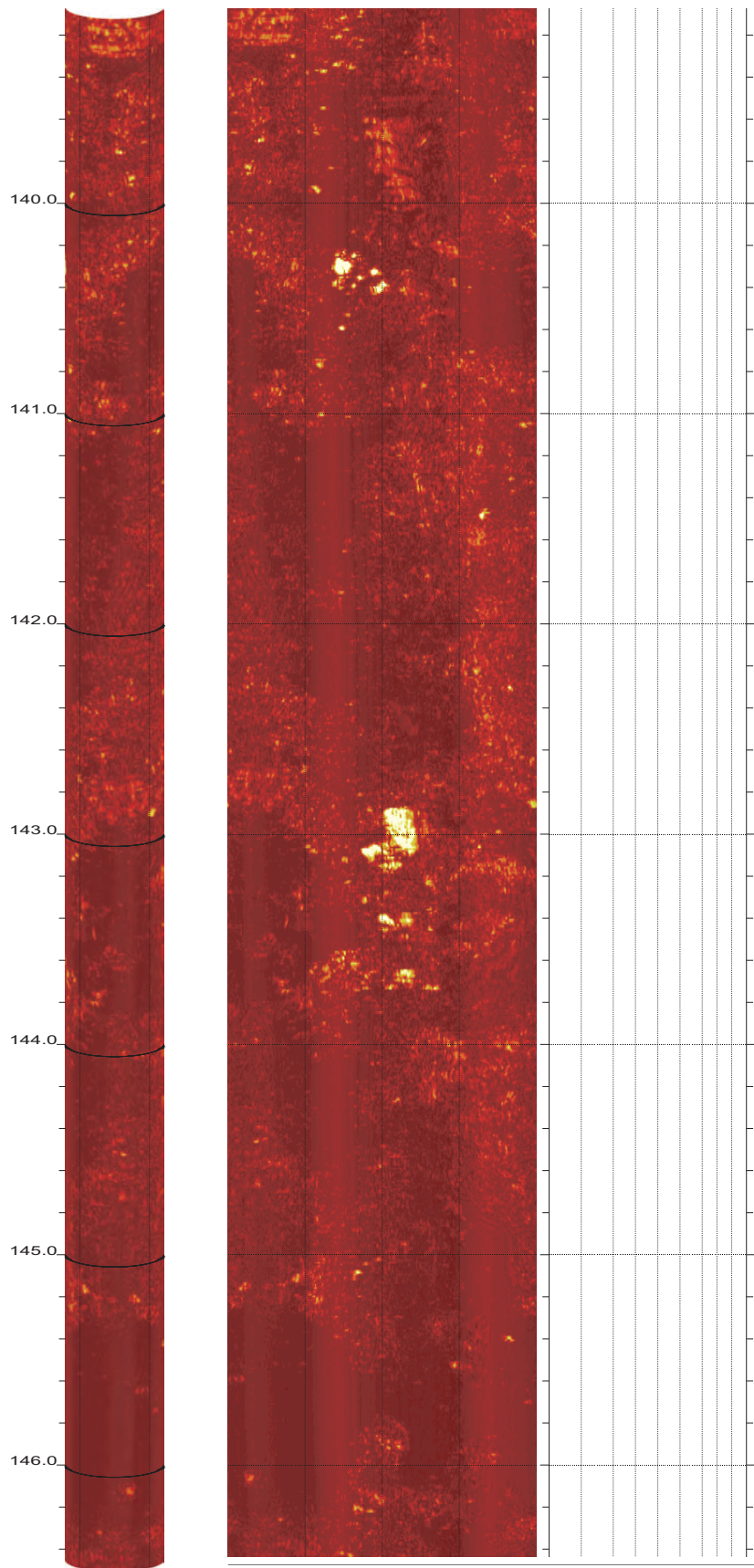
131.704 to 124.336ft

18





SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 19 of 38

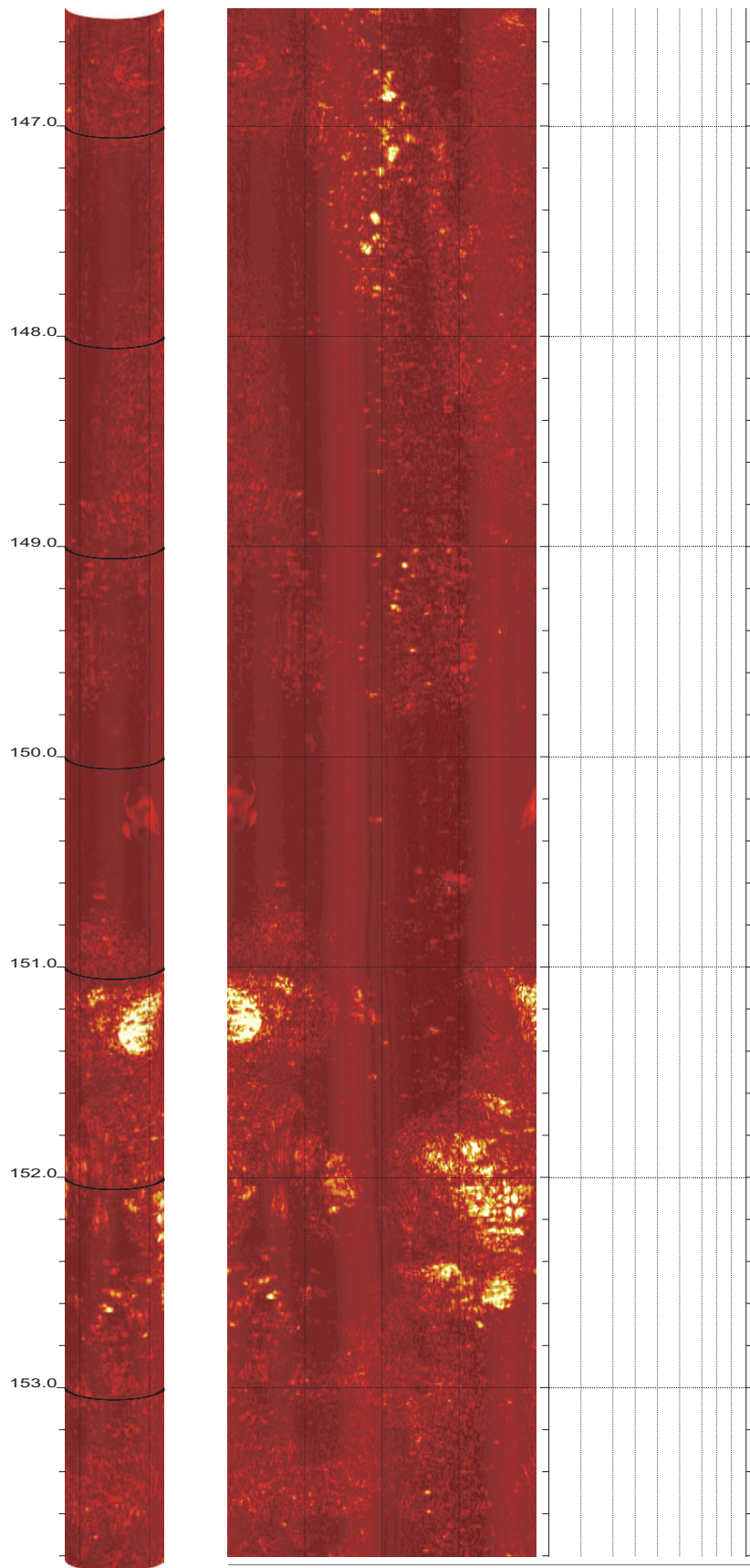


Z3-B4

146.440 to 139.072ft

20

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 20 of 38

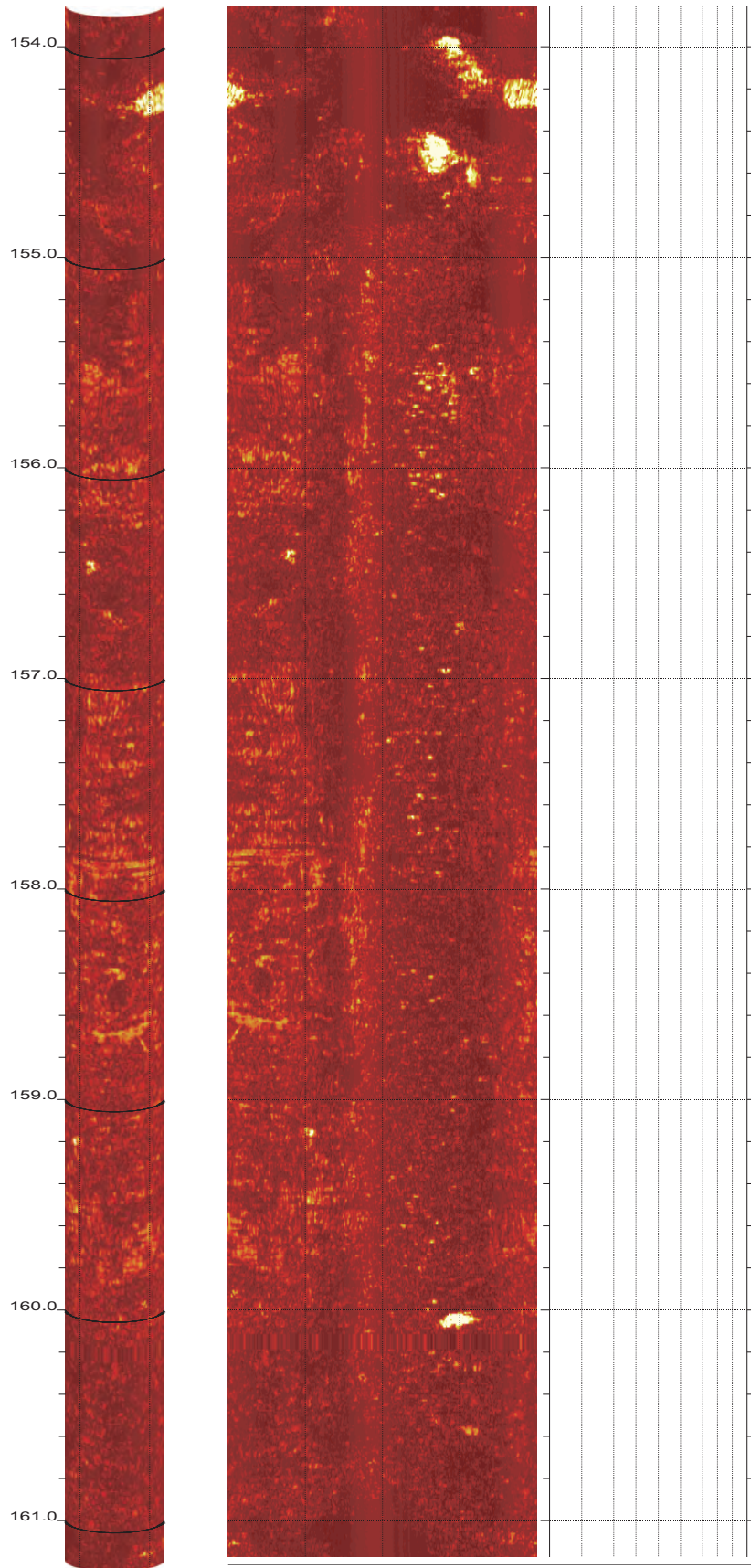


Z3-B4

153.808 to 146.440ft

21

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 21 of 38

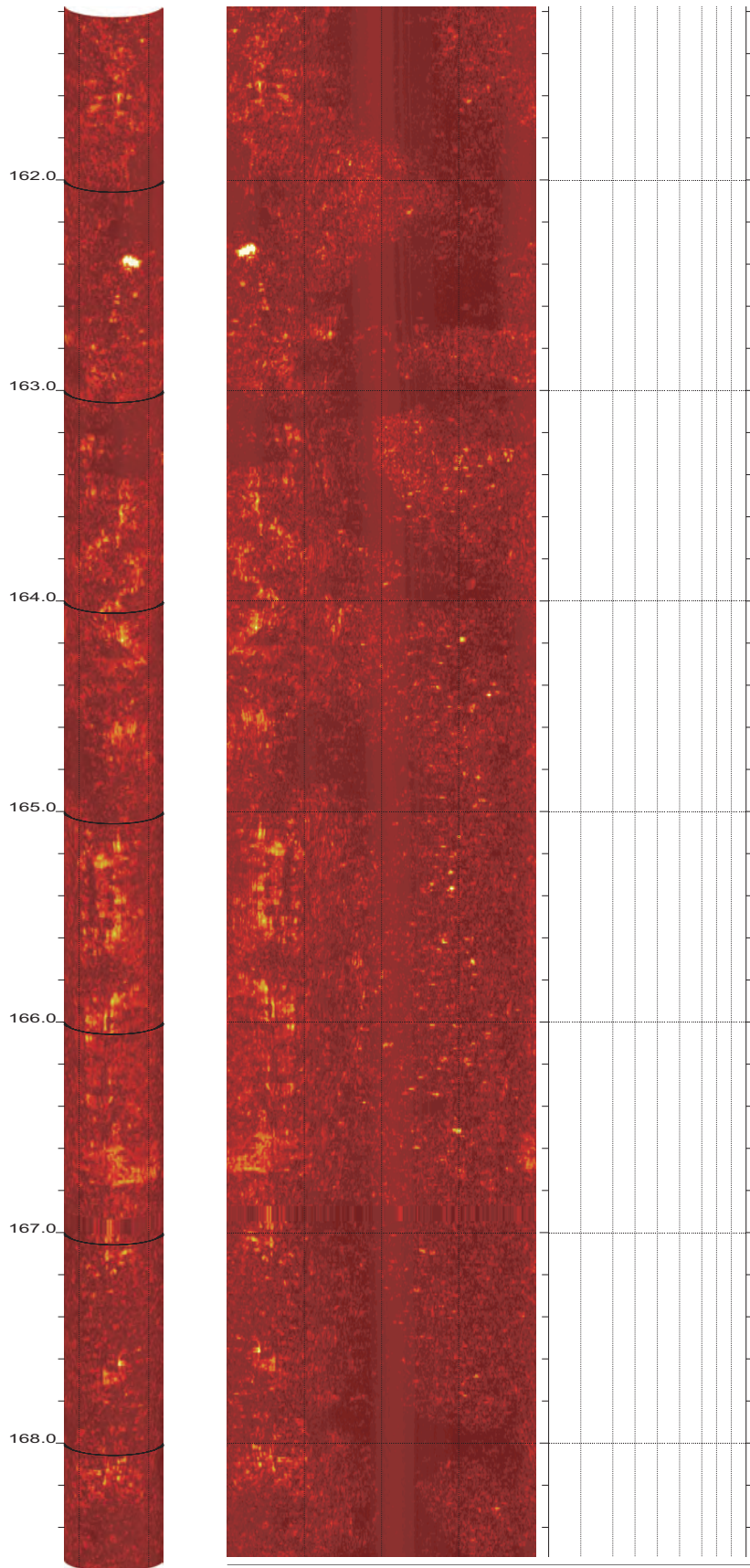


Z3-B4

161.176 to 153.808ft

22

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 22 of 38

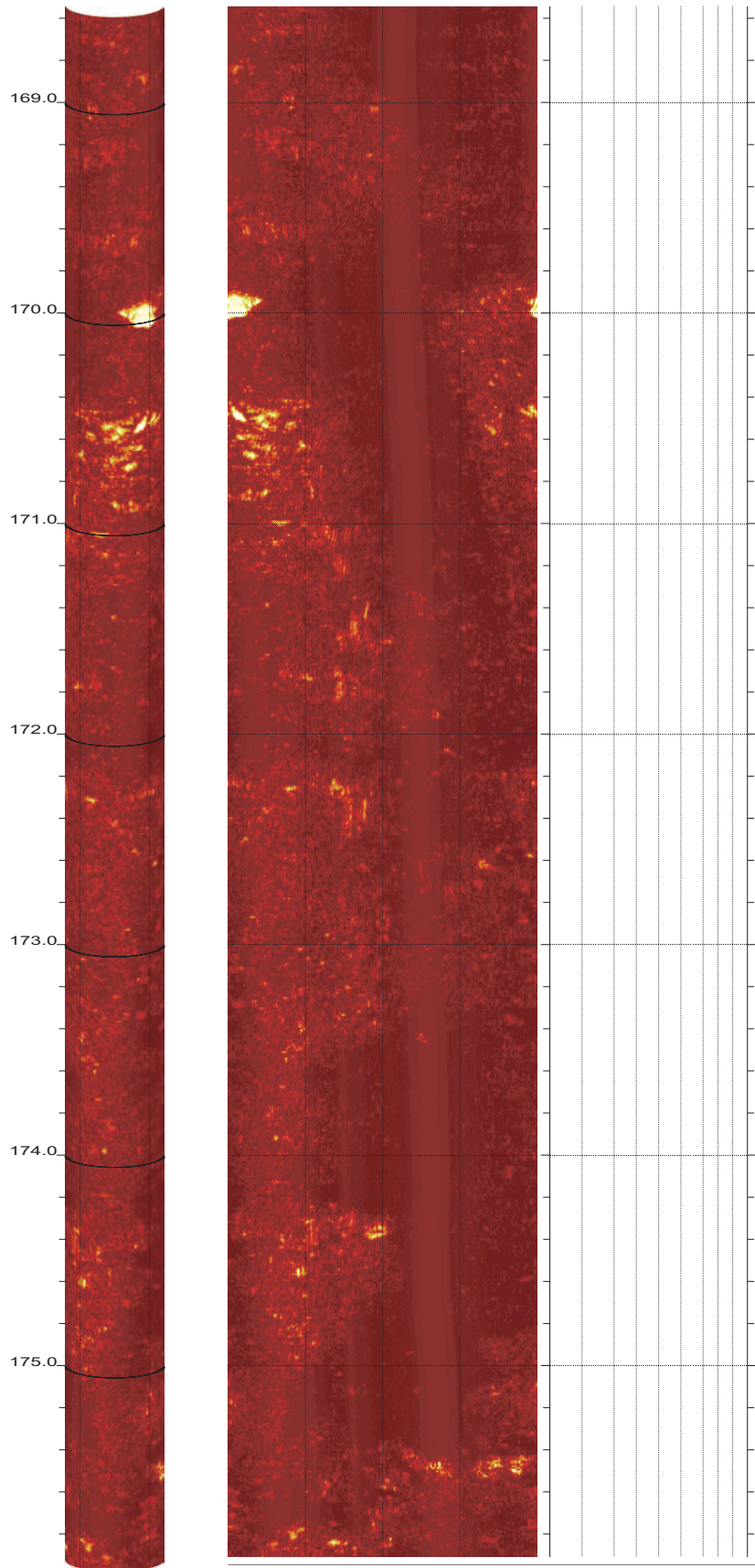


Z3-B4

168.544 to 161.176ft

23

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 23 of 38

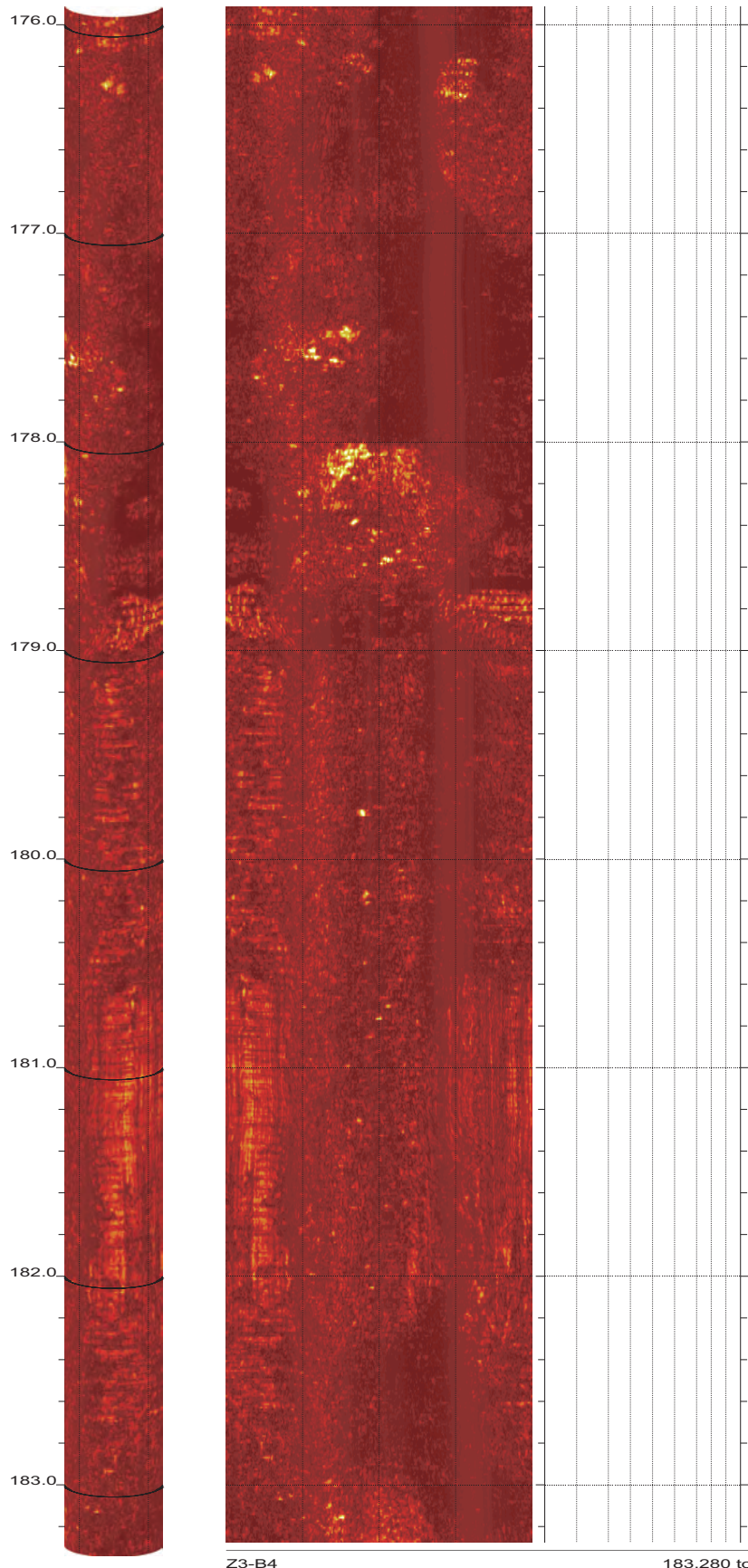


Z3-B4

175.912 to 168.544ft

24

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 24 of 38

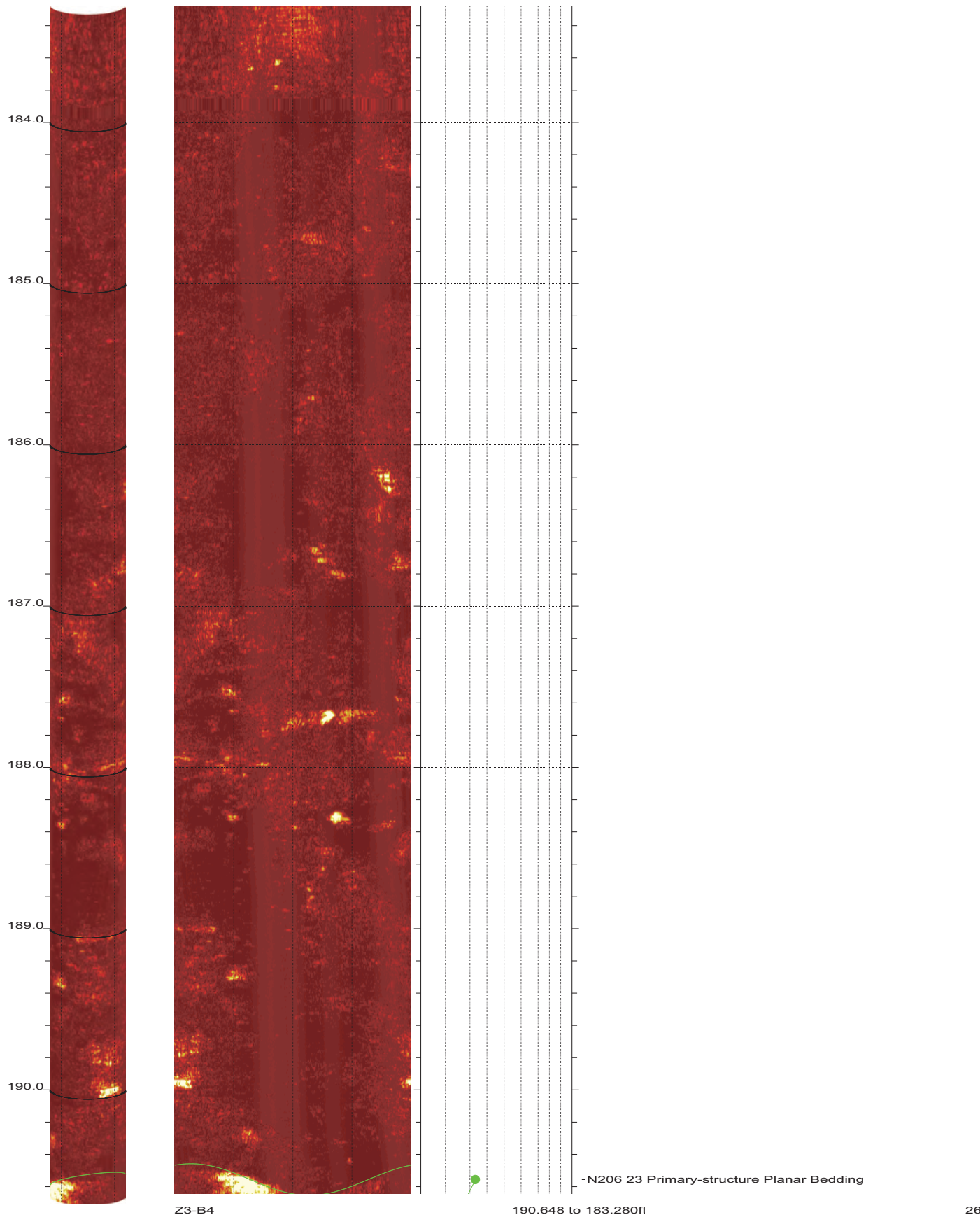


Z3-B4

183.280 to 175.912ft

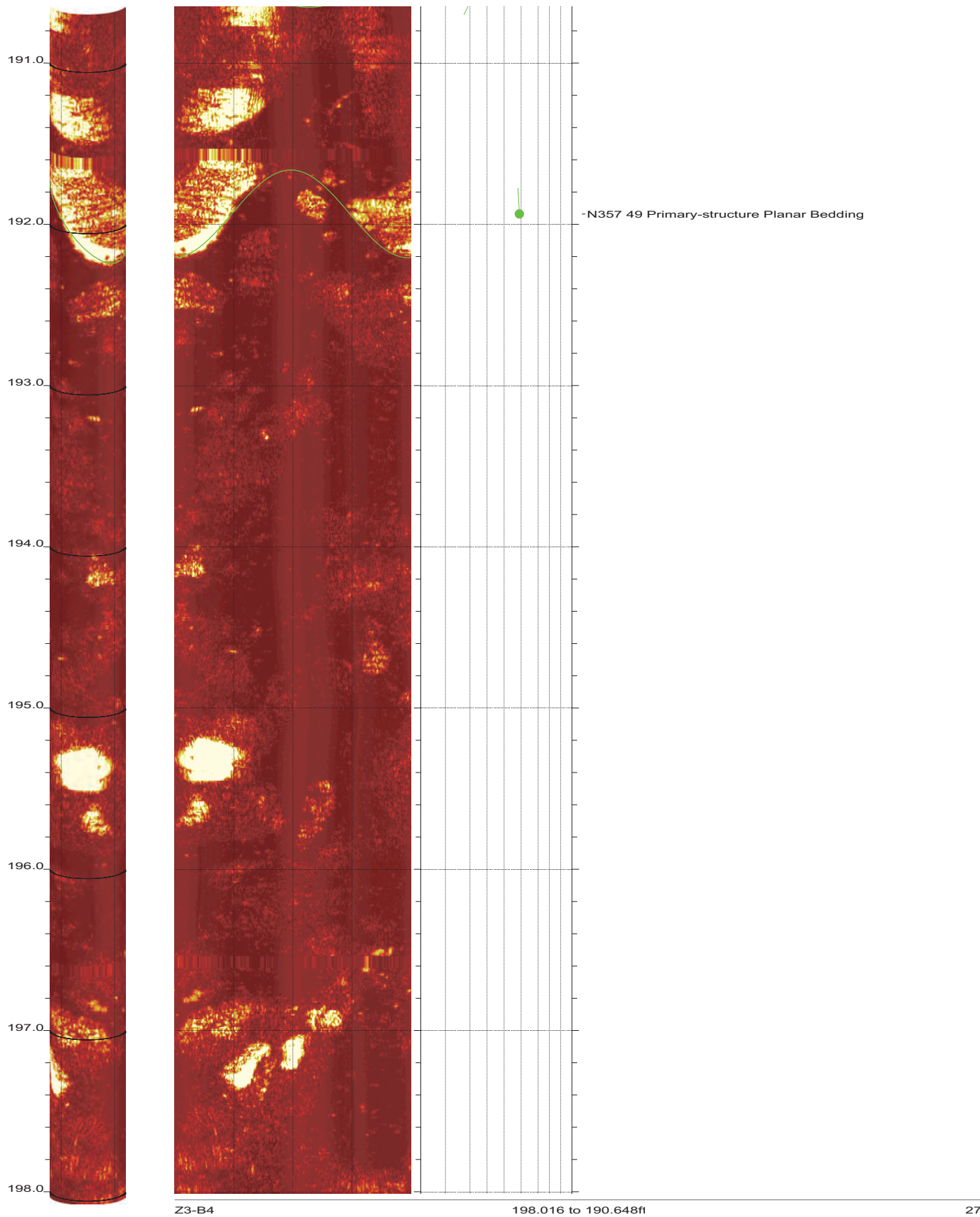
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SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 25 of 38

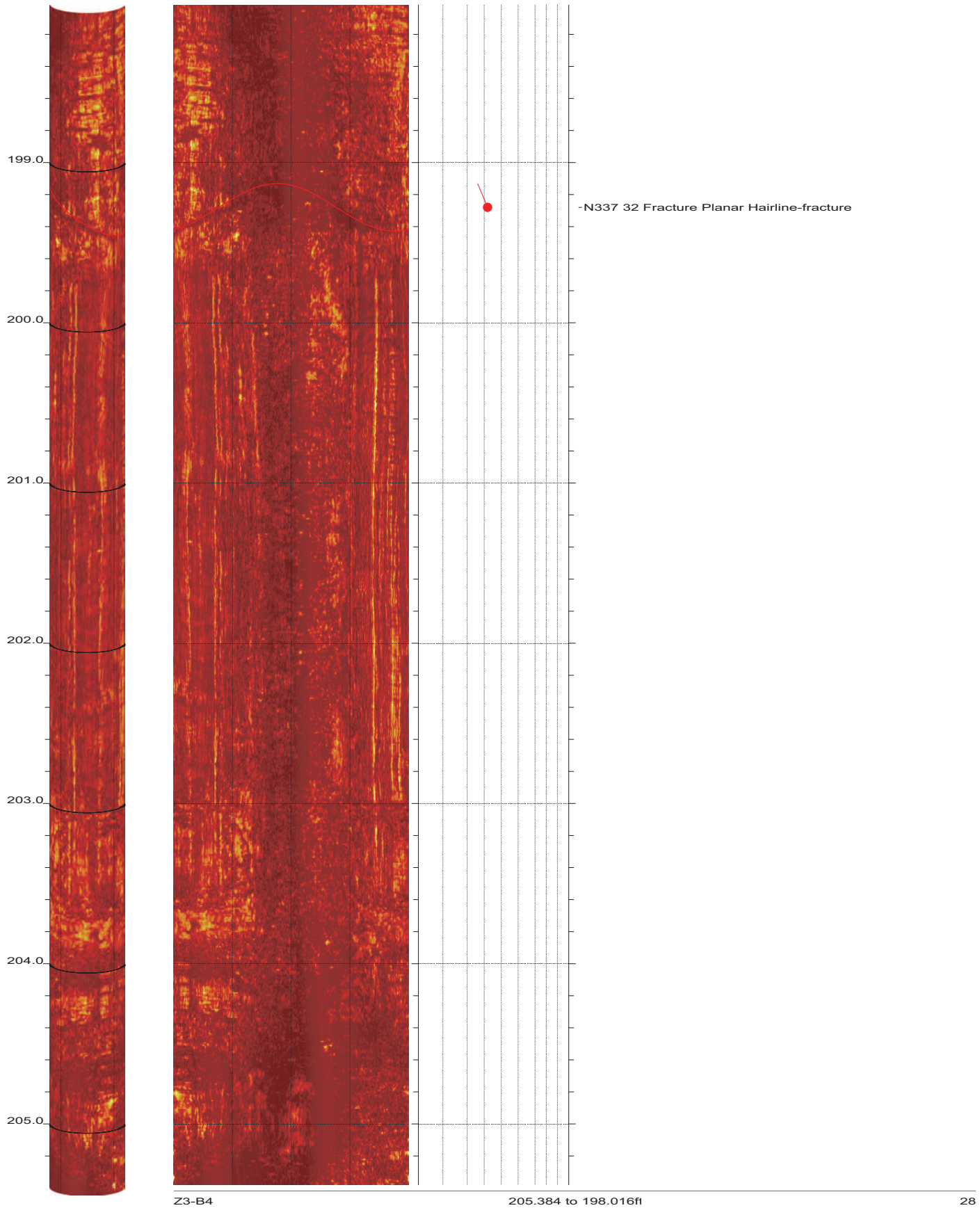


SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 26 of 38

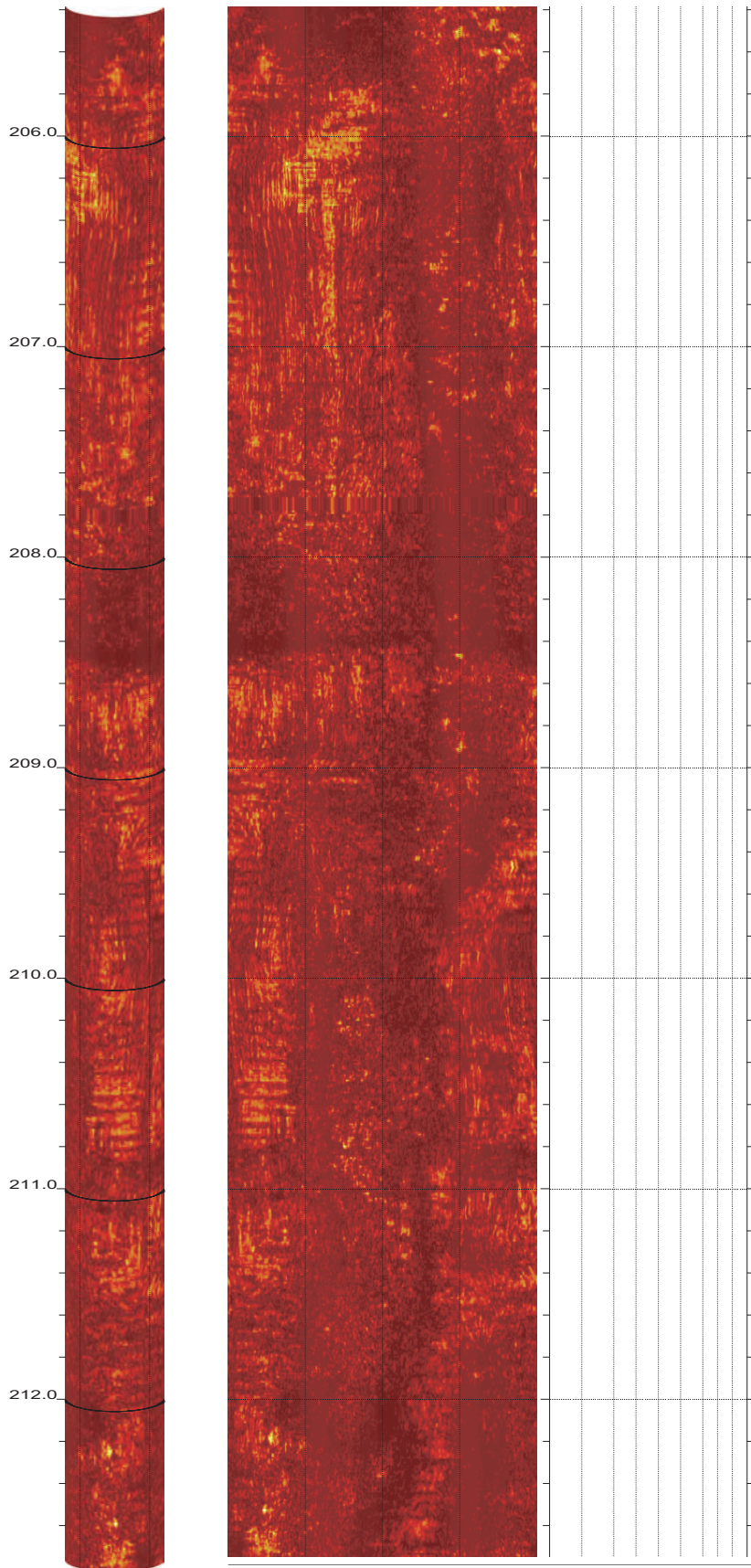




SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 27 of 38



SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 28 of 38

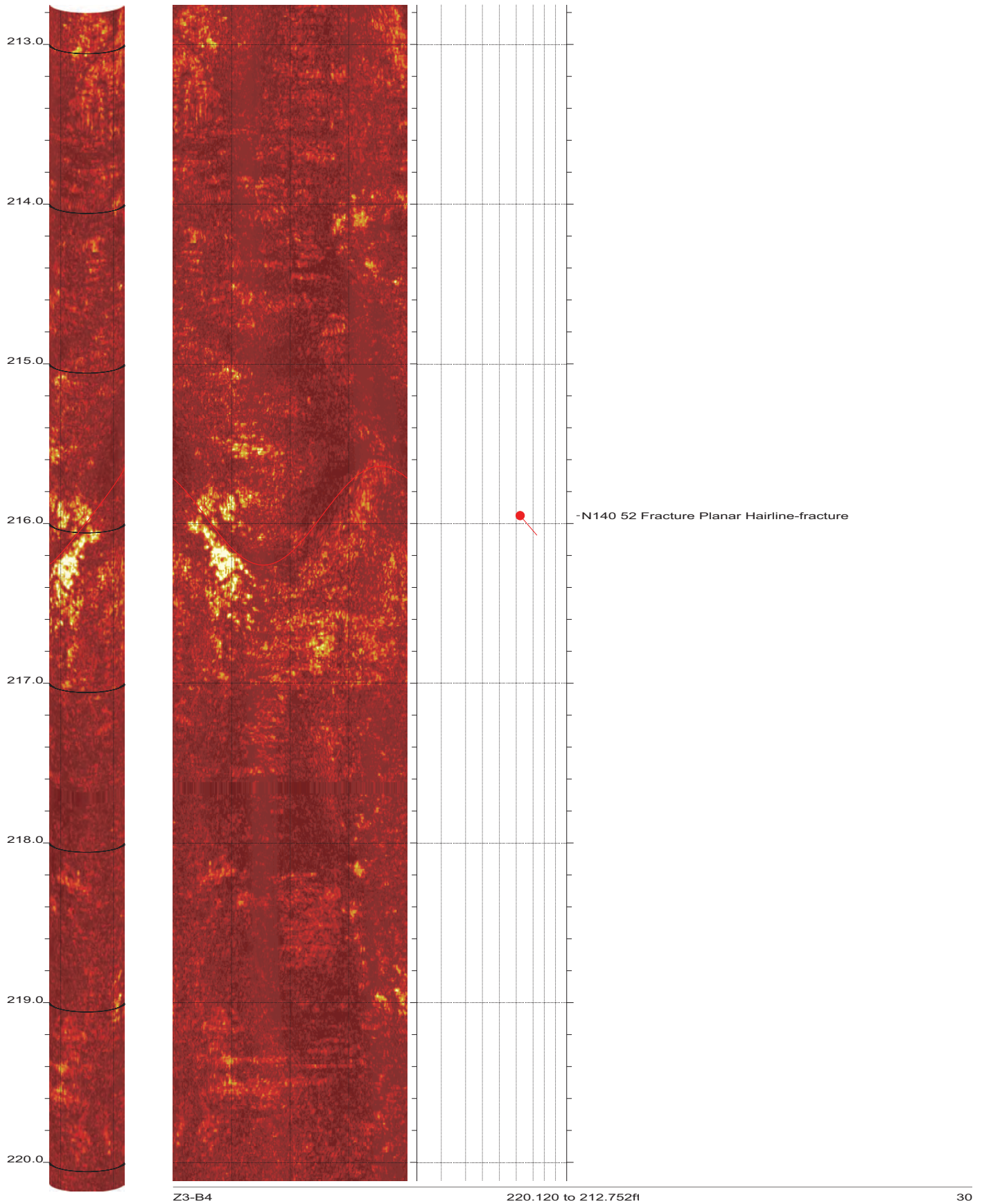


Z3-B4

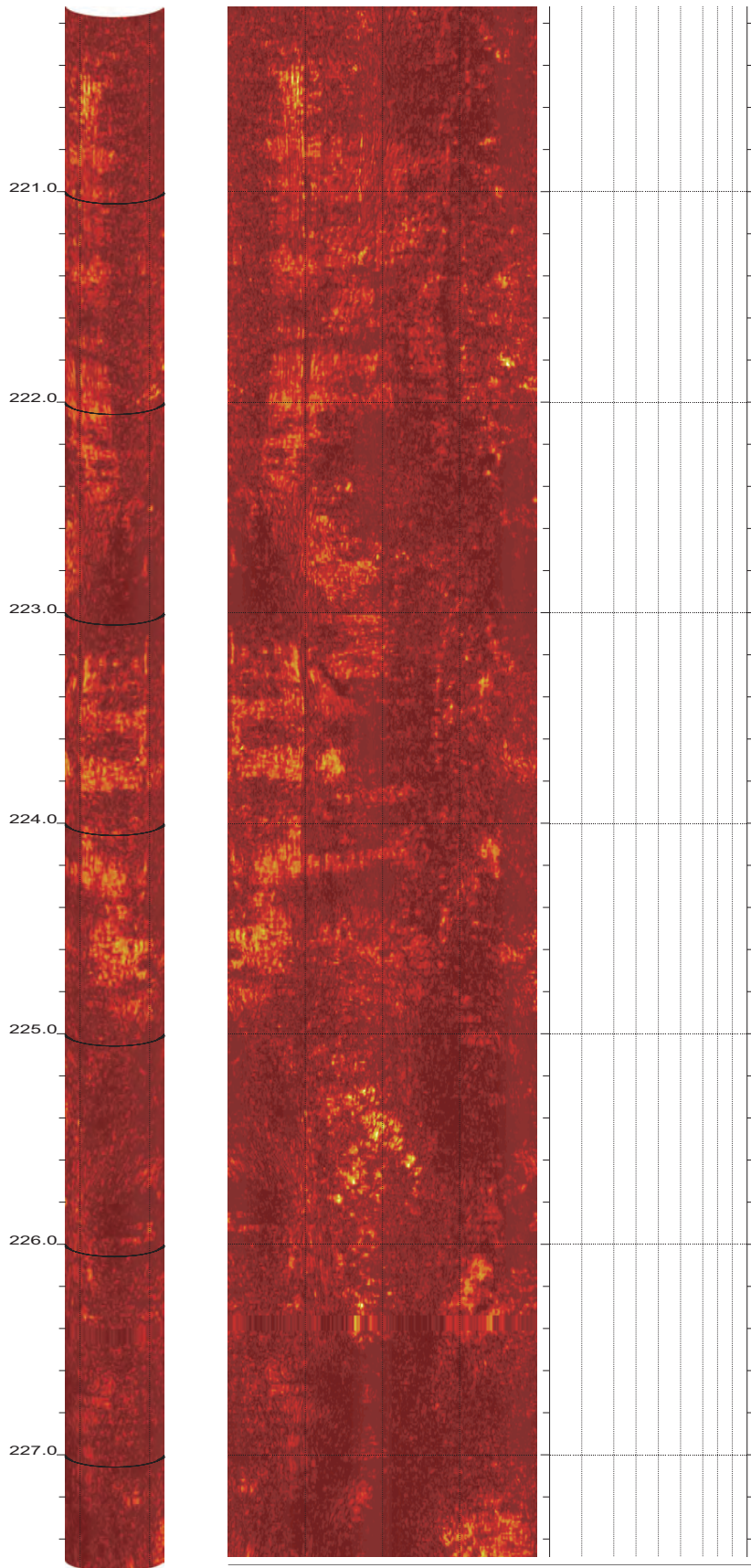
212.752 to 205.384ft

29

SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 29 of 38



SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 30 of 38

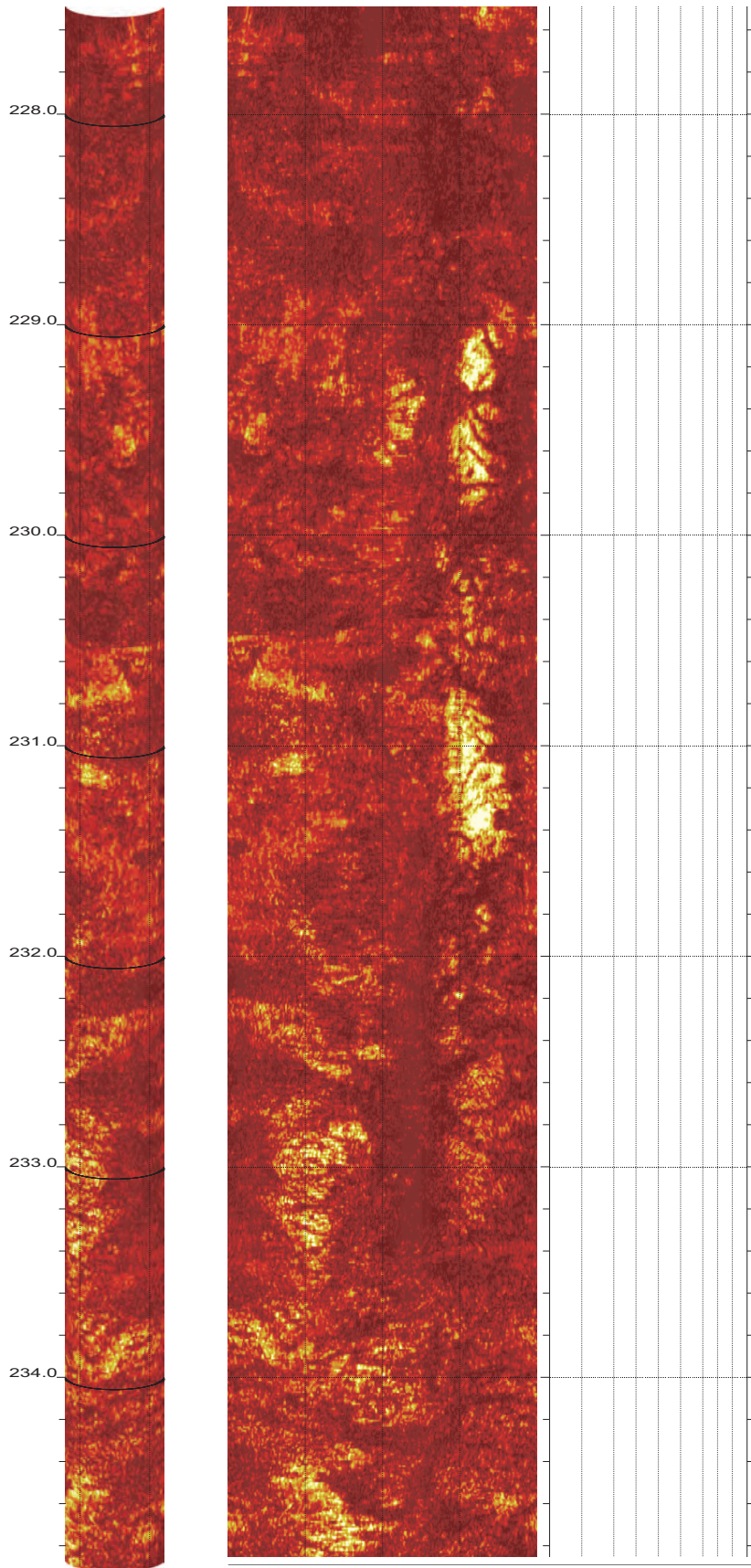


Z3-B4

227.488 to 220.120ft

31

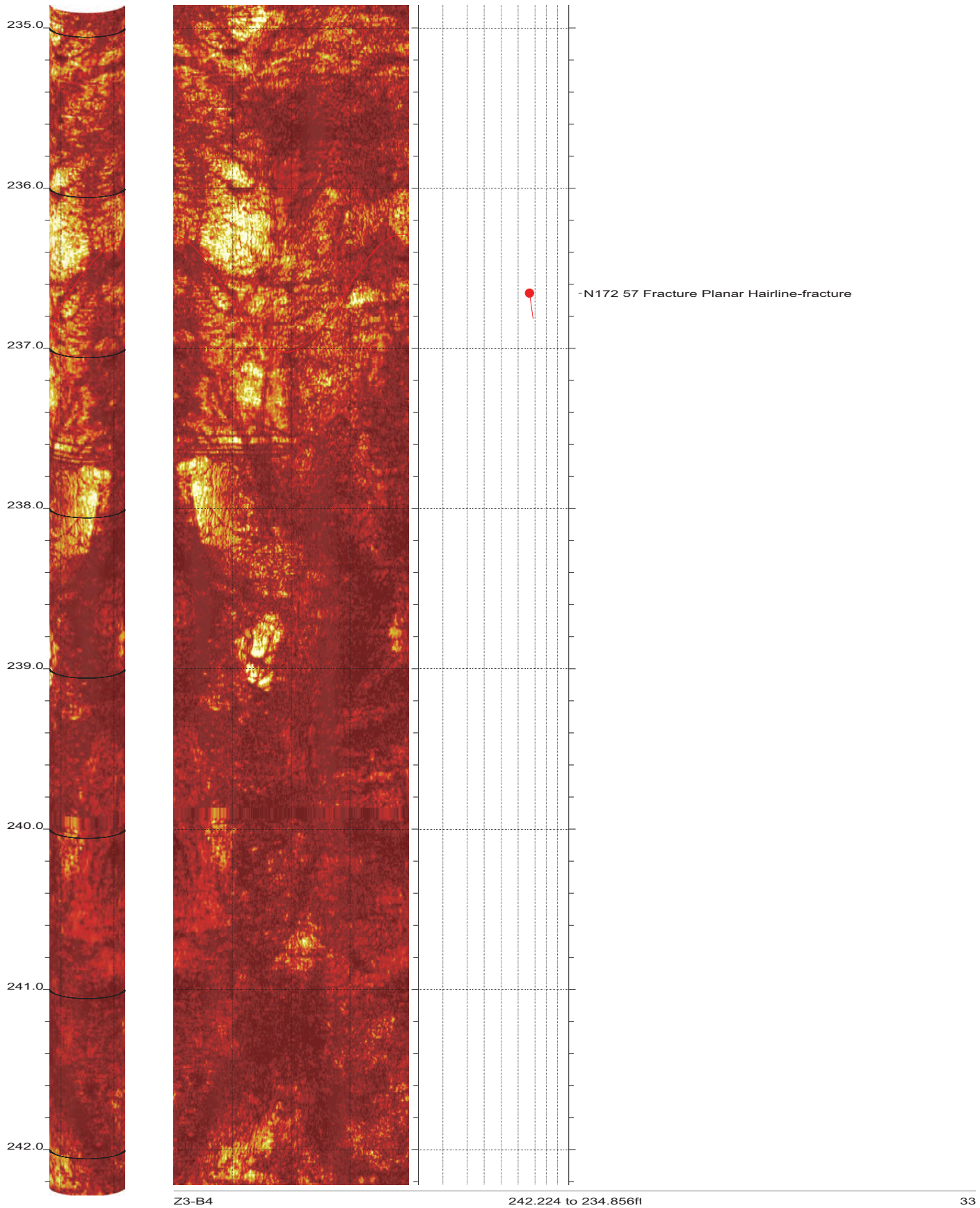
SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 31 of 38



Z3-B4

234.856 to 227.488ft

32

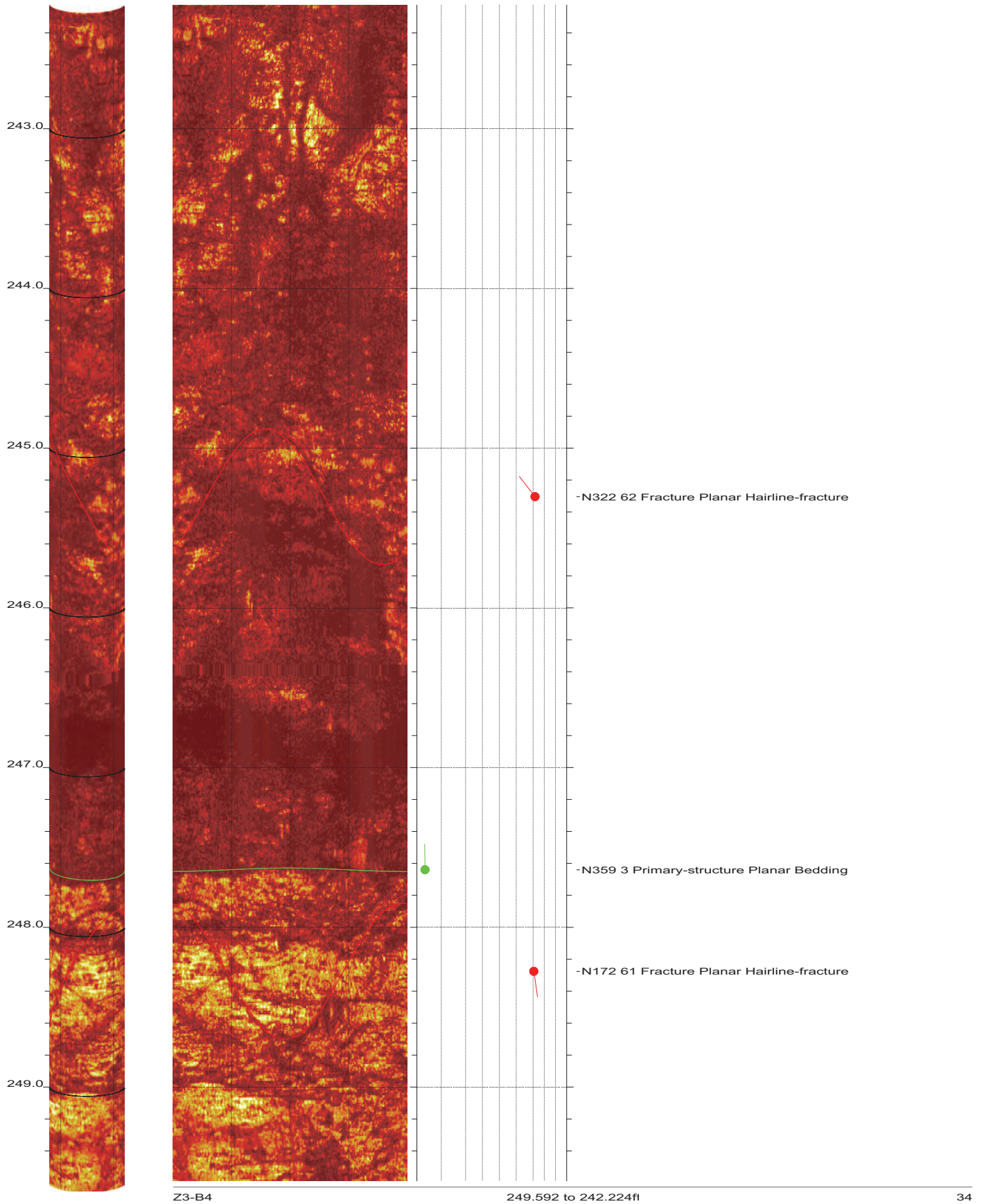


Z3-B4

242.224 to 234.856ft

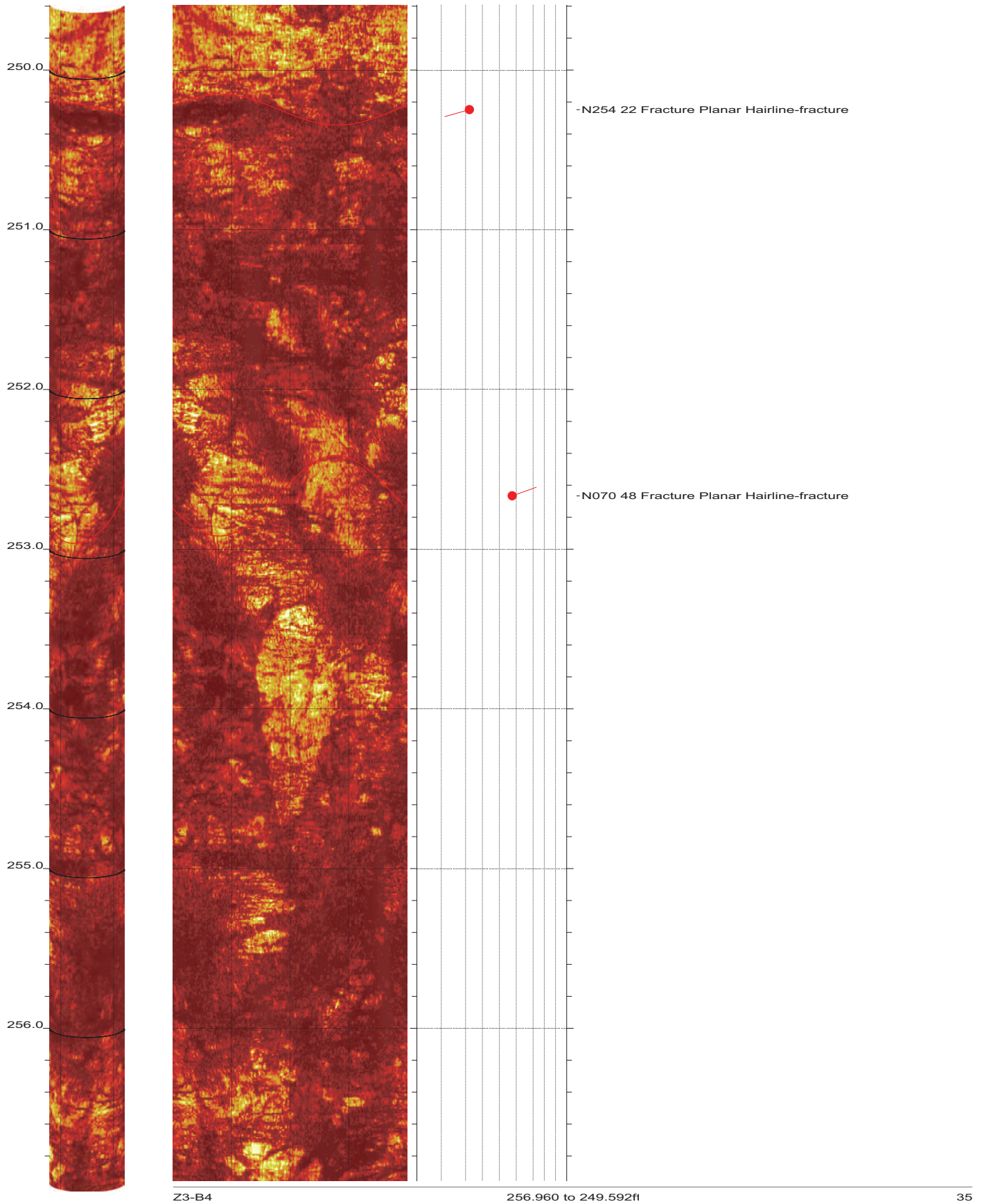
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SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 33 of 38

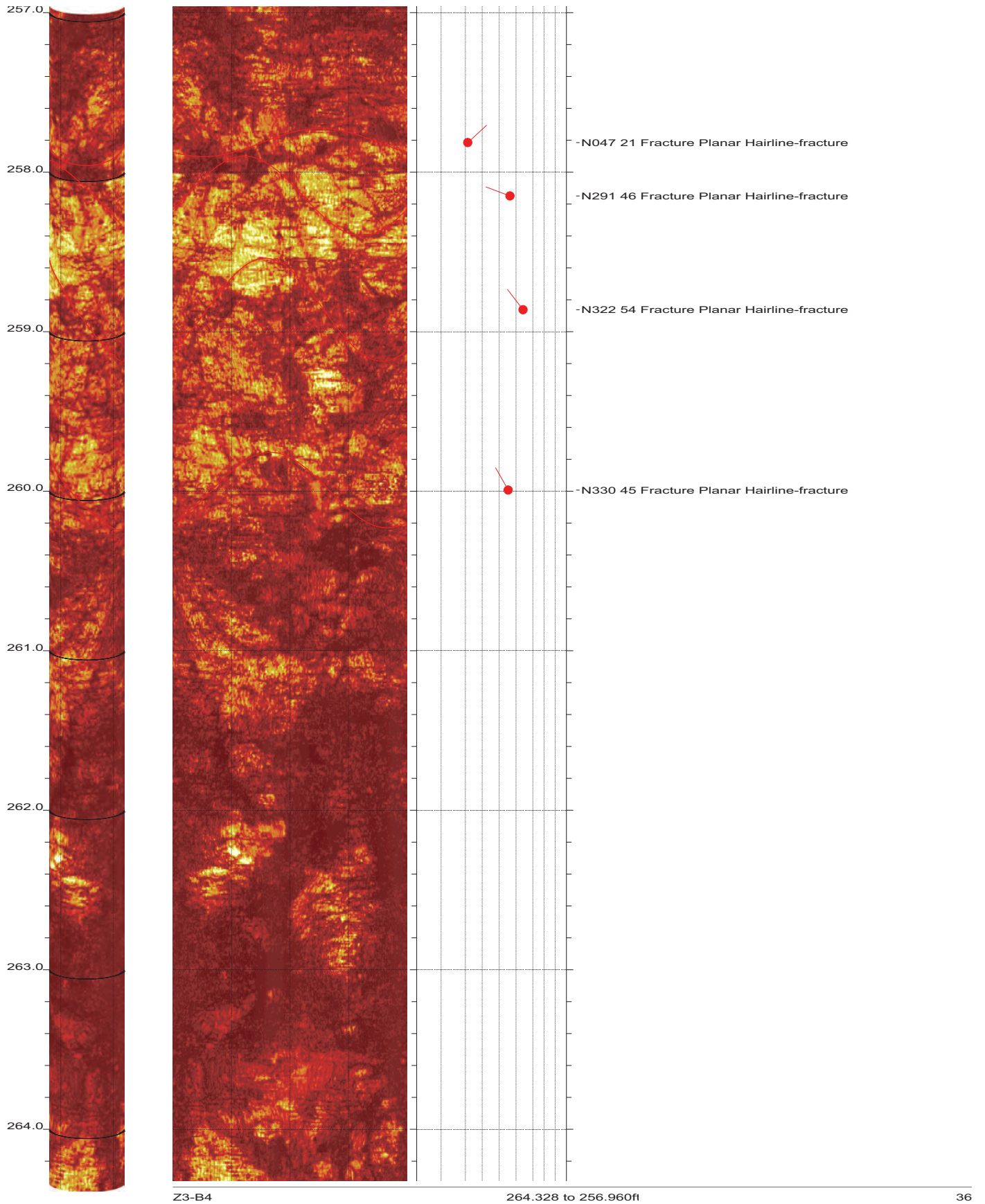


SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 34 of 38

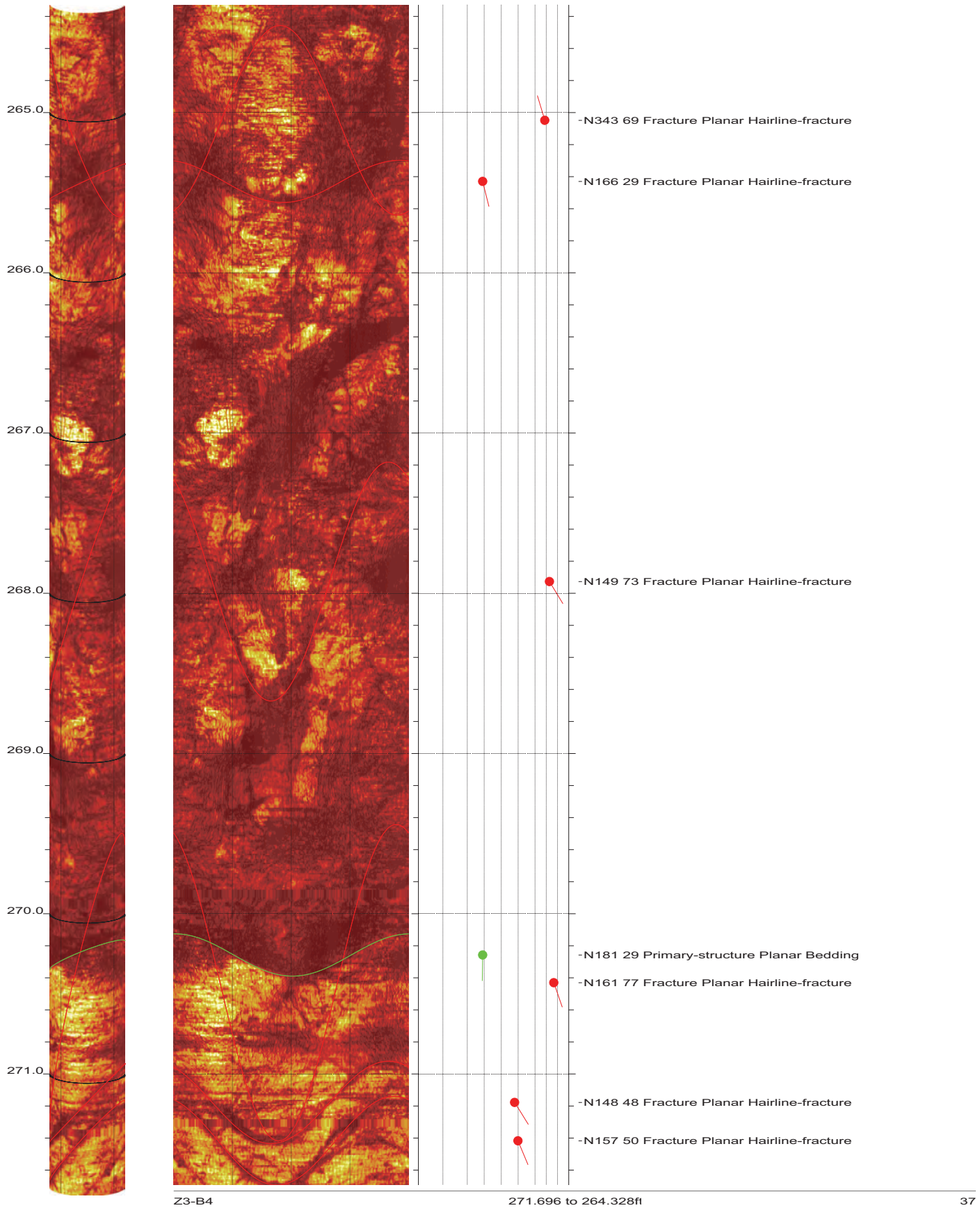




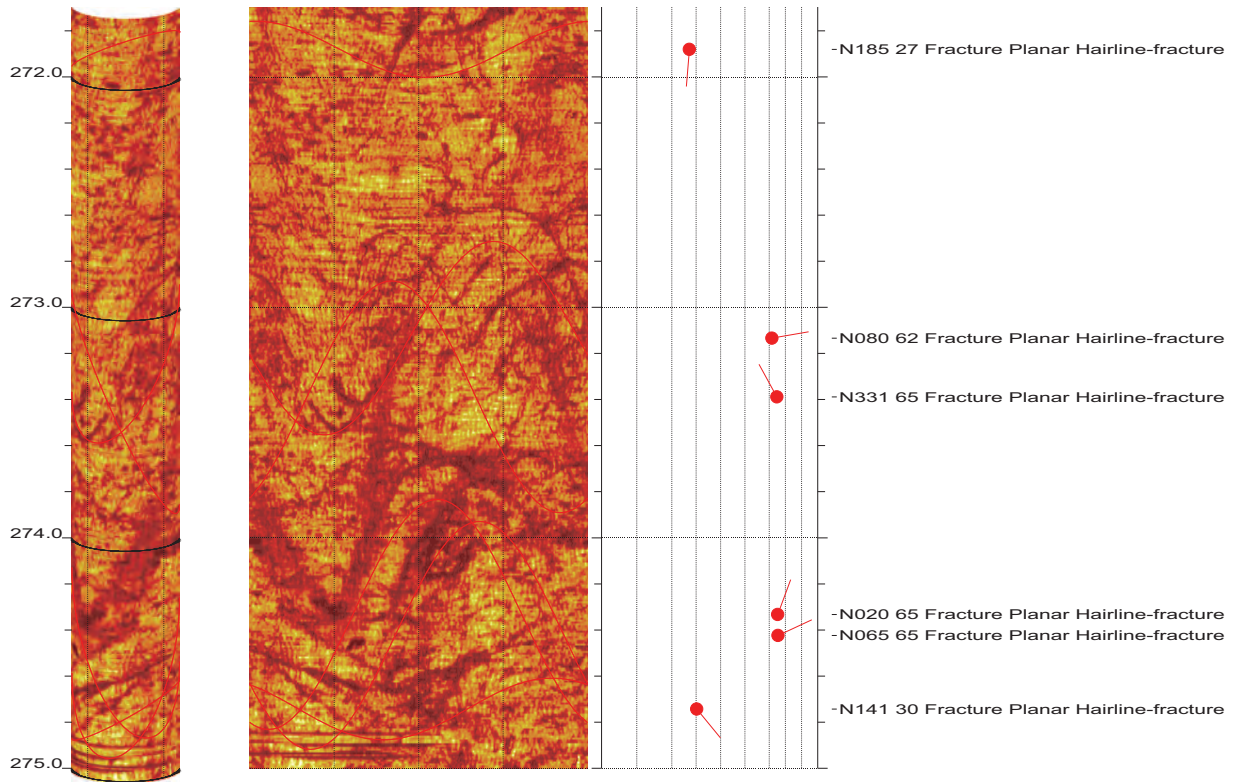
SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 35 of 38



SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 36 of 38



SR-710 Boring Z3-B4 Acoustic Televiewer Dips rev 1 Sheet 37 of 38





BHTV DATA PROCESSING  
 RGLDIP vsn 6.2  
 INTERPRETED BHTV DIPS LOG

CASCADE DRILLING

Borehole: Z3-B6

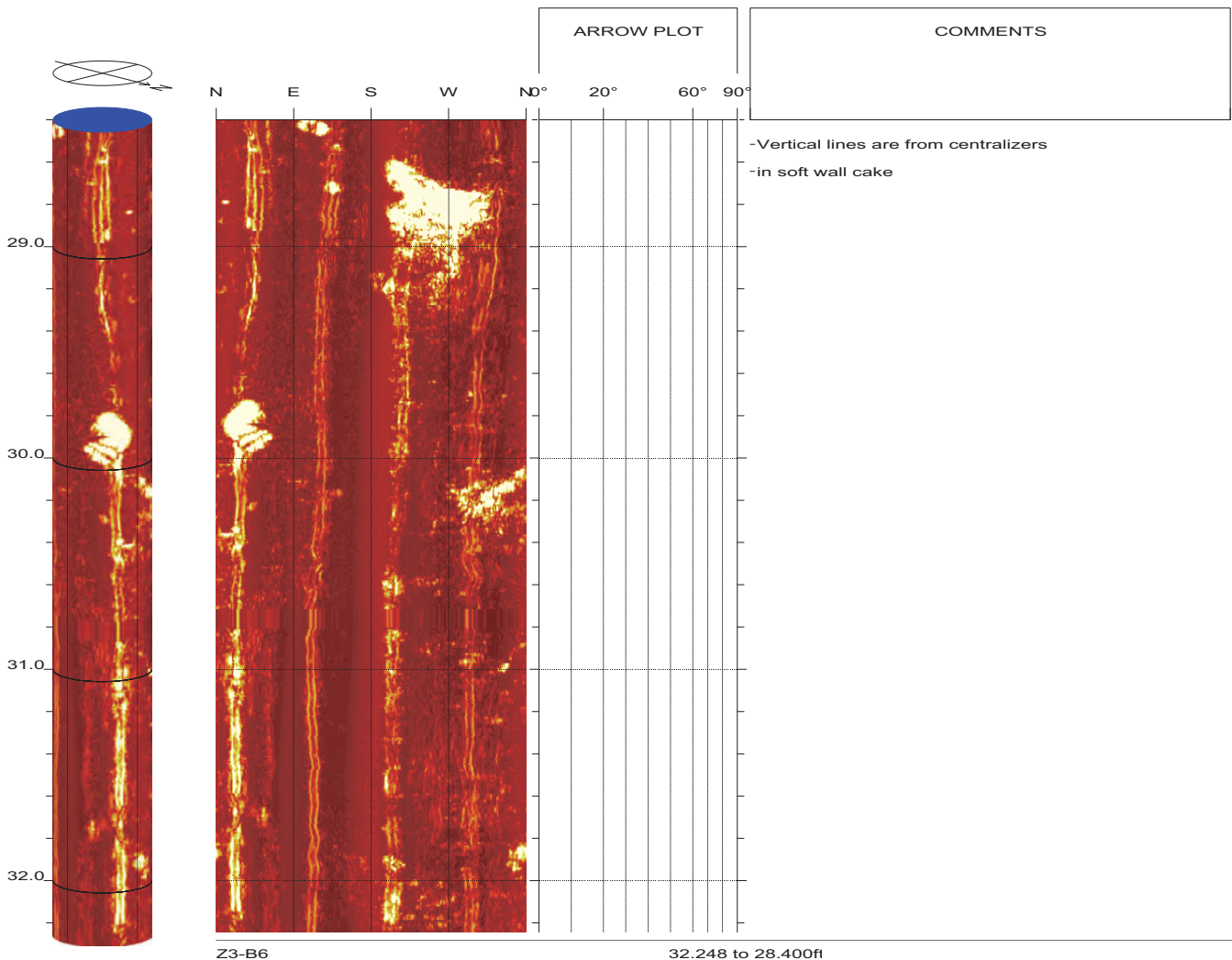
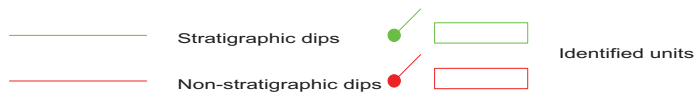
SR-710 TUNNEL INVESTIGATION

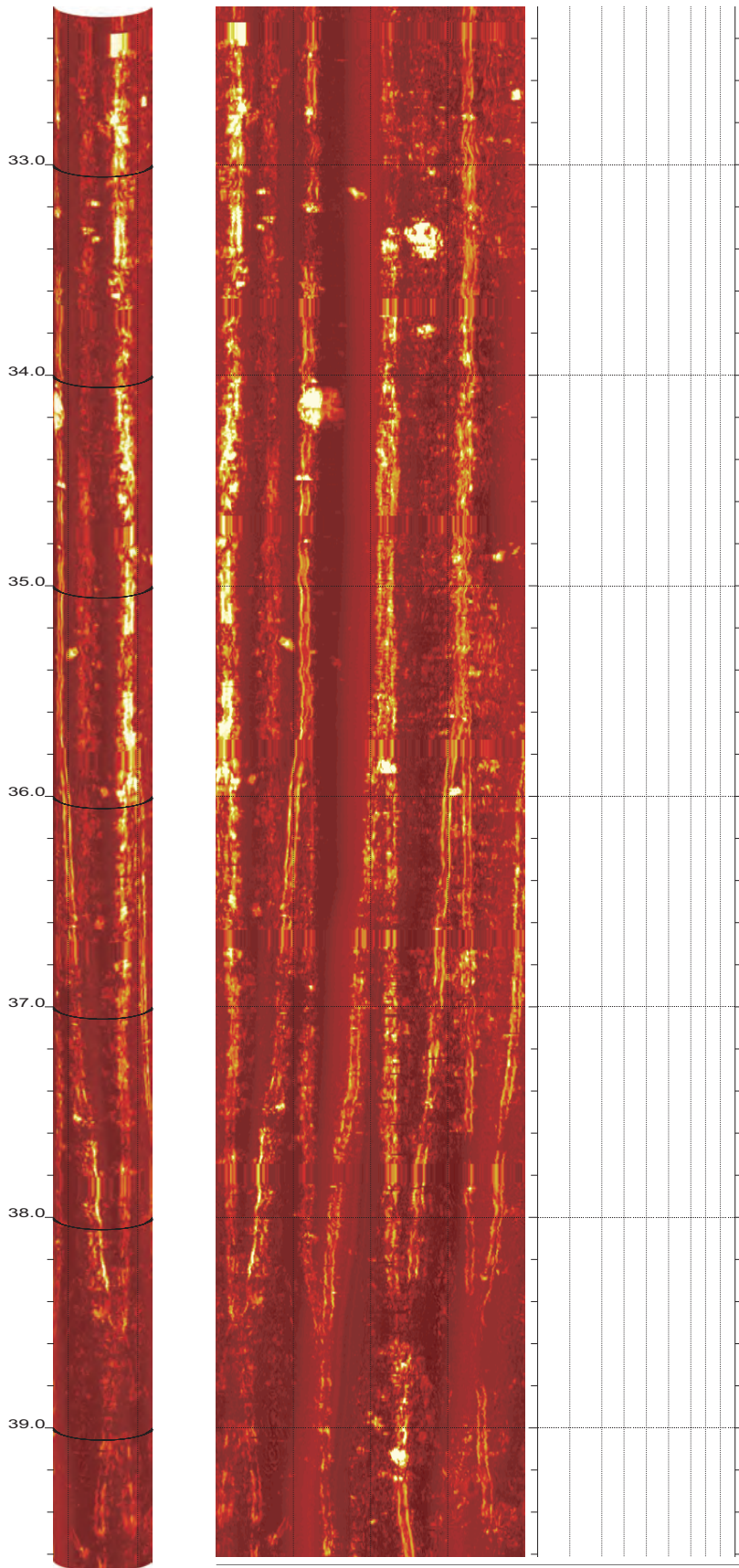
top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

Zone from 318.600 to 28.400ft  
 Format: BHTV-NESWN

Borehole diam: 5.600inch  
 Vertical = borehole-axis  
 Image: Amplitude

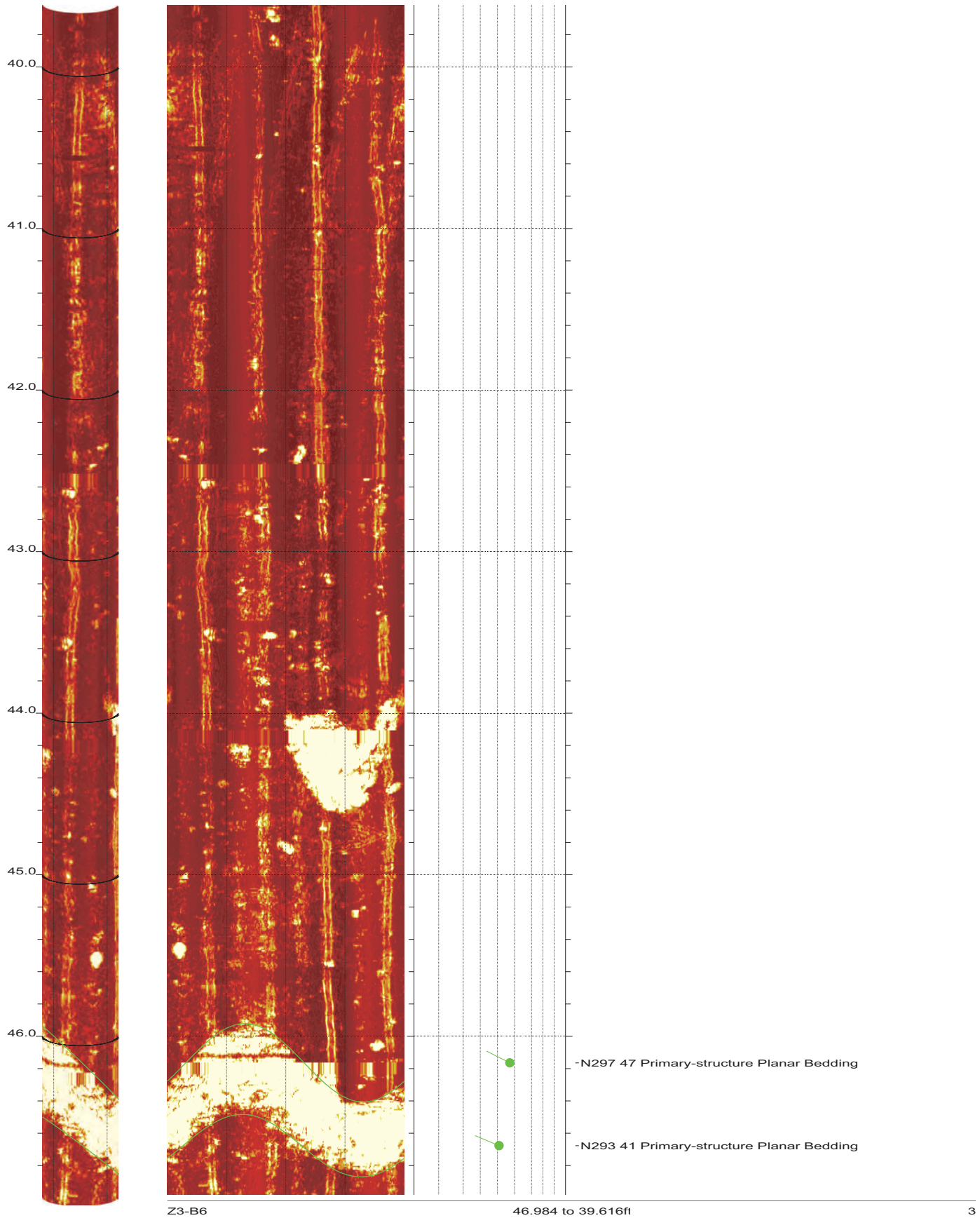




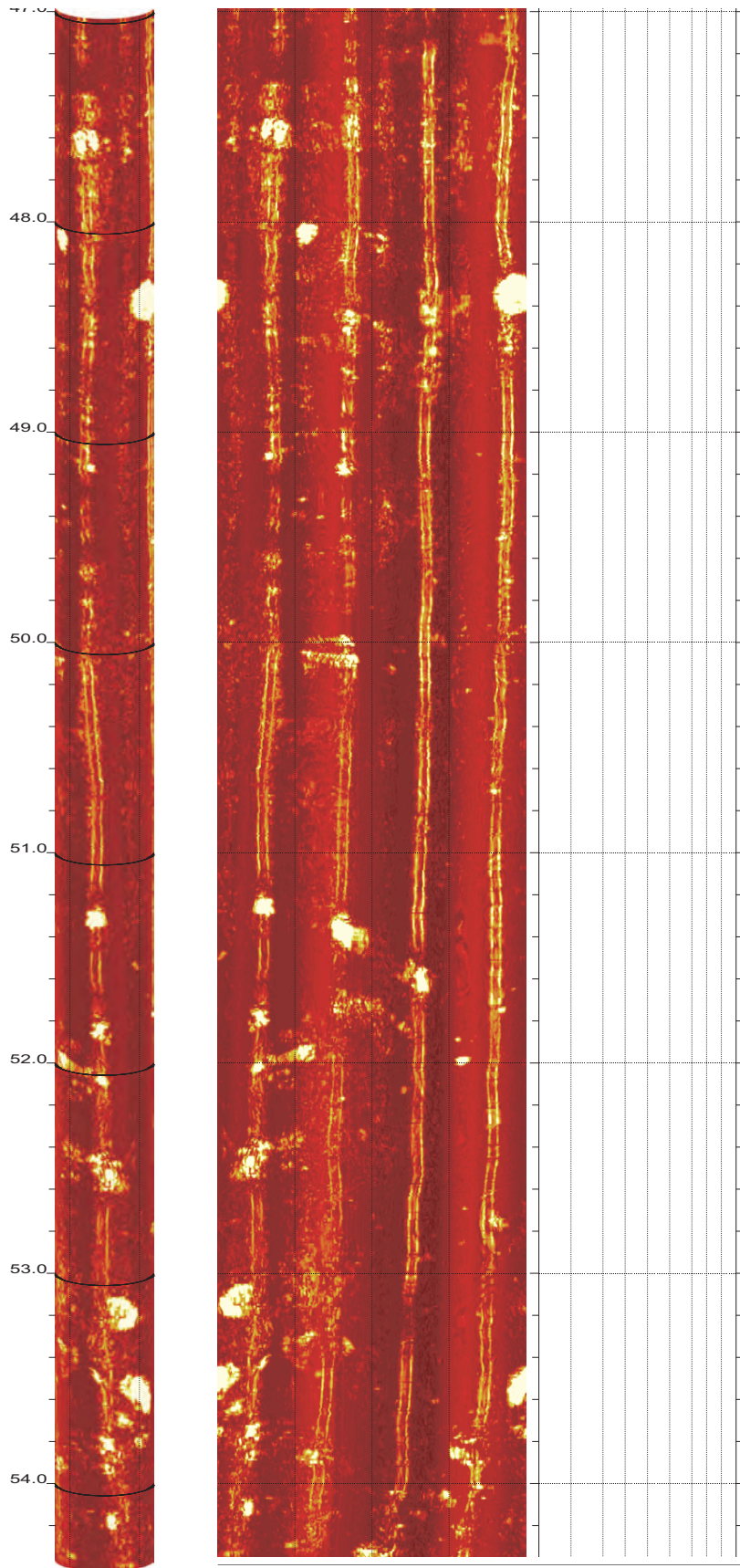
Z3-B6

39.616 to 32.248ft

2



SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 3 of 40

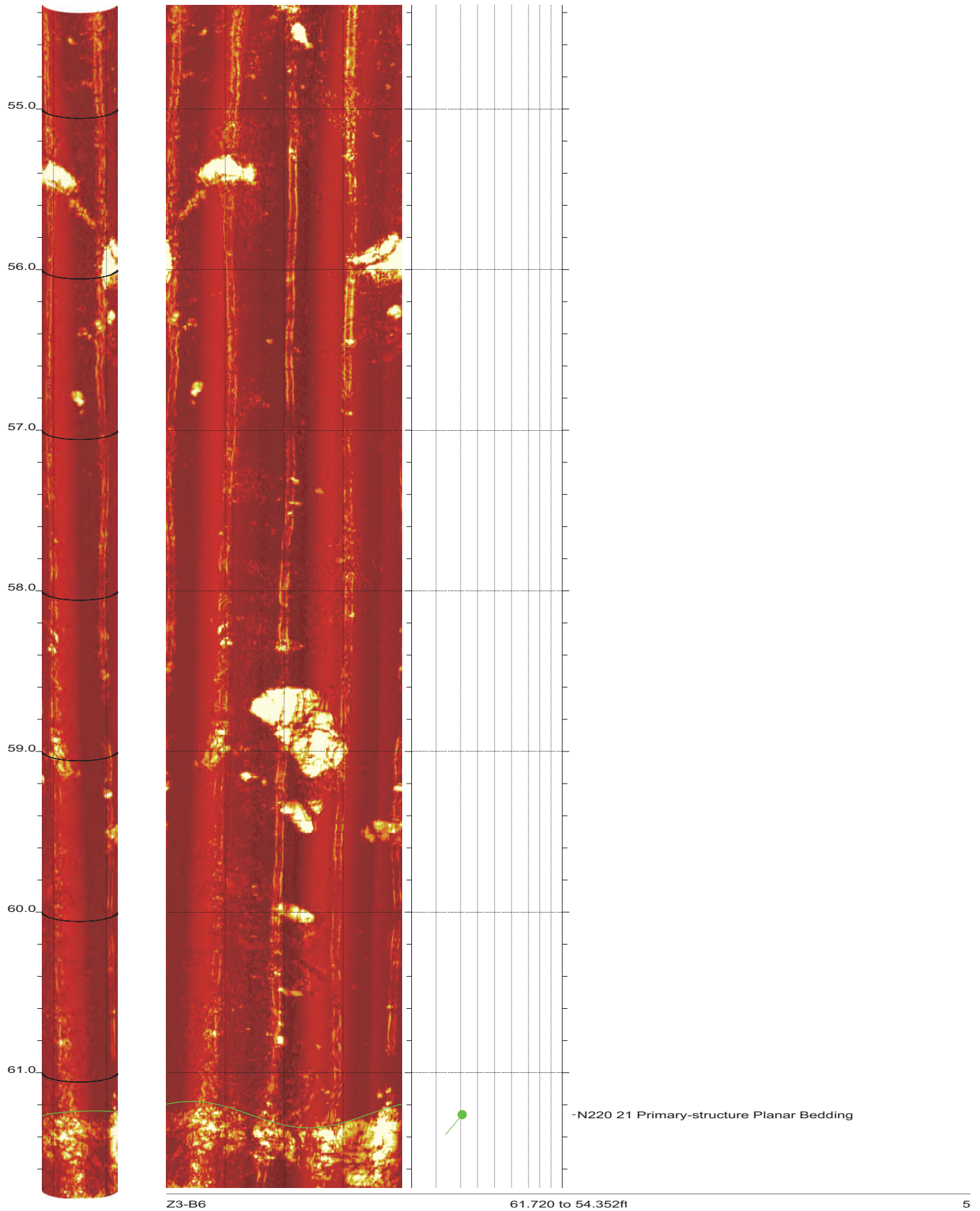


Z3-B6

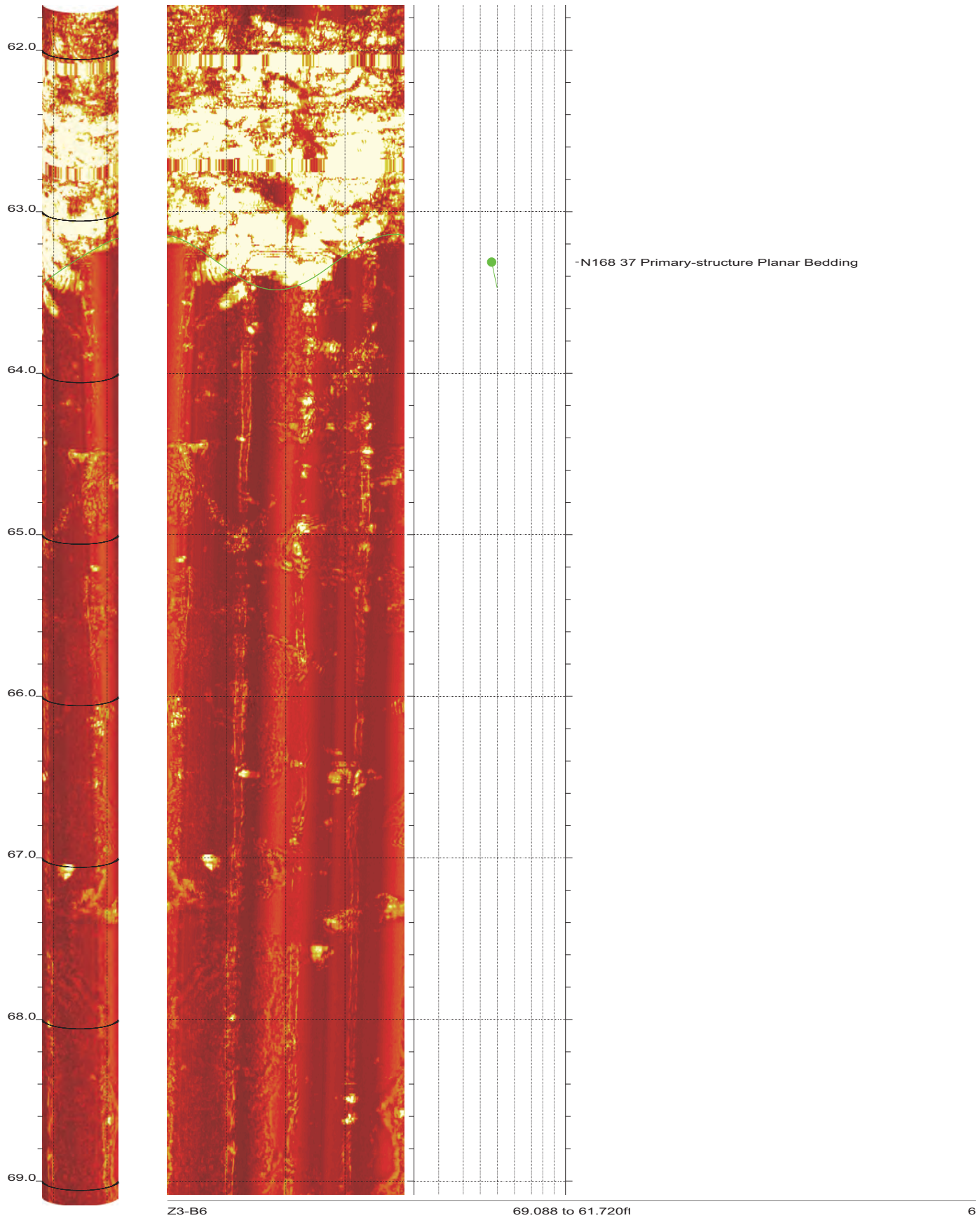
54.352 to 46.984ft

4

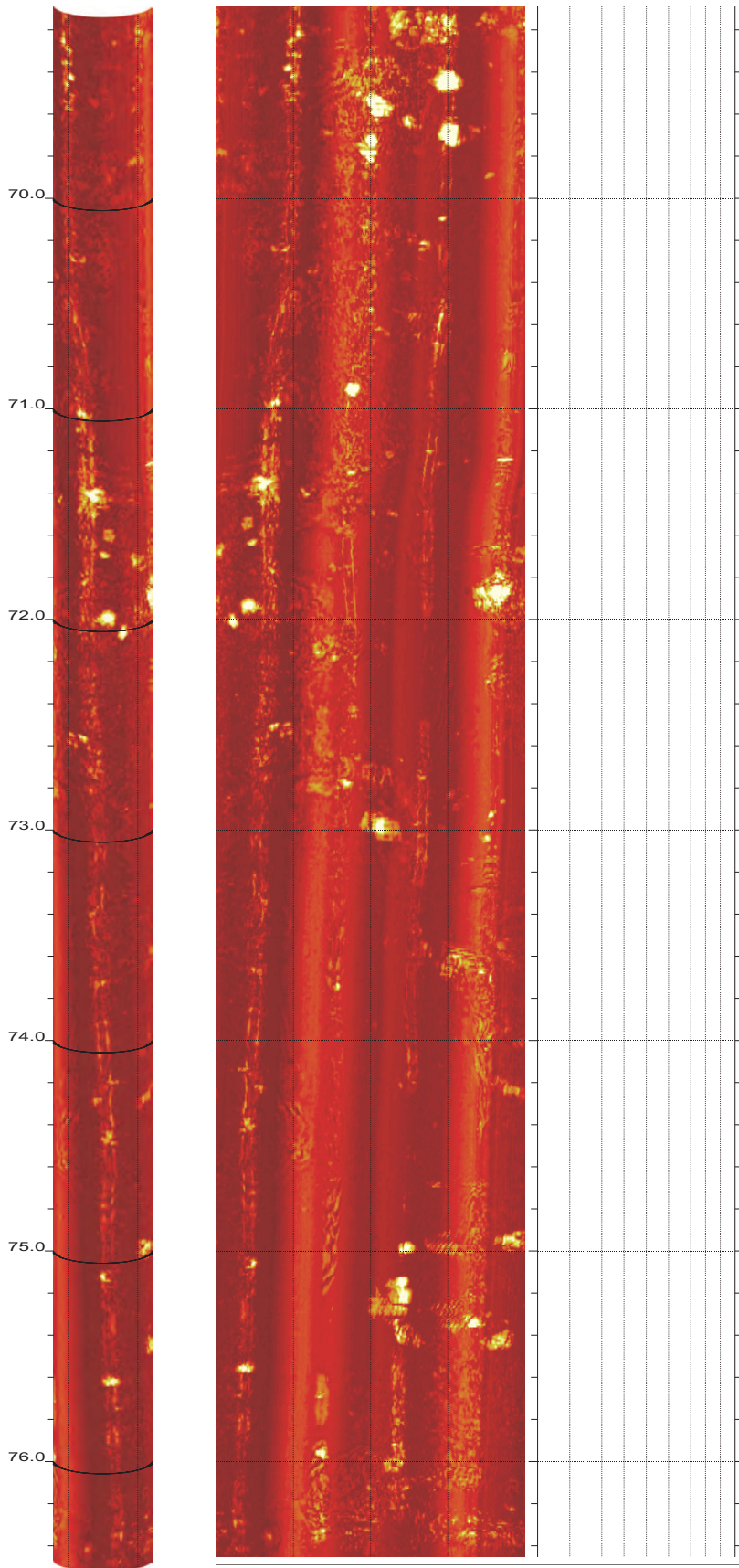




SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 5 of 40



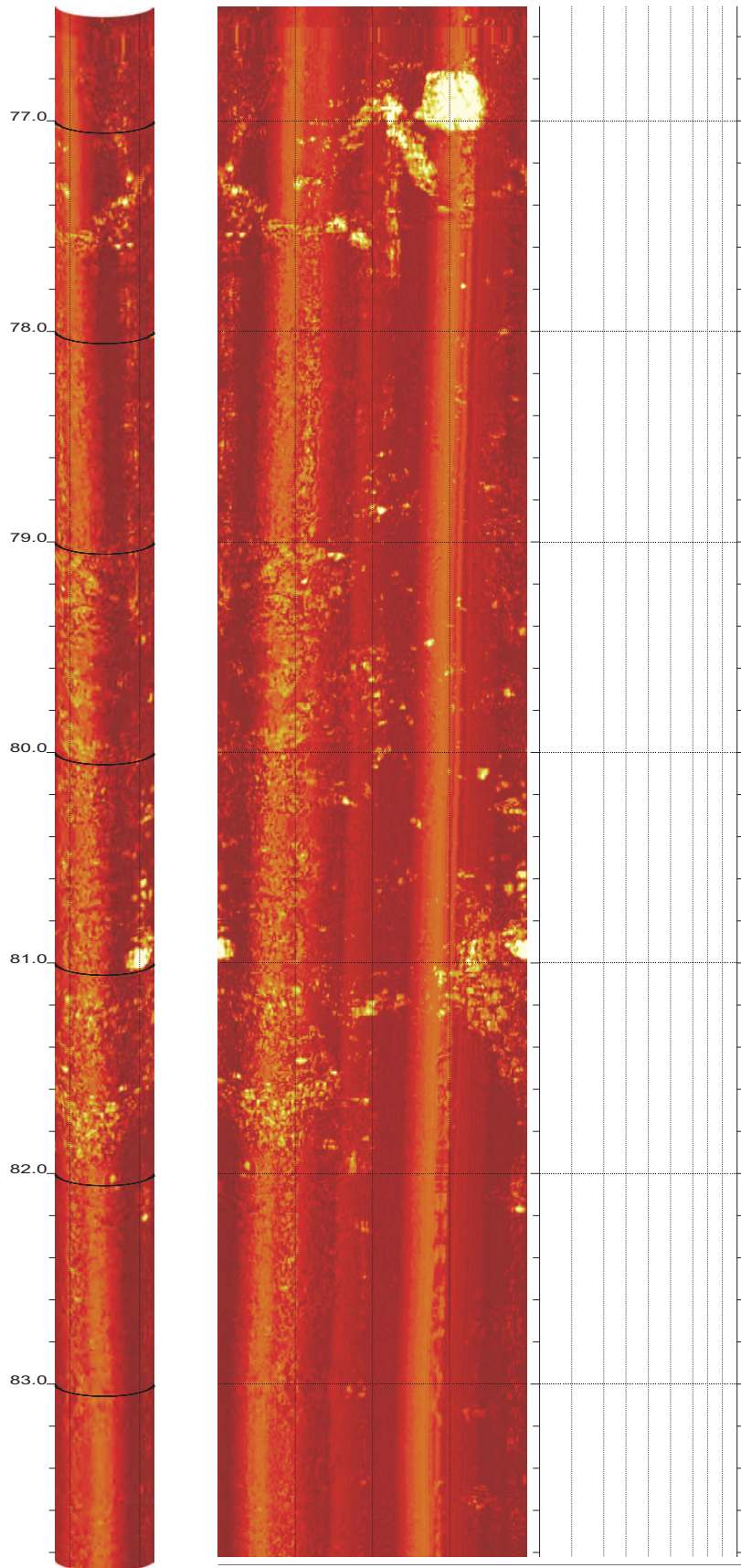
SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 6 of 40



Z3-B6

76.456 to 69.088ft

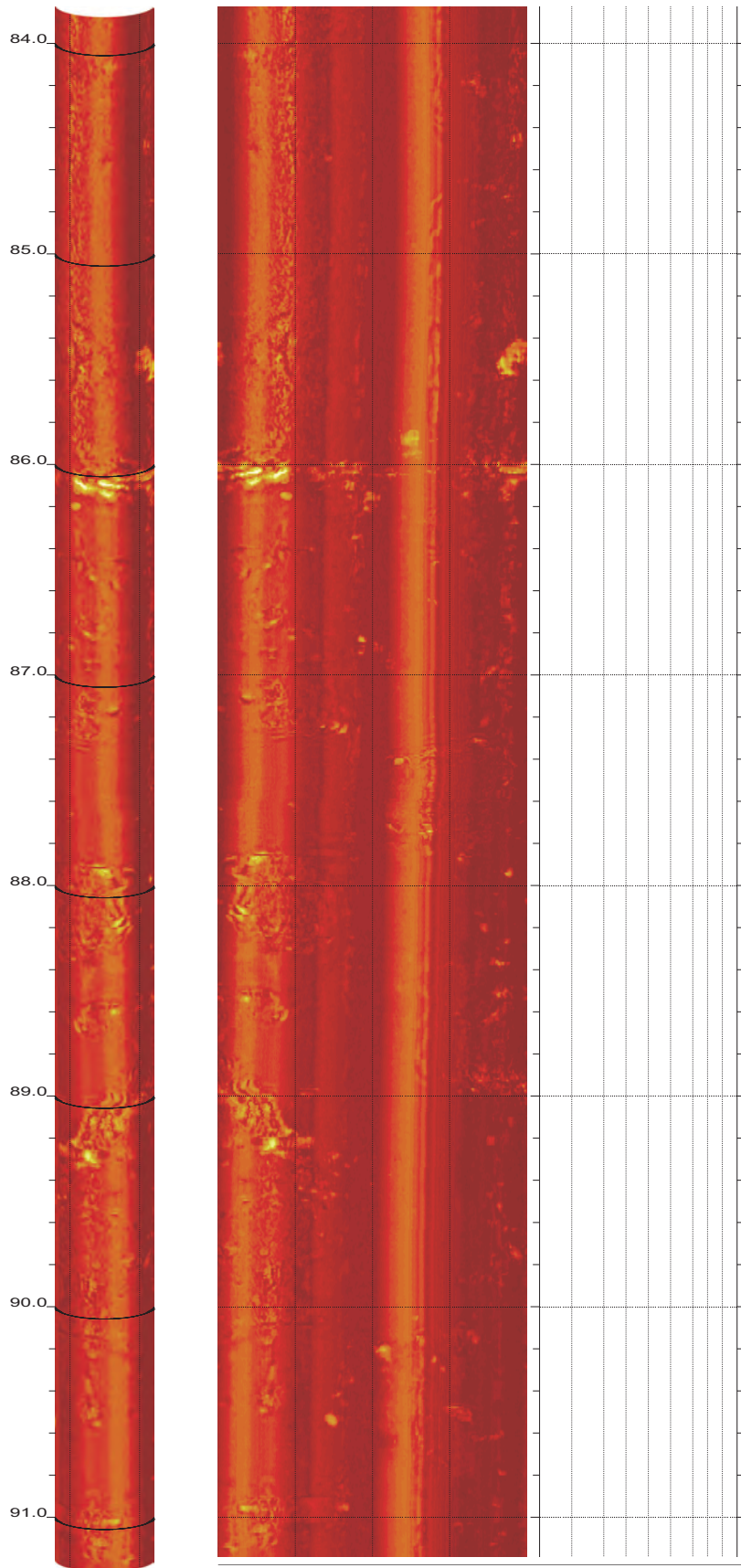
7



Z3-B6

83.824 to 76.456ft

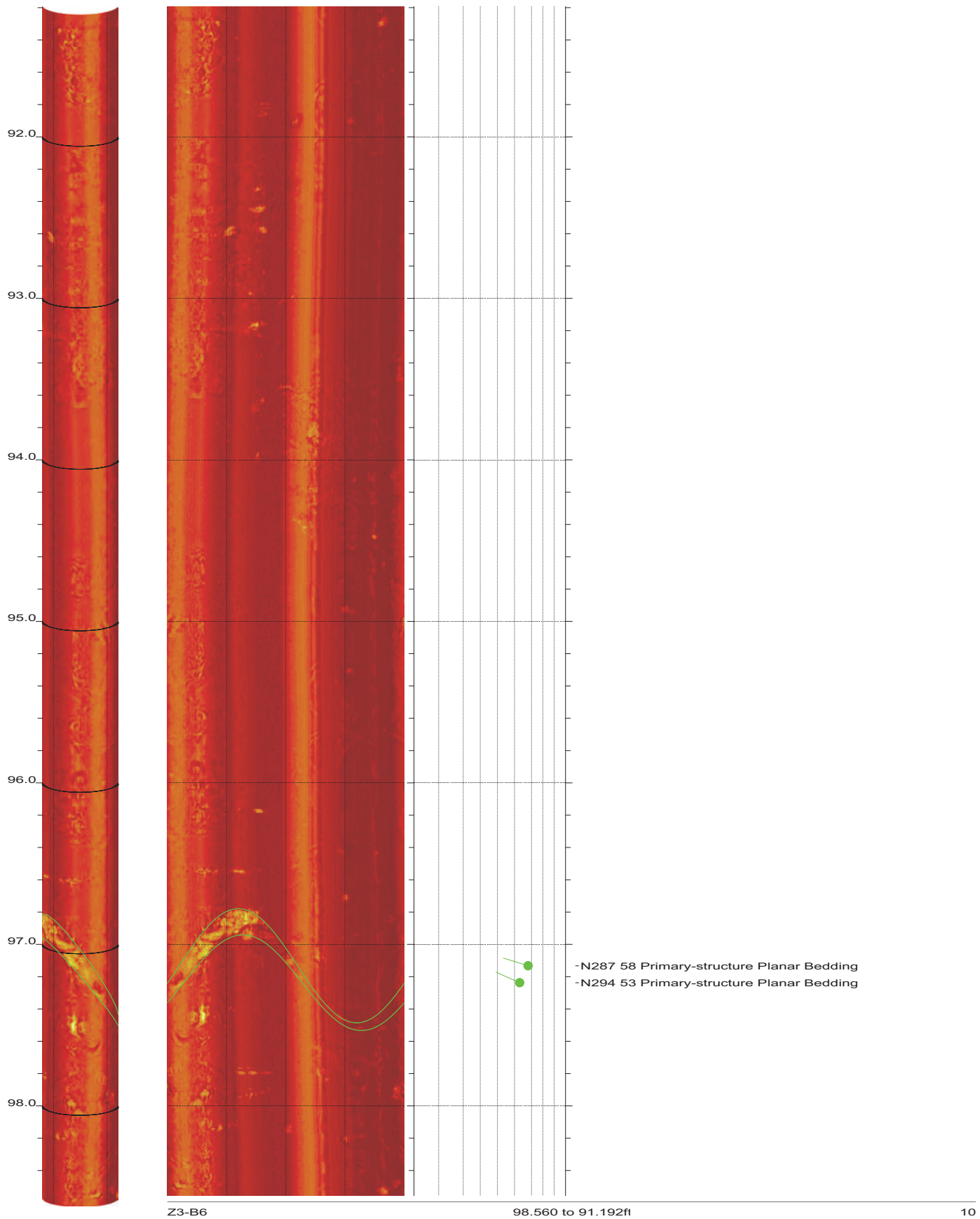
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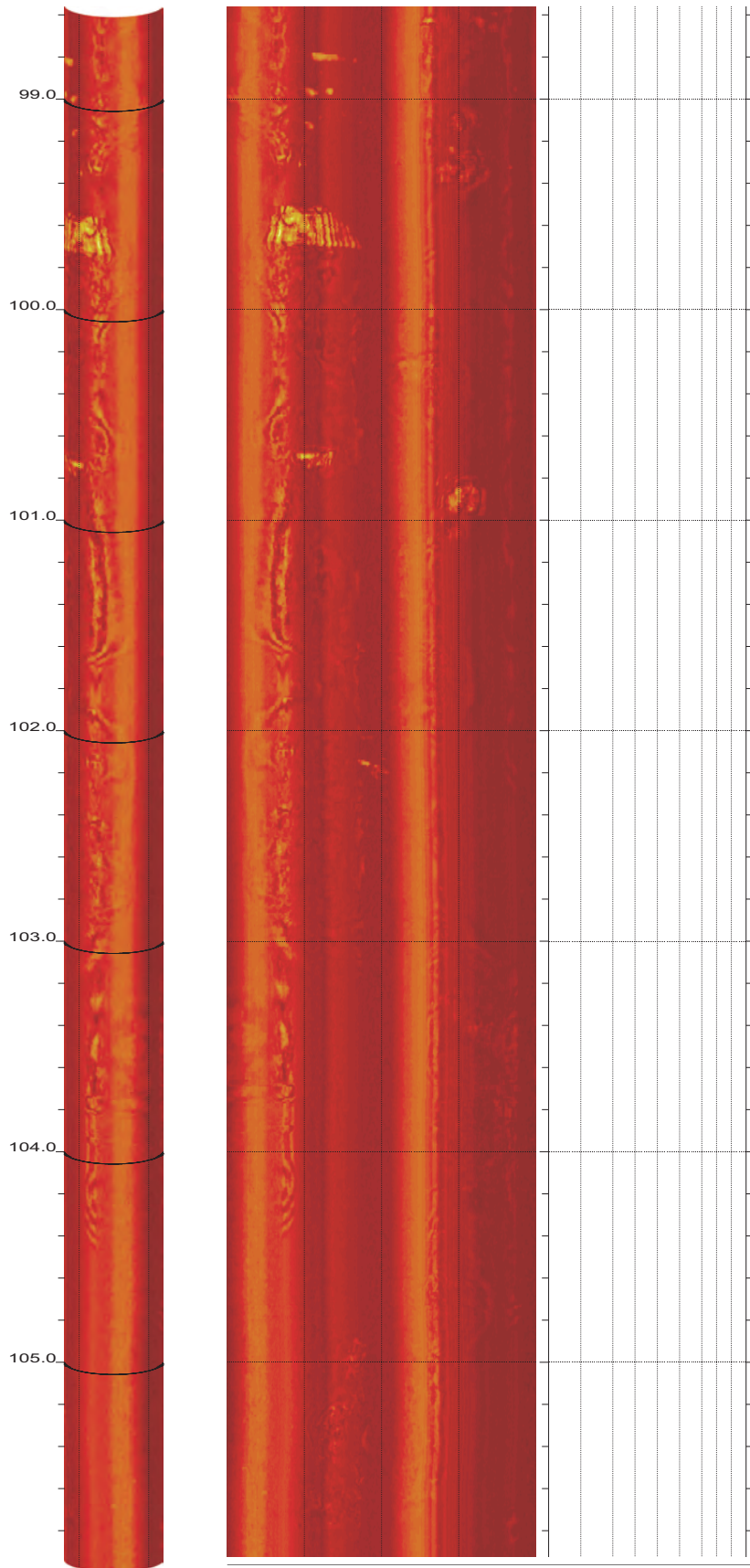
Z3-B6

91.192 to 83.824ft

9



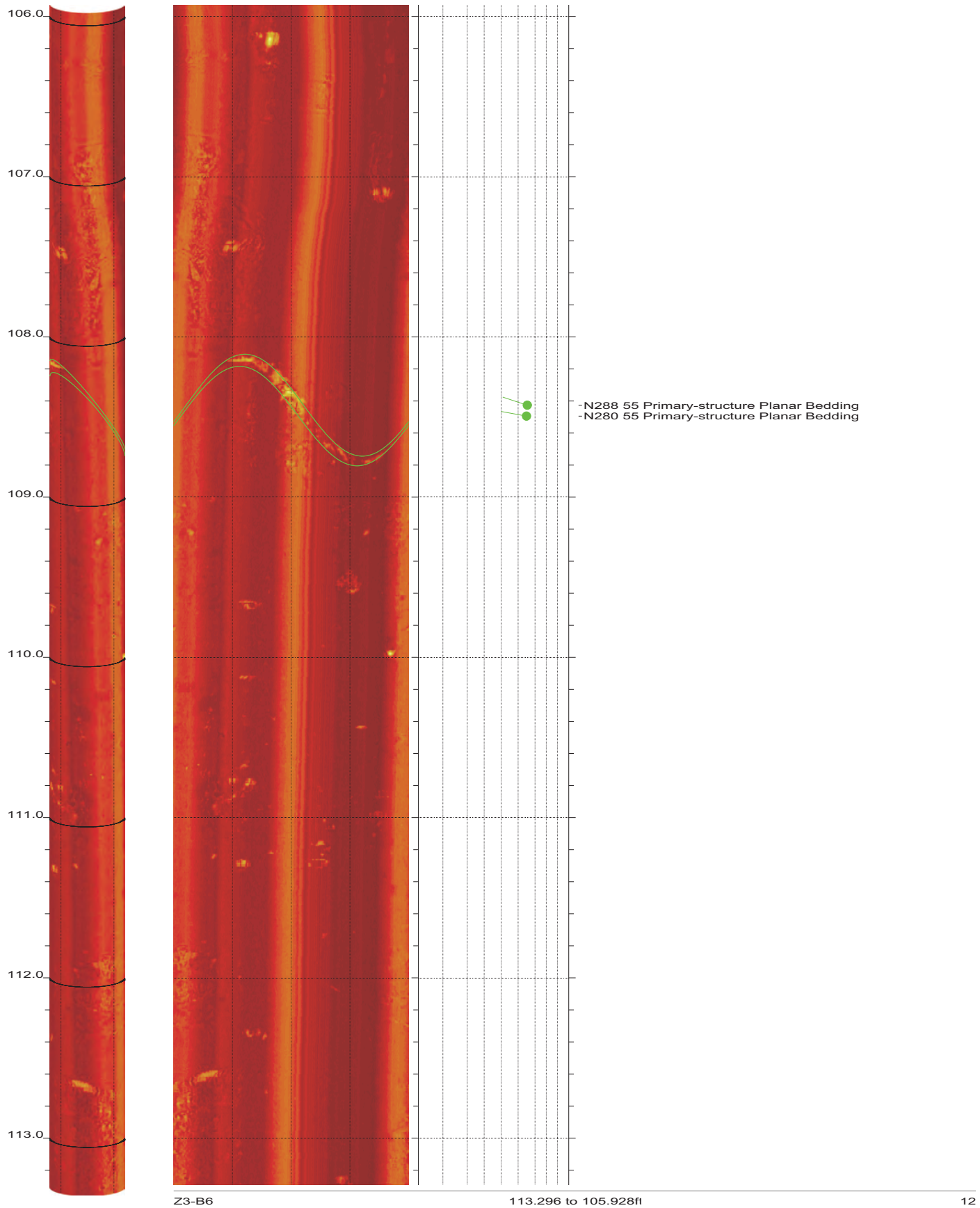
SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 10 of 40



Z3-B6

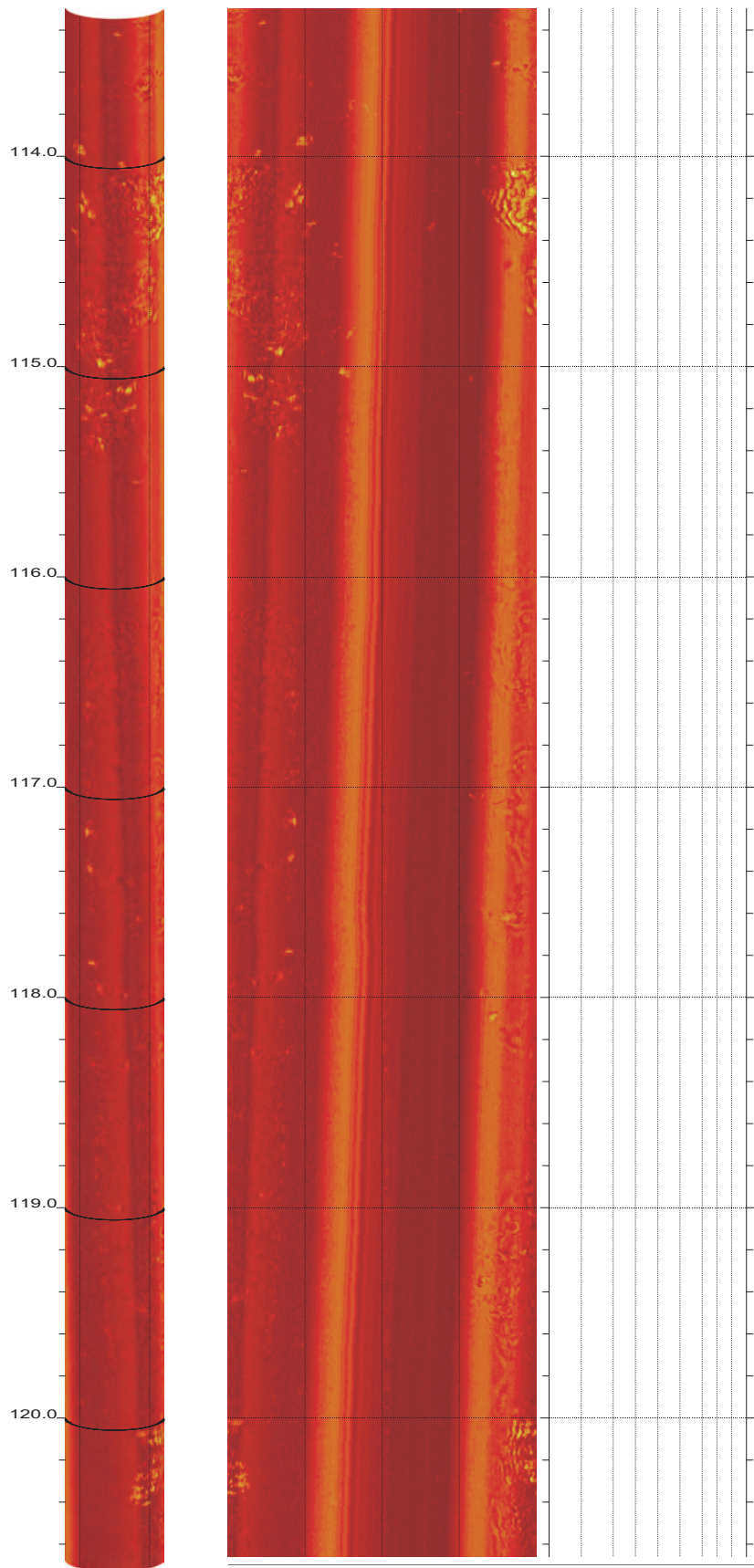
105.928 to 98.560ft

11



SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 12 of 40



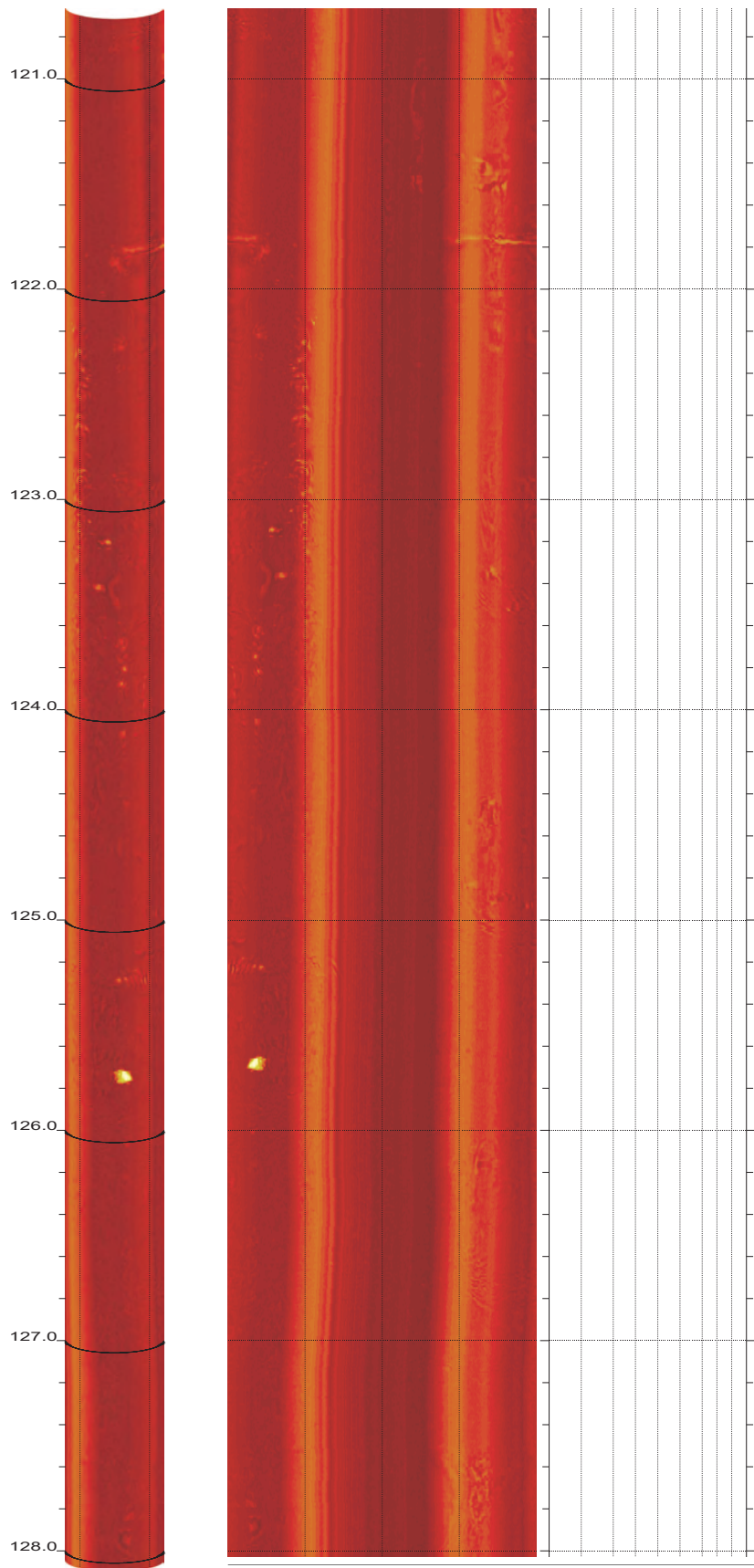


Z3-B6

120.664 to 113.296ft

13

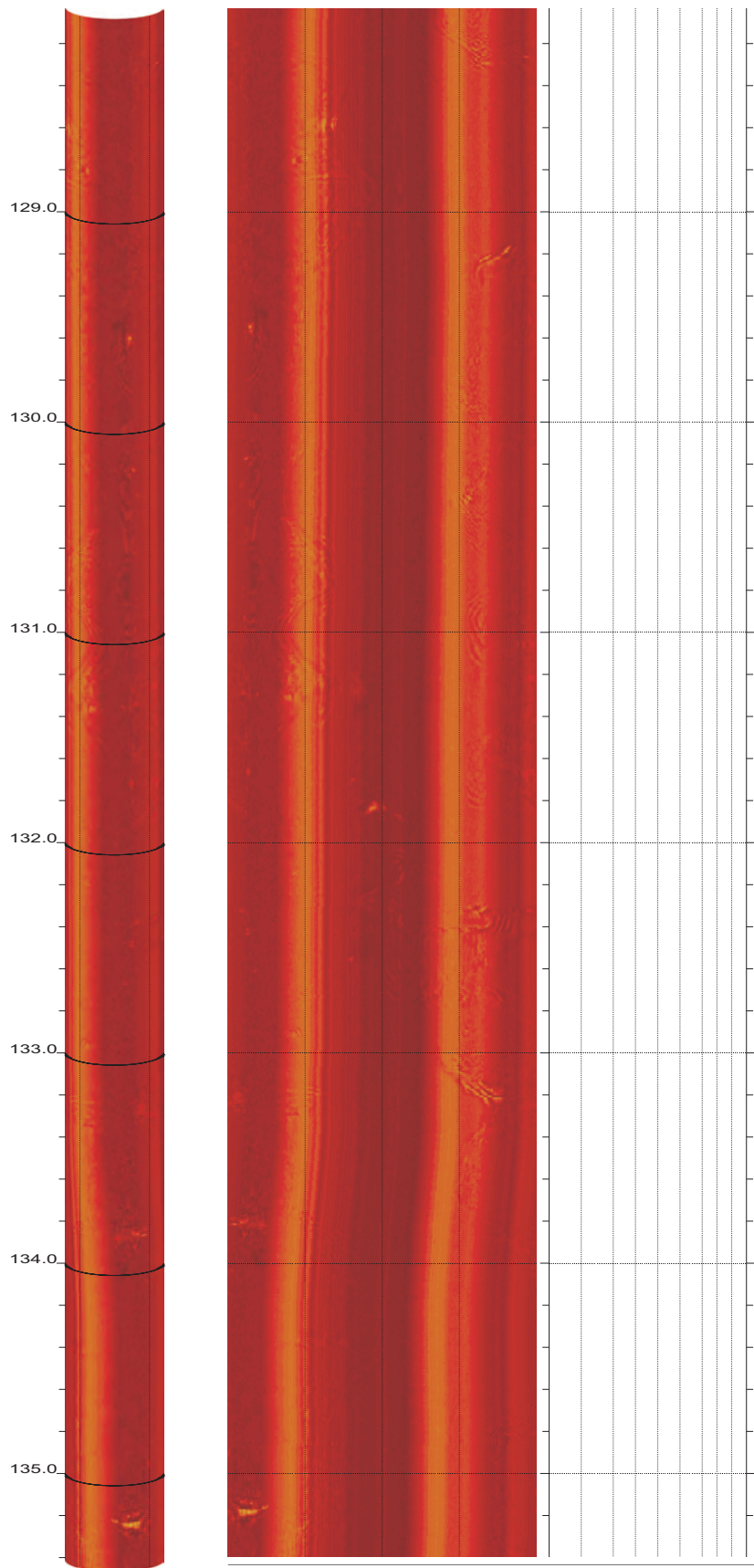
SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 13 of 40



Z3-B6

128.032 to 120.664ft

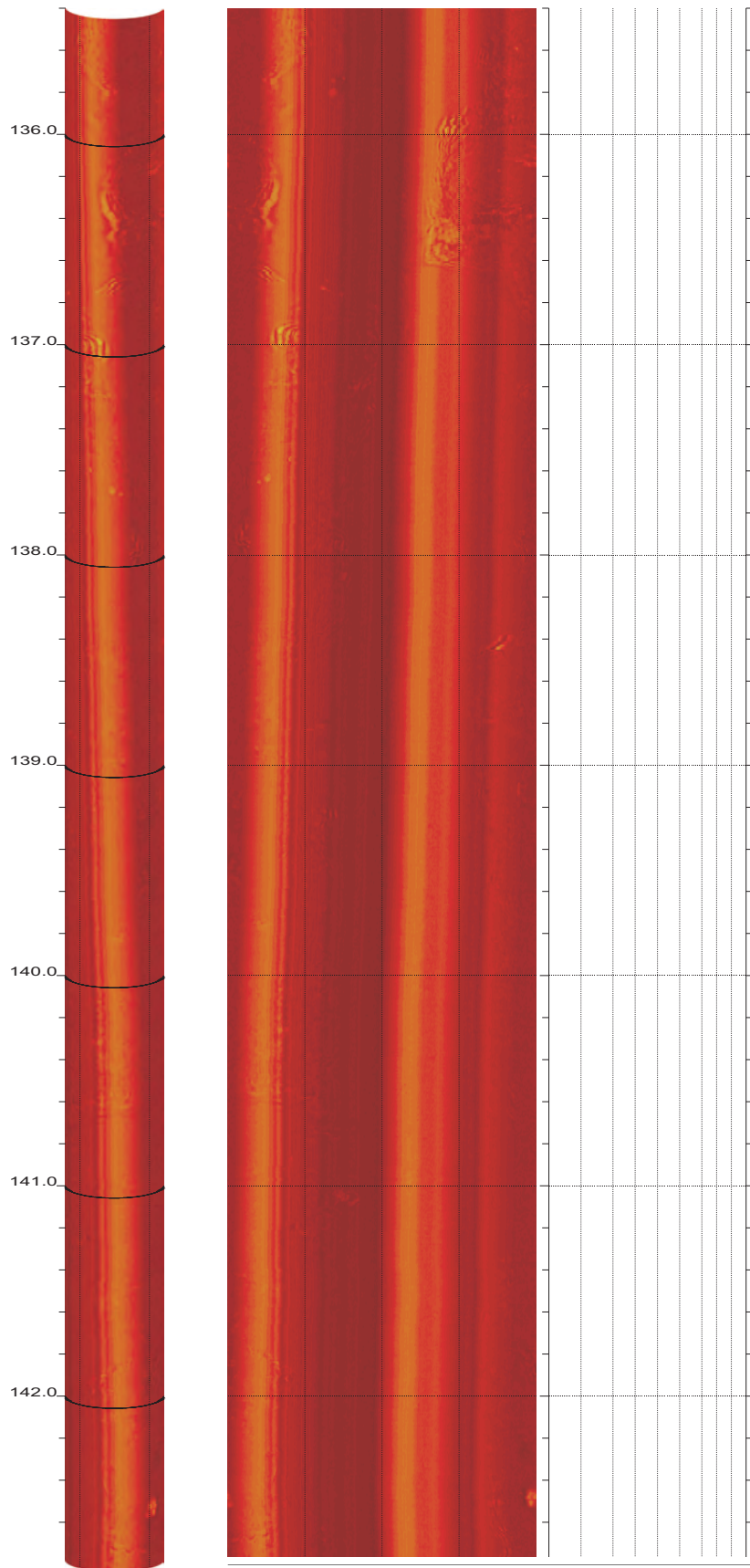
14



Z3-B6

135.400 to 128.032ft

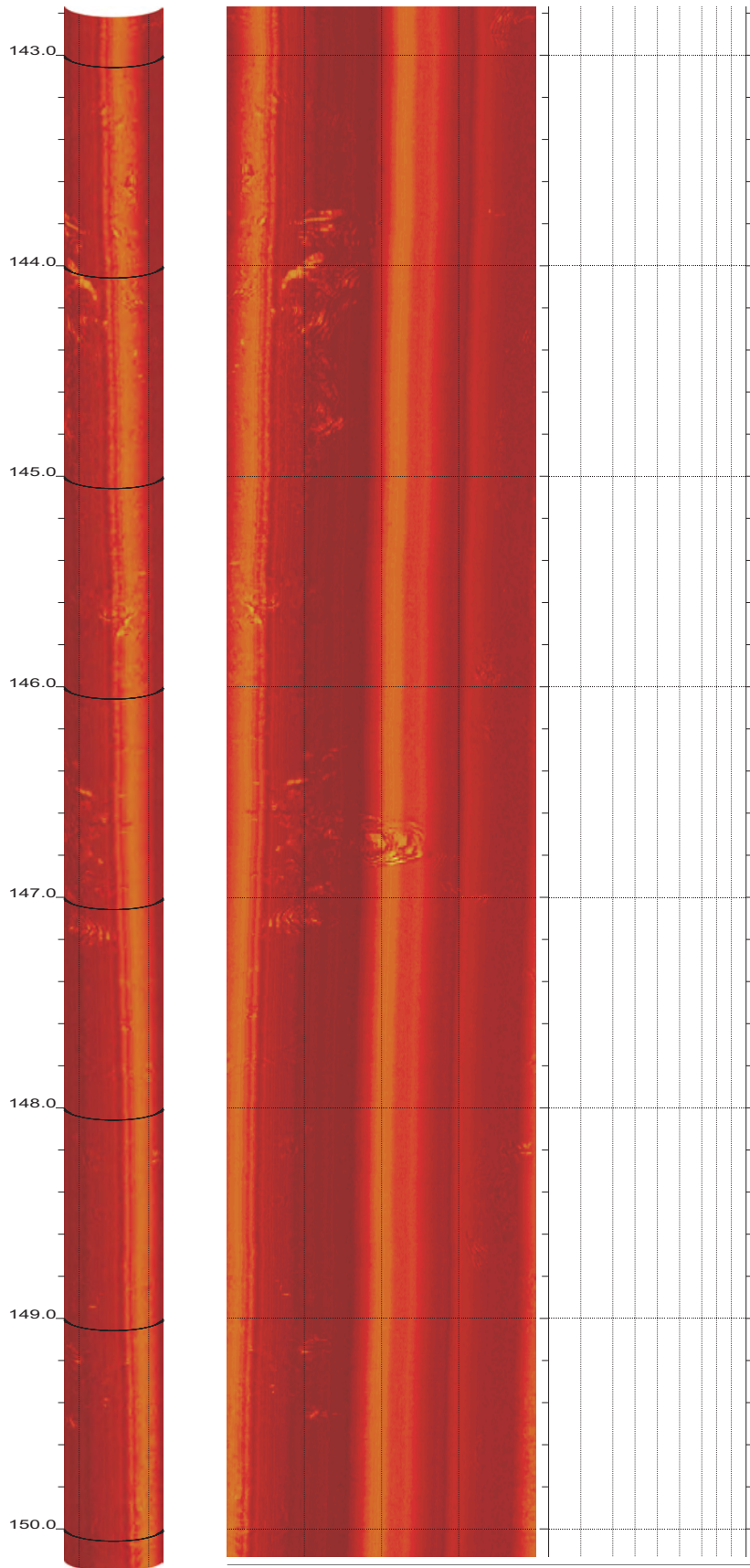
15



Z3-B6

142.768 to 135.400ft

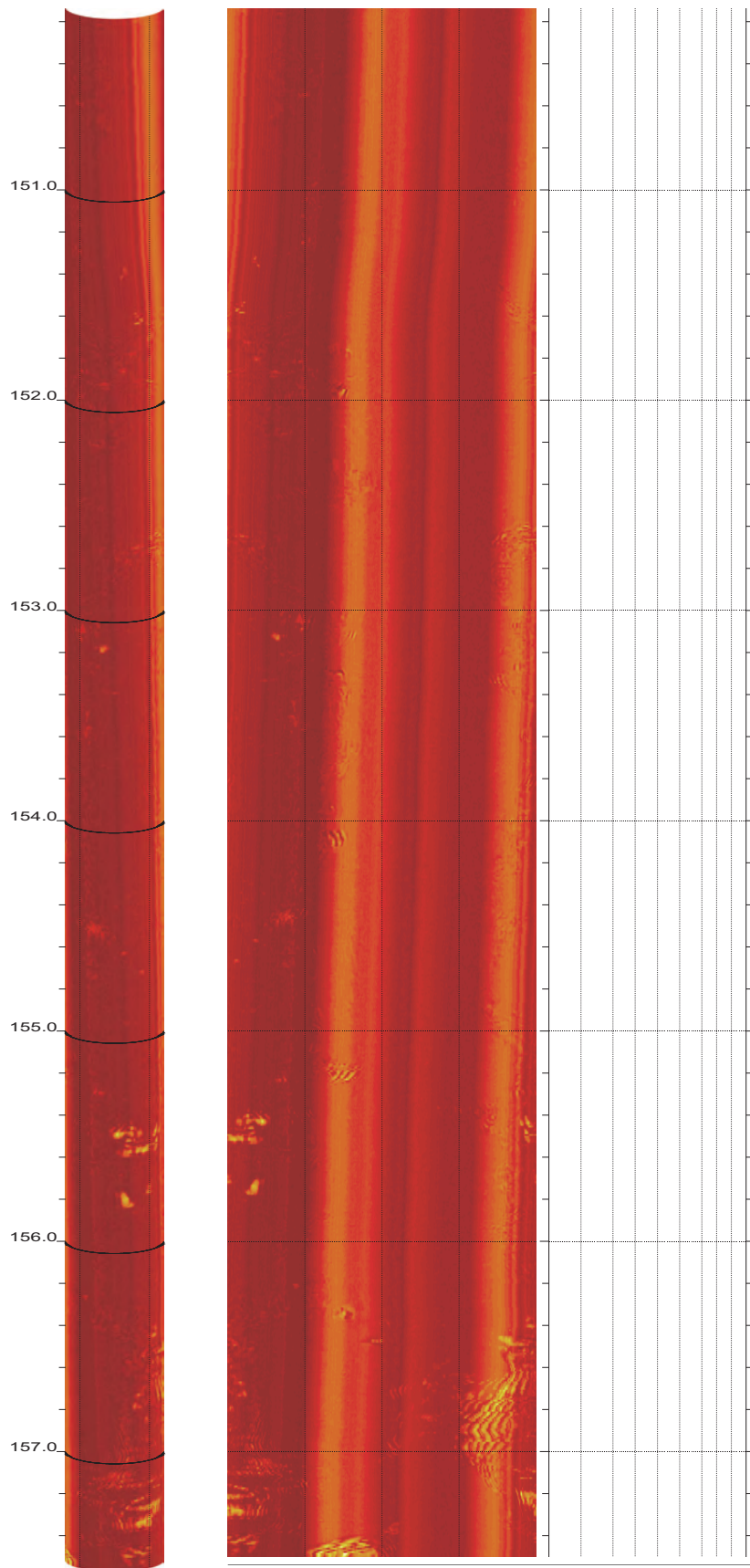
16



Z3-B6

150.136 to 142.768ft

17

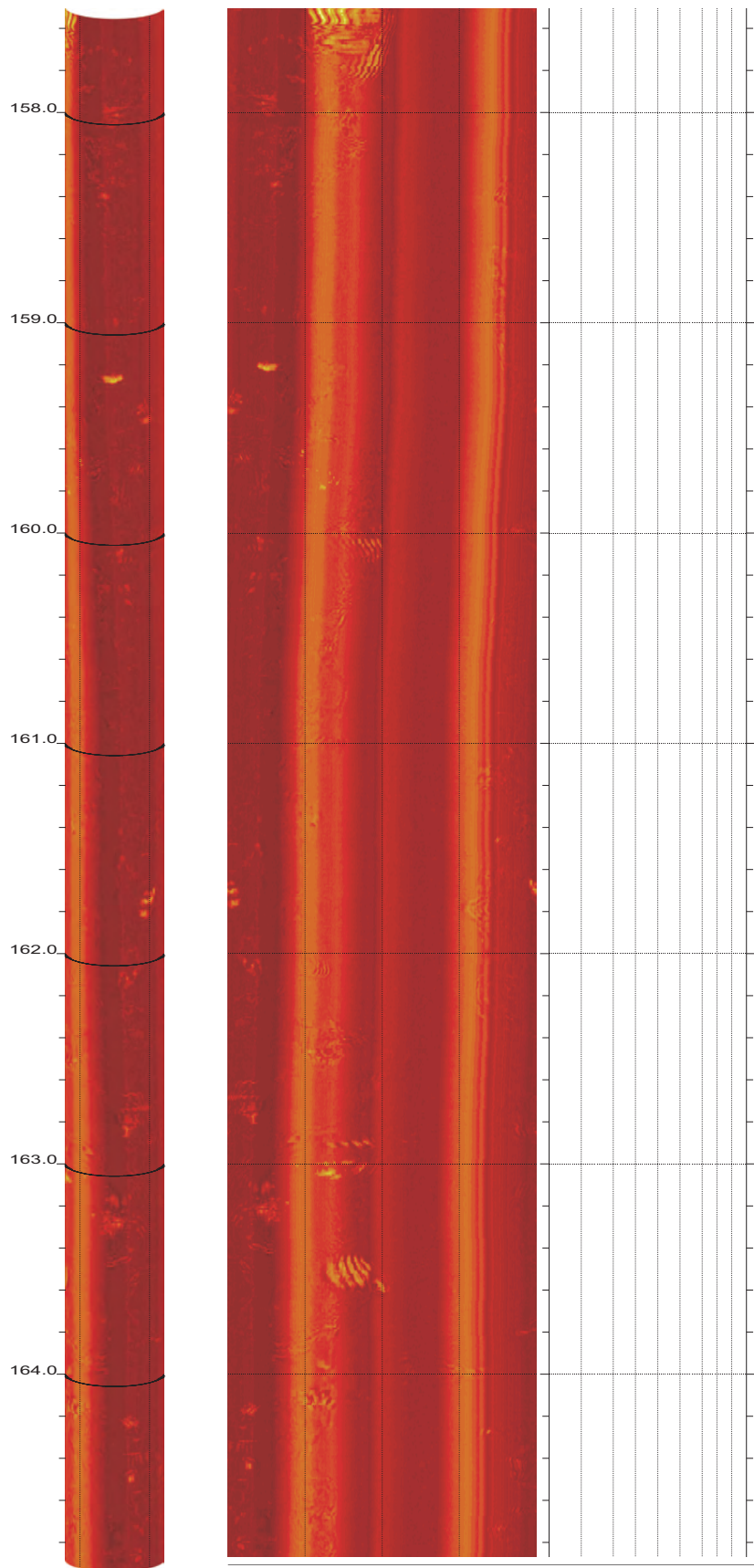


Z3-B6

157.504 to 150.136ft

18

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 18 of 40

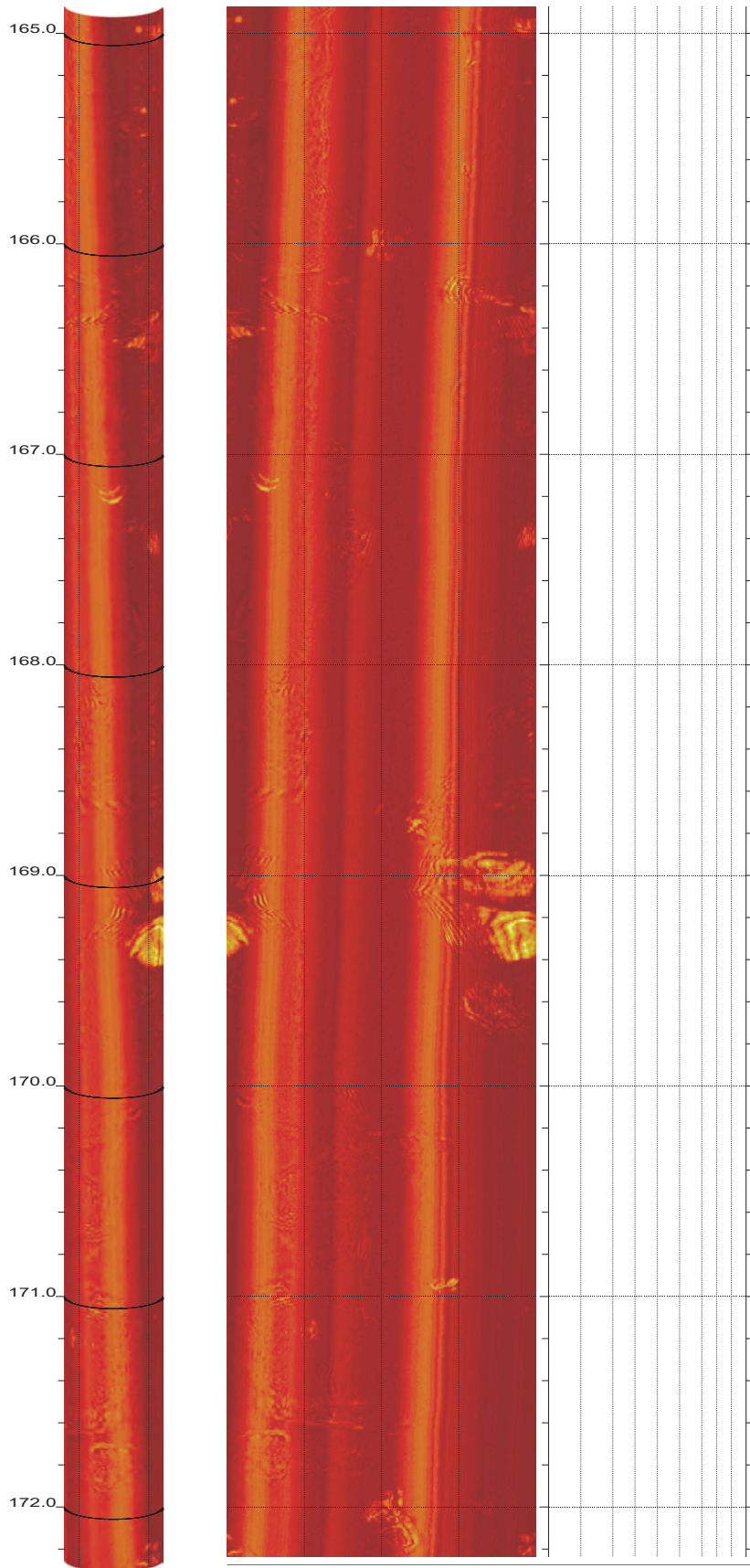


Z3-B6

164.872 to 157.504ft

19

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 19 of 40



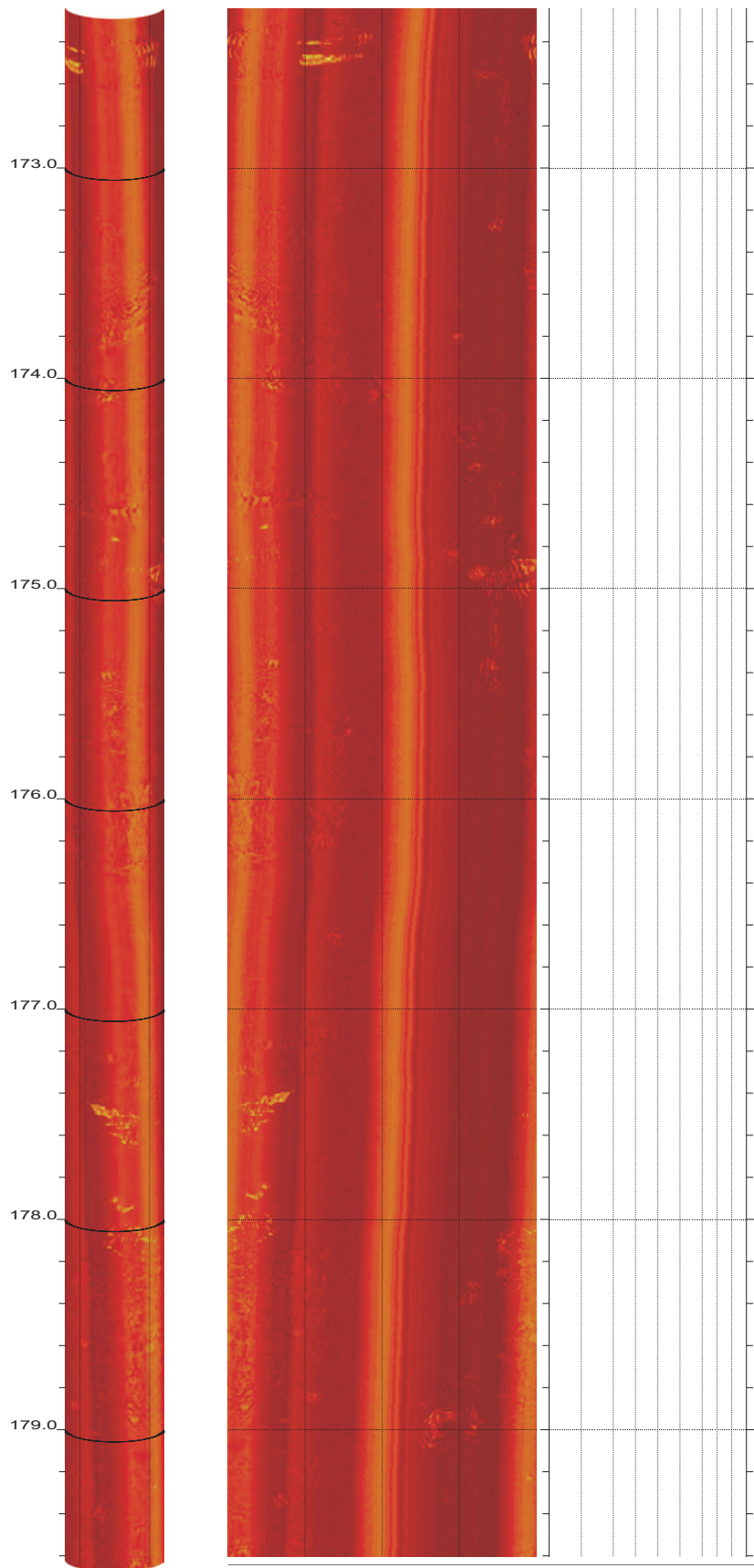
Z3-B6

172.240 to 164.872ft

20

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 20 of 40



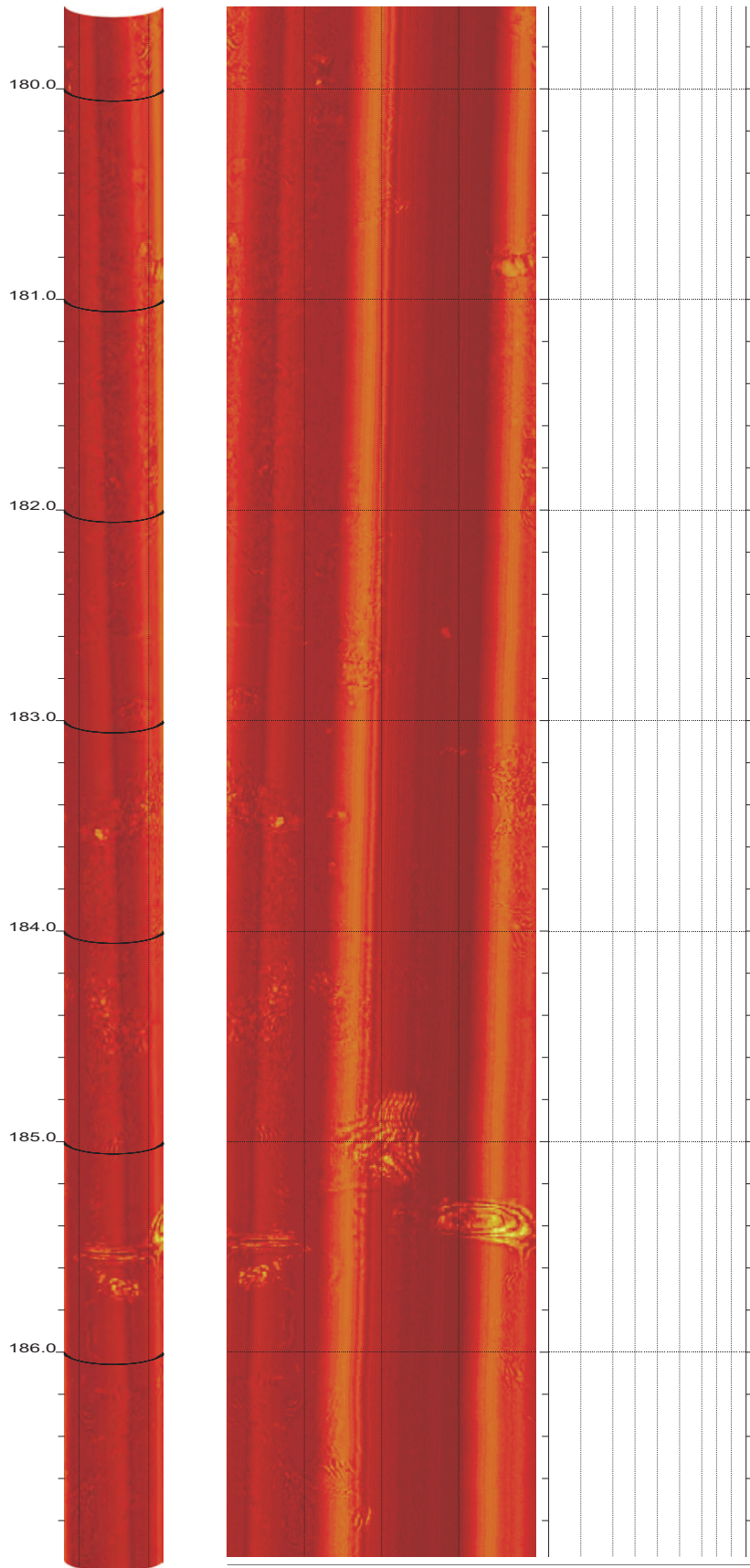


Z3-B6

179.608 to 172.240ft

21

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 21 of 40

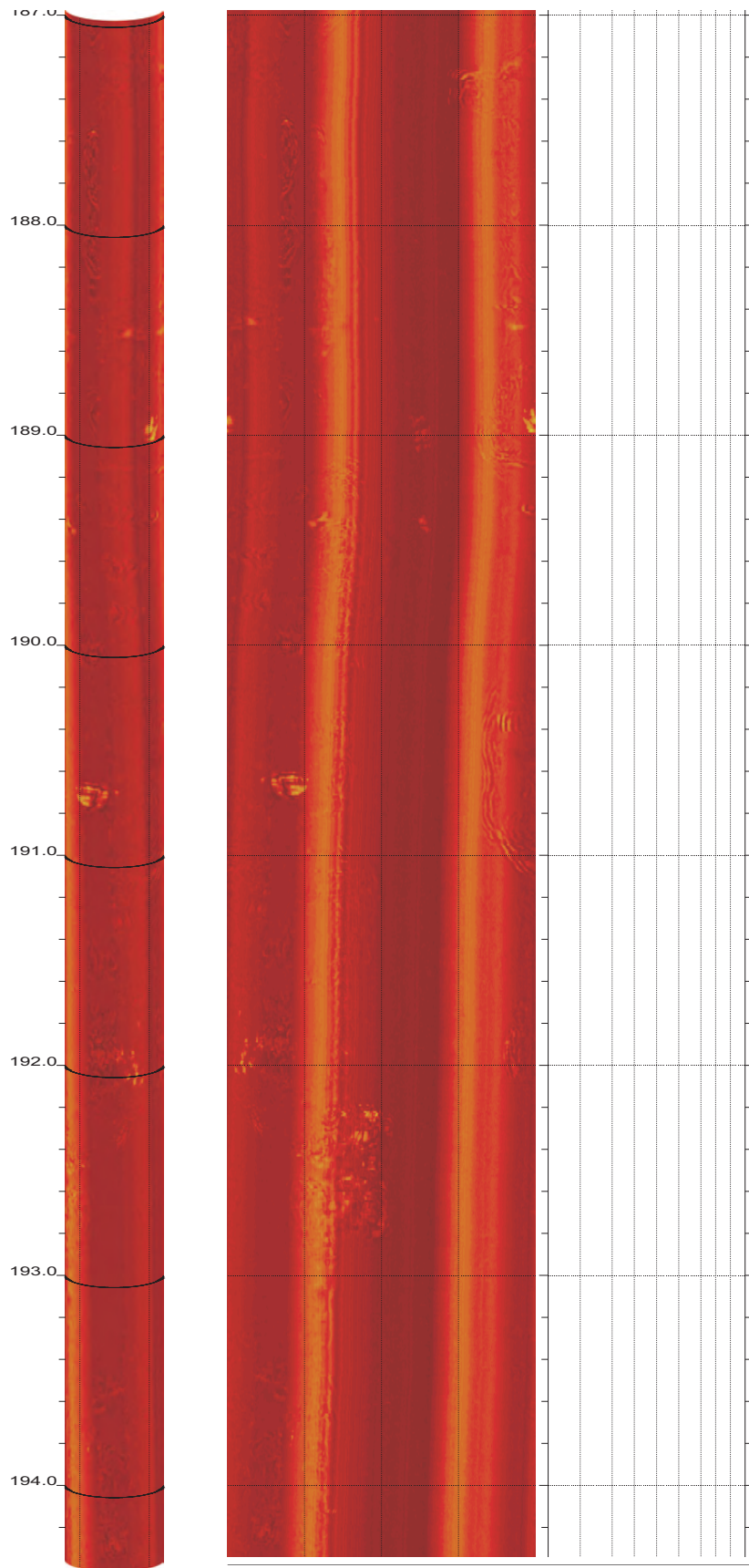


Z3-B6

186.976 to 179.608ft

22

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 22 of 40

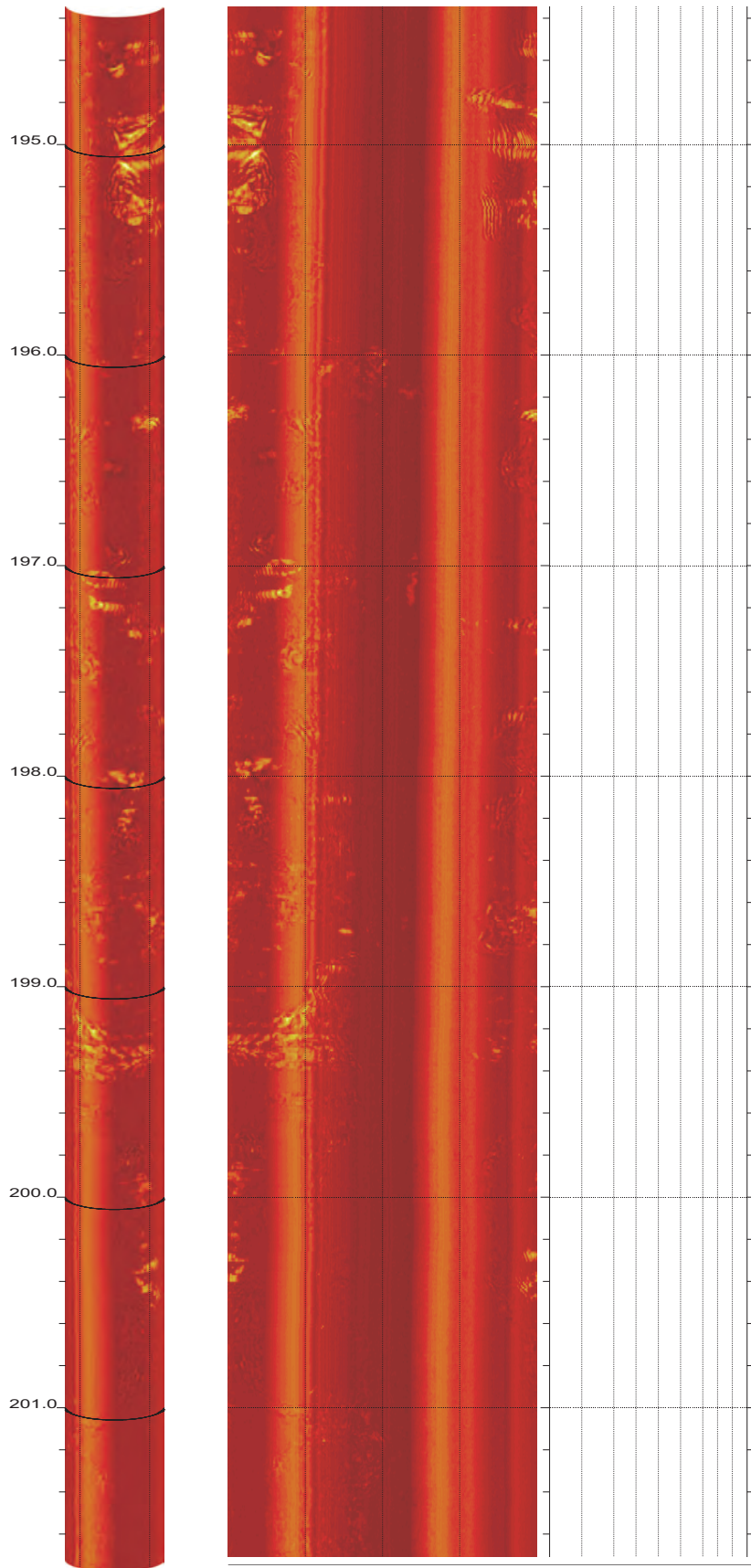


Z3-B6

194.344 to 186.976ft

23

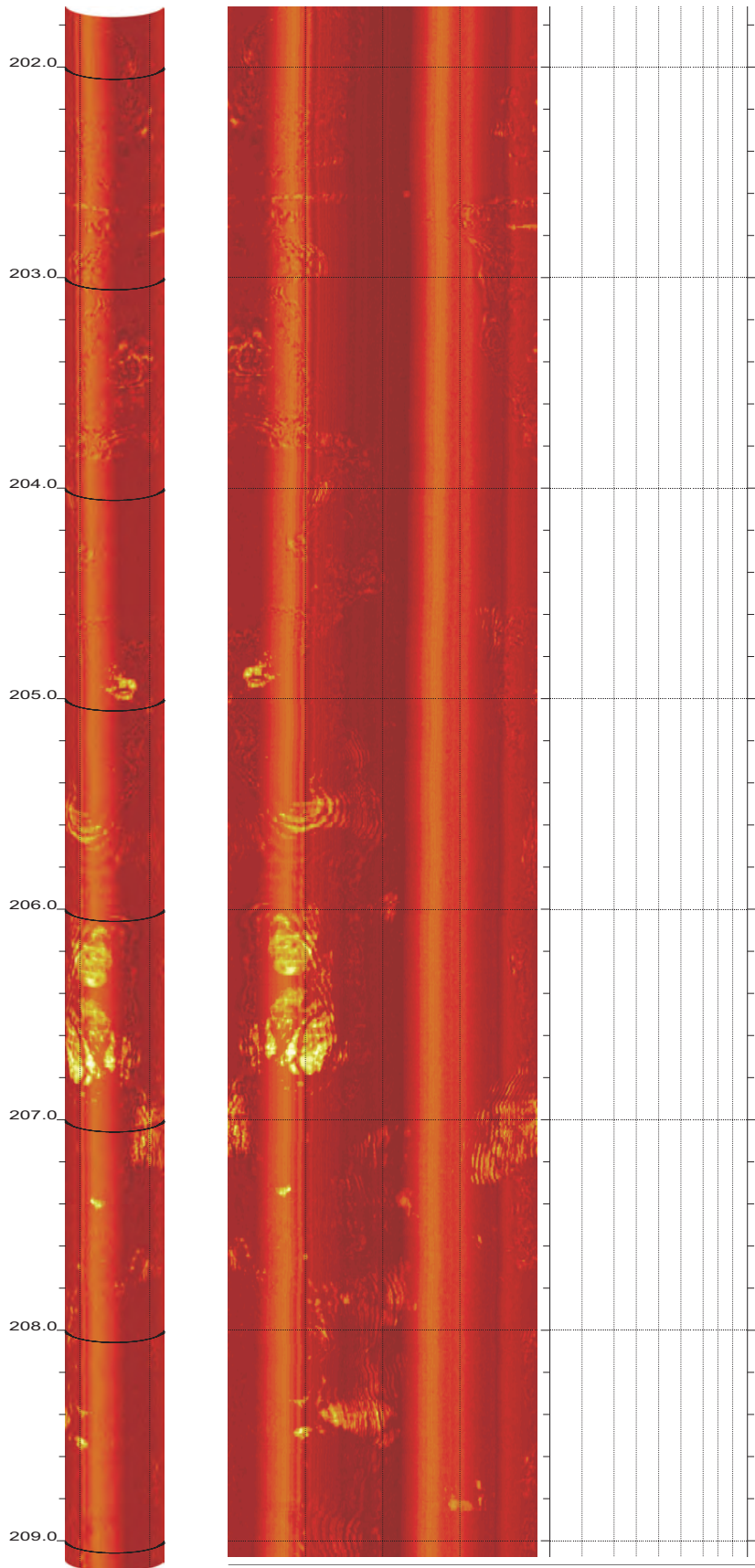
SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 23 of 40



Z3-B6

201.712 to 194.344ft

24

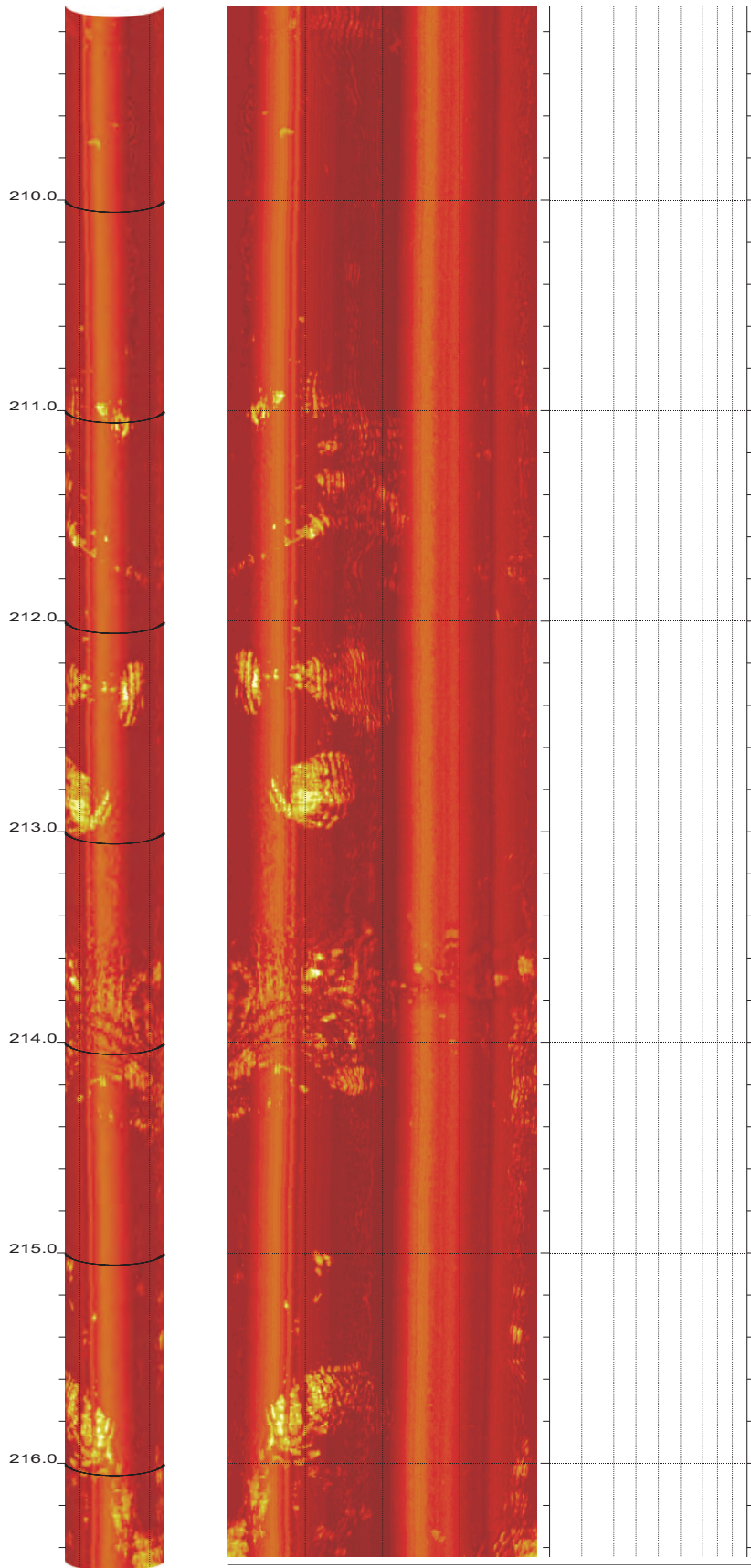


Z3-B6

209.080 to 201.712ft

25

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 25 of 40

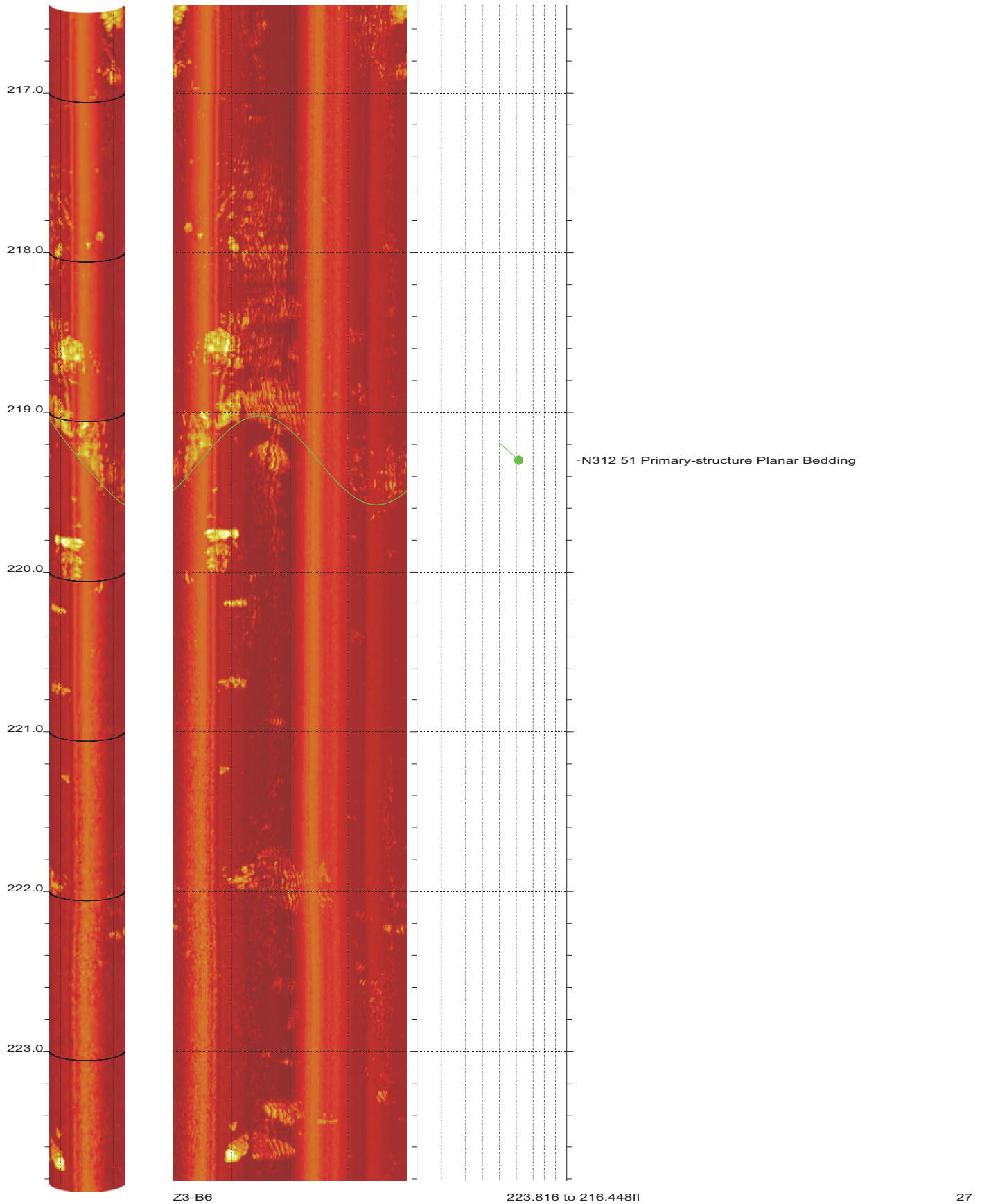


Z3-B6

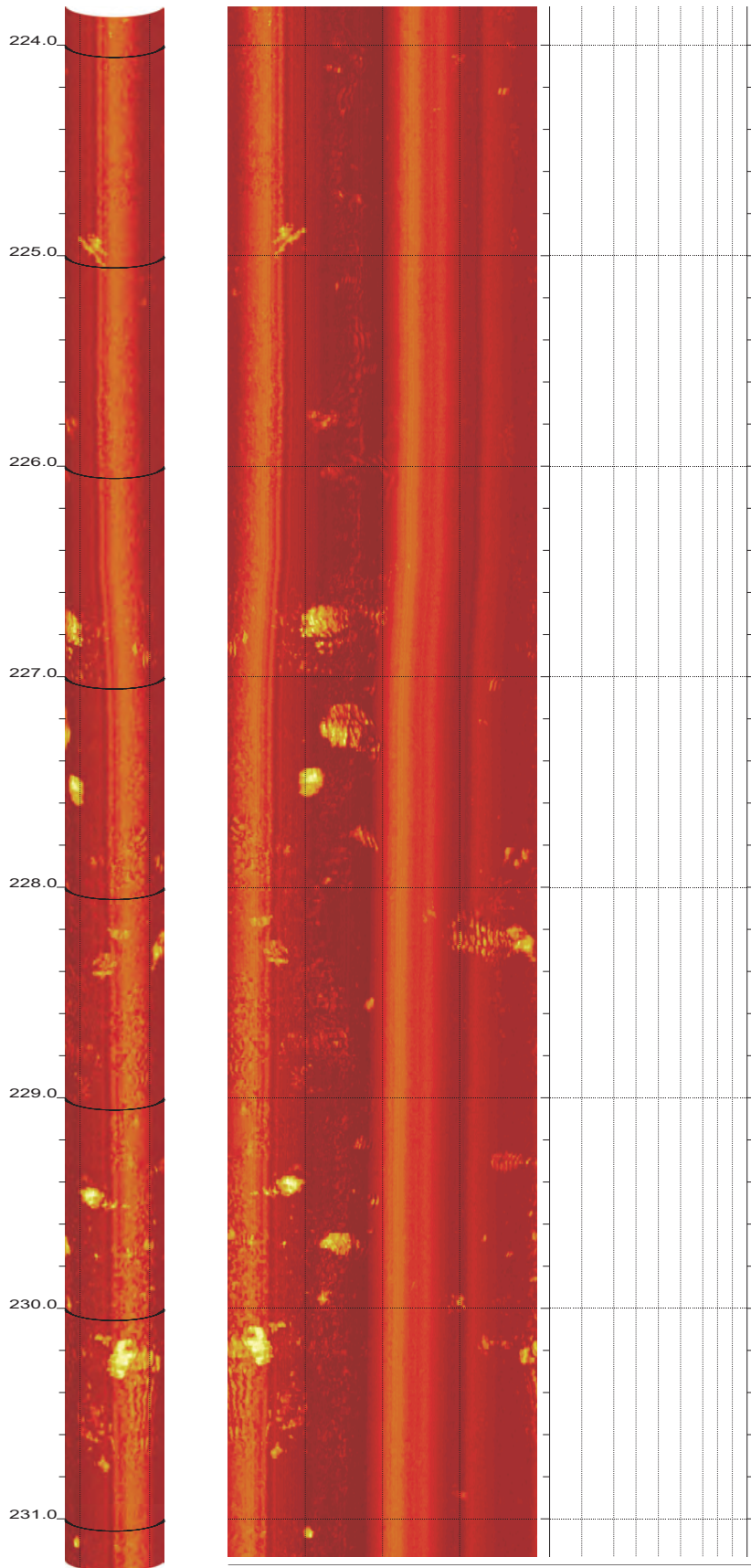
216.448 to 209.080ft

26

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 26 of 40



SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 27 of 40



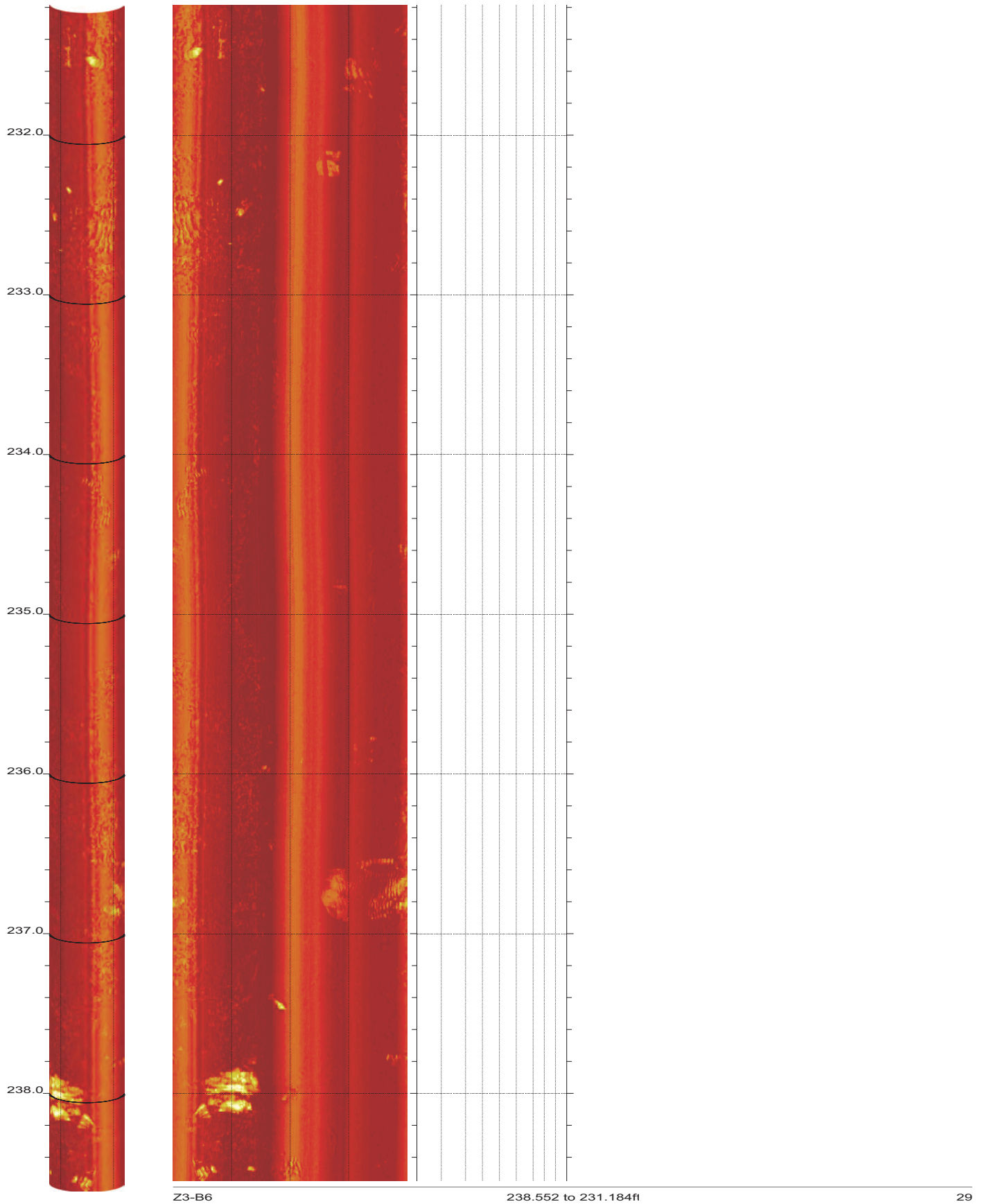
Z3-B6

231.184 to 223.816ft

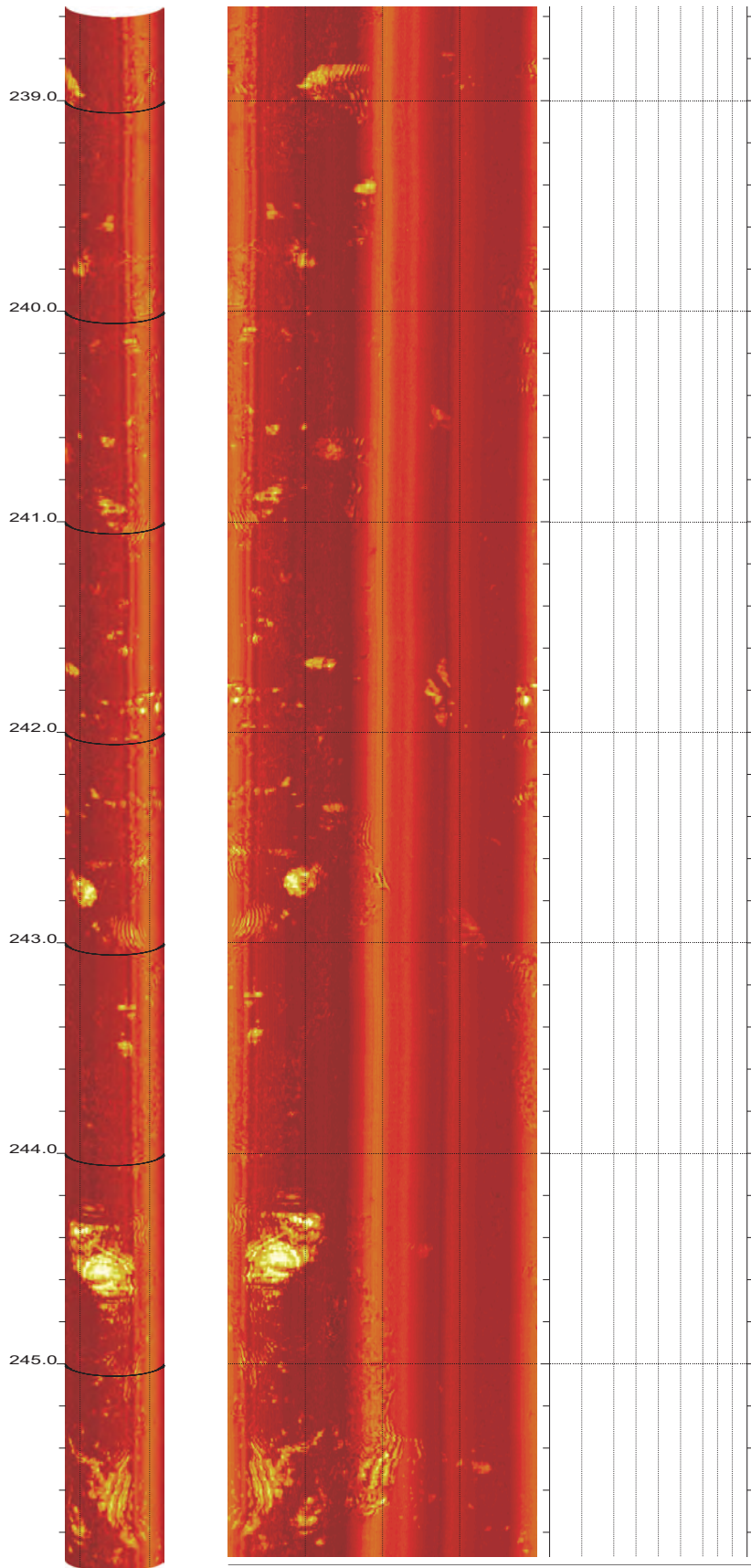
28

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 28 of 40





SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 29 of 40

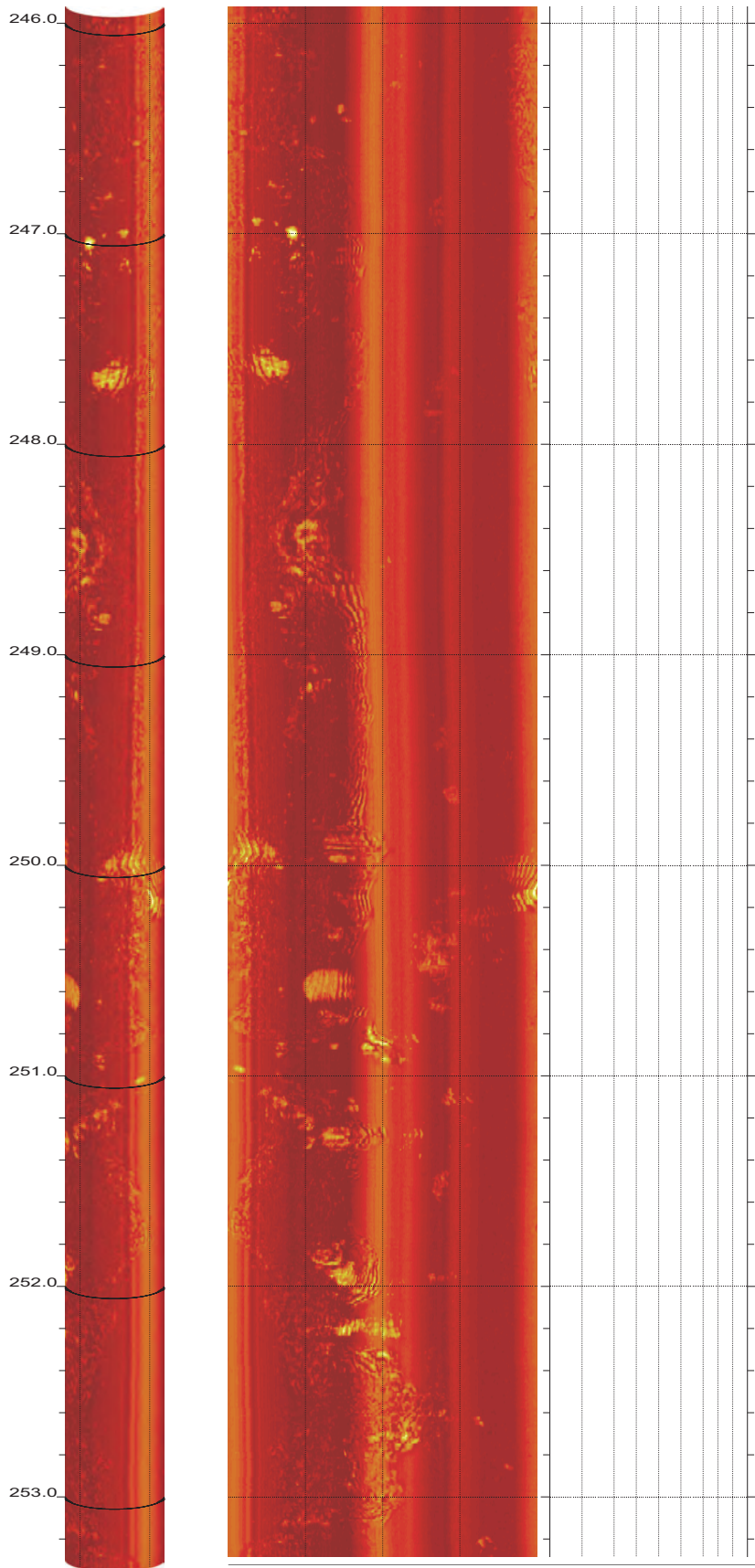


Z3-B6

245.920 to 238.552ft

30

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 30 of 40

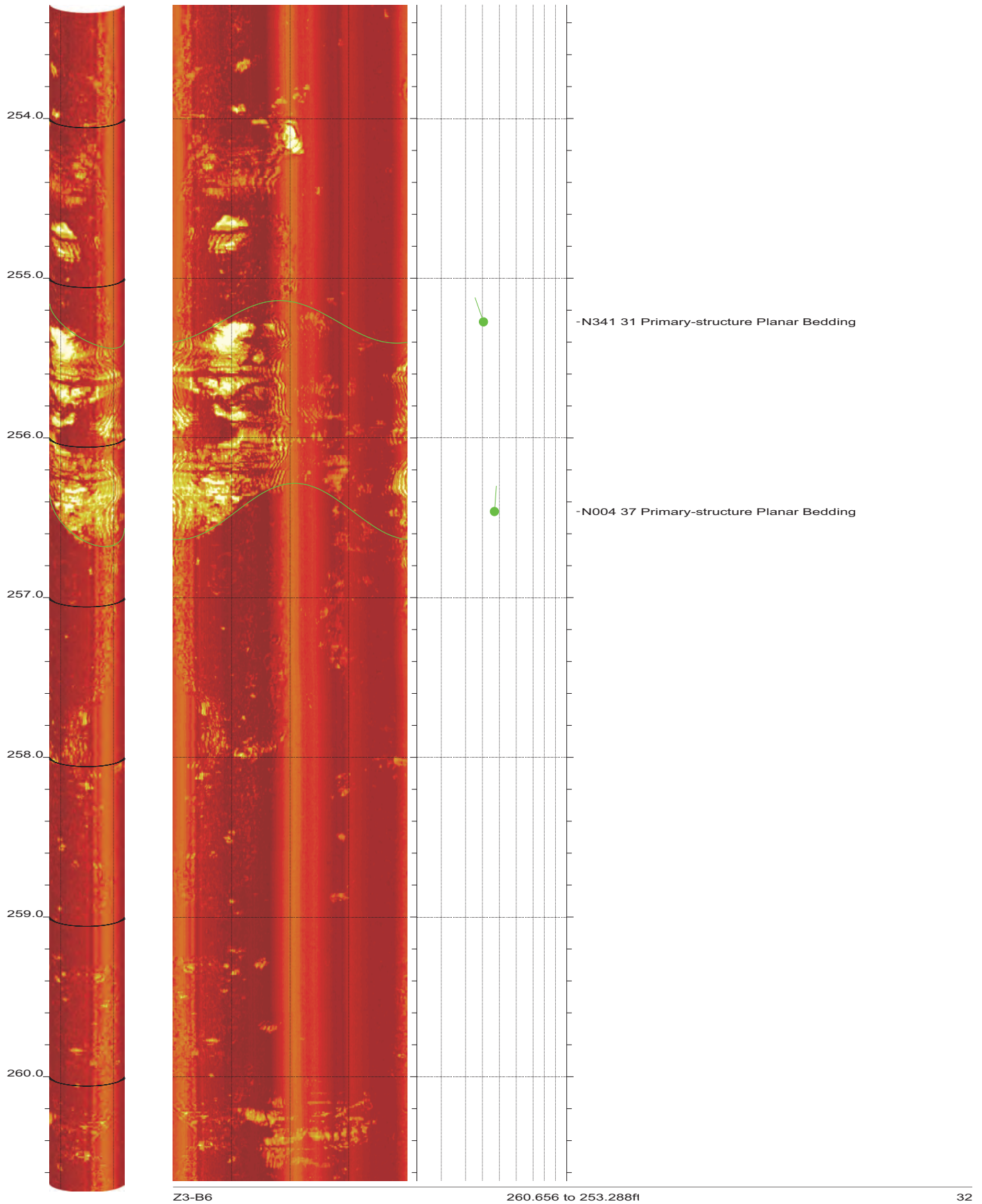


Z3-B6

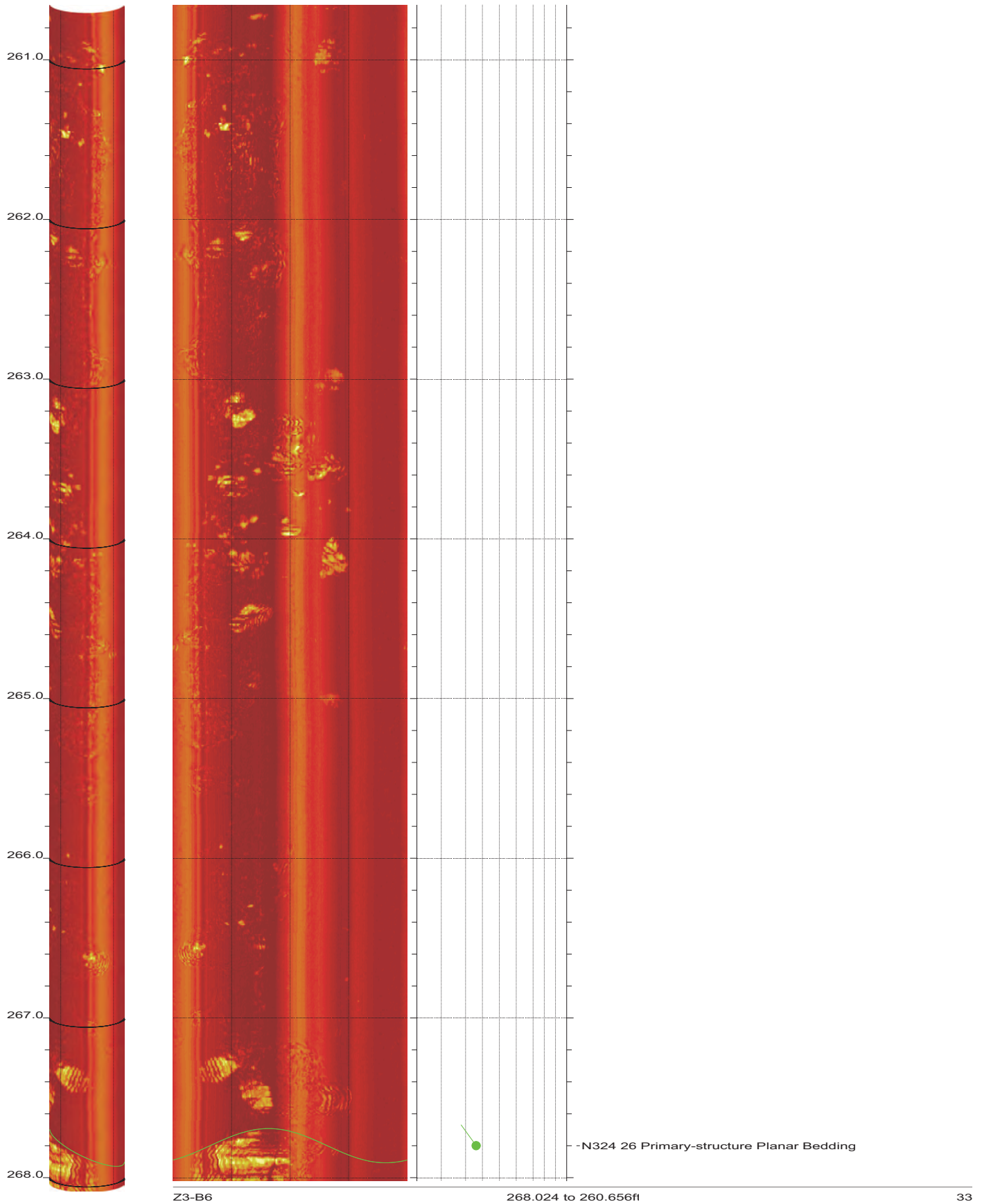
253.288 to 245.920ft

31

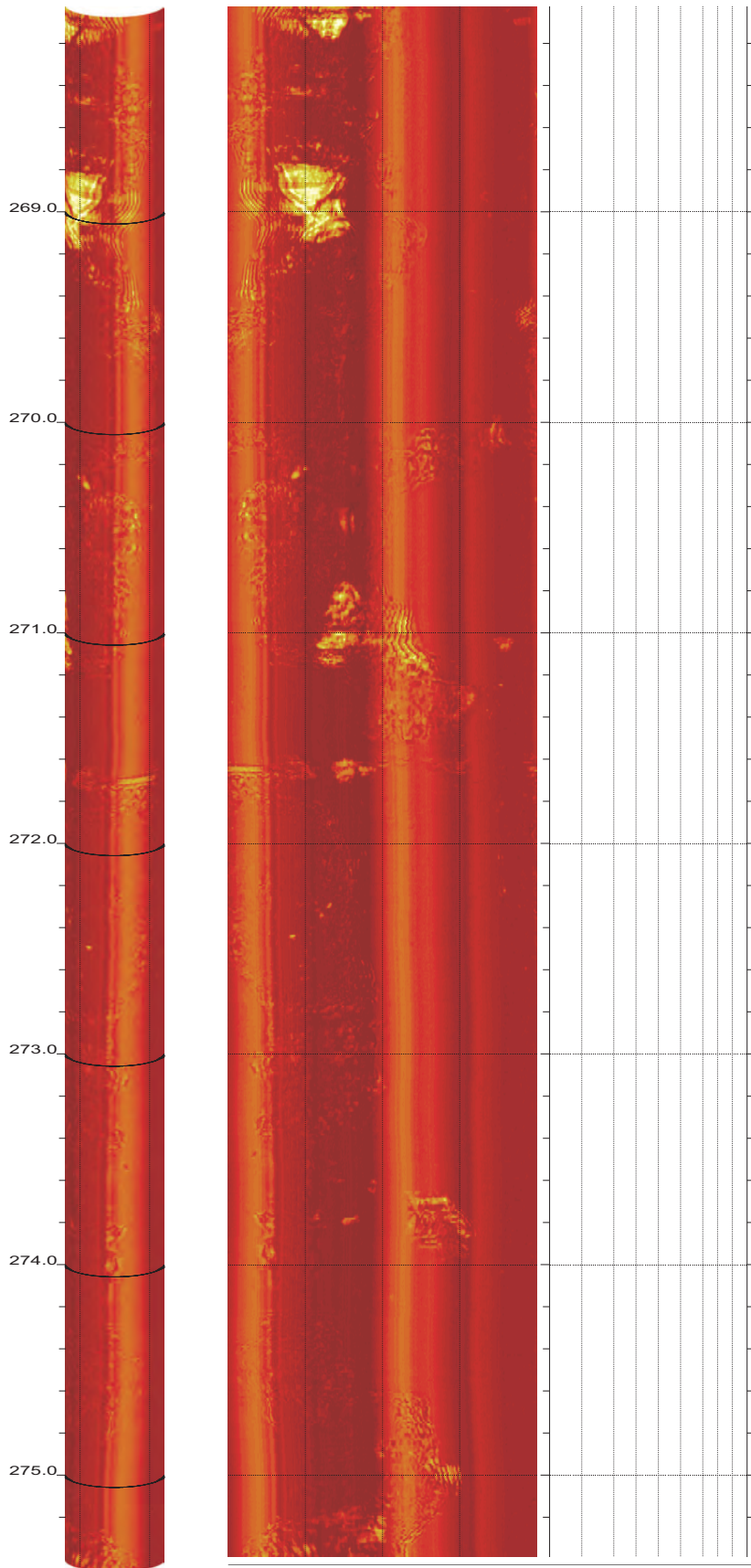
SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 31 of 40



SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 32 of 40



SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 33 of 40

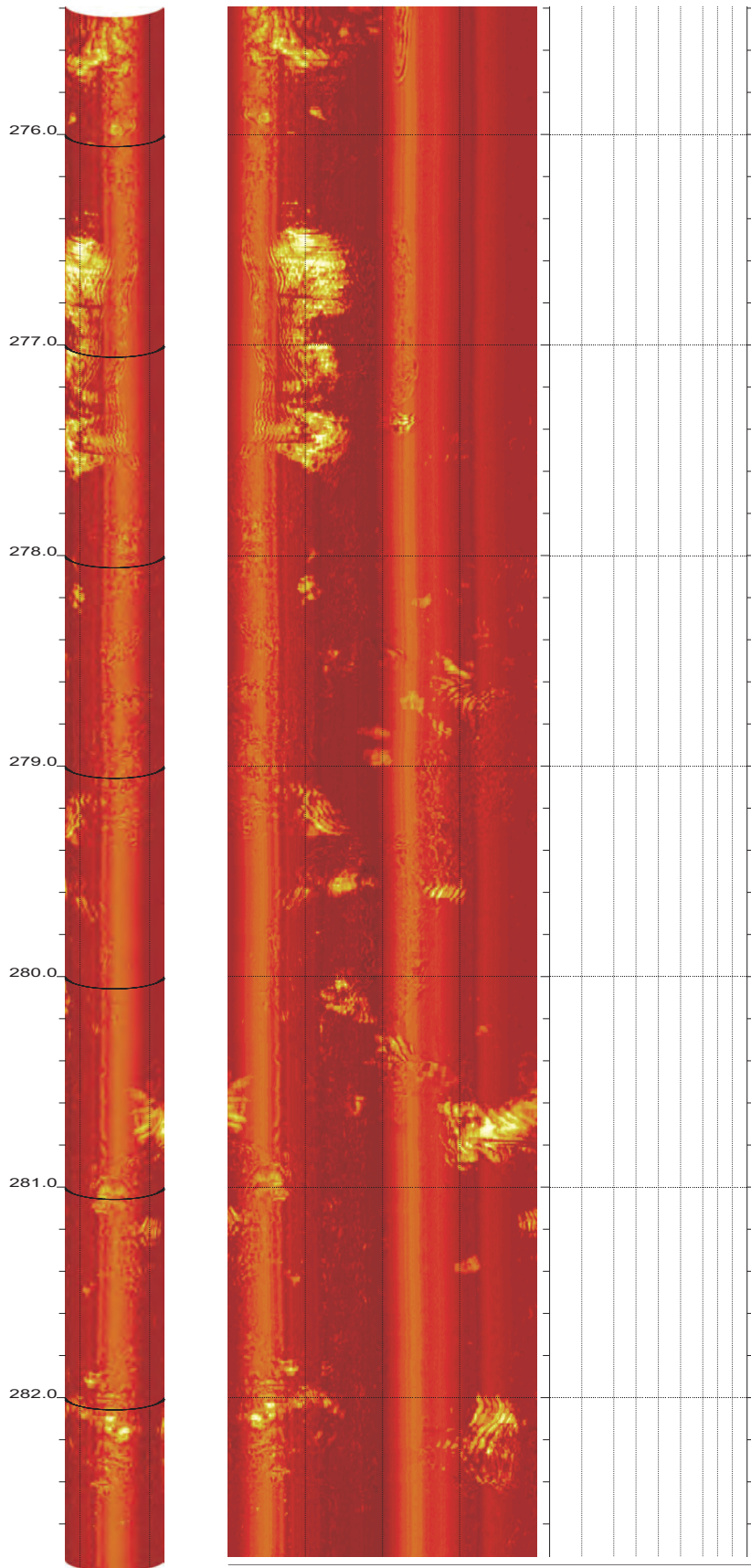


Z3-B6

275.392 to 268.024ft

34

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 34 of 40

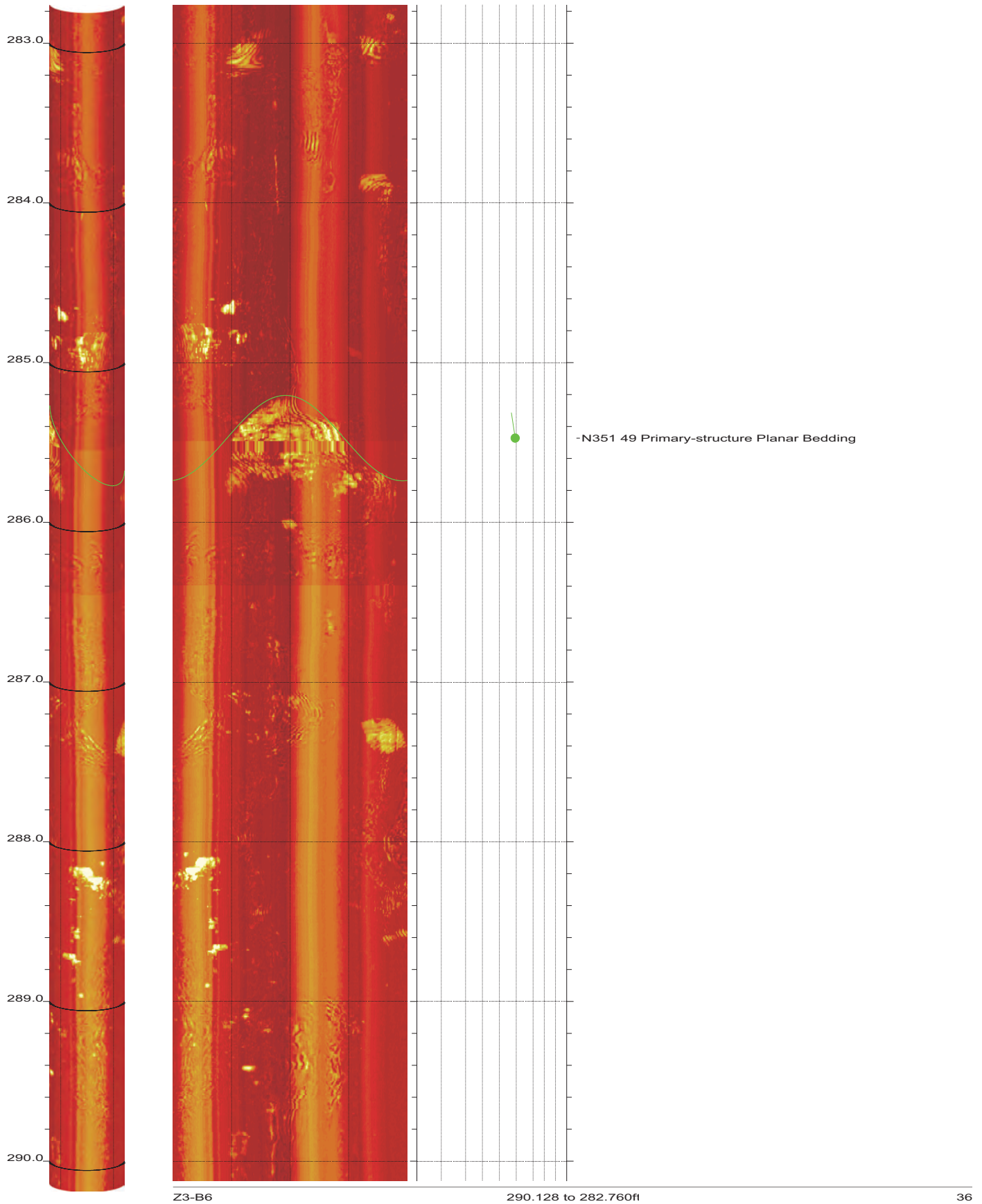


Z3-B6

282.760 to 275.392ft

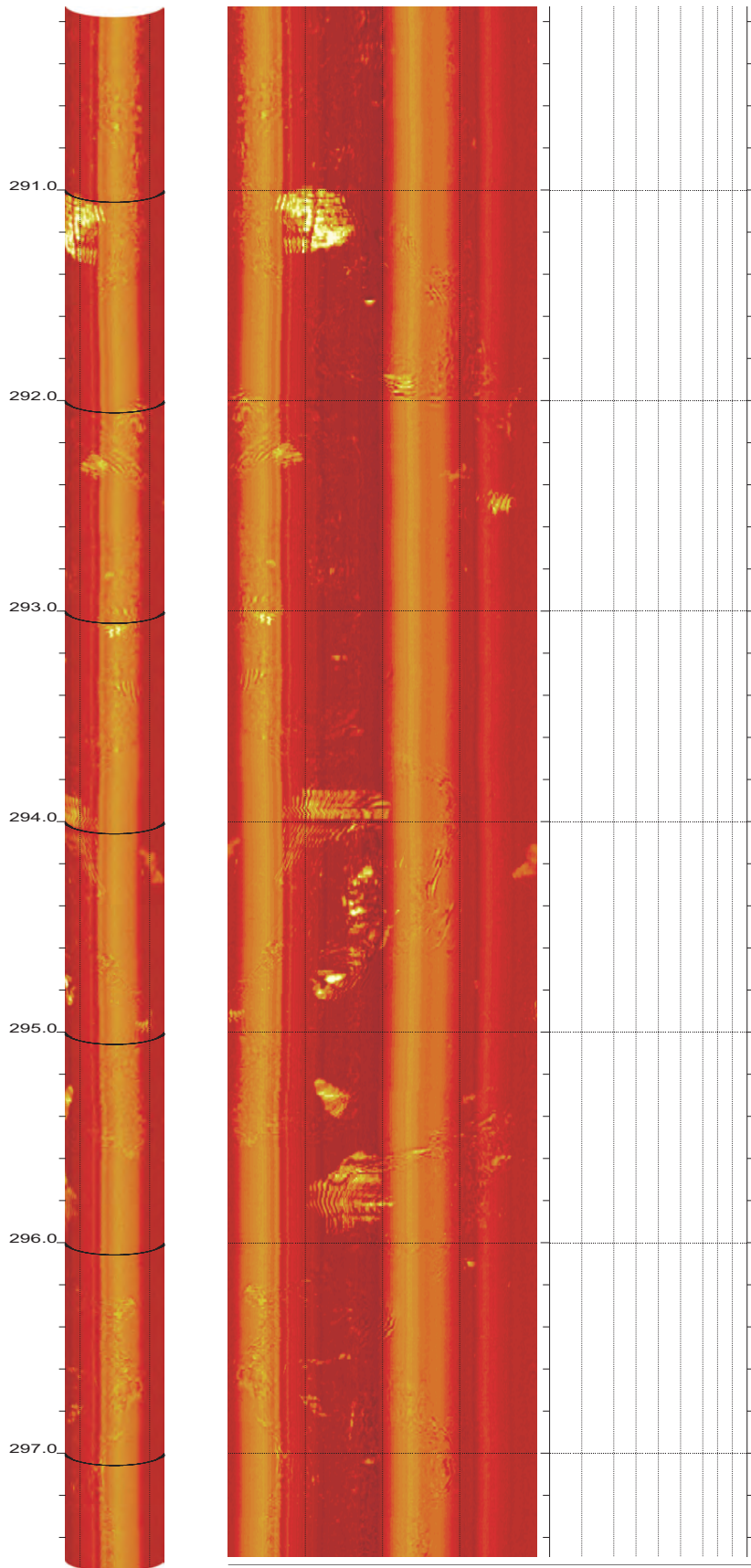
35

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 35 of 40



SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 36 of 40



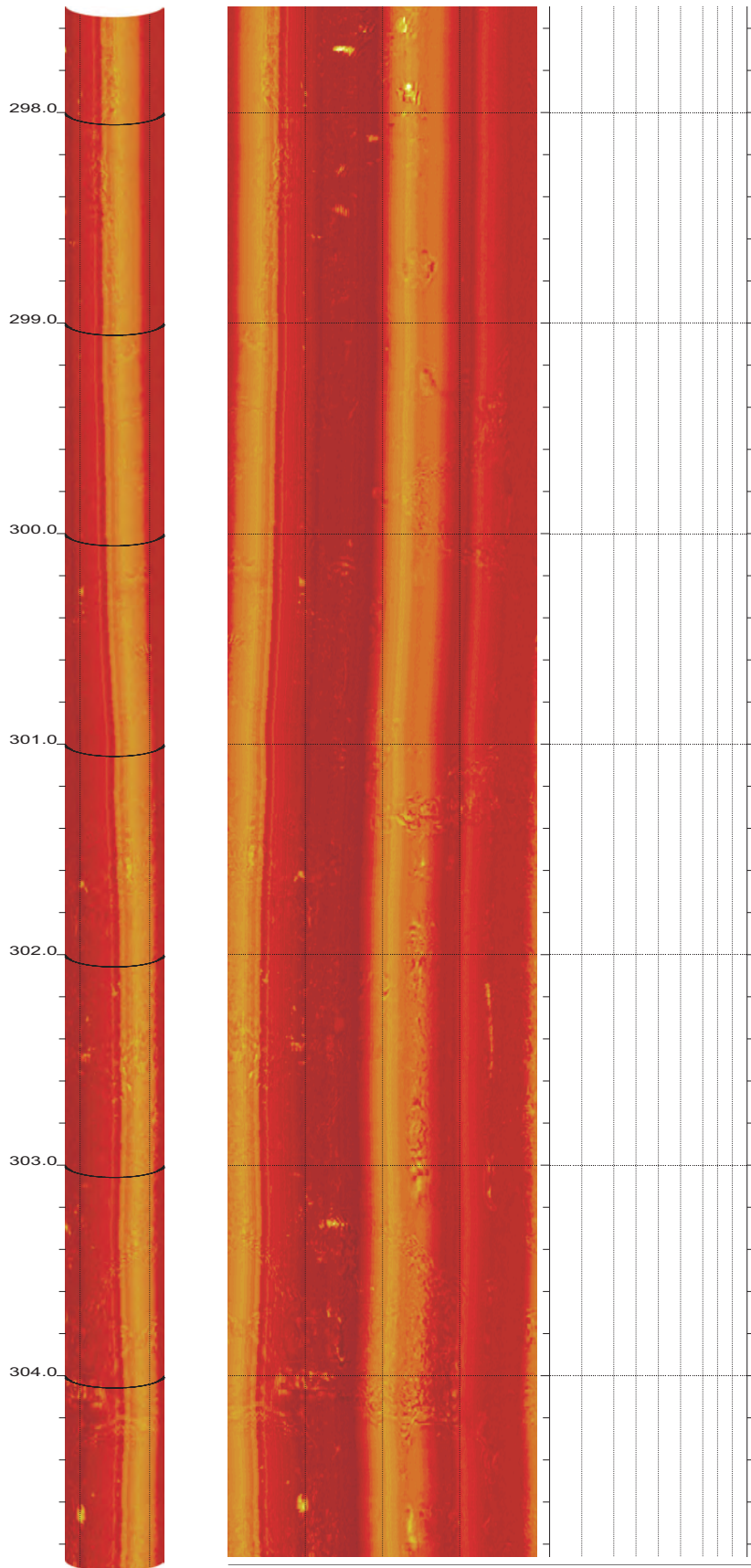


Z3-B6

297.496 to 290.128ft

37

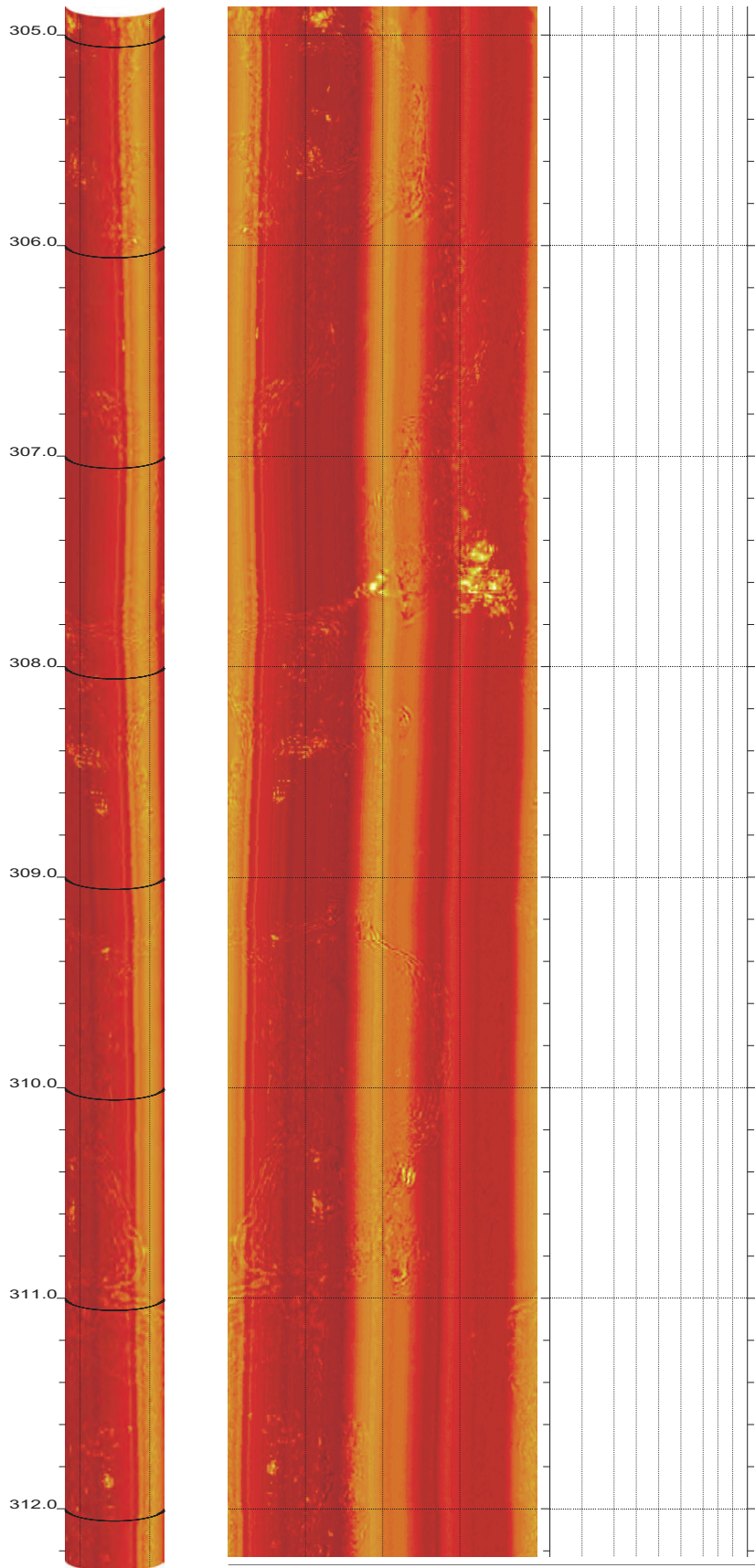
SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 37 of 40



Z3-B6

304.864 to 297.496ft

38

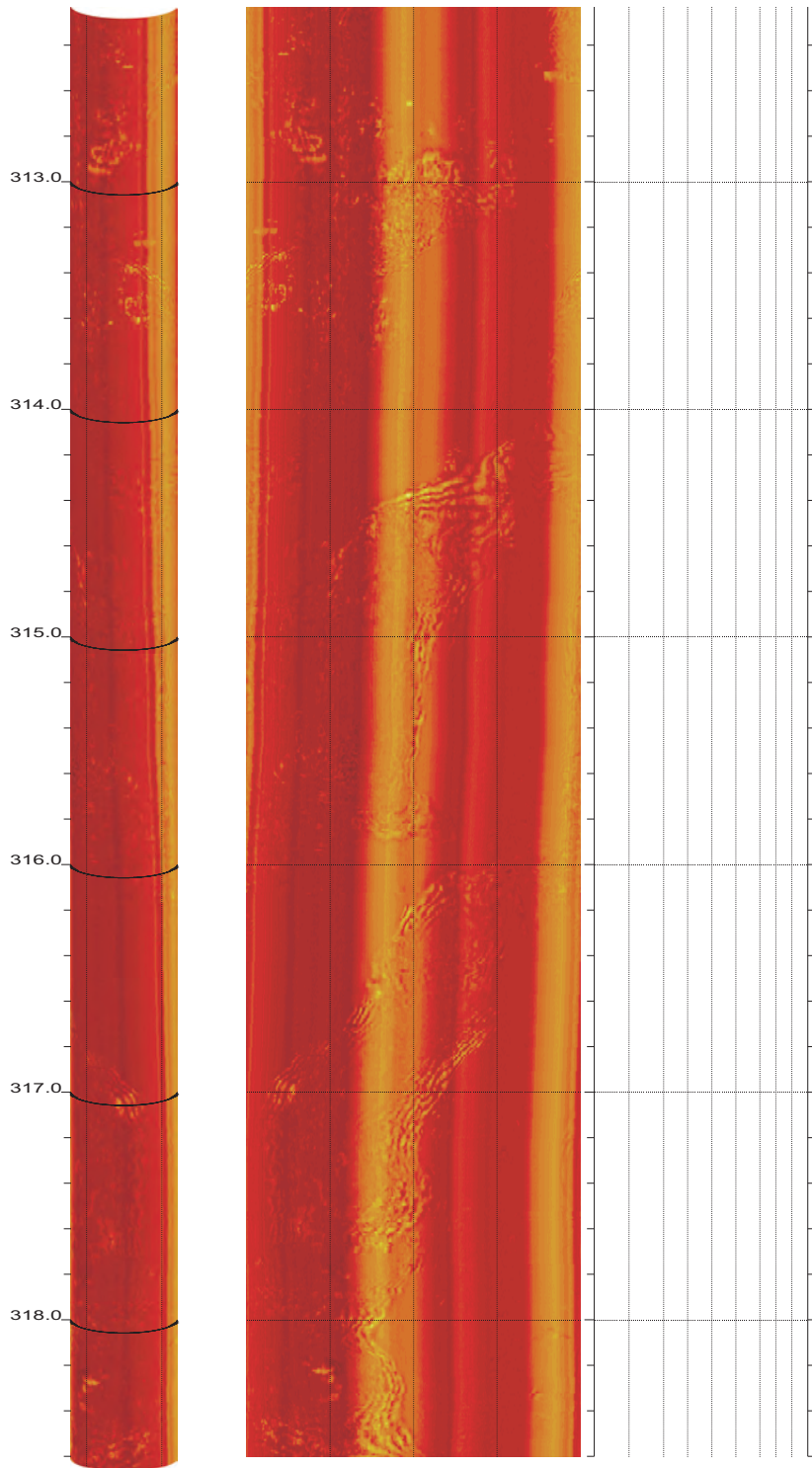


Z3-B6

312.232 to 304.864ft

39

SR-710 Boring Z3-B6 Acoustic Televiewer Dips rev 1 Sheet 39 of 40





BHTV DATA PROCESSING  
 RGLDIP vsn 6.2  
 INTERPRETED BHTV DIPS LOG

CASCADE DRILLING

Borehole: Z3-B12

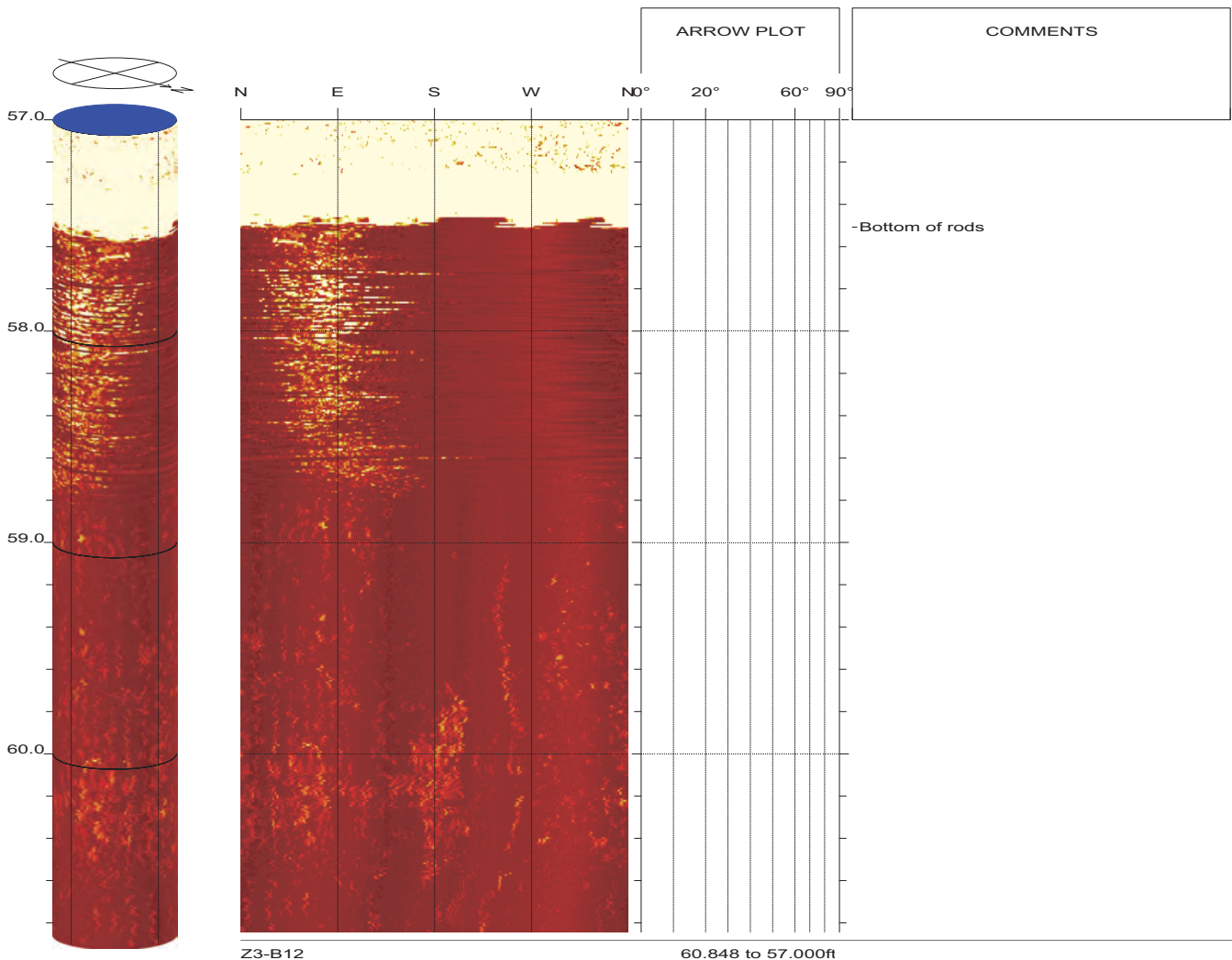
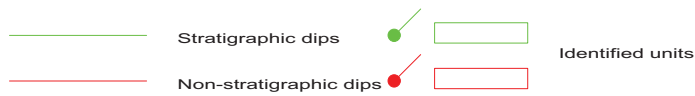
SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

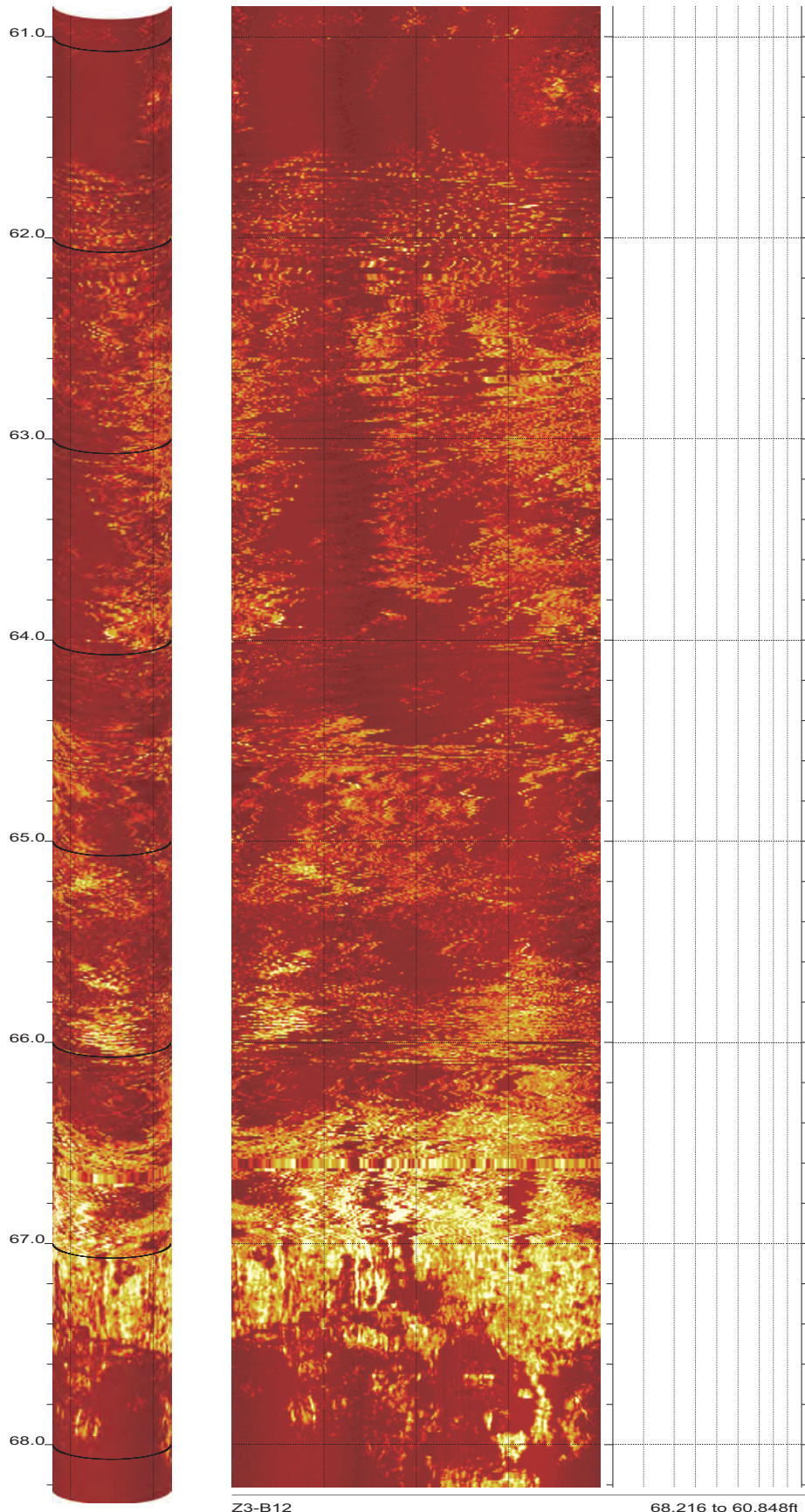
North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

Zone from 182.400 to 57.000ft  
 Format: BHTV-NESWN

Borehole diam: 7.000inch  
 Vertical = borehole-axis  
 Image: Amplitude



SR-710 Boring Z3-B12 Acoustic Televiwer Dips rev 1 Sheet 1 of 18

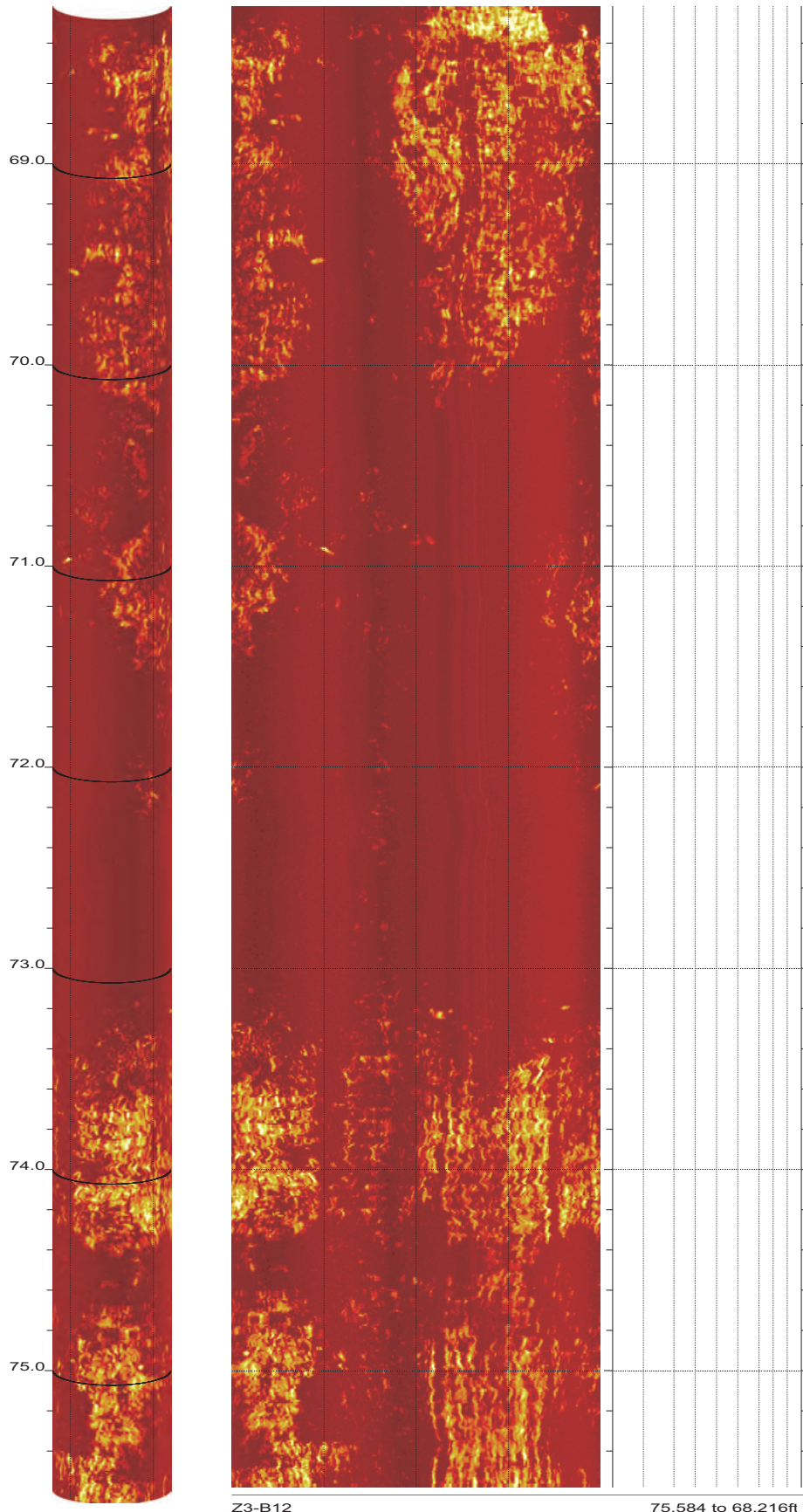


Z3-B12

68.216 to 60.848ft

2

SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 2 of 18

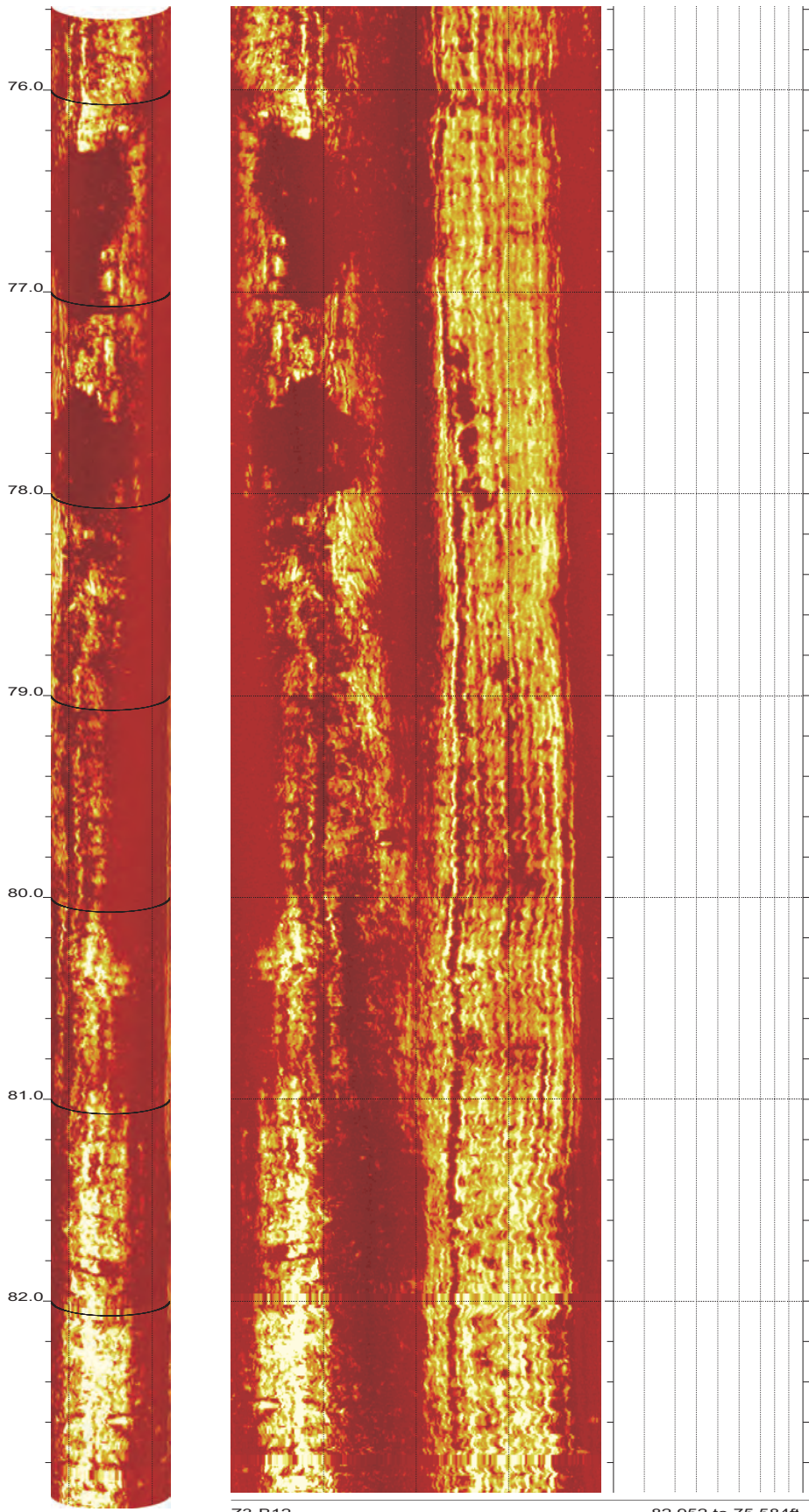


Z3-B12

75.584 to 68.216ft

3

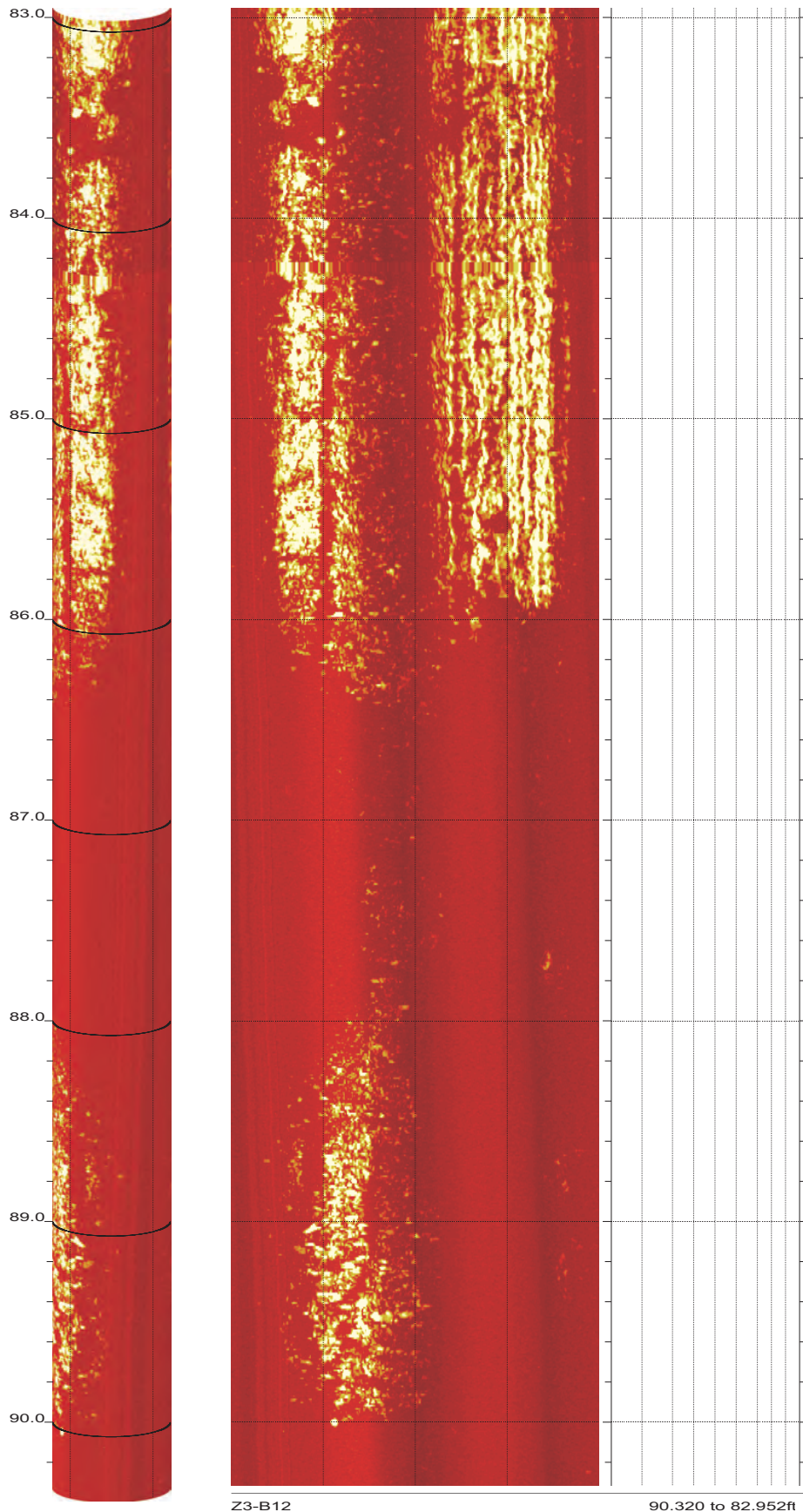
SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 3 of 18



Z3-B12

82.952 to 75.584ft



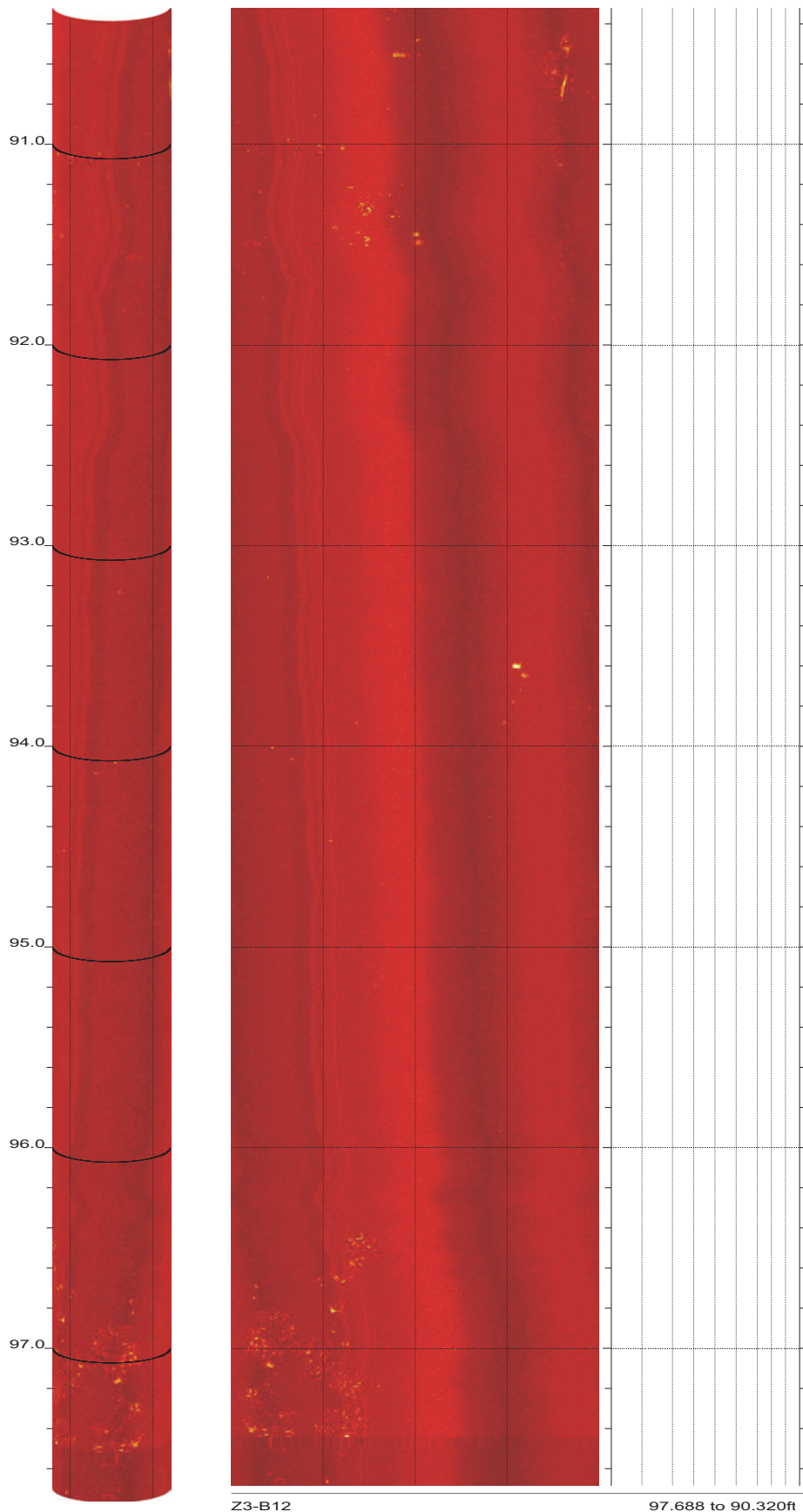


Z3-B12

90.320 to 82.952ft

5

SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 5 of 18

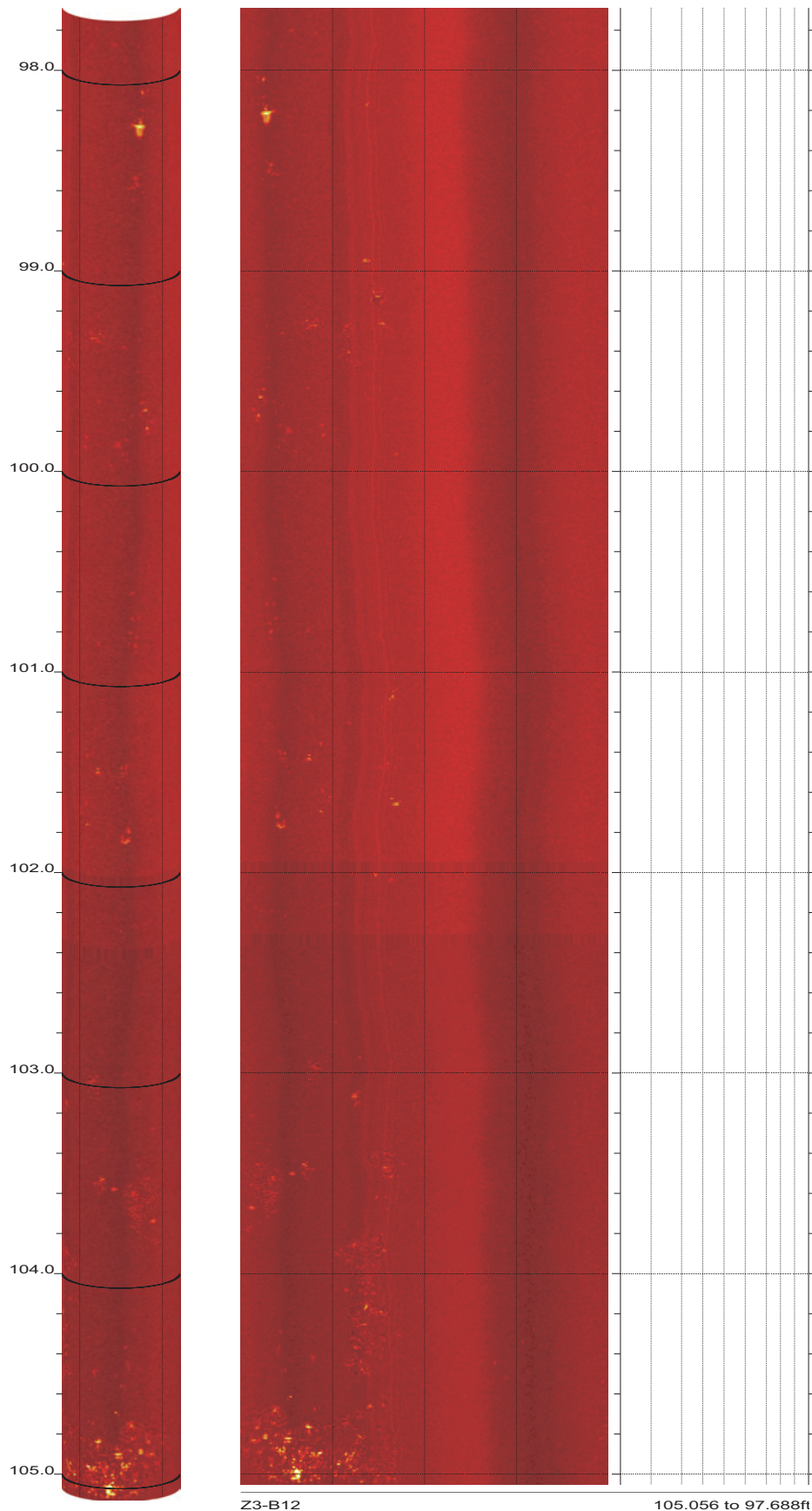


Z3-B12

97.688 to 90.320ft

6

SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 6 of 18

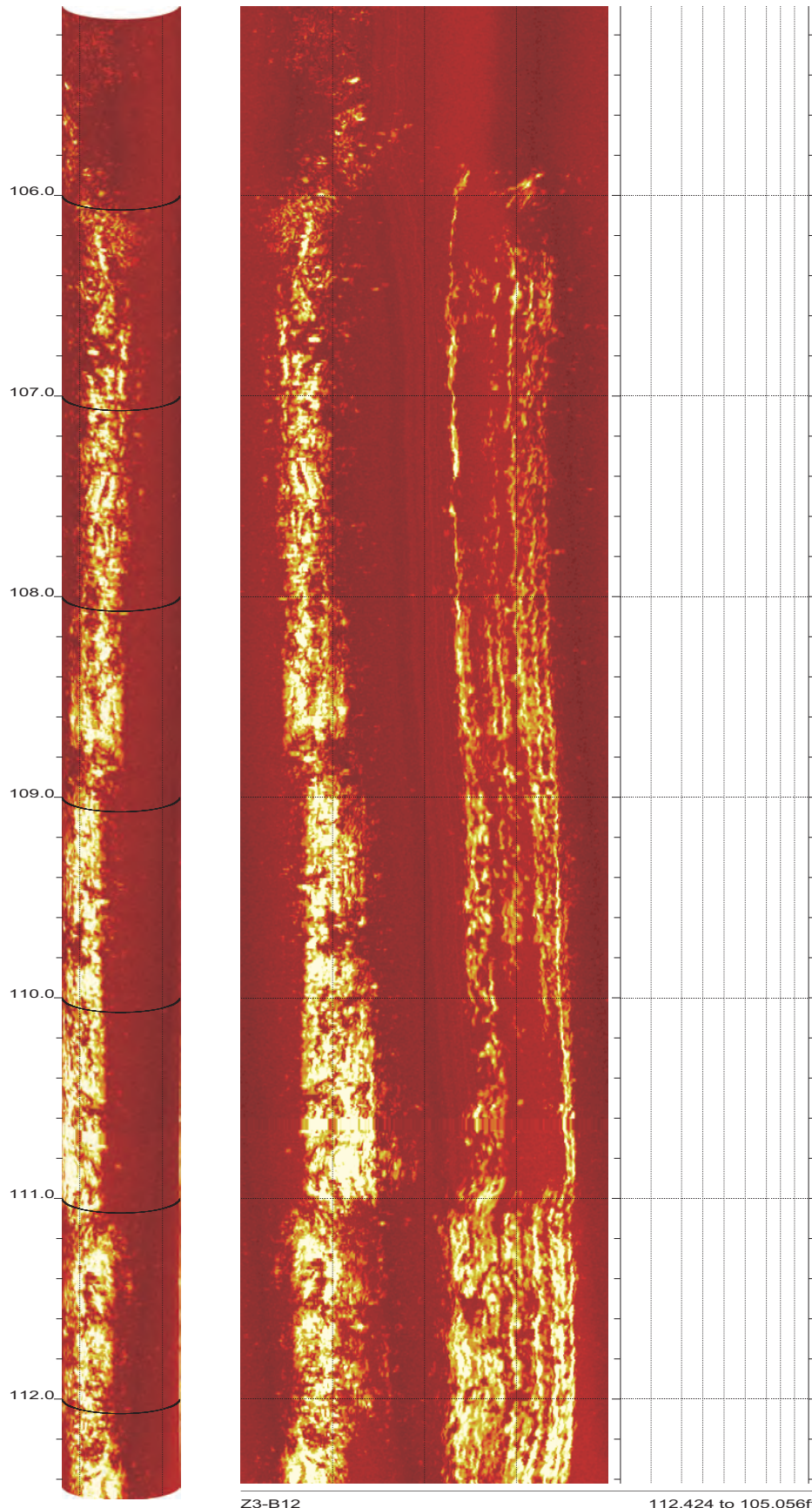


Z3-B12

105.056 to 97.688ft

7

SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 7 of 18

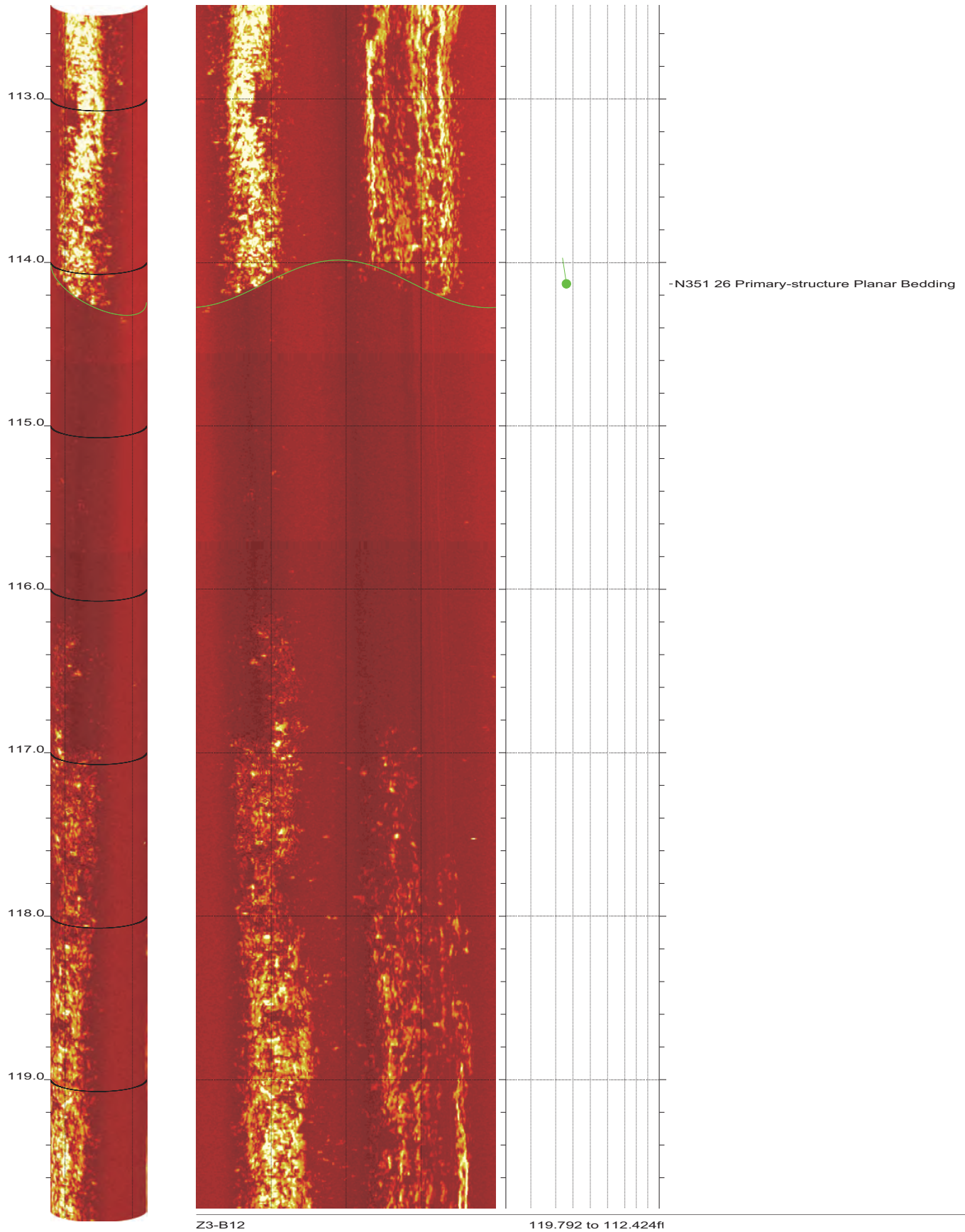


Z3-B12

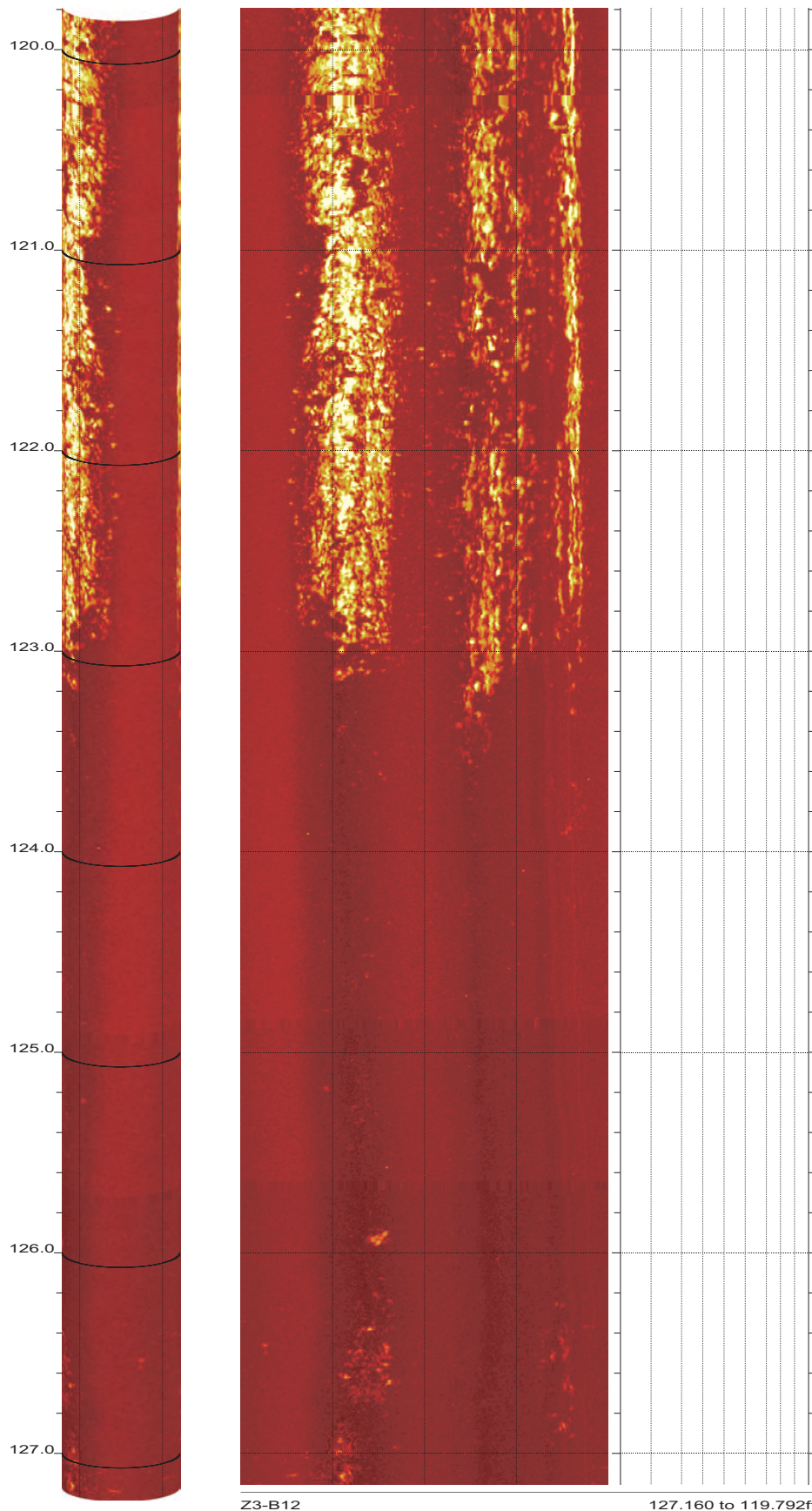
112.424 to 105.056ft

8

SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 8 of 18



SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 9 of 18

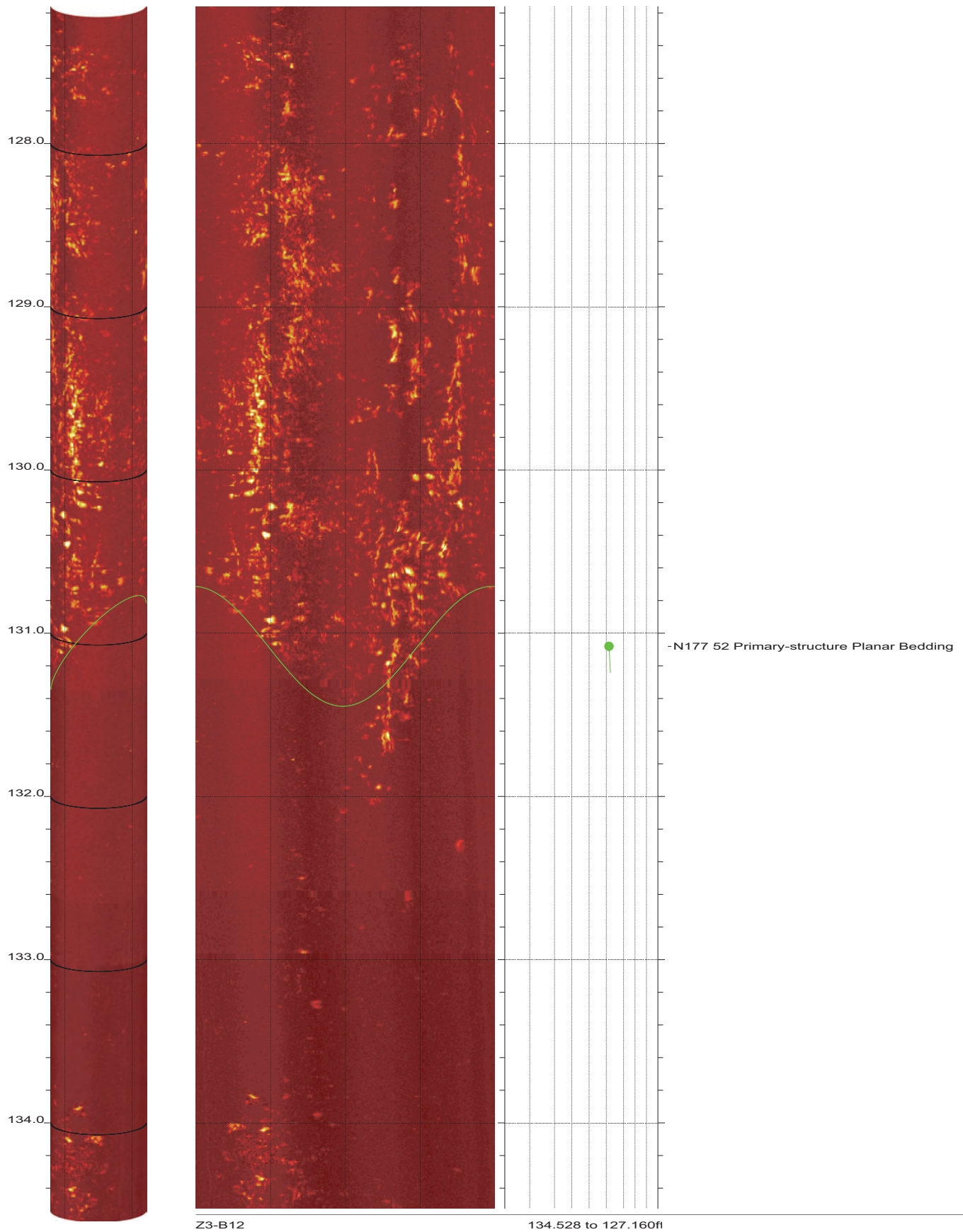


Z3-B12

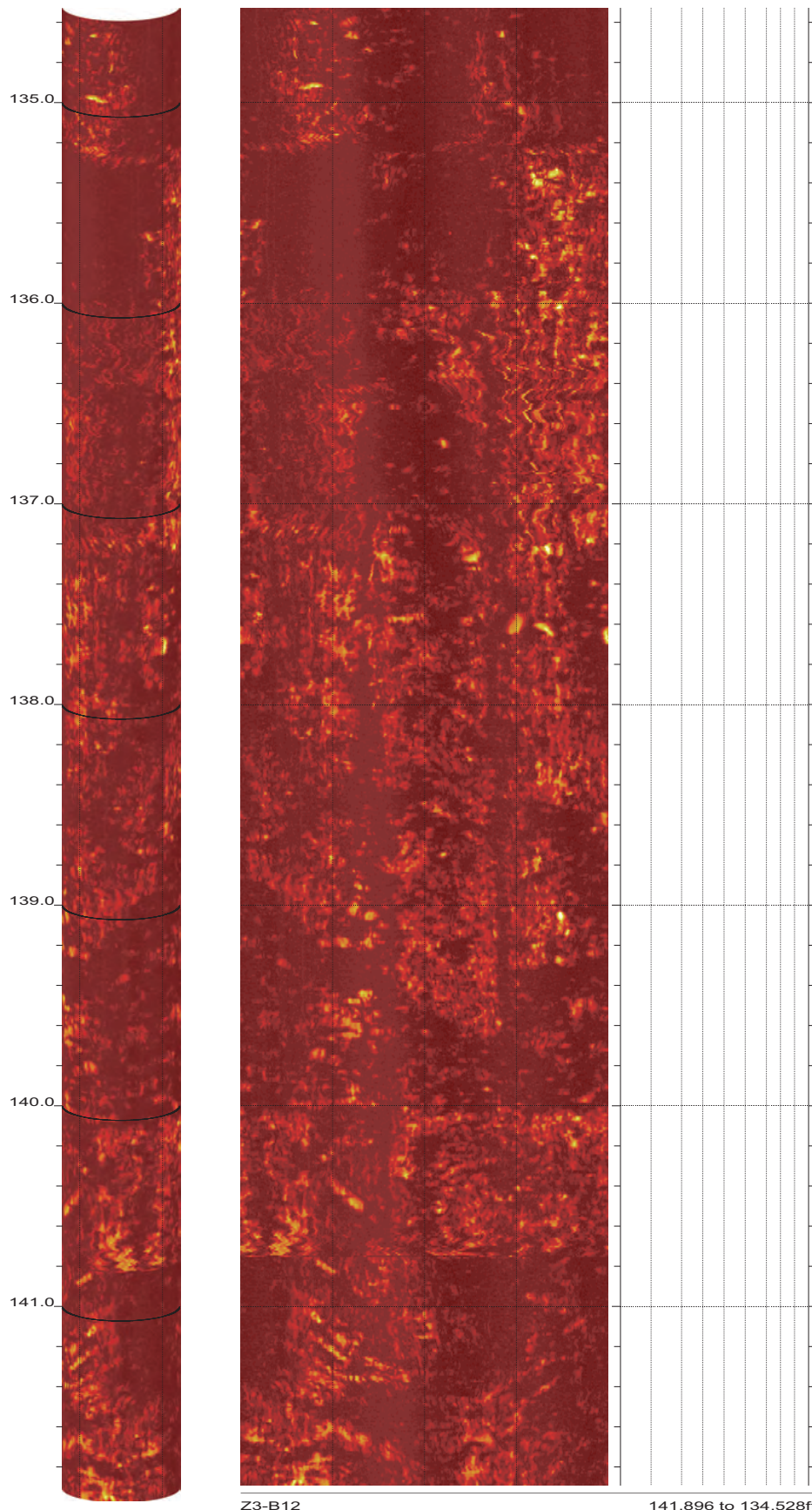
127.160 to 119.792ft

10

SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 10 of 18



SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 11 of 18



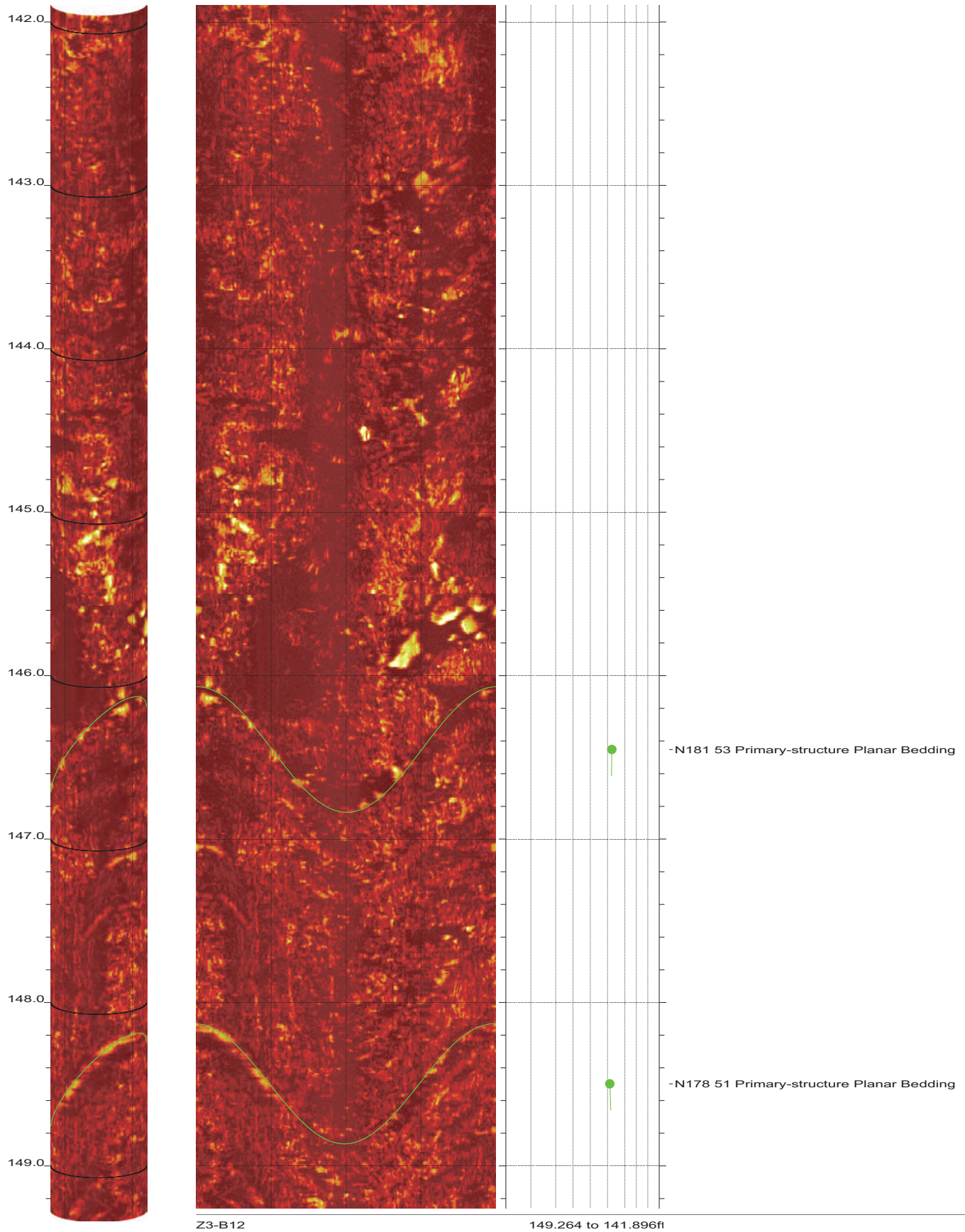
Z3-B12

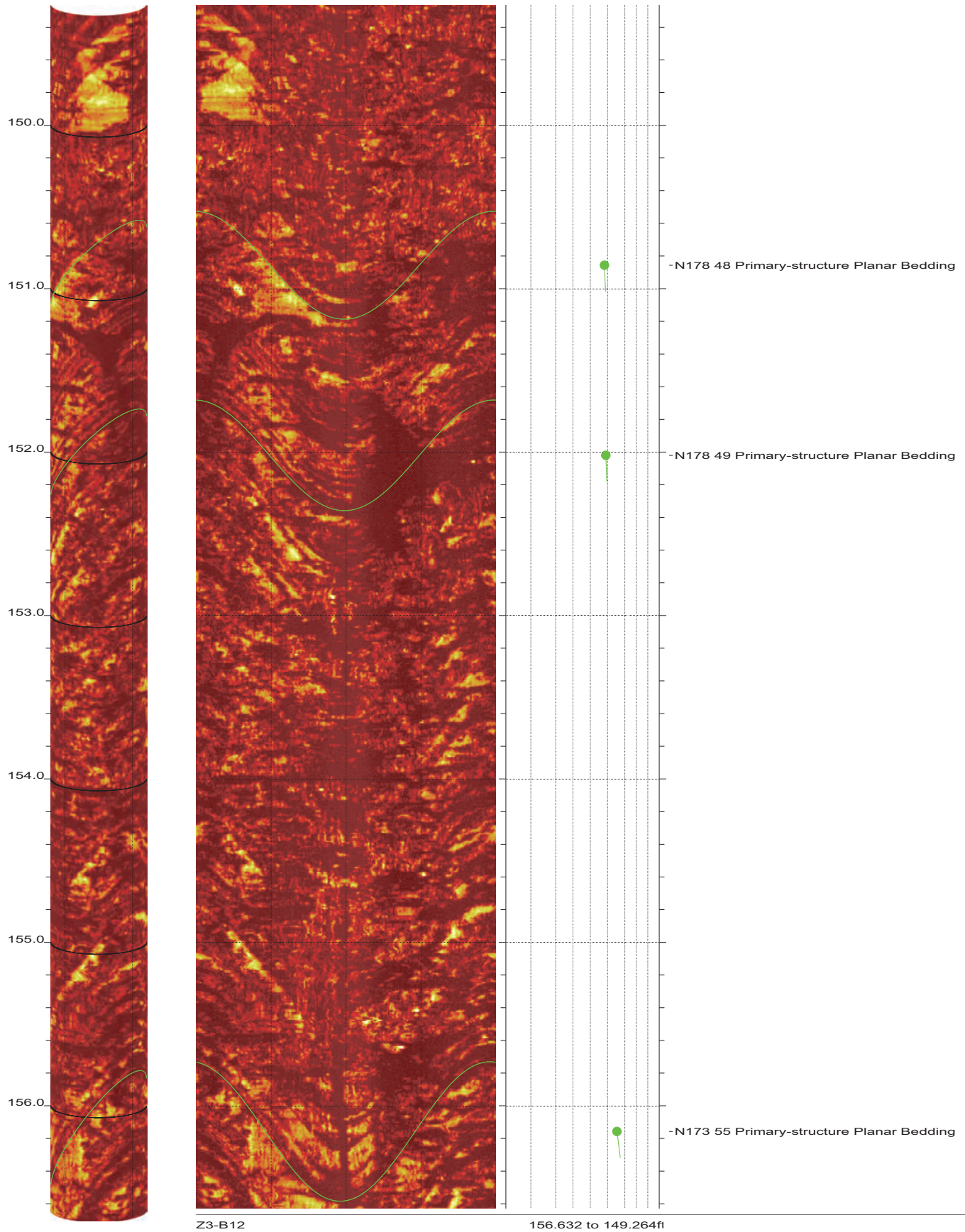
141.896 to 134.528ft

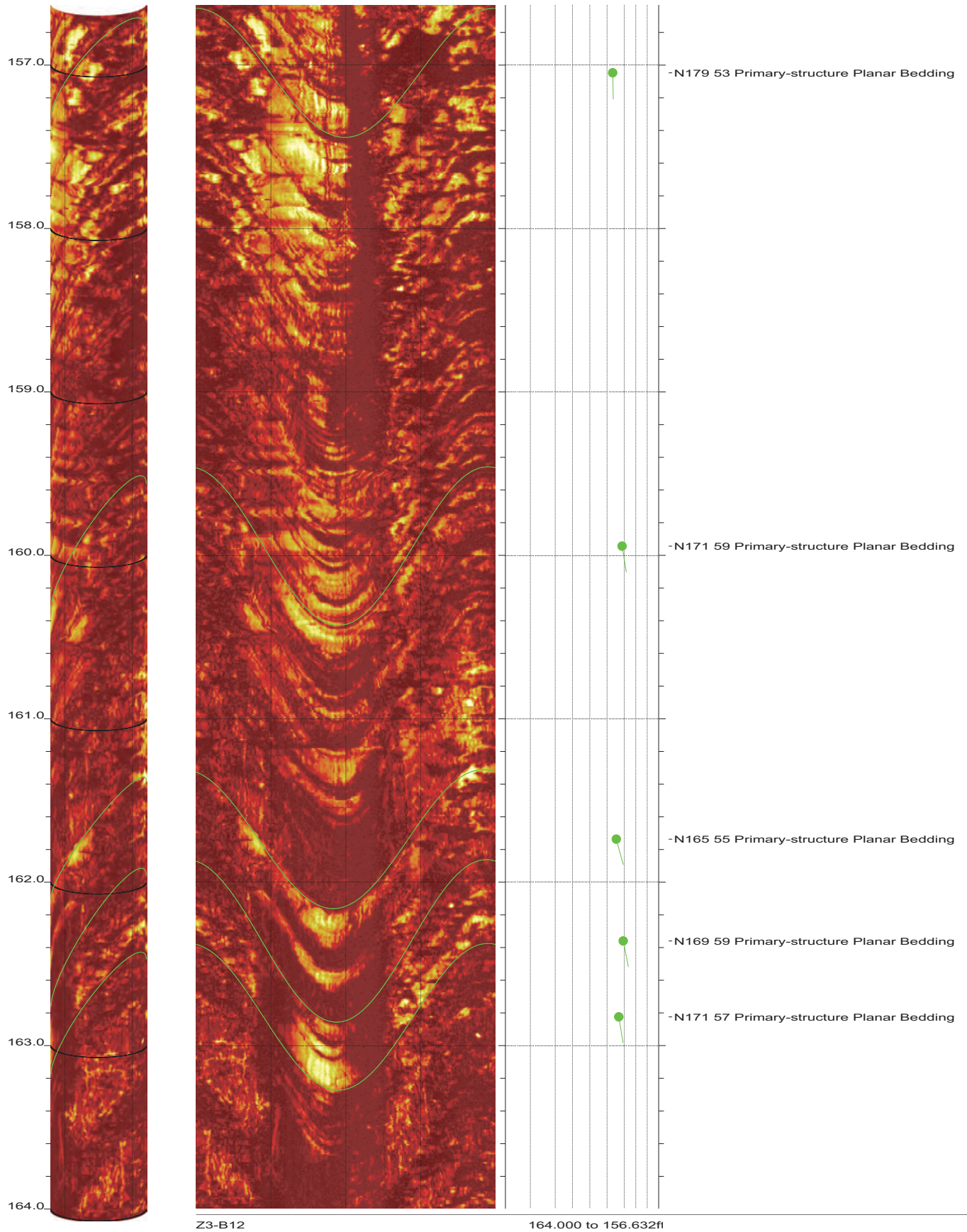
12

SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 12 of 18

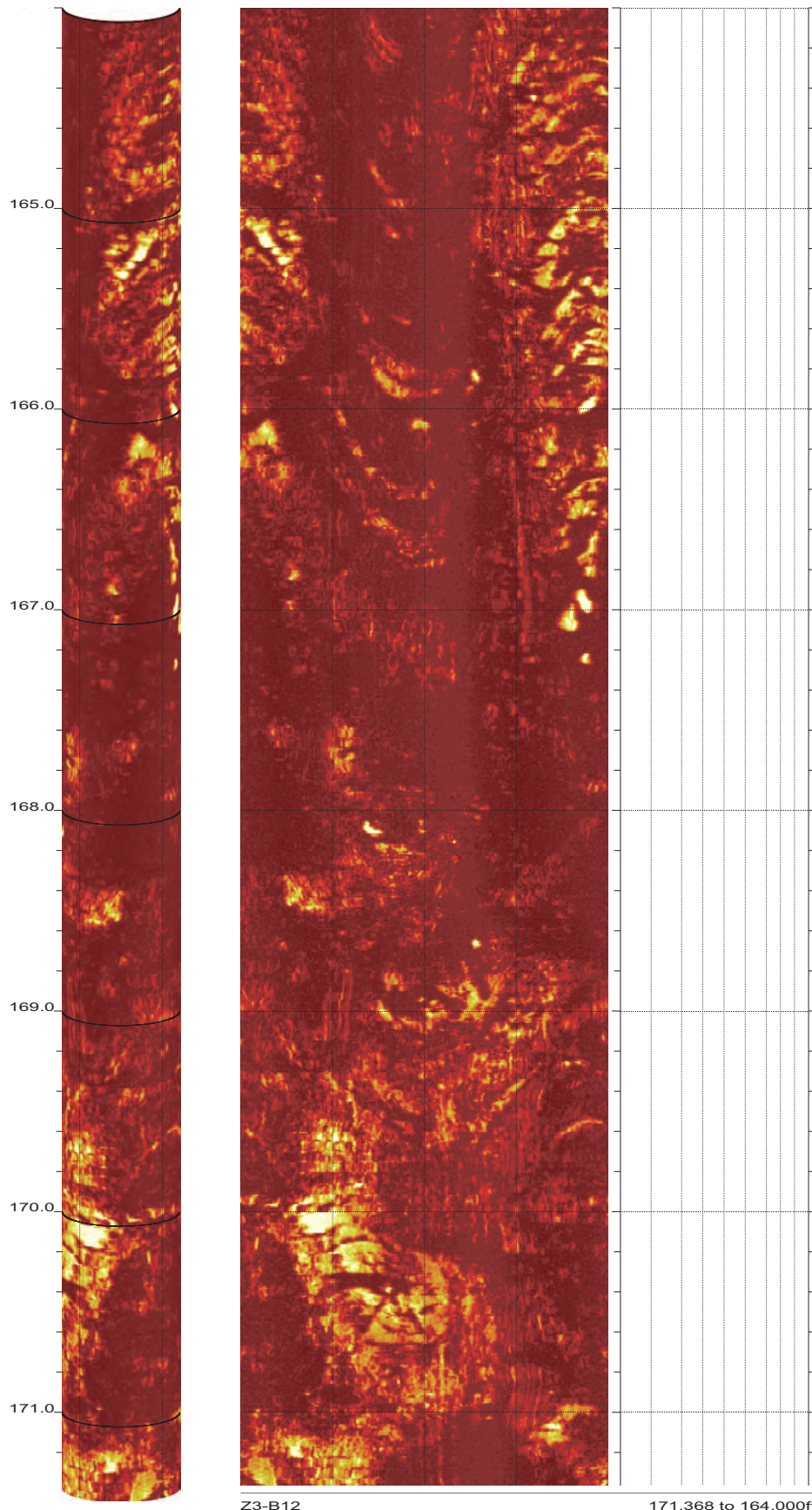








SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 15 of 18

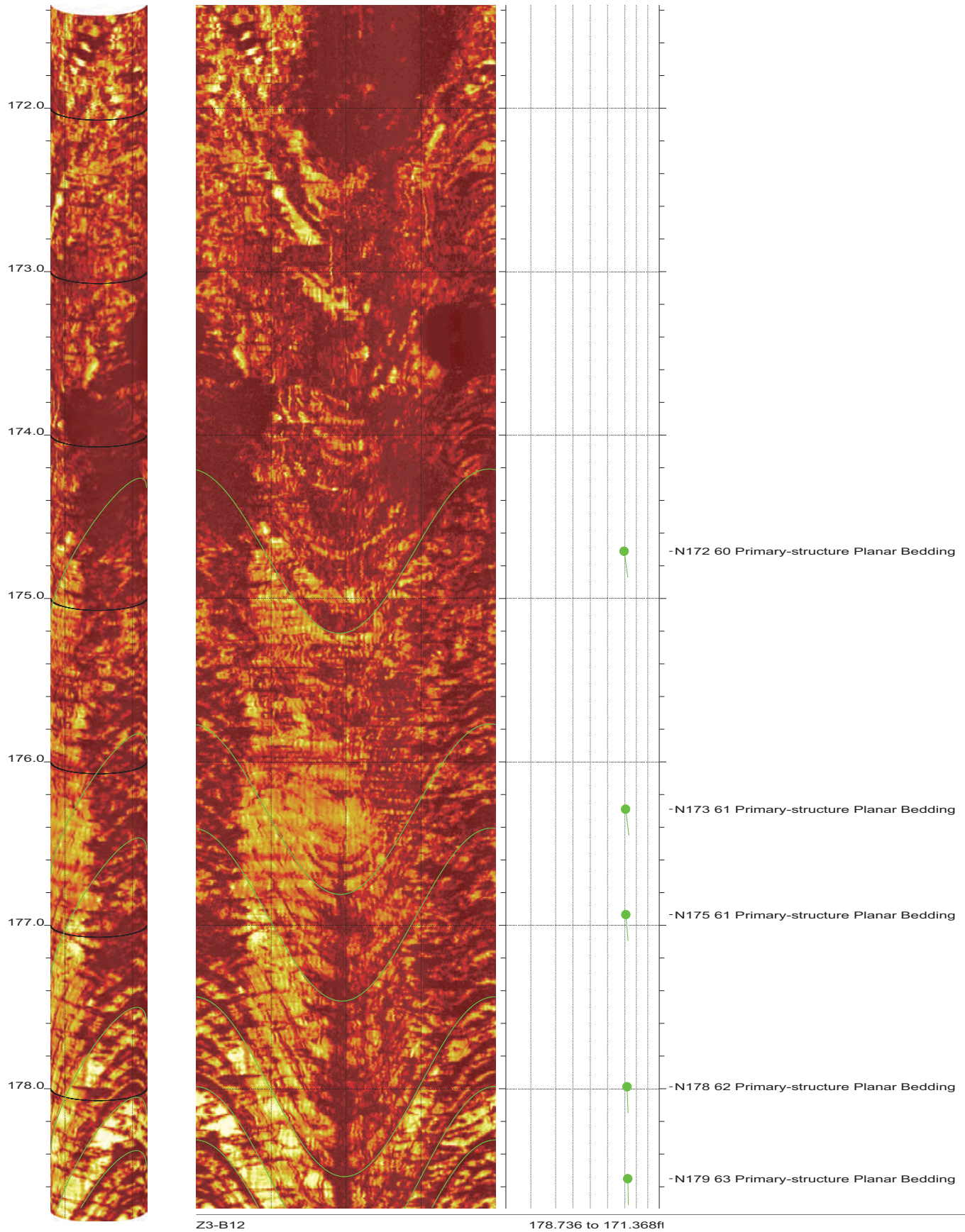


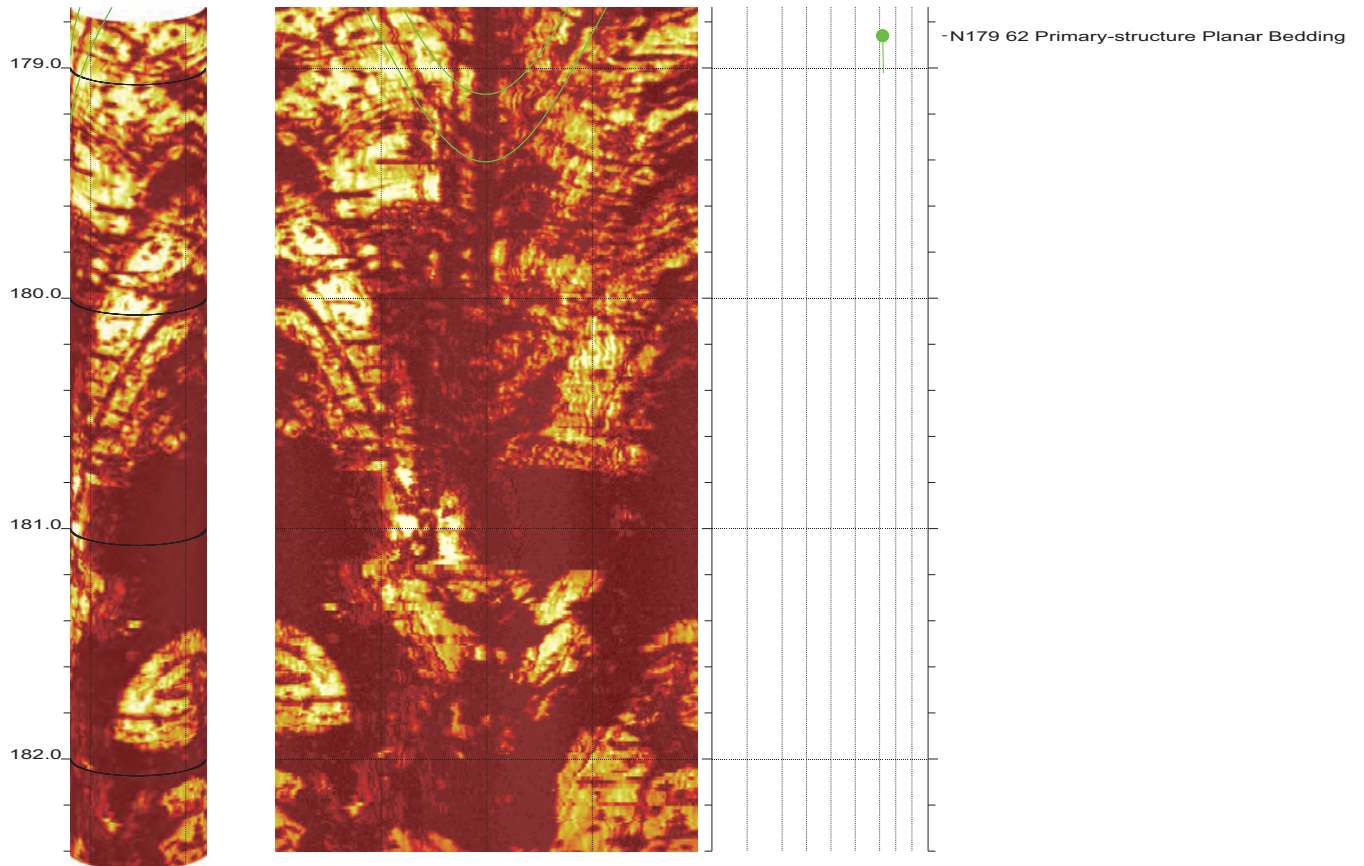
Z3-B12

171.368 to 164.000ft

16

SR-710 Boring Z3-B12 Acoustic Televiewer Dips rev 1 Sheet 16 of 18







CASCADE DRILLING

Borehole: Z4-B4

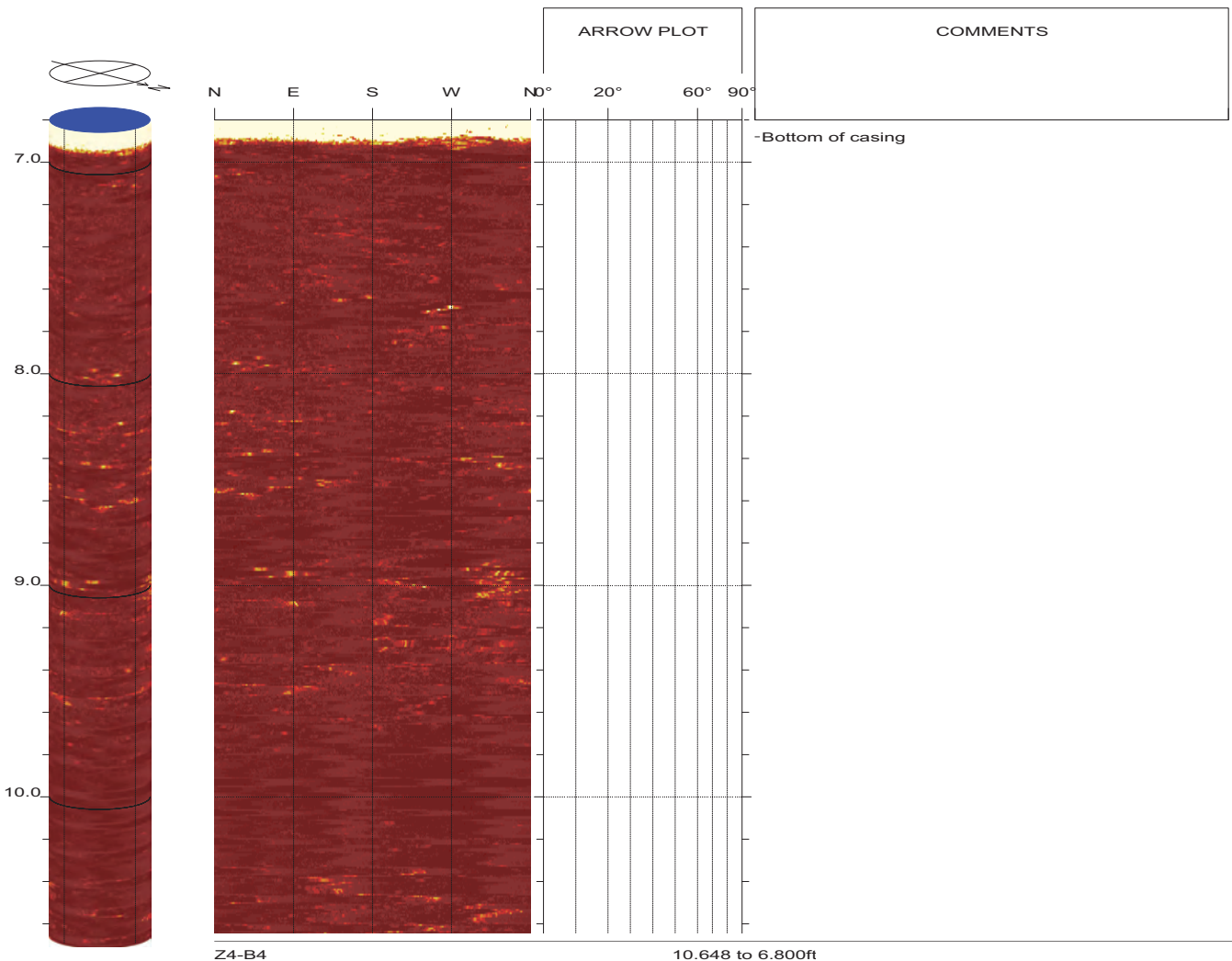
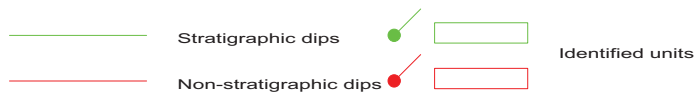
SR-710 TUNNEL INVESTIGATION

top of borehole.....  
 East: \_  
 North: \_  
 Elev: \_

North ref. is true  
 Depth units are feet  
 Vertical scale: 1/10  
 Horiz scale = 1.00x Vert scale

Zone from 275.000 to 6.800ft  
 Format: BHTV-NESWN

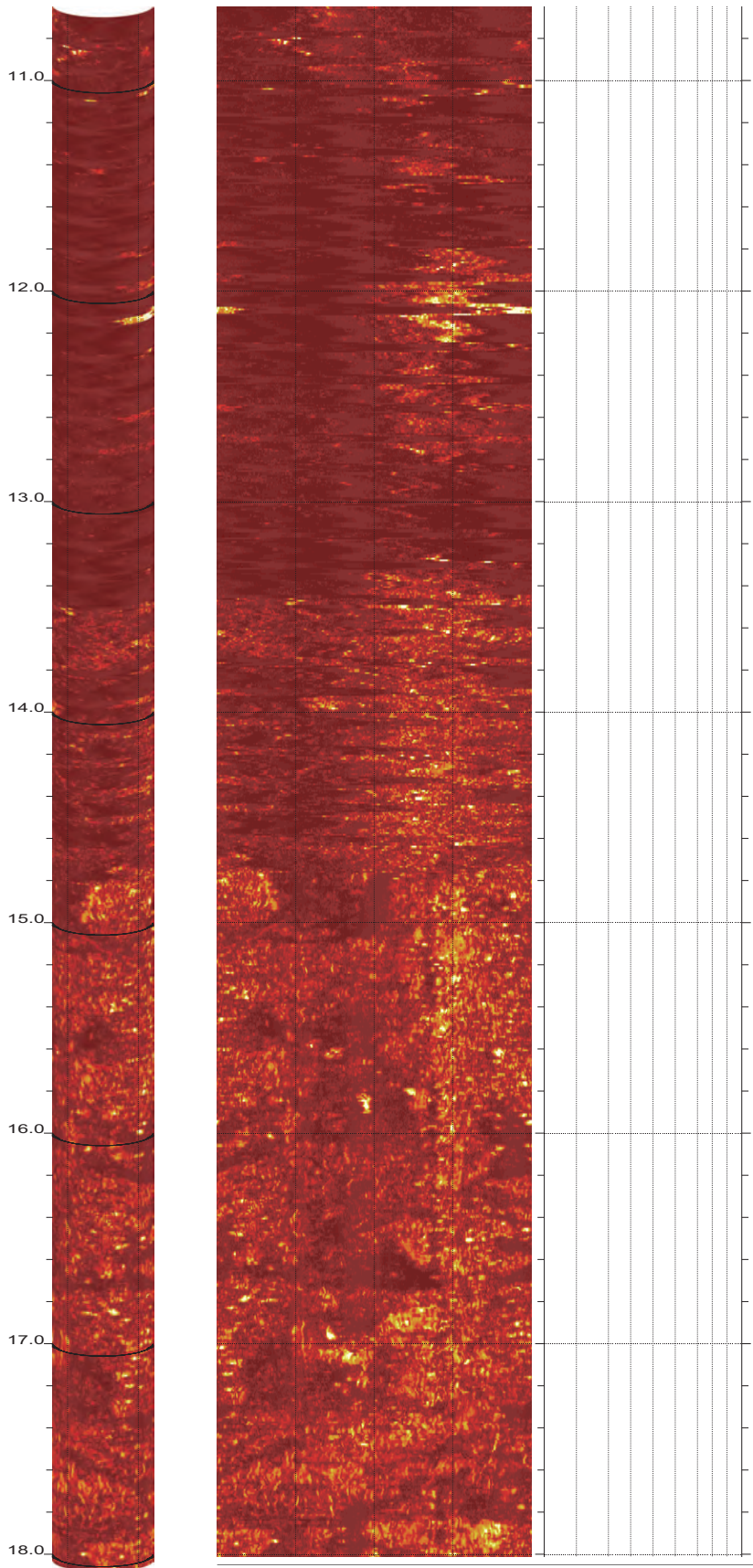
Borehole diam: 5.700inch  
 Vertical = borehole-axis  
 Image: Amplitude



Z4-B4

10.648 to 6.800ft

1



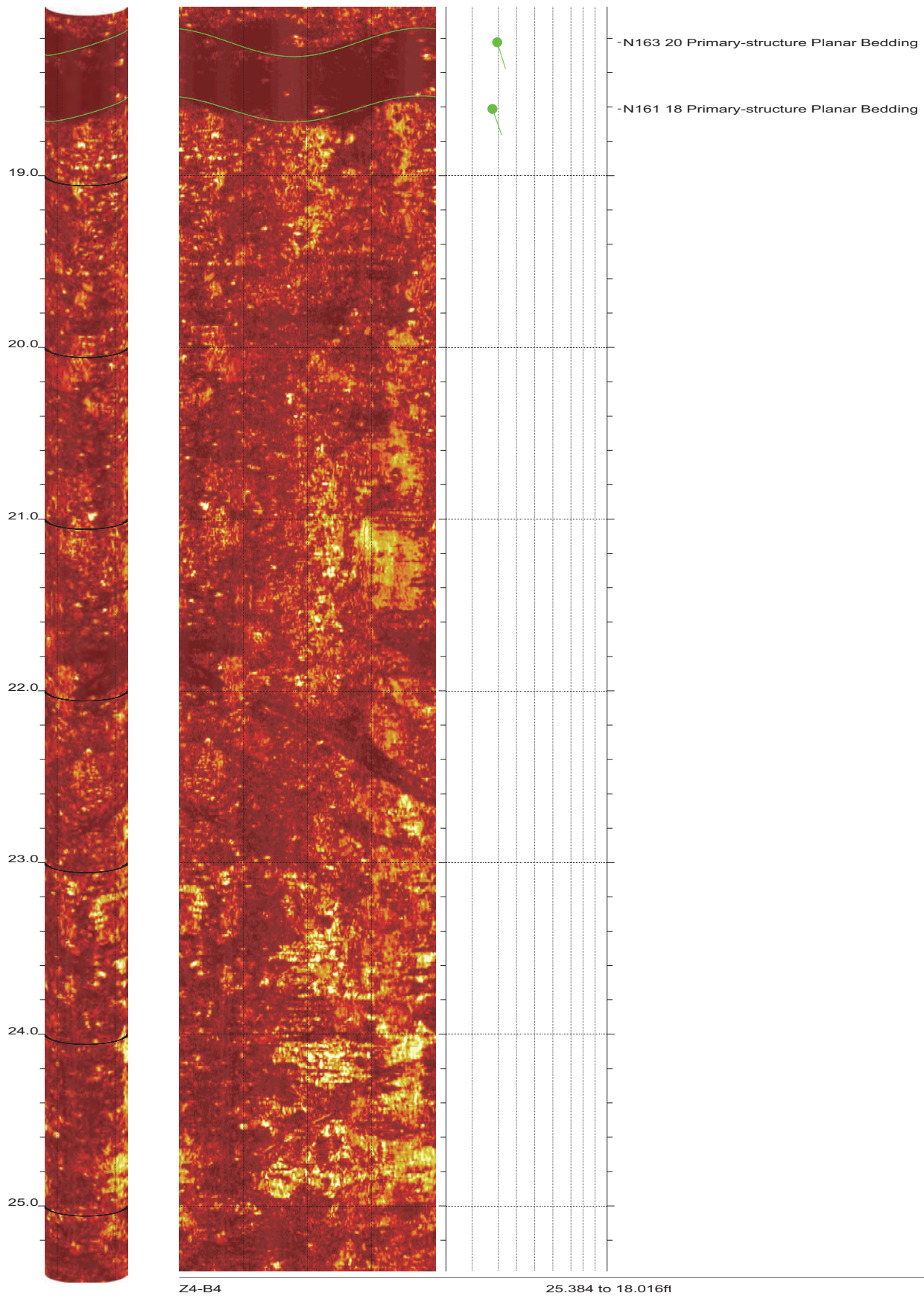
Z4-B4

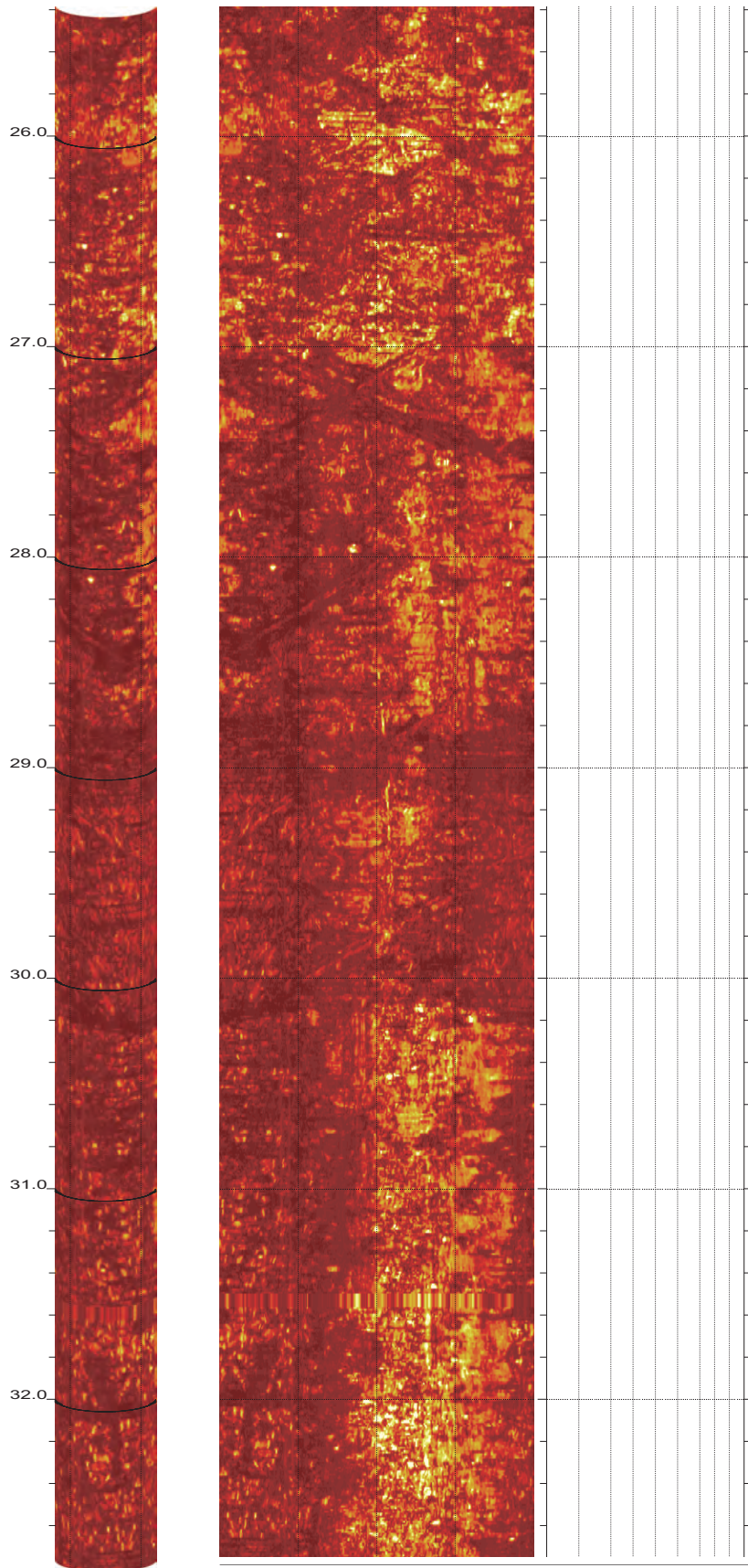
18.016 to 10.648ft

2

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 2 of 37





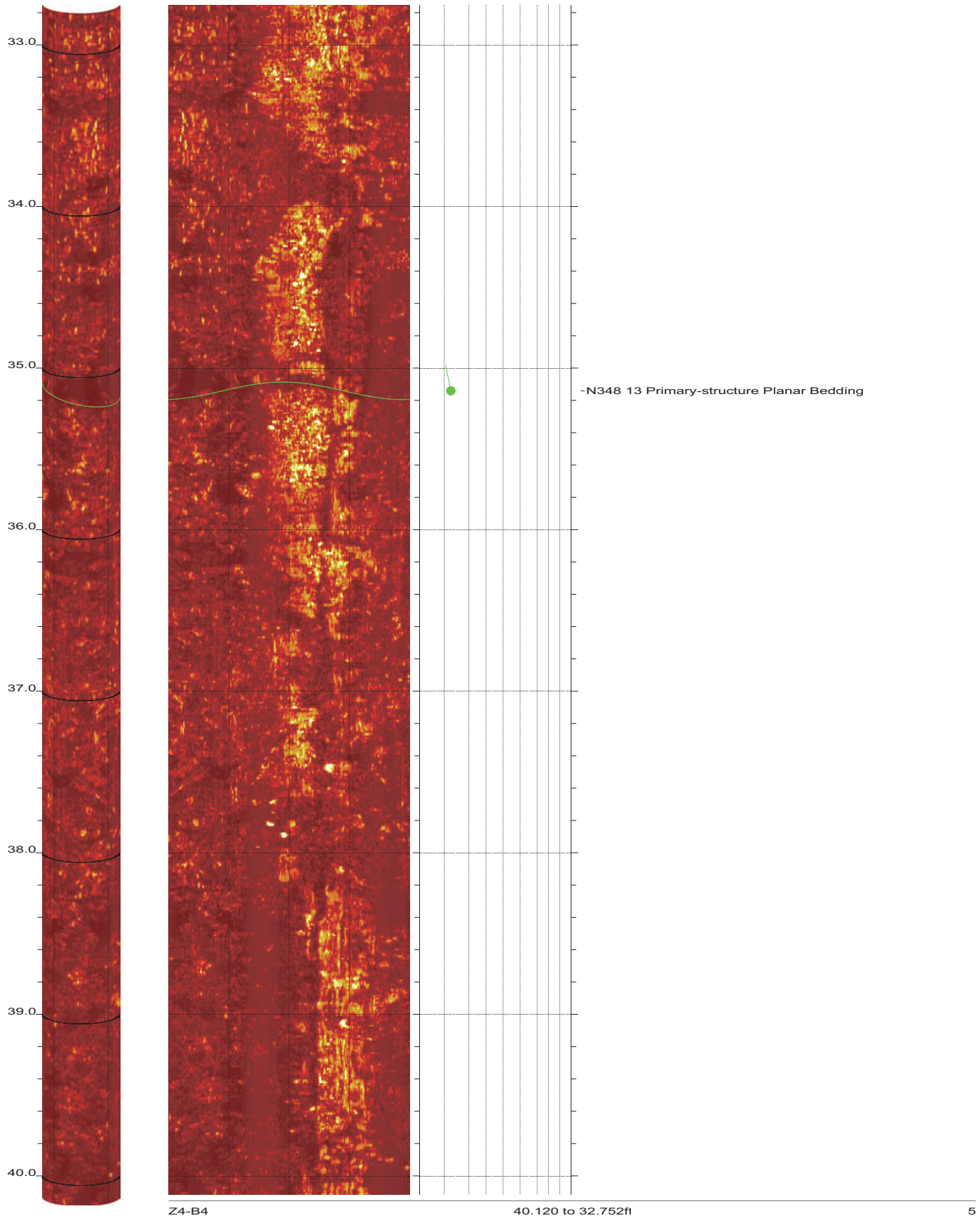


Z4-B4

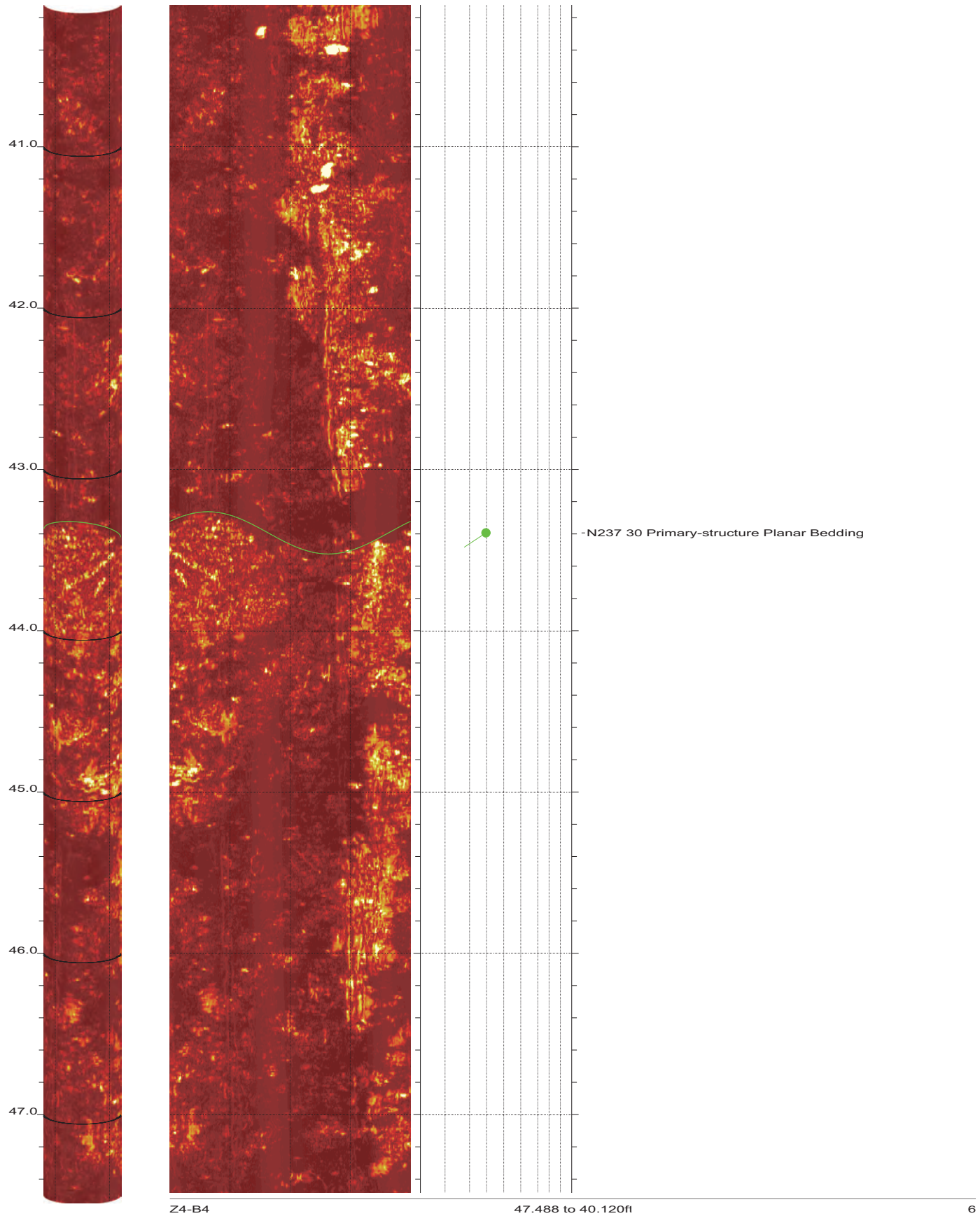
32.752 to 25.384ft

4

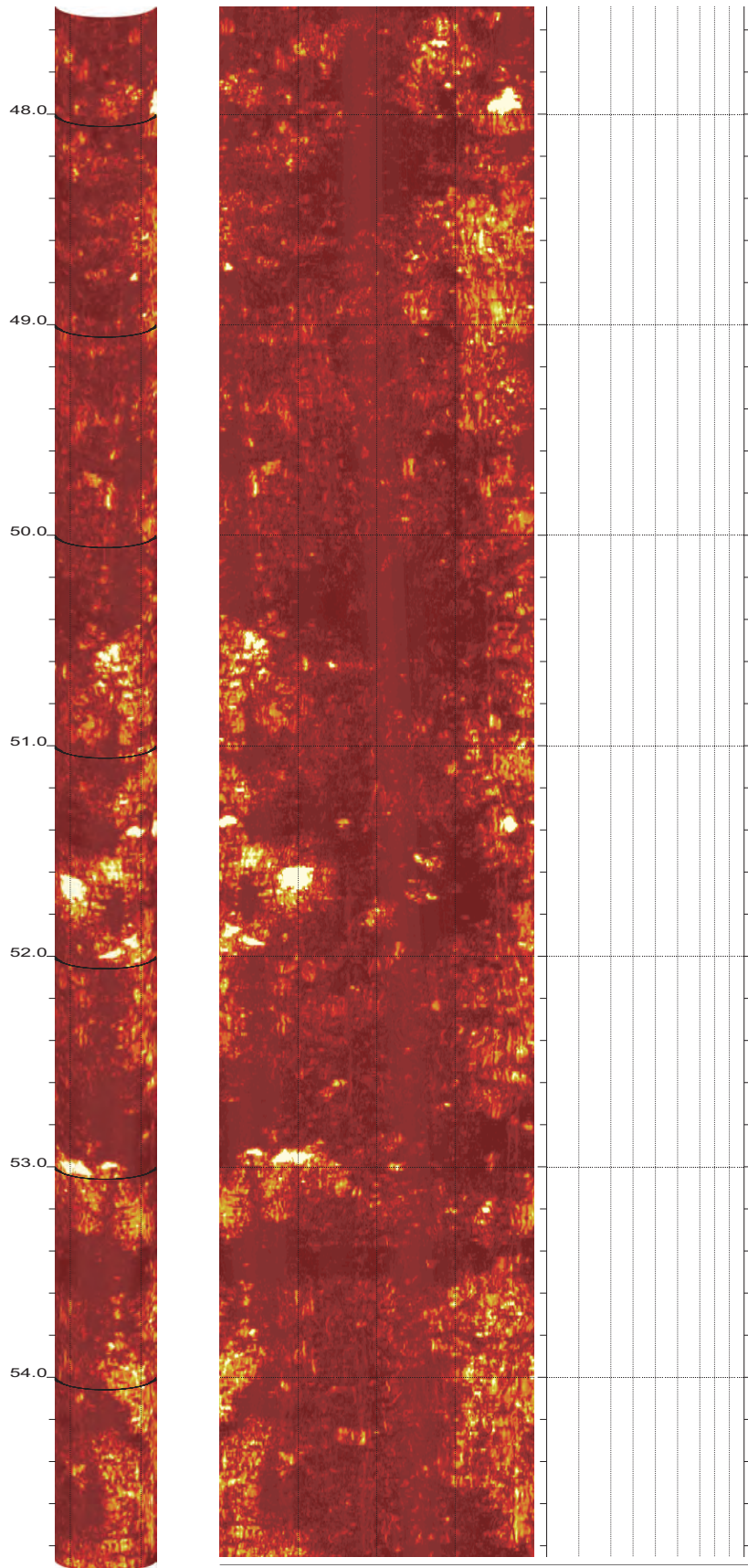
SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 4 of 37



SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 5 of 37



SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 6 of 37

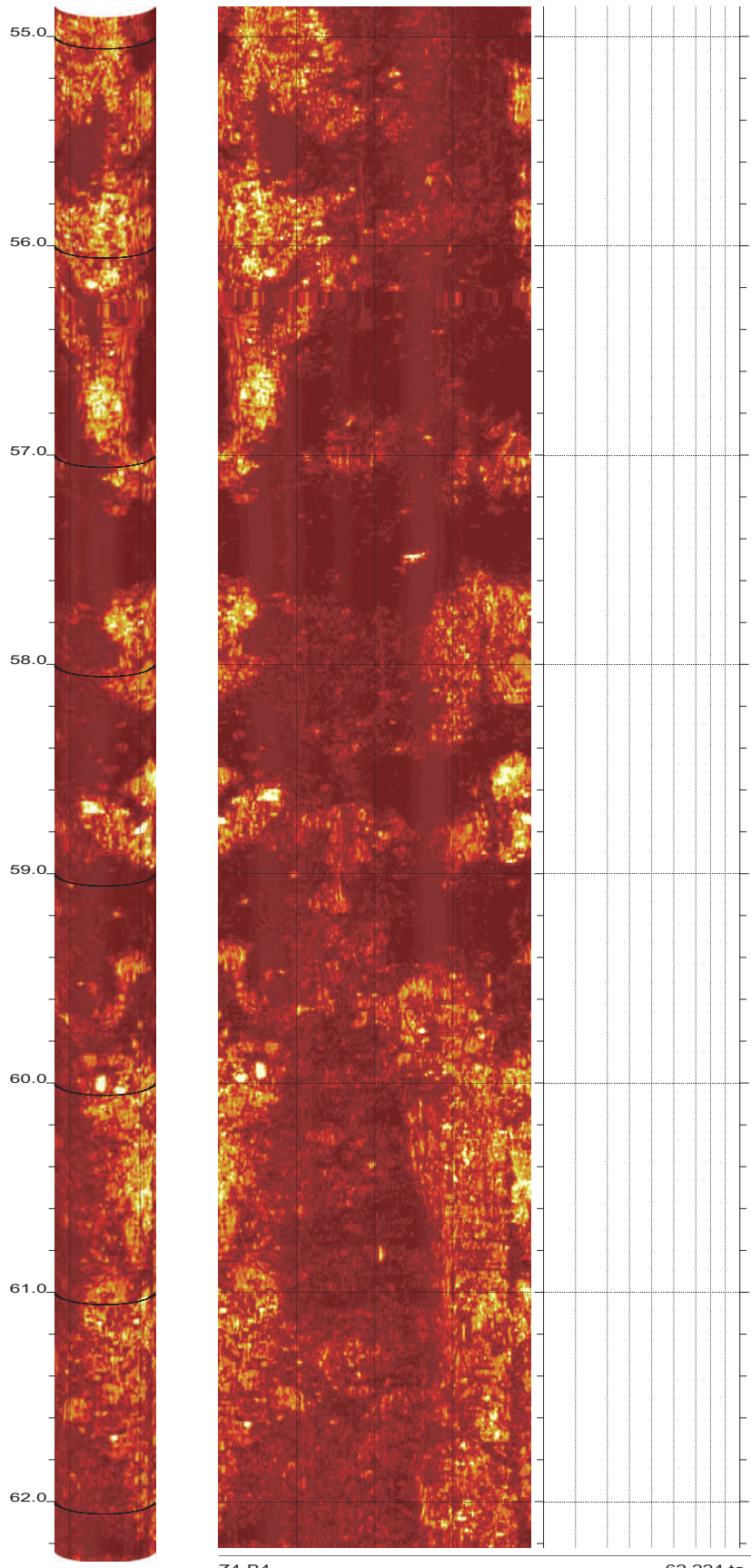


Z4-B4

54.856 to 47.488ft

7

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 7 of 37

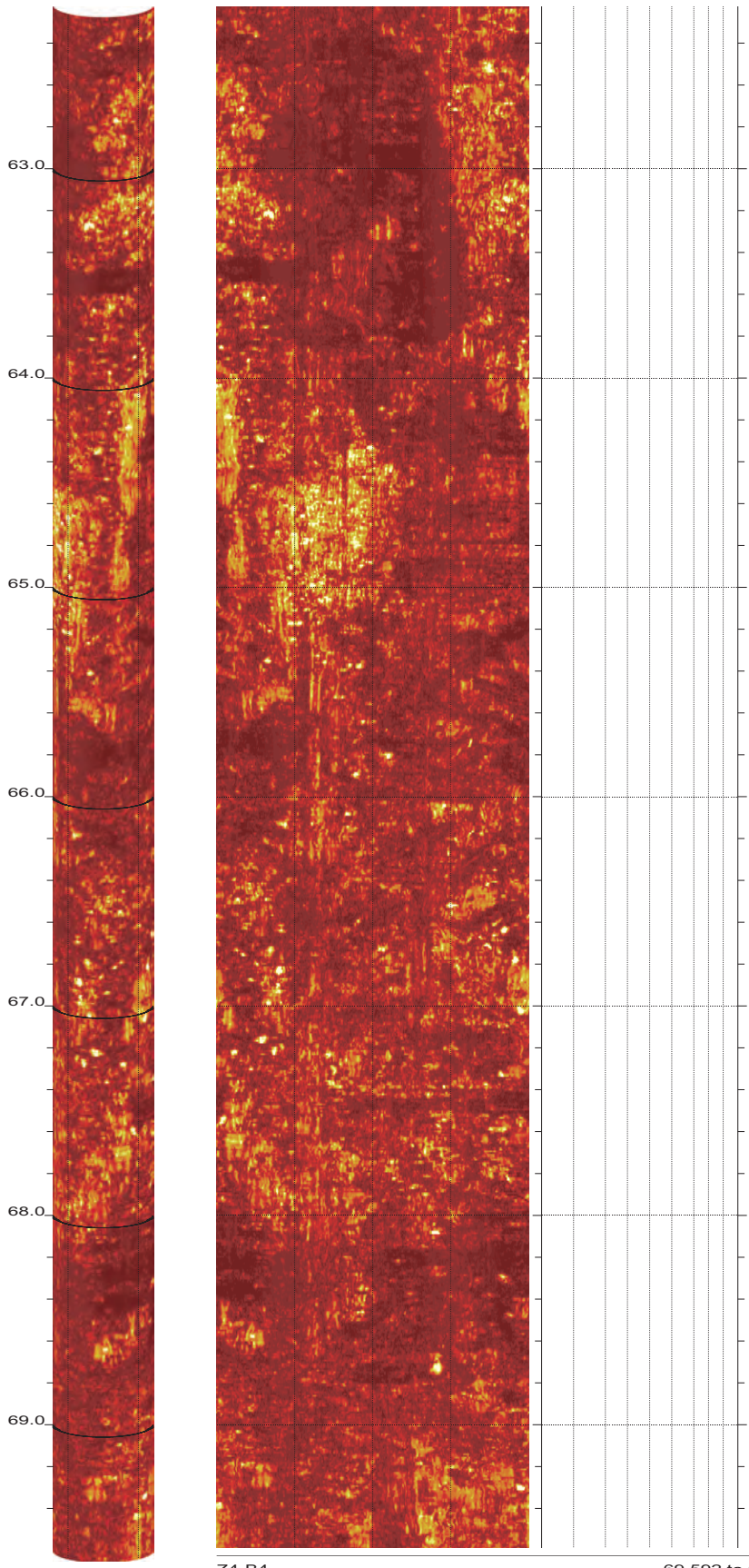


Z4-B4

62.224 to 54.856ft

8

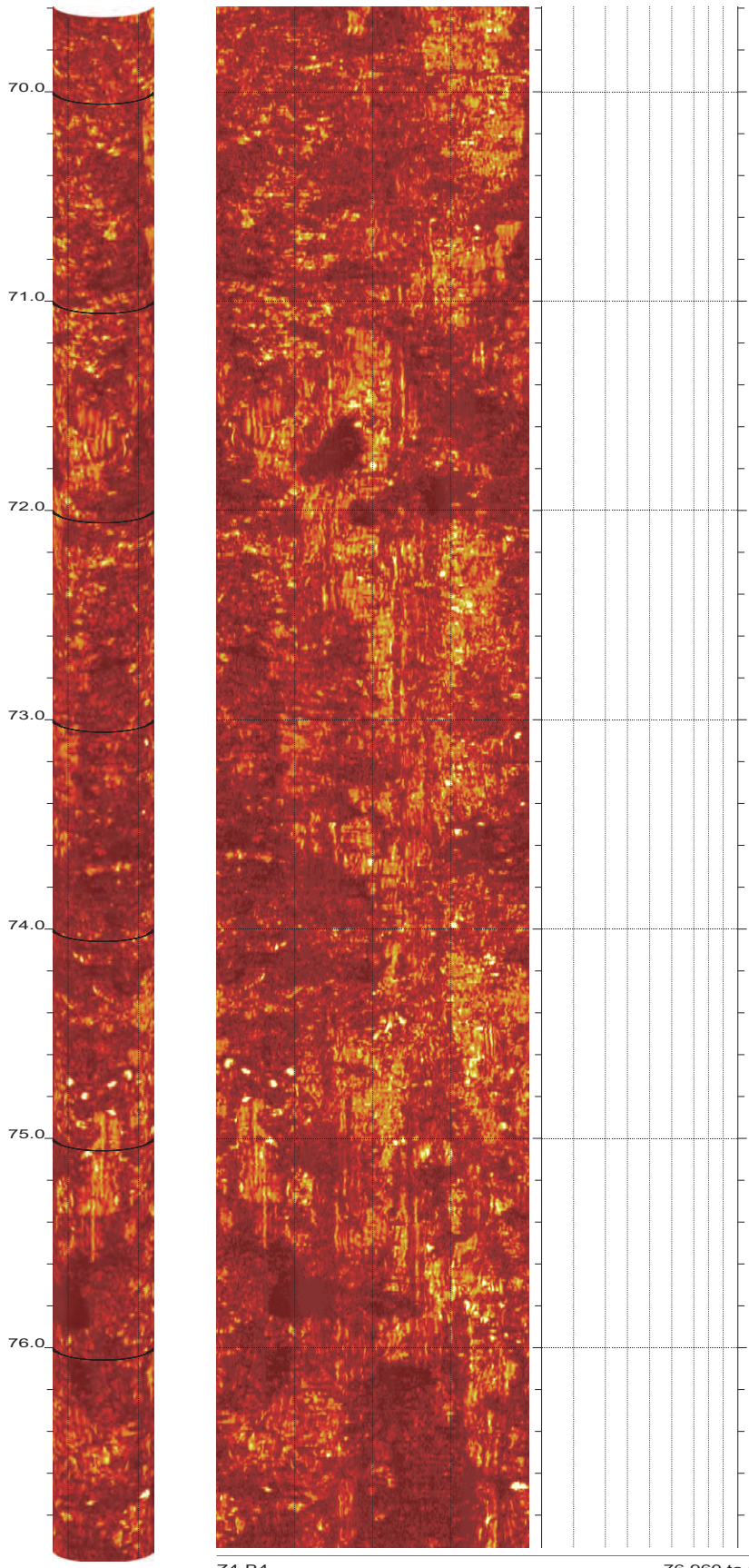
SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 8 of 37



Z4-B4

69.592 to 62.224ft

9



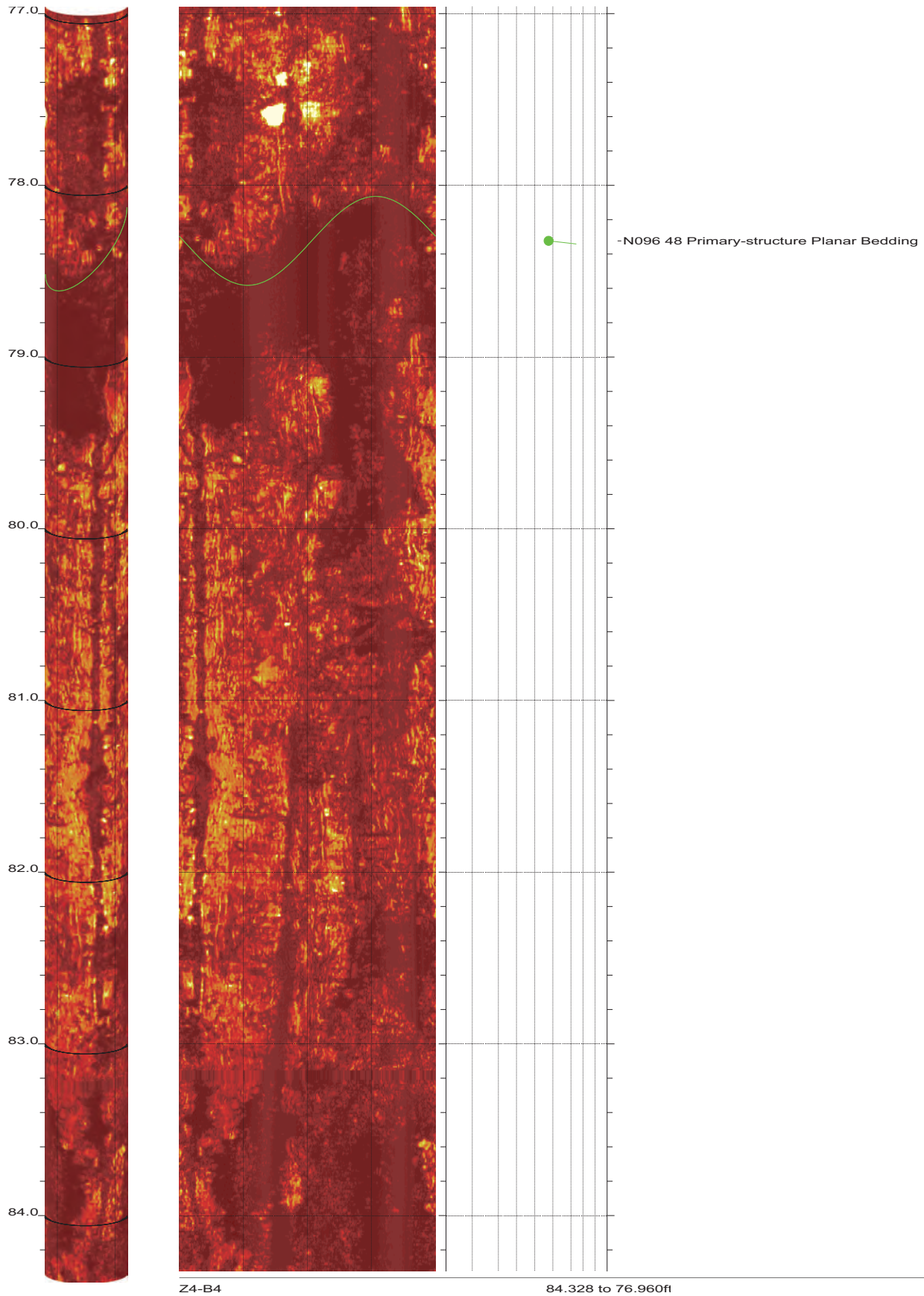
Z4-B4

76.960 to 69.592ft

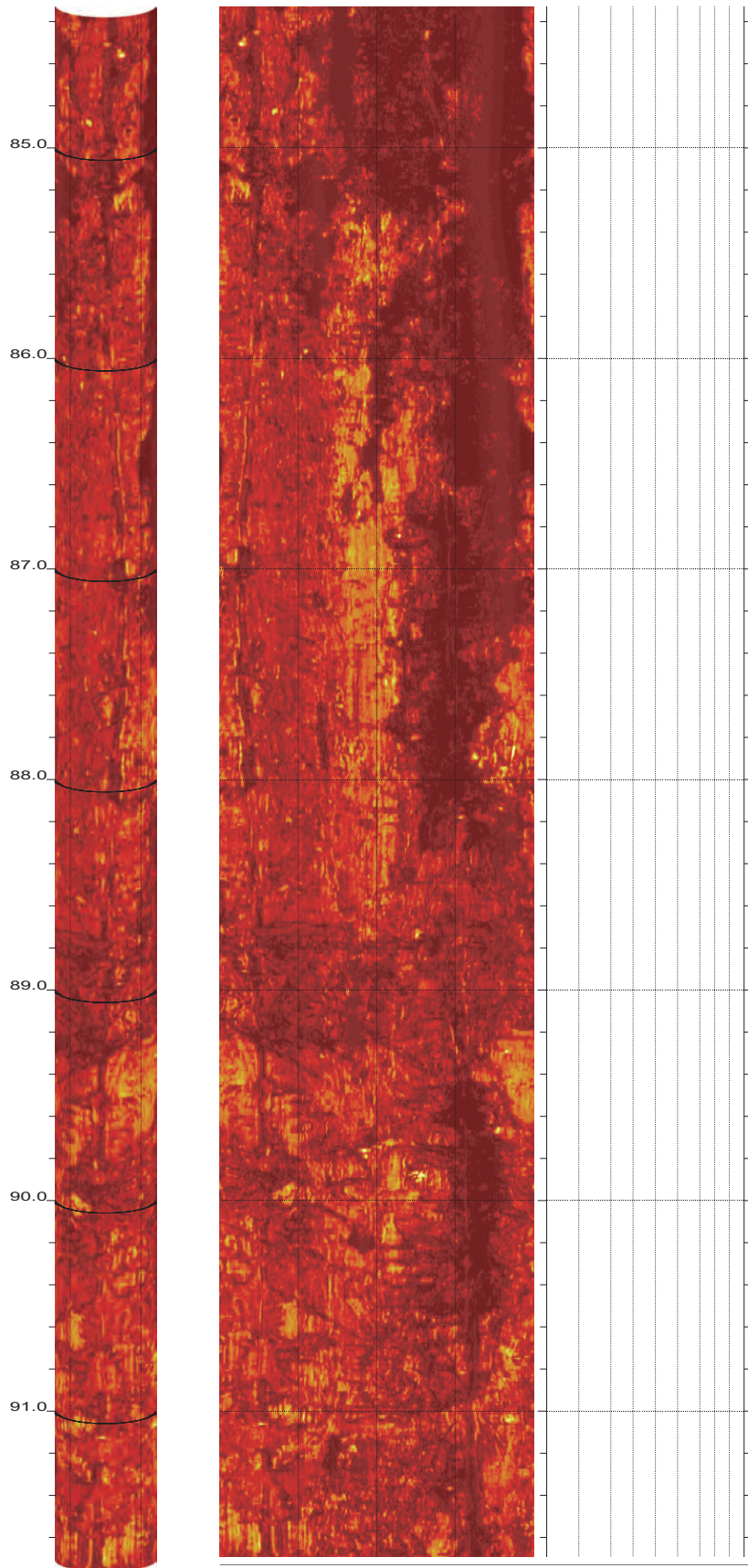
10

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 10 of 37





SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 11 of 37

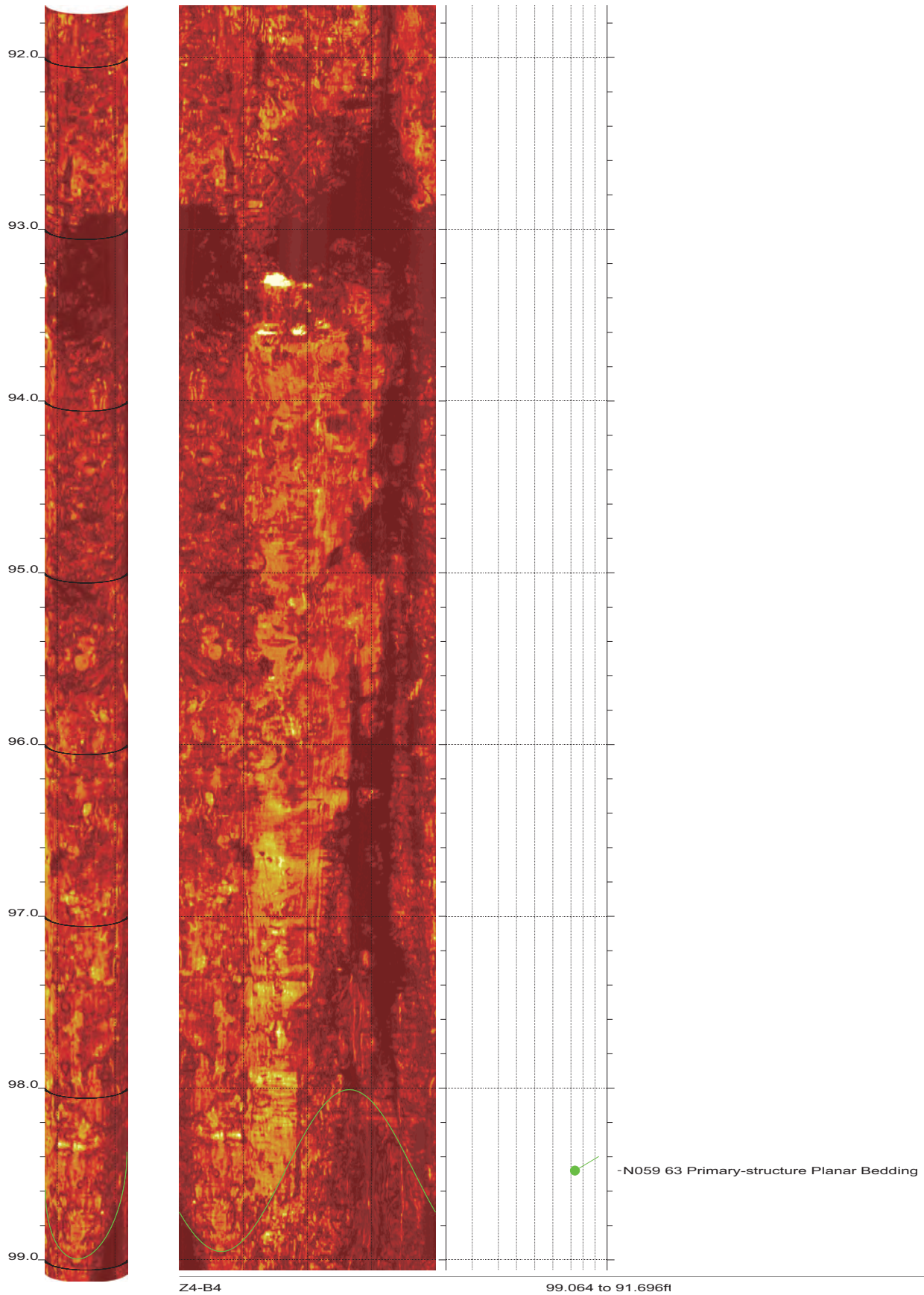


Z4-B4

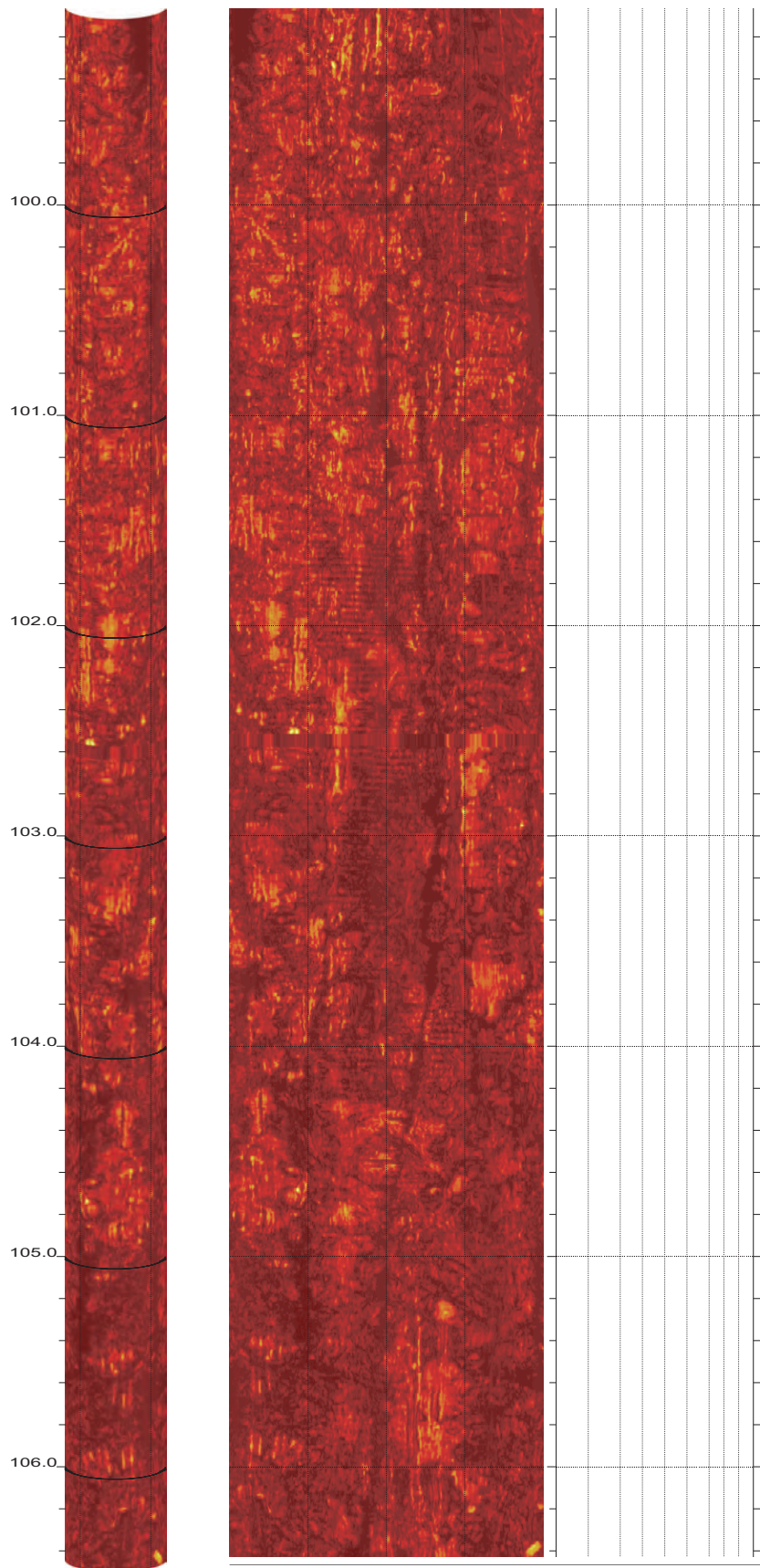
91.696 to 84.328ft

12

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 12 of 37



SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 13 of 37

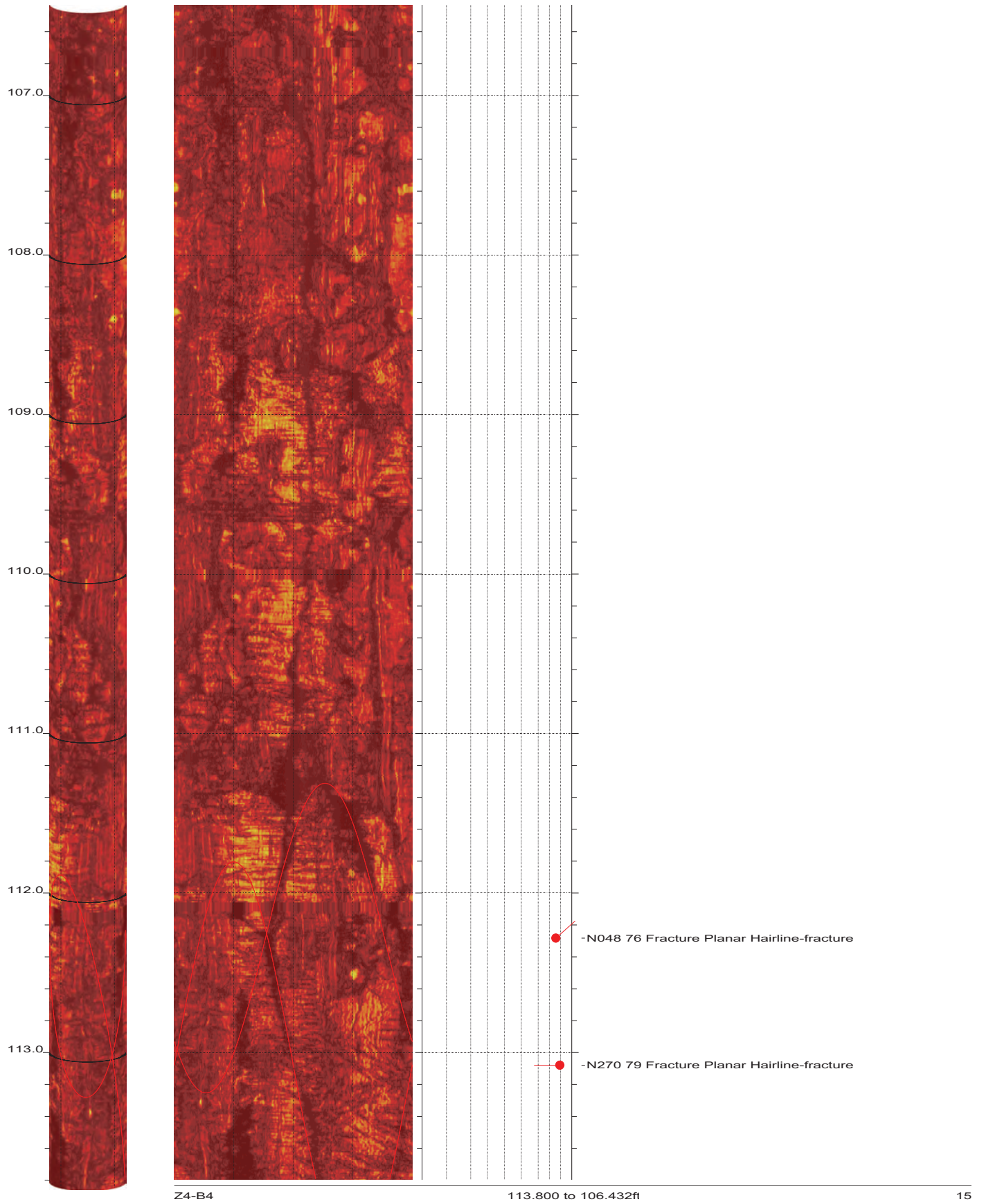


Z4-B4

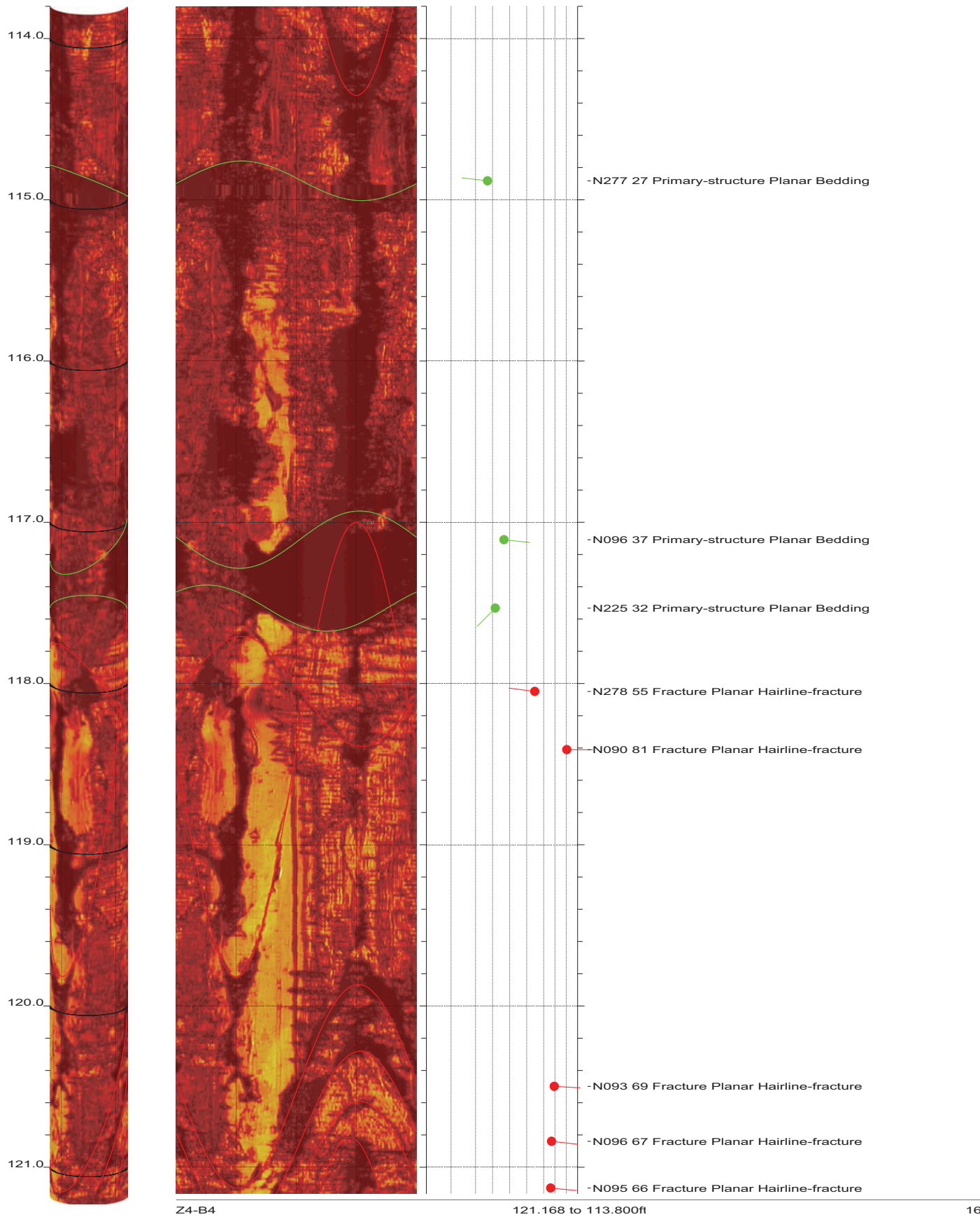
106.432 to 99.064ft

14

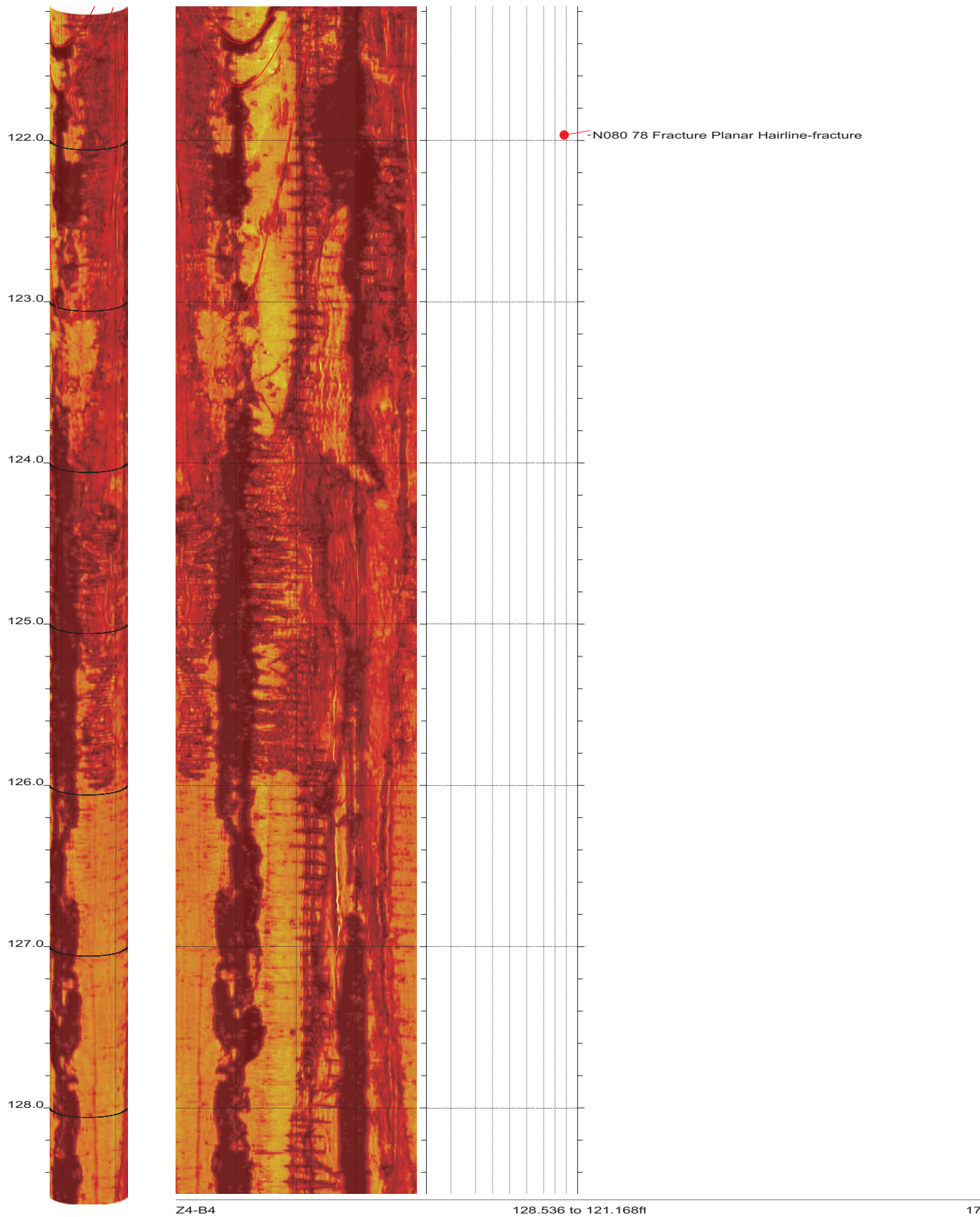
SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 14 of 37



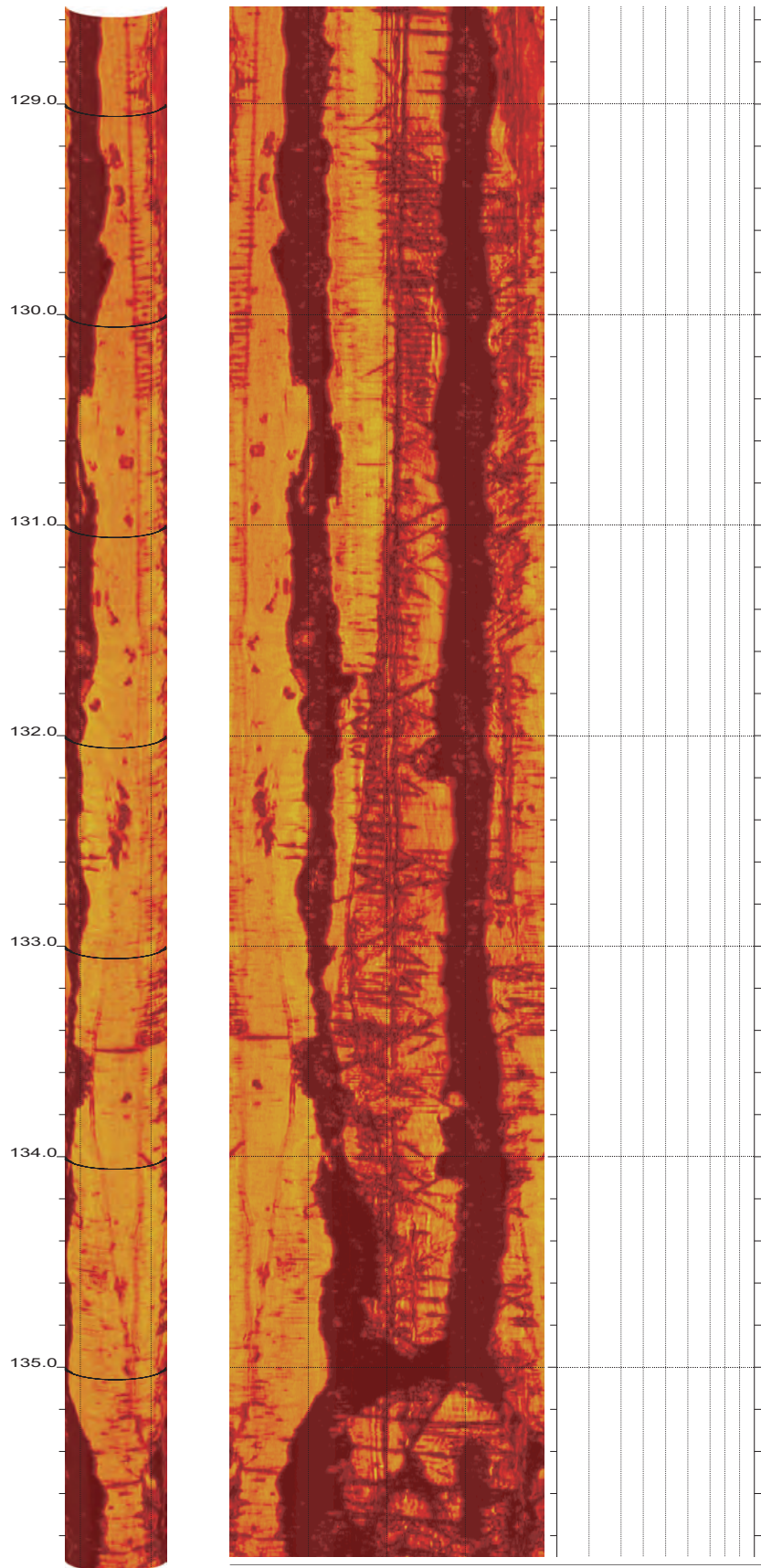
SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 15 of 37



SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 16 of 37



SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 17 of 37



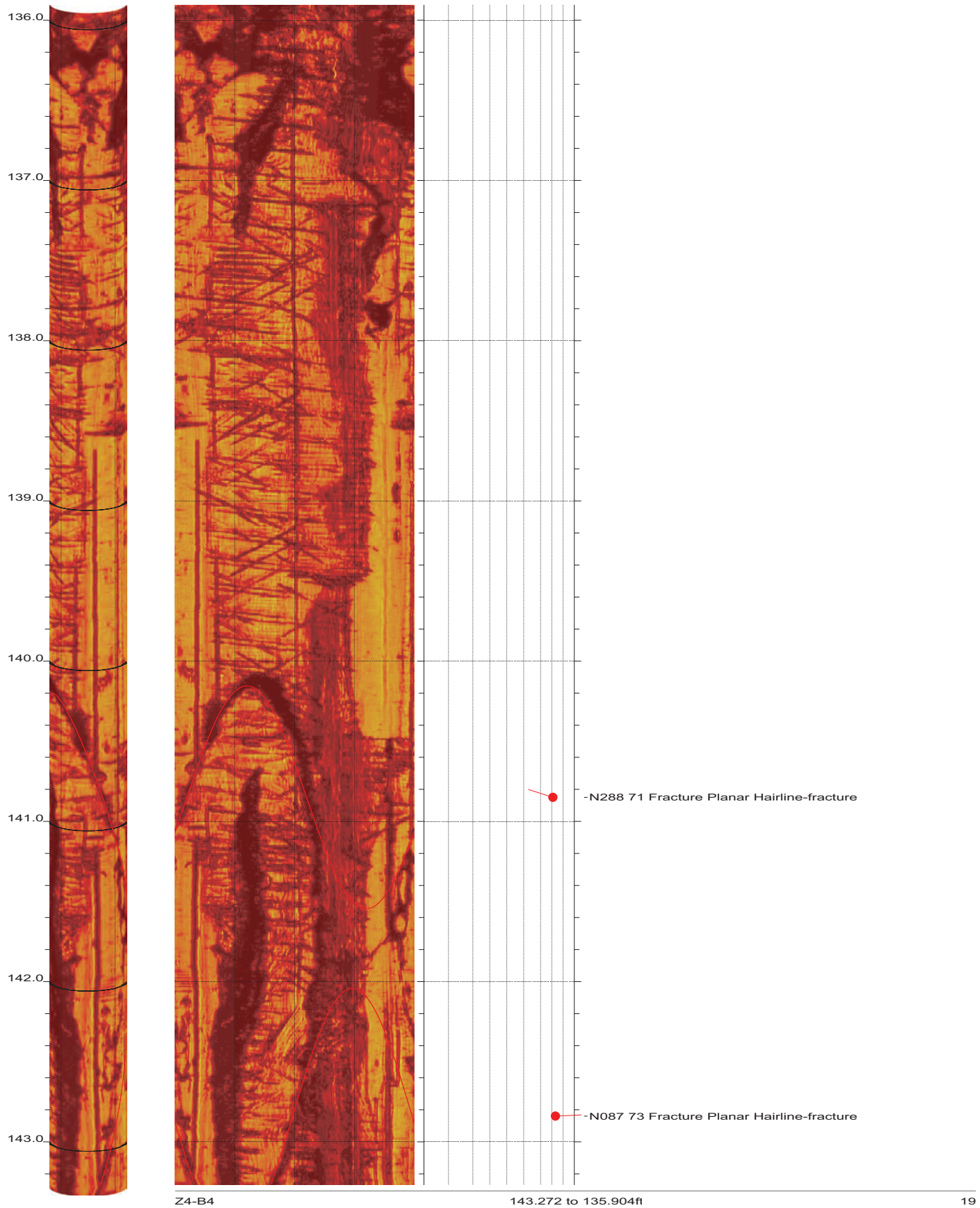
Z4-B4

135.904 to 128.536ft

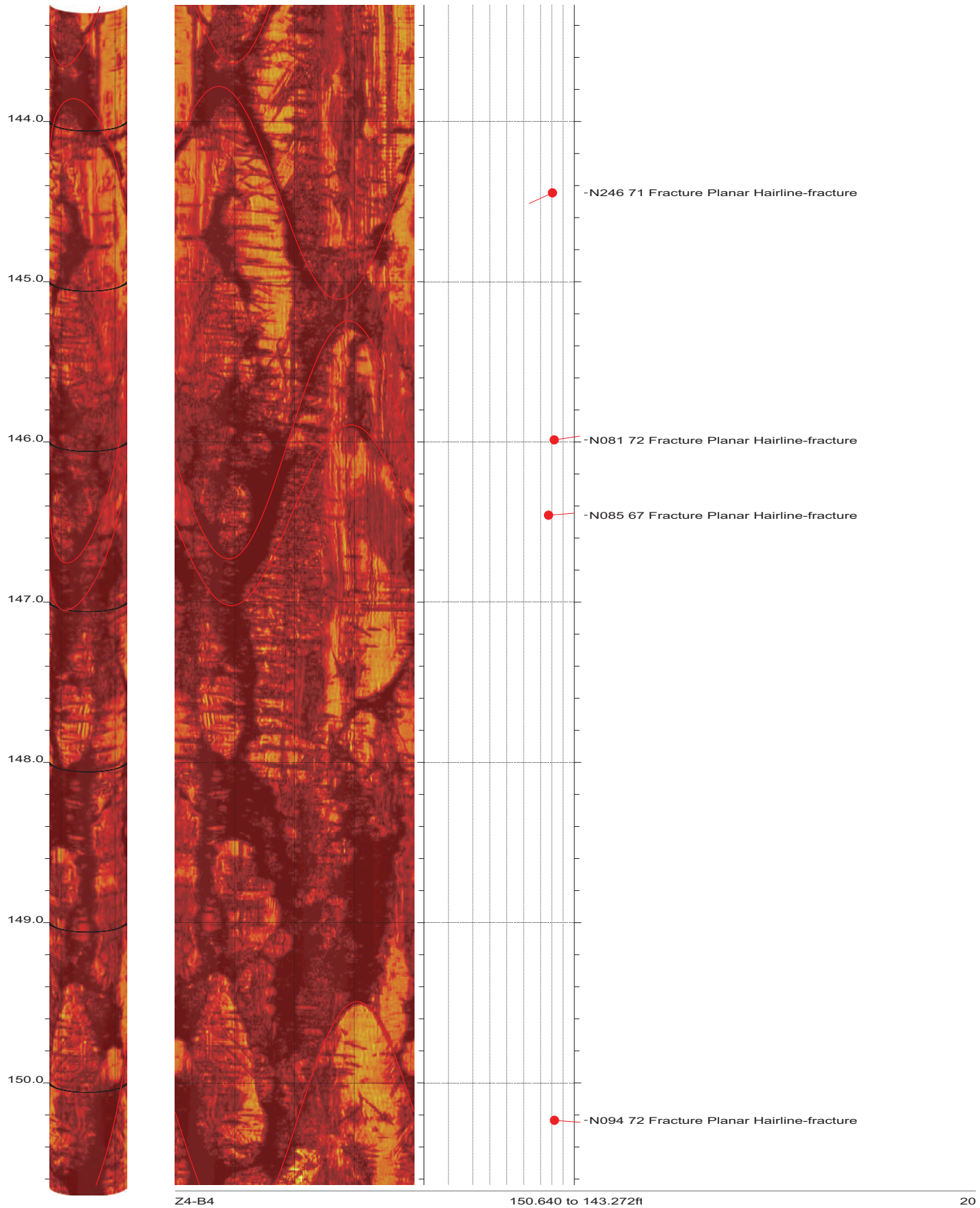
18

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 18 of 37

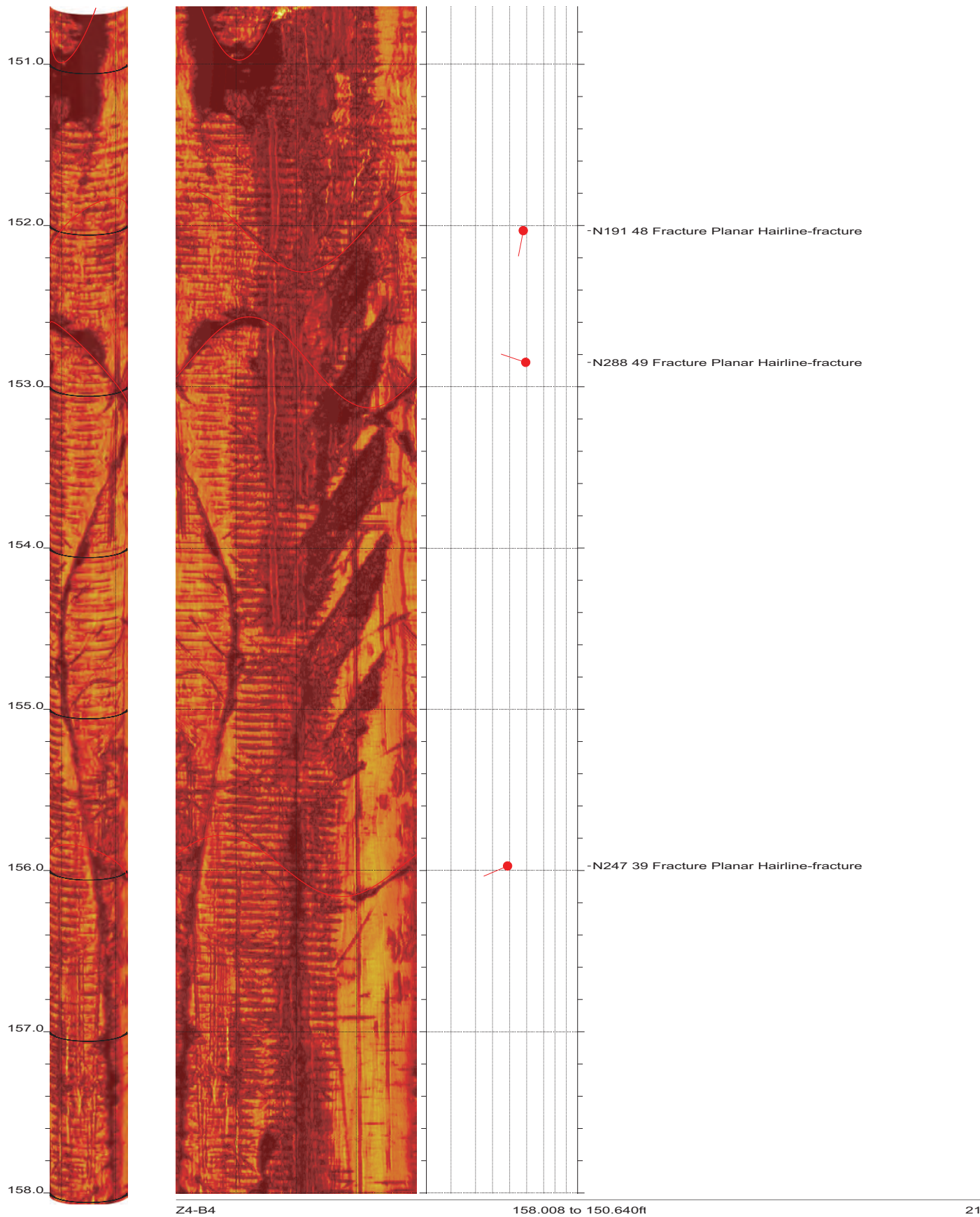




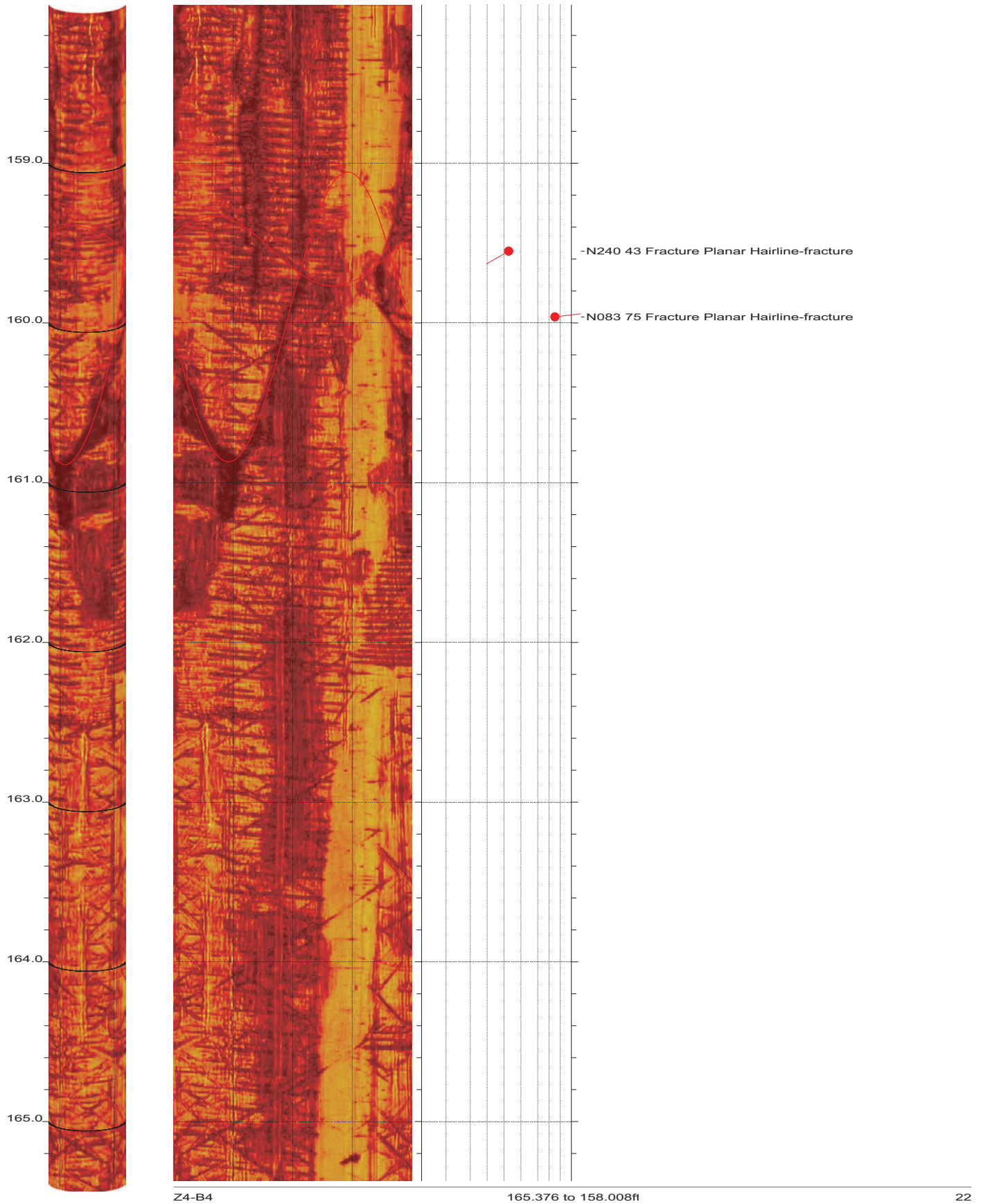
SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 19 of 37



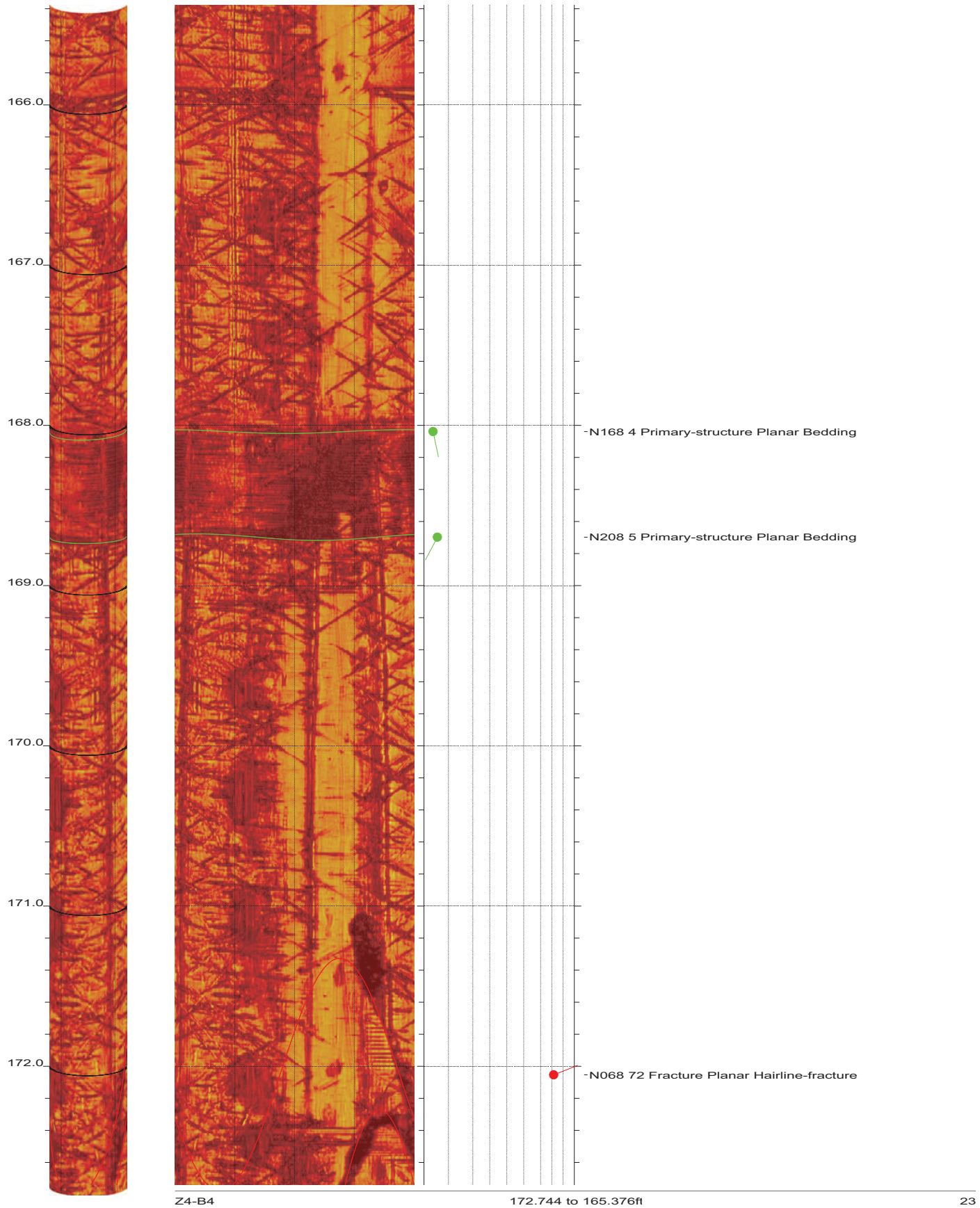
SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 20 of 37



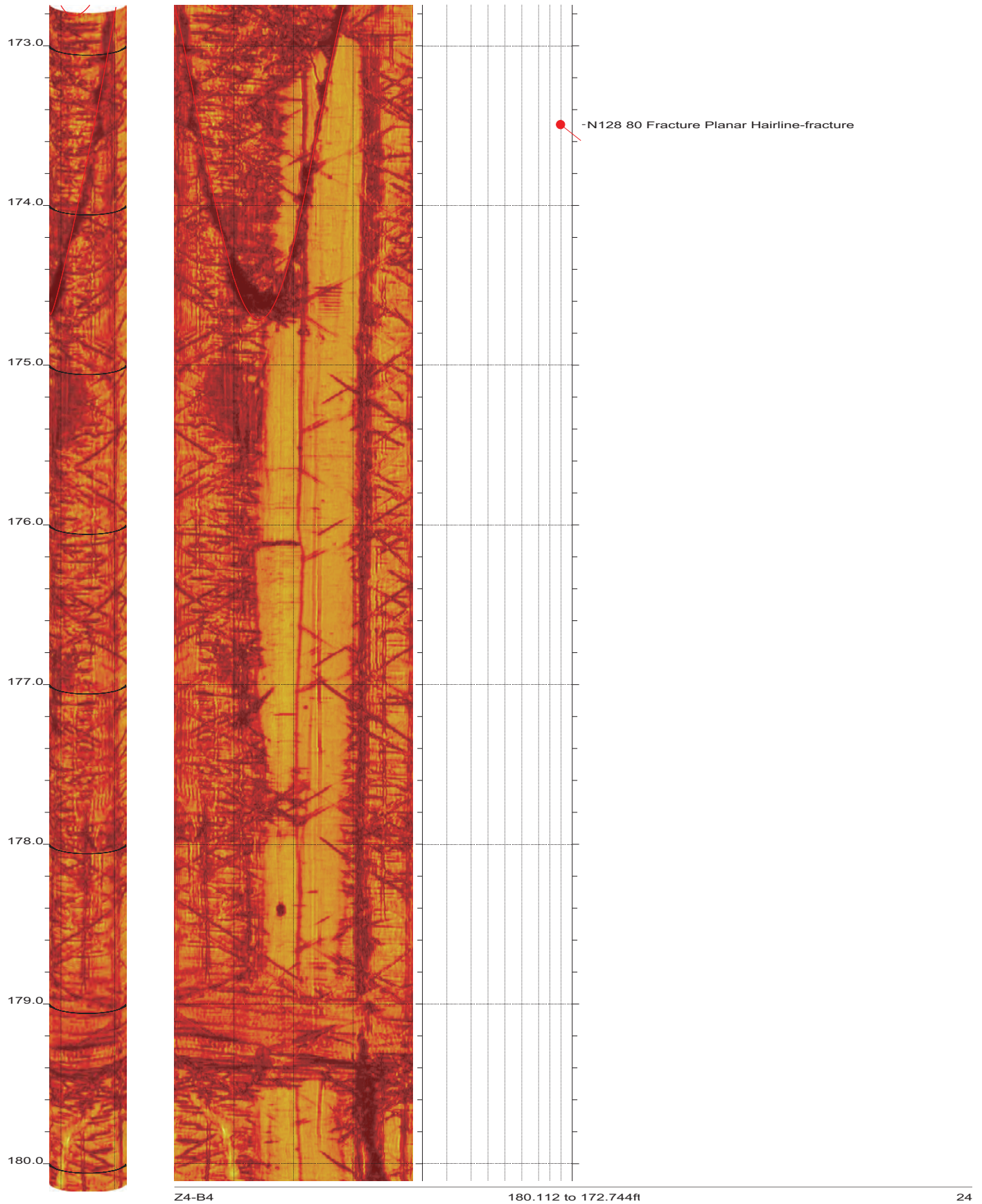
SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 21 of 37



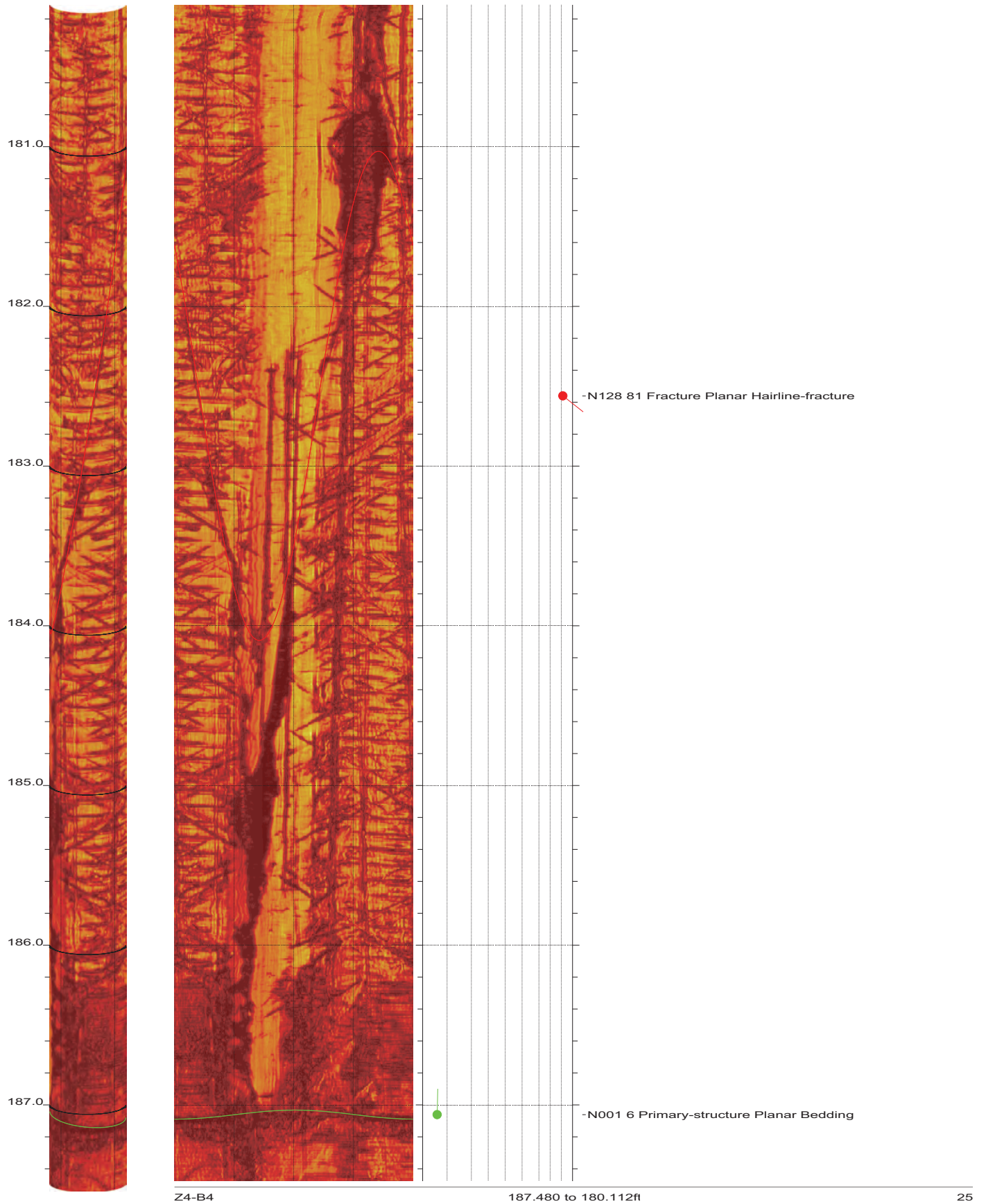
SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 22 of 37



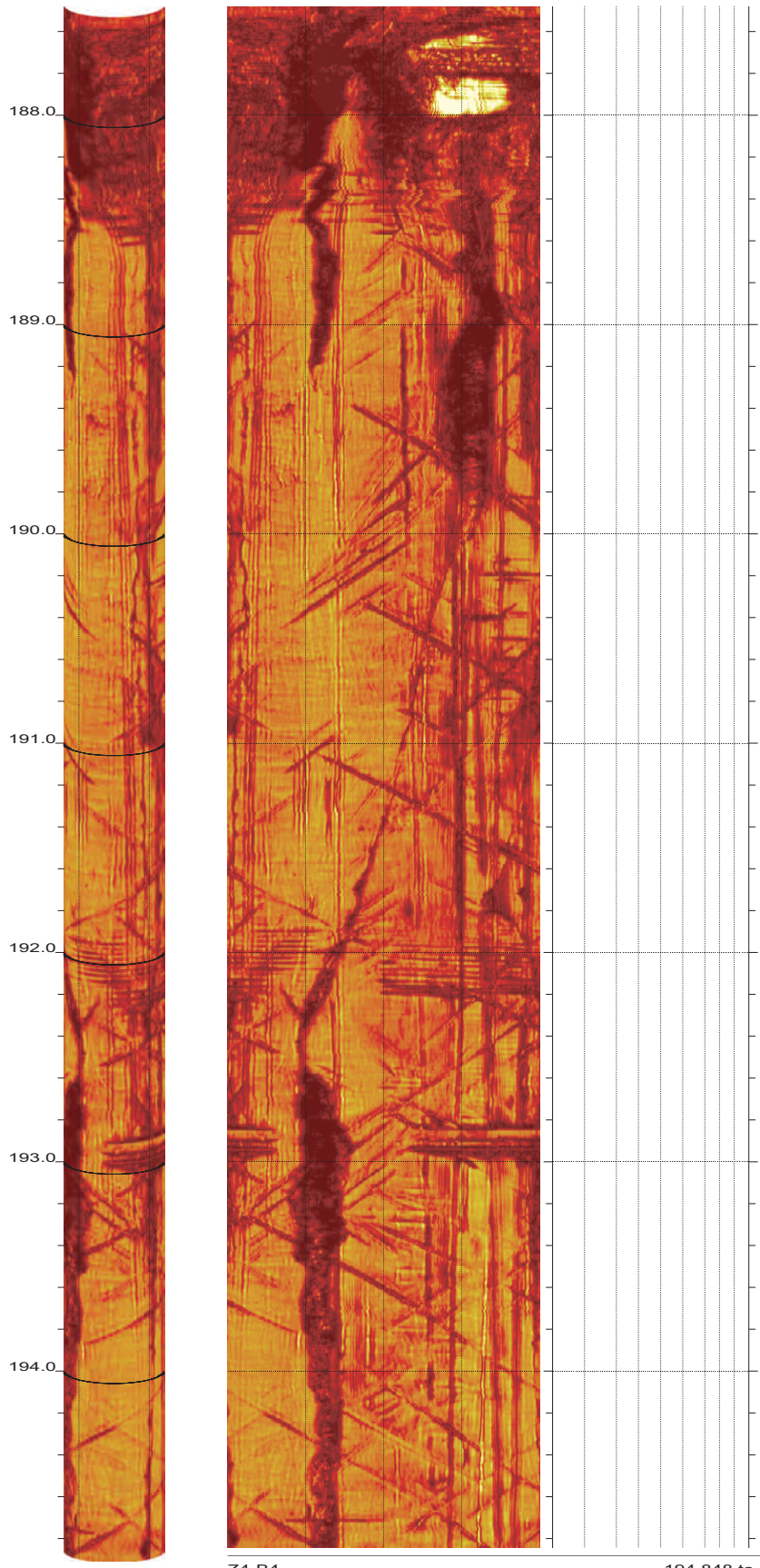
SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 23 of 37



SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 24 of 37



SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 25 of 37



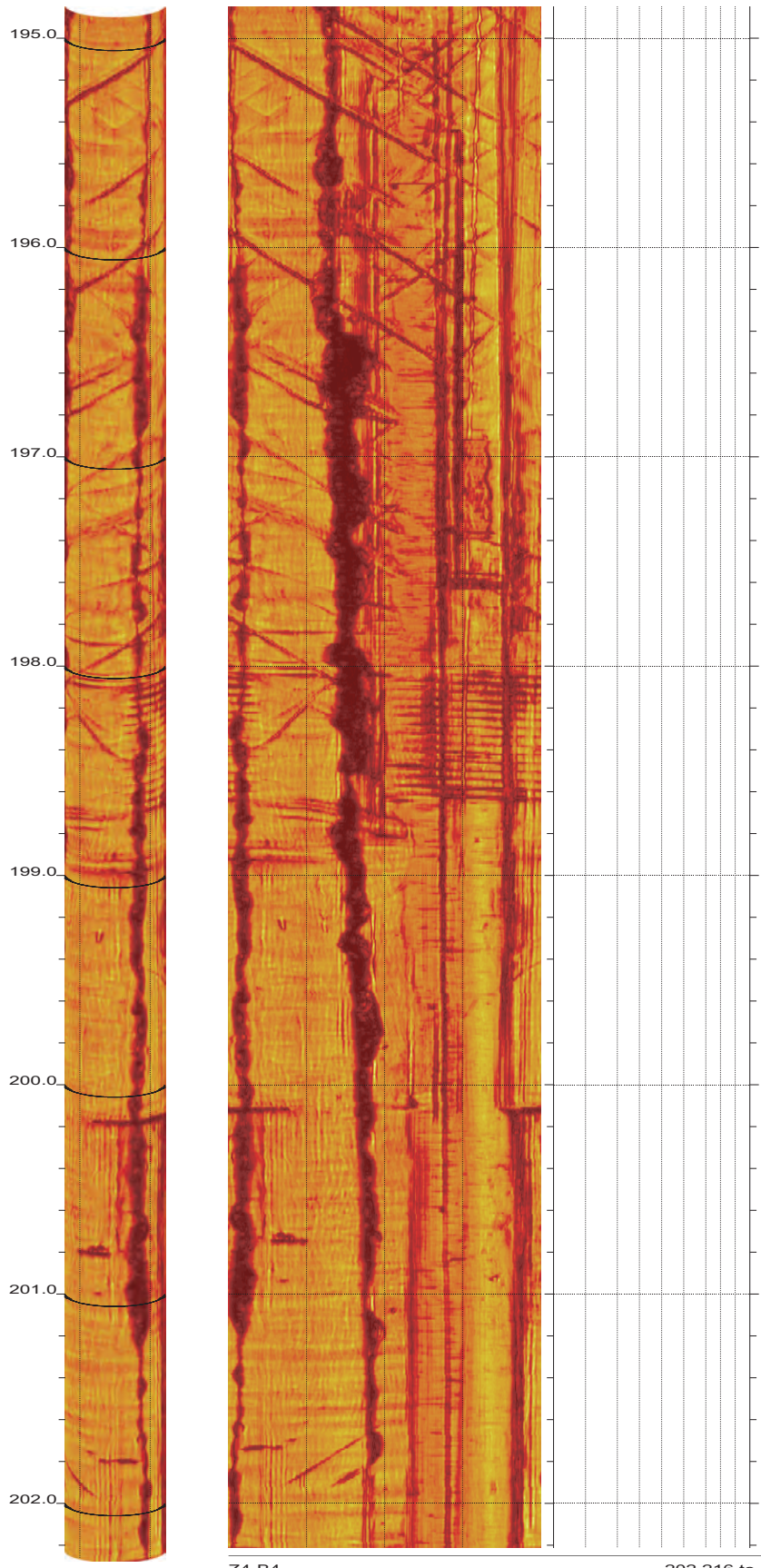
Z4-B4

194.848 to 187.480ft

26

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 26 of 37



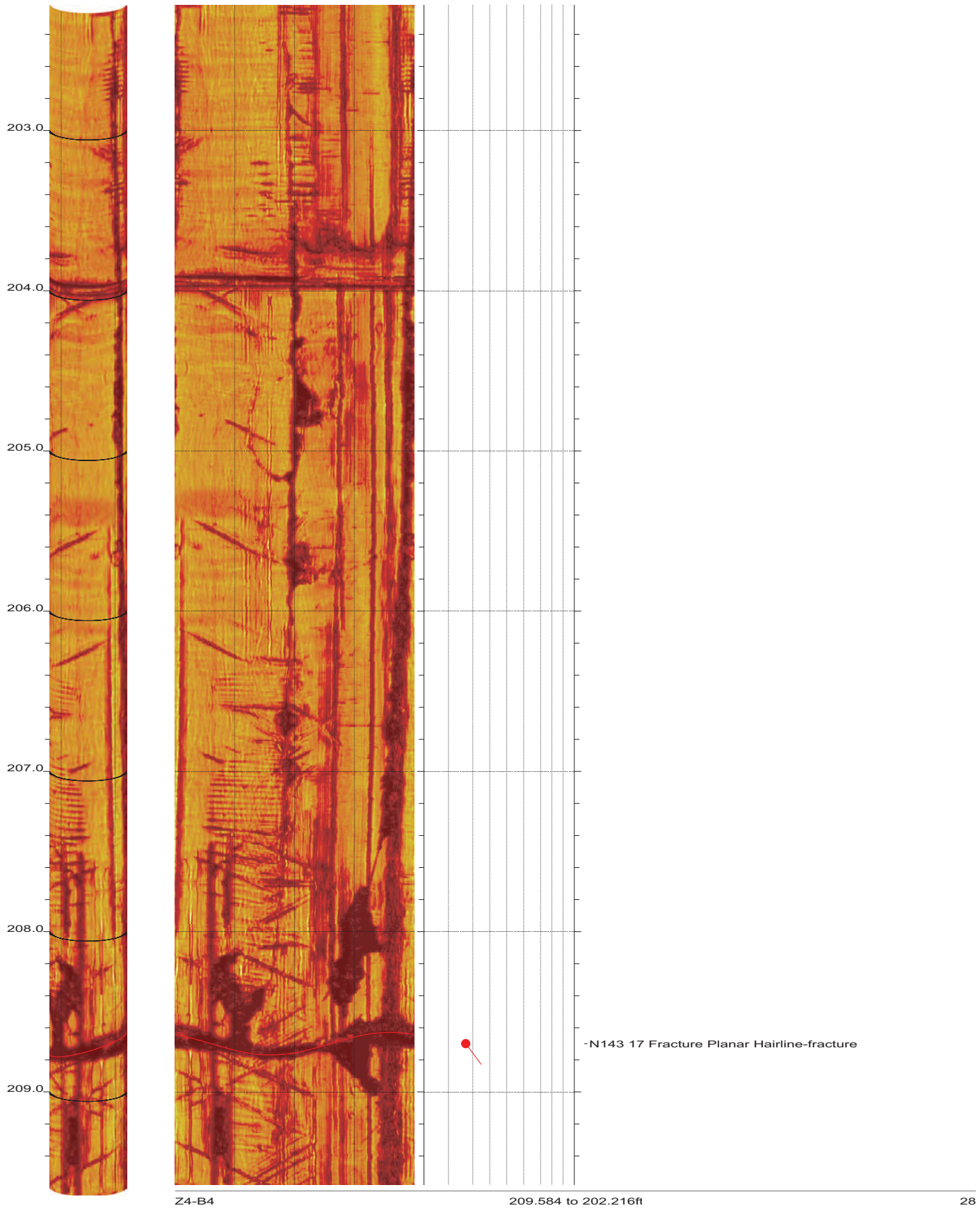


Z4-B4

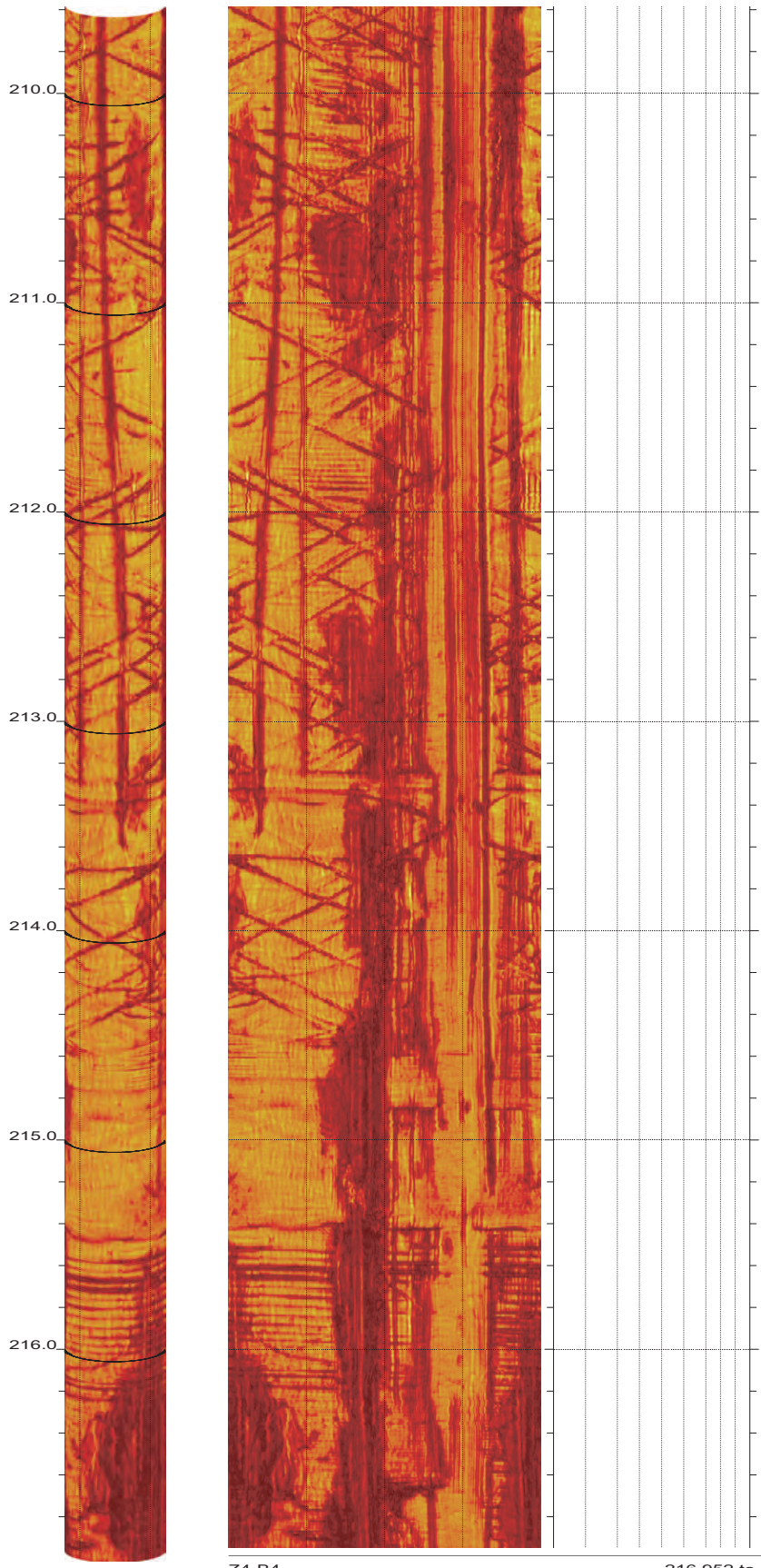
202.216 to 194.848ft

27

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 27 of 37



SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 28 of 37

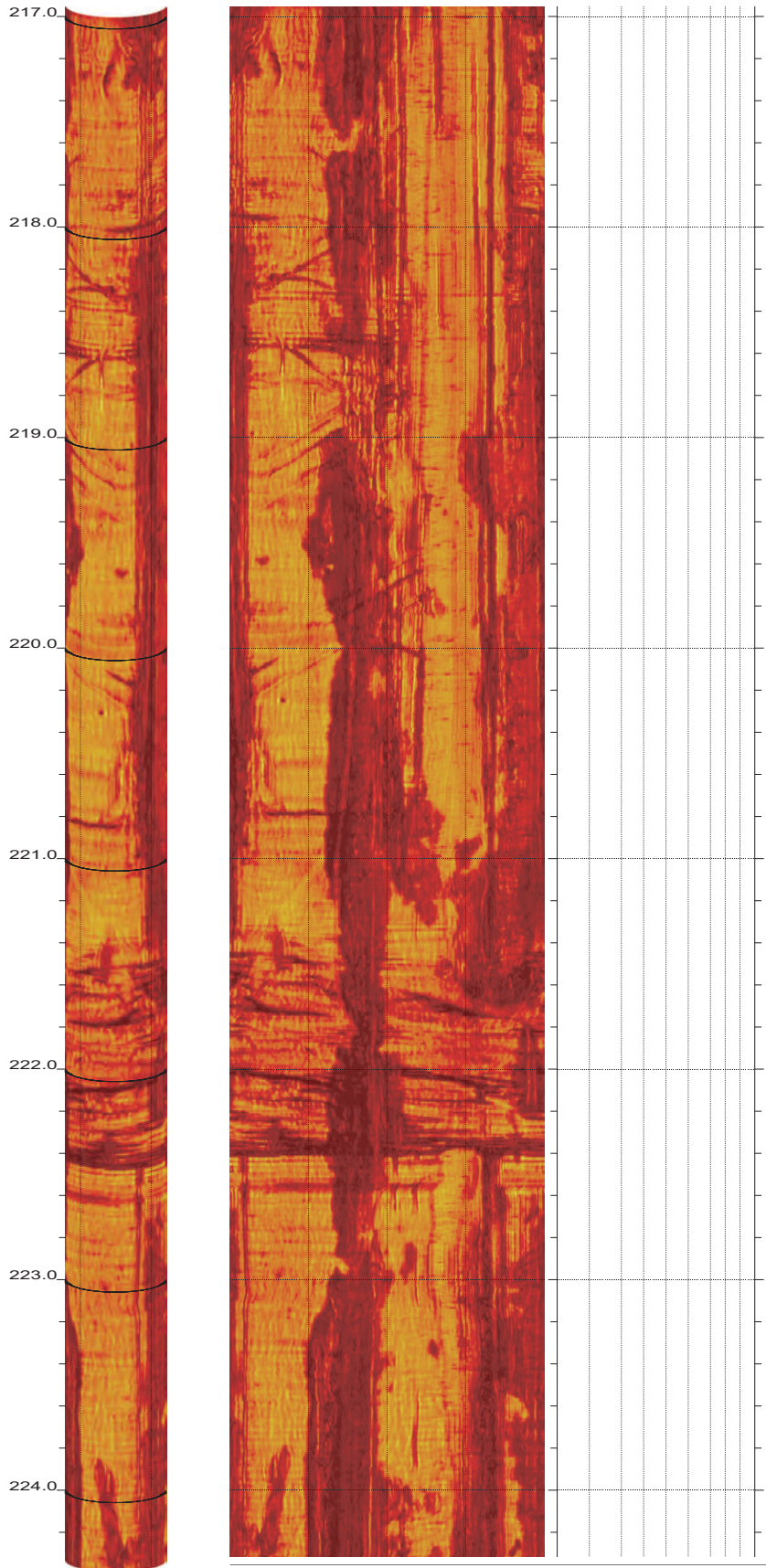


Z4-B4

216.952 to 209.584ft

29

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 29 of 37

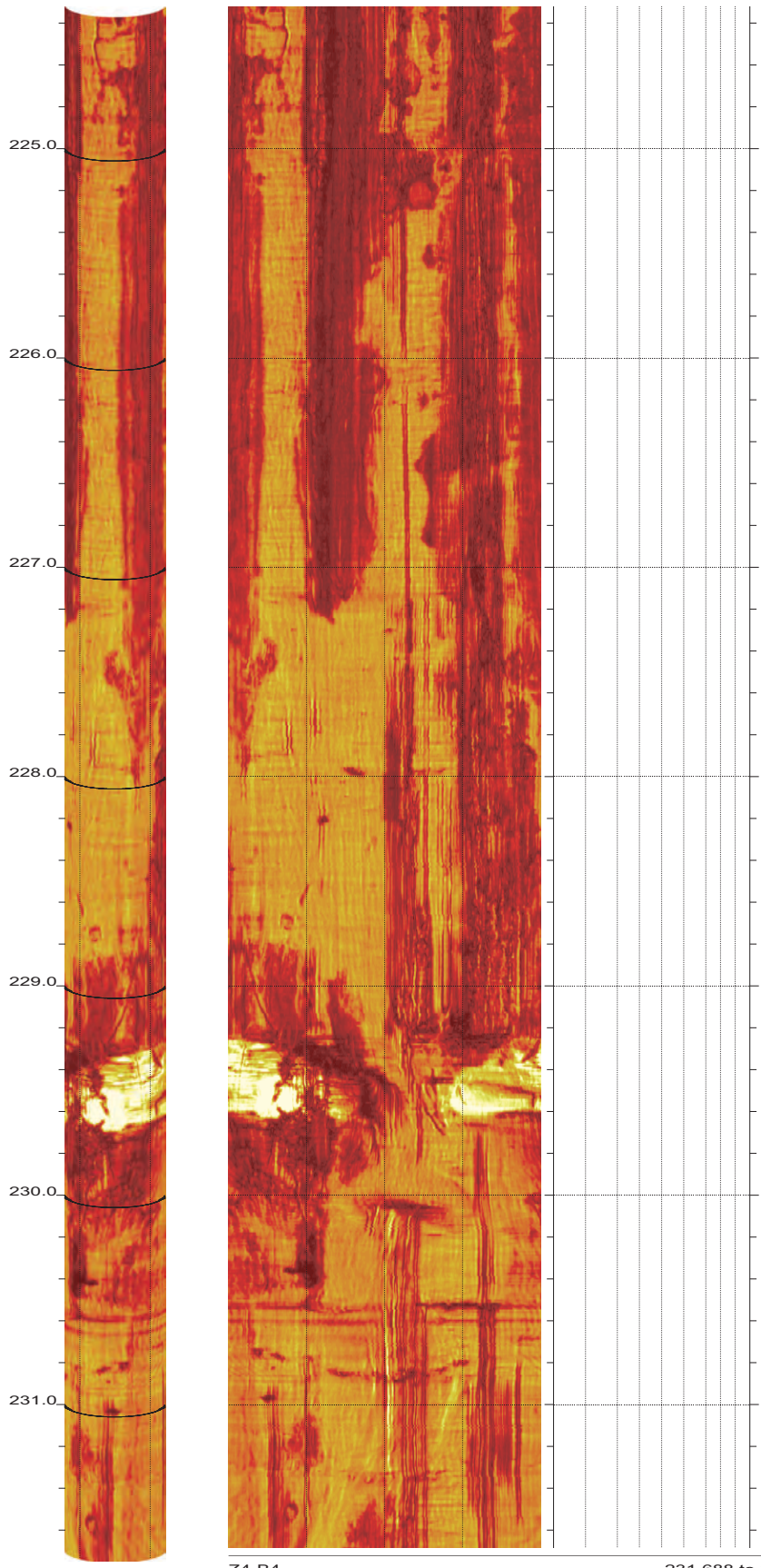


Z4-B4

224.320 to 216.952ft

30

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 30 of 37

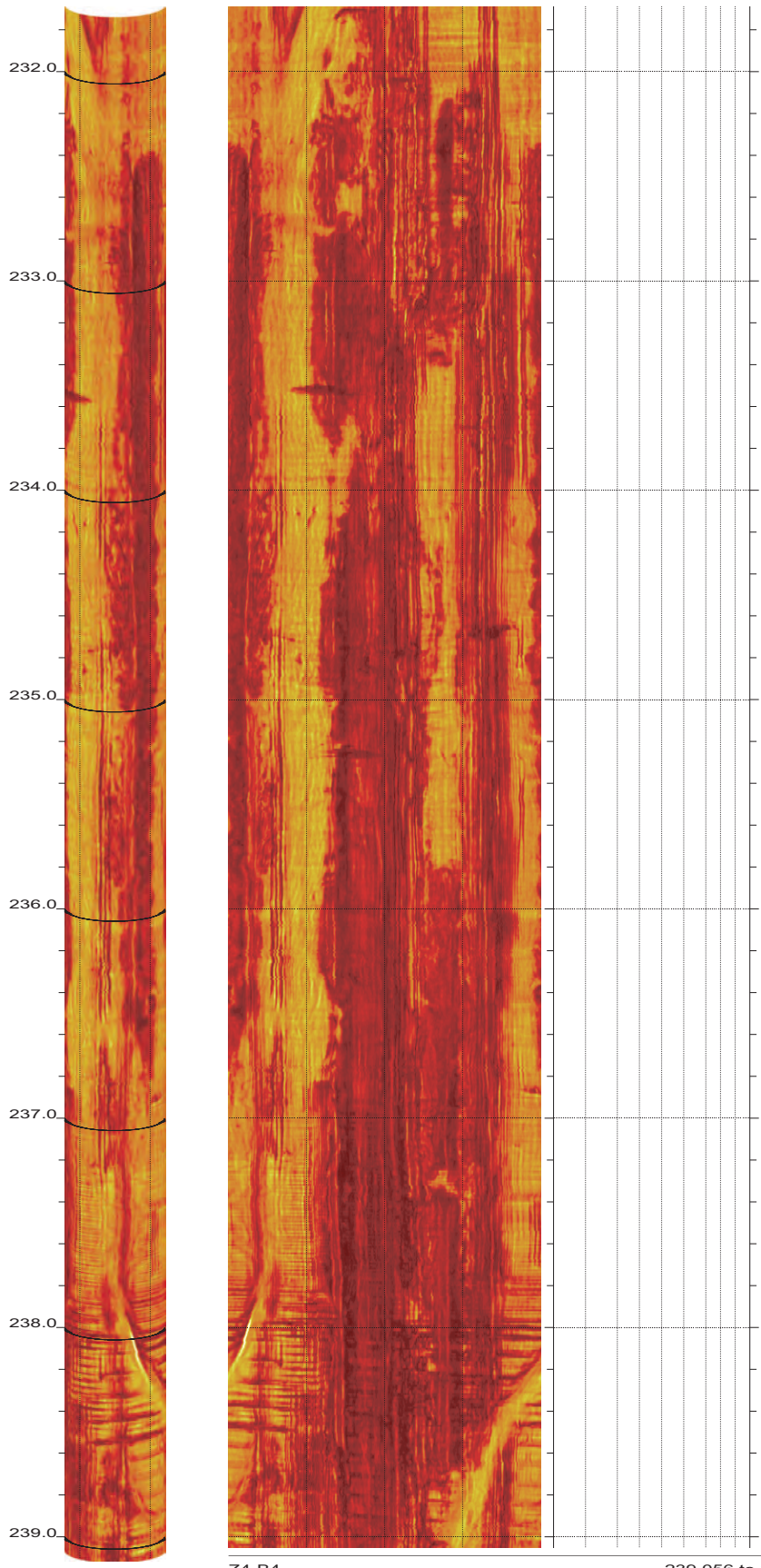


Z4-B4

231.688 to 224.320ft

31

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 31 of 37

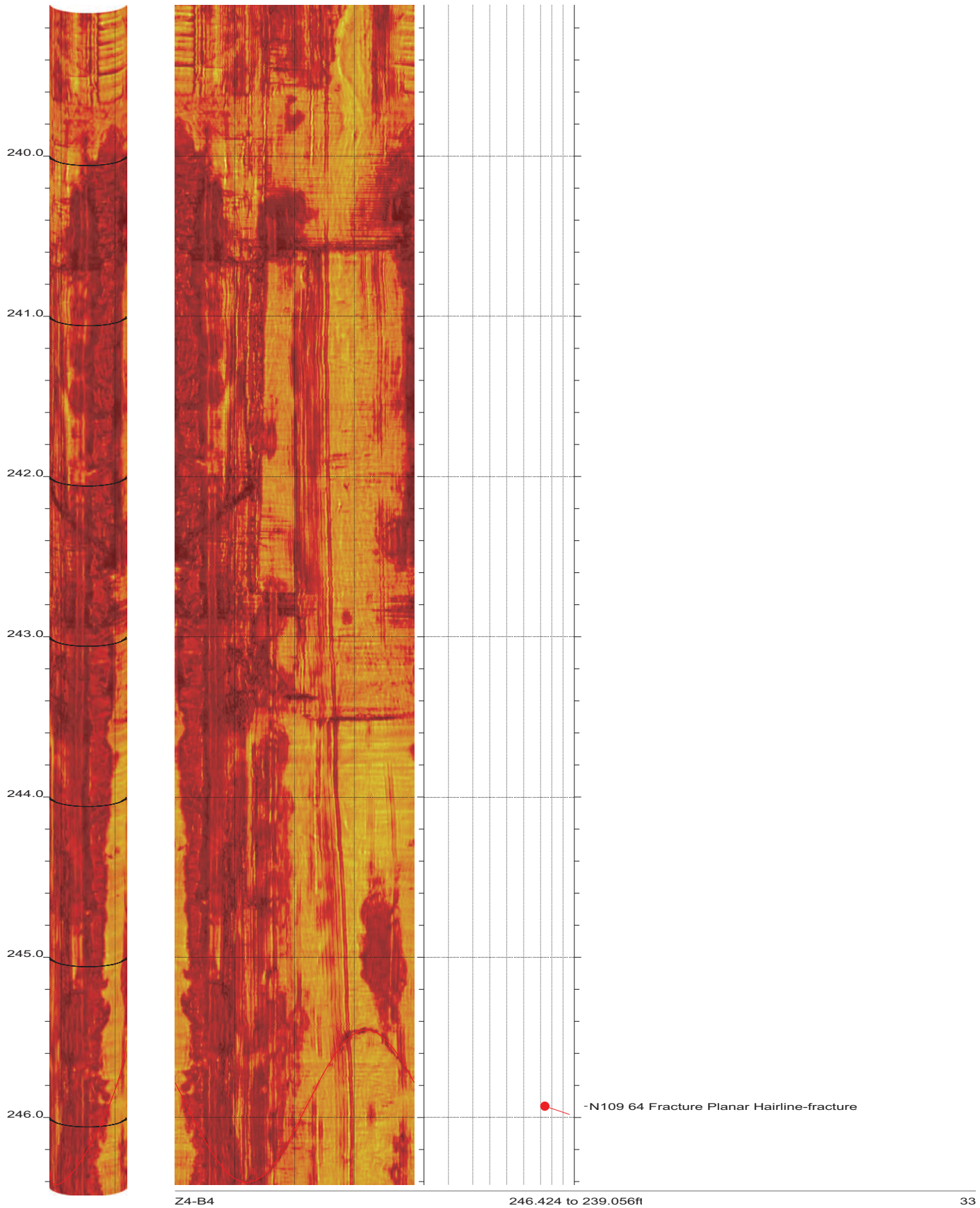


Z4-B4

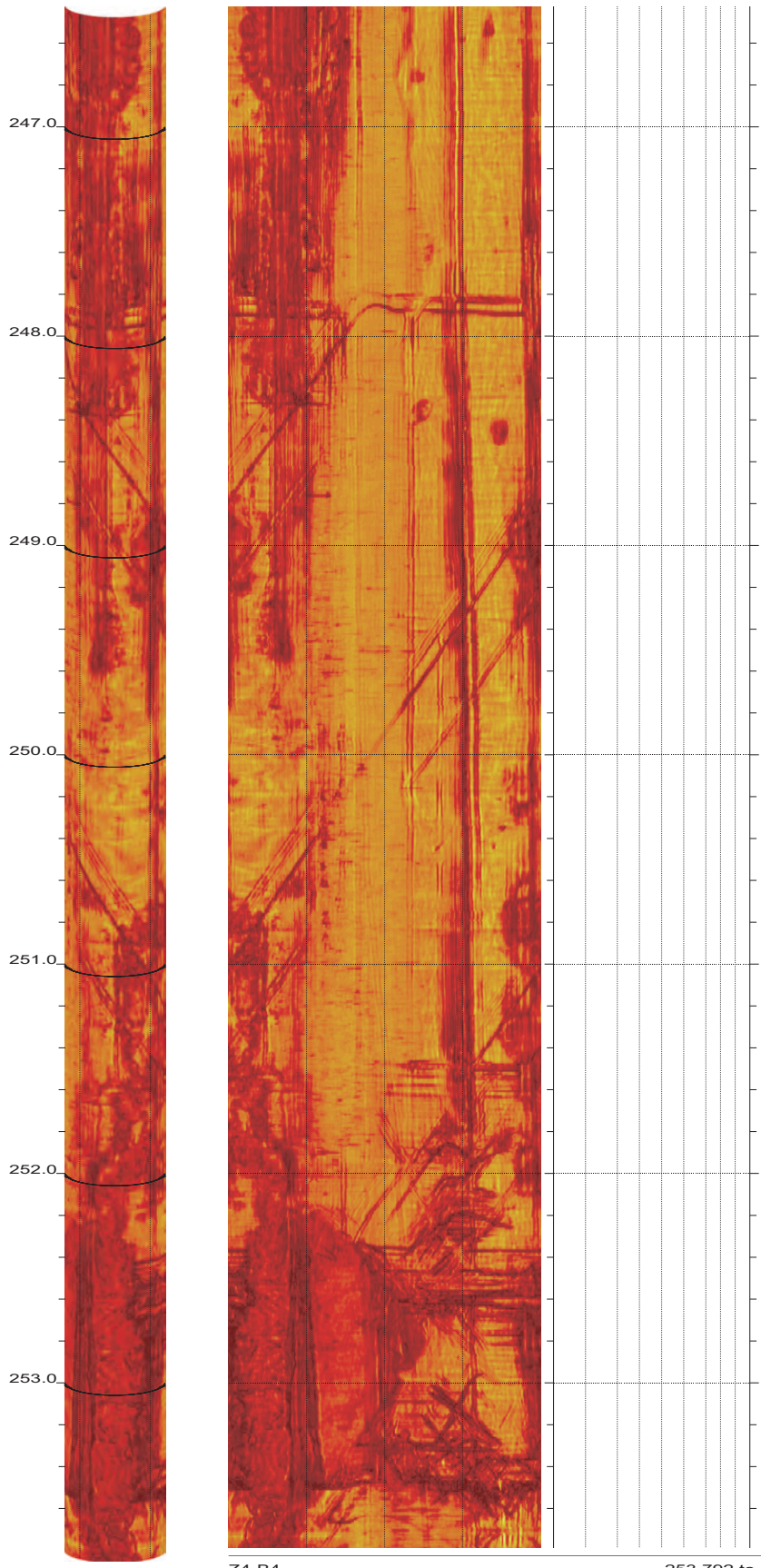
239.056 to 231.688ft

32

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 32 of 37



SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 33 of 37



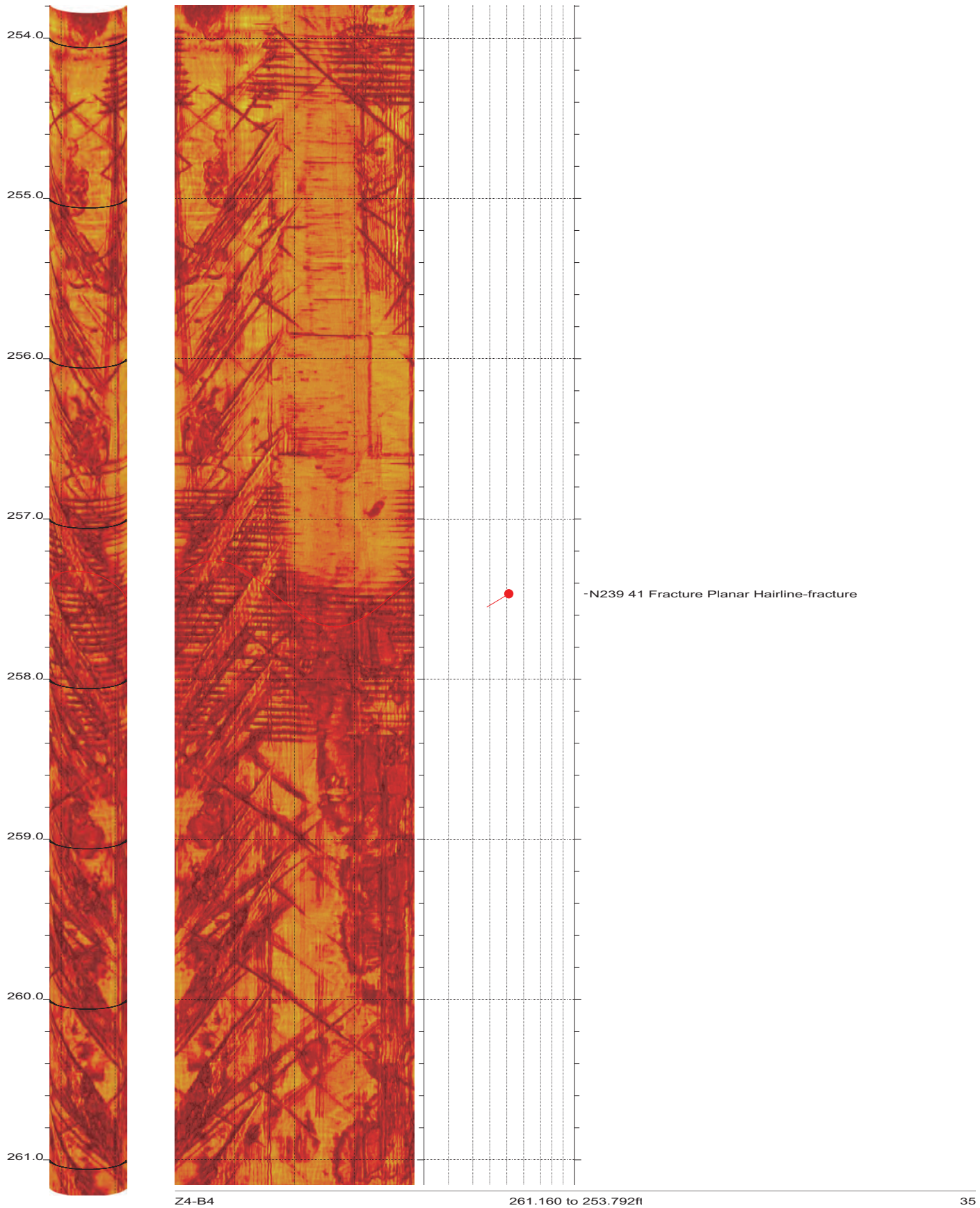
Z4-B4

253.792 to 246.424ft

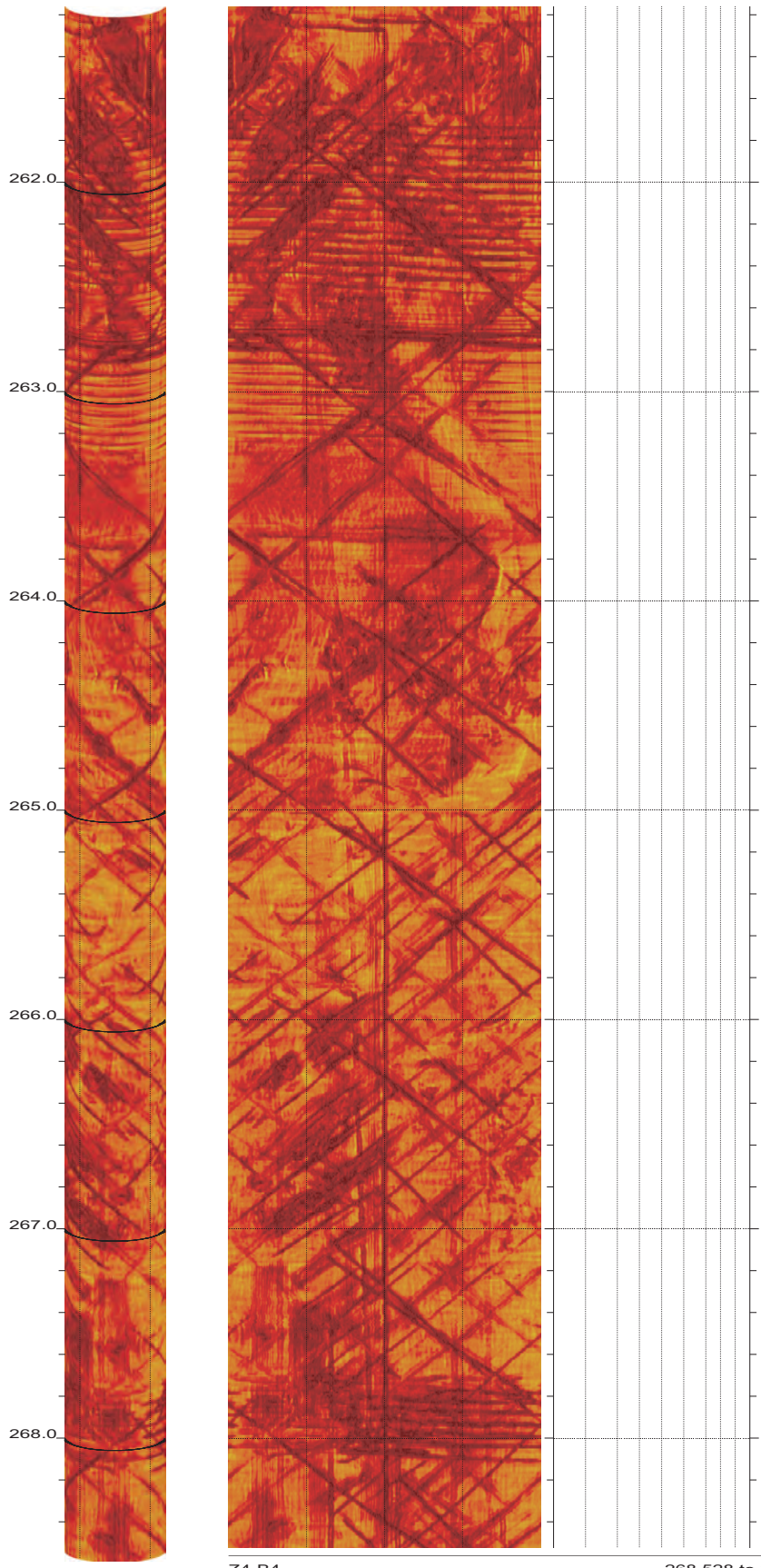
34

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 34 of 37





SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 35 of 37

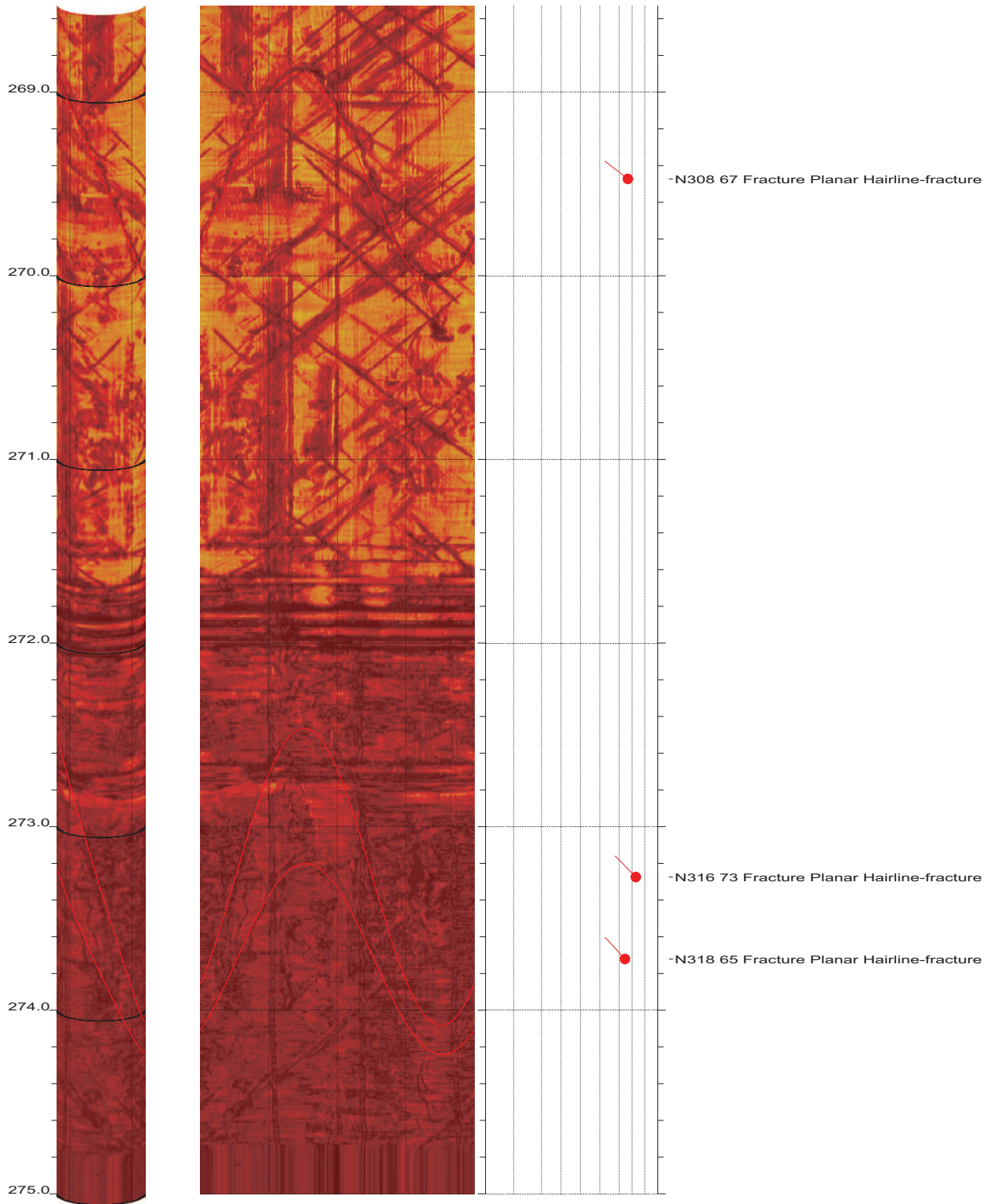


Z4-B4

268.528 to 261.160ft

36

SR-710 Boring Z4-B4 Acoustic Televiewer Dips rev 1 Sheet 36 of 37



**APPENDIX D**

**GEOPHYSICAL LOGGING SYSTEMS – NIST  
TRACEABLE CALIBRATION PROCEDURES AND  
CALIBRATION RECORDS**

# CALIBRATION PROCEDURE FOR GEOVision SEISMIC RECORDER/LOGGER

Reviewed 4/6/06

## Objective

The timing/sampling accuracy of seismic recorders or data loggers is required for several GEOVision field procedures including Seismic Refraction, Downhole Seismic Velocity Logging, and P-S Suspension Logging. This procedure describes the method for measuring the timing accuracy of a seismic data logger, such as the OYO Model 170, OYO/Robertson Model 3403, Geometrics Strataview or Geometrics Geode. The objective of this procedure is to verify that the timing accuracy of the recorder is accurate to within 1%.

## Frequency of Calibration

The calibration of each GEOVision seismic data logger is twelve (12) months. In the case of rented seismic data loggers, calibration must be performed prior to use.

## Test Equipment Required

The following equipment is required. Item #2 must have current NIST traceable calibration.

1. Function generator, Krohn Hite 5400B or equivalent
2. Frequency counter, HP 5315A or equivalent
3. Test cables, from item 1 to item 2, and from item 1 to subject data logger.

## Procedure

This procedure is designed to be performed using the accompanying Seismograph Calibration Data Sheet with the same revision number. All data must be entered and the procedure signed by the technician performing the test.

1. Record all identification data on the form provided.
2. Connect function generator to data logger (such as OYO Model 170) using test cable
3. Connect the function generator to the frequency counter using test cable.



Seismic Recorder/Logger Calibration Procedure  
Revision 1.30 Page 1

4. Set up generator to produce a 100.0 Hz, 0.25 volt (amplitude is approximate, modify as necessary to yield less than full scale waveforms on logger display) peak square wave or sine wave. Verify frequency using the counter and initial space on the data sheet.
5. Initialize data logger and record a data record of at least 0.1 second using a 100 microsecond or less sample period.
6. Measure the recorded square wave frequency by measuring the duration of 9 cycles of data. This measurement can be made using the data logger display device, or by printing out a paper tape. If a paper tape can be printed, the resulting printout must be attached to this procedure. Record the data in the space provided.
7. Repeat steps 5 and 6 three more times using separate files.

**Criteria**

The duration for 9 cycles in any file must be 90.0 milliseconds plus or minus 0.9 milliseconds, corresponding to an average frequency for the nine cycles of 100.0 Hz plus or minus 1 Hz (obtained by dividing 9 cycles by the duration in milliseconds).

If the results are outside this range, the data logger must be marked with a GEOVision REJECT tag until it can be repaired and retested.

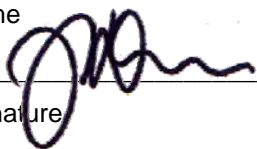
If results are acceptable affix label indicating the initials of the person performing the calibration, the date of calibration, and the due date for the next calibration (12 months).

**Procedure Approval**

Approved by:

\_\_\_\_\_ John G. Diehl \_\_\_\_\_

Name

\_\_\_\_\_  
  
 \_\_\_\_\_

Signature

\_\_\_\_\_ President \_\_\_\_\_

Title

\_\_\_\_\_ April 6, 2006 \_\_\_\_\_

Date

Client Approval (if required):

\_\_\_\_\_

Name

\_\_\_\_\_


Signature

\_\_\_\_\_

Title

\_\_\_\_\_

Date

	Seismic Recorder/Logger Calibration Procedure Revision 1.30 Page 2
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# GEOVision SUSPENSION PS SEISMIC LOGGER/RECORDER CALIBRATION PROCEDURE

Reviewed 7/21/08

## Objective

The timing/sampling accuracy of seismic recorders or data loggers is required for several GEOVision field procedures including Seismic Refraction, Downhole P-S Seismic Velocity Logging, and Suspension P-S Seismic Velocity Logging. This procedure describes the method for measuring the timing accuracy of a seismic data logger, such as the OYO Model 170 or OYO/Robertson Model 3403. The objective of this procedure is to verify that the timing accuracy of the recorder is accurate to within 1%.

## Frequency of Calibration

The calibration of each GEOVision seismic data logger is twelve (12) months. In the case of rented seismic logger/recorders, calibration must be performed prior to use.

## Test Equipment Required

The following equipment is required. Item #2 must have current NIST traceable calibration.

1. Function generator, Krohn Hite 5400B or equivalent
2. Frequency counter, HP 5315A or equivalent
3. Test cables, from item 1 to item 2, and from item 1 to subject data logger.

## Procedure

This procedure is designed to be performed using the accompanying Suspension P-S Seismic Logger/Recorder Calibration Data Form with the same revision number. All data must be entered and the procedure signed by the technician performing the test.

1. Record all identification data on the form provided.
2. Connect function generator to data logger (such as OYO Model 170) using test cable
3. Connect the function generator to the frequency counter using test cable.
4. Set signal generator to target frequency specified on data form, 0.25 volt (amplitude is approximate, modify as necessary to yield less than full scale waveforms on



Suspension PS Seismic Logger/Recorder Calibration Procedure  
Revision 2.0 Page 1

logger display) peak sine wave. Verify frequency using the counter and note actual frequency on the data form.

5. Set data logger to file length specified on data form and record a data file to disk. Note file name on data form.
6. Measure the duration of 9 complete sine wave cycles on the data file. This measurement must be made using the analysis program PSLOG.EXE version 1.00, and saved as a .sps pick file. Note the duration in milliseconds in the spaces provided on the data form. Calculate average recorded sine wave frequency for each channel pair (Hn, Hr, V) by dividing the duration by 9. Note the average frequency of each channel pair on the data form.
7. Repeat steps 4 through 6 until all target frequencies have been recorded, producing 6 separate data and pick files.

**Criteria**

The average frequency for the nine cycles (obtained by dividing 9 cycles by the duration in seconds) must be within plus or minus 1% of the actual frequency for each of the 6 records.

If the results are outside this range, the data logger must be marked with a GEOVision REJECT tag until it can be repaired and retested.

If results are acceptable affix label indicating the initials of the person performing the calibration, the date of calibration, and the due date for the next calibration (12 months).

**Procedure Approval**

Approved by:

\_\_\_\_\_ John G. Diehl \_\_\_\_\_

Name

Signature



\_\_\_\_\_ President \_\_\_\_\_

Title

Date

\_\_\_\_\_ July 21, 2008 \_\_\_\_\_


Calibration Laboratory Approval (if required):

\_\_\_\_\_ Name \_\_\_\_\_

\_\_\_\_\_ Title \_\_\_\_\_

\_\_\_\_\_ Signature \_\_\_\_\_

\_\_\_\_\_ Date \_\_\_\_\_

	Suspension PS Seismic Logger/Recorder Calibration Procedure
	Revision 2.0 Page 2



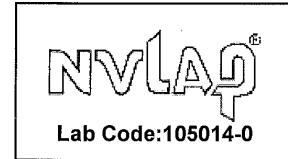


# Calibration Report



**Metrology**  
7300 Fenwick Lane  
Westminster, CA 92683  
Phone: 866-723-2257

*NVLAP Accredited  
Calibration*  
**GEOVision Geophysical Services**  
1124 Olympic Drive  
Corona, CA 92881-3390



**Manufacturer:** Oyo  
**Model Number:** 3403  
**Description:** Unit, Suspension Telemetry,  
**Asset Number:** 160024  
**Serial Number:** 160024  
**PO Number:** 8200-080122-01

**Condition As Found:** In Tolerance  
**Condition As Left:** In Tolerance  
**Calibration Date:** 08/01/2008  
**Calibration Due Date:** 08/01/2009  
**Calibration Interval:** 12 Months

**Remarks:**

This unit was calibrated with the customer's old procedure and specifications which have been reviewed by Metrology Engineering and documented in SCE Document M013684. The data can be found on page 2 of this report with the original observation data on page 3. The unit was then calibrated with the customer's new procedure and specification's which have been reviewed by Metrology Engineering and documented in SCE Document M013987. The data can be found on pages 4 and 5 of this report with the original observation data on page 6 of this report. Corrected Copy: This record created to add missing maximum error calculations on page 6 of 6. CAB 8-5-08

**Standards Utilized**

I.D. No.	Mfg.	Model No.	Description	Cal. Date	Due Date
S1-01252	Hewlett Packard	5335A OPT 010,203040	Counter, Universal,	07/17/2008	01/17/2009
S1-01347	Hewlett Packard	3325A	Generator, Function, Synthesizer	04/24/2008	10/24/2008
S1-03686	Fluke	910	Standard, Frequency, Controlled, Gps	01/22/2008	01/22/2009

**Procedure:** Customer  
**Temperature:** 23° C  
**Humidity:** 52% RH  
**Test No.:** 558549

Calibration Performed By:			Quality Reviewer:	
Branson, Craig A	Metrologist	714-895-0714	<i>[Signature]</i>	8-5-08
<small>Name</small>	<small>Title</small>	<small>Phone</small>	<small>Name</small>	<small>Date</small>

This report may not be reproduced, except in full, without written permission of this laboratory. This report must not be used by the client to claim product certification, approval, or endorsement by NVLAP, NIST, or any agency of the Federal Government. The results stated in this report relate only to the items tested or calibrated. Measurements reported herein are traceable to SI units via national standards maintained by NIST. This calibration is in compliance with NVLAP laboratory accreditation criteria established by NIST/NVLAP under the specific scope of accreditation for lab code 105014-0.

[www.edisonmudcats.com](http://www.edisonmudcats.com)

[www.edisonmetrology.com](http://www.edisonmetrology.com)

Page 1 of 6

Test No. 558549  
 Asset No. 160024

## Custom Specification Report

Oyo 3403 Unit, Suspension Telemetry,

Page 2 of 6

STEP NUM	FUNCTION TESTED	NOMINAL VALUE	AS FOUND	AS LEFT	Out of Tol	CALIBRATION TOLERANCE
	CH HN Frequency Square Wave	100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
		100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
	Sine Wave	100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
		100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
	CH HR Frequency Square Wave	100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
		100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
	Sine Wave	100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
		100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
	CH V Frequency Square Wave	100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
		100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
	Sine Wave	100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
		100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500 Hz]
Remarks:						

MudCats CPM: Version 2.2.2 (Professional)  
 Src DUI: {4A70366A-164D-4E33-8F79-34E3FDFFA198} (c)  
 Doc DUI: {293A3A00-D536-43A0-A1E5-945133CD4CF7} (o)

**ATTACHMENT 1**  
 Page 1 of 1

Customer

**SEISMOGRAPH CALIBRATION DATA SHEET REV 4/6/06**

**INSTRUMENT DATA**

SYSTEM MFR: <u>OYO</u>	MODEL NO.: <u>3403</u>
SERIAL NO.: <u>160024</u>	CALIBRATION DATE: <u>8/1/2008</u>
BY: <u>CRAIG BRANSON</u>	DUE DATE: <u>8/1/2009</u>
COUNTER MFR: <u>HEWLETT PACKARD</u>	MODEL NO.: <u>5335A</u>
SERIAL NO.: <u>2626A09881</u>	CALIBRATION DATE: <u>7/17/2008</u>
BY: <u>SCE #S1-01252</u>	DUE DATE: <u>1/17/2009</u>
FCTN GEN MFR: <u>HEWLETT PACKARD</u>	MODEL NO.: <u>3325A</u>
SERIAL NO.: <u>2652A25647</u>	CALIBRATION DATE: <u>4/24/2008</u>
BY: <u>SCE #S1-01347</u>	DUE DATE: <u>10/24/2008</u>

**SYSTEM SETTINGS:**

GAIN:	<u>2</u>
FILTER:	<u>10 KHZ</u>
RANGE:	<u>100 MILLISEC</u>
DELAY:	<u>0</u>
STACK: 1 (STD)	<u>1</u>
PULSE:	<u>1.6</u>
DISPLAY:	<u>NA</u>
SYSTEM: DATE = CORRECT DATE & TIME	<u>8/1/2008 715</u>

**PROCEDURE:**

SET FREQUENCY TO 100.0 HZ SQUAREWAVE WITH AMPLITUDE APPROXIMATELY 0.25 VOLT PEAK. RECORD BOTH ON DISK AND PAPER TAPE, IF AVAILABLE. ANALYZE AND PRINT WAVEFORMS FROM ANALYSIS UTILITY. ATTACH PAPER COPIES OF PRINTOUT AND PAPER TAPES, IF AVAILABLE, TO THIS FORM. AVERAGE FREQUENCY MUST BE BETWEEN 99.0 AND 101.0 HZ.

AS FOUND 100.0 HZ AS LEFT 100.0 HZ

WAVEFORM	FILE NO	FREQUENCY	TIME FOR 9 CYCLES Hr	TIME FOR 9 CYCLES Hr	TIME FOR 9 CYCLES V	AVERAGE FREQ.
SQUARE	501	100.0	90.00ms	90.00ms	90.00ms	100.0 HZ
SQUARE	502	100.0	90.00ms	90.00ms	90.00ms	100.0 HZ
SINE	503	100.0	90.00ms	90.00ms	90.00ms	100.0 HZ
SINE	504	100.0	90.00ms	90.00ms	90.00ms	100.0 HZ

CALIBRATED BY: CRAIG BRANSON 8/1/2008 Craig Branson  
 NAME DATE SIGNATURE

Test No. 558549  
 Asset No. 160024

## Custom Specification Report

Oyo 3403 Logger/Recorder, Seismic, PS Suspension

Page 4 of 6

STEP NUM	FUNCTION TESTED	NOMINAL VALUE	AS FOUND	AS LEFT	Out of Tol	CALIBRATION TOLERANCE
	CH HN Frequency Sine Wave	50.00 Hz	50.00	Same		49.50 to 50.50 Hz [EMU 0.000250]
		100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500]
		200.0 Hz	200.0	Same		198.0 to 202.0 Hz [EMU 0.001000]
		500.0 Hz	500.0	Same		495.0 to 505.0 Hz [EMU 0.002500]
		1000 Hz	1000	Same		990 to 1010 Hz [EMU 0.005000]
		2000 Hz	2000	Same		1980 to 2020 Hz [EMU 0.010000]
	CH HR Frequency Sine Wave	50.00 Hz	49.95	Same		49.50 to 50.50 Hz [EMU 0.000250]
		100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500]
		200.0 Hz	200.2	Same		198.0 to 202.0 Hz [EMU 0.001000]
		500.0 Hz	500.0	Same		495.0 to 505.0 Hz [EMU 0.002500]
		1000 Hz	1001	Same		990 to 1010 Hz [EMU 0.005000]
		2000 Hz	2000	Same		1980 to 2020 Hz [EMU 0.010000]
	CH V Frequency Sine Wave	50.00 Hz	50.00	Same		49.50 to 50.50 Hz [EMU 0.000250]
		100.0 Hz	100.0	Same		99.0 to 101.0 Hz [EMU 0.000500]
		200.0 Hz	199.8	Same		198.0 to 202.0 Hz [EMU 0.001000]
		500.0 Hz	500.0	Same		495.0 to 505.0 Hz [EMU 0.002500]
<b>Remarks:</b>						

MudCats CPM: Version 2.2.2 (Professional)  
 Src DUI: {9548AF3D-C74D-4C9F-AEEF-21EF560BC451} (c)  
 Doc DUI: {AAAE8731-399D-47BC-98B7-62728C8250BE} (c)

**ATTACHMENT 2**  
 Page 1 of 2

Customer



## SUSPENSION PS SEISMIC LOGGER/RECORDER CALIBRATION DATA FORM

**INSTRUMENT DATA**

System mfg.:	Oyo	Model no.:	3403
Serial no.:	160024	Calibration date:	8/1/2008
By:	Craig Branson	Due date:	8/1/2009
Counter mfg.:	Hewlett-Packard	Model no.:	5335A
Serial no.:	2626A09881	Calibration date:	7/17/2008
By:	SCE #S1-01252	Due date:	1/17/2009
Signal generator mfg.:	Hewlett-Packard	Model no.:	3325A
Serial no.:	2652A25647	Calibration date:	4/24/2008
By:	SCE #S1-01347	Due date:	10/24/2008

**SYSTEM SETTINGS:**

Gain:	2
Filter	10KHz
Range:	See sample period in table below
Delay:	0
Stack (1 std)	1
System date = correct date and time	8/1/2008      728

**PROCEDURE:**

Set sine wave frequency to target frequency with amplitude of approximately 0.25 volt peak  
 Note actual frequency on data form.  
 Set sample period and record data file to disk. Note file name on data form.  
 Pick duration of 9 cycles using PSLOG.EXE program, note duration on data form, and save as .sps file. Calculate average frequency for each channel pair and note on data form.  
 Average frequency must be within +/- 1% of actual frequency at all data points.

Maximum error ((AVG-ACT)/ACT\*100)%      As found      0.10%      As left      0.10%

Target Frequency (Hz)	Actual Frequency (Hz)	Sample Period (microS)	File Name	Time for 9 cycles Hn (msec)	Average Frequency Hn (Hz)	Time for 9 cycles Hr (msec)	Average Frequency Hr (Hz)	Time for 9 cycles V (msec)	Average Frequency V (Hz)
50.00	50.00	200	505	180.0	50.00	180.2	49.95	180.0	50.00
100.0	100.0	100	506	90.00	100.0	90.00	100.0	90.00	100.0
200.0	200.0	50	507	45.00	200.0	44.95	200.2	45.05	199.8
500.0	500.0	20	508	18.00	500.0	18.00	500.0	18.00	500.0
1000	1000	10	509	9.000	1000	8.990	1001	9.000	1000
2000	2000	5	510	4.500	2000	4.500	2000	4.505	1998

Calibrated by:	Craig Branson	8/1/2008	<i>Craig Branson</i>
	Name	Date	Signature
Witnessed by:	Robert Steller	8/1/2008	<i>R Steller</i>
	Name	Date	Signature

Suspension PS Seismic Recorder/Logger Calibration Data Form Rev 2.0 July 21, 2008

## GEOVision Borehole Geophysics depth wheel verification

Performed by Robert Steller

	Depth reading in #1	Depth reading out	Depth reading in #2
Depth wheel S/N 101 500 pulse/revolution (gear 1:5, encoder 100 ppr) Circumference = 983mm (3225.07 millifeet)	100.1 feet (30.51 m) September 23, 2006	99.95 feet (30.46 m) September 23, 2006	100.05 feet (30.50 m) September 23, 2006
Depth wheel S/N 103 500 pulse/revolution (gear 1:5, encoder 100 ppr) Circumference = 994mm (3261.15 millifeet)	100.00 feet (30.48) m September 23, 2006	100.00 feet (30.48 m) September 23, 2006	100.00 feet (30.48) m September 23, 2006
Aries winch 200 pulse/revolution (gear 1:1, encoder 200 ppr) Circumference = 305.9mm (1003.51 millifeet)	100.05 feet (30.50 m) September 23, 2006	100.05 feet (30.50 m) September 23, 2006	100.00 feet (30.48 m) September 23, 2006
Robertson Depth wheel For MiniWinch 1000 pulse/revolution (gear 1:1, encoder 1000 ppr) Circumference = 400mm (1312 millifeet)	99.92 feet (30.46 m) Re-verified June 7, 2007	100.10 feet (30.51 m) Re-verified June 7, 2007	99.90 feet (30.45 m) Re-verified June 7, 2007
Robertson Smartwinch 200 S/N 5802 5000 pulse/revolution (gear 1:4, encoder 1250 ppr) Circumference = 404mm (1326 millifeet)	99.99 feet (30.48 m) June 6, 2007	99.97 feet (30.47 m) June 6, 2007	100.00 feet (30.48 m) June 6, 2007
Comprobe winch 500 pulse/revolution (gear 1:1, encoder 500 ppr) Circumference = 1000mm (3.281 feet)	100.1 feet (30.5 m) Re-verified June 7, 2007	100.1 feet (30.5 m) Re-verified June 7, 2007	100.1 feet (30.5 m) Re-verified June 7, 2007

All measurements taken with a Stanley 100-foot flexible stainless steel tape model number 34-130, and a Keeson 300-foot fiberglass tape, both marked in feet, inches and 1/8ths of inches. Enough cable was spooled off of the winch to allow the cable and tape measures to be laid flat on the parking lot surface side-by-side. A permanent marker was used to mark a 100.0-foot interval on the cable, and the marks were also tagged with electrical tape for visibility. The cable was then spooled back onto the winch. When the first mark was at the top of the measuring wheel, a matching permanent mark was placed, and the recording system (Robertson Micrologger) was set to 0.0 feet depth. The cable was spooled in to the second mark, and the distance was recorded. The recording system was set to 0.0 feet again, and the cable spooled out to the first mark again, and the distance was recorded. The process was repeated one more time to spool the cable back onto the winch, and the distance was recorded.

Estimated accuracy is of these measurements is +/- 0.1 foot or +/- 0.03m.

## GEOVision Suspension PS probe Receiver 1–Receiver 2 (R1-R2) spacing verification

Performed by Robert Steller on September 23, 2006

	R2 center to R1 center hanging dry	R2 center to R1 center hanging submerged	R1 bottom to source center hanging submerged with 1m isolation tube S/N 280068	R1 center to source center hanging submerged with 1m isolation tube S/N 280068
Receiver S/N 30086	40.2in 1.02m	40.0in 1.02m	76.0in 1.93m	83.5in 2.12m
Receiver S/N 20042	39.8in 1.01m	39.6in 1.01m	75.7in 1.92m	83.2in 2.11m
Receiver S/N 12008	40.2in 1.02m	40.0in 1.02m	76.0in 1.93m	83.5in 2.12m

All measurements taken with a Lufkin 3.7m flexible steel tape model number HV1034DM, marked in mm and 100<sup>th</sup> of feet. Probe suspended in 3-inch diameter clear PVC pipe, using chain clamp placed between bottom and center of Receiver 2 hard section (See Figure). Probe “bounced” to establish unrestricted hanging length before measurement. Probe allowed to relax for 5 minutes prior to each measurement. Water level set to submerge bottom of Receiver 2 hard section.. Estimated accuracy due to hysteresis in rubber section approximately +/- 0.01’ or +/- 0.003m.





**APPENDIX E**

**BORING GEOPHYSICAL LOGGING**

**FIELD MEASUREMENT PROCEDURES**

# PROCEDURE FOR OYO P-S SUSPENSION SEISMIC VELOCITY LOGGING

## Background

This procedure describes a method for measuring shear and compressional wave velocities in soil and rock. The OYO P-S Suspension Method is applied by generating shear and compressional waves in a borehole using the OYO P-S Suspension Logger borehole tool and measuring the travel time between two receiver geophones or hydrophones located in the same tool.

## Objective

The outcome of this procedure is a plot and table of P and  $S_H$  wave velocity versus depth for each borehole. Standard analysis is performed on receiver to receiver data. Data is presented in report format, with digital data files transmitted in Excel, Word or ASCII format.

## Instrumentation

1. OYO Model 170 Digital Logging Recorder or equivalent
2. OYO P-S Suspension Logger probe or equivalent, including two sets horizontal and vertical geophones, seismic source, and power supply for the source and receivers
3. Winch and winch controller, with logging cable
4. Batteries to operate P-S Logger and winch

The Suspension P-S Logger system, manufactured by OYO Corporation, or the Robertson Digital P-S Suspension Probe with the Robertson Micrologger2 are currently the only commercially available suspension logging systems. As shown in Figure 1, these systems consists of a borehole probe suspended by a cable and a recording/control electronics package on the surface.

The suspension system probe consists of a combined reversible polarity solenoid horizontal shear-wave generator ( $S_H$ ) and compressional-wave generator (P), joined to



two biaxial geophones by a flexible isolation cylinder. The separation of the two geophones is one meter, allowing average wave velocity in the region between the geophones to be determined by inversion of the wave travel time between the two geophones. The total length of the probe is approximately 7 meters; the center point of the geophones is approximately 4 meters above the bottom end of the probe.

The probe receives control signals from, and sends the amplified geophone signals to, the instrumentation package on the surface via an armored 4 or 7 conductor cable. The cable is wound onto the drum of a winch and is used to support the probe. Cable travel is measured by a rotary encoder to provide probe depth data.

The entire probe is suspended by the cable and may be centered in the borehole by nylon "whiskers." Therefore, source motion is not coupled directly to the borehole walls; rather, the source motion creates a horizontally propagating pressure wave in the fluid filling the borehole and surrounding the source. This pressure wave produces a horizontal displacement of the soil forming the wall of the borehole. This displacement propagates up and down the borehole wall, in turn causing a pressure wave to be generated in the fluid surrounding the geophones as the soil displacement wave passes their location.

### **Environmental Conditions**

The OYO P-S Suspension Logging Method can be used in either cased or uncased boreholes. For best results, the uncased borehole must be between 10 and 20 cm in diameter, or 4 to 8 inches. A cased borehole may be as small as 3 inches, if properly grouted (see below) and the grout annulus does not exceed 1 inch.

Uncased boreholes are preferred because the effects of the casing and grouting are removed. It is recommended that the borehole be drilled using the rotary mud method. This method does little damage to the borehole wall, and the drilling fluid coats and seals the borehole wall reducing fluid loss and wall collapse. The borehole fluid is required for the logging, and must be well circulated prior to logging.

If the borehole must be cased, the casing must be PVC and properly installed and grouted. Any voids in the grout will cause problems with the data. Likewise, large grout bulbs used to fill cavities will also cause problems. The grout must be set before testing. This means the grouting must take place at least 48 hours before testing.

For borehole casing, applicable preparation procedures are presented in ASTM Standard D4428/D4428M-91 Section 4.1 (see ASTM website for copy).

### **Calibration**

Calibration of the digital recorder is required. Calibration is limited to the timing accuracy of the recorder. GEOVision's Seismograph Calibration Procedure or equivalent should be used. Calibration must be performed on an annual basis.



## Measurement Procedure

The entire probe is lowered into the borehole to a specific measurement depth by the winch. A measurement sequence is then initiated by the operator from the instrumentation package control panel. No further operator intervention is then needed to complete the measurement sequence described below.

The system electronics activates the SH-wave source in one direction and records the output of the two horizontally oriented geophone axes which are situated parallel to the axis of motion of the source. The source is then activated in the opposite direction, and the horizontal output signals are again recorded, producing a SH-wave record of polarity opposite to the previous record. The source is finally actuated in the first direction again, and the responses of the vertical geophone axes to the resultant P-wave are recorded during this sampling.

The data from each geophone during each source activation is recorded as a different channel on the recording system. The seismograph has at least six channels (two simultaneous recording channels), each with at least a 12 bit 1024 sample record. Newer seismographs may have longer record lengths. The recorded data is displayed on a CRT or LCD display and possibly on paper tape output as six channels with a common time scale. Data is stored on digital media for further processing. Up to 8 sampling sequences can be stacked (averaged) to improve the signal to noise ratio of the signals.

Review of the data on the display or paper tape allows the operator to set the gains, filters, delay time, pulse length (energy), sample rate, and stacking number in order to optimize the quality of the data before recording. In the case of the Model 170, printed data is verified by the operator prior to moving the probe. In the case of the Robertson Micrologger2, storage on the hard disk should be verified from time-to-time, certainly before exiting the borehole.

Typical depth spacing for measurements is 1.0 meters, or 3.3 feet. Alternative spacing is 0.5 meter, or 1.6 feet.

## Required Field Records

- 1) Field log for each borehole showing
  - a) Borehole identification
  - b) Date of test
  - c) Tester or data recorder



- d) Description of measurement
  - e) Any deviations from test plan and action taken as a result
  - f) QA Review
- 2) Paper output records are no longer required, since the Micrologger2 cannot generate them. However, data must be stored in at least 2 places prior to leaving the site
  - 3) List of record ID numbers (for data on digital media) and corresponding depth
  - 4) Diskettes, CD Rom, or USB flash drives with backup copies of data on hard disk, labeled with borehole designation, record ID numbers, date, and tester name.

An example Field Log is attached to this procedure.

## Analysis

Following completion of field work, the recorded digital records are processed by computer using the OYO Corporation software program PSLOG and interactively analyzed by an experienced geophysicist to produce plots and tables of P and S<sub>H</sub> wave velocity versus depth.

The digital time series records from each depth are transferred to a personal computer for analysis. Figure 2 shows a sample of the data from a single depth. These digital records are analyzed to locate the first minima on the vertical axis records, indicating the arrival of P-wave energy. The difference in travel time between these arrivals is used to calculate the P-wave velocity for that 1-meter interval. When observable, P-wave arrivals on the horizontal axis records are used to verify the velocities determined from the vertical axis data. In addition, the soil velocity calculated from the travel time from source to first receiver is compared to the velocity derived from the travel time between receivers.

The digital records are studied to establish the presence of clear SH-wave pulses, as indicated by the presence of opposite polarity pulses on each pair of horizontal records. Ideally, the SH-wave signals from the 'normal' and 'reverse' source pulses are very nearly inverted images of each other. Digital FFT – IFFT lowpass filtering are used to remove the higher frequency P-wave signal from the SH-wave signal.

The first maxima are picked for the 'normal' signals and the first minima are picked for the 'reverse' signals. The absolute arrival time of the 'normal' and 'reverse' signals may vary by +/- 0.2 milliseconds, due to differences in actuation time of the solenoid source caused by constant mechanical bias in the source or by borehole inclination. This variation does not affect the velocity determinations, as the differential time is measured between arrivals of waves created by the same source actuation. The final velocity



value is the average of the values obtained from the 'normal' and 'reverse' source actuations.

In Figure 2, the time difference over the 1-meter interval of 1.70 millisecond is equivalent to a SH-wave velocity of 588 m/sec. Whenever possible, time differences are determined from several phase points on the  $S_H$ -wave pulse trains to verify the data obtained from the first arrival of the  $S_H$ -wave pulse. In addition, the soil velocity calculated from the travel time from source to first receiver is compared to the velocity derived from the travel time between receivers.

Figure 3 is a sample composite plot of the far normal horizontal geophone records for a range of depths. This plot shows the waveforms at each depth, clearly showing the S-wave arrivals. This display format is used during analysis to observe trends in velocity with changing depth.

Once the proper picks are entered in PSLOG, the picks are transferred to an Excel spreadsheet where  $V_s$  and  $V_p$  are calculated. The spreadsheet allows output for presentation in charts and tables.

Standard analysis is performed on receiver 1 to receiver 2 data, with separate analysis performed on source to receiver data as a quality assurance procedure.

Registered Geophysicist *Antony Mertz* Date 9/11/06

QA Review *[Signature]* Date 9/11/06

References:

1. "In Situ P and S Wave Velocity Measurement", Ohya, S. 1986. Proceedings of In-Situ '86, *Use of In-Situ Tests In Geotechnical Engineering*, an ASCE Specialty Conference sponsored by the Geotechnical Engineering Division of ASCE and co-sponsored by the Civil Engineering Dept of Virginia Tech.
2. Guidelines for Determining Design Basis Ground Motions, Report TR-102293, Electric Power Research Institute, Palo Alto, California, November 1993, Sections 7 and 8.
3. "Standard test Methods for Crosshole Seismic Testing", ASTM Standard D4428/D4428M-91, July 1991, Philadelphia, PA

# OYO SUSPENSION P-S VELOCITY LOGGING SETUP

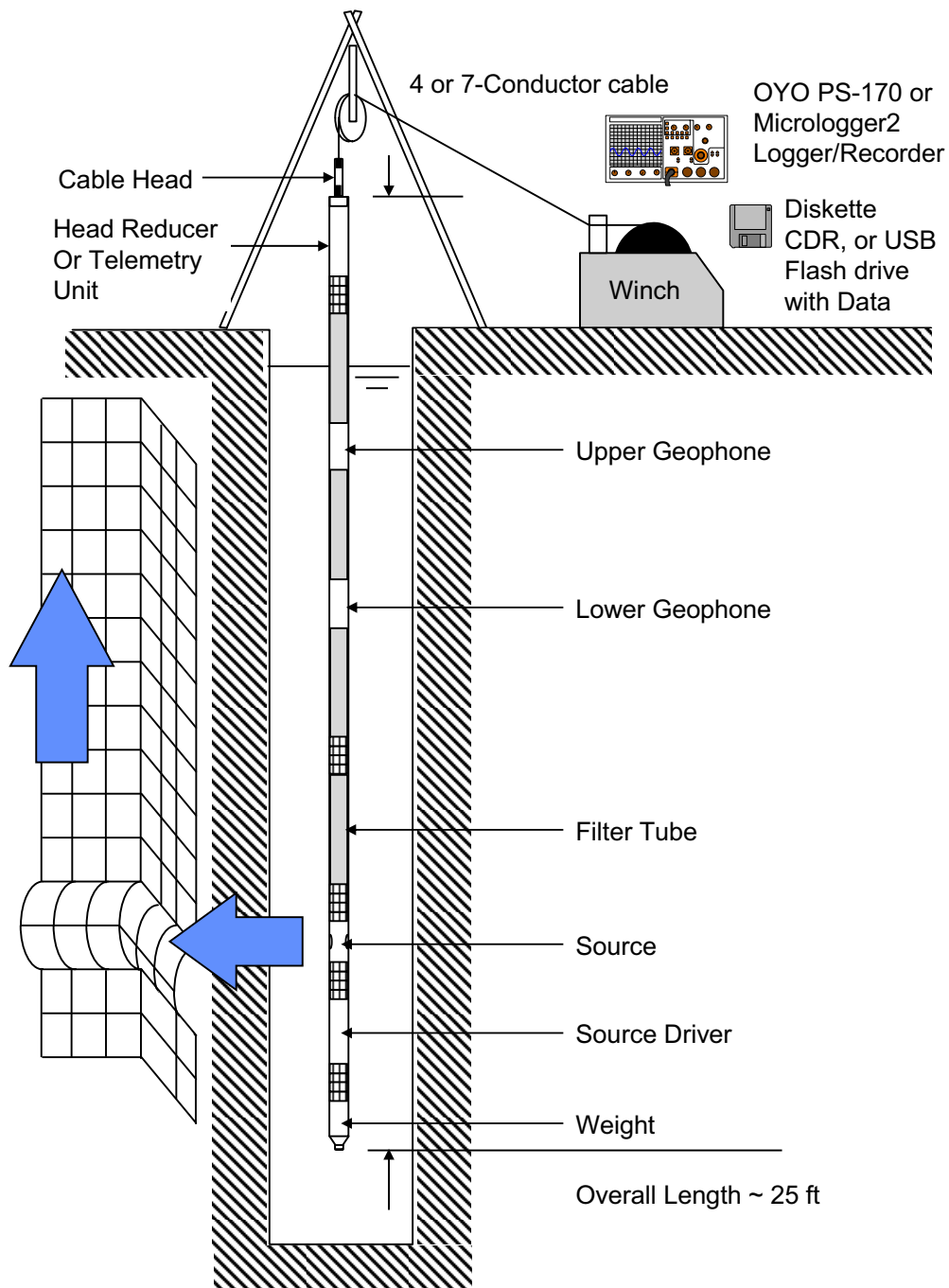


Figure 1. Suspension PS logging method setup

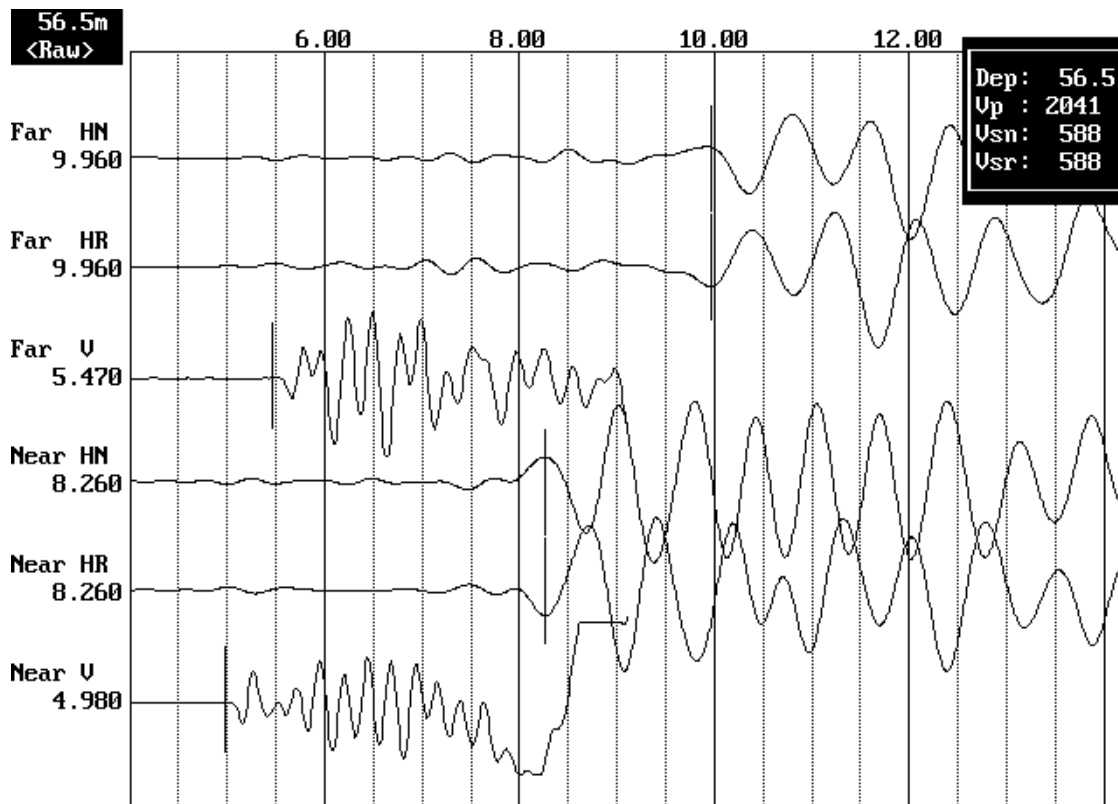


Figure 2. Sample suspension method waveform data showing horizontal normal and reversed (HR and HN), and vertical (V) waveforms received at the near (bottom 3 channels) and far (top 3 channels) geophones. The arrivals in milliseconds for each pick are shown on the left. The box in the upper right corner shows the depth in the borehole and the velocities calculated based on the picks.



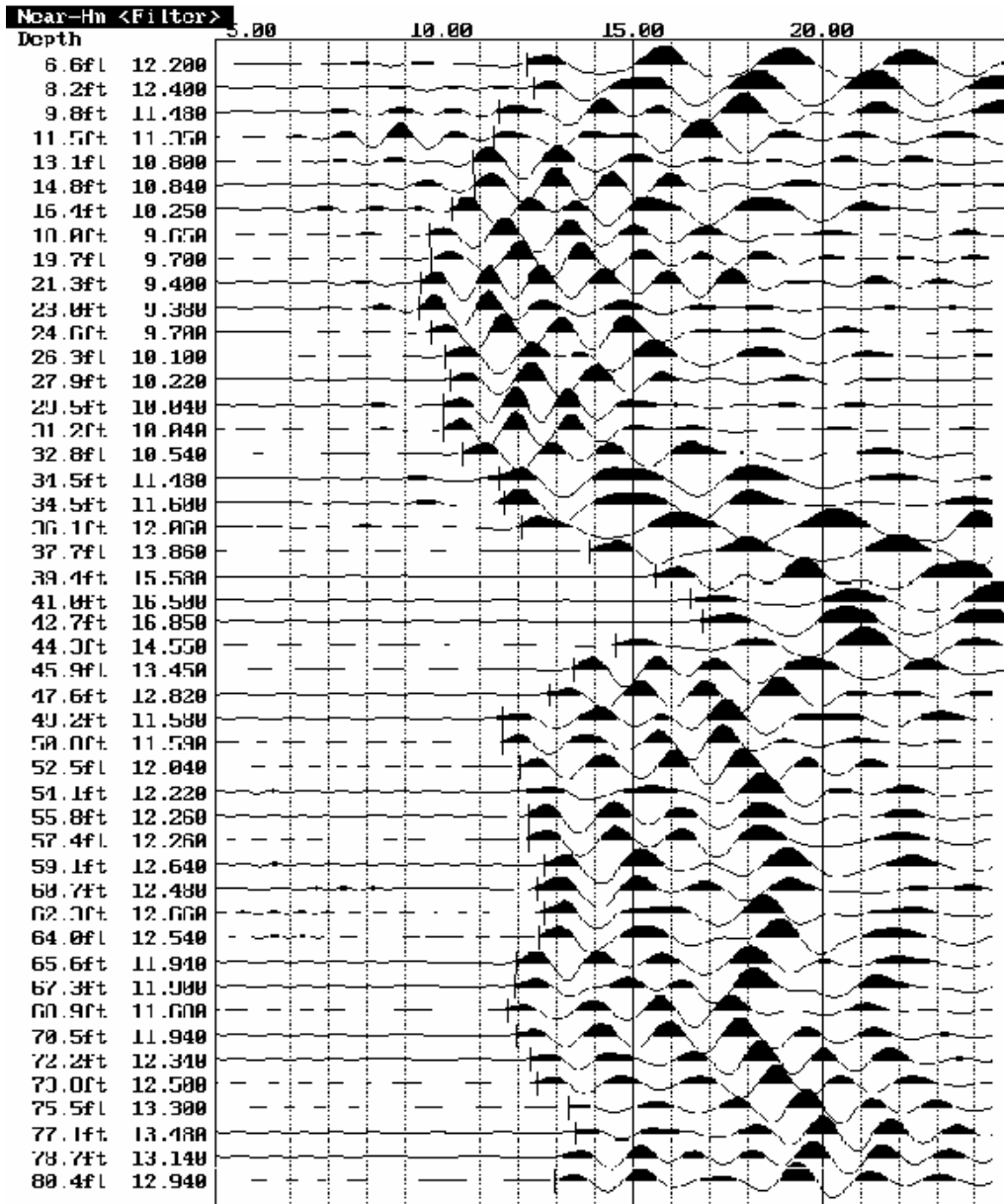


Figure 3. Sample composite waveform plot for normal shear waves received at the near geophone in a single borehole



**P-S SUSPENSION VELOCITY FIELD LOG**

SITE: \_\_\_\_\_ DATE: \_\_\_\_\_

CLIENT: \_\_\_\_\_ JOB: \_\_\_\_\_

AUTHOR: \_\_\_\_\_ PAGE 1 OF \_\_\_\_\_

CONTACT: \_\_\_\_\_ OFFICE PHONE: \_\_\_\_\_

PHONE: \_\_\_\_\_

CONTACT: \_\_\_\_\_ OFFICE PHONE: \_\_\_\_\_

PHONE: \_\_\_\_\_

CONTACT: \_\_\_\_\_ PHONE: \_\_\_\_\_

PHONE: \_\_\_\_\_

CONTACT: \_\_\_\_\_ PHONE: \_\_\_\_\_

PHONE: \_\_\_\_\_

DRILLER: \_\_\_\_\_ PHONE: \_\_\_\_\_

COMPANY: \_\_\_\_\_ PHONE: \_\_\_\_\_

DIRECTIONS TO SITE: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

GENERAL SITE CONDITIONS/LOCATION: \_\_\_\_\_  
 \_\_\_\_\_

EA#: \_\_\_\_\_

BOREHOLE DESIGNATION: \_\_\_\_\_ LOCATION: \_\_\_\_\_

COUNTY: \_\_\_\_\_ RANGE: \_\_\_\_\_ TOWNSHIP: \_\_\_\_\_ SECTION: \_\_\_\_\_

BOREHOLE CONSTRUCTION: CASED \_\_\_\_\_ UNCASD \_\_\_\_\_

DIAMETERS AND DEPTH RANGES: \_\_\_\_\_ 0 TO \_\_\_\_\_ ; \_\_\_\_\_, \_\_\_\_\_ TO \_\_\_\_\_

BOREHOLE TOTAL DEPTH AS DRILLED: \_\_\_\_\_

CONDUCTOR CASING?: YES \_\_\_\_\_ DEPTH TO BOTTOM OF CASING \_\_\_\_\_ ; NO \_\_\_\_\_

DEPTH TO BEDROCK: \_\_\_\_\_ DEPTH TO WATER TABLE: \_\_\_\_\_

BOREHOLE FLUID: WATER \_\_\_\_\_ ; FRESH WATER MUD \_\_\_\_\_ ; SALT WATER MUD \_\_\_\_\_ ;

OTHER: \_\_\_\_\_

DEPTH TO BOREHOLE FLUID: \_\_\_\_\_ TIME SINCE LAST CIRCULATION: \_\_\_\_\_



SITE: \_\_\_\_\_ DATE: \_\_\_\_\_  
CLIENT: \_\_\_\_\_ JOB: \_\_\_\_\_  
AUTHOR: \_\_\_\_\_ PAGE 2 OF \_\_\_\_\_

LOGGING CREW: \_\_\_\_\_  
VEHICLE(S) USED AND MILEAGE: \_\_\_\_\_  
MOBILIZED FROM: \_\_\_\_\_ DEPARTURE TIME: \_\_\_\_\_  
ARRIVED ON SITE: \_\_\_\_\_  
STANDBY TIME: \_\_\_\_\_ CAUSE: \_\_\_\_\_  
LOGGING STARTED: \_\_\_\_\_ LOGGING COMPLETED: \_\_\_\_\_  
STANDBY TIME: \_\_\_\_\_ CAUSE: \_\_\_\_\_  
LOGGING STARTED: \_\_\_\_\_ LOGGING COMPLETED: \_\_\_\_\_  
DEMOBILIZED TO: \_\_\_\_\_ ARRIVAL TIME: \_\_\_\_\_  
ADDITIONAL DEMOB TIME: \_\_\_\_\_ REASON: \_\_\_\_\_

BATTERIES CHANGED BEFORE LOGGING: YES \_\_\_\_\_; NO \_\_\_\_\_; STORED WITH NEW \_\_\_\_\_  
WINCH COMPROBE  GREY  OYO  RG  OTH   
INSTRUMENT OYO 12004  15014  19029  RG 160023  160024   
RECEIVER S/N 12008  20042  26066  11001  23053

MAINTENANCE PERFORMED ON SITE: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

EQUIPMENT PROBLEMS OR FAILURES: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

SUGGESTIONS, ADDITIONS, CHANGES: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

COMMENTS: \_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_  
\_\_\_\_\_

# GEOVISION SUSPENSION LOGGING FIELD NOTES

SITE: \_\_\_\_\_ DATE: \_\_\_\_\_  
 CLIENT: \_\_\_\_\_ JOB: \_\_\_\_\_  
 AUTHOR: \_\_\_\_\_ PAGE \_\_\_\_\_ OF \_\_\_\_\_

DEPTH METERS	DEPTH FEET	UNFILTERED FILE NO.	FILTERED FILE NO.	COMMENTS CASING, WATER, ROCK, ETC
0.5	1.64			
1.0	3.28			
1.5	4.92			
2.0	6.56			
2.5	8.20			
3.0	9.84			
3.5	11.48			
4.0	13.12			
4.5	14.76			
5.0	16.40			
5.5	18.04			
6.0	19.69			
6.5	21.33			
7.0	22.97			
7.5	24.61			
8.0	26.25			
8.5	27.89			
9.0	29.53			
9.5	31.17			
10.0	32.81			
10.5	34.45			
11.0	36.09			
11.5	37.73			
12.0	39.37			
12.5	41.01			
13.0	42.65			
13.5	44.29			
14.0	45.93			
14.5	47.57			
15.0	49.21			
15.5	50.85			
16.0	52.49			
16.5	54.13			
17.0	55.77			
17.5	57.41			
18.0	59.06			

# GEOVISION SUSPENSION LOGGING FIELD NOTES

SITE: \_\_\_\_\_ DATE: \_\_\_\_\_  
 CLIENT: \_\_\_\_\_ JOB: \_\_\_\_\_  
 AUTHOR: \_\_\_\_\_ PAGE \_\_\_\_\_ OF \_\_\_\_\_

DEPTH METERS	DEPTH FEET	UNFILTERED FILE NO.	FILTERED FILE NO.	COMMENTS CASING, WATER, ROCK, ETC
18.5	60.70			
19.0	62.34			
19.5	63.98			
20.0	65.62			
20.5	67.26			
21.0	68.90			
21.5	70.54			
22.0	72.18			
22.5	73.82			
23.0	75.46			
23.5	77.10			
24.0	78.74			
24.5	80.38			
25.0	82.02			
25.5	83.66			
26.0	85.30			
26.5	86.94			
27.0	88.58			
27.5	90.22			
28.0	91.86			
28.5	93.50			
29.0	95.14			
29.5	96.78			
30.0	98.43			
30.5	100.07			
31.0	101.71			
31.5	103.35			
32.0	104.99			
32.5	106.63			
33.0	108.27			
33.5	109.91			
34.0	111.55			
34.5	113.19			
35.0	114.83			
35.5	116.47			
36.0	118.11			

## PROCEDURE FOR USING THE ROBERTSON GEOLOGGING HI-RESOLUTION ACOUSTIC TELEVIEWER (HIRAT)

Reviewed 2/13/06

### Background

The acoustic televiewer is a device for producing a qualitative image of the wall of a borehole. Because it uses ultrasound rather than visible light it is able to work in dirty or opaque borehole fluids, although heavy drilling mud will cause excessive dispersion of the acoustic beam. The picture below shows the sonde's lower nylon section, and one of the bowspring attachments which are used to centralize the sonde in the borehole.



Pulses of ultrasound (0.5 - 1.5MHz) are generated by a piezo-electric resonator. The pulses are transmitted through the oil in which the resonator is immersed, through the wall of the acoustic housing, then propagate through the borehole fluid and are reflected from the wall of the borehole. The reflected energy is picked up by the same transducer, from which is recorded both the **amplitude** of the returned pulse and the **travel-time** which have elapsed. Blanking must be applied to prevent the transducer from registering reflections from the inside surface of the acoustic housing. The material of the housing is chosen so that its acoustic properties are similar to the oil which fills it. The housing is not designed to withstand borehole fluid pressures, but has a piston device to allow equalization between inside and outside pressure.

The **amplitude** of the returned pulse is a function of the acoustic reflectivity of the borehole wall. If the beam strikes a hard borehole wall normally to the surface the energy will be returned to the transducer and a strong return will be recorded. If the formation is softer, then less energy will be reflected. Also, if the surface of the borehole is rough, or effectively missing because of the presence of a fracture or other structure, then energy will be dispersed and a poor return will be recorded.

The **travel-time** is a simple function of the diameter of the borehole and the velocity of sound in the borehole fluid (typically 1.5Km/sec). An A/D converter monitors the output from the transducer once the blanking period has expired and a comparator is used to detect the peak amplitude during the sampling window.

The coaxially-mounted transducer has a planar radiating surface, but the vibration characteristics are such that the acoustic pulse is emitted as a 'pencil' beam. The emitted beam is deflected by a planar mirror so that it leaves the acoustic housing at right angles to the sonde axis. The mirror is rotated to scan the borehole wall. The ultrasound pulses are synchronized with rotation of the mirror so that up to 360 pulses are emitted in every revolution. Because of the time which must elapse for the two-way transit of the borehole fluid, there is an upper limit upon the number of radial samples that may be acquired from a borehole of a particular radius. In larger boreholes, therefore, it may be necessary to reduce the number of radial samples. The sonde is able to operate at 90, 180 or 360 samples per revolution.

An image of the borehole wall is produced by moving the sonde along the borehole axis while it is scanning radially. By the same logic as shown above, it can be seen that any horizontal point will be imaged by more than one sweep of the acoustic beam so long as the axial movement of the sonde during one complete sweep is no greater than the beam diameter. An upper limit is therefore imposed upon the logging speed which will be a function of the rotational speed of the transducer, the radial sampling interval and borehole diameter.

## Objective

The objective of this procedure is to provide a pseudo “core” of the borehole, and map the orientation and angles of cracks and voids in rock boreholes.

## Instrumentation

This procedure is written specifically for the Robertson Geologging High-Resolution Acoustic Televiwer (HiRAT). The required equipment includes:

1. The Robertson High-Resolution Acoustic Televiwer (HiRAT) sonde with centralizers
2. A 4-conductor wire-line winch with cable at least 30m (100ft) longer than the depth of the borehole (RG Smart Winch or equivalent. GEOVision has adapted all our 4-conductor winches)
3. A sheave with depth encoder with minimum 500 pulse/revolution
4. A Robertson Geologging Micrologger II
5. A laptop with Winlogger installed and the following minimum system requirements:
  - Windows 98SE or above
  - 64M System memory
  - 800x600x24 SVGA Display with DirectX 8.0
  - 500Mhz CPU
  - USB 2.0 connection
6. Battery power supply with cables

## Environmental Conditions

This tool is designed for fluid-filled boreholes between 67 and 150mm (3-6in) in rock. Since fine cracks are usually not visible in the walls of soil borings, the televiwers add very little information from a soil boring than a simple video. Now if the boring has soil AND rock, televiwer visuals in the soil may still be useful.



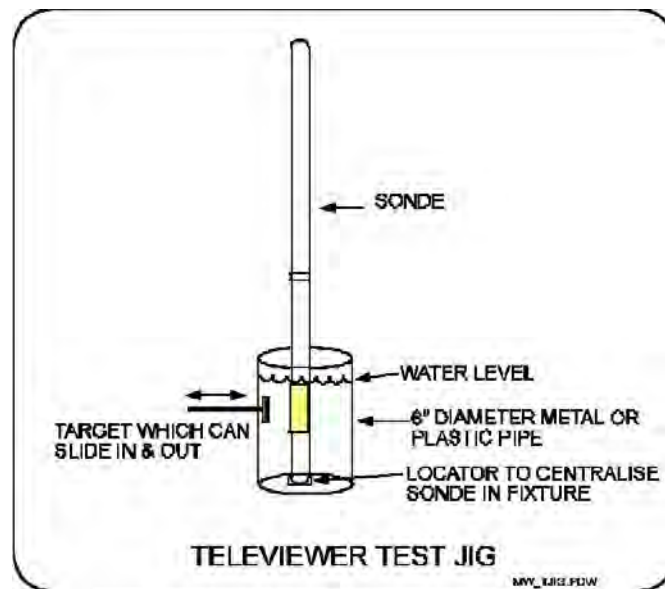
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## Calibration

The acoustic televiewer uses the variability in reflectance and the travel time to make an image of the borehole wall, mostly resulting from relative differences of materials and the physical characteristics of the wall. Since these are relative measurements, no field calibration of the sonde is required. However, it is important that the same location in the borehole be checked at the start and finish of the logging to make sure that the response or functionality haven't changed during the measurement.

A test fixture may be used to check function of the acoustic televiewer prior to use. This test fixture should comprise a plastic pipe, with a known internal diameter between 3 and 6 inches. This should be filled with water and the sonde stood upright in the fixture. A target made of metal or metal foil is glued on the inside of the container, or optionally on a seal and shaft so that it can be moved in and out on a line radial to the center-line of the pipe. A representation of this is shown in the figure below.

The purpose of this test fixture is to check the ability of the sonde to differentiate between materials of different acoustic reflectances, and different travel times, and to check the calibration of the caliper function of the sensor using the measured diameter of the pipe. However, if calibrated caliper measurements are required, it is recommended that a mechanical 3-arm caliper tool be used for this purpose because it can be calibrated in the field prior to use. The HiRAT will give very accurate results but this procedure does not cover calibration.



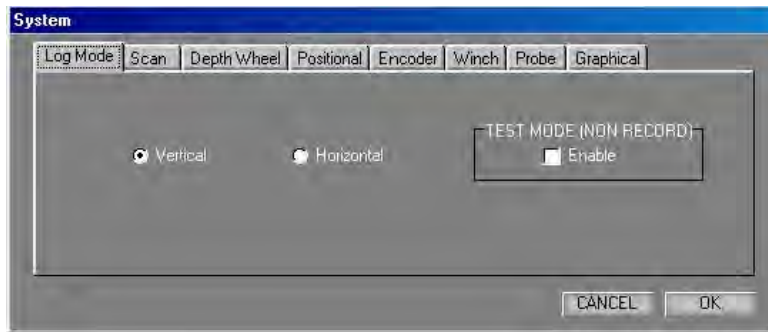


## Hi-RAT Field Procedure

Because the logging software is a standalone module, there are a number of settings which must be initialized independently of the WinLogger software. These include the depth measurement subsystem and sonde operating modes. Click on 'System' on the menu bar to show the following dialog boxes:

### 1.0 Log Mode

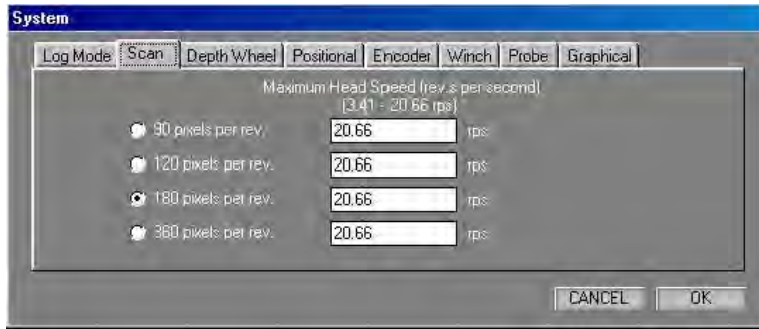
The sonde can operate in three distinct modes:



- Vertical mode is used for boreholes which are drilled from the surface and are deviated at less than 70 degrees from the vertical. Most exploration boreholes will fall into this class. In this mode the image is orientated according to compass directions (magnetic co-ordinates).
- Horizontal mode is used for boreholes which are sub-horizontal so their inclination will probably exceed 70 degrees from the vertical. Boreholes in this class would normally be drilled as part of ground investigations for tunneling and mining, drilling ahead of a drive to determine the nature and extent of fracturing. In this mode the image is orientated according to gravitational coordinates (up/down) since there is no unique point of the image circle which can be orientated to North with any precision.
- Test mode is used to exercise all sonde functions without creating a log. The image will scroll on the screen in the normal fashion, and orientation readouts will be refreshed continuously.

### 2.0 Scan Parameters

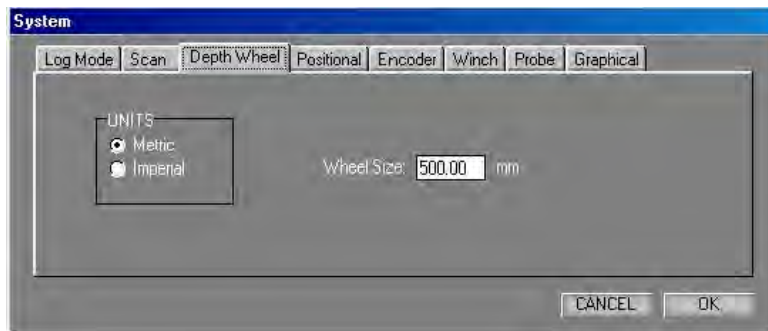
The scan parameters control the radial sampling of the borehole. The values will be retained between logging sessions, so the sonde will be initialized correctly at power-on. There are three parameters in the dialog:



- The radial sampling rate can be set to one of 90, 120, 180, 360 samples per revolution. There is a relationship between the logging speed and the radial sampling rate, since the time taken to send the dataset to the surface depends upon its length. The size of the log file is also determined by the radial sampling rate. The probe will always try to use the maximum head speed entered. If limited by a low Baud rate or a large 'window' setting then the probe will reduce its head speed automatically to compensate - see sonde operation section.

### 3.0 Depth Wheel Configuration

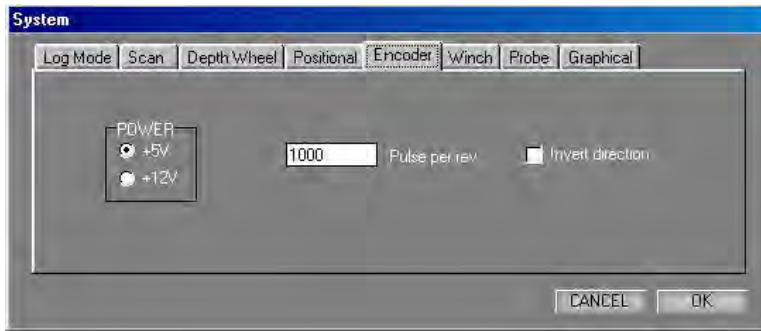
The depth measurement system is dependent upon the combination of depth measurement wheel with its calibrated groove, and the shaft encoder which translates rotation into pulses which are counted by the logging system controller. Two parameters are therefore required: depth wheel circumference and encoder pulse rate. The encoder parameters are covered in a subsequent topic.



- Select Metric or Imperial depth measurement units from the left-hand pane.
- Type the circumference of the depth measurement wheel into the 'wheel size' box. The standard sizes of GEOVision wheels are 1000mm. If you are measuring in Imperial units (or changing back to metric units), the standard wheel size can be converted automatically by clicking the left mouse button and choosing the appropriate conversion. The size is always specified in units of 1/1000 of the depth unit i.e. millimetres (mm) or millifeet (mft).

#### 4.0 Encoder Configuration

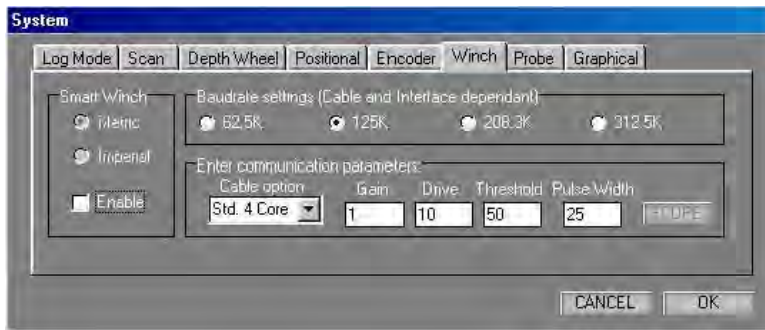
The depth measurement system is dependent upon the combination of depth measurement wheel with its calibrated groove, and the shaft encoder which translates rotation into pulses which are counted by the logging system controller. The depth wheel circumference is covered in a previous topic. In order to accommodate a variety of encoders, their operational characteristics can be configured in the software.



- Select supply voltage from the radio buttons in the left-hand pane. The options are 5 Volt and 12 Volt. GEOVision encoders are always specified for 5 Volt operation.
- Type the number of pulses emitted per revolution into the central box. The standard values for all GEOVision winches are 500 pulses/rev.
- The logical direction of movement can be reversed if required to accommodate the directional characteristics (phase lead or lag) of the different encoder types.

#### 5.0 Winch and Cable Configuration

Support for remote control of the RG Smart Winch is provided, and can be enabled by checking the **Enable** control in the left-hand Smart Winch pane. If the Smart Winch control is enabled, it is also necessary to select the measure units in force - select **Metric** or **Imperial** from the radio buttons on offer.



The Baud settings can be chosen to match the *quality* of the communication channel. The channel will be effected by cable type and length. Typically a Baudrate of 312.5K is used. The remaining controls in the dialog relate to the communications parameters. The operation is entirely compatible with the WinLogger software operation and the values would be expected to be the same as those in force for logging six-channel type sondes with that software. (Certain probe types may be fitted with a digital interface that does not require set-up and in this case the parameter edit boxes will not appear.)

- **Cable Option** is used to select the logging cable type which is available on the winch. The options are *Not Connected, Std. 4 Core, Differential* and *Monocable*. The only cable types used in GEOVision systems is Std. 4 Core. Select the appropriate type from the drop-down menu box. Note this value can only be changed when the probe power is turned off.
- **Gain** is related to cable length and uphole signal attenuation. Gain values range from 0-3 and control the amplification applied to the incoming signal. Use the *Scope* dialog to visualize the incoming signals. Gain should be set so that the signal reaches between 70% and 100% of the height of the display, generally obtained with a setting of 0 for GEOVision winches. If the peak height exceeds this level, clipping will result in artifacts which will be detected erroneously. Click *Apply* to set the parameters before proceeding to the *Scope* dialog.
- **Threshold** is the level at which the incoming signals are detected. Gain and Threshold are related, and can be visualized using the *Scope* dialog. Set the gain so that the signal reaches between 70% and 100% of the height of the display. Then adjust the threshold so that it is between 50% and 70% of the height of the pulses displayed and clear of any region of 'overshoot' of the positive and negative pulses. This will ensure that peaks are detected and noise is ignored. Generally a setting of 25 is used for GEOVision winches. When the scope dialog is displayed, the position of the mouse is reported as a threshold value to make it simpler to infer the correct setting. The scope option is greyed out when the probe power is turned off.
- **Drive** sets the strength of the downhole signal. It is not possible to visualize the downhole signal, but the effect of insufficient drive is to disable downhole communication, which will result in the commands being ignored by the sonde. Values range from 0 -127, and for GEOVision winches will be around 10. Increase the drive for longer cables.
- **Pulse Width** This is the width of the transmitted communication pulses in 100nS steps. The default is 25 equivalent to 2.5uS. The range is from 8 to 64. The pulse width can be reduced to prevent signal overshoot on short cables. The default value is used in most cases. Note any changes only come into effect during a log. (Note setting too large a pulse width when using the highest Baud rates will automatically be prevented within the probe and the pulse width reduced.)

**IMPORTANT** Please note the effects of changing 'Baud' will not appear until the first new log is made. The setting for 'threshold' may be effected by an increase in the 'Baud' rate please recheck 'threshold' if 'Baud' is altered using the 'Scope' function after making a short test log.

The parameters which are entered will be applied automatically if you close the dialog with **OK**. The above parameters once set correctly will be remembered by the system and should never need to be altered.

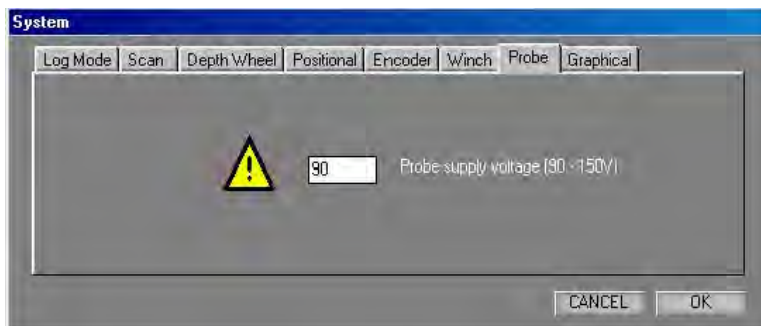
## 6.0 Probe Configuration

The probe is normally energized at 90 Volts from the surface. However, it may be necessary to compensate for voltage drop on longer cables due to the higher power draw of this sonde. The voltage at



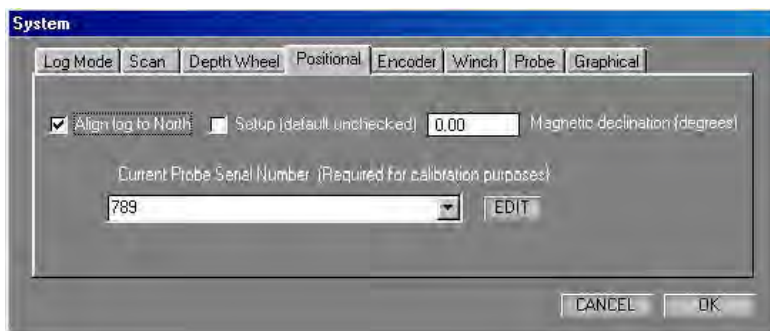
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the surface may be increased in order to deliver 90 Volts at the sonde. Simply type the value into the text box provided. The voltage should be set at 90V for all GEOVision winches. Values outside the indicated range will be rejected.



## 7.0 Positional Configuration

The probe includes a 3-axis orientation package, and is capable of producing a borehole image aligned to geographic North. This is achieved by determining and applying two image rotation parameters:



- **Magnetic Declination** is used to correct for the difference between Magnetic North and True North. The value varies from place to place, so the local value must be inserted here if you wish to perform this correction during data collection. This correction may also be made during processing. If the value is zero, the log will be referred to Magnetic North.
- **Align to North** is a check-box used to select image rotation to start at Magnetic North. If in addition a value is set for Magnetic Declination (see above) the image will be rotated to start at True North. If the box is not checked, the image will not be oriented to geographic co-ordinates, but will use the local co-ordinate frame of the sonde (X, Y, Z axis of the orientation module). This mode may be used to inspect the inside of magnetic casing, where an orientated image would be subjected to random effects caused by the metalwork.
- Set-up mode is selected by checking the **Setup** box, and is used to determine the required image rotation offset to correct for the angle between the axis of the orientation package and the index mark of the rotating transducer section. In set-up mode the normal sonde azimuth display is modified, and will instead show the 'relative bearing' which is measured between the high side of the borehole and the orientation sensor index. Check **Setup**, then OK to close the dialog. The icon adjacent to the sonde azimuth readout at the top of the screen is modified with the legend CAL when the system is in set-up mode. The sonde must now be placed in a stand or jig so that it

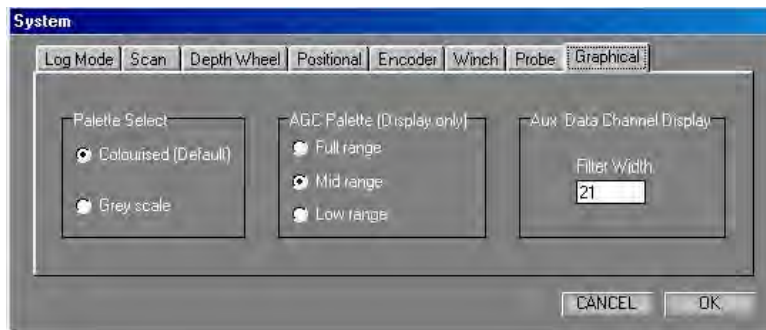


is inclined at about 20 degrees to the vertical, and adjacent to a target fixed to the jig so that it is directly above the transducer in the vertical plane. Lower the sonde with its attachment into a large bucket of water so that the transducer and target are fully immersed. Start the radial amplitude display, when it will be possible to see the strong signal returning from the target. Rotate the sonde so that the image of the target moves to the top of the display. When the two are coincident, the 'relative bearing' reads out the image rotation offset. This value is fixed for the sonde unless it is disassembled and rebuilt, at which point the procedure MUST be repeated. Please see the additional topic on the Radial Amplitude Display for further details.

- The **Serial Number** list box is used to select the sonde which is in use. When the appropriate sonde is selected, the image rotation offset determined by the above procedure is selected. To edit the image offset click the **'Edit'** and enter the new offset. Several serial numbers and associated offsets can be stored and selected as required.

## 8.0 Graphical

The palette can be changed between a colored and grey scale setting. The changes affect the log screen palette display and are also applied when replaying a log. Selecting Full range in the 'AGC Palette' will cause the software to spread the palette over the full 16bit signal. 'Mid range' will spread the palette over the first quarter of the 16bit range and 'Low range' will spread the palette over the first eighth of the 16 bit range. In most cases the 'Low range' selection is used. Note these settings do not affect the stored log data in any way. The 'Filter Width' is applied to the Natural Gamma trace data and is a simply running average filter. The range of the filter width is from 1 to 50 ( x 10 millidepth units ie. mm or mft).



## 9.0 Sonde Operation

When the operations specified above have been reviewed and the correct settings have been selected, the system is ready for use. The main screen area is divided into 3 horizontal elements. At the top is the depth and orientation readout, together with the scale headings for the scrolling display of unwrapped borehole image.

On the left side of the depth track is the travel time display, with text boxes for sonde inclination, azimuth and head temperature.



On the right side is the display of amplitude and indication of current operating mode. Located in the center above the depth track are the text boxes for depth and cable speed (computed at the surface). The ranges for the 'Natural Gamma' channel overlay (optional) are shown above the Amplitude.



The central area is utilized for the scrolling display of unwrapped borehole data. The display is orientated with the left edge corresponding to North point of the aligned image data (if orientation is selected) according to the outputs of the sonde's orientation package.

The lower area has controls for the winch (applicable to RG Smart Winch only), depth initialization and sonde control.



The winch control area is only displayed when RG SmartWinch operation is enabled - see section 5 - and has four controls. Set Target Speed by typing the required speed into the window and pressing Enter.

Cable movement is initiated by clicking on either the UP or DOWN arrow control.

Cable movement is halted by clicking on the square STOP control.



Depth is initialized by typing the required value into the entry box and pressing Enter. The entry box is not available at times when the system is in logging mode and the depth should not be changed by user entry.

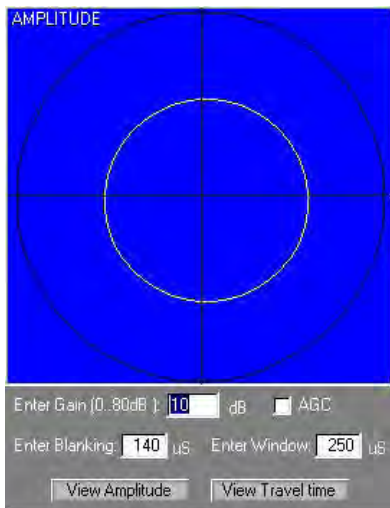
Sonde power is applied by clicking on the green-colored 1 button. Power is turned off by clicking on the red-colored 0 button. There is no indicator for the state of the power supply on the desktop, so the external indicators should be observed for this purpose.

To make a log ensure that the Test Mode is disabled - see section 1, Log Mode setting. Click File|New Log and select a filename. Old logs may be overwritten if necessary -TAKE CARE. The header editor will be started automatically. A previous set of header data may be loaded by clicking LOAD and choosing a template.

To start logging, click on the red Record (circle) control. The log data will start to scroll down the screen after a brief pause for synchronization. The messages "DSP2: Detecting data stream" and "Updating probe settings" will be observed at the bottom of the screen during this process. Note that the screen scrolling direction is not affected by the actual direction of movement of the sonde. To cease logging, click on the black STOP control (square). The data should be immediately backed up to a USB drive, CD, or other data storage prior to beginning another log.

If the data display from a probe which is properly connected appears to occupy only half of the track area,

with the remainder filled with random colors such as green which are not part of the regular palette, then it is most likely that the downhole data communication is not functioning properly. This symptom is due to the fact that the probe settings cannot be communicated properly, and it is operating in its default power-up mode. If this is the case, the Drive setting of the System|Winch dialog should be increased or decreased accordingly. See section 5 for full details.



To adjust the sonde gain it is necessary to use the Radial Amplitude plot, which is enabled by clicking on the circle with cross-hairs symbol. When the dialog is active a new window will open on top of the unwrapped data display. In this display, the data is presented as a 'polar' plot. Press the 'View Amplitude' button to display the amplitude plot. This plot shows amplitude increasing towards the outside of the circle and the compass direction following the sweep of the transducer. The line indicating the data is drawn in the regular palette, so that high amplitudes are drawn in white and low amplitudes in black/brown. The picture here shows the image of the inside of a cylinder.

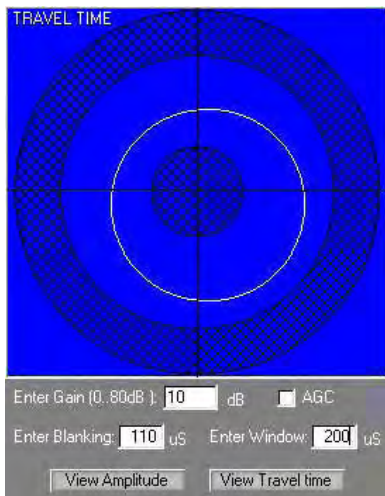
If the data is concentrated in a small circle at the center, the gain is too low and should be increased. If the data is obviously clipped at the outside of the circle, then the gain should be reduced. Type the new gain value into the entry box and press Enter. The ideal would be to set a gain value which allows the peak values to be displayed without clipping, with the majority of the data around the half-way level. It may also be necessary to adjust the blanking to ensure that internal reflections from the acoustic housing are not detected at the new gain value. This will be apparent in the unwrapped data display as pronounced patterning unrelated to the true target. The AGC option causes the probe to set gain automatically thus preventing signal saturation in most cases. (The gain is varied in 6dB steps

Blanking Period and window length can be set independently. Blanking is set to avoid reflections from the housing of the acoustic transducer or random reflections from a rugose borehole, and window length is set to accommodate the range of borehole radius that might be expected. An error will be indicated if the sum of the blanking period and window length would be greater than 409 microseconds, which is the maximum range of the timer. The default value for the blanking period is 145 microseconds, which is the minimum required for the two-way transit from the transceiver to the outer surface of the acoustic housing. It is not advisable to reduce this value beyond the default setting, although it may be increased for larger boreholes at the rate of 1.5mm of one-way travel per microsecond.

Window Length (sample time) defines the period during which the arrival gate remains open to detect the returned acoustic pulse. The acoustic pulse will travel in water at a speed of approximately 1.5mm per microsecond. The default window length is 150 microseconds, which is equivalent to 225 mm of (two-way) travel in the borehole fluid, or approximately 110mm of borehole diameter. If this is added to the default blanking period, which is equivalent to the outside diameter of the acoustic housing, it can be seen that the default set-up will be correct for boreholes up to 150mm. An error will be indicated if the sum of the blanking period and window length would be greater than 409 microseconds, which is the maximum range of the timer. Choose your window setting to best match the borehole diameter.



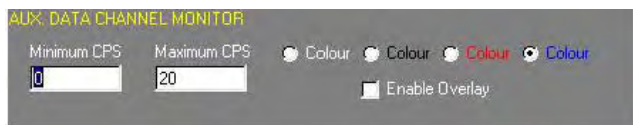
Pressing the 'View Travel time' button changes the display to that shown below:



The un-hatched ring between the two cross hatched zones represents the sample window. The width of this ring will vary with window length value. The profile of a cylinder is represented here appearing as a circle in the sample window.



Pressing this button displays the following dialog box:



This box allows you to enable the Natural Gamma option by checking the 'Enable Overlay' check box. The Overlay appears as a trace upon the Amplitude plot. The trace range and color can also be set by

this dialog. The level of filtering can also be altered (see section 8) (note that any displayed trace data is automatically aligned with the acoustic scan data but only when logging up. The Natural Gamma sensor occupies a higher position in the probe so sufficient data has to be prebuffered so that the acoustic data can depth aligned with gamma. The prebuffering results in a delay at the start of a log before correct gamma data appears this is normal.)

## Data Analysis and Interpretation

RG-DIP, the manufacturer's image interpretation package, offers manual and automatic feature recognition options. Feature orientations (dip/strike and azimuth) are automatically calculated. Display options include stereographic projections of zone axes, orientation frequency plots and 'synthetic cores' for comparison with real core data. The last option is invaluable for orientating core samples, particularly in the case of incomplete recovery.



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## Reporting

The final report will include the objective and scope of the survey, location of the boreholes, discussion of instrumentation and procedures in the field and lab. For each borehole there will be a plot showing the dip/strike and azimuth of features. The next page shows an example.

Assumptions and limitations of the results will be discussed. Supporting references will be listed as necessary

## Required Field Records

Field log for each borehole showing

- a) Location and description of the borehole
- b) Date of test
- c) Field personnel
- d) Instrumentation
- e) Any deviations from test plan and action taken as a result

This procedure has been reviewed and approved by the undersigned:

Professional Geophysicist Antony Merta Date Feb 13, 2006

QA Review [Signature] Date Feb 13, 2006



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