WESTSIDE SUBWAY EXTENSION

Air Quality
Technical Report

Metro

August 2010

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Acronyms and Abbreviations

AA	Alternatives Analysis
AADT	average annual daily traffic
ADA	*Americans with Disabilities Act* (42 USC 126)
APM	automated people mover
CAA	U.S. Clean Air Act
CAAA	Clean Air Act Amendments
CAAQS	California Ambient Air Quality Standards
CalEPA	California Environmental Protection Agency
Caltrans	California Department of Transportation
CARB	California Air Resource Board
CCAA	California Clean Air Act
CCTV	closed-circuit television
CEQ	President's Council on Environmental Quality
CH_4	methane
CO	carbon monoxide
CSOP	control standard operating procedure
DE	diesel exhaust
DPM	diesel particulate matter
EIR	environmental impact report
EIS	environmental impact statement
USEPA	U.S. Environmental Protection Agency
Expo I	Exposition Boulevard Light Rail Phase 1
Expo II	Exposition Boulevard Light Rail Phase 2
FAI	fresh air intakes
GLAVA	Greater Los Angeles Veterans Administration
HAP	hazardous air pollutant
HC	hydrocarbons
HEI	Health Effects Institute
HOV	high-occupancy vehicle
HRT	heavy rail transit
HRV	heavy rail vehicles
I-10	Interstate 10 Freeway

I-405	Interstate 405 Freeway
IRIS	Integrated Risk Information System
ISTEA	*Intermodal Surface Transportation Efficiency Act of 1991*
LADOT	Los Angeles Department of Transportation
LAWA	Los Angeles World Airports
LAX	Los Angeles Airport
LOS	level of service
LPA	Locally Preferred Alternative
LRT	light rail transit
LRTP	Long Range Transportation Plan
Metro	Los Angeles County Metropolitan Transportation Authority
$\mu g/m^3$	micrograms per cubic meter
MOS	minimum operable segments
mph	miles per hour
MSAT	mobile source air toxic
NAAQS	National Ambient Air Quality Standards
NH_3	ammonia
NO	nitric oxide
NO_2	nitrogen dioxide
NOA	naturally occurring asbestos
NO_x	nitrogen oxide
O_3	ozone
OTE	over track exhaust
PAH	polycyclic aromatic hydrocarbons
Pb	lead
PM	particulate matter
$PM_{2.5}$	particulate matter smaller than or equal to 2.5 microns in size
PM_{10}	particulate matter smaller than or equal to 10 microns in size
POM	polycyclic organic matter
ppm	parts per million
PTEL	passenger assistance telephones
RCEM	road construction emissions model
ROC	Rail Operations Center

ROG	*reactive organic gases*
RTIP	*Regional Transportation Improvement Plan*
RTP	*Regional Transportation Plan*
SCAB	South Coast Air Basin
SCAG	Southern California Association of Governments
SCAQMD	South Coast Air Quality Management District
SIP	state implementation plan
SMAQMD	Sacramento Metropolitan Air Quality Management District
SO_2	sulfur dioxide
SOP	standard operating procedure
TAC	toxic air contaminant
TEA-21	*Transportation Equity Act for the 21st Century*
TIP	Transportation Improvement Program
TOG	total organic gases
TPIS	transit passenger information system
TPSS	traction power substation
TSM	transportation system management
TVM	ticket vending machines
UPE	under platform exhaust
UPRR	Union Pacific Railroad
URBEMIS	Urban Emissions Model
VA	Veterans Affairs
VHT	vehicle hours traveled
VMT	vehicle miles traveled
VOC	volatile organic compounds
vpd	vehicles per day

1.0 INTRODUCTION

This Air Quality Technical Report has been prepared in support of the Westside Subway Extension. The objective of this report is to evaluate the project's potential air quality impacts within the study area and suggest mitigation measures for significant impacts where feasible. This includes the following:

- Evaluate the project's impact on regional air quality levels
- Evaluate whether this project will cause or contribute to a new localized exceedance of CO ambient air quality standards or increase the frequency or severity of any existing exceedance
- Evaluate potential particulate matter (PM_{10} and $PM_{2.5}$) impacts of the project
- Evaluate the mobile source air toxic (MSAT) impacts of the project
- Evaluate the construction emissions of the project and compare estimated vehicle and fugitive dust emissions with South Coast Air Quality Management District significance thresholds

The related climate change issues, including greenhouse gas emissions, are addressed in a separate Climate Change Technical Report.

2.0 PROJECT DESCRIPTION

This chapter describes the alternatives that have been considered to best satisfy the Purpose and Need and have been carried forward for further study in the Draft Environmental Impact Statement/Environmental Impact Report (EIS/EIR). Details of the No Build, Transportation Systems Management (TSM), and the five Build Alternatives (including their station and alignment options and phasing options (or minimum operable segments [MOS]) are presented in this chapter.

2.1 No Build Alternative

The No Build Alternative provides a comparison of what future conditions would be like if the Project were not built. The No Build Alternative includes all existing highway and transit services and facilities, and the committed highway and transit projects in the Metro LRTP and the SCAG RTP. Under the No Build Alternative, no new transportation infrastructure would be built within the Study Area, aside from projects currently under construction or projects funded for construction, environmentally cleared, planned to be in operation by 2035, and identified in the adopted Metro LRTP.

2.2 TSM Alternative

The TSM Alternative emphasizes more frequent bus service than the No Build Alternative to reduce delay and enhance mobility. The TSM Alternative contains all elements of the highway, transit, Metro Rail, and bus service described under the No Build Alternative. In addition, the TSM Alternative increases the frequency of service for Metro Bus Line 720 (Santa Monica–Commerce via Wilshire Boulevard and Whittier Boulevard) to between three and four minutes during the peak period.

In the TSM Alternative, Metro Purple Line rail service to the Wilshire/Western Station would operate in each direction at 10-minute headways during peak and off-peak periods. The Metro Red Line service to Hollywood/Highland Station would operate in each direction at five-minute headways during peak periods and at 10-minute headways during midday and off-peak periods.

2.3 Build Alternatives

The Build Alternatives are considered to be the “base” alternatives with “base” stations. Alignment (or segment) and station options were developed in response to public comment, design refinement, and to avoid and minimize impacts to the environment.

The Build Alternatives extend heavy rail transit (HRT) service in subway from the existing Metro Purple Line Wilshire/Western Station. HRT systems provide high speed (maximum of 70 mph), high capacity (high passenger-carrying capacity of up to 1,000 passengers per train and multiple unit trains with up to six cars per train), and reliable service since they operate in an exclusive grade-separated right-of-way. The subway will operate in a tunnel at least 30 to 70 feet below ground and will be electric powered.

Furthermore, the Build Alternatives include changes to the future bus services. Metro Bus Line 920 would be eliminated and a portion of Line 20 in the City of Santa Monica would be eliminated since it would be duplicated by the Santa Monica Blue Bus Line 2. Metro Rapid

Bus Line 720 would operate less frequently since its service route would be largely duplicated by the Westside Subway route. In the City of Los Angeles, headways (time between buses) for Line 720 are between 3 and 5 minutes under the existing network and will be between 5 and 11.5 minutes under the Build Alternatives, but no change in Line 720 would occur in the City of Santa Monica segment. Service frequencies on other Metro Rail lines and bus routes in the corridor would be the same as for the No Build Alternative.

2.3.1 Alternative 1—Westwood/UCLA Extension

This alternative extends the existing Metro Purple Line from the Wilshire/Western Station to a Westwood/UCLA Station (Figure 2-1). From the Wilshire/Western Station, Alternative 1 travels westerly beneath Wilshire Boulevard to the Wilshire/Rodeo Station and then southwesterly toward a Century City Station. Alternative 1 then extends from Century City and terminates at a Westwood/UCLA Station. The alignment is approximately 8.60 miles in length.

Alternative 1 would operate in each direction at 3.3-minute headways during morning and evening peak periods and at 10-minute headways during midday. The estimated one-way running time is 12 minutes 39 seconds from the Wilshire/Western Station.

2.3.2 Alternative 2—Westwood/Veterans Administration (VA) Hospital Extension

This alternative extends the existing Metro Purple Line from the Wilshire/Western Station to a Westwood/VA Hospital Station (Figure 2-2). Similar to Alternative 1, Alternative 2 extends the subway from the Wilshire/Western Station to a Westwood/UCLA Station. Alternative 2 then travels westerly under Veteran Avenue and continues west under the I-405 Freeway, terminating at a Westwood/VA Hospital Station. This alignment is 8.96 miles in length from the Wilshire/Western Station.

Alternative 2 would operate in each direction at 3.3-minute headways during the morning and evening peak periods and at 10-minute headways during the midday, off-peak period. The estimated one-way running time is 13 minutes 53 seconds from the Wilshire/Western Station.

2.3.3 Alternative 3—Santa Monica Extension

This alternative extends the existing Metro Purple Line from the Wilshire/Western Station to the Wilshire/4th Station in Santa Monica (Figure 2-3). Similar to Alternative 2, Alternative 3 extends the subway from the Wilshire/Western Station to a Westwood/VA Hospital Station. Alternative 3 then continues westerly under Wilshire Boulevard and terminates at the Wilshire/4th Street Station between 4th and 5th Streets in Santa Monica. The alignment is 12.38 miles.

Alternative 3 would operate in each direction at 3.3-minute headways during the morning and evening peak periods and operate with 10-minute headways during the midday, off-peak period. The estimated one-way running time is 19 minutes 27 seconds from the Wilshire/Western Station.

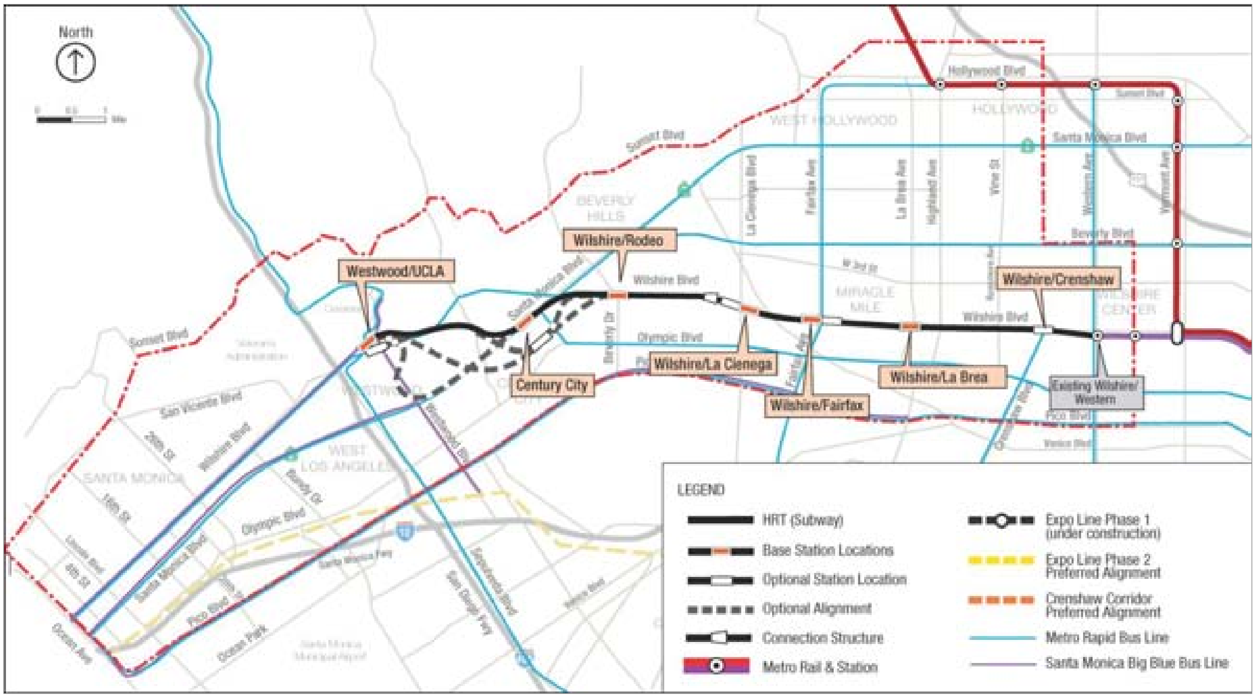


Figure 2-1. Alternative 1—Westwood/UCLA Extension

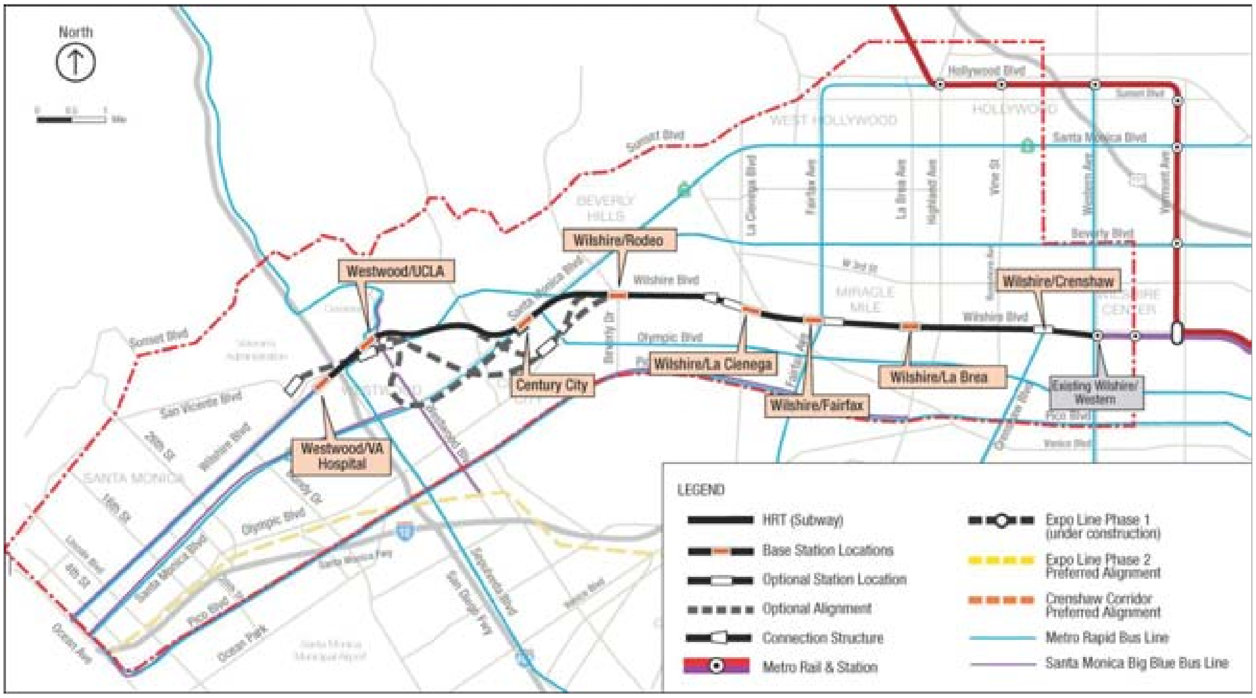


Figure 2-2. Alternative 2—Westwood/Veterans Administration (VA) Hospital Extension

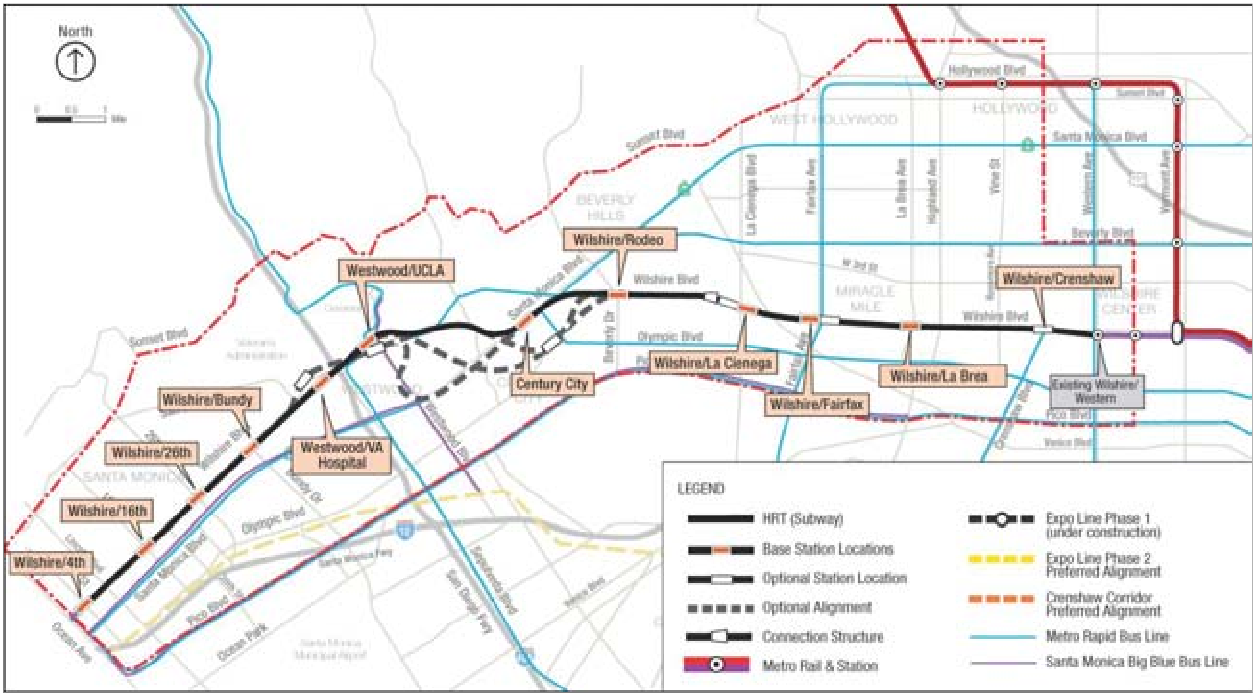


Figure 2-3. Alternative 3—Santa Monica Extension

2.3.4 Alternative 4—Westwood/VA Hospital Extension plus West Hollywood Extension

Similar to Alternative 2, Alternative 4 extends the existing Metro Purple Line from the Wilshire/Western Station to a Westwood/VA Hospital Station. Alternative 4 also includes a West Hollywood Extension that connects the existing Metro Red Line Hollywood/Highland Station to a track connection structure near Robertson and Wilshire Boulevards, west of the Wilshire/La Cienega Station (Figure 2-4). The alignment is 14.06 miles long.

Alternative 4 would operate from Wilshire/Western to a Westwood/VA Hospital Station in each direction at 3.3-minute headways during morning and evening peak periods and 10-minute headways during the midday off-peak period. The West Hollywood extension would operate at 5-minute headways during peak periods and 10-minute headways during the midday, off-peak period. The estimated one-way running time for the Metro Purple Line extension is 13 minutes 53 seconds, and the running time for the West Hollywood from Hollywood/Highland to Westwood/VA Hospital is 17 minutes and 2 seconds.

2.3.5 Alternative 5—Santa Monica Extension plus West Hollywood Extension

Similar to Alternative 3, Alternative 5 extends the existing Metro Purple Line from the Wilshire/Western Station to the Wilshire/4th Station and also adds a West Hollywood Extension similar to the extension described in Alternative 4 (Figure 2-5). The alignment is 17.49 miles in length. Alternative 5 would operate the Metro Purple Line extension in each direction at 3.3-minute headways during the morning and evening peak periods and 10-minute headways during the midday, off-peak period. The West Hollywood extension would operate in each direction at 5-minute headways during peak periods and 10-minute headways during the midday, off-peak period. The estimated one-way running time for the

Metro Purple Line extension is 19 minutes 27 seconds, and the running time from the Hollywood/Highland Station to the Wilshire/4th Station is 22 minutes 36 seconds.

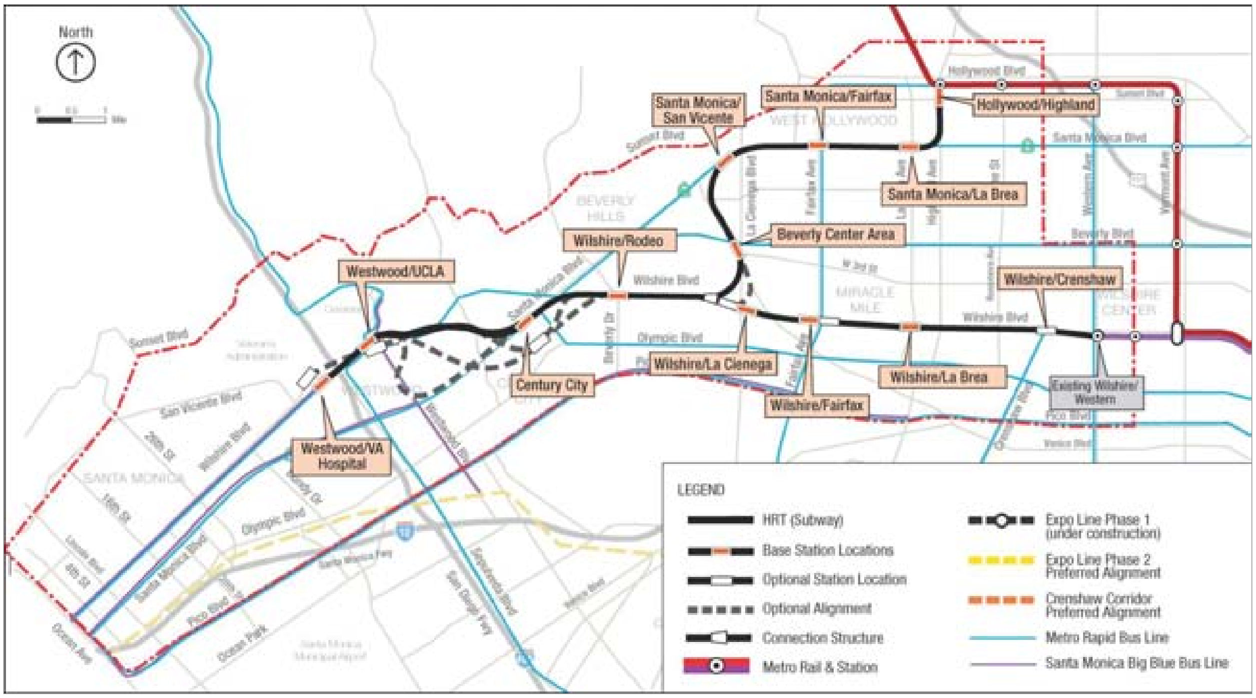


Figure 2-4. Alternative 4—Westwood/VA Hospital Extension plus West Hollywood Extension

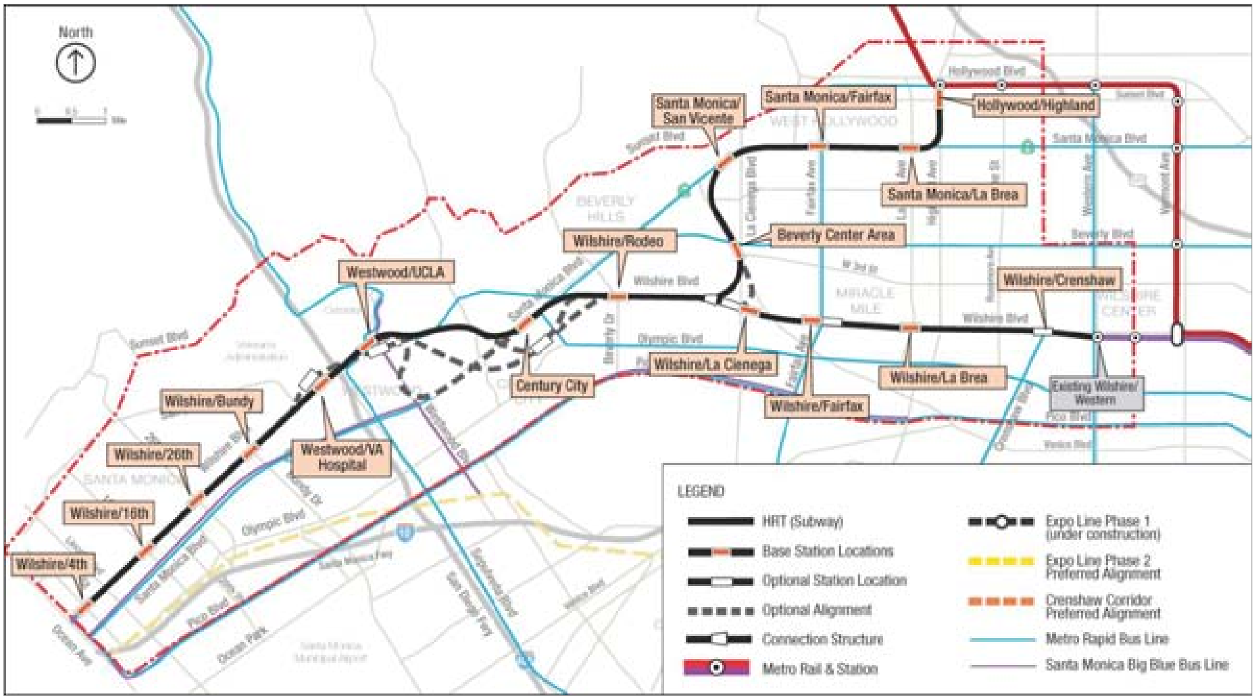


Figure 2-5. Alternative 5—Santa Monica Extension plus West Hollywood Extension

2.4 Stations and Segment Options

HRT stations consist of a station "box," or area in which the basic components are located. The station box can be accessed from street-level entrances by stairs, escalators, and elevators that would bring patrons to a mezzanine level where the ticketing functions are located. The 450-foot platforms are one level below the mezzanine level and allow level boarding (i.e., the train car floor is at the same level as the platform). Stations consist of a center or side platform. Each station is equipped with under-platform exhaust shafts, over-track exhaust shafts, blast relief shafts, and fresh air intakes. In most stations, it is anticipated that only one portal would be constructed as part of the Project, but additional portals could be developed as a part of station area development (by others). Stations and station entrances would comply with the *Americans with Disabilities Act of 1990*, Title 24 of the California Code of Regulations, the California Building Code, and the Department of Transportation Subpart C of Section 49 CFR Part 37.

Platforms would be well-lighted and include seating, trash receptacles, artwork, signage, safety and security equipment (closed-circuit television, public announcement system, passenger assistance telephones), and a transit passenger information system. The fare collection area includes ticket vending machines, fare gates, and map cases.

Table 2-1 lists the stations and station options evaluated and the alternatives to which they are applicable. Figure 2-6 shows the proposed station and alignment options. These include:

- Option 1—Wilshire/Crenshaw Station Option
- Option 2—Fairfax Station Option
- Option 3—La Cienega Station Option
- Option 4—Century City Station and Alignment Options
- Option 5—Westwood/UCLA Station Option
- Option 6—Westwood/VA Hospital Station Option

Table 2-1. Alternatives and Stations Considered

Stations	Alternatives				
	1	2	3	4	5
	Westwood/ UCLA Extension	Westwood/ VA Hospital Extension	Santa Monica Extension	Westwood/ VA Hospital Extension Plus West Hollywood Extension	Santa Monica Extension Plus West Hollywood Extension
Base Stations					
Wilshire/Crenshaw	●	●	●	●	●
Wilshire/La Brea	●	●	●	●	●
Wilshire/Fairfax	●	●	●	●	●
Wilshire/La Cienega	●	●	●	●	●
Wilshire/Rodeo	●	●	●	●	●
Century City (Santa Monica Blvd)	●	●	●	●	●
Westwood/UCLA (Off-street)	●	●	●	●	●
Westwood/VA Hospital		●	●	●	●
Wilshire/Bundy			●		●
Wilshire/26th			●		●
Wilshire/16th			●		●
Wilshire/4th			●		●
Hollywood/Highland				●	●
Santa Monica/La Brea				●	●
Santa Monica/Fairfax				●	●
Santa Monica/San Vicente				●	●
Beverly Center Area				●	●
Station Options					
1—No Wilshire/Crenshaw	●	●	●	●	●
2—Wilshire/Fairfax East	●	●	●	●	●
3—Wilshire/La Cienega (Transfer Station)	●	●	●	●	●
4—Century City (Constellation Blvd)	●	●	●	●	●
5—Westwood/UCLA (On-street)	●	●	●	●	●
6—Westwood/VA Hospital North		●	●	●	●

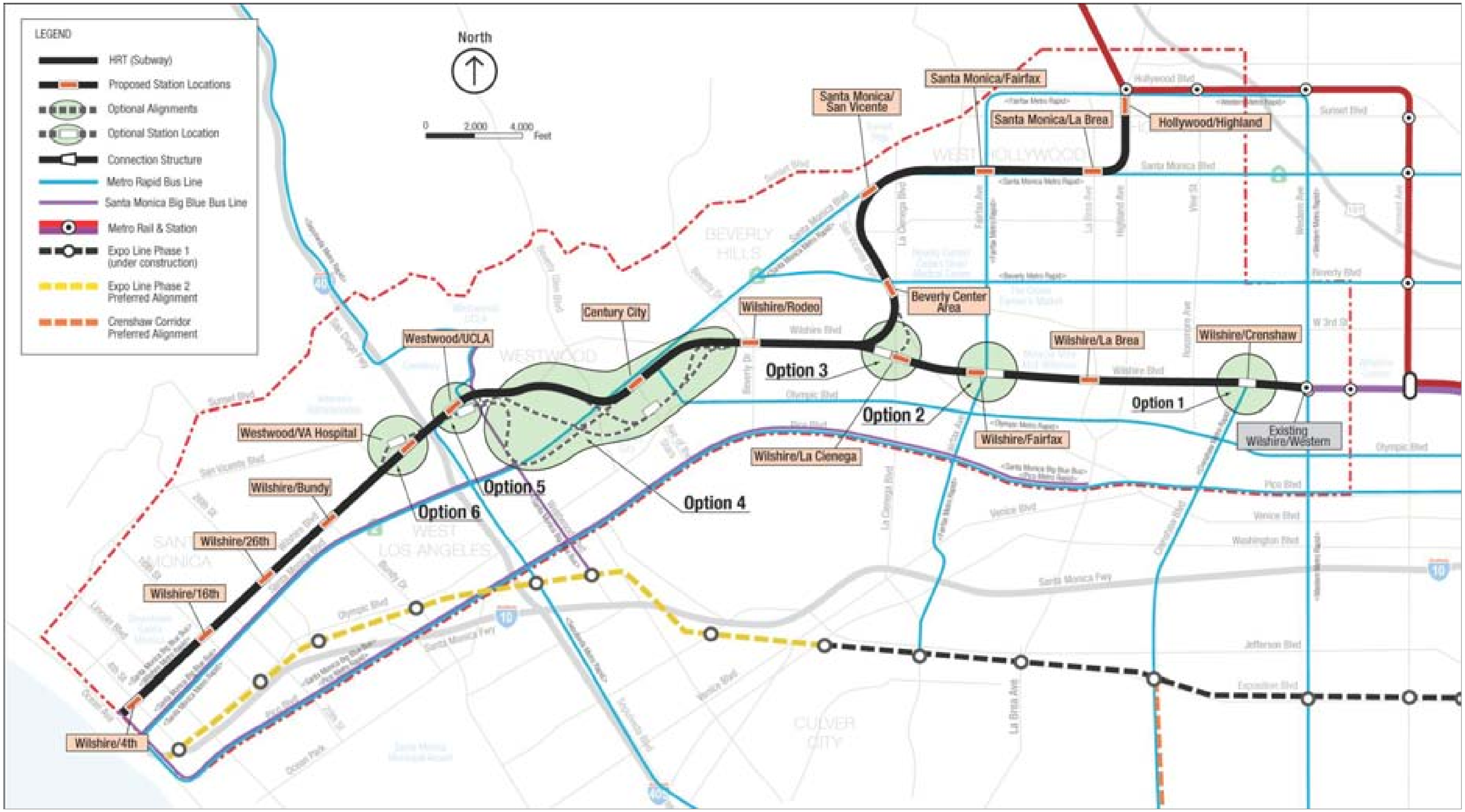


Figure 2-6. Station and Alignment Options

2.4.1 Option 1—Wilshire/Crenshaw Station Option

- **Base Station: Wilshire/Crenshaw Station**—The base station straddles Crenshaw Boulevard, between Bronson Avenue and Lorraine Boulevard.

- **Station Option: Remove Wilshire/Crenshaw Station**—This station option would delete the Wilshire/Crenshaw Station. Trains would run from the Wilshire/Western Station to the Wilshire/La Brea Station without stopping at Crenshaw. A vent shaft would be constructed at the intersection of Western Avenue and Wilshire Boulevard (Figure 2-7).

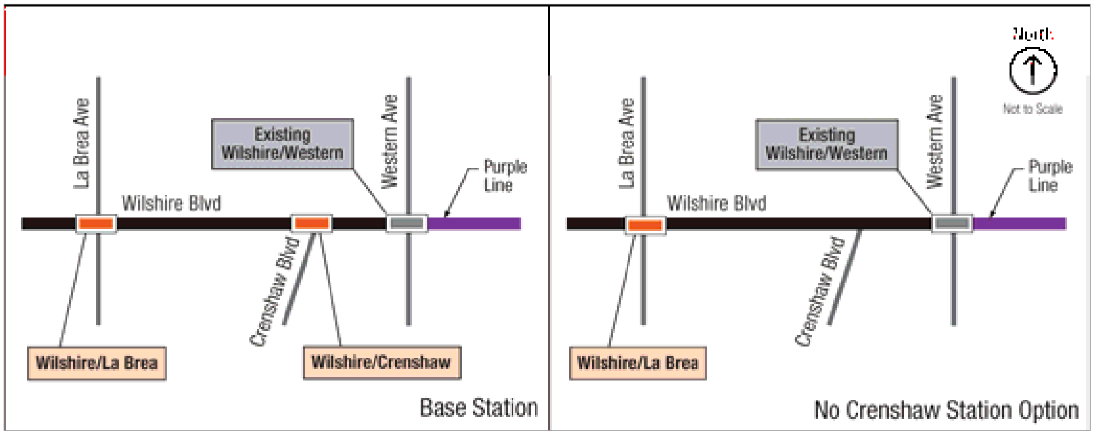


Figure 2-7. Option 1—No Wilshire/Crenshaw Station Option

2.4.2 Option 2—Wilshire/Fairfax Station East Option

- **Base Station: Wilshire/Fairfax Station**—The base station is under the center of Wilshire Boulevard, immediately west of Fairfax Avenue.

- **Station Option: Wilshire/Fairfax Station East Station Option**—This station option would locate the Wilshire/Fairfax Station farther east, with the station underneath the Wilshire/Fairfax intersection (Figure 2-8). The east end of the station box would be east of Orange Grove Avenue in front of LACMA, and the west end would be west of Fairfax Avenue.

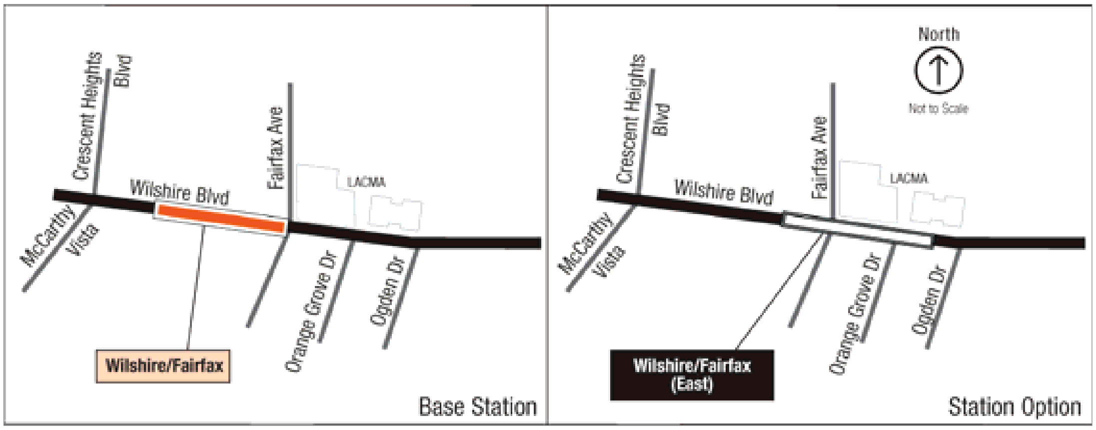


Figure 2-8. Option 2—Fairfax Station Option

2.4.3 Option 3—Wilshire/La Cienega Station Option

- **Base Station: Wilshire/La Cienega Station**—The base station would be under the center of Wilshire Boulevard, immediately east of La Cienega Boulevard. A direct transfer between the Metro Purple Line and the potential future West Hollywood Line is not provided with this station. Instead, a connection structure is proposed west of Robertson Boulevard as a means to provide a future HRT connection to the West Hollywood Line.

- **Station Option: Wilshire/La Cienega Station West with Connection Structure**—The station option would be located west of La Cienega Boulevard, with the station box extending from the Wilshire/Le Doux Road intersection to just west of the Wilshire/Carson Road intersection (Figure 2-9). It also contains an alignment option that would provide an alternate HRT connection to the future West Hollywood Extension. This alignment portion of Option 3 is only applicable to Alternatives 4 and 5.

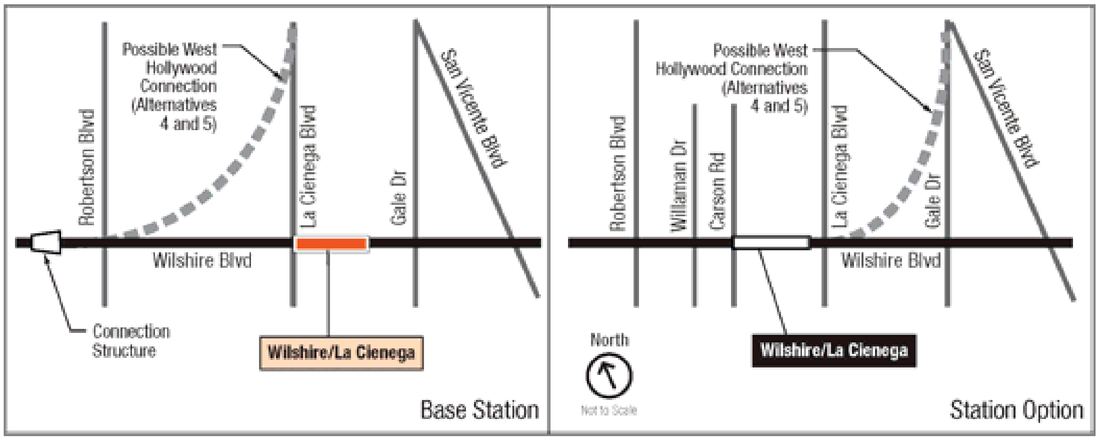


Figure 2-9. Option 3—La Cienega Station Option

2.4.4 Option 4—Century City Station and Segment Options

2.4.4.1 Century City Station and Beverly Hills to Century City Segment Options

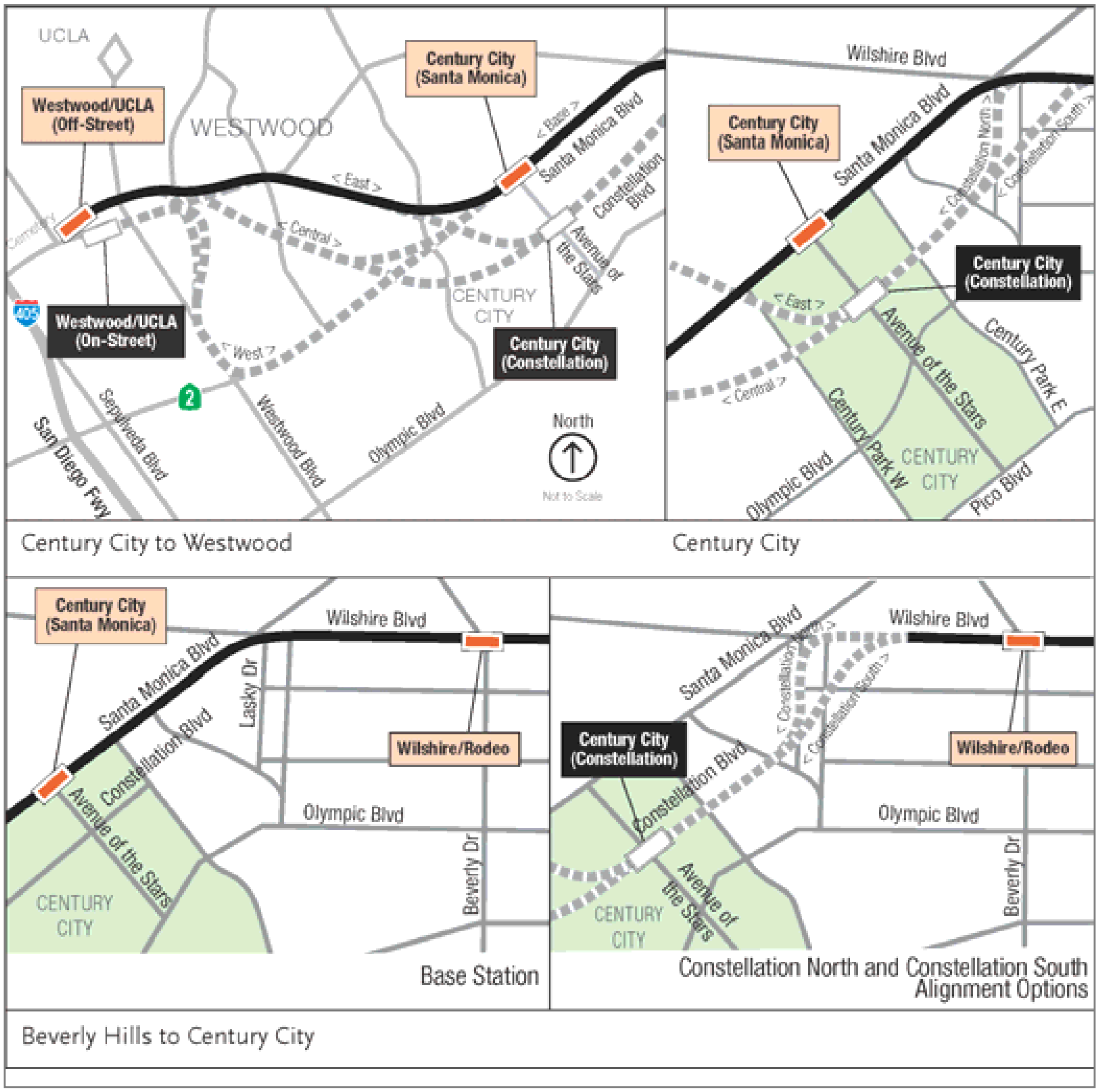
- **Base Station: Century City (Santa Monica) Station**—The base station would be under Santa Monica Boulevard, centered on Avenue of the Stars.

- **Station Option: Century City (Constellation) Station**—With Option 4, the Century City Station has a location option on Constellation Boulevard (Figure 2-10), straddling Avenue of the Stars and extending westward to east of MGM Drive.

- **Segment Options**—Two route options are proposed to connect the Wilshire/Rodeo Station to Century City (Constellation) Station: Constellation North and Constellation South. As shown in Figure 2-10, the base segment to the base Century City (Santa Monica) Station is shown in the solid black line and the segment options to Century City (Constellation) Station are shown in the dashed grey lines.

2.4.4.2 Century City to Westwood Segment Options

Three route options considered for connecting the Century City and Westwood stations include: East, Central, and West. As shown in Figure 2-10, each of these three segments would be accessed from both Century City Stations and both Westwood/UCLA Stations. The base segment is shown in the solid black line and the options are shown in the dashed grey lines.



Century City to Westwood

Century City

Beverly Hills to Century City

Figure 2-10. Century City Station Options

2.4.5 Option 5—Westwood/UCLA Station Options

- **Base Station: Westwood/UCLA Station Off-Street Station Option**—The base station is located under the UCLA Lot 36 on the north side of Wilshire Boulevard between Gayley and Veteran Avenues.

- **Station Option: Westwood/UCLA On-Street Station Option**—This station option would be located under the center of Wilshire Boulevard, immediately west of Westwood Boulevard (Figure 2-11).

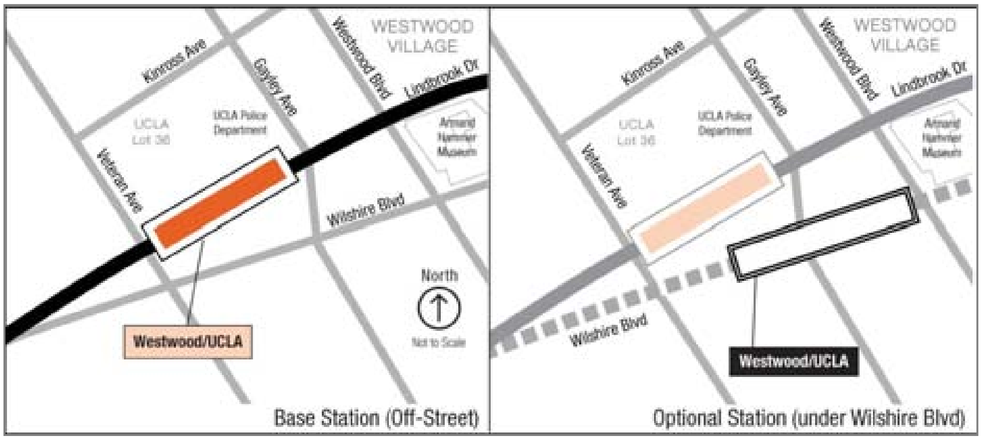


Figure 2-11. Option 5—Westwood/UCLA Station Options

2.4.6 Option 6—Westwood/VA Hospital Station Option

- **Base Station: Westwood/VA Hospital**—The base station would be below the VA Hospital parking lot on the south side of Wilshire Boulevard in between the I-405 exit ramp and Bonsall Avenue.

- **Station Option: Westwood/VA Hospital North Station**—This station option would locate the Westwood/VA Hospital Station on the north side of Wilshire Boulevard between Bonsall Avenue and Wadsworth Theater. (Shown in Figure 2-12)

To access the Westwood/VA Hospital Station North, the alignment would extend westerly from the Westwood/UCLA Station under Veteran Avenue, the Federal Building property, the I-405 Freeway, and under the Veterans Administration property just east of Bonsall Avenue.

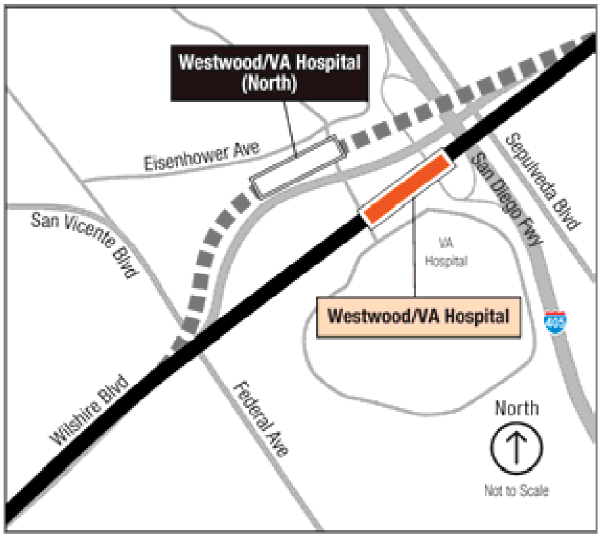


Figure 2-12. Option 6—Westwood/VA Hospital Station North

2.5 Base Stations

The remaining stations (those without options) are described below.

- **Wilshire/La Brea Station**—This station would be located between La Brea and Cloverdale Avenues.

- **Wilshire/Rodeo Station**—This station would be under the center of Wilshire Boulevard, beginning just west of South Canon Drive and extending to El Camino Drive.

- **Wilshire/Bundy Station**—This station would be under Wilshire Boulevard, east of Bundy Drive, extending just east of Saltair Avenue.
- **Wilshire/26th Station**—This station would be under Wilshire Boulevard, with the eastern end east of 26th Street and the western end west of 25th Street, midway between 25th Street and Chelsea Avenue.
- **Wilshire/16th Station**—This station would be under Wilshire Boulevard with the eastern end just west of 16th Street and the western end west of 15th Street.
- **Wilshire/4th Station**—This station would be under Wilshire Boulevard and 4th Street in Santa Monica.
- **Hollywood/Highland Station**—This station would be located under Highland Avenue and would provide a transfer option to the existing Metro Red Line Hollywood/Highland Station under Hollywood Boulevard.
- **Santa Monica/La Brea Station**—This station would be under Santa Monica Boulevard, just west of La Brea Avenue, and would extend westward to the center of the Santa Monica Boulevard/Formosa Avenue.
- **Santa Monica/Fairfax Station**—This station is under Santa Monica Boulevard and would extend from just east of Fairfax Avenue to just east of Ogden Drive.
- **Santa Monica/San Vicente Station**—This station would be under Santa Monica Boulevard and would extend from just west of Hancock Avenue on the west to just east of Westmount Drive on the east.
- **Beverly Center Area Station**—This station would be under San Vicente Boulevard, extending from just south of Gracie Allen Drive to south of 3rd Street.

2.6 Other Components of the Build Alternatives

2.6.1 Traction Power Substations

Traction power substations (TPSS) are required to provide traction power for the HRT system. Substations would be located in the station box or in a box located with the crossover tracks and would be located in a room that is about 50 feet by 100 feet in a below grade structure.

2.6.2 Emergency Generators

Stations at which the emergency generators would be located are Wilshire/La Brea, Wilshire/La Cienega, Westwood/UCLA, Westwood/VA Hospital, Wilshire/26th, Highland/Hollywood, Santa Monica/La Brea, and Santa Monica/San Vicente. The emergency generators would require approximately 50 feet by 100 feet of property in an off-street location. All would require property acquisition, except for the one at the Wilshire/La Brea Station, which uses Metro's property.

2.6.3 Mid-Tunnel Vent Shaft

Each alternative would require mid-tunnel ventilation shafts. The vent shafts are emergency ventilation shafts with dampers, fans, and sound attenuators generally placed at both ends of a station box to exhaust smoke. In addition, emergency vent shafts could be used for station cooling and gas mitigation. The vent shafts are also required in tunnel segments with more than 6,000 feet between stations to meet fire/life safety requirements. There would be a connecting corridor between the two tunnels (one for each direction of train movement) to provide emergency egress and fire-fighting ingress. A vent shaft is approximately 150 square feet; with the opening of the shaft located in a sidewalk and covered with a grate about 200 square feet.

Table 2-2. Mid-Tunnel Vent Shaft Locations

Alternative/Option	Location
Alternatives 1 through 5, MOS 2	Part of the connection structure on Wilshire Boulevard, west of Robertson Boulevard
Alternatives 2 through 5	West of the Westwood/VA Hospital Station on Army Reserve property at Federal Avenue and Wilshire Boulevard
Option 4 via East route	At Wilshire Boulevard/Manning Avenue intersection
Option 4 to Westwood/UCLA Off-Street Station via Central route	On Santa Monica Boulevard just west of Beverly Glen Boulevard
Option 4 to Westwood/UCLA On-Street Station via Central route	At Santa Monica Boulevard/Beverly Glen Boulevard intersection
Options 4 via West route	At Santa Monica Boulevard/Glendon Avenue intersection
Options 4 from Constellation Station via Central route	On Santa Monica Boulevard between Thayer and Pandora Avenues
Option from Constellation Station via West route	On Santa Monica Boulevard just east of Glendon Avenue

2.6.4 Trackwork Options

Each Build Alternative requires special trackwork for operational efficiency and safety (Table 2-3):

- Tail tracks—a track, or tracks, that extends beyond a terminal station (the last station on a line)
- Pocket tracks—an additional track, or tracks, adjacent to the mainline tracks generally at terminal stations
- Crossovers—a pair of turnouts that connect two parallel rail tracks, allowing a train on one track to cross over to the other
- Double crossovers—when two sets of crossovers are installed with a diamond allowing trains to cross over to another track

Table 2-3. Special Trackwork Locations

Station	Alternative 1 Westwood/ UCLA Extension	Alternative 2 Westwood/ VA Hospital Extension	Alternative 3 Santa Monica Extension	Alternative 4 Westwood/VA Hospital Extension Plus West Hollywood Extension	Alternative 5 Santa Monica Extension Plus West Hollywood Extension
Special Trackwork Locations—Base Trackwork Alternatives					
Wilshire/Crenshaw	None	None	None	None	None
Wilshire/La Brea	Double Crossover	Double Crossover	Double Crossover	Double Crossover	Double Crossover
Wilshire/Fairfax	None *MOS 1 Only: Terminus Station with Tail tracks*	None *MOS 1 Only: Terminus Station with Tail tracks*	None *MOS 1 Only: Terminus Station with Tail tracks*	None *MOS 1 Only: Terminus Station with Tail tracks*	None *MOS 1 Only: Terminus Station with Tail tracks*
Wilshire/La Cienega	None	None	None	None	None
Station Option 3 - Wilshire/La Cienega West	Turnouts	Turnouts	Turnouts		
Wilshire/Robertson Connection Structure	Equilateral Turnouts—for future West Hollywood connection	Equilateral Turnouts—for future West Hollywood connection	Equilateral Turnouts—for future West Hollywood connection	Equilateral Turnouts	Equilateral Turnouts
Wilshire/Rodeo	None	None	None	None	None
Century City	Double Crossover *MOS 2 Only: Terminus Station with Double Crossover and tail tracks*	Double Crossover *MOS 2 Only: Terminus Station with Double Crossover and tail tracks*	Double Crossover *MOS 2 Only: Terminus Station with Double Crossover and tail tracks*	Double Crossover *MOS 2 Only: Terminus Station with Double Crossover and tail tracks*	Double Crossover *MOS 2 Only: Terminus Station with Double Crossover and tail tracks*
Westwood/UCLA	End Terminal with Double Crossover and tail tracks	Double Crossover	Double Crossover	Double Crossover	Double Crossover
Westwood/VA Hospital	N/A	End Terminal with Turnouts and tail tracks	Turnouts	End Terminal with Turnouts and tail tracks	Turnouts
Wilshire/Bundy	N/A	N/A	None	N/A	None
Wilshire/26th	N/A	N/A	None	N/A	None
Wilshire/16th	N/A	N/A	None	N/A	None
Wilshire/4th	N/A	N/A	End Terminal with Double Crossover. Pocket Track with Double Crossover, Equilateral Turnouts and tail tracks	N/A	End Terminal with Double Crossover, Pocket Track with Double Crossover, Equilateral Turnouts and tail tracks
Hollywood/ Highland	N/A	N/A	N/A	Double Crossover and tail tracks	Double Crossover and tail tracks
Santa Monica/La Brea	N/A	N/A	N/A	None	None
Santa Monica/Fairfax	N/A	N/A	N/A	None	None
Santa Monica/ San Vicente	N/A	N/A	N/A	Double Crossover	Double Crossover
Beverly Center	N/A	N/A	N/A	None	None
Additional Special Trackwork Location (Optional Trackwork)					
Wilshire/Fairfax	Double Crossover	Double Crossover	Double Crossover	Double Crossover	Double Crossover
Wilshire/La Cienega	Double Crossover	Double Crossover	Double Crossover	Double Crossover	Double Crossover
Wilshire/ Rodeo	Pocket Track	Pocket Track	Pocket Track	Pocket Track	Pocket Track
Wilshire/26th	N/A	N/A	Double Crossover	N/A	Double Crossover

2.6.5 Rail Operations Center

The existing Rail Operations Center (ROC), shown on the figure below, located in Los Angeles near the intersection of Imperial Highway and the Metro Blue Line does not have sufficient room to accommodate the new transit corridors and line extensions in Metro's expansion program. The Build Alternatives assume an expanded ROC at this location.

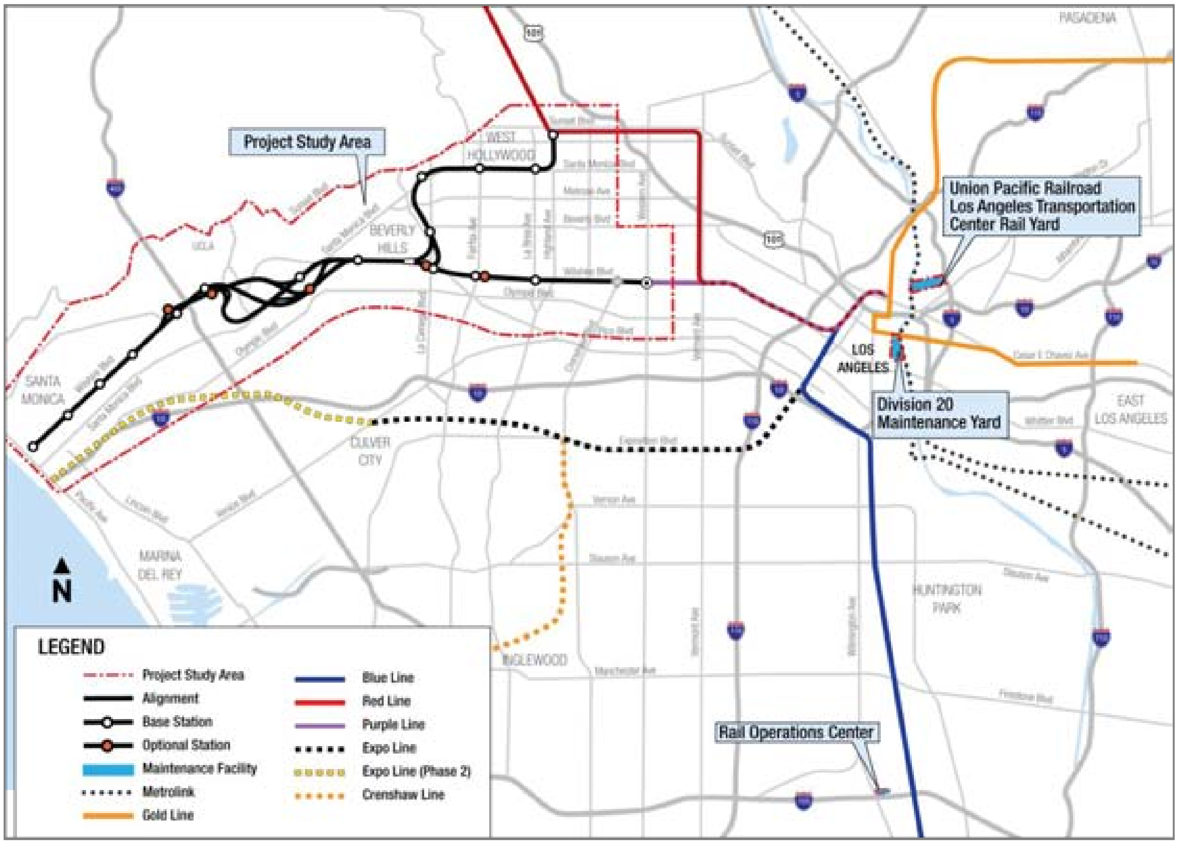


Figure 2-13. Location of the Rail Operations Center and Maintenance Yards

2.6.6 Maintenance Yards

If any of the Build Alternatives are chosen, additional storage capacity would be needed. Two options for providing this expanded capacity are as follows:

- The first option requires purchasing 3.9 acres of vacant private property abutting the southern boundary of the Division 20 Maintenance and Storage Facility, which is located between the 4th and 6th Street Bridges. Additional maintenance and storage tracks would accommodate up to 102 vehicles, sufficient for Alternatives 1 and 2.

- The second option is a satellite facility at the Union Pacific (UP) Los Angeles Transportation Center Rail Yard. This site would be sufficient to accommodate the vehicle fleet for all five Build Alternatives. An additional 1.3 miles of yard lead tracks from the Division 20 Maintenance and Storage Facility and a new bridge over the Los Angeles River would be constructed to reach this yard (Figure 2-14).

Figure 2-14. UP Railroad Rail Bridge

Figure 2-15. Maintenance Yard Options

2.7 Minimum Operable Segments

Due to funding constraints, it may be necessary to construct the Westside Subway Extension in shorter segments. A Minimum Operable Segment (MOS) is a phasing option that could be applied to any of the Build Alternatives.

2.7.1 MOS 1—Fairfax Extension

MOS 1 follows the same alignment as Alternative 1, but terminates at the Wilshire/Fairfax Station rather than extending to a Westwood/UCLA Station. A double crossover for MOS 1 is located on the west end of the Wilshire/La Brea Station box, west of Cloverdale Avenue. The alignment is 3.10 miles in length.

2.7.2 MOS 2—Century City Extension

MOS 2 follows the same alignment as Alternative 1, but terminates at a Century City Station rather than extending to a Westwood/UCLA Station. The alignment is 6.61 miles from the Wilshire/Western Station.

3.0 AFFECTED ENVIRONMENT

"Air Pollution" is a general term that refers to one or more chemical substances that degrade the quality of the atmosphere. Individual air pollutants degrade the atmosphere by reducing visibility, damaging property, reducing the productivity or vigor of crops or natural vegetation, and/or reducing human or animal health. Air quality also has climate change implications discussed in the separate Climate Change Technical Report. Air quality is a term used to describe the amount of air pollution the public is exposed to.

Air quality in the United States is governed by the Federal Clean Air Act (CAA) and is administered by the U.S. Environmental Protection Agency (USEPA). In addition to being subject to the requirements of the CAA, air quality in California is also governed under the California Clean Air Act (CCAA).

The CCAA, as amended in 1992, requires all air districts in the State to endeavor to achieve and maintain State Ambient Air Quality Standards. The California Air Resources Board (CARB) administers the CCAA statewide. A brief description of these and other involved agencies are described below, as is the CAA.

3.1 U.S. Environmental Protection Agency

The USEPA is responsible for establishing the National Ambient Air Quality Standards (NAAQS) and enforcing the Clean Air Act, and regulates emission sources, such as aircraft, ships, and certain types of locomotives, under the exclusive authority of the federal government. The USEPA also has jurisdiction over emission sources outside state waters (e.g., beyond the outer continental shelf) and establishes various emission standards, including those for vehicles sold in states other than California. Automobiles sold in California must meet the stricter emission standards established by CARB. For additional information about the USEPA, the reader can contact its general internet address found at www.epa.gov. Additional information on the activities of USEPA Region IX, which includes California, can be found at www.epa.gov/region9. Finally, additional information on the activities of USEPA's Office of Mobile Sources can be found at www.epa.gov/omswww/mshome.htm.

3.1.1 California Air Resources Board

CARB, which became part of the California Environmental Protection Agency (CalEPA) in 1991, is responsible for ensuring implementation of the CCAA, meeting state requirements of the CAA, and establishing State Ambient Air Quality Standards. It is also responsible for setting emission standards for vehicles sold in California and for other emission sources such as consumer products and certain off-road equipment. CARB also established passenger vehicle fuel specifications. The internet address for CalEPA is www.calepa.cahwet.gov; the address for CARB is www.arb.ca.gov.

CARB also oversees the functions of local air pollution control districts and air quality management districts, which in turn administer air quality activities at the regional and county level. The CCAA is administered by CARB at the state level and by the Air Quality Management Districts at the regional level.

3.1.2 South Coast Air Quality Management District

The South Coast Air Quality Management District (SCAQMD) was created to protect the public from the harmful effects of air pollution, achieve and maintain air quality standards, foster community involvement, and develop and implement cost-effective programs meeting state and federal mandates, considering environmental and economic impacts.

Specifically, the SCAQMD is responsible for monitoring air quality and planning, implementing, and enforcing programs designed to attain and maintain state and federal ambient air quality standards in the district. Programs developed implement air quality rules and regulations that regulate stationary source emissions, including area sources and point sources and certain mobile source emissions. The SCAQMD is also responsible for establishing permitting requirements for stationary sources and ensuring that new, modified, or relocated stationary sources do not create net emissions increases and, therefore, are consistent with the region's air quality goals. The SCAQMD enforces air quality rules and regulations through a variety of means, including inspections, educational or training programs, or fines, when necessary.

3.1.3 Clean Air Act Amendments of 1990

The Clean Air Act Amendments of 1990 (CAAA) direct the USEPA to implement environmental policies and regulations that will ensure acceptable levels of air quality.

Under the CAAA, a project cannot:

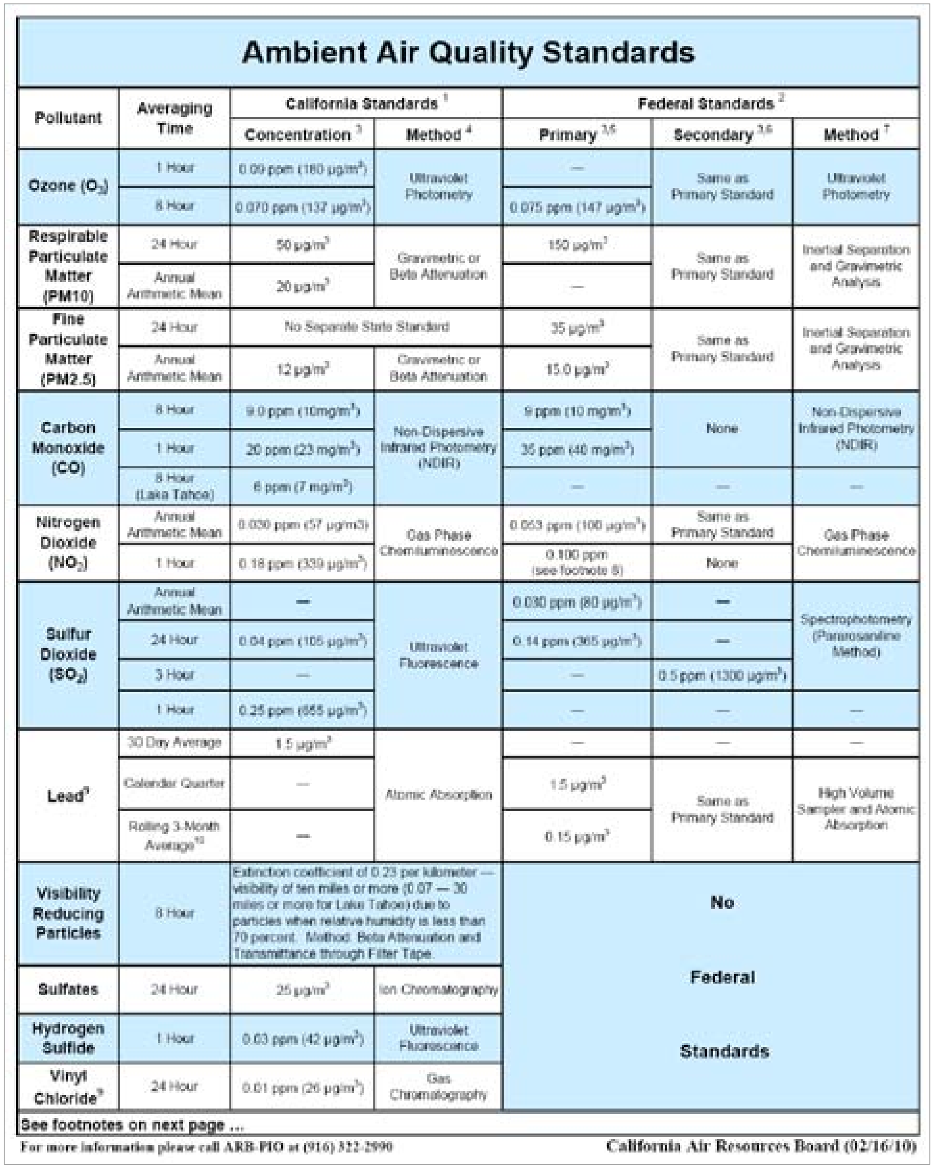
- Cause or contribute to any new violation of any National Ambient Air Quality Standards (NAAQS) in any area
- Increase the frequency or severity of any existing violation of any NAAQS in any area
- Delay timely attainment of any NAAQS or any required interim emission reductions or other milestones in any area

3.1.4 National and State Ambient Air Quality Standards

As required by the Clean Air Act, NAAQS have been established for six major air pollutants. These pollutants are: carbon monoxide, nitrogen dioxide, ozone, particulate matter (PM_{10} and $PM_{2.5}$), sulfur dioxide, and lead. The State of California has also established ambient air quality standards, known as the California Ambient Air Quality Standards (CAAQS). These standards are generally more stringent than the corresponding federal standards and incorporate additional standards for sulfates, hydrogen sulfide, vinyl chloride, and visibility reducing particles.

Both State and Federal standards are summarized in Table 3-1. The "primary" standards have been established to protect the public health. The "secondary" standards are intended to protect the nation's welfare and account for air pollutant effects on soil, water, visibility, materials, vegetation and other aspects of the general welfare.

Table 3-1. State and Federal Air Quality Standards



Ambient Air Quality Standards

Pollutant	Averaging Time	California Standards [1]		Federal Standards [2]		
		Concentration [3]	Method [4]	Primary [3,5]	Secondary [3,6]	Method [7]
Ozone (O_3)	1 Hour	0.09 ppm (180 μg/m^3)	Ultraviolet Photometry	—	Same as Primary Standard	Ultraviolet Photometry
	8 Hour	0.070 ppm (137 μg/m^3)		0.075 ppm (147 μg/m^3)		
Respirable Particulate Matter (PM10)	24 Hour	50 μg/m^3	Gravimetric or Beta Attenuation	150 μg/m^3	Same as Primary Standard	Inertial Separation and Gravimetric Analysis
	Annual Arithmetic Mean	20 μg/m^3		—		
Fine Particulate Matter (PM2.5)	24 Hour	No Separate State Standard		35 μg/m^3	Same as Primary Standard	Inertial Separation and Gravimetric Analysis
	Annual Arithmetic Mean	12 μg/m^3	Gravimetric or Beta Attenuation	15.0 μg/m^3		
Carbon Monoxide (CO)	8 Hour	9.0 ppm (10mg/m^3)	Non-Dispersive Infrared Photometry (NDIR)	9 ppm (10 mg/m^3)	None	Non-Dispersive Infrared Photometry (NDIR)
	1 Hour	20 ppm (23 mg/m^3)		35 ppm (40 mg/m^3)		
	8 Hour (Lake Tahoe)	6 ppm (7 mg/m^3)		—	—	—
Nitrogen Dioxide (NO_2)	Annual Arithmetic Mean	0.030 ppm (57 μg/m3)	Gas Phase Chemiluminescence	0.053 ppm (100 μg/m^3)	Same as Primary Standard	Gas Phase Chemiluminescence
	1 Hour	0.18 ppm (339 μg/m^3)		0.100 ppm (see footnote 8)	None	
Sulfur Dioxide (SO_2)	Annual Arithmetic Mean	—	Ultraviolet Fluorescence	0.030 ppm (80 μg/m^3)	—	Spectrophotometry (Pararosaniline Method)
	24 Hour	0.04 ppm (105 μg/m^3)		0.14 ppm (365 μg/m^3)	—	
	3 Hour	—		—	0.5 ppm (1300 μg/m^3)	
	1 Hour	0.25 ppm (655 μg/m^3)		—	—	—
Lead[9]	30 Day Average	1.5 μg/m^3	Atomic Absorption	—	—	—
	Calendar Quarter	—		1.5 μg/m^3	Same as Primary Standard	High Volume Sampler and Atomic Absorption
	Rolling 3-Month Average[10]	—		0.15 μg/m^3		
Visibility Reducing Particles	8 Hour	Extinction coefficient of 0.23 per kilometer — visibility of ten miles or more (0.07 — 30 miles or more for Lake Tahoe) due to particles when relative humidity is less than 70 percent. Method: Beta Attenuation and Transmittance through Filter Tape.		**No Federal Standards**		
Sulfates	24 Hour	25 μg/m^3	Ion Chromatography			
Hydrogen Sulfide	1 Hour	0.03 ppm (42 μg/m^3)	Ultraviolet Fluorescence			
Vinyl Chloride[9]	24 Hour	0.01 ppm (26 μg/m^3)	Gas Chromatography			

See footnotes on next page ...

For more information please call ARB-PIO at (916) 322-2990

California Air Resources Board (02/16/10)

1. California standards for ozone, carbon monoxide (except Lake Tahoe), sulfur dioxide (1 and 24 hour), nitrogen dioxide, suspended particulate matter—PM10, PM2.5, and visibility reducing particles, are values that are not to be exceeded. All others are not to be equaled or exceeded. California ambient air quality standards are listed in the Table of Standards in Section 70200 of Title 17 of the California Code of Regulations.

2. National standards (other than ozone, particulate matter, and those based on annual averages or annual arithmetic mean) are not to be exceeded more than once a year. The ozone standard is attained when the fourth highest eight hour concentration in a year, averaged over three years, is equal to or less than the standard. For PM10, the 24 hour standard is attained when the expected number of days per calender year with a 24-hour average concentration above 150 μg/m^3 is equal to or less than one. For PM2.5, the 24 hour standard is attained when 98 percent of the daily concentrations, averaged over three years, are equal to or less than the standard. Contact U.S. EPA for further clarification and current federal policies.

3. Concentration expressed first in units in which it was promulgated. Equivalent units given in parentheses are based upon a reference temperature of 25°C and a reference pressure of 760 torr. Most measurements of air quality are to be corrected to a reference temperature of 25°C and a reference pressure of 760 torr; ppm in this table refers to ppm by volume, or micromoles of pollutant per mole of gas.

4. Any equivalent procedure which can be shown to the satisfaction of the ARB to give equivalent results at or near the level of the air quality standard may be used.

5. National Primary Standards: The levels of air quality necessary, with an adequate margin of safety to protect the public health.

6. National Secondary Standards: The levels of air quality necessary to protect the public welfare from any known or anticipated adverse effects of a pollutant.

7. Reference method as described by the EPA. An "equivalent method" of measurement may be used but must have a "consistent relationship to the reference method" and must be approved by the EPA.

8. To attain this standard, the 3-year average of the 98th percentile of the daily maximum 1-hour average at each monitor within an area must not exceed 0.100 ppm (effective January 22, 2010).

9. The ARB has identified lead and vinyl chloride as 'toxic air contaminants' with no threshold level of exposure for adverse health effects determined. These actions allow for the implementation of control measures at levels below the ambient concentrations specified for these pollutants.

10. National lead standard, rolling 3-month average: final rule signed October 15, 2008.

3.2 Ambient Air Quality Data

3.2.1 Local Meteorology

The surrounding atmosphere is an important element in assessing an area's ambient air quality. The study area is located in the South Coast Air Basin (SCAB), which includes all of Los Angeles and Orange counties, as well as portions of Riverside and San Bernardino counties.

The SCAB is bordered by the Pacific Ocean to the west and the San Bernardino mountains to the east. Prevailing winds in the SCAB are mainly out of the west. These prevailing winds are due to the proximity of the SCAB to the coast and the blocking nature of the San Bernardino Mountains to the east; air masses pushed onshore into the basin are often trapped by the San Bernardino Mountains.

During the summer the SCAB is generally influenced by a Pacific Subtropical High cell that sits off the coast, inhibiting cloud formation and encouraging daytime solar heating. The SCAB is rarely influenced by cold air masses moving south from Canada and Alaska, as these frontal systems are weak and diffuse by the time they reach the basin. The SCAB is classified as a dry-hot desert climate.

3.2.2 Local Monitored Air Quality

The South Coast air pollutant levels are measured at monitoring stations that CARB maintains. The monitoring stations nearest the project study area are located in Los Angeles at Veterans Hospital and 1630 North Main Street. The last three years of available monitored data for these locations are summarized in Table 3-2 to illustrate the study area's general air quality trends.

Table 3-2. Air Quality Summary for Study Area Monitoring Station

Air Polluant	Standard/ Exceedance**	Veterans Hospital West Los Angeles			North Main Street Los Angeles		
		2006	2007	2008	2006	2007	2008
Carbon Monoxide (CO)	Year Coverage*	99%	94%	96%	95%	95%	97%
	Max. 1-hour Concentration (ppm)	2.9	2.7	2.7	3.5	3.2	2.9
	Max. 8-hour Concentration (ppm)	2.0	1.96	1.76	2.68	2.15	1.96
	# Days>Federal 1-hour Std. of >35 ppm	0	0	0	0	0	0
	# Days>Federal 8-hour Std. of >9 ppm	0	0	0	0	0	0
	# Days>California 8-hour Std. of >9.0 ppm	0	0	0	0	0	0
Ozone (O3)	Year Coverage*	98%	98%	96%	98%	97%	96%
	Max. 1-hour Concentration (ppm)	0.099	0.117	0.111	0.108	0.115	0.109
	Max. 8-hour Concentration (ppm)	0.074	0.088	0.097	0.079	0.103	0.090
	# Days>Federal 8-hour Std. Of >0.075 ppm	0	2	2	3	3	3
	# Days>California 1-hour Std. Of >0.09 ppm	3	2	3	8	3	3
	# Days>California 8-hour Std. Of >0.07 ppm	2	2	8	7	6	6
Nitrogen Dioxide (NO2)	Year Coverage*	94%	93%	96%	97%	96%	95%
	Max. 1-hour Concentration (ppm)	0.078	0.082	0.090	0.111	0.104	0.122
	Annual Average (ppm)	0.017	0.019	0.018	0.029	0.030	0.027
	# Days>California 1-hour Std. of >0.18 ppm	0	0	0	0	0	0
Sulfur Dioxide (SO2)	Year Coverage*	NM	NM	NM	99%	90%	96%
	Max. 24-hour Concentration (ppm)	NM	NM	NM	0.006	0.005	0.003
	Annual Average (ppm)	NM	NM	NM	0.001	0.000	0.000
	# Days>Federal 24-hour Std. of >0.14 ppm	NM	NM	NM	0	0	0
Suspended Particulates (PM10)	Year Coverage*	NM	NM	NM	95%	93%	79%
	Max. 24-hour Concentration (µg/m3)	NM	NM	NM	59.0	78.0	66.0
	#Days>Fed. 24-hour Std. of>150 µg/m3	NM	NM	NM	0	0	0
	#Days>California 24-hour Std. of>50 µg/m3	NM	NM	NM	3	5	2
	State Annual Average (µg/m3)	NM	NM	NM	30.1	33.0	NA
Suspended Particulates (PM2.5)	Year Coverage*	NM	NM	NM	90%	86%	88%
	Max. 24-hour Concentration (µg/m3)	NM	NM	NM	56.2	64.1	78.3
	State Annual Average (µg/m3)	NM	NM	NM	16.0	NA	16.2
	#Days>Fed. 24-hour Std. of>35 µg/m3	NM	NM	NM	11	20	10
	National Annual Average (µg/m3)	NM	NM	NM	15.5	16.7	15.9
Lead	Maximum Monthly Concentration (µg/m3)	NM	NM	NM	NM	NM	NM
	# Months Exceeding Federal Std.	NM	NM	NM	NM	NM	NM
	# Months Exceeding State Std.	NM	NM	NM	NM	NM	NM
Sulfates	Max. 24-hour Concentration (µg/m3)	NM	NM	NM	NM	NM	NM
	#Samples>California 24-hour Std.>=25 µg/m3	NM	NM	NM	NM	NM	NM

Sources: California Air Resources Board, 2010: http://www.arb.ca.gov/adam/welcome.html. EPA AIRSData (for 1-Hour CO only): http://www.epa.gov/air/data/geosel.html

NM = not measured; NA = not applicable

*Year Coverage indicates how extensive monitoring was during the time of year when high pollutant concentrations were expected.

**The number of days above the standard is not necessarily the number of violations of the standard for the year.

3.3 Pollutant Description

3.3.1 Criteria Pollutants

Pollutants that have established national standards are referred to as "criteria pollutants." The sources of these pollutants, their effects on human health and the nation's welfare, and their final deposition in the atmosphere vary considerably. A brief description of each pollutant is provided below.

3.3.1.1 Ozone

Ozone (O_3) is a colorless toxic gas. As shown in Figure 3-1, O_3 is found in both the Earth's upper and lower atmospheric levels. In the upper atmosphere, O_3 is a naturally occurring gas that helps to prevent the sun's harmful ultraviolet rays from reaching the Earth. In the lower layer of the atmosphere, O_3 is man-made. Although O_3 is not directly emitted, it forms in the lower atmosphere through a chemical reaction between hydrocarbons (HC), also referred to as volatile organic compounds (VOC), and nitrogen oxides (NOx), which are emitted from industrial sources and from automobiles. HC are compounds comprised primarily of atoms of hydrogen and carbon. Total organic gases (TOG) and reactive organic gases (ROG) are the two classes of HC that are inventoried by CARB and SCAQMD. ROG have relatively high photochemical reactivity. The principal nonreactive HC is methane (CH_4), which is also a greenhouse gas. The major source of ROG is the incomplete combustion of fossil fuels in internal combustion engines. Other sources of ROG include the evaporative emissions associated with the use of paints and solvents, the application of asphalt paving, and the use of household consumer products. Adverse effects on human health are not caused directly by ROG, but rather by reactions of ROG to form secondary pollutants. ROG are also transformed into organic aerosols in the atmosphere, contributing to higher levels of fine particulate matter and lower visibility. The term "ROG" is used by CARB for air quality analysis, and is defined the same as the Federal term "volatile organic compound" (VOC).

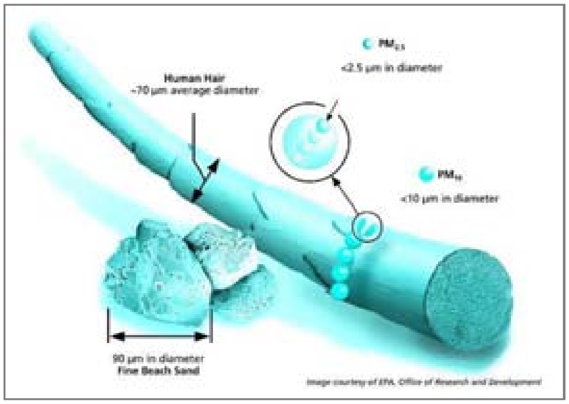
Source: Ozone NY

Figure 3-1. Ozone in the Atmosphere

Substantial O_3 formations generally require a stable atmosphere with strong sunlight; thus high levels of O_3 are generally a concern in the summer. O_3 is the main ingredient of smog. O_3 enters the bloodstream through the respiratory system and interferes with the transfer of oxygen, depriving sensitive tissues in the heart and brain of oxygen. O_3 also damages vegetation by inhibiting its growth. The effects of changes in VOC and NOx emissions for the proposed project are examined on a regional and statewide level.

3.3.1.2 Particulate Matter

Particulate pollution is composed of solid particles or liquid droplets that are small enough to remain suspended in the air. In general, particulate pollution can include dust, soot, and smoke; these can be irritating but usually are not poisonous. Particulate pollution also can include bits of solid or liquid substances that can be highly toxic. Of particular concern are those particles that are smaller than, or equal to, 10 microns (PM_{10}) or 2.5 microns ($PM_{2.5}$) in size.



Source: EPA Office of Air and Radiation

Figure 3-2. Relative Particulate Matter Size

PM_{10} refers to particulate matter less than 10 microns in diameter, about one-seventh the thickness of a human hair (Figure 3-2). Particulate matter pollution consists of very small liquid and solid particles floating in the air, which can include smoke, soot, dust, salts, acids, and metals. Particulate matter also forms when gases emitted from motor vehicles undergo chemical reactions in the atmosphere.

Major sources of PM_{10} include motor vehicles; wood-burning stoves and fireplaces; dust from construction, landfills, and agriculture; wildfires and brush/waste burning; industrial sources; windblown dust from open lands; and atmospheric chemical and photochemical reactions. Suspended particulates produce haze and reduce visibility.

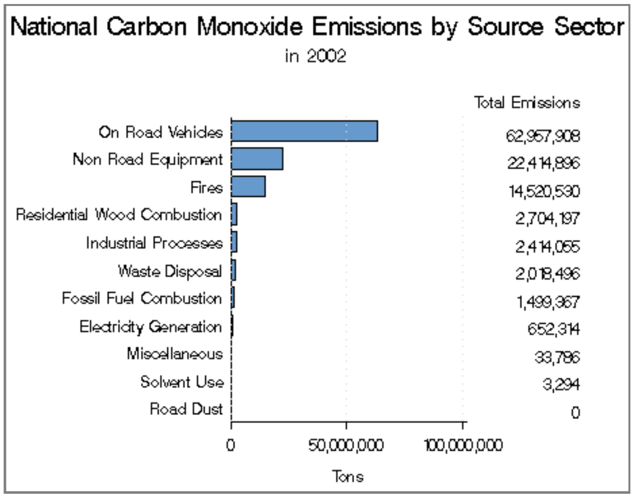
Data collected through numerous nationwide studies indicate that most of the PM_{10} comes from the following:

- Fugitive dust
- Wind erosion
- Agricultural and forestry sources

A small portion of particulate matter is the product of fuel combustion processes. In the case of $PM_{2.5}$, the combustion of fossil fuels accounts for a significant portion of this pollutant. The main health effect of airborne particulate matter is on the respiratory system. $PM_{2.5}$ refers to particulates that are 2.5 microns or less in diameter, roughly 1/28th the diameter of a human hair. $PM_{2.5}$ results from fuel combustion (from motor vehicles, power generation, and industrial facilities), residential fireplaces, and wood stoves. In addition, $PM_{2.5}$ can be formed in the atmosphere from gases such as sulfur dioxide, nitrogen oxides, and volatile organic compounds. Like PM_{10}, $PM_{2.5}$ can penetrate the human respiratory system's natural defenses and damage the respiratory tract when inhaled. Whereas particles 2.5 to 10 microns in diameter tend to collect in the upper portion of the respiratory system, particles 2.5 microns or less are so tiny that they can penetrate deeper into the lungs and damage lung tissues. The effects of PM_{10} and $PM_{2.5}$ emissions for the project are examined on a localized, or microscale, basis, a regional basis and a statewide basis.

3.3.1.3 Carbon Monoxide

CO is a colorless gas that interferes with the transfer of oxygen to the brain. CO is emitted almost exclusively from the incomplete combustion of fossil fuels. As shown in Figure 3-3, on-road motor vehicle exhaust is the primary source of CO. In cities, 85 to 95 percent of all CO emissions may come from motor vehicle exhaust. Prolonged exposure to high levels of CO can cause headaches, drowsiness, loss of equilibrium, or heart disease. CO levels are generally highest in the colder months of the year when inversion conditions (when warmer air traps colder air near the ground) are more frequent.



Source: USEPA

Figure 3-3. Sources of CO

CO concentrations can vary greatly over relatively short distances. Relatively high concentrations of CO are typically found near congested intersections, along heavily used roadways carrying slow-moving traffic, and in areas where atmospheric dispersion is inhibited by urban "street canyon" conditions. Consequently, CO concentrations must be predicted on a microscale basis.

3.3.1.4 Nitrogen Dioxide

NO_2 is a brownish gas that irritates the lungs. It can cause breathing difficulties at high concentrations. As with O_3, NO_2 is not directly emitted but is formed through a reaction between nitric oxide (NO) and atmospheric oxygen. NO and NO_2 are collectively referred to as nitrogen oxides (NO_x) and are major contributors to ozone formation. NO_2 also contributes to the formation of PM_{10}. At atmospheric concentrations, NO_2 is only potentially irritating. In high concentrations, the result is a brownish-red cast to the atmosphere and reduced visibility. There is some indication of a relationship between NO_2 and chronic pulmonary fibrosis. An increase in bronchitis in children (two and three years old) has also been observed at concentrations below 0.3 parts per million (ppm).

3.3.1.5 Lead

Lead (Pb) is a stable element that persists and accumulates both in the environment and in animals. Its principal effects in humans are on the blood-forming, nervous, and renal systems. Lead levels from mobile sources in the urban environment have decreased significantly due to the federally-mandated switch to lead-free gasoline, and they are expected to continually decrease. An analysis of lead emissions from transportation projects is therefore not warranted.

3.3.1.6 Sulfur Dioxide

SO_2 is a product of high-sulfur fuel combustion. The main sources of SO_2 are coal and oil used in power stations, industry, and domestic heating. Industrial chemical manufacturing is another source of SO_2. SO_2 is an irritant gas that attacks the throat and lungs. It can cause acute respiratory symptoms and diminished ventilator function in children. SO_2 can also yellow plant leaves and corrode iron and steel. Although diesel-fueled heavy duty vehicles emit SO_2, transportation sources are not considered by EPA (and other regulatory agencies) to be significant sources of this pollutant.

3.3.2 Toxic and Non-Criteria Pollutants

3.3.2.1 Asbestos

Asbestos has also become a pollutant of concern in regard to demolition and soil disturbance. Asbestos minerals occur in rock and soil as the result of natural geologic processes, often in veins near earthquake faults in the coastal ranges and the foothills of the Sierra Nevada Mountains and other areas of California. Naturally occurring asbestos (NOA) takes the form of long, thin, flexible, separable fibers. Natural weathering or human disturbance can break NOA down to microscopic fibers, easily suspended in air. When inhaled, these thin fibers irritate tissues and resist the body's natural defenses.

Asbestos is a known human carcinogen. It causes cancers of the lung and the lining of internal organs, as well as asbestosis and pleural disease that inhibit lung function. The USEPA is working to address concerns about potential effects of NOA in a number of areas in California.

3.3.2.2 Air Toxics

A toxic air contaminant (TAC) is defined by California law as an air pollutant that "may cause or contribute to an increase in mortality or an increase in serious illness, or which may pose a present or potential hazard to human health."[1] EPA uses the term hazardous air pollutant (HAP) in a similar sense. Controlling air toxic emissions became a national priority with the passage of the CAAA, whereby Congress mandated that the EPA regulate 188 air toxics, also known as hazardous air pollutants.

The EPA has assessed this expansive list in their latest rule on the Control of Hazardous Air Pollutants from Mobile Sources[2] and identified a group of 93 compounds emitted from mobile sources that are listed in their Integrated Risk Information System.[3] EPA identified seven compounds with significant contributions from mobile sources that are among the national and regional-scale cancer risk drivers from their 1999 National Air Toxics Assessment. These are acrolein, benzene, 1,3-butadiene, diesel particulate matter plus diesel exhaust organic gases (diesel PM), formaldehyde, naphthalene, and polycyclic organic matter. While the FHWA considers these the priority Mobile Source Air Toxics (MSATs), the list is subject to change and may be adjusted in consideration of future EPA rules. A brief description of these MSATs is given below.

Acrolein is a water-white or yellow liquid that burns easily, is readily volatilized, and has a disagreeable odor. It is present as a product of incomplete combustion in the exhausts of stationary equipment (e.g., boilers and heaters) and mobile sources. It is also a secondary pollutant, formed through the photochemical reaction of VOC and NO_X in the atmosphere.

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[1] California Health and Safety Code §39655(a).

[2] Federal Register, Vol. 72, No. 37, page 8430, February 26, 2007

[3] U.S. Environmental Protection Agency. 2009. *Integrated Risk Information System*. http://www.epa.gov/ncea/iris/index.html

Acrolein is considered to have high acute toxicity, and it causes upper respiratory tract irritation and congestion in humans. The major effects from chronic (long-term) inhalation exposure to acrolein in humans consist of general respiratory congestion and eye, nose, and throat irritation. No information is available on the reproductive, developmental, or carcinogenic effects of acrolein in humans. EPA considers acrolein data to be inadequate for an assessment of human carcinogenic potential.

Benzene is a volatile, colorless, highly flammable liquid with a sweet odor. Most of the benzene in ambient air is from incomplete combustion of fossil fuels and evaporation from gasoline service stations. Acute inhalation exposure to benzene causes neurological symptoms, such as drowsiness, dizziness, headaches, and unconsciousness in humans. Chronic inhalation of certain levels of benzene causes disorders in the blood in humans. Benzene specifically affects bone marrow (the tissues that produce blood cells). Aplastic anemia, excessive bleeding, and damage to the immune system (by changes in blood levels of antibodies and loss of white blood cells) may develop. Available human data on the developmental effects of benzene are inconclusive due to concomitant exposure to other chemicals, inadequate sample size, and lack of quantitative exposure data. EPA has classified benzene as a known human carcinogen by inhalation.

1,3-Butadiene is a colorless gas with a mild gasoline-like odor. Sources of 1,3-butadiene released into the air include motor vehicle exhaust, manufacturing and processing facilities, forest fires or other combustion, and cigarette smoke. Acute exposure to 1,3-butadiene by inhalation in humans results in irritation of the eyes, nasal passages, throat, and lungs. Neurological effects, such as blurred vision, fatigue, headache, and vertigo, have also been reported at very high exposure levels. One epidemiological study reported that chronic exposure to 1,3-butadiene via inhalation resulted in an increase in cardiovascular diseases, such as rheumatic and arteriosclerotic heart diseases, while other human studies have reported effects on the blood. No information is available on reproductive or developmental effects of 1,3-butadiene in humans. EPA has classified 1,3-butadiene as a probable human carcinogen by inhalation.

Diesel Particulate Matter/Diesel Exhaust Organic Gases are a complex mixture of hundreds of constituents in either a gaseous or particle form. Gaseous components of diesel exhaust (DE) include CO_2, oxygen, nitrogen, water vapor, CO, nitrogen compounds, sulfur compounds, and numerous low-molecular-weight hydrocarbons. Among the gaseous hydrocarbon components of DE that are individually known to be of toxicological relevance are several carbonyls (e.g., formaldehyde, acetaldehyde, acrolein), benzene, 1,3-butadiene, and polycyclic aromatic hydrocarbons (PAHs) and nitro-PAHs. PAHs are a group of chemicals that are formed during the incomplete burning of coal, oil, gas, wood, garbage, or other organic substances, such as tobacco and charbroiled meat. Human exposure to PAHs is typically to a mixture of PAH chemicals, not to individual PAH chemicals. Diesel particulate matter (DPM) is composed of a center core of elemental carbon and adsorbed organic compounds, as well as small amounts of sulfate, nitrate, metals, and other trace elements. DPM consists primarily of $PM_{2.5}$, including a subgroup with a large number of particles having a diameter <0.1 µm. Collectively, these particles have a large surface area, which makes them an excellent medium for adsorbing organics. Also, their small size makes them highly respirable and able to reach the deep lung. A number of potentially toxicologically-relevant organic compounds, including PAHs, nitro-PAHs, and oxidized PAH derivatives, are on the particles. Diesel exhaust is emitted from on-road mobile sources, such as automobiles and trucks, and from off-road mobile sources (e.g., diesel locomotives, marine vessels, and construction equipment). DPM is directly emitted from diesel-powered engines (primary particulate matter) and can be formed from the gaseous compounds emitted by diesel engines (secondary particulate matter).

Acute or short-term (e.g., episodic) exposure to DE can cause acute irritation (e.g., eye, throat, bronchial), neurophysiological symptoms (e.g., lightheadedness, nausea), and respiratory symptoms (cough, phlegm). Evidence also exists for an exacerbation of allergenic responses to known allergens and asthma-like symptoms. Information from the available human studies is inadequate for a definitive evaluation of possible non-cancer health effects from chronic exposure to DE. However, on the basis of extensive animal evidence, DE is judged to pose a chronic respiratory hazard to humans. EPA has determined that DE is "likely to be carcinogenic to humans by inhalation" and that this hazard applies to environmental exposures.

Formaldehyde is a colorless gas with a pungent, suffocating odor at room temperature. The major emission sources of formaldehyde appear to be power plants, manufacturing facilities, incinerators, and automobile exhaust. However, most of the formaldehyde in ambient air is a result of secondary formation through photochemical reaction of VOCs and NO_X. The major toxic effects caused by acute formaldehyde exposure via inhalation are eye, nose, and throat irritation and effects on the nasal cavity. Other effects seen from exposure to high levels of formaldehyde in humans are coughing, wheezing, chest pains, and bronchitis. Chronic exposure to formaldehyde by inhalation in humans has been associated with respiratory symptoms and eye, nose, and throat irritation. EPA considers formaldehyde to be a probable human carcinogen.

Naphthalene is used in the production of phthalic anhydride; it is also used in mothballs. Acute (short-term) exposure of humans to naphthalene by inhalation, ingestion, and dermal contact is associated with hemolytic anemia, damage to the liver, and neurological damage. Cataracts have also been reported in workers acutely exposed to naphthalene by inhalation and ingestion. Chronic (long-term) exposure of workers and rodents to naphthalene has been reported to cause cataracts and damage to the retina. Hemolytic anemia has been reported in infants born to mothers who "sniffed" and ingested naphthalene (as mothballs) during pregnancy. Available data are inadequate to establish a causal relationship between exposure to naphthalene and cancer in humans. EPA has classified naphthalene as a Group C, possible human carcinogen.

The term **Polycyclic Organic Matter** (POM) defines a broad class of compounds that includes the polycyclic aromatic hydrocarbon compounds (PAH) compounds, of which benzo[a]pyrene is a member. POM compounds are formed primarily from combustion and are present in the atmosphere in particulate form. Sources of air emissions are diverse and include cigarette smoke, vehicle exhaust, home heating, laying tar, and grilling meat. Cancer is the major concern from exposure to POM. Epidemiologic studies have reported an increase in lung cancer in humans exposed to coke oven emissions, roofing tar emissions, and cigarette smoke; all of these mixtures contain POM compounds. Animal studies have reported respiratory tract tumors from inhalation exposure to benzo[a]pyrene and stomach tumors, leukemia, and lung tumors from oral exposure to benzo[a]pyrene. EPA has classified seven PAHs (benzo[a]pyrene, benz[a]anthracene, chrysene, benzo[b]fluoranthene, benzo[k]fluoranthene, dibenz[a,h]anthracene, and indeno[1,2,3-cd]pyrene) as Group B2, probable human carcinogens.

3.4 Attainment Status

Section 107 of the 1977 Clean Air Act Amendment requires that the USEPA publish a list of all geographic areas in compliance with the NAAQS, plus those not attaining the NAAQS. Areas not in NAAQS compliance are deemed non-attainment areas. Areas that have insufficient data to make a determination are deemed unclassified, and are treated as being attainment areas until proven otherwise. An area's designation is based on the data collected by the state monitoring network on a pollutant-by-pollutant basis.

The project area is located in Los Angeles County. As shown Table 3-3, the USEPA has classified Los Angeles County as a severe nonattainment area for ozone, a serious nonattainment area for PM_{10}, and a nonattainment area for $PM_{2.5}$. Los Angeles County is listed as a maintenance area for carbon monoxide, as it was previously a nonattainment area for carbon monoxide. This analysis focuses on these criteria pollutant(s).

Table 3-3. Project Area Attainment Status

Pollutant	Federal Attainment Status
Ozone (O_3)	Nonattainment
Nitrogen Dioxide (NO_2)	Attainment
Carbon Monoxide (CO)	Attainment/Maintenance
Particulate Matter (PM_{10})	Nonattainment
Particulate Matter ($PM_{2.5}$)	Nonattainment
All others	Attainment/Unclassified

Source: Environmental Protection Agency (EPA), 2010

3.5 State Implementation Plan and Transportation Improvement Program Status

The Regional Transportation Plan (RTP) presents the transportation vision for the six-county region of Imperial, Los Angeles, Orange, Riverside, San Bernardino and Ventura Counties through the year 2035 and provides a long-term investment framework for addressing the region's transportation and related challenges. Under the CAAA, the Intermodal Surface Transportation Efficiency Act of 1991 (ISTEA), and the Transportation Equity Act for the 21st Century (TEA-21), proposed transportation projects must be derived from a long-range transportation plan or RTP that conforms with the state air quality plans as outlined in the State Implementation Plan (SIP). The SIP sets forth the state's strategies for achieving air quality standards. Projects must also be included in a Transportation Improvement Program (TIP) that conforms with the SIP, and localized impacts from proposed projects must conform to state air quality plans in non-attainment and maintenance areas.

A metropolitan planning organization (MPO) is the designated local decision-making body that is responsible for carrying out the metropolitan transportation planning process for an urban area. SCAG, as the federally designated MPO for most of Southern California, is required to adopt and periodically update a long-range transportation plan and develop an

RTP and TIP for Los Angeles, Orange, San Bernardino, Riverside, Ventura, and Imperial Counties.

The Westside Subway Extension project was included in the regional emissions analysis conducted by SCAG for the conforming 2008 RTP as Project ID #UT1014 as well as Project ID #1TR1002 and #1TR1003 in Draft Amendment #3 to the RTP[5]. The project's design concept and scope have not changed significantly from what was analyzed in the 2008 RTP and Draft Amendment #3. This analysis found that the plan and, therefore, the individual projects contained in the plan, are conforming projects, and will have air quality impacts consistent with those identified in the SIPs for achieving the NAAQS. The 2008 RTP was adopted by SCAG on May 8, 2008.

The Westside Subway Extension project is included in the Draft Amendment #08-346 to the 2008 Regional Transportation Improvement Plan (RTIP)[7] as Project ID #UT101, #1TR1002 and #1TR1003 (refer to page 5 of Draft Amendment). The Westside Subway Extension is also included in Metro's 2009 LRTP [8] under Candidates for Private Sector Financial Participation – Transit Projects (refer to Figure K on page 25).

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[4] RTP available at http://www.scag.ca.gov/rtp2008/index.htm

[5] Draft Amendment available at http://www.scag.ca.gov/rtp2008/pdfs/amendrtp/amend03_2008RTP_PD.pdf

[6] Draft Amendment available at http://www.scag.ca.gov/rtp2008/pdfs/amendrtp/amend03_2008RTP_PD.pdf

[7] RTIP available at http://www.scag.ca.gov/RTIP/rtip2008/adopted.htm

[8] LRTP available at http://www.metro.net/projects_studies/images/final-2009-LRTP.pdf

4.0 ENVIRONMENTAL IMPACT/ ENVIRONMENTAL CONSEQUENCES

Pollutants that can be traced principally to motor vehicles are relevant to the evaluation of the project's impacts; these pollutants include CO, HC, NO_x, O_3, PM_{10}, $PM_{2.5}$, and MSAT. Transportation sources account for a small percentage of regional emissions of SO_x and Pb; thus, a detailed analysis is not required.

HC (VOC) and NO_x emissions from automotive sources are a concern primarily because they are precursors in the formation of ozone and particulate matter. Ozone is formed through a series of reactions that occur in the atmosphere in the presence of sunlight. Since the reactions are slow and occur as the pollutants are diffusing downwind, elevated ozone levels often are found many miles from the sources of the precursor pollutants. Therefore, the effects of HC and NO_x emissions generally are examined on a regional or "mesoscale" basis.

PM_{10} and $PM_{2.5}$ impacts are both regional and local. A significant portion of particulate matter, especially PM_{10}, comes from disturbed vacant land, construction activity, and paved road dust. $PM_{2.5}$ also comes from these sources. Motor vehicle exhaust, particularly from diesel vehicles, is also a source of PM_{10} and $PM_{2.5}$. PM_{10}, and especially $PM_{2.5}$, can also be created by secondary formation from precursor elements such as SO_2, NO_X, VOCs, and ammonia (NH_3). Secondary formation occurs due to chemical reaction in the atmosphere generally downwind some distance from the original emission source. Thus it is appropriate to predict concentrations of PM_{10} and $PM_{2.5}$ on both a regional and a localized basis.

CO impacts are generally localized. Even under the worst meteorological conditions and most congested traffic conditions, high concentrations are limited to a relatively short distance (300 to 600 feet) of heavily traveled roadways. Vehicle emissions are the major sources of CO. The Westside Subway Extension project could change traffic patterns within the project area. Consequently, it is appropriate to predict concentrations of CO on both a regional and a localized or "microscale" basis.

MSAT impacts are both regional and local. On February 3, 2006, the FHWA released "*Interim Guidance on Air Toxic Analysis in NEPA Documents.*" This guidance was superseded on September 30, 2009 by FHWA's "*Interim Guidance Update on Air Toxic Analysis in NEPA Documents.*" According to these documents, regardless of the alternative chosen, MSAT emissions will likely be lower than present levels in the design year as a result of EPA's national control programs that are projected to reduce annual MSAT emissions by 72 percent between 1999 and 2050. Local conditions may differ from these national projections in terms of fleet mix and turnover, vehicle miles traveled (VMT) growth rates, and local control measures. However, the magnitude of the EPA-projected reductions is so great (even after accounting for VMT growth) that MSAT emissions in the study area are likely to be lower in the future in nearly all cases.

4.1 Regional Emissions Analysis

The regional emission burden analysis of a project determines a project's overall impact on air quality levels. For this project, an analysis was conducted for the study area and for the entire region. The "region" is the 5 County Region which includes Los Angeles, Ventura, San Bernardino, Riverside and Orange Counties, and the "Study Area" is in western Los Angeles County and encompasses approximately 38 square miles. The Study Area, shown in Figure 4-1, is east-west oriented and includes portions of five jurisdictions: the cities of Los Angeles, West Hollywood, Beverly Hills, and Santa Monica, as well as portions of unincorporated Los Angeles County. The boundaries of the Study Area generally extend north to the base of the Santa Monica Mountains along Hollywood, Sunset and San Vicente Boulevards, east to the Metro Rail stations at Hollywood/Highland and Wilshire/Western, south to Pico Boulevard, and west to the Pacific Ocean.

The regional emissions analysis was conducted for the No Build and eight build alternatives. The analysis was based on regional VMT estimates and vehicle hours traveled (VHT) estimates. Emission factors were obtained from CARB's emission factor program, EMFAC2007, the latest emission inventory model for the calculation of mobile source emission factors for vehicles operating on roads in California, using parameters set within the program for Los Angeles County. The results for the study area are shown in Table 4-1. The results for the region are shown in Table 4-2. As shown in these tables, the project, with the exception of the TSM alternative, is predicted to slightly lower all regional pollutant burden levels on both the study area and regional level. Impacts of the project are below the regional significance thresholds developed by the SCAQMD. While all alternatives, with the exception of the TSM alternative within the study area, are predicted to slightly reduce overall emission burden levels, Alternative 5 (Santa Monica Extension plus West Hollywood Extension) is estimated to lower emissions the most within the study area and on a regional level.

Figure 4-1. Corridor Study Area

Table 4-1. Study Area Emission Burden Assessment

	VMT		CO			TOG			NOx			PM10			PM2.5		
	Daily Vehicle Miles Traveled	Percent change from No Build	Emission Burden (Kg/day)	Change from No Build (Kg/day)	Percent change from No Build	Emission Burden (Kg/day)	Change from No Build (Kg/day)	Percent change from No Build	Emission Burden (Kg/day)	Change from No Build (Kg/day)	Percent change from No Build	Emission Burden (Kg/day)	Change from No Build (Kg/day)	Percent change from No Build	Emission Burden (Kg/day)	Change from No Build (Kg/day)	Percent change from No Build
No Build	5,056,227		5,182.3		-	326.0		-	1,146.0		-	278.1	-		194.3	-	
TSM	5,056,227	0.00%	5,185.4	3.1	0.1%	326.4	0.4	0.00%	1,146.5	0.5	0.0%	278.6	0.4	0.2%	194.7	0.4	0.2%
MOS 1	5,040,990	-0.30%	5,169.4	-12.8	-0.2%	325.2	-0.8	-0.30%	1,143.1	-2.9	-0.3%	277.5	-0.7	-0.2%	193.9	-0.4	-0.2%
MOS 2	5,032,122	-0.48%	5,160.1	-22.1	-0.4%	324.6	-1.4	-0.48%	1,141.0	-5.0	-0.4%	276.9	-1.2	-0.4%	193.5	-0.8	-0.4%
Alt. 1	5,027,245	-0.57%	5,116.5	-65.8	-1.3%	319.0	-7.0	-0.57%	1,130.9	-15.1	-1.3%	273.1	-5.0	-1.8%	189.8	-4.5	-2.3%
Alt. 2	5,024,328	-0.63%	5,116.5	-65.8	-1.3%	319.0	-7.0	-0.63%	1,130.8	-15.2	-1.3%	273.1	-5.0	-1.8%	189.8	-4.5	-2.3%
Alt. 3	5,018,459	-0.75%	5,107.2	-75.0	-1.4%	318.4	-7.6	-0.75%	1,128.8	-17.2	-1.5%	272.6	-5.5	-2.0%	189.4	-4.9	-2.5%
Alt. 4	5,021,440	-0.69%	5,110.3	-72.0	-1.4%	318.6	-7.4	-0.69%	1,129.5	-16.5	-1.4%	272.8	-5.4	-1.9%	189.5	-4.8	-2.5%
Alt. 5	5,014,584	-0.82%	5,103.3	-78.9	-1.5%	318.1	-7.8	-0.82%	1,128.0	-18.0	-1.6%	272.4	-5.7	-2.1%	189.3	-5.0	-2.6%
SCAQMD Significance Threshold			249 (550 lbs/day)			24.9 (55 lbs/day)			24.9 (55 lbs/day)			68 (150 lbs/day)			24.9 (55 lbs/day)		

Table 4-2. Regional Emission Burden Assessment

	VMT		CO			TOG			NOx			PM10			PM2.5		
	Daily Vehicle Miles Traveled	Percent change from No Build	Emission Burden (Kg/day)	Change from No Build (Kg/day)	Percent change from No Build	Emission Burden (Kg/day)	Change from No Build (Kg/day)	Percent change from No Build	Emission Burden (Kg/day)	Change from No Build (Kg/day)	Percent change from No Build	Emission Burden (Kg/day)	Change from No Build (Kg/day)	Percent change from No Build	Emission Burden (Kg/day)	Change from No Build (Kg/day)	Percent change from No Build
No Build	504,281,492		550,123.9		-	40,766.2		-	125,151.1		-	30,856.7	-		22,329.6	-	
TSM	504,281,492	-0.01%	550,103.7	-20.2	-0.01%	40,766.1	-0.1	0.0%	125,147.2	-4.0	0.0%	30,856.0	-0.7	0.0%	22,329.3	-0.3	0.0%
MOS 1	504,281,492	-0.07%	549,734.7	-389.2	-0.07%	40,735.5	-30.7	-0.1%	125,061.9	-89.2	-0.1%	30,834.4	-22.3	-0.1%	22,313.2	-16.4	-0.1%
MOS 2	504,281,492	-0.07%	549,729.2	-394.6	-0.07%	40,735.1	-31.0	-0.1%	125,060.6	-90.5	-0.1%	30,834.2	-22.5	-0.1%	22,313.1	-16.5	-0.1%
Alt. 1	504,281,492	-0.07%	549,734.3	-389.5	-0.07%	40,737.0	-29.2	-0.1%	125,062.4	-88.7	-0.1%	30,834.8	-21.8	-0.1%	22,313.8	-15.8	-0.1%
Alt. 2	504,281,492	-0.07%	549,737.2	-386.7	-0.07%	40,738.2	-28.0	-0.1%	125,063.5	-87.7	-0.1%	30,835.2	-21.5	-0.1%	22,314.1	-15.5	-0.1%
Alt. 3	504,281,492	-0.07%	549,715.4	-408.4	-0.07%	40,736.7	-29.5	-0.1%	125,059.7	-91.5	-0.1%	30,833.5	-23.1	-0.1%	22,314.2	-15.4	-0.1%
Alt. 4	504,281,492	-0.07%	549,732.9	-391.0	-0.07%	40,737.8	-28.3	-0.1%	125,062.5	-88.6	-0.1%	30,834.9	-21.7	-0.1%	22,313.9	-15.6	-0.1%
Alt. 5	504,281,492	-0.07%	549,714.7	-409.1	-0.1%	40,735.0	-31.2	-0.1%	125,057.8	-93.3	-0.1%	30,833.5	-23.1	-0.1%	22,312.7	-16.9	-0.1%
SCAQMD Significance Threshold			249 (550 lbs/day)			24.9 (55 lbs/day)			24.9 (55 lbs/day)			68 (150 lbs/day)			24.9 (55 lbs/day)		

4.2 Local Impacts and Hot Spot Assessment

The localized assessment of air quality was conducted to address CO, PM_{10} and $PM_{2.5}$ impacts, as well as MSAT

4.2.1 Carbon Monoxide

CO Microscale air quality modeling was performed using the most recent version of CARB's mobile source emission factor model (EMFAC2007) and EPA's CAL3QHC (Version 2.0) air quality dispersion model to estimate existing and future No Build Alternative and future Build Alternatives CO levels at selected locations in the project area.

4.2.1.1 Site Selection and Receptor Locations

A screening analysis was performed to identify which intersections in the project study area would be adversely affected by the project. 194 intersections within the study area were screened based on changes in intersection volume, delay and level of service (LOS) between the No Build and Build Alternatives. Sites fail the screening evaluation if the LOS decreases below D due to any of the Build Alternatives, or if the delay and/or volume increase from the No Build with any of the Build Alternatives along with a LOS below D. Based on the screening criteria, 110 sites failed the screening analysis. Details of the screening analysis are highlighted in Appendix A of this report. From this subset of sites, five sites were chosen for detailed analysis. These sites, listed in Table 4-3 and shown in Figure 4-2, are those sites within the study area that have the highest volumes, highest delays, and/or the highest volume increases due to the project.

Table 4-3. CO Microscale Analysis Sites

Analysis Site #	Location
1	26th Street & Wilshire Boulevard
2	Veteran Avenue & Wilshire Boulevard
3	Glendon Avenue & Wilshire Boulevard
4	La Cienega Boulevard & Beverly Boulevard
5	La Brea Avenue and Olympic Boulevard

Microscale CO levels were modeled at these five using the USEPA-authorized CAL3QHC program.

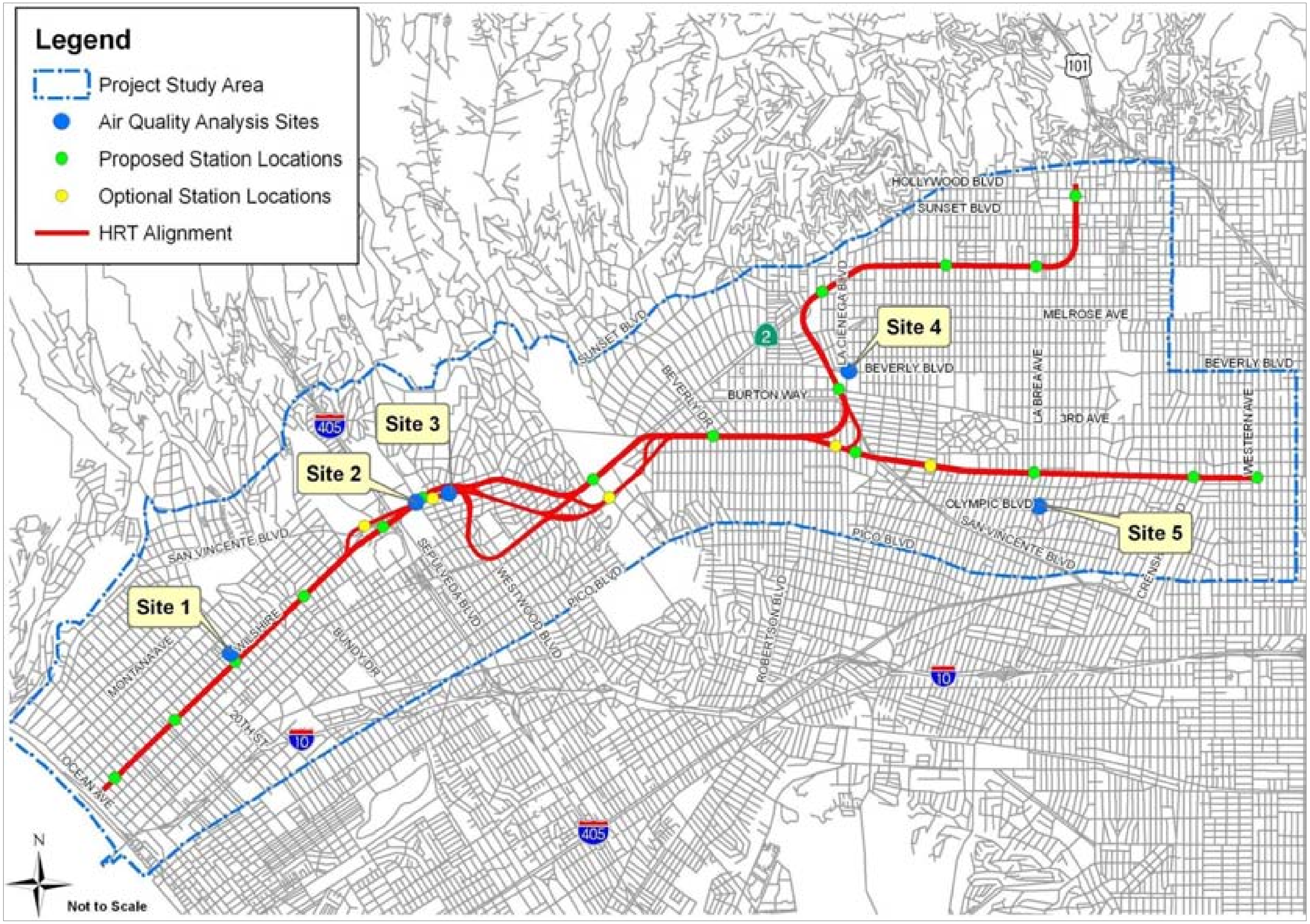


Figure 4-2. Air Quality Analysis Sites

4.2.1.2 Emission Model

Vehicular Emissions were estimated using CARB's EMFAC2007 (January 2008) emission factor program. EMFAC2007 is a mobile source emission estimate program that provides current and future estimates of emissions from highway motor vehicles. The latest in the EMFAC series, EMFAC2007 was designed by CARB to address a wide variety of air pollution modeling needs. This latest version incorporates updated information on basic emission rates, more realistic driving patterns, separation of start and running emissions, improved correction factors, and changing fleet composition. The emissions used for the microscale analysis are presented in Appendix B.

4.2.1.3 Dispersion Model

Mobile source models are the basic analytical tools used to estimate CO concentrations expected under given traffic, roadway geometry, and meteorological conditions. The mathematical expressions and formulations that comprise the various models attempt to describe an extremely complex physical phenomenon as closely as possible. The dispersion modeling program used in this study for estimating pollutant concentrations near roadway intersections is the CAL3QHC (Version 2.0) dispersion model developed by the EPA and released in 1992.

CAL3QHC is a Gaussian model recommended in the *EPA Guidelines for Modeling Carbon Monoxide from Roadway Intersections* (EPA-454/R-92-005). Gaussian models assume that the dispersion of pollutants downwind of a pollution source follow a normal distribution from the center of the pollution source.

Different emission rates occur when vehicles are stopped (idling), accelerating, decelerating, and moving at different average speeds. CAL3QHC simplifies these different emission rates into two components:

- Emissions when vehicles are stopped (idling) during the red phase of a signalized intersection

- Emissions when vehicles are in motion during the green phase of a signalized intersection

The CAL3QHC (Version 2.0) air quality dispersion model has undergone extensive testing by EPA and has been found to provide reliable estimates of inert (nonreactive) pollutant concentrations resulting from motor vehicle emissions. A complete description of the model is in the *User's Guide to CAL3QHC version 2.0: A Modeling Methodology for Predicting Pollutant Concentrations near Roadway Intersections* (EPA-454/R-92-006). The CAL3QHC input and output files used for the microscale modeling are presented in Appendix C.

4.2.1.4 Meteorological Conditions

The transport and concentration of pollutants emitted from motor vehicles are influenced by three principal meteorological factors: wind direction, wind speed, and the temperature profile of the atmosphere. The values for these parameters were chosen to maximize pollutant concentrations at each prediction site (i.e., to establish a conservative worst case situation).

- **Wind Direction**—Maximum CO concentrations are normally found when the wind is assumed to blow approximately parallel to a single roadway adjacent to the receptor location. At complex intersections, however, it is difficult to predict which wind angle will result in maximum concentrations. At each receptor location, therefore, the approximate wind angle that would result in maximum pollutant concentrations was used in the analysis. All wind angles from 0° to 360° (in 5° increments) were considered.

- **Wind Speed**—CO concentrations are greatest at low wind speeds. A conservative wind speed of 1.0 meter per second (2.2 miles per hour) was used to predict CO concentrations during peak traffic periods.
- **Temperature and Profile of the Atmosphere**—An ambient temperature of 56° F, a "mixing" height (the height in the atmosphere to which pollutants rise) of 1000 meters, and neutral atmospheric stability (stability class D) conditions will be used in estimating microscale CO concentrations.

The selection of these meteorological parameters was based on recommendations from the CEQA Air Quality Handbook and EPA's Guidelines. This data was found to be the most representative of the conditions existing in the project area.

4.2.1.5 Persistence Factor

Peak eight-hour concentrations of CO were obtained by multiplying the highest peak hour CO estimates by a persistence factor. The persistence factor accounts for the fact that:

- Over eight-hours (as distinct from a single hour) vehicle volumes will fluctuate downward from the peak hour.
- Vehicle speeds may vary.
- Meteorological conditions including wind speed and wind direction will vary compared to the conservative assumptions used for the single hour.

A persistence factor of 0.7 was used in this analysis. This factor is recommended for use by the EPA.

4.2.1.6 Background Concentrations

Microscale modeling is used to predict CO concentrations resulting from emissions from motor vehicles using roadways immediately adjacent to the locations at which predictions are being made. A CO background level must be added to this value to account for CO entering the area from other sources upwind of the receptors. The CO background level should be located away from the influence of local traffic congestion. For the project area, the data collected at the West Los Angeles monitoring station located at the Veterans Administration Hospital at Wilshire Boulevard and Sawtelle Boulevard was used for a background concentration. The use of this monitor is conservative because, though it is the closest monitor to the general study area and it has a neighborhood spatial scale, it is influenced by traffic. The second highest monitored value was used as a background concentration. The second highest monitored one-hour CO concentration during the period of 2006 – 2008 (2009 data is not validated yet) was 2.8 ppm; the second highest eight-hour average was 1.9 ppm. These values were conservatively used as the background for all CO modeling analyses. Future CO background levels are anticipated to be lower than existing levels due to mandated emission source reductions.

4.2.1.7 Traffic Information

Traffic data for the air quality analysis were derived from traffic counts and other information developed as part of an overall traffic analysis for the project. Output from the "Synchro6" signal timing traffic model was used to obtain signal timing parameters. The microscale CO analysis was performed based on data from this analysis for the AM and PM peak traffic periods. These are the periods when maximum traffic volumes occur on local streets and when the greatest traffic and air quality effects of the proposed project are expected.

4.2.1.8 Analysis Years

CO concentrations were predicted for the existing and design year (2035) for the project.

4.2.2 Analysis Results

Maximum one-hour and eight-hour CO levels were predicted at receptor sites along the proposed project. Maximum one-hour CO concentrations are shown in Table 4-4. Maximum eight-hour CO concentrations are shown in Table 4-5.

The existing conditions have the highest predicted one-hour and eight-hour CO concentrations, with Site 5 (La Brea Avenue and Olympic Boulevard) having the highest concentrations of 4.00 ppm (one-hour) and 2.74 ppm (eight-hour).

Of the future MOS alternatives, both MOS 1 and 2 have lower predicted CO concentrations, when compared to No Build, at Sites 1, 2 and 3. CO concentrations at Sites 3 and 4 are the same for MOS 1 and 2 as for No Build.

For the future Build Alternatives (1 through 5), CO concentrations range from slightly lower than to the same as for No Build; at no locations are CO concentrations for the Build Alternatives predicted to be higher than for No Build.

No violations of the NAAQS are predicted under any alternative.

Table 4-4. Predicted One-hour CO Concentrations (ppm)

No.	Site Description	Existing		No Build		MOS 1		MOS 2		Alternative 1		Alternative 2		Alternative 3		Alternative 4		Alternative 5	
		AM	PM	AM	PM	AM	PM	AM	PM	AM	PM	AM	PM	AM	PM	AM	PM	AM	PM
1	26th Street & Wilshire Boulevard	3.60	3.60	3.00	3.00	2.80	2.80	2.80	2.80	2.80	2.80	2.80	2.80	3.00	3.00	2.80	2.80	3.00	3.00
2	Veteran Avenue & Wilshire Boulevard	3.80	3.80	3.20	3.10	2.80	2.80	2.80	2.80	3.20	3.10	3.10	3.10	3.20	3.10	3.20	3.10	3.20	3.10
3	Glendon Avenue & Wilshire Boulevard	3.70	3.70	3.10	3.10	2.80	2.80	2.80	2.80	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10
4	La Cienega Boulevard & Beverly Boulevard	3.60	3.70	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00
5	La Brea Avenue and Olympic Boulevard	4.00	4.00	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10

Concentrations include one-hour CO background = 2.8 ppm
One-hour NAAQS = 35 ppm
SAAQS = 20 ppm

Table 4-5. Predicted Eight-hour CO Concentrations (ppm)

No.	Site Description	Existing	No Build	MOS 1	MOS 2	Alternative 1	Alternative 2	Alternative 3	Alternative 4	Alternative 5
1	26th Street & Wilshire Boulevard	2.46	2.04	1.90	1.90	1.90	1.90	2.04	1.90	2.04
2	Veteran Avenue & Wilshire Boulevard	2.60	2.18	1.90	1.90	2.18	2.11	2.18	2.18	2.18
3	Glendon Avenue & Wilshire Boulevard	2.53	2.11	1.90	1.90	2.11	2.11	2.11	2.11	2.11
4	La Cienega Boulevard & Beverly Boulevard	2.53	2.04	2.04	2.04	2.04	2.04	2.04	2.04	2.04
5	La Brea Avenue and Olympic Boulevard	2.74	2.11	2.11	2.11	2.11	2.11	2.11	2.11	2.11

Concentrations include one-hour CO background = 2.8 ppm
One-hour NAAQS = 35 ppm
SAAQS = 20 ppm

4.2.3 Particulate Matter (PM10 and PM2.5)

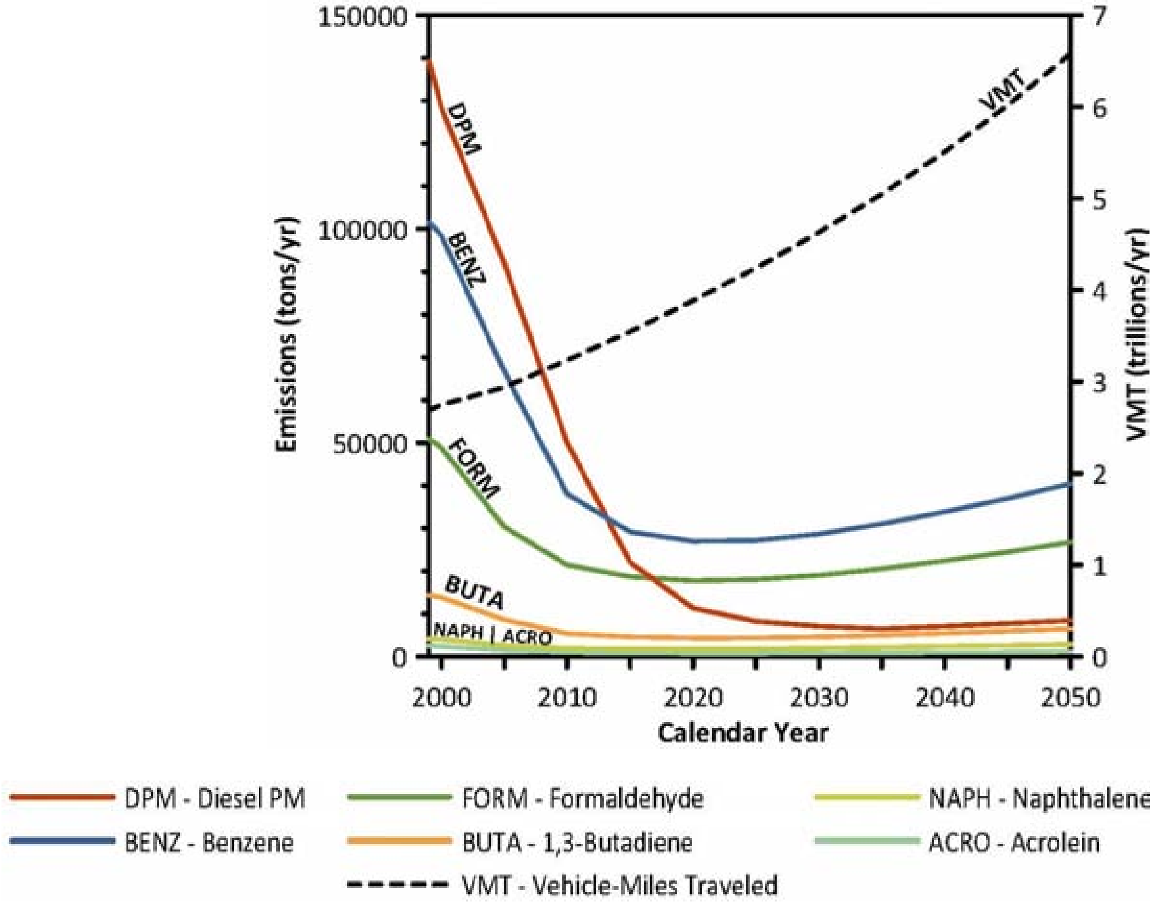
Because the project area is classified as a nonattainment area for PM_{10} and $PM_{2.5}$, a PM_{10} and $PM_{2.5}$ qualitative hotspot analysis following EPA's March 29, 2006 guidance "*Transportation Conformity Guidance for Qualitative Hot-spot Analyses in* $PM_{2.5}$ *and* PM_{10} *Nonattainment and Maintenance Areas* (EPA420-B-06-902) will be conducted, as recommended in EPA's Final Rule regarding the localized or "hot-spot" analysis of $PM_{2.5}$ and PM_{10} (40 CFR Part 93 – issued on March 10, 2006).

The proposed project will be electrically powered. Buses servicing stations will be powered by compressed natural gas. As such, the project is not anticipated to increase diesel traffic within the study area and is considered a project not of air quality concern. An interagency consultation, following SCAG procedures, is being scheduled to confirm this finding.

4.2.4 Mobile Source Air Toxics

The USEPA is the lead federal agency for administering the CAA and has certain responsibilities regarding the health effects of Mobile Source Air Toxics (MSATs). The USEPA issued a Final Rule on Controlling Emissions of Hazardous Air Pollutants from Mobile Sources (66 Federal Register 17229, March 29, 2001). This rule was issued under the authority in Section 202 of the CAA. In its rule, USEPA examined the impacts of existing and newly promulgated mobile source control programs, including its reformulated gasoline program, its national low emission vehicle standards, its Tier 2 motor vehicle emissions standards and gasoline sulfur control requirements, and its proposed heavy duty engine and vehicle standards and on-highway diesel fuel requirements. Future emissions likely would be lower than present levels as result of the USEPA's national control programs that are projected to reduce MSAT emissions by 72 percent from 1999 to 2050, even if VMT increases by 145 percent, as shown in Figure 4-3.

On February 9, 2007 and under authority of CAA Section 202(l), USEPA signed a Final Rule, Control of Hazardous Air Pollutants from Mobile Sources, which sets standards to control MSATs from motor vehicles. Under this rule, USEPA is setting standards on fuel composition, vehicle exhaust emissions, and evaporative losses from portable containers. The new standards are estimated to reduce total emissions of MSATs by 330,000 tons in 2030, including 61,000 tons of benzene. Concurrently, total emissions of VOCs will be reduced by over 1 .1 million tons in 2030 as a result of adopting these standards.



Source: U.S. Environmental Protection Agency. MOBILE6.2 Model run 20 August 2009.

Figure 4-3. National MSAT Emission Trends 1999 – 2050 for Vehicles Operating on Roadways Using USEPA's Mobile6.2 Model

On February 3, 2006, the FHWA released "*Interim Guidance on Air Toxic Analysis in NEPA Documents.*" This guidance was superseded on September 30, 2009 by FHWA's "*Interim Guidance Update on Air Toxic Analysis in NEPA Documents.*" The purpose of FHWA's guidance is to advise on when and how to analyze MSATs in the NEPA process for highways. This guidance is interim because MSAT science is still evolving. As the science progresses, FHWA will update the guidance.

A qualitative analysis provides a basis for identifying and comparing the potential differences among MSAT emissions, if any, from the various alternatives. The qualitative assessment presented below is derived in part from a study conducted by the FHWA entitled *A Methodology for Evaluating Mobile Source Air Toxic Emissions Among Transportation Project Alternatives*, found at: www.fhwa.dot.gov/environment/airtoxic/msatcompare/msatemissions.htm. FHWA's Interim Guidance groups projects into the following tier categories:

- No analysis for projects with no potential for meaningful MSAT Effects;
- Qualitative analysis for projects with low potential MSAT effects; or
- Quantitative analysis to differentiate alternatives for projects with higher potential MSAT effects.

Based on the recommended tiering approach, this project falls within the Tier 2 approach. Tier 2 is appropriate for this project because it does not fall under the Tier 1 category, which includes:

- Projects qualifying as a categorical exclusion under 23 CFR, Part 771.117(c);
- Projects exempt under the Clean Air Act conformity rule under 40 CFR, Part 93.126; or
- Other projects with no meaningful impacts on traffic volumes or vehicle mix.

The project also does not fall under the Tier 3 category. Tier 3 includes projects that:

- Create or significantly alter a major intermodal freight facility that has the potential to concentrate high levels of diesel particulate matter in a single location; or
- Create new or add significant capacity to urban highways such as interstates, urban arterials, or urban collector-distributor routes with traffic volumes where the average annual daily traffic (AADT) is projected to be in the range of 140,000 to 150,000 vehicles per day (vpd), or greater, by the design year.

And also:

- Proposed to be located in proximity to populated areas.

As stated in FHWA's guidance, Tier 2 includes projects that "serve to improve operations of highway, transit or freight without adding substantial new capacity or without creating a facility that is likely to meaningfully increase MSAT emissions. This category covers a broad range of projects." Based on this guidance, the project was analyzed using the Tier 2 approach.

For each detailed study alternative in this analysis, the amount of MSATs emitted would be proportional to the VMT assuming that other variables such as fleet mix are the same for each detailed study alternative. Table 4-1 and Table 4-2 show the 2035 estimated total VMT for the project alternatives, as well as for the No-Build Alternative. The VMT estimated for each of the project alternatives is lower or the same as for the No-Build Alternative, on both the study area and regional level. Alternative 4 is predicted to demonstrate the largest VMT reduction of all the alternatives on a regional level and Alternative 5 is predicted to demonstrate the largest VMT reduction of all the alternatives within the study area. Along with the reduction in VMT, the alternatives are predicted to show a very slight improvement in overall network speed. According to USEPA's Mobile6.2 emissions model, emissions of all of the priority MSATs except for diesel particulate matter decrease as speed increases. However, the extent to which these speed-related emissions decreases will affect overall MSATs levels cannot be reliably projected because of the inherent deficiencies of technical models.

Based upon these results, the proposed project is predicted to reduce MSATs in the overall project area in comparison to the No-Build Alternative. Also, regardless of the alternative chosen, emissions likely would be lower than present levels in the design year as a result of USEPA's national control programs that are projected to reduce annual MSAT emissions by 72 percent between 1999 and 2050. Local conditions may differ from these national projections in terms of fleet mix and turnover, VMT growth rates, and local control measures. However, the magnitude of the USEPA-projected reductions is so great (even after accounting for VMT growth) that MSAT emissions in the project area likely would be lower in the future in nearly all cases.

As the majority of the project is located underground, localized impacts of MSATs would be limited to areas where additional traffic may be generated. These locations would generally be around station sites where increased bus and commuter traffic would be generated. Based on the traffic analysis generated for the project, the largest increase in intersection volume (272 vehicles) is predicted to occur at the relatively low volume intersection of Gayley Avenue and Le Conte Avenue (less than 2,500 vehicles during the peak periods), under Alternative 1. This intersection is predicted to operate at a LOS of B and D for the AM and PM peak periods respectively under all alternatives. The highest volume intersection in the study area is the intersection of Veteran Avenue and Wilshire Boulevard, with an overall peak volume of approximately 11,000 vehicles. This intersection, which operates at a LOS of F in both peak periods under all alternatives, will experience an increase of 119 vehicles under Alternative 2. Under several alternatives, this intersection will experience a decrease in overall traffic volumes. Also, the traffic is not expected to move closer to any sensitive land uses in these areas. Effects of the increased traffic will be mitigated by a decrease of duplicate bus service, as well as the use of CNG buses, which generally emit less MSAT than traditional diesel buses. Ambient concentrations of MSATs could be higher at some locations than under the No Build Alternative. Future MSAT emissions could be lower, however, where there are increases in localized speeds and reductions in congestion (which are associated with lower MSAT emissions). In addition, MSAT emissions would be lower in other locations when traffic shifts away from them.

In summary, for all of the detailed study alternatives in the design year, it is expected that there would be reduced MSAT emissions in both the study area and on a regional basis, relative to the No-Build Alternative, as a result of the reduced VMT associated with the use of mass transit and USEPA's MSAT reduction programs. In comparing various project alternatives, MSAT levels could be higher in some locations than others, but current tools and science are not adequate to quantify them. Regardless, on a regional basis, USEPA's vehicle and fuel regulations, coupled with fleet turnover, will over time cause substantial reductions that, in almost all cases, will cause region-wide MSAT levels to be significantly lower than today.

This document has provided a qualitative analysis of MSAT emissions and has acknowledged that the detailed study alternatives could increase exposure to MSAT emissions in certain locations, although the concentrations and duration of exposures are uncertain. However, available technical tools do not enable prediction of the project-specific health impacts of the emission changes associated with the detailed study alternatives. Because of these limitations, the following discussion is included in accordance with the President's Council on Environmental Quality (CEQ) regulations (40 CFR, Section 1502.22[b]) regarding incomplete or unavailable information.

4.2.5 Information that is Unavailable or Incomplete

In FHWA's view, information is incomplete or unavailable to credibly predict the project-specific health impacts due to changes in MSAT emissions associated with a proposed set of highway alternatives (although this project is a proposed subway system, it will affect the traffic patterns of roadways and highways in the project area). The outcome of such an assessment, adverse or not, would be influenced more by the uncertainty introduced into the process through assumption and speculation rather than any genuine insight into the actual health impacts directly attributable to MSAT exposure associated with a proposed action.

The USEPA is responsible for protecting the public health and welfare from any known or anticipated effect of an air pollutant. They are the lead authority for administering the Clean Air Act and its amendments and have specific statutory obligations with respect to hazardous air pollutants and MSAT. The USEPA is in the continual process of assessing human health effects, exposures, and risks posed by air pollutants. They maintain the Integrated Risk Information System (IRIS), which is "a compilation of electronic reports on specific substances found in the environment and their potential to cause human health effects" (USEPA, http://www.epa.gov/ncea/iris/index.html). Each report contains assessments of non-cancerous and cancerous effects for individual compounds and quantitative estimates of risk levels from lifetime oral and inhalation exposures with uncertainty spanning perhaps an order of magnitude.

Other organizations are also active in the research and analyses of the human health effects of MSAT, including the Health Effects Institute (HEI). Two HEI studies are summarized in Appendix D of FHWA's Interim Guidance Update on Mobile Source Air Toxic Analysis in NEPA Documents. Among the adverse health effects linked to MSAT compounds at high exposures are cancer in humans in occupational settings; cancer in animals; and irritation to the respiratory tract, including the exacerbation of asthma. Less obvious is the adverse human health effects of MSAT compounds at current environmental concentrations (HEI, http://pubs.healtheffects.org/view.php?id=282) or in the future as vehicle emissions substantially decrease (HEI, http://pubs.healtheffects.org/view.php?id=306).

4.2.5.1 Emissions

The methodologies for forecasting health impacts include emissions modeling; dispersion modeling; exposure modeling; and then final determination of health impacts, each step in the process building on the model predictions obtained in the previous step. All are encumbered by technical shortcomings or uncertain science that prevents a more complete differentiation of the MSAT health impacts among a set of project alternatives. These difficulties are magnified for lifetime (i.e., 70 year) assessments, particularly because unsupportable assumptions would have to be made regarding changes in travel patterns and vehicle technology (which affects emissions rates) over that time frame, since such information is unavailable. The results produced by the USEPA's MOBILE6.2 model, the California EPA's Emfac2007 model, and the USEPA's DraftMOVES2009 model in forecasting MSAT emissions are highly inconsistent. Indications from the development of the MOVES model are that MOBILE6.2 significantly underestimates diesel particulate matter (PM) emissions and significantly overestimates benzene emissions.

4.2.5.2 Dispersion

Regarding air dispersion modeling, an extensive evaluation of USEPA's guideline CAL3QHC model was conducted in an NCHRP study (http://www.epa.gov/scram001/dispersion_alt.htm#hyroad), which documents poor model performance at ten sites across the country - three where intensive monitoring was conducted plus an additional seven with less intensive monitoring. The study indicates a bias of the CAL3QHC model to overestimate concentrations near highly congested intersections and underestimate concentrations near uncongested intersections. The consequence of this is a tendency to overstate the air quality benefits of mitigating congestion at intersections. Such poor model performance is less difficult to manage for demonstrating compliance with National Ambient Air Quality Standards for relatively short time frames than it is for forecasting individual exposure over an entire lifetime, especially given that some information needed for estimating 70-year lifetime exposure is unavailable. It is particularly difficult to reliably forecast MSAT exposure near roadways, and to determine the portion of time that people are actually exposed at a specific location.

4.2.5.3 Exposure Levels and Health Effects

There are considerable uncertainties associated with the existing estimates of toxicity of the various MSAT, because of factors such as low-dose extrapolation and translation of occupational exposure data to the general population, a concern expressed by Health Effects Institute (HEI) (http://pubs.healtheffects.org/view.php?id=282). As a result, there is no national consensus on air dose-response values assumed to protect the public health and welfare for MSAT compounds, and in particular for diesel PM. The USEPA (http://www.epa.gov/risk/basicinformation.htm#g) and the HEI (http://pubs.healtheffects.org/getfile.php?u=395) have not established a basis for quantitative risk assessment of diesel PM in ambient settings.

There is also the lack of a national consensus on an acceptable level of risk. The current context is the process used by the USEPA as provided by the Clean Air Act to determine whether more stringent controls are required in order to provide an ample margin of safety to protect public health or to prevent an adverse environmental effect for industrial sources subject to the maximum achievable control technology standards, such as benzene emissions from refineries. The decision framework is a two-step process. The first step requires the USEPA to determine a "safe" or "acceptable" level of risk due to emissions from a source, which is generally no greater than approximately 100 in a million. Additional factors are considered in the second step, the goal of which is to maximize the number of people with risks less than 1 in a million due to emissions from a source. The results of this statutory two-step process do not guarantee that cancer risks from exposure to air toxics are less than 1 in a million; in some cases, the residual risk determination could result in maximum individual cancer risks that are as high as approximately 100 in a million. In a June 2008 decision, the U.S. Court of Appeals for the District of Columbia Circuit upheld USEPA's approach to addressing risk in its two-step decision framework. Information is incomplete or unavailable to establish that even the largest of highway projects would result in levels of risk greater than safe or acceptable

Because of the limitations in the methodologies for forecasting health impacts described, any predicted difference in health impacts between alternatives is likely to be much smaller than the uncertainties associated with predicting the impacts. Consequently, the results of such assessments would not be useful to decision makers, who would need to weigh this information against project benefits, such as reducing traffic congestion, accident rates, and fatalities plus improved access for emergency response, that are better suited for quantitative analysis.

4.3 Construction Assessment

An assessment of the air quality construction impacts was conducted. The assessment utilized CARB's Urban Emissions Model (URBEMIS), the Road Construction Emissions Model, Version 6.3.2 (RCEM) developed by the Sacramento Metropolitan Air Quality Management District (SMAQMD), and the SCAQMD OFFROAD 2007 emission factors. The RCEM model estimates emissions of fugitive dust PM_{10} based on a screening emission factor of 20 pounds per day per acre of unpaved activity, and applies an estimated 50% fugitive dust reduction if the user indicates that water trucks will be used for dust control. SCAQMD OFFROAD2007 was used to develop emission factors from off-road construction equipment. Worker and delivery trip emissions factors were estimated using the EMFAC2007 emission factor model. Using these various data sources, daily construction emission levels were developed. These values were compared to the air quality construction significance thresholds shown in Table 4-5 to determine if the project would meet or exceed these values. As the construction schedule is very preliminary at this time, construction emissions were estimated for each major activity.

As shown in Table 4-7, SCAQMD thresholds would be exceeded for NOx for all design elements and PM_{10} would be exceeded for a typical station with mining. Mitigation measures such as watering, the use of soil stabilizers, etc. will be applied to reduce the predicted PM_{10} levels to below the SCAQMD daily construction threshold levels. NOx levels would be elevated due partially to the proposed use of diesel locomotives to extract soil during the tunnel boring process. Mitigation measures could help to reduce these impacts, but it is unlikely, given the current construction plan, that these levels would be below the SCAQMD threshold. Specific mitigation measures include:

- All station exposed excavation and surface soil will be watered a certain amount of times a day/week.
- All station construction and cut and cover construction sites neighborhoods will have streets washed by watering trucks a certain amount of times a day/week.
- All tunnel locomotives will be powered by propane, not diesel.
- All electricity will be secured from the grid; generators will not be used.

Once a detailed construction schedule is developed, a more refined construction analysis will be conducted to determine the air quality impacts of construction.

4.4 Conformity Assessment

The proposed project is not predicted to cause or exacerbate a violation of the applicable ambient air quality standards. An application to the Transportation Conformity Working Group of SCAG is being prepared to determine if the project is one of air quality concern in regard to $PM_{10}/PM_{2.5}$. The project is predicted to reduce regional emission burden levels. The Westside Subway Extension project is included in the Draft Amendment #08-34 to the 2008 RTIP as Project ID #UT101, #1TR1002 and #1TR1003 (refer to page 5 of Draft

Amendment). The Westside Subway Extension is also included in Metro's 2009 LRTP under Candidates for Private Sector Financial Participation – Transit Projects (refer to Figure K on page 25).

4.5 Cumulative Impacts

Cumulative impacts are impacts on the environment that result from the incremental impact of a project when added to other past, present, and reasonably foreseeable future actions regardless of what agency (Federal or non-Federal) or person undertakes such other actions. Cumulative impacts can result from individually minor but collectively significant actions taking place over a period of time. (40 CFR § 1508.7)

CEQA defines cumulative impact as follows:

- Two or more individual effects which, when considered together, are considerable or which compound or increase other environmental impacts, and
- The change in the environment which results from the incremental impact of the project when added to other closely related past, present, or reasonably foreseeable future projects, and can result from individually minor, but collectively significant, projects taking place over a period of time. (*CEQA Air Quality Handbook,* Page 9-11)

CEQA has put forth several possible assumptions to determine whether a project is significant enough to warrant a cumulative impact analysis. These include whether the project reduces the rate of growth in VMT, reduces emissions by a certain amount each year, or increases average vehicle ridership (CEQA Air Quality Handbook, Page 9-12). This approach is not mandatory under CEQA, but is a possible way to determine whether a project is significant.

This project is predicted to reduce regional VMT and regional emission burden levels. It is included in the Draft Amendment #08-34 to the 2008 RTIP as Project ID #UT101, #1TR1002 and #1TR1003 (refer to page 5 of Draft Amendment). The Westside Subway Extension is also included in Metro's 2009 LRTP under Candidates for Private Sector Financial Participation – Transit Projects (refer to Figure K on page 25). The plan includes a transportation conformity determination for the entire region, as it accounts for future emissions from all mobile sources and ensures that attainment will not be delayed by future projects.

Constructing the Build alternatives, including stations, support facilities, subway tunnels and infrastructure, would result in emissions from construction equipment and dust from excavations. Except for nitrous oxides (NOx), construction emissions of criteria pollutants would be below SCAQMD thresholds. The Build Alternatives would contribute to a cumulative effect of NOx emissions during construction. Although with the implementation of mitigation measures emissions of PM_{10} and $PM_{2.5}$ for the Build Alternatives would be below SCAQMD thresholds, the Study Area is in a nonattainment area for these pollutants. The Build Alternatives would contribute to cumulative effects in regards to PM_{10} and $PM_{2.5}$. When combined with construction-related emissions generated by other transit and transportation projects, the cumulative air quality impact for NOx and particulate matter would be significant, though temporary.

Table 4-6. SCAQMD Air Quality Significance Thresholds

Mass Daily Thresholds[1]		
Pollutant	**Construction[2]**	**Operation[3]**
Nitrogen Oxides (NO_x)	100 lbs/day	55 lbs/day
Volatile Organic Compounds (VOC)	75 lbs/day	55 lbs/day
Respirable Particulate Matter (PM_{10})	150 lbs/day	150 lbs/day
Fine Particulate Matter ($PM_{2.5}$)	55 lbs/day	55 lbs/day
Sulfur Oxides (SO_x)	150 lbs/day	150 lbs/day
Carbon Monoxide (CO)	550 lbs/day	550 lbs/day
Lead (Pb)	3 lbs/day	3 lbs/day
Carbon Dioxide equivalents (CO_2[5])	Being developed at this time	Being developed at this time
Toxic Air Contaminants (TACs) and Odor Thresholds		
TACs (including carcinogens and non-carcinogens)	Maximum Incremental Cancer Risk ≥ 10 in 1 million Cancer Burden > 0.5 excess cancer cases (in areas ≥ 1 in 1 million) Hazard Index ≥ 1.0 (project increment)	
Odor	Project creates an odor nuisance pursuant to SCAQMD Rule 402	
Ambient Air Quality for Criteria Pollutants[4]		
NO2 1-hour average annual average	SCAQMD is in attainment; project is significant if it causes or contributes to an exceedance of the following attainment standards: 0.18 ppm (state) 0.03 ppm (state)	
PM10 24-hour average annual average	10.4 µg/m3 (construction)[5] & 2.5 µg/m3 (operation) 1.0 µg/m3	
PM2.5 24-hour average	10.4 µg/m3 (construction)[5] & 2.5 µg/m3 (operation)	
Sulfate 24-hour average	1 µg/m3	
CO 1-hour average 8-hour average	SCAQMD is in attainment; project is significant if it causes or contributes to an exceedance of the following attainment standards: 20 ppm (state) 9.0 ppm (state/federal)	

[1] *Source: SCAQMD CEQA Handbook (SCAQMD, Rev. March 2009).*

[2] Construction thresholds apply to both the South Coast Air Basin and Coachella Valley (Salton Sea and Mojave Desert Air Basins).

[3] For Coachella Valley, the mass daily thresholds for operation are the same as the construction thresholds.

[4] Ambient air quality thresholds for criteria pollutants based on SCAQMD Rule 1303, Table A-2 unless otherwise stated.

[5] Ambient air quality threshold based on SCAQMD Rule 403.

KEY: lbs/day = pounds per day
ppm = parts per million
µg/m3 = microgram per cubic meter
≥ = greater than or equal to

Table 4-7. Estimated Construction Impacts for Project Design Elements (lbs/day)

Activity	VOC	CO	NOx	PM_{10}	$PM_{2.5}$
Typical Station with Mining					
Construction Equipment	69	300	1053	38	37
Dust Generated from Dirt Handling (Excavation, Backfilling, etc.)				231	
Mobile Sources (Deliveries, worker trips, hauling of material, etc.)	3	24	42	2	2
Total	72	324	1095	272	39
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**
Typical Station with No Mining					
Construction Equipment	16	64	108	5	5
Dust Generated from Dirt Handling (Excavation, Backfilling, etc.)				120	
Mobile Sources (Deliveries, worker trips, hauling of material, etc.)	3	19	33	1	1
Total	19	83	141	126	6
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**
Maintenance Facility					
Construction Equipment	27	102	228	8	8
Dust Generated from Dirt Handling (Excavation, Backfilling, etc.)				TBD	
Mobile Sources (Deliveries, worker trips, hauling of material, etc.)	3	19	33	1	1
Total	30	121	261	9	9
SCAQMD Thresholds	**75**	**550**	**100**	**150**	**55**

5.0 REFERENCES

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SCAQMD 1993	South Coast Air Quality Management District, *CEQA Air Quality Handbook*. April 1993.

SMAQMD 2009	Sacramento Metropolitan Air Quality Management District, 2009, *Roadway Construction Emission Model, Version 6.3.2,* http://www.airquality.org/ceqa/RoadConstructionModelVer6.3-2.xls
UC Davis 1997	University of California, Davis, *Transportation Project-Level Carbon Monoxide Protocol.* December 1997.

Appendix A

Monitored Data

AirData - Monitor Values Report - Criteria Air Pollutants
Generated on Thursday, March 11, 2010

AirData

You are here: EPA Home Air & Radiation AirData Reports and Maps Select Geography Select Report/Map Monitor Values Report Criteria Monitor Values Report

EPA is assessing its data systems, including AirData reports and maps. Data updates are suspended while the assessment is underway. The last update included data through January 10, 2009; see database status for details. For more recent air quality data, visit the AirExplorer and Air Emission Sources sites.

Monitor Values Report - Criteria Air Pollutants

Geographic Area: California
Pollutant: Carbon Monoxide
Year: 2006, 2007, 2008

EPA Air Quality Standards:
Carbon Monoxide: 35 ppm (1-hour average), 9 ppm (8-hour average)

ppm = parts per million

220 Rows
See Disclaimer

	CO (ppm)													
	1-Hour Values				8-Hour Values			Monitor Number						
Row #	# Obs	1st Max	2nd Max	# Exceed	1st Max	2nd Max	# Exceed		Year	Site ID	Site Address	City	County	Sta
SORT	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲
26	8,210	2.7	2.6	0	1.9	1.8	0	1	2006	060711004	1350 San Bernardino Rd., Upland	Upland	San Bernardino Co	CA
27	8,309	2.4	2.2	0	1.7	1.6	0	1	2007	060711004	1350 San Bernardino Rd., Upland	Upland	San Bernardino Co	CA
28	5,491	2.1	1.9	0	1.4	1.2	0	1	2008	060711004	1350 San Bernardino Rd., Upland	Upland	San Bernardino Co	CA
29	8,225	2.2	2.2	0	1.6	1.5	0	1	2006	060710306	14306 Park Ave., Victorville, Ca	Victorville	San Bernardino Co	CA
30	8,348	2.1	2.0	0	1.6	1.5	0	1	2007	060710306	14306 Park Ave., Victorville, Ca	Victorville	San Bernardino Co	CA
31	5,587	1.4	1.4	0	0.9	0.9	0	1	2008	060710306	14306 Park Ave., Victorville, Ca	Victorville	San Bernardino Co	CA
32	1,388	1.3	1.1	0	0.8	0.8	0	1	2008	060712002	14360 Arrow Blvd., Fontana	Fontana	San Bernardino Co	CA

33	7,805	14.3	3.1	0	2.7	1.7	0	1	2006	060251003	150 9th St., El Centro	El Centro	Imperial Co	CA
34	8,360	2.5	2.4	0	1.7	1.6	0	1	2007	060251003	150 9th St., El Centro	El Centro	Imperial Co	CA
35	6,270	2.5	2.3	0	1.7	1.7	0	1	2008	060251003	150 9th St., El Centro	El Centro	Imperial Co	CA
36	7,724	4.1	3.8	0	2.9	2.6	0	1	2006	060850005	158b Jackson St, San Jose, Ca	San Jose	Santa Clara Co	CA
37	8,311	3.5	3.5	0	2.7	2.4	0	1	2007	060850005	158b Jackson St, San Jose, Ca	San Jose	Santa Clara Co	CA
38	6,177	3.3	3.0	0	2.1	1.9	0	1	2008	060850005	158b Jackson St, San Jose, Ca	San Jose	Santa Clara Co	CA
39	8,265	3.5	3.3	0	2.7	2.5	0	1	2006	060371103	1630 N Main St, Los Angeles	Los Angeles	Los Angeles Co	CA
40	8,148	3.2	3.1	0	2.2	2.1	0	1	2007	060371103	1630 N Main St, Los Angeles	Los Angeles	Los Angeles Co	CA
41	5,560	2.9	2.8	0	2.0	1.9	0	1	2008	060371103	1630 N Main St, Los Angeles	Los Angeles	Los Angeles Co	CA
42	8,342	4.5	4.3	0	2.9	2.9	0	1	2006	060590007	1630 W. Pampas Lane	Anaheim	Orange Co	CA
43	7,681	3.6	3.6	0	2.9	2.3	0	1	2007	060590007	1630 W. Pampas Lane	Anaheim	Orange Co	CA
44	5,560	3.3	3.0	0	2.4	2.1	0	1	2008	060590007	1630 W. Pampas Lane	Anaheim	Orange Co	CA
45	8,375	4.8	4.7	0	3.5	3.4	0	1	2006	060371201	18330 Gault St., Reseda	Reseda	Los Angeles Co	CA
46	7,954	3.7	3.5	0	2.8	2.7	0	1	2007	060371201	18330 Gault St., Reseda	Reseda	Los Angeles Co	CA
47	5,594	3.4	3.3	0	2.3	2.1	0	1	2008	060371201	18330 Gault St., Reseda	Reseda	Los Angeles Co	CA
48	8,291	2.5	2.3	0	1.4	1.3	0	1	2006	060131004	1865 D Rumrill Blvd, San Pablo, Ca	San Pablo	Contra Costa Co	CA
49	8,313	2.4	2.2	0	1.2	1.2	0	1	2007	060131004	1865 D Rumrill Blvd, San Pablo, Ca	San Pablo	Contra Costa Co	CA
50	6,225	2.5	2.1	0	1.3	0.9	0	1	2008	060131004	1865 D Rumrill Blvd, San	San Pablo	Contra Costa Co	CA

											Pablo, Ca			
Grand Total				0			0		2007					
				0			1		2006					
				0			0		2008					

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EPA is assessing its data systems, including AirData reports and maps. Data updates are suspended while the assessment is underway. The last update included data through January 10, 2009; see database status for details. For more recent air quality data, visit the AirExplorer and Air Emission Sources sites.

Monitor Values Report - Criteria Air Pollutants

Geographic Area: California
Pollutant: Carbon Monoxide
Year: 2006, 2007, 2008

EPA Air Quality Standards:
Carbon Monoxide: 35 ppm (1-hour average), 9 ppm (8-hour average)

ppm = parts per million

220 Rows

See Disclaimer

	CO (ppm)													
	1-Hour Values				8-Hour Values			Monitor Number						
Row #	**# Obs**	**1st Max**	**2nd Max**	**# Exceed**	**1st Max**	**2nd Max**	**# Exceed**		**Year**	**Site ID**	**Site Address**	**City**	**County**	**St**
SORT	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲
201	8,351	1.5	1.5	0	0.8	0.7	0	1	2007	060655001	Fs-590 Racquet Club Ave, Palm Springs	Palm Springs	Riverside Co	C
202	5,574	1.0	0.9	0	0.5	0.5	0	1	2008	060655001	Fs-590 Racquet Club Ave, Palm Springs	Palm Springs	Riverside Co	C
203	8,321	4.4	4.3	0	2.3	2.2	0	1	2006	060771002	Hazelton-Hd, Stockton	Stockton	San Joaquin Co	C
204	8,216	3.6	3.6	0	2.3	2.1	0	1	2007	060771002	Hazelton-Hd, Stockton	Stockton	San Joaquin Co	C
205	5,546	2.6	2.5	0	1.6	1.6	0	1	2008	060771002	Hazelton-Hd, Stockton	Stockton	San Joaquin Co	C
206	8,258	1.8	1.7	0	1.7	1.7	0	1	2006	060831025	Lfc #1-Las Flores Canyon	Capitan	Santa Barbara Co	C
207	8,151	1.4	1.3	0	1.1	0.9	0	1	2007	060831025	Lfc #1-Las Flores Canyon	Capitan	Santa Barbara Co	C
208	6,182	3.5	2.5	0	1.7	0.9	0	1	2008	060831025	Lfc #1-Las Flores	Capitan	Santa Barbara	C

											Canyon		Co	
209	8,290	3.8	3.3	0	2.1	1.9	0	1	2006	060190242	Sierra Skypark#2-Blythe & Chnnlt, Fresno	Fresno	Fresno Co	C
210	8,152	2.6	2.6	0	1.4	1.2	0	1	2007	060190242	Sierra Skypark#2-Blythe & Chnnlt, Fresno	Fresno	Fresno Co	C
211	5,519	1.6	1.5	0	1.0	1.0	0	1	2008	060190242	Sierra Skypark#2-Blythe & Chnnlt, Fresno	Fresno	Fresno Co	C
212	8,229	0.3	0.3	0	0.3	0.3	0	1	2006	060834003	Sts Power Plant, Vandenberg Afb	Vandenberg Air Force Base	Santa Barbara Co	C
213	8,161	1.2	1.2	0	0.9	0.8	0	1	2007	060834003	Sts Power Plant, Vandenberg Afb	Vandenberg Air Force Base	Santa Barbara Co	C
214	6,097	1.6	1.3	0	0.7	0.6	0	1	2008	060834003	Sts Power Plant, Vandenberg Afb	Vandenberg Air Force Base	Santa Barbara Co	C
215	4,597	2.2	0.5	0	0.6	0.3	0	1	2006	060430003	Turtleback Dome, Yosemite Natl' Pk 95389	Yosemite National Park	Mariposa Co	C
216	6,396	1.2	0.9	0	0.6	0.5	0	1	2007	060430003	Turtleback Dome, Yosemite Natl' Pk 95389	Yosemite National Park	Mariposa Co	C
217	2,746	0.9	0.9	0	0.5	0.5	0	1	2006	061130004	Uc Davis-Campus, Davis	Davis	Yolo Co	C
218	8,365	2.9	2.8	0	2.0	1.9	0	1	2006	060370113	Va Hospital, West Los Angeles	West Los Angeles	Los Angeles Co	C
219	8,267	2.7	2.5	0	2.0	1.6	0	1	2007	060370113	Va Hospital, West Los Angeles	West Los Angeles	Los Angeles Co	C
220	5,552	2.7	2.3	0	1.8	1.7	0	1	2008	060370113	Va Hospital, West Los Angeles	West Los Angeles	Los Angeles Co	C
Grand Total				0			0		2007					
				0			1		2006					
				0			0		2008					

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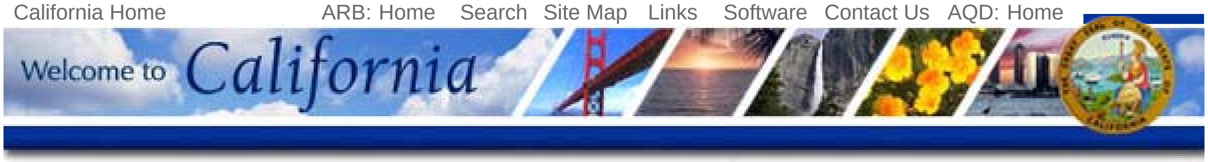

Air Resources Board

iADAM

Highest 4 Daily Maximum 8-Hour Ozone Averages

Los Angeles-North Main Street

FAQs

Year:	2006		2007		2008	
	Date	8-Hr Average	Date	8-Hr Average	Date	8-Hr Average
National:						
First High:	Jul 15	0.079	Sep 2	0.102	May 18	0.090
Second High:	Jul 22	0.077	Sep 3	0.093	Jun 21	0.081
Third High:	Sep 3	0.076	Aug 19	0.078	May 17	0.076
Fourth High:	Jun 3	0.075	May 19	0.072	Jun 15	0.073
California:						
First High:	Jul 15	0.079	Sep 2	0.103	May 18	0.090
Second High:	Jul 22	0.077	Sep 3	0.094	Jun 21	0.081
Third High:	Sep 3	0.077	Aug 19	0.079	May 17	0.076
Fourth High:	Jun 3	0.076	May 19	0.073	Jun 15	0.074
National:						
# Days Above '08 Nat'l Std.:		3		3		3
'08 Nat'l Std. Design Value:		0.074		0.072		0.073
National Year Coverage:		97		96		95
California:						
# Days Above State Standard:		7		6		6
California Designation Value:		0.085		0.085		0.081
Expected Peak Day Conc.:		0.087		0.085		0.085
California Year Coverage:		97		96		94

Go Backward One Year New Top 4 Summary Go Forward One Year

Notes: All averages are expressed in parts per million.
National exceedances are shown in **orange** . State exceedances are shown in **yellow** .
An exceedance is not necessarily a violation.
Year Coverage indicates the extent to which available monitoring data represent the time of the year when concentrations are expected to be highest. 0 means that data represent none of the high period; 100 means that data represent the entire high period. A high Year Coverage does not mean that there was sufficient data for annual statistics to be considered valid.
* There was insufficient (or no) data available to determine the value.

Switch: Hourly Ozone | PM2.5 | PM10 | Carbon Monoxide | Nitrogen Dioxide | Sulfur Dioxide | Hydrogen Sulfide

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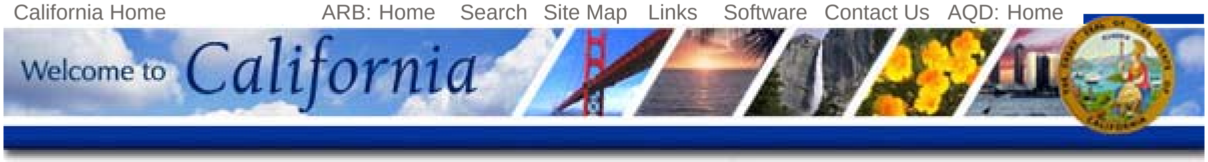

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Highest 4 Daily Maximum 8-Hour Ozone Averages

West Los Angeles-VA Hospital

FAQs

Year:	2006		2007		2008	
	Date	8-Hr Average	Date	8-Hr Average	Date	8-Hr Average
National:						
First High:	May 14	0.074	Sep 2	0.087	May 18	0.096
Second High:	Sep 18	0.074	Sep 3	0.083	Apr 28	0.082
Third High:	Jun 3	0.069	Aug 19	0.069	Apr 27	0.075
Fourth High:	Aug 23	0.068	May 19	0.067	Jun 21	0.073
California:						
First High:	May 14	0.074	Sep 2	0.088	May 18	0.097
Second High:	Sep 18	0.074	Sep 3	0.084	Apr 28	0.082
Third High:	Jun 3	0.069	Aug 19	0.070	Apr 27	0.075
Fourth High:	Aug 23	0.068	May 19	0.068	Jun 21	0.074
National:						
# Days Above '08 Nat'l Std.:		0		2		2
'08 Nat'l Std. Design Value:		0.073		0.070		0.069
National Year Coverage:		98		98		96
California:						
# Days Above State Standard:		2		2		8
California Designation Value:		0.084		0.077		0.075
Expected Peak Day Conc.:		0.084		0.081		0.079
California Year Coverage:		98		97		96

Go Backward One Year | New Top 4 Summary | Go Forward One Year

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Switch: Hourly Ozone | PM2.5 | PM10 | Carbon Monoxide | Nitrogen Dioxide | Sulfur Dioxide | Hydrogen Sulfide

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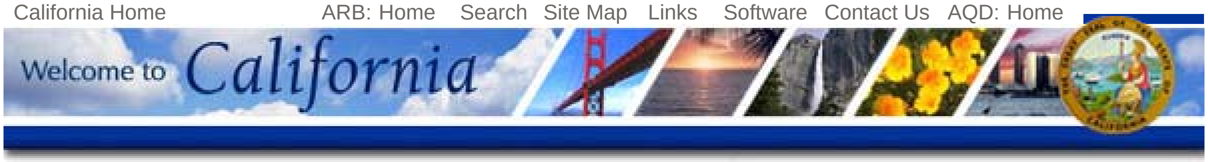

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Highest 4 Daily Maximum 8-Hour Carbon Monoxide Averages

Los Angeles-North Main Street

FAQs

Year:	2006		2007		2008	
	Date	8-Hr Average	Date	8-Hr Average	Date	8-Hr Average
National:						
First High:	Jan 13	2.68	Dec 5	2.15	Jan 11	1.96
Second High:	Feb 9	2.45	Nov 20	2.13	Feb 9	1.93
Third High:	Jan 12	2.35	Jan 16	2.04	Nov 14	1.91
Fourth High:	Dec 6	2.26	Jan 8	2.00	Jan 12	1.88
California:						
First High:	Jan 12	2.68	Dec 4	2.15	Jan 11	1.96
Second High:	Feb 8	2.45	Nov 20	2.13	Feb 8	1.93
Third High:	Jan 11	2.35	Jan 16	2.04	Nov 13	1.91
Fourth High:	Dec 5	2.26	Jan 8	2.00	Jan 12	1.79
# Days Above Nat'l Standard:		0		0		0
# Days Above State Standard:		0		0		0
Year Coverage:		95		95		97

Go Backward One Year | New Top 4 Summary | Go Forward One Year

Notes: All averages are expressed in parts per million.

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Switch: Hourly Ozone | 8-Hour Ozone | PM2.5 | PM10 | Nitrogen Dioxide | Sulfur Dioxide | Hydrogen Sulfide

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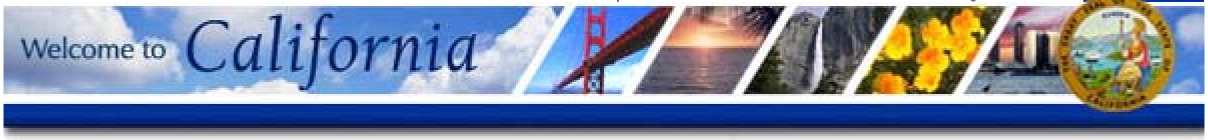

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Highest 4 Daily Maximum 8-Hour Carbon Monoxide Averages

West Los Angeles-VA Hospital

FAQs

Year:	2006		2007		2008	
	Date	8-Hr Average	Date	8-Hr Average	Date	8-Hr Average
National:						
First High:	Dec 7	2.00	Dec 5	1.96	Jan 11	1.76
Second High:	Jan 13	1.93	Oct 26	1.63	Jan 12	1.74
Third High:	Dec 15	1.90	Dec 5	1.61	Nov 14	1.58
Fourth High:	Jan 12	1.83	Nov 15	1.55	Feb 9	1.56
California:						
First High:	Dec 7	2.00	Dec 5	1.96	Jan 11	1.76
Second High:	Jan 13	1.93	Oct 26	1.63	Jan 12	1.74
Third High:	Dec 15	1.90	Nov 14	1.55	Nov 13	1.58
Fourth High:	Jan 12	1.83	Mar 11	1.54	Feb 8	1.56
# Days Above Nat'l Standard:		0		0		0
# Days Above State Standard:		0		0		0
Year Coverage:		99		94		96

Go Backward One Year | New Top 4 Summary | Go Forward One Year

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Switch: Hourly Ozone | 8-Hour Ozone | PM2.5 | PM10 | Nitrogen Dioxide | Sulfur Dioxide | Hydrogen Sulfide

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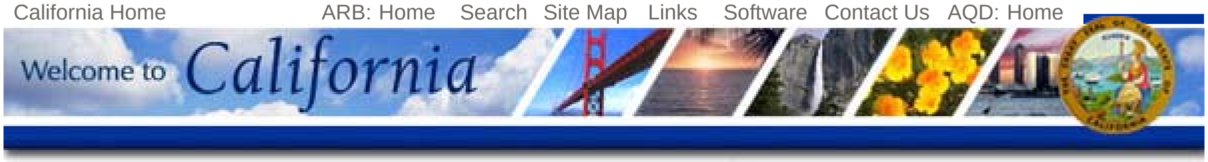

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Highest 4 Daily Maximum Hourly Ozone Measurements

Los Angeles-North Main Street

FAQs

Year:	2006		2007		2008	
	Date	Measurement	Date	Measurement	Date	Measurement
First High:	Jul 22	0.108	Sep 3	0.115	May 18	0.109
Second High:	Jul 23	0.108	Sep 2	0.111	Jun 21	0.103
Third High:	Jun 3	0.103	Sep 1	0.099	May 17	0.095
Fourth High:	Jul 24	0.100	Aug 19	0.093	Jun 22	0.090
# Days Above State Standard:		8		3		3
California Designation Value:		0.11		0.11		0.11
Expected Peak Day Conc.:		0.111		0.108		0.107
# Days Above Nat'l Standard:		*0*		*0*		*0*
National Design Value:		*0.108*		*0.111*		*0.108*
Year Coverage:		98		97		96

Go Backward One Year New Top 4 Summary Go Forward One Year

Notes: All concentrations are expressed in parts per million.

The national 1-hour ozone standard was revoked in June 2005 and is no longer in effect. Statistics related to the revoked standard are shown in *italics* or *italics* .

State exceedances are shown in **yellow** . Exceedances of the revoked national 1-hour standard are shown in *orange* .

An exceedance is not necessarily a violation.

Year Coverage indicates the extent to which available monitoring data represent the time of the year when concentrations are expected to be highest. 0 means that data represent none of the high period; 100 means that data represent the entire high period. A high Year Coverage does not mean that there was sufficient data for annual statistics to be considered valid.

* There was insufficient (or no) data available to determine the value.

Switch: 8-Hour Ozone | PM2.5 | PM10 | Carbon Monoxide | Nitrogen Dioxide | Sulfur Dioxide | Hydrogen Sulfide

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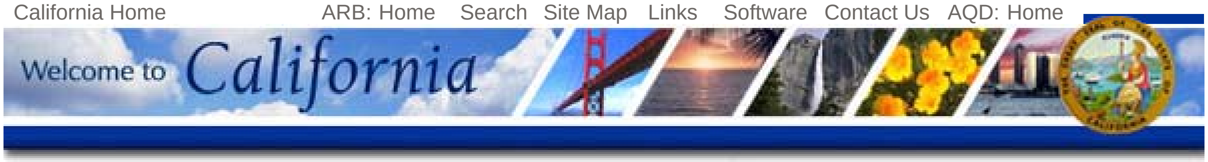

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Highest 4 Daily Maximum Hourly Ozone Measurements

West Los Angeles-VA Hospital

FAQs

Year:	2006		2007		2008	
	Date	Measurement	Date	Measurement	Date	Measurement
First High:	Jul 15	0.099	Sep 3	0.117	May 18	0.111
Second High:	Jun 3	0.098	Sep 2	0.105	Apr 28	0.101
Third High:	Sep 5	0.097	Aug 19	0.090	Oct 27	0.098
Fourth High:	Aug 23	0.093	Jul 26	0.085	Oct 1	0.093
# Days Above State Standard:		3		2		3
California Designation Value:		0.11		0.10		0.10
Expected Peak Day Conc.:		0.107		0.103		0.100
# Days Above Nat'l Standard:		*0*		*0*		*0*
National Design Value:		*0.107*		*0.109*		*0.101*
Year Coverage:		98		98		96

Go Backward One Year New Top 4 Summary Go Forward One Year

Notes: All concentrations are expressed in parts per million.

The national 1-hour ozone standard was revoked in June 2005 and is no longer in effect. Statistics related to the revoked standard are shown in *italics* or *italics* .

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Switch: 8-Hour Ozone | PM2.5 | PM10 | Carbon Monoxide | Nitrogen Dioxide | Sulfur Dioxide | Hydrogen Sulfide

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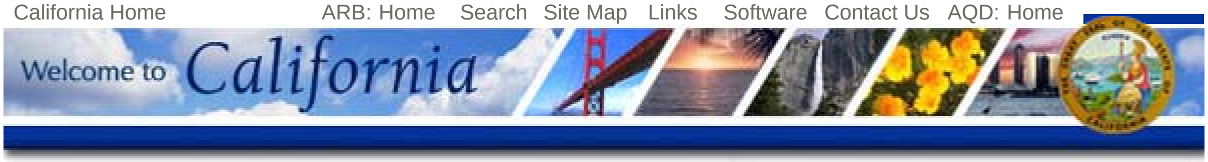

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Highest 4 Daily Maximum Hourly Nitrogen Dioxide Measurements

Los Angeles-North Main Street

FAQs

Year:	2006		2007		2008	
	Date	Measurement	Date	Measurement	Date	Measurement
First High:	Nov 17	0.111	Oct 26	0.104	Dec 1	0.122
Second High:	Feb 3	0.096	Feb 6	0.095	Nov 19	0.110
Third High:	Sep 28	0.096	Sep 12	0.094	Oct 27	0.099
Fourth High:	Jun 28	0.092	Aug 20	0.092	Nov 13	0.098
# Days Above State Standard:		0		0		0
Annual Average:		0.029		0.030		0.027
Year Coverage:		97		96		95

Go Backward One Year | New Top 4 Summary | Go Forward One Year

Notes: All averages are expressed in parts per million.

National exceedances are shown in **orange** . State exceedances are shown in **yellow** .

An exceedance is not necessarily a violation.

Year Coverage indicates the extent to which available monitoring data represent the time of the year when concentrations are expected to be highest. 0 means that data represent none of the high period; 100 means that data represent the entire high period. A high Year Coverage does not mean that there was sufficient data for annual statistics to be considered valid.

* There was insufficient (or no) data available to determine the value.

Switch: Hourly Ozone | 8-Hour Ozone | PM2.5 | PM10 | Carbon Monoxide | Sulfur Dioxide | Hydrogen Sulfide

Go to: Data Statistics Home Page | Top 4 Summaries Start Page

Highest 4 Daily Maximum Hourly Nitrogen Dioxide Measurements

West Los Angeles-VA Hospital

FAQs

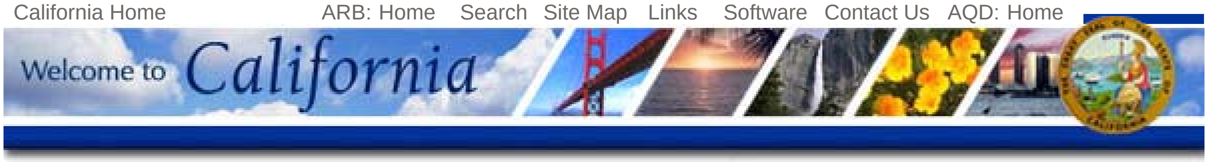
Year:	2006		2007		2008	
	Date	Measurement	Date	Measurement	Date	Measurement
First High:	Dec 7	0.078	Mar 12	0.082	Nov 14	0.090
Second High:	Oct 20	0.071	Jan 24	0.067	Oct 29	0.088
Third High:	Jan 13	0.068	Oct 26	0.067	Nov 13	0.088
Fourth High:	Nov 8	0.065	Feb 7	0.066	Oct 8	0.081
# Days Above State Standard:		0		0		0
Annual Average:		0.017		0.019		0.018
Year Coverage:		94		93		96

Go Backward One Year | New Top 4 Summary | Go Forward One Year

Notes: All averages are expressed in parts per million.
National exceedances are shown in **orange** . State exceedances are shown in **yellow** .
An exceedance is not necessarily a violation.
Year Coverage indicates the extent to which available monitoring data represent the time of the year when concentrations are expected to be highest. 0 means that data represent none of the high period; 100 means that data represent the entire high period. A high Year Coverage does not mean that there was sufficient data for annual statistics to be considered valid.
* There was insufficient (or no) data available to determine the value.

Switch: Hourly Ozone | 8-Hour Ozone | PM2.5 | PM10 | Carbon Monoxide | Sulfur Dioxide | Hydrogen Sulfide

Go to: Data Statistics Home Page | Top 4 Summaries Start Page



Air Resources Board

iADAM

Highest 4 Daily 24-Hour PM10 Averages

Los Angeles-North Main Street

FAQs

Year:	2006		2007		2008	
	Date	24-Hr Average	Date	24-Hr Average	Date	24-Hr Average
National:						
First High:	Feb 4	59.0	Apr 12	78.0	Nov 20	66.0
Second High:	May 11	55.0	Nov 20	77.0	Dec 2	65.0
Third High:	May 17	55.0	Oct 21	63.0	Oct 21	50.0
Fourth High:	Feb 10	48.0	Oct 27	58.0	Oct 27	49.0
California:						
First High:	Feb 4	58.0	Apr 12	77.0	Nov 20	64.0
Second High:	May 11	55.0	Nov 20	76.0	Dec 2	63.0
Third High:	May 17	54.0	Oct 21	62.0	Oct 21	49.0
Fourth High:	Feb 10	48.0	Oct 27	57.0	Nov 14	48.0
Measured:						
# Days Above Nat'l Standard:		0		0		0
# Days Above State Standard:		3		5		2
Estimated:						
3-Yr Avg # Days Above Nat'l Std:		0.0		0.0		*
# Days Above Nat'l Standard:		0.0		0.0		*
# Days Above State Standard:		18.1		31.0		*
State 3-Yr Maximum Average:		32		33		33
State Annual Average:		30.1		33.0		*
National 3-Year Average:		*31*		*31*		*29*
National Annual Average:		*30.1*		*33.3*		*24.0*
Year Coverage:		95		93		79

Go Backward One Year | New Top 4 Summary | Go Forward One Year

Notes: All concentrations are expressed in micrograms per cubic meter.

The national annual average PM10 standard was revoked in December 2006 and is no longer in effect. Statistics related to the revoked standard are shown in *italics* or *italics* .

National exceedances are shown in **orange** . State exceedances are shown in **yellow** .

An exceedance is not necessarily a violation.

Statistics may include data that are related to an exceptional event.

State and national statistics may differ for the following reasons:

State statistics are based on California approved samplers, whereas national statistics are based on samplers using federal reference or equivalent methods.

State and national statistics may therefore be based on different samplers.

State statistics for 1998 and later are based on *local* conditions (except for sites in the South Coast Air Basin, where State statistics for 2002 and later are based on *local* conditions).

National statistics are based on *standard* conditions.

State criteria for ensuring that data are sufficiently complete for calculating valid annual averages are more stringent than the national criteria.

Measurements are usually collected every six days. Measured days counts the days that a measurement was greater than the level of the standard; Estimated days mathematically estimates how many days concentrations would have been greater than the level of the standard had each day been monitored.

3-Year statistics represent the listed year and the 2 years before the listed year.

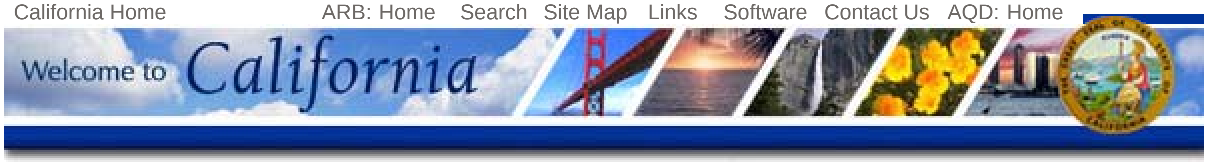
Year Coverage indicates the extent to which available monitoring data represent the time of the year when concentrations are expected to be highest. 0 means that data represent none of the high period; 100 means that data represent the entire high period. A high Year Coverage does not mean that there was sufficient data for annual statistics to be considered valid.

* There was insufficient (or no) data available to determine the value.

Switch: Hourly Ozone | 8-Hour Ozone | PM2.5 | Carbon Monoxide | Nitrogen Dioxide | Sulfur Dioxide | Hydrogen Sulfide

Go to: Data Statistics Home Page | Top 4 Summaries Start Page

California Home ARB: Home Search Site Map Links Software Contact Us AQD: Home



Air Resources Board

iADAM

Highest 4 Daily 24-Hour PM2.5 Averages

Los Angeles-North Main Street

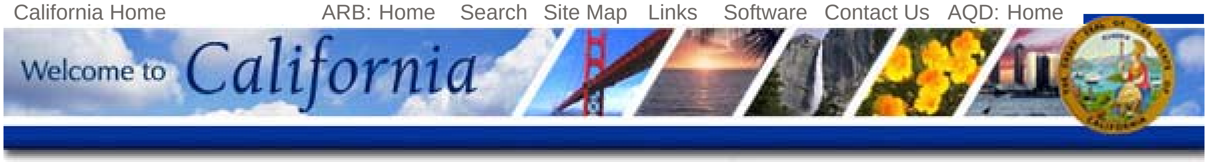
FAQs

Year:	2006		2007		2008	
	Date	24-Hr Average	Date	24-Hr Average	Date	24-Hr Average
National:						
First High:	Feb 4	56.2	Nov 18	64.1	Nov 16	78.3
Second High:	Nov 24	45.7	Nov 20	61.1	Dec 3	59.9
Third High:	Feb 11	43.2	Nov 19	60.4	Dec 2	54.5
Fourth High:	Oct 25	42.0	Nov 21	56.7	Nov 23	50.0
California:						
First High:	Feb 4	56.2	Nov 18	64.1	Nov 16	78.3
Second High:	Nov 24	45.7	Nov 20	62.0	Dec 3	59.9
Third High:	Feb 11	43.2	Nov 19	60.4	Jul 4	54.6
Fourth High:	Oct 25	42.0	Nov 21	56.7	Dec 2	54.5
Estimated Days > Nat'l 24-Hr Std:		11.7		*		11.3
Measured Days > Nat'l 24-Hr Std:		11		20		10
Nat'l 24-Hr Std Design Value:		49		48		43
Nat'l 24-Hr Std 98th Percentile:		38.9		51.2		40.3
National Annual Std Design Value:		17.7		16.7		16.1
National Annual Average:		15.5		16.7		15.9
State Ann'l Std Designation Value:		18		18		16
State Annual Average:		16.0		*		16.2
Year Coverage:		90		86		88

Go Backward One Year New Top 4 Summary Go Forward One Year

Notes: All concentrations are expressed in micrograms per cubic meter.
National exceedances are shown in **orange** . State exceedances are shown in **yellow** .
An exceedance is not necessarily a violation.
State and national statistics may differ for the following reasons:
State statistics are based on California approved samplers, whereas national statistics are based on samplers using federal reference or equivalent methods.
State and national statistics may therefore be based on different samplers.
State criteria for ensuring that data are sufficiently complete for calculating valid annual averages are more stringent than the national criteria.
Year Coverage indicates the extent to which available monitoring data represent the time of the year when concentrations are expected to be highest. 0 means that data represent none of the high period; 100 means that data represent the entire high period. A high Year Coverage does not mean that there was sufficient data for annual statistics to be considered valid.
* There was insufficient (or no) data available to determine the value.

Switch: Hourly Ozone | 8-Hour Ozone | PM10 | Carbon Monoxide | Nitrogen Dioxide | Sulfur Dioxide | Hydrogen Sulfide
Go to: Data Statistics Home Page | Top 4 Summaries Start Page



Air Resources Board

iADAM

Highest 4 Daily Maximum State 24-Hour Sulfur Dioxide Averages

Los Angeles-North Main Street

FAQs

Year:	2006		2007		2008	
	Date	24-Hr Average	Date	24-Hr Average	Date	24-Hr Average
First High:	Nov 8	0.006	Feb 6	0.005	Sep 29	0.003
Second High:	Jul 4	0.006	Jan 26	0.004	Oct 8	0.003
Third High:	Jul 5	0.006	Jan 24	0.004	Oct 2	0.002
Fourth High:	Jul 2	0.005	Jan 19	0.004	Jul 5	0.002
Annual Average:		0.001		0.000		0.000
Year Coverage:		99		90		96

Go Backward One Year New Top 4 Summary Go Forward One Year

Notes: All averages are expressed in parts per million.
State exceedances are shown in **yellow** .
An exceedance is not necessarily a violation.
Year Coverage indicates the extent to which available monitoring data represent the time of the year when concentrations are expected to be highest. 0 means that data represent none of the high period; 100 means that data represent the entire high period. A high Year Coverage does not mean that there was sufficient data for annual statistics to be considered valid.
* There was insufficient (or no) data available to determine the value.

Switch: Hourly Ozone | 8-Hour Ozone | PM2.5 | PM10 | Carbon Monoxide | Nitrogen Dioxide | Hydrogen Sulfide

Go to: Data Statistics Home Page | Top 4 Summaries Start Page

AirData - Monitor Values Report - Criteria Air Pollutants
Generated on Thursday, March 11, 2010

AirData

You are here: EPA Home Air & Radiation AirData Reports and Maps Select Geography Select Report/Map Monitor Values Report Criteria Monitor Values Report

EPA is assessing its data systems, including AirData reports and maps. Data updates are suspended while the assessment is underway. The last update included data through January 10, 2009; see database status for details. For more recent air quality data, visit the AirExplorer and Air Emission Sources sites.

Monitor Values Report - Criteria Air Pollutants

Geographic Area: California
Pollutant: Sulfur Dioxide
Year: 2006, 2007, 2008

EPA Air Quality Standards:
Sulfur Dioxide: 0.5 ppm (3-hour average), 0.14 ppm (24-hour average), 0.030 ppm (annual mean)

ppm = parts per million

107 Rows
See Disclaimer

	SO2 (ppm)														
	1-Hour Values			3-Hour Values			24-Hour Values			Annual		Monitor Number			
Row #	# Obs	1st Max	2nd Max	1st Max	2nd Max	# Exceed	1st Max	2nd Max	# Exceed	Mean	# Exceed		Year	Site ID	S Add
SORT	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲ ▼	▲
26	8,339	0.009	0.008	0.005	0.005	0	0.003	0.003	0	0.002	0	1	2006	060712002	1436 Arro Blvd Font
27	8,168	0.010	0.009	0.007	0.006	0	0.004	0.003	0	0.002	0	1	2007	060712002	1436 Arro Blvd Font
28	5,501	0.006	0.005	0.005	0.004	0	0.003	0.003	0	0.002	0	1	2008	060712002	1436 Arro Blvd Font
29	8,363	0.028	0.022	0.021	0.011	0	0.006	0.006	0	0.002	0	1	2006	060371103	163 Mai Los Ange
30	7,948	0.010	0.009	0.006	0.006	0	0.004	0.004	0	0.001	0	1	2007	060371103	163 Mai Los Ange
31	5,563	0.010	0.007	0.004	0.004	0	0.002	0.002	0	0.001	0	1	2008	060371103	163 Mai Los Ange
32	7,907	0.017	0.016	0.012	0.011	0	0.005	0.005	0	0.002	0	1	2006	060131004	186 Rum Blvd Pabl

33	8,063	0.017	0.016	0.012	0.012	0	0.005	0.005	0	0.002	0	1	2007	060131004	1865 Rum Blvd Pabl
34	5,935	0.018	0.013	0.012	0.009	0	0.004	0.004	0	0.001	0	1	2008	060131004	1865 Rum Blvd Pabl
35	8,279	0.009	0.007	0.005	0.005	0	0.004	0.003	0	0.001	0	2	2006	060371002	228 Palm Ave. Burb
36	8,337	0.008	0.006	0.005	0.005	0	0.003	0.003	0	0.001	0	2	2007	060371002	228 Palm Ave. Burb
37	5,557	0.006	0.006	0.005	0.005	0	0.003	0.003	0	0.001	0	2	2008	060371002	228 Palm Ave. Burb
38	8,006	0.012	0.011	0.009	0.007	0	0.004	0.004	0	0.002	0	1	2006	060591003	2850 Mesa Verd East Cost Mesa
39	8,172	0.029	0.015	0.017	0.006	0	0.004	0.003	0	0.001	0	1	2007	060591003	2850 Mesa Verd East Cost Mesa
40	5,571	0.009	0.008	0.006	0.005	0	0.003	0.003	0	0.001	0	1	2008	060591003	2850 Mesa Verd East Cost Mesa
41	7,980	0.025	0.022	0.018	0.018	0	0.007	0.005	0	0.001	0	1	2006	060130002	2956 Trea Boul
42	7,949	0.021	0.021	0.015	0.015	0	0.005	0.005	0	0.001	0	1	2007	060130002	2956 Trea Boul
43	5,971	0.019	0.018	0.012	0.011	0	0.004	0.004	0	0.001	0	1	2008	060130002	2956 Trea Boul
44	7,903	0.016	0.015	0.012	0.011	0	0.004	0.004	0	0.001	0	1	2006	060950004	304 Tuol St., Valle
45	7,935	0.020	0.020	0.010	0.008	0	0.004	0.004	0	0.001	0	1	2007	060950004	304 Tuol St., Valle
46	5,957	0.008	0.008	0.006	0.005	0	0.003	0.002	0	0.001	0	1	2008	060950004	304 Tuol St., Valle
47	6,879	0.240	0.230	0.216	0.093	0	0.052	0.038	0	0.007	0	1	2007	060190008	3425 First Fres
															3425

48	5,562	0.060	0.060	0.050	0.046	0	0.027	0.027	0	0.010	0	1	2008	060190008	First Fres
49	8,345	0.027	0.025	0.023	0.023	0	0.010	0.008	0	0.002	0	2	2006	060374002	364 Lon Bea Blvd Lon Bea
50	8,298	0.037	0.036	0.028	0.017	0	0.009	0.009	0	0.003	0	2	2007	060374002	364 Lon Bea Blvd Lon Bea
Grand Total						0			0		0		2007		
						0			0		0		2006		
						0			0		0		2008		

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Disclaimer: AirData reports are produced from a monthly extract of EPA's air pollution database, AQS. Data for this report were extracted on January 10, 2009. They represent the best information available to EPA from state agencies on that date. However, some values may be absent due to incomplete reporting, and some values subsequently may be changed due to quality assurance activities. The AQS database is updated daily by state and local organizations who own and submit the data. Please contact the pertinent state agency to report errors.

Readers are cautioned not to infer a qualitative ranking order of geographic areas based on AirData reports. Air pollution levels measured in the vicinity of a particular monitoring site may not be representative of the prevailing air quality of a county or urban area. Pollutants emitted from a particular source may have little impact on the immediate geographic area, and the amount of pollutants emitted does not indicate whether the source is complying with applicable regulations.

Appendix B

Intersection Screening Data

WEST SIDE METRO
AIR QUALITY ANALYSIS
SITE SELECTION SCREENING PROCESS

Site #	N/S Street	E/W Street	No Build						MOS 1						MOS 2						ALT 1						ALT 2						ALT 3						ALT 4						ALT 5					
			AM			PM			AM			PM			AM			PM			AM			PM			AM			PM			AM			PM			AM			PM			AM			PM		
			LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume	LOS	Del	Volume
1	Normandie Ave/Irolo St	Wilshire Boulevard	F	117.5	6,314	F	300.7	5,912	E	78.9	6,265	F	299.8	5,992	E	73.6	6,338	F	301.2	5,958	E	78.8	6,278	F	301.6	5,897	E	78.4	6,298	F	296.6	5,946	E	78.3	6,288	F	279.6	5,929	E	60.9	6,138	F	304.0	5,950	E	78.2	6,338	F	277.4	5,859
2	Western Ave	6th Street	E	68.0	5,714	F	98.0	6,222	E	56.3	5,616	F	96.1	6,221	E	72.5	5,772	F	96.7	6,214	E	55.4	5,612	F	94.1	6,185	E	55.5	5,603	F	91.3	6,146	E	61.0	5,618	F	100.3	6,238	E	58.8	5,650	F	89.1	6,127	E	65.6	5,712	F	97.0	6,214
3	Western Ave	Wilshire Boulevard	F	198.8	6,780	F	247.1	6,931	F	176.1	6,645	F	249.8	6,976	F	203.0	6,813	F	242.6	6,843	F	180.0	6,649	F	242.7	6,912	F	172.3	6,646	F	239.6	6,871	F	184.3	6,687	F	245.1	6,971	F	177.9	6,643	F	250.9	6,925	F	186.7	6,730	F	247.6	6,911
4	Western Ave	8th Street	F	83.3	4,541	E	68.4	4,757	E	78.9	4,441	E	68.6	4,771	E	74.3	4,532	E	59.8	4,684	E	75.0	4,440	E	65.2	4,727	E	75.5	4,420	E	61.5	4,682	E	76.8	4,506	E	63.7	4,728	E	76.6	4,451	E	61.4	4,702	E	74.1	4,561	E	67.9	4,760
5	Western Ave	Olympic Boulevard	F	140.4	7,036	F	141.0	7,295	F	133.2	6,938	F	144.5	7,212	F	137.0	6,962	F	131.0	7,128	F	134.7	6,950	F	142.0	7,201	F	126.7	6,862	F	136.9	7,139	F	133.7	6,947	F	134.9	7,110	F	130.3	6,916	F	133.5	7,154	F	128.1	6,928	F	138.0	7,184
6	Wilton Place	Wilshire Boulevard	F	104.0	7,223	F	141.9	7,582	F	96.9	7,310	F	140.3	7,579	F	107.7	7,341	F	144.5	7,618	F	87.8	7,244	F	134.0	7,602	F	105.8	7,303	F	136.7	7,601	F	104.3	7,316	F	132.2	7,557	F	108.3	7,334	F	124.0	7,611	F	106.2	7,273	F	127.9	7,560
7	Norton Ave	Wilshire Boulevard	D	38.1	5,077	B	11.0	4,661	D	38.7	5,129	B	10.9	4,661	D	41.4	5,140	B	11.4	4,744	D	36.0	5,070	B	11.6	4,705	D	38.0	5,152	B	10.3	4,668	D	36.2	5,106	B	10.3	4,583	D	35.5	5,107	B	11.2	4,700	D	38.8	5,114	B	10.9	4,635
8	Crenshaw Blvd	Wilshire Boulevard	F	123.6	5,332	F	140.3	5,574	F	122.9	5,377	F	143.0	5,623	F	120.0	5,341	F	138.0	5,656	F	119.6	5,315	F	139.8	5,590	F	121.8	5,384	F	137.0	5,608	F	115.8	5,319	F	137.9	5,547	F	125.3	5,329	F	144.6	5,599	F	119.8	5,364	F	143.5	5,568
9	Crenshaw Blvd	8th Street	C	22.7	3,166	C	22.5	3,540	C	21.6	3,157	C	22.7	3,540	C	22.8	3,238	C	22.3	3,543	C	22.0	3,121	C	22.8	3,563	C	21.2	3,155	C	22.3	3,493	C	23.4	3,177	C	23.1	3,522	C	22.3	3,143	C	21.7	3,562	C	21.8	3,194	C	23.2	3,583
10	Crenshaw Blvd	Olympic Boulevard	F	284.8	7,649	F	249.5	7,513	F	280.2	7,631	F	236.6	7,422	F	278.9	7,641	F	237.6	7,403	F	276.4	7,586	F	244.7	7,474	F	281.8	7,640	F	235.8	7,368	F	276.8	7,556	F	232.9	7,337	F	275.9	7,584	F	237.8	7,409	F	279.0	7,600	F	239.6	7,428
11	Lucerne Ave	Wilshire Boulevard	D	35.9	4,515	D	50.7	4,780	C	34.2	4,495	D	51.7	4,853	C	30.1	4,480	D	51.0	4,700	C	34.4	4,510	D	48.6	4,798	C	34.4	4,512	D	47.6	4,754	C	32.1	4,495	D	54.6	4,837	C	33.8	4,498	D	51.8	4,777	C	34.9	4,516	D	46.6	4,776
12	Rossmore Ave	Wilshire Boulevard	E	67.5	4,796	D	46.0	4,051	E	59.0	4,675	D	46.1	4,093	E	65.9	4,631	D	47.9	3,999	E	57.5	4,661	D	47.9	4,061	E	68.9	4,674	D	51.0	4,108	E	62.3	4,712	D	45.1	4,024	E	65.6	4,722	D	46.2	4,026	E	60.9	4,661	D	44.6	4,036
13	Sycamore Ave	Wilshire Boulevard	A	7.7	3,791	B	12.5	3,993	A	8.1	3,820	B	12.4	4,087	A	8.2	3,860	B	12.2	4,141	A	7.9	3,822	B	12.2	4,045	A	7.8	3,781	B	11.3	3,995	A	7.6	3,807	B	11.4	3,972	A	7.9	3,796	B	11.7	4,011	A	7.9	3,790	B	11.5	4,005
14	La Brea Ave	Beverly Blvd	F	268.1	7,453	F	296.8	8,105	F	272.7	7,470	F	298.6	8,180	F	249.3	7,384	F	292.9	8,114	F	253.9	7,443	F	299.2	8,160	F	255.0	7,415	F	297.9	8,125	F	268.8	7,435	F	292.7	8,071	F	263.9	7,415	F	300.3	8,141	F	261.0	7,427	F	291.5	8,057
15	La Brea Ave	3rd Street	F	103.8	7,421	F	113.2	6,976	F	107.1	7,482	F	109.8	7,088	F	101.4	7,402	F	118.1	7,000	F	101.2	7,395	F	114.6	6,970	F	101.2	7,377	F	104.1	7,032	F	105.2	7,427	F	111.3	6,947	F	100.4	7,376	F	116.2	6,953	F	100.1	7,380	F	111.1	6,948
16	La Brea Ave	6th Street	F	175.0	6,729	F	189.5	7,241	F	173.3	6,730	F	191.4	7,320	F	169.4	6,676	F	188.3	7,246	F	170.4	6,700	F	186.7	7,243	F	170.4	6,686	F	186.3	7,239	F	169.4	6,690	F	191.0	7,244	F	169.4	6,670	F	192.3	7,273	F	167.8	6,672	F	185.4	7,208
17	La Brea Ave	Wilshire Boulevard	F	165.6	7,832	F	193.7	8,147	F	169.0	7,850	F	197.1	8,252	F	166.9	7,866	F	195.4	8,258	F	166.0	7,835	F	194.5	8,171	F	162.2	7,766	F	194.6	8,155	F	168.4	7,783	F	196.4	8,162	F	162.2	7,745	F	194.7	8,196	F	136.1	7,757	F	198.4	8,120
18	La Brea Ave	8th Street	B	19.6	4,652	F	85.6	5,423	B	19.1	4,657	E	76.1	5,461	B	18.6	4,652	E	77.6	5,416	B	18.6	4,634	E	72.7	5,420	B	18.6	4,624	E	70.9	5,321	B	18.9	4,614	E	70.2	5,364	B	18.2	4,568	E	66.3	5,391	B	17.6	4,589	E	67.1	5,406
19	La Brea Ave	Olympic Boulevard	F	203.7	7,969	F	282.2	8,635	F	207.5	7,913	F	282.0	8,681	F	201.6	7,893	F	281.5	8,663	F	205.6	7,921	F	277.0	8,574	F	203.5	7,858	F	285.2	8,543	F	206.4	7,817	F	284.8	8,567	F	201.7	7,844	F	283.3	8,607	F	197.8	7,798	F	271.7	8,543
20	Detroit St	Wilshire Boulevard	B	14.2	3,829	E	58.6	4,420	B	14.2	3,826	E	62.1	4,472	B	14.6	3,792	E	60.1	4,457	B	14.8	3,783	E	61.2	4,398	B	15.0	3,749	E	59.3	4,440	B	15.1	3,733	E	63.2	4,442	B	13.6	3,758	E	59.9	4,429	B	14.0	3,759	E	55.9	4,333
21	Curson Ave	Wilshire Boulevard	F	90.1	4,307	D	42.8	4,281	E	77.6	4,297	D	44.9	4,331	E	74.0	4,273	D	39.4	4,287	E	72.7	4,257	D	39.1	4,292	E	76.6	4,257	D	40.9	4,252	E	73.0	4,265	D	35.3	4,286	E	75.1	4,274	D	40.8	4,295	E	79.8	4,224	D	40.0	4,233
22	Spaulding Ave	Wilshire Boulevard	B	15.7	3,561	B	16.3	3,594	B	15.7	3,578	B	16.4	3,640	B	15.7	3,548	B	16.3	3,644	B	15.7	3,546	B	16.4	3,651	B	15.7	3,542	B	16.4	3,597	B	15.6	3,528	B	16.1	3,611	B	17.1	3,550	B	16.2	3,639	B	15.7	3,523	B	16.1	3,586
23	Fairfax Ave	Beverly Blvd	D	45.5	5,819	F	105.7	6,330	D	48.5	5,817	F	105.8	6,364	D	48.3	5,820	F	103.1	6,305	D	52.2	5,886	F	104.9	6,348	D	43.8	5,818	F	105.9	6,338	D	51.0	5,830	F	102.3	6,317	D	49.1	5,834	F	104.1	6,326	D	42.6	5,788	F	105.6	6,336
24	Fairfax Ave	3rd Street	F	154.9	5,702	F	128.6	5,954	F	151.8	5,666	F	130.3	5,919	F	157.0	5,693	F	125.6	5,886	F	154.1	5,712	F	124.6	5,901	F	148.3	5,663	F	127.8	5,901	F	149.0	5,649	F	124.3	5,843	F	148.4	5,667	F	129.6	5,932	F	141.7	5,619	F	129.9	5,915
25	Fairfax Ave	6th Street	C	22.8	3,756	C	34.3	3,813	C	24.1	3,759	C	33.0	3,795	C	23.9	3,762	C	33.3	3,766	C	25.4	3,775	C	32.5	3,794	C	23.8	3,741	C	34.1	3,767	C	24.6	3,707	C	31.6	3,833	C	24.8	3,697	C	35.0	3,837	C	25.2	3,697	C	33.3	3,785
26	Fairfax Ave	Wilshire Boulevard	F	175.9	6,753	F	248.4	7,586	F	175.4	6,789	F	251.0	7,690	F	176.3	6,773	F	249.8	7,607	F	179.6	6,788	F	248.5	7,559	F	176.6	6,748	F	252.6	7,583	F	175.6	6,705	F	244.1	7,530	F	177.6	6,687	F	248.8	7,610	F	174.5	6,684	F	239.7	7,538
27	Fairfax Ave	Del Valle Dr/8th St	B	17.3	3,094	C	23.5	3,118	B	16.5	3,122	C	28.3	3,203	B	17.8	3,128	C	23.9	3,163	B	17.3	3,157	C	21.8	3,133	B	17.2	3,162	C	22.1	3,121	B	17.5	3,149	C	21.9	3,075	B	17.9	3,144	C	23.5	3,130	B	17.6	3,115	C	21.7	3,108
28	San Vicente Boulevard	Olympic Boulevard	F	364.9	7,117	F	294.4	6,778	F	356.1	7,173	F	294.5	6,781	F	346.4	7,115	F	283.1	6,662	F	352.2	7,113	F	288.0	6,680	F	344.8	7,071	F	294.4	6,858	F	346.8	7,066	F	285.3	6,750	F	347.7	7,128	F	279.7	6,634	F	343.6	7,063	F	285.0	6,698
29	Fairfax Ave	San Vicente Boulevar	F	226.8	5,871	F	121.6	5,661	F	231.7	5,931	F	125.8	5,679	F	231.1	5,908	F	125.1	5,643	F	221.8	5,923	F	116.1	5,594	F	225.1	5,876	F	121.2	5,677	F	217.8	5,844	F	126.0	5,668	F	208.2	5,908	F	117.6	5,597	F	209.3	5,867	F	123.7	5,660
30	Fairfax Ave	Olympic Boulevard	F	232.9	5,621	F	311.4	5,780	F	230.9	5,633	F	314.5	5,785	F	223.1	5,588	F	314.4	5,782	F	222.9	5,575	F	311.6	5,755	F	222.0	5,569	F	311.9	5,773	F	219.3	5,526	F	304.8	5,700	F	223.4	5,576	F	314.2	5,702	F	220.4	5,542	F	313.1	5,686
31	Fairfax Ave	Pico Boulevard	F	119.4	5,100	F	98.1	4,526	F	120.6	5,105	F	99.7	4,521	F	116.3	5,105	F	100.0	4,525	F	113.3	5,068	F	91.8	4,474	F	114.2	5,028	F	91.6	4,512	F	112.1	5,025	F	95.8	4,532	F	113.7	5,062	F	89.2	4,503	F	110.7	5,039	F	90.1	4,488
32	Crescent Heights Blvd/N	Wilshire Boulevard	F	119.2	5,575	C	34.0	5,879	F	116.7	5,556	C	34.2	5,934	F	120.0	5,534	C	25.1	5,809	F	108.7	5,537	C	25.0	5,760	F	106.4	5,507	C	25.3	5,923	F	99.7	5,460	C	34.2	5,956	F	115.8	5,620	C	34.8	5,809	F	102.2	5,475	C	34.0	5,816
33	San Vicente Boulevard	Wilshire Boulevard	F	118.6	6,925	F	224.8	7,480	F	113.8	6,910	F	222.6	7,455	F	105.9	6,855	F	226.0	7,515	F	105.0	6,833	F	223.9	7,463	F	112.1	6,814	F	220.2	7,354	F	102.5	6,759	F	210.9	7,319	F	105.3	6,808	F	218.9	7,401	F	107.0	6,782	F	206.8	7,398
34	Gale Dr	Wilshire Boulevard	B	17.9	3,997	B	13.0	4,244	B	18.0	4,011	B	12.9	4,245	B	17.6	3,927	B	12.6	4,221	B	17.6	3,928	B	12.6	4,187	B	17.7	3,946	B	12.2	4,104	B	17.6	3,883	B	12.6	4,139	B	17.8	3,922	B	12.8	4,234	B	17.5	3,897	B	13.0	4,256
35	La Cienega Boulevard	3rd Street	F	228.5	6,484	F	164.1	6,795	F	222.6	6,536	F	167.3	6,899	F	231.3	6,454	F	168.1	6,907	F	215.9	6,505	F	166.7	6,837	F	211.1	6,459	F	167.1	6,860	F	211.8	6,458	F	165.9	6,879	F	213.7	6,458	F	161.9	6,796	F	202.0	6,389	F	164.2	6,815
36	San Vicente Boulevard	Burton Way	F	82.6	4,156	F	141.6	4,114	E	77.1	4,161	E	78.3	4,148	E	76.3	4,109	E	78.6	4,120	E	73.9	4,071	E	78.3	4,217	E	74.4	4,048	E	75.8	4,146	E	79.2	4,067	E	77.5	4,129	E	74.2	4,019	E	77.9	4,146	E	71.5	4,081	E	76.9	4,145
37	La Cienega Boulevard	San Vicente Boulevar	F	87.3	7,419	C	34.8	7,885	F	89.2	7,492	C	33.7	7,907	F	84.8	7,405	C	33.8	7,941	F	81.9	7,365	C	34.0	7,940	F	83.3	7,267	C	34.7	7,884	F	83.7	7,343	C	35.0	7,886	F	83.6	7,297	C	34.1	7,846	F	81.5	7,317	C	34.4	7,933
38	La Cienega Boulevard	Clifton Way	B	14.8	4,045	D	47.0	4,656	B	17.4	4,115	D	53.9	4,682	B	14.4	4,050	D	44.0	4,644	B	14.2	4,121	D	44.0	4,661	B	13.1	4,016	D	42.1	4,619	B	14.9	4,045	D	41.8	4,635	B	13.1	4,116	D	45.5	4,625	B	13.9	4,015	D	40.2	4,644
39	La Cienega Boulevard	Wilshire Boulevard	F	208.2	8,047	F	205.9	8,455	F	208.2	8,108	F	205.7	8,463	F	205.6	7,991	F	205.8	8,404	F	208.4	8,018	F	205.7	8,406	F	198.8	7,957	F	201.7	8,387	F	203.9	7,947	F	200.2	8,337	F	206.3	8,025	F	206.0	8,390	F	193.8	7,914	F	200.7	8,370
40	La Cienega Boulevard	Gregory Way	F	91.3	5,375	F	97.1	5,337	F	88.5	5,382	F	97.9	5,366	F	89.3	5,375	F	95.3	5,273	F	87.1	5,389	F	95.7	5,330	F	87.5	5,296	F	96.1	5,408	F	89.0	5,335	F	95.5	5,323	F	87.4	5,378	F	99.6	5,329	F	86.1	5,277	F	96.0	5,303
41	La Cienega Boulevard	Olympic Boulevard	F	190.0	9,132	F	283.2	9,176	F	185.3	9,110	F	281.3	9,203	F	178.8	9,112	F	286.6	9,137	F	178.5	9,067	F	282.2	9,150	F	178.0	8,968	F	285.6	9,124	F	189.7	8,956	F	285.7	9,034	F	183.1	9,041	F	282.0	9,104	F	174.2	8,970	F	285.4	9,043
42	La Cienega Boulevard	Pico Boulevard	F	143.6	7,697	F	225.5	7,515	F	146.2	7,705	F	223.5	7,493	F	145.0	7,730	F	224.2	7,490	F	144.0	7,698	F	226.3	7,487	F	138.8	7,627	F	223.5	7,472	F	134.6	7,560	F	229.4	7,426	F	139.4	7,664	F	216.1	7,425	F	141.4	7,638	F	221.3	7,442
43	San Vicente Boulevard	3rd Street	E	72.0	4,539	F	103.8	4,905	E	72	4539	F	104	4905	E	71.5	4,503	F	97.9	4,819	E	69.4	4,504	F	100.9	4,886	E	66.2	4,501	F	106.8	4,892	E	67.2	4,452	F	104.2	4,819	E	69.4	4,515	F	104.7	4,865	E	64.7	4,443	F	93.9	4,811
44	Willaman Dr	Wilshire Boulevard	B	12.0	4,549	B	11.4	4,818	B	12	4549	B	11	4818	B	12.4	4,494	B	10.9	4,802	B	11.2	4,481	B	10.9	4,759	B	11.3	4,479	B	11.3	4,739	B	11.6	4,471	B	11.1	4,733	B	11.3	4,480	B	11.0	4,795	B	11.4	4,444	B	11.1	4,748
45	Robertson Blvd	Burton Way	F	85.7	4,007	F	113.1	4,119	F	86	4007	F	113	4119	E	76.1	3,993	F	104.7	4,107	E	74.9	3,976	F	104.9	4,138	E	75.0	3,931	F	116.8	4,144	E	76.7	3,976	F	92.4	4,121	E	74.3	3,958	F	97.1	4,141	E	76.4	3,937	F	108.4	4,094
46	Robertson Blvd	Wilshire Boulevard	F	140.2	6,041	F	139.5	6,472	F	140	6041	F	140	6472	F	130.2	5,911	F	139.8	6,459	F	129.1	5,909	F	140.8	6,467	F	136.1	5,880	F	137.3	6,444	F	128.1	5,856	F	134.2	6,435	F	126.3	5,880	F	139.0	6,506	F	128.4	5,870	F	140.9	6,419
47	Robertson Blvd	Olympic Boulevard	F	151.5	6,957	F	209.2	7,106	F	152	6957	F	209	7106	F	143.1	6,888	F	208.0	7,124	F	141.7	6,846	F	202.7	7,137	F	139.2	6,821	F	205.8	7,161	F	140.2	6,842	F	206.2	7,052	F	138.2	6,831	F	202.9	7,144	F	140.3	6,813	F	199.1	7,082
48	Doheny Dr	Wilshire Boulevard	F	154.1	6,020	F	127.8	6,083	F	154	6020	F	128	6083	F	146.2	5,965	F	131.8	6,080	F	142.1	5,911	F	122.4	6,030	F	150.4	5,946	F	122.3	6,048	F	146.8	5,906	F	118.7	5,965	F	139.3	5,877	F	128.8	6,065	F	145.6	5,890	F	122.2	5,998
49	Canon Dr	Santa Monica Bouleva	F	136.8	4,616	F	214.1	5,523	F	137	4616	F	214	5523	F	136.8	4,638	F	206.8	5,575	F	138.0	4,624	F	205.6	5,566	F	131.6	4,580	F	209.4	5,565	F	132.0	4,585	F	203.8	5,501	F	133.6	4,587	F	201.4	5,508	F	122.1	4,508	F	210.8	5,481
50	Canon Dr	Dayton Drive	B	13.7	960	B	15.6	1,778	B	14	960	B	16	1778	B	13.5	962	B	16.4	1,787	B	14.3	862	B	16.9	1,746	B	13.9	839	B	15.6	1,739	B	14.1	861	B	15.5	1,732	B	13.6	929	B	16.7	1,726	B	13.9	922	B	16.3	1,756
51	Canon Dr (jogged)	Wilshire Boulevard	E	72.8	4,865	D	45.2	5,004	E	73	4865	D	45	5004	E	69.3	4,768	C	34.4	4,836	E	74.4	4,833	C	34.5	4,889	E	62.7	4,760	C	34.7	4,851	E	68.8	4,715	C	34.4	4,976	E	76.8	4,774	C	33.8	4,872	E	76.2	4,766	C	34.8	4,929
52	Beverly Dr	Santa Monica Bouleva	F	257.1	5,416	F	247.4	5,978	F	257	5416	F	247	5978	F	257.1	5,432	F	246.9	6,037	F	255.3	5,427	F	251.4	6,080	F	219.5	5,362	F	251.4	6,063	F	231.0	5,331	F	252.1	6,087	F	248.1	5,331	F	251.9	6,094	F	205.4	5,299	F	245.0	5,990
53	Beverly Dr	Little Santa Monica	F	194.5	4,601	F	141.9	4,986	F	195	4601	F	142	4986	F	193.2	4,586	F	146.2	5,024	F	191.5	4,597	F	144.7	5,021	F	180.7	4,607	F	144.4	4,975	F	178.4	4,583	F	146.2	5,055	F	184.4	4,589	F	146.5	5,051	F	175.6	4,542	F	146.6	5,040
54	Beverly Dr	Dayton Drive	C	29.8	2,203	C	28.7	2,835	C	30	2203	C	29	2835	C	28.8	2,191	C	33.2	2,901	C	27.1	2,071	C	30.6	2,826	C	25.8	2,071	C	27.9	2,786	C	24.3	2,054	C	33.2	2,885	C	24.2	2,108	C	33.7	2,859	C	25.8	2,129	C	31.5	2,911
55	Beverly Dr	Wilshire Boulevard	F	95.5	6,370	F	127.8	7,031	F	96	6370	F	128	7031	F	93.4	6,355	F	131.9	7,132	F	100.4	6,354	F	128.8	7,093	F	95.7	6,267	F	131.7	7,091	F	97.3	6,300	F	132.3	7,128	F	94.4	6,325	F	132.5	7,180	F	98.4	6,305	F	123.6	7,071
56	Beverly Dr	Charleville Blvd	C	24.0	3,282	C	27.0	3,490	C	24	3282	C	27	3490	C	23.4	3,257	C	27.5	3,491	C	23.7	3,324	C	26.2	3,445	C	22.4	3,239	C	26.1	3,415	C	22.8	3,291	C	27.0	3,464	C	22.6	3,268	C	26.9	3,471	C	23.1	3,279	C	26.4	3,457
57	Beverwil Dr	Olympic Boulevard	F	297.5	6,651	F	296.6	6,726	F	298	6651	F	297	6726	F	278.0	6,531	F	295.1	6,709	F	277.8	6,458	F	273.3	6,674	F	273.4	6,473	F	292.9	6,715	F	271.9	6,437	F	297.4	6,624	F	281.4	6,418	F	291.2	6,643	F	270.7	6,429	F	296.2	6,622
58	Beverly Dr	Olympic Boulevard	F	294.2	6,808	F	300.3	7,313	F	294	6808	F	300	7313	F	280.1	6,709	F	299.1	7,350	F	281.4	6,728	F	282.4	7,348	F	279.9	6,720	F	296.9	7,322	F	279.2	6,697	F	303.2	7,309	F	288.1	6,700	F	303.9	7,341	F	275.9	6,705	F	302.5	7,268
59	Rodeo Drive	Dayton Drive	C	20.7	994	E	58.3	1,978	C	21	994	E	58	1978	C	20.6	987	D	52.9	1,917	C	20.3	903	D	54.5	1,902	C	20.3	905	D	48.5	1,908	C	20.3	908	D	54.6	1,943	C	20.5	963	D	51.0	1,956	C	20.6	974	D	48.2	1,905
60	Rodeo Drive	Wilshire Boulevard	D	43.5	4,577	D	44.4	5,583	D	44	4577	D	44	5583	C	34.5	4,547	D	47.7	5,644	C	33.1	4,504	D	47.2	5,614	C	34.9	4,457	D	46.0	5,622	C	34.8	4,452	D	47.5	5,643	C	33.4	4,480	D	51.4	5,678	C	33.9	4,480	D	44.5	5,578
61	Camden Dr/Dayton Dr	Wilshire Boulevard	F	204.0	4,734	F	297.2	5,585	F	204	4734	F	297	5585	F	194.9	4,702	F	298.0	5,658	F	190.1	4,568	F	275.6	5,604	F	193.4	4,529	F	278.3	5,603	F	194.9	4,526	F	281.1	5,608	F	188.5	4,616	F	281.6	5,633	F	191.5	4,617	F	294.5	5,574
62	Santa Monica Boulevar	Wilshire Boulevard	F	499.0	8,551	F	512.7	8,328	F	499	8551	F	513	8328	F	491.8	8,547	F	516.6	8,383	F	480.2	8,481	F	509.0	8,333	F	481.3	8,387	F	515.5	8,398	F	477.7	8,388	F	507.0	8,330	F	486.7	8,446	F	517.1	8,405	F	467.5	8,319	F	497.9	8,319
63	Little Santa Monica	Wilshire Boulevard	F	347.2	5,855	F	325.6	6,269	F	347	5855	F	326	6269	F	350.7	5,853	F	329.5	6,288	F	343.5	5,914	F	329.2	6,317	F	334.3	5,856	F	329.8	6,327	F	338.3	5,861	F	327.8	6,347	F	343.5	5,825	F	329.8	6,355	F	324.6	5,732	F	328.0	6,339
64	Century Park East	Santa Monica Bouleva	F	173.0	6,354	F	129.6	6,243	F	173	6354	F	130	6243	F	151.3	6,319	F	120.4	6,315	F	141.6	6,338	F	115.4	6,202	F	161.1	6,267	F	117.0	6,253	F	157.2	6,220	F	101.6	6,184	F	157.7	6,291	F	115.7	6,249	F	152.3	6,257	F	104.5	6,134
65	Century Park East	Constellation Blvd	D	42.0	2,914	F	81.1	3,260	D	42	2914	F	81	3260	C	34.8	2,876	F	80.6	3,323	C	34.5	2,816	F	85.2	3,316	C	34.9	2,797	F	82.8	3,219	C	33.7	2,871	F	83.7	3,174	C	30.8	2,768	F	81.1	3,307	C	34.0	2,820	F	83.6	3,226
66	Century Park East	Olympic Boulevard	F	159.0	8,209	F	130.8	8,304	F	159	8209	F	131	8304	F	152.2	8,192	F	134.2	8,395	F	149.2	8,107	F	131.6	8,280	F	149.1	8,084	F	131.1	8,273	F	147.2	8,139	F	129.2	8,187	F	147.2	8,071	F	133.3	8,321	F	144.2	8,053	F	129.0	8,231
67	Avenue of the Stars	Santa Monica Bouleva	F	107.7	5,636	E	69.1	5,818	F	108	5636	E	69	5818	F	99.4	5,651	E	69.2	5,743	F	104.3	5,674	E	66.8	5,825	F	95.6	5,625	E	61.3	5,884	F	90.8	5,515	E	65.1	5,826	F	95.6	5,622	E	62.1	5,783	F	92.7	5,599	E	61.8	5,735
68	Avenue of the Stars	Constellation Blvd	F	112.3	4,692	E	56.2	5,152	F	112	4692	E	56	5152	F	94.9	4,616	E	56.6	5,192	F	85.2	4,596	E	58.9	5,129	F	97.7	4,611	E	58.4	5,105	F	94.9	4,538	E	55.8	5,152	F	100.3	4,592	E	59.9	5,125	F	96.8	4,588	E	60.9	5,160
69	Avenue of the Stars (So	Olympic Boulevard	B	10.5	3,005	B	10.3	2,999	B	11	3005	B	10	2999	B	11.1	2,942	A	9.2	2,995	B	11.4	2,973	A	9.8	2,867	B	12.5	3,016	A	9.6	2,888	B	12.3	2,924	A	9.4	2,940	B	12.9	3,009	A	9.3	2,874	B	12.6	2,997	A	9.9	2,940
70	Avenue of the Stars (No	Olympic Boulevard	B	16.0	3,125	B	13.4	2,909	B	16	3125	B	13	2909	B	14.9	3,013	B	13.1	2,920	B	15.2	3,041	B	13.3	2,870	B	15.5	3,017	B	13.5	2,917	B	15.3	2,988	B	13.4	2,946	B	15.8	3,040	B	13.1	2,855	B	15.6	3,019	B	13.8	2,939
71	Avenue of the Stars	Galaxy Way	B	18.6	2,793	C	21.6	2,764	B	19	2793	C	22	2764	B	18.3	2,678	C	21.8	2,767	B	17.7	2,706	C	21.7	2,736	B	17.7	2,685	C	21.6	2,766	B	17.6	2,656	C	20.7	2,790	B	17.5	2,704	C	21.7	2,708	B	17.2	2,685	C	20.7	2,783
72	Avenue of the Stars	Pico Boulevard	F	326.6	5,643	F	82.0	5,958	F	327	5643	F	82	5958	F	323.1	5,591	E	78.6	5,946	F	316.3	5,570	E	77.9	5,935	F	315.2	5,545	E	78.6	5,999	F	310.4	5,505	E	77.5	5,912	F	319.7	5,509	E	77.7	5,903	F	303.0	5,513	E	71.3	5,923
73	Century Park West	Santa Monica Bouleva	F	241.2	6,206	F	132.9	6,173	F	241	6206	F	133	6173	F	241.2	6,222	F	132.0	6,255	F	231.8	6,181	F	129.8	6,161	F	227.9	6,079	F	131.3	6,194	F	228.1	6,064	F	131.6	6,169	F	226.1	6,126	F	129.5	6,168	F	227.6	6,091	F	128.7	6,119
74	Century Park West	Constellation Blvd	D	40.3	2,190	C	28.8	2,271	D	40	2190	C	29	2271	C	33.0	2,200	C	34.5	2,458	C	33.7	2,151	C	23.7	2,272	C	31.4	2,108	C	23.9	2,295	C	34.5	2,110	C	26.9	2,330	C	32.6	2,147	C	26.4	2,323	C	28.1	2,092	C	24.1	2,301
75	Century Park West	Olympic Boulevard	F	190.7	6,700	F	88.0	5,748	F	191	6700	F	88	5748	F	187.3	6,680	E	77.9	5,885	F	175.4	6,676	E	77.7	5,813	F	176.4	6,688	E	76.7	5,733	F	181.2	6,623	E	75.7	5,772	F	176.1	6,689	E	77.0	5,837	F	175.5	6,664	E	79.2	5,734
76	Beverly Glen Blvd	Wilshire Boulevard	F	177.3	8,377	F	156.8	8,003	F	177	8377	F	157	8003	F	181.6	8,437	F	159.9	8,075	F	174.1	8,311	F	158.4	8,048	F	175.1	8,343	F	160.5	8,061	F	173.7	8,291	F	153.2	7,971	F	175.9	8,371	F	158.4	7,989	F	171.5	8,279	F	155.3	7,984
77	Beverly Glen Blvd	Santa Monica Bouleva	F	519.6	8,508	F	590.3	8,463	F	520	8508	F	590	8463	F	522.2	8,477	F	588.3	8,536	F	520.1	8,404	F	584.3	8,474	F	506.1	8,355	F	586.7	8,483	F	514.9	8,404	F	581.1	8,391	F	512.9	8,416	F	594.4	8,387	F	507.7	8,402	F	574.0	8,440
78	Beverly Glen Blvd	Olympic Boulevard	F	235.8	9,202	F	165.9	8,605	F	236	9202	F	166	8605	F	230.4	9,017	F	168.1	8,710	F	229.6	9,029	F	168.4	8,742	F	232.2	9,020	F	167.4	8,768	F	221.4	9,021	F	161.1	8,505	F	229.8	9,059	F	164.7	8,590	F	232.1	9,108	F	162.7	8,631
79	Hilgard Ave	Sunset Boulevard	F	182.2	3,948	F	373.9	4,826	F	182	3948	F	374	4826	F	182	3948	F	374	4826	F	160.8	3,944	F	359.7	4,779	F	180.8	3,936	F	367.0	4,736	F	167.9	3,945	F	377.0	4,781	F	157.6	3,922	F	371.3	4,752	F	171.4	3,997	F	378.6	4,747
80	Hilgard Ave	Le Conte Ave	C	27.7	1,953	F	95.6	2,574	C	28	1953	F	96	2574	C	28	1953	F	96	2574	C	27.7	1,936	F	92.7	2,559	C	28.2	1,956	F	98.7	2,530	C	27.3	1,956	F	93.3	2,546	C	28.1	1,959	F	87.3	2,539	C	28.7	1,988	F	83.7	2,542
81	Glendon Ave/Tiverton A	Lindbrook Ave	C	31.4	2,361	F	495.1	3,435	C	31	2361	F	495	3435	C	31	2361	F	495	3435	C	32.6	2,405	F	445.7	3,426	C	33.9	2,400	F	468.2	3,418	C	28.9	2,297	F	474.3	3,444	C	32.2	2,372	F	441.7	3,459	C	31.1	2,488	F	439.6	3,473
82	Glendon Ave	Wilshire Boulevard	F	124.1	6,962	F	688.1	7,493	F	124	6962	F	688	7493	F	124	6962	F	688	7493	F	128.1	6,987	F	651.4	7,473	F	127.8	7,030	F	690.6	7,510	F	120.6	6,870	F	673.1	7,418	F	127.1	6,963	F	661.5	7,524	F	128.9	6,977	F	653.5	7,494
83	Westwood Blvd	Le Conte Ave	C	23.4	1,920	B	18.7	2,336	C	23	1920	B	19	2336	C	23	1920	B	19	2336	C	23.6	1,937	B	17.9	2,322	C	23.8	1,944	B	17.9	2,340	C	23.3	1,921	B	18.1	2,337	C	23.6	1,926	B	17.9	2,328	C	23.2	1,933	B	17.5	2,294
84	Westwood Blvd	Weyburn Ave	C	24.6	1,902	D	44.2	2,566	C	25	1902	D	44	2566	C	25	1902	D	44	2566	C	24.9	1,927	D	42.8	2,499	C	24.9	1,934	D	42.2	2,521	C	22.5	1,909	D	41.2	2,511	C	24.6	1,913	D	39.9	2,512	C	21.3	1,918	D	42.9	2,488
85	Westwood Blvd	Lindbrook Ave	D	52.1	2,651	F	147.1	3,921	D	52	2651	F	147	3921	D	52	2651	F	147	3921	D	50.0	2,635	F	151.0	3,968	D	47.8	2,593	F	142.6	3,930	D	47.8	2,516	F	146.3	3,882	D	48.6	2,611	F	149.7	3,999	D	55.0	2,718	F	147.0	3,946
86	Westwood Blvd	Wilshire Boulevard	F	360.3	8,985	F	566.1	9,881	F	360	8985	F	566	9881	F	360	8985	F	566	9881	F	352.1	8,843	F	569.8	9,866	F	337.3	8,723	F	568.3	9,943	F	364.3	8,837	F	555.2	9,827	F	342.5	8,786	F	562.2	9,796	F	350.3	8,779	F	565.5	9,798
87	Westwood Blvd	Wellworth Ave	F	417.0	3,865	F	592.0	4,638	F	417	3865	F	592	4638	F	417	3865	F	592	4638	F	388.1	3,833	F	535.6	4,587	F	388.3	3,673	F	536.9	4,618	F	419.6	3,819	F	530.8	4,607	F	373.2	3,793	F	527.3	4,565	F	402.4	3,753	F	516.8	4,506
88	Westwood Blvd	Ohio Ave	F	186.2	4,009	F	328.3	4,965	F	186	4009	F	328	4965	F	186	4009	F	328	4965	F	184.1	3,986	F	322.4	4,957	F	171.0	3,856	F	322.9	4,970	F	167.3	3,859	F	320.0	4,939	F	180.6	3,966	F	330.0	5,016	F	177.0	3,920	F	314.5	4,900
89	Westwood Blvd	Santa Monica Blvd	F	302.6	8,307	F	285.4	8,866	F	303	8307	F	285	8866	F	303	8307	F	285	8866	F	292.2	8,271	F	269.8	8,882	F	284.8	8,159	F	280.3	8,891	F	281.8	8,140	F	254.4	8,818	F	282.7	8,208	F	285.7	8,969	F	281.9	8,168	F	279.3	8,847
90	Westwood Blvd	Olympic Boulevard	F	206.5	8,064	F	206.9	9,177	F	207	8064	F	207	9177	F	207	8064	F	207	9177	F	192.6	7,935	F	209.4	9,187	F	206.9	7,931	F	208.5	9,187	F	210.6	7,919	F	207.5	9,179	F	201.9	7,921	F	209.3	9,193	F	193.3	7,918	F	207.7	9,176
91	Westwood Blvd	Pico Boulevard	F	165.0	6,996	F	206.6	8,074	F	165	6996	F	207	8074	F	165	6996	F	207	8074	F	165.4	7,007	F	206.8	8,133	F	159.8	6,874	F	210.1	8,096	F	167.7	6,877	F	208.3	8,115	F	165.4	6,929	F	207.7	8,104	F	158.0	6,852	F	201.9	8,119
92	Gayley Ave	Le Conte Ave	B	11.1	1,374	D	40.4	2,371	B	11	1374	D	40	2371	B	11	1374	D	40	2371	B	11.0	1,599	D	39.6	2,416	B	11.0	1,621	D	39.7	2,401	B	11.1	1,646	D	39.0	2,489	B	11.1	1,645	D	39.6	2,402	B	11.4	1,379	D	39.5	2,421
93	Gayley Ave	Lindbrook Ave	D	54.8	2,205	F	252.9	2,973	D	55	2205	F	253	2973	D	55	2205	F	253	2973	D	54.2	2,271	F	246.7	2,971	D	51.9	2,229	F	250.2	2,961	D	52.6	2,186	F	185.9	2,985	D	48.9	2,217	F	253.8	2,980	D	54.3	2,229	F	232.0	2,998
94	Gayley Ave/Midvale	Wilshire Boulevard	F	327.9	8,774	F	438.7	9,016	F	328	8774	F	439	9016	F	328	8774	F	439	9016	F	326.7	8,724	F	421.9	8,968	F	314.1	8,598	F	434.1	9,058	F	330.7	8,708	F	428.6	9,046	F	321.4	8,692	F	415.8	8,830	F	321.6	8,624	F	420.0	8,963
95	Veteran Ave	Sunset Boulevard	F	187.9	5,290	F	177.3	5,248	F	188	5290	F	177	5248	F	188	5290	F	177	5248	F	188.7	5,394	F	181.6	5,328	F	175.8	5,131	F	180.4	5,330	F	183.1	5,161	F	180.0	5,374	F	191.0	5,316	F	180.6	5,401	F	187.8	5,405	F	176.4	5,286
96	Veteran Ave	Wilshire Boulevard	F	580.6	10,884	F	483.3	10,991	F	581	10884	F	483	10991	F	581	10884	F	483	10991	F	579.8	10,884	F	486.2	11,102	F	553.4	10,679	F	485.0	11,110	F	562.9	10,719	F	487.0	11,020	F	572.0	10,864	F	483.9	10,945	F	553.7	10,740	F	484.3	11,074
97	Sepulveda Blvd	Wilshire Boulevard	F	472.7	10,069	F	456.2	9,732	F	473	10069	F	456	9732	F	473	10069	F	456	9732	F	476.6	9,983	F	448.1	9,627	F	474.9	10,101	F	450.8	9,626	F	450.7	9,887	F	460.6	9,713	F	464.8	10,025	F	457.8	9,672	F	471.2	10,041	F	453.0	9,666
98	Sepulveda Blvd	Olympic Boulevard	F	120.6	7,969	F	169.1	8,989	F	121	7969	F	169	8989	F	121	7969	F	169	8989	F	123.7	7,778	F	165.1	8,917	F	110.0	7,850	F	162.7	8,920	F	118.6	7,807	F	159.5	8,927	F	123.0	7,828	F	166.4	8,928	F	113.6	7,833	F	163.8	8,959
99	Sepulveda Blvd	Pico Boulevard	F	129.7	7,383	F	206.7	8,299	F	130	7383	F	207	8299	F	130	7383	F	207	8299	F	114.9	7,189	F	208.5	8,421	F	130.8	7,383	F	184.1	8,144	F	116.1	7,088	F	186.1	8,261	F	114.5	7,225	F	204.0	8,285	F	125.7	7,228	F	185.8	8,254
100	San Vicente/Federal	Wilshire Boulevard	F	218.9	7,162	F	149.9	6,619	F	219	7162	F	150	6619	F	219	7162	F	150	6619	F	219	7162	F	150	6619	F	218.1	7,138	F	151.5	6,599	F	208.7	7,135	F	153.0	6,613	F	207.9	7,125	F	150.9	6,559	F	218.8	7,029	F	150.8	6,587
101	Barrington Ave	W San Vicente Blvd	F	226.4	3,879	F	214.0	4,332	F	226	3879	F	214	4332	F	226	3879	F	214	4332	F	226	3879	F	214	4332	F	194.9	3,788	F	216.0	4,379	F	212.5	3,753	F	197.6	4,359	F	207.3	3,794	F	208.0	4,379	F	164.8	3,853	F	203.4	4,329
102	Barrington Ave	Wilshire Boulevard	F	109.9	5,176	F	537.1	5,116	F	110	5176	F	537	5116	F	110	5176	F	537	5116	F	110	5176	F	537	5116	F	101.3	5,205	F	525.7	5,119	F	101.1	5,171	F	537.4	5,076	F	113.8	5,229	F	539.7	5,028	F	104.7	5,176	F	536.8	5,076
103	Barrington Ave	Texas Ave	A	10.0	1,725	E	63.8	2,272	A	10	1725	E	64	2272	A	10	1725	E	64	2272	A	10	1725	E	64	2272	A	9.1	1,718	D	47.2	2,238	A	9.3	1,718	D	51.3	2,266	A	10.0	1,700	D	43.3	2,221	A	9.3	1,717	D	43.2	2,210
104	Barrington Ave	Santa Monica Bouleva	F	122.2	5,021	F	112.0	4,982	F	122	5021	F	112	4982	F	122	5021	F	112	4982	F	122	5021	F	112	4982	F	110.6	4,897	F	109.7	5,114	F	107.5	4,919	F	114.1	5,105	F	113.2	4,929	F	109.1	5,062	F	107.4	4,907	F	100.2	4,992
105	Barrington Ave	Olympic Boulevard	F	87.3	6,308	F	86.6	6,653	F	87	6308	F	87	6653	F	87	6308	F	87	6653	F	87	6308	F	87	6653	F	86.4	6,252	E	78.9	6,637	F	86.7	6,199	E	76.2	6,590	F	90.5	6,255	E	79.0	6,651	F	88.5	6,215	E	78.2	6,610
106	Westgate Ave (NB appr	Wilshire Boulevard	B	19.8	4,118	C	23.6	4,482	B	20	4118	C	24	4482	B	20	4118	C	24	4482	B	20	4118	C	24	4482	B	17.2	4,072	C	26.7	4,520	B	18.0	4,108	C	21.8	4,460	B	17.6	4,108	C	20.3	4,400	B	16.7	4,013	C	21.9	4,452
107	Brockton Ave	Wilshire Boulevard	B	13.3	3,713	C	25.1	4,336	B	13	3713	C	25	4336	B	13	3713	C	25	4336	B	13	3713	C	25	4336	B	13.1	3,746	C	25.8	4,388	B	13.3	3,707	C	23.1	4,347	B	13.2	3,788	C	22.3	4,287	B	12.9	3,686	C	24.3	4,351
108	Bundy Dr	San Vicente Blvd	F	81.9	4,367	E	72.8	4,477	F	82	4367	E	73	4477	F	82	4367	E	73	4477	F	82	4367	E	73	4477	E	70.2	4,357	E	71.6	4,514	E	77.4	4,288	E	70.8	4,524	E	68.0	4,286	E	71.8	4,513	E	66.4	4,283	E	69.8	4,502
109	Bundy Dr	Wilshire Boulevard	F	160.4	5,589	F	193.9	6,103	F	160	5589	F	194	6103	F	160	5589	F	194	6103	F	160	5589	F	194	6103	F	163.2	5,660	F	195.8	6,187	F	154.2	5,509	F	192.2	6,230	F	165.3	5,653	F	196.2	6,161	F	165.0	5,633	F	195.4	6,116
110	Bundy Dr	Texas Ave	B	15.3	2,704	D	39.8	3,301	B	15	2704	D	40	3301	B	15	2704	D	40	3301	B	15	2704	D	40	3301	B	13.6	2,740	D	44.3	3,331	B	15.0	2,675	D	40.6	3,325	B	15.1	2,747	D	46.5	3,387	B	12.7	2,726	D	39.6	3,300
111	Bundy Dr	Santa Monica Bouleva	E	78.6	5,433	F	87.7	5,651	E	79	5433	F	88	5651	E	79	5433	F	88	5651	E	79	5433	F	88	5651	E	78.7	5,422	F	89.3	5,764	E	69.9	5,324	F	91.2	5,713	E	79.6	5,492	F	91.9	5,711	E	78.0	5,378	F	90.8	5,679
112	Bundy Dr	Olympic Boulevard	F	214.1	7,921	F	135.2	7,811	F	214	7921	F	135	7811	F	214	7921	F	135	7811	F	214	7921	F	135	7811	F	198.6	7,758	F	132.8	7,824	F	200.2	7,762	F	133.3	7,800	F	201.1	7,796	F	133.6	7,859	F	193.1	7,706	F	127.4	7,752
113	Bundy Dr	Pico Boulevard	F	122.8	5,639	F	180.5	6,538	F	123	5639	F	181	6538	F	123	5639	F	181	6538	F	123	5639	F	181	6538	F	122.7	5,583	F	166.6	6,527	F	120.5	5,568	F	164.7	6,495	F	121.9	5,635	F	172.1	6,589	F	121.7	5,529	F	160.8	6,480

114	Centinela Ave (NB appr	Wilshire Boulevard	F	89.7	3,586	D	50.6	3,851	F	90	3586	D	51	3851	F	90	3586	D	51	3851	F	90	3586	D	51	3851	F	90	3586	D	51	3851	F	81.3	3,532	D	52.8	3,900	F	90	3586	D	51	3851	F	93.9	3,540	D	44.0	3,822
115	Las Palmas Ave	Hollywood Blvd	A	7.7	2,650	B	19.0	2,568	A	8	2650	B	19	2568	A	8	2650	B	19	2568	A	8	2650	B	19	2568	A	8	2650	B	19	2568	A	8	2650	B	19	2568	A	8.6	2,733	B	17.4	2,540	A	8.1	2,729	B	19.0	2,586
116	Highland Ave	Hollywood Blvd	F	131.7	5,451	F	150.0	5,702	F	132	5451	F	150	5702	F	132	5451	F	150	5702	F	132	5451	F	150	5702	F	132	5451	F	150	5702	F	132	5451	F	150	5702	F	130.4	5,484	F	139.4	5,610	F	132.4	5,432	F	142.3	5,650
117	Highland Ave	Selma Ave	C	21.2	3,871	C	28.8	4,218	C	21	3871	C	29	4218	C	21	3871	C	29	4218	C	21	3871	C	29	4218	C	21	3871	C	29	4218	C	21	3871	C	29	4218	C	20.1	3,918	C	28.5	4,167	C	20.6	3,886	C	29.0	4,206
118	Highland Ave	Sunset Boulevard	F	125.5	7,187	F	172.9	8,043	F	126	7187	F	173	8043	F	126	7187	F	173	8043	F	126	7187	F	173	8043	F	126	7187	F	173	8043	F	126	7187	F	173	8043	F	129.1	7,201	F	166.1	7,980	F	125.2	7,166	F	176.6	8,050
119	Highland Ave	Santa Monica Bouleva	F	150.0	6,730	F	149.6	7,353	F	150	6730	F	150	7353	F	150	6730	F	150	7353	F	150	6730	F	150	7353	F	150	6730	F	150	7353	F	150	6730	F	150	7353	F	152.3	6,786	F	149.7	7,276	F	154.7	6,866	F	147.9	7,249
120	Orange Dr	Hollywood Blvd	F	142.8	2,268	E	68.2	2,224	F	143	2268	E	68	2224	F	143	2268	E	68	2224	F	143	2268	E	68	2224	F	143	2268	E	68	2224	F	143	2268	E	68	2224	F	147.1	2,327	E	58.1	2,165	F	146.7	2,273	E	62.7	2,171
121	Orange Dr	Santa Monica Bouleva	B	10.4	3,175	C	21.1	3,577	B	10	3175	C	21	3577	B	10	3175	C	21	3577	B	10	3175	C	21	3577	B	10	3175	C	21	3577	B	10	3175	C	21	3577	A	9.8	3,184	C	20.3	3,562	A	9.7	3,198	C	21.4	3,569
122	La Brea Ave	Hollywood Blvd	F	168.4	5,453	F	120.7	5,121	F	168	5453	F	121	5121	F	168	5453	F	121	5121	F	168	5453	F	121	5121	F	168	5453	F	121	5121	F	168	5453	F	121	5121	F	156.1	5,394	F	117.4	5,106	F	145.4	5,324	F	119.4	5,076
123	La Brea Ave	Sunset Boulevard	F	204.5	6,707	F	254.7	6,738	F	205	6707	F	255	6738	F	205	6707	F	255	6738	F	205	6707	F	255	6738	F	205	6707	F	255	6738	F	205	6707	F	255	6738	F	190.3	6,615	F	240.1	6,735	F	192.4	6,616	F	226.1	6,800
124	La Brea Ave	Fountain Ave	F	190.9	5,848	F	80.6	5,949	F	191	5848	F	81	5949	F	191	5848	F	81	5949	F	191	5848	F	81	5949	F	191	5848	F	81	5949	F	191	5848	F	81	5949	F	194.3	5,845	F	84.9	5,976	F	186.1	5,746	F	82.2	5,937
125	La Brea Ave	Santa Monica Bouleva	F	162.2	6,220	F	206.8	6,991	F	162	6220	F	207	6991	F	162	6220	F	207	6991	F	162	6220	F	207	6991	F	162	6220	F	207	6991	F	162	6220	F	207	6991	F	152.7	6,197	F	199.6	6,949	F	161.1	6,176	F	203.9	6,922
126	La Brea Ave	Romaine St	C	26.4	3,703	F	95.8	4,616	C	26	3703	F	96	4616	C	26	3703	F	96	4616	C	26	3703	F	96	4616	C	26	3703	F	96	4616	C	26	3703	F	96	4616	C	28.8	3,736	F	97.4	4,637	C	30.3	3,728	F	94.6	4,601
127	La Brea Ave	Willoughby Ave	C	26.8	4,507	D	52.3	5,390	C	27	4507	D	52	5390	C	27	4507	D	52	5390	C	27	4507	D	52	5390	C	27	4507	D	52	5390	C	27	4507	D	52	5390	C	26.9	4,507	D	52.4	5,430	C	26.4	4,456	D	46.7	5,388
128	La Brea Ave	Melrose Ave	F	81.3	6,726	F	145.6	7,181	F	81	6726	F	146	7181	F	81	6726	F	146	7181	F	81	6726	F	146	7181	F	81	6726	F	146	7181	F	81	6726	F	146	7181	E	79.7	6,701	F	144.8	7,242	E	79.0	6,707	F	142.8	7,200
129	Formosa Ave	Santa Monica Bouleva	B	11.2	3,087	D	46.9	3,593	B	11	3087	D	47	3593	B	11	3087	D	47	3593	B	11	3087	D	47	3593	B	11	3087	D	47	3593	B	11	3087	D	47	3593	B	12.3	3,038	D	44.1	3,468	B	11.2	3,040	D	43.9	3,516
130	Genessee Avenue	Santa Monica Bouleva	A	7.7	2,666	A	6.6	3,164	A	8	2666	A	7	3164	A	8	2666	A	7	3164	A	8	2666	A	7	3164	A	8	2666	A	7	3164	A	8	2666	A	7	3164	A	7.9	2,704	A	5.9	3,059	A	6.1	2,640	A	6.2	3,078
131	Fairfax Ave	Sunset Boulevard	F	82.1	5,709	F	109.8	6,720	F	82	5709	F	110	6720	F	82	5709	F	110	6720	F	82	5709	F	110	6720	F	82	5709	F	110	6720	F	82	5709	F	110	6720	E	78.8	5,563	F	95.8	6,659	E	67.4	5,538	F	102.9	6,712
132	Fairfax Ave	Fountain Ave	F	126.1	4,926	F	128.8	5,410	F	126	4926	F	129	5410	F	126	4926	F	129	5410	F	126	4926	F	129	5410	F	126	4926	F	129	5410	F	126	4926	F	129	5410	F	121.4	4,862	F	123.7	5,404	F	117.7	4,804	F	131.4	5,459
133	Fairfax Ave	Norton Ave	A	6.0	2,678	B	16.5	3,133	A	6	2678	B	17	3133	A	6	2678	B	17	3133	A	6	2678	B	17	3133	A	6	2678	B	17	3133	A	6	2678	B	17	3133	A	5.9	2,644	B	18.3	3,165	A	6.0	2,594	B	18.1	3,167
134	Fairfax Ave	Santa Monica Bouleva	F	266.9	5,325	F	374.8	5,983	F	267	5325	F	375	5983	F	267	5325	F	375	5983	F	267	5325	F	375	5983	F	267	5325	F	375	5983	F	267	5325	F	375	5983	F	256.0	5,335	F	369.5	5,942	F	248.6	5,218	F	375.0	5,951
135	Fairfax Ave	Willoughby Ave	B	16.2	3,354	C	24.5	3,933	B	16	3354	C	25	3933	B	16	3354	C	25	3933	B	16	3354	C	25	3933	B	16	3354	C	25	3933	B	16	3354	C	25	3933	B	16.1	3,324	C	28.2	4,010	B	17.8	3,339	C	26.7	3,954
136	Fairfax Ave	Melrose Ave	D	50.0	5,498	D	55.0	5,761	D	50	5498	D	55	5761	D	50	5498	D	55	5761	D	50	5498	D	55	5761	D	50	5498	D	55	5761	D	50	5498	D	55	5761	D	47.9	5,426	D	54.7	5,743	D	44.7	5,396	D	52.7	5,746
137	Crescent Heights Blvd	Santa Monica Bouleva	E	73.9	5,032	F	93.2	5,263	E	74	5032	F	93	5263	E	74	5032	F	93	5263	E	74	5032	F	93	5263	E	74	5032	F	93	5263	E	74	5032	F	93	5263	E	74.9	5,146	F	95.0	5,256	E	61.7	5,067	F	96.5	5,290
138	Orlando Avenue	Beverly Blvd	C	30.6	3,196	F	98.2	3,973	C	25.7	3,197	E	76	3,971	C	32.5	3,209	E	79.6	3,932	C	28.90	3,191	E	74.80	3,944	C	28.80	3,187	E	76.9	3,930	C	29.00	3,192	E	78.6	3,925	C	27.8	3,173	E	78.9	4,017	C	28.7	3,183	E	73.3	3,919
139	Holloway Dr	Santa Monica Bouleva	C	30.6	3,513	C	30.2	4,182	C	31	3513	C	30	4182	C	31	3513	C	30	4182	C	31	3513	C	30	4182	C	31	3513	C	30	4182	C	31	3513	C	30	4182	C	32.2	3,535	C	28.1	4,166	C	30.7	3,483	C	29.1	4,199
140	La Cienega Boulevard	Sunset Boulevard	F	259.0	4,139	F	265.8	4,498	F	259	4139	F	266	4498	F	259	4139	F	266	4498	F	259	4139	F	266	4498	F	259	4139	F	266	4498	F	259	4139	F	266	4498	F	253.0	4,066	F	268.6	4,479	F	237.0	4,038	F	265.1	4,537
141	La Cienega Boulevard	Fountain Ave	F	94.4	3,833	F	347.0	4,421	F	94	3833	F	347	4421	F	94	3833	F	347	4421	F	94	3833	F	347	4421	F	94	3833	F	347	4421	F	94	3833	F	347	4421	F	80.8	3,746	F	348.5	4,388	F	89.7	3,796	F	349.1	4,472
142	La Cienega Boulevard	Holloway Drive	F	116.9	4,450	F	170.5	4,974	F	117	4450	F	171	4974	F	117	4450	F	171	4974	F	117	4450	F	171	4974	F	117	4450	F	171	4974	F	117	4450	F	171	4974	F	114.4	4,398	F	172.6	4,976	F	119.2	4,420	F	167.3	4,928
143	La Cienega Boulevard	Santa Monica Bouleva	F	211.3	6,176	F	250.0	7,143	F	211	6176	F	250	7143	F	211	6176	F	250	7143	F	211	6176	F	250	7143	F	211	6176	F	250	7143	F	211	6176	F	250	7143	F	196.6	6,116	F	246.2	7,101	F	193.4	6,151	F	246.6	7,186
144	La Cienega Boulevard	Melrose Ave	F	161.1	5,245	F	171.5	5,732	F	161	5245	F	172	5732	F	161	5245	F	172	5732	F	161	5245	F	172	5732	F	161	5245	F	172	5732	F	161	5245	F	172	5732	F	160.0	5,238	F	168.0	5,685	F	157.0	5,231	F	167.0	5,730
145	La Cienega Boulevard	Oakwood Ave	E	60.5	3,594	E	79.7	3,814	E	63.0	3,667	E	77.0	3,907	E	60.3	3,605	E	78.1	3,790	E	63.3	3,612	E	75.0	3,846	E	56.3	3,584	E	77.6	3,863	E	57.5	3,599	E	77.9	3,806	E	59.8	3,581	E	77.1	3,760	E	58.3	3,567	E	75.8	3,824
146	La Cienega Boulevard	Beverly Blvd	F	160.0	6,058	F	237.2	7,227	F	158.5	6,145	F	240.8	7,309	F	155.5	6,088	F	237.4	7,263	F	159.0	6,070	F	232.3	7,252	F	153.4	6,049	F	237.8	7,203	F	157.2	6,059	F	231.8	7,267	F	155.6	6,024	F	227.6	7,226	F	149.6	6,016	F	239.8	7,226
147	San Vicente Boulevard	Beverly Blvd	F	83.2	4,671	F	86.9	5,511	E	71.9	4,710	F	89.6	5,509	E	72.9	4,713	F	90.3	5,464	E	72.0	4,677	F	86.6	5,541	E	66.5	4,640	F	90.3	5,514	E	77.3	4,630	F	90.8	5,470	E	75.2	4,649	F	91.1	5,496	E	70.2	4,659	F	90.0	5,431
148	Holloway Dr	Sunset Boulevard	D	38.7	3,561	C	30.7	4,110	D	39	3561	C	31	4110	D	39	3561	C	31	4110	D	39	3561	C	31	4110	D	39	3561	C	31	4110	D	39	3561	C	31	4110	D	38.0	3,555	C	23.4	4,027	D	36.6	3,536	C	25.9	4,073
149	San Vicente Boulevard	Santa Monica Bouleva	F	231.1	5,479	F	239.5	6,795	F	231	5479	F	240	6795	F	231	5479	F	240	6795	F	231	5479	F	240	6795	F	231	5479	F	240	6795	F	231	5479	F	240	6795	F	235.4	5,435	F	242.8	6,828	F	227.7	5,389	F	232.6	6,744
150	San Vicente Boulevard	Melrose Ave	E	72.1	4,137	F	120.0	4,630	E	72	4137	F	120	4630	E	72	4137	F	120	4630	E	72	4137	F	120	4630	E	72	4137	F	120	4630	E	72	4137	F	120	4630	E	69.4	4,099	F	117.7	4,601	E	66.0	4,052	F	118.3	4,559
151	San Vicente Boulevard	Sunset Boulevard	F	256.6	4,716	F	378.2	5,019	F	257	4716	F	378	5019	F	257	4716	F	378	5019	F	257	4716	F	378	5019	F	257	4716	F	378	5019	F	257	4716	F	378	5019	F	249.3	4,670	F	368.3	4,985	F	248.4	4,699	F	354.4	4,915
152	San Vicente Boulevard	Cynthia Street	F	93.1	2,191	C	30.2	2,880	F	93	2191	C	30	2880	F	93	2191	C	30	2880	F	93	2191	C	30	2880	F	93	2191	C	30	2880	F	93	2191	C	30	2880	E	70.3	2,177	C	30.5	2,909	E	79.1	2,163	C	26.9	2,849
153	Robertson Blvd	Santa Monica Bouleva	F	143.0	4,209	F	192.4	4,768	F	143	4209	F	192	4768	F	143	4209	F	192	4768	F	143	4209	F	192	4768	F	143	4209	F	192	4768	F	143	4209	F	192	4768	F	139.3	4,147	F	196.0	4,792	F	127.7	4,096	F	192.9	4,768
154	Robertson Blvd	Beverly Blvd	F	124.4	3,816	F	107.4	4,212	F	121.8	3,842	F	100.5	4,217	F	121.3	3,838	F	99.7	4,183	F	119.2	3,836	F	102.40	4,221	F	119.20	3,814	F	99.8	4,230	F	116.5	3,800	F	97.9	4,180	F	122.2	3,830	F	100.1	4,207	F	122.6	3,835	F	99.4	4,191
155	Doheny Dr	Santa Monica Bouleva	F	373.1	4,406	F	550.5	5,224	F	373	4406	F	551	5224	F	373	4406	F	551	5224	F	373	4406	F	551	5224	F	373	4406	F	551	5224	F	373	4406	F	551	5224	F	363.1	4,378	F	540.1	5,236	F	349.7	4,317	F	536.0	5,213
156	Yale Street	Wilshire Boulevard	A	10.0	3,287	C	23.8	3,800	A	10	3287	C	24	3800	A	10	3287	C	24	3800	A	10	3287	C	24	3800	A	10	3287	C	24	3800	A	9.4	3,222	C	25.6	3,847	A	10	3287	C	24	3800	A	8.7	3,174	C	23.8	3,810
157	Yale Street	Santa Monica Bouleva	F	143.6	3,398	F	201.1	3,828	F	144	3398	F	201	3828	F	144	3398	F	201	3828	F	144	3398	F	201	3828	F	144	3398	F	201	3828	F	145.7	3,306	F	204.9	3,883	F	144	3398	F	201	3828	F	139.6	3,291	F	197.5	3,815
158	26th Street	Montana Avenue	C	20.1	2,406	C	28.2	2,666	C	20	2406	C	28	2666	C	20	2406	C	28	2666	C	20	2406	C	28	2666	C	20	2406	C	28	2666	C	20.2	2,381	C	27.6	2,655	C	20	2406	C	28	2666	C	20.5	2,405	C	28.4	2,666
159	26th Street	Wilshire Boulevard	F	206.2	4,429	F	226.8	4,943	F	206	4429	F	227	4943	F	206	4429	F	227	4943	F	206	4429	F	227	4943	F	206	4429	F	227	4943	F	196.3	4,379	F	230.7	5,048	F	206	4429	F	227	4943	F	187.6	4,306	F	226.8	4,988
160	26th Street	Arizona Ave	B	19.2	2,196	C	22.5	2,389	B	19	2196	C	23	2389	B	19	2196	C	23	2389	B	19	2196	C	23	2389	B	19	2196	C	23	2389	B	17.3	2,143	C	25.8	2,475	B	19	2196	C	23	2389	B	18.3	2,135	C	23.6	2,417
161	26th Street	Santa Monica Bouleva	E	60.6	4,096	E	62.6	4,347	E	61	4096	E	63	4347	E	61	4096	E	63	4347	E	61	4096	E	63	4347	E	61	4096	E	63	4347	E	57.7	4,059	E	60.8	4,374	E	61	4096	E	63	4347	E	61.6	4,045	E	58.8	4,322
162	20th Street	Wilshire Boulevard	D	40.8	4,066	F	98.3	4,512	D	41	4066	F	98	4512	D	41	4066	F	98	4512	D	41	4066	F	98	4512	D	41	4066	F	98	4512	D	38.8	4,035	F	100.3	4,521	D	41	4066	F	98	4512	D	39.5	3,990	F	102.7	4,539
163	20th Street	Santa Monica Bouleva	E	55.2	4,460	F	89.0	4,765	E	55	4460	F	89	4765	E	55	4460	F	89	4765	E	55	4460	F	89	4765	E	55	4460	F	89	4765	E	56.4	4,430	F	92.9	4,794	E	55	4460	F	89	4765	E	59.6	4,426	F	91.8	4,752
164	17th Street	Wilshire Boulevard	D	47.2	3,286	D	35.2	3,604	D	47	3286	D	35	3604	D	47	3286	D	35	3604	D	47	3286	D	35	3604	D	47	3286	D	35	3604	D	41.4	3,199	D	37.7	3,598	D	47	3286	D	35	3604	D	43.7	3,209	D	38.8	3,610
165	17th Street	Arizona Ave	C	21.6	1,521	C	28.6	1,604	C	22	1521	C	29	1604	C	22	1521	C	29	1604	C	22	1521	C	29	1604	C	22	1521	C	29	1604	C	22.5	1,492	C	28.8	1,593	C	22	1521	C	29	1604	C	21.8	1,493	C	22.0	1,561
166	17th Street	Santa Monica Bouleva	F	87.0	3,302	F	183.7	3,705	F	87	3302	F	184	3705	F	87	3302	F	184	3705	F	87	3302	F	184	3705	F	87	3302	F	184	3705	E	55.7	3,215	F	188.3	3,651	F	87	3302	F	184	3705	E	63.6	3,238	F	184.9	3,713
167	16th Street (unsignalize	Wilshire Boulevard	F	**	2,634	F	**	3,124	F	**	2634	F	**	3124	F	**	2634	F	**	3124	F	**	2634	F	**	3124	F	**	2634	F	**	3124	F	>200	2,597	F	>200	3,079	F	**	2634	F	**	3124	F	>200	2,567	F	>200	3,104
168	14th Street	Wilshire Boulevard	C	21.3	2,868	C	21.4	3,609	C	21	2868	C	21	3609	C	21	2868	C	21	3609	C	21	2868	C	21	3609	C	21	2868	C	21	3609	C	21.1	2,830	C	20.8	3,580	C	21	2868	C	21	3609	C	21.5	2,801	C	20.2	3,598
169	14th Street	Arizona Ave	B	13.1	1,342	B	14.9	1,698	B	13	1342	B	15	1698	B	13	1342	B	15	1698	B	13	1342	B	15	1698	B	13	1342	B	15	1698	B	12.9	1,328	B	15.1	1,690	B	13	1342	B	15	1698	B	12.7	1,317	B	14.9	1,683
170	14th Street	Santa Monica Bouleva	B	19.2	2,618	D	39.2	3,310	B	19	2618	D	39	3310	B	19	2618	D	39	3310	B	19	2618	D	39	3310	B	19	2618	D	39	3310	B	19.4	2,616	D	45.1	3,375	B	19	2618	D	39	3310	B	17.5	2,580	D	40.8	3,288
171	11th Street	Wilshire Boulevard	C	32.1	3,190	C	29.1	3,667	C	32	3190	C	29	3667	C	32	3190	C	29	3667	C	32	3190	C	29	3667	C	32	3190	C	29	3667	C	29.4	3,120	C	29.0	3,678	C	32	3190	C	29	3667	C	30.5	3,117	C	28.4	3,654
172	Lincoln Boulevard	Wilshire Boulevard	F	193.6	3,618	F	221.9	3,943	F	194	3618	F	222	3943	F	194	3618	F	222	3943	F	194	3618	F	222	3943	F	194	3618	F	222	3943	F	178.8	3,630	F	211.8	3,822	F	194	3618	F	222	3943	F	176.2	3,542	F	212.6	3,893
173	Lincoln Boulevard	Santa Monica Bouleva	C	32.5	3,256	E	62.2	3,963	C	33	3256	E	62	3963	C	33	3256	E	62	3963	C	33	3256	E	62	3963	C	33	3256	E	62	3963	C	32.4	3,297	E	61.8	3,887	C	33	3256	E	62	3963	C	32.3	3,242	E	62.3	3,971
174	7th Street	Wilshire Boulevard	C	31.4	2,681	E	63.0	3,340	C	31	2681	E	63	3340	C	31	2681	E	63	3340	C	31	2681	E	63	3340	C	31	2681	E	63	3340	C	30.9	2,631	E	63.9	3,300	C	31	2681	E	63	3340	C	34.3	2,684	E	65.4	3,315
175	7th Street	Santa Monica Bouleva	C	20.4	1,969	C	25.5	2,565	C	20	1969	C	26	2565	C	20	1969	C	26	2565	C	20	1969	C	26	2565	C	20	1969	C	26	2565	C	20.4	1,931	C	25.9	2,573	C	20	1969	C	26	2565	C	22.1	2,007	C	24.5	2,569
176	5th Street	Wilshire Boulevard	B	17.8	2,221	B	20.0	2,854	B	18	2221	B	20	2854	B	18	2221	B	20	2854	B	18	2221	B	20	2854	B	18	2221	B	20	2854	B	18.4	2,204	B	19.7	2,817	B	18	2221	B	20	2854	B	20.0	2,209	B	19.8	2,850
177	4th Street	California Ave	B	10.9	1,024	B	18.3	1,574	B	11	1024	B	18	1574	B	11	1024	B	18	1574	B	11	1024	B	18	1574	B	11	1024	B	18	1574	B	10.6	1,010	B	20.0	1,598	B	11	1024	B	18	1574	B	10.6	1,032	B	18.7	1,555
178	4th Street	Wilshire Boulevard	C	25.4	2,563	C	25.5	3,130	C	25	2563	C	26	3130	C	25	2563	C	26	3130	C	25	2563	C	26	3130	C	25	2563	C	26	3130	C	24.9	2,519	C	26.0	3,047	C	25	2563	C	26	3130	C	25.6	2,493	C	24.4	2,998
179	4th Street	Arizona Ave	B	13.8	1,578	B	18.5	2,216	B	14	1578	B	19	2216	B	14	1578	B	19	2216	B	14	1578	B	19	2216	B	14	1578	B	19	2216	B	13.9	1,558	B	18.2	2,170	B	14	1578	B	19	2216	B	14.1	1,574	B	18.1	2,183
180	4th Street	Santa Monica Bouleva	E	74.9	1,948	F	145.9	2,579	E	75	1948	F	146	2579	E	75	1948	F	146	2579	E	75	1948	F	146	2579	E	75	1948	F	146	2579	E	69.4	1,932	F	138.9	2,580	E	75	1948	F	146	2579	E	56.8	1,906	F	127.7	2,568
181	3rd Street	Wilshire Boulevard	B	11.1	906	A	9.7	1,749	B	11	906	A	10	1749	B	11	906	A	10	1749	B	11	906	A	10	1749	B	11	906	A	10	1749	B	11.1	881	A	9.7	1,822	B	11	906	A	10	1749	B	11.1	853	A	9.7	1,767
182	Ocean Ave	California Ave	D	38.0	2,315	E	57.4	2,738	D	38	2315	E	57	2738	D	38	2315	E	57	2738	D	38	2315	E	57	2738	D	38	2315	E	57	2738	D	39.4	2,351	E	61.2	2,822	D	38	2315	E	57	2738	D	36.7	2,325	E	61.4	2,787
183	Ocean Ave	Wilshire Boulevard	B	11.6	2,220	B	18.8	2,640	B	12	2220	B	19	2640	B	12	2220	B	19	2640	B	12	2220	B	19	2640	B	12	2220	B	19	2640	B	10.1	2,221	B	17.7	2,640	B	12	2220	B	19	2640	B	10.6	2,229	B	17.6	2,596
184	Ocean Ave	Santa Monica Bouleva	A	6.6	1,744	B	11.5	2,488	A	7	1744	B	12	2488	A	7	1744	B	12	2488	A	7	1744	B	12	2488	A	7	1744	B	12	2488	A	6.7	1,778	B	11.6	2,522	A	7	1744	B	12	2488	A	6.6	1,765	B	13.0	2,535
185	Veteran Ave	Ohio Ave	F	119.4	3,053	F	146.2	3,283	F	119	3053	F	146	3283	F	119	3053	F	146	3283	F	114.4	2,998	F	144.3	3,263	F	118.4	2,958	F	149.4	3,262	F	108.9	2,945	F	148.9	3,258	F	113.9	3,007	F	148.0	3,264	F	123.3	2,982	F	146.2	3,214
186	Veteran Ave	Santa Monica Blvd	F	258.7	6,027	F	209.0	6,198	F	259	6027	F	209	6198	F	259	6027	F	209	6198	F	219.0	6,047	F	197.9	6,220	F	222.1	5,946	F	187.7	6,261	F	225.4	5,951	F	193.9	6,181	F	233.4	5,957	F	204.6	6,296	F	234.6	5,949	F	188.5	6,205
187	Sepulveda Blvd	Ohio Ave	F	219.6	4,838	F	152.0	5,020	F	220	4838	F	152	5020	F	220	4838	F	152	5020	F	211.3	4,604	F	154.0	4,976	F	208.7	4,793	F	151.9	4,968	F	182.2	4,615	F	156.1	5,032	F	205.0	4,741	F	155.4	4,994	F	182.8	4,712	F	156.7	4,984
188	Sepulveda Blvd	Santa Monica Blvd	F	101.9	6,888	F	148.0	7,026	F	102	6888	F	148	7026	F	102	6888	F	148	7026	F	88.9	6,752	F	132.1	6,986	F	92.7	6,821	F	140.7	7,058	F	82.5	6,722	F	138.7	6,960	F	89.1	6,784	F	131.6	7,016	F	95.8	6,752	F	143.7	6,995
189	I-405 NB Ramps	Santa Monica Blvd	D	47.2	6,283	F	108.5	7,138	D	47	6283	F	109	7138	D	47	6283	F	109	7138	D	46.8	6,301	F	110.6	7,126	D	46.3	6,296	F	98.9	7,100	D	47.2	6,313	F	110.2	7,160	D	48.1	6,236	F	108.1	7,139	D	45.6	6,257	F	111.5	7,133
190	I-405 SB Ramps	Santa Monica Blvd	E	66.5	6,343	C	34.4	5,790	E	67	6343	C	34	5790	E	67	6343	C	34	5790	E	55.7	6,256	C	35.0	5,798	E	70.5	6,407	C	33.5	5,706	E	57.0	6,225	C	34.9	5,892	E	55.8	6,279	C	34.7	5,888	E	65.7	6,283	C	33.2	5,647
191	Sawtelle	Ohio Ave	F	178.0	2,924	F	392.4	2,984	F	178	2924	F	392	2984	F	178	2924	F	392	2984	F	150.1	2,892	F	347.9	3,073	F	178.7	2,912	F	359.3	3,052	F	157.2	2,842	F	370.5	3,150	F	166.4	2,896	F	396.3	3,043	F	169.3	2,962	F	395.8	3,084
192	Federal	Santa Monica Blvd	C	24.7	4,300	D	38.8	4,486	C	25	4300	D	39	4486	C	25	4300	D	39	4486	C	25	4300	D	39	4486	B	19.1	4,213	D	36.3	4,600	B	19.1	4,205	D	45.1	4,555	B	19.3	4,229	D	40.9	4,555	B	18.8	4,208	D	35.7	4,505
208	Bundy Dr (SB)	San Vicente Blvd			4,767			4,958	0	0	4767	0	0	4958	0	0	4767	0	0	4958	0	0	4767	0	0	4958			4,758			5,006			4,681			5,002			4,674			4,979			4,664			4,967
230	Genessee Av (NB)	Santa Monica Blvd			2,606			3,115	0	0	2606	0	0	3115	0	0	2606	0	0	3115	0	0	2606	0	0	3115	0	0	2606	0	0	3115	0	0	2606	0	0	3115			2,637			3,009			2,579			3,028

Appendix C

CAL3QHC

Input/Output Files

Site 1 – 26th & Wilshire
Input Files

```
Site 1 26th & Wilshire (S1EXAM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Existing AM                       24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1111 3.3  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1071 3.3  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        58       2.0 1071   20.5 1287 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      40 3.3  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        55       2.0   40   20.5  180 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1198 3.3  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1302 3.3  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1181 3.3  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        56       2.0 1181   20.5 1190 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     121 3.3  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
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        90        50       2.0  121   20.5  168 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1248 3.3  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     723 3.3  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     591 3.3  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  591   20.5 1242 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     132 3.3  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        50       2.0  132   20.5  336 1 3
  1
SB        26 LT     AG   672.   845.  1384.   114.     688 3.3  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     563 3.3  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     485 3.3  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  485   20.5 1245 1 3
  1
NB        26 L      AG   818.   710.   705.   832.      78 3.3  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        53       2.0   78   20.5  252 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     565 3.3  0.  32   30.
1.0   04 1000.   0Y  5  0 72
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Site 1 26th & Wilshire (S1EXPM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Existing PM                       24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1229 3.3  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1142 3.3  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        59       2.0 1142   20.5 1285 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      87 3.3  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        54       2.0   87   20.5  182 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1326 3.3  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1384 3.3  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1181 3.3  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        57       2.0 1181   20.5 1196 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     127 3.3  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
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        90        52       2.0  127   20.5  176 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1479 3.3  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     694 3.3  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     555 3.3  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  555   20.5 1236 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     139 3.3  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        50       2.0  139   20.5  252 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     656 3.3  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     727 3.3  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     616 3.3  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  616   20.5 1239 1 3
  1
NB        26 L      AG   818.   710.   705.   832.     111 3.3  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0  111   20.5  358 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     700 3.3  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1NBAM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 No Build AM                       24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1288 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1248 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        59       2.0 1248   4.1 1290 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      40 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        55       2.0   40   4.1  182 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1363 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1617 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1496 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        56       2.0 1496   4.1 1190 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     121 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
```

```
        90        51       2.0  121   4.1  170 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1515 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     817 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     715 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  715   4.1 1242 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     102 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        49       2.0  102   4.1  166 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     812 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     707 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     629 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        56       2.0  629   4.1 1245 1 3
  1
NB        26 L      AG   818.   710.   705.   832.      78 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0   78   4.1  172 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     739 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1NBPM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 No Build PM                       24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1495 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1408 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        57       2.0 1408   4.1 1289 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      87 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        55       2.0   87   4.1  182 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1726 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1697 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1570 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        56       2.0 1570   4.1 1196 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     127 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
```

```
        90        51       2.0  127   4.1  169 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1707 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     830 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     661 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        57       2.0  661   4.1 1236 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     169 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        51       2.0  169   4.1  174 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     762 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     921 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     810 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  810   4.1 1239 1 3
  1
NB        26 L      AG   818.   710.   705.   832.     111 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0  111   4.1  177 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     748 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1B3AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Build Alt3 AM                     24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1275 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1235 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        59       2.0 1235   4.1 1288 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      40 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        55       2.0   40   4.1  182 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1352 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1613 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1492 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        56       2.0 1492   4.1 1190 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     121 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
```

```
        90        51       2.0  121   4.1  170 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1491 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     822 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     714 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  714   4.1 1208 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     108 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        50       2.0  108   4.1  198 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     808 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     669 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     591 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  591   4.1 1210 1 3
  1
NB        26 L      AG   818.   710.   705.   832.      78 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0   78   4.1  172 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     725 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1B3PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Build Alt3 PM                     24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1509 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1422 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        57       2.0 1422   4.1 1287 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      87 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        53       2.0   87   4.1  175 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1766 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1713 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1586 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        56       2.0 1586   4.1 1196 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     127 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
```

```
        90        51       2.0  127   4.1  169 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1728 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     852 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     680 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        57       2.0  680   4.1 1200 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     169 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        52       2.0  169   4.1  174 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     765 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     974 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     863 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        58       2.0  863   4.1 1204 1 3
  1
NB        26 L      AG   818.   710.   705.   832.     111 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0  111   4.1  177 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     793 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1B5AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Build Alt5 AM                     24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1254 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1214 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        59       2.0 1214   4.1 1289 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      40 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        55       2.0   40   4.1  182 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1331 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1560 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1439 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        56       2.0 1439   4.1 1190 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     121 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
```

```
        90        50       2.0  121   4.1  170 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1550 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     823 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     715 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        56       2.0  715   4.1 1196 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     108 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        50       2.0  108   4.1  198 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     812 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     669 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     591 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        57       2.0  591   4.1 1199 1 3
  1
NB        26 L      AG   818.   710.   705.   832.      78 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        52       2.0   78   4.1  172 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     707 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 1 26th & Wilshire (S1B5PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  967.      615.       5.0
SE 164 S                  874.      710.       5.0
SE 82 S                   816.      771.       5.0
SE CNR                    768.      826.       5.0
SE 82 E                   819.      886.       5.0
SE 164 E                  877.      944.       5.0
SE MID E                  996.     1059.       5.0
NE MID E                  916.     1134.       5.0
NE 164 E                  800.     1020.       5.0
NE 82 E                   741.      962.       5.0
NE CNR                    680.      915.       5.0
NE 82 N                   628.      964.       5.0
NE 164 N                  570.     1023.       5.0
NE MID N                  454.     1143.       5.0
NW MID N                  391.     1100.       5.0
NW 164 N                  514.      974.       5.0
NW 82 N                   571.      914.       5.0
NW CNR                    621.      855.       5.0
NW 82 W                   570.      797.       5.0
NW 164 W                  512.      740.       5.0
NW MID W                  412.      643.       5.0
SW MID W                  484.      558.       5.0
SW 164 W                  589.      658.       5.0
SW 82 W                   649.      715.       5.0
SW CNR                    707.      765.       5.0
SW 82 S                   763.      714.       5.0
SW 164 S                  820.      656.       5.0
SW MID S                  919.      554.       5.0
Site 1 Build Alt5 PM                     24  1   0
  1
EB        Wil AP    AG   -15.   139.   583.   699.    1492 0.8  0.  44   30.
  1
EB        Wil T+R   AG   584.   699.   715.   824.    1405 0.8  0.  44   30.
  2
EB        Wil T+R Q AG   672.   783.   587.   701.      0.  24   2
        90        57       2.0 1405   4.1 1289 1 3
  1
EB        Wil LT    AG   569.   717.   698.   843.      87 0.8  0.  32   30.
  2
EB        Wil LT Q  AG   654.   800.   574.   722.      0.  12   1
        90        53       2.0   87   4.1  171 1 3
  1
EB        Wil DP    AG   715.   824.  1421.  1528.    1722 0.8  0.  44   30.
  1
WB        Wil AP    AG  1393.  1557.   810.   982.    1720 0.8  0.  44   30.
  1
WB        Wil T+R   AG   806.   986.   684.   868.    1593 0.8  0.  56   30.
  2
WB        Wil T+R Q AG   717.   900.   803.   984.      0.  36   3
        90        55       2.0 1593   4.1 1196 1 3
  1
WB        Wil LT    AG   824.   966.   707.   850.     127 0.8  0.  32   30.
  2
WB        Wil LT Q  AG   737.   880.   821.   964.      0.  12   1
```

```
        90        50       2.0  127   4.1  164 1 3
  1
WB        Wil DP    AG   687.   864.   -35.   163.    1718 0.8  0.  44   30.
  1
SB        26 AP     AG   553.   971.    -6.  1547.     846 0.8  0.  32   30.
  1
SB        26 T+R    AG   549.   968.   670.   841.     677 0.8  0.  44   30.
  2
SB        26 T+R Q  AG   633.   880.   551.   966.      0.  24   2
        90        57       2.0  677   4.1 1190 1 3
  1
SB        26 LT     AG   563.   978.   679.   856.     169 0.8  0.  32   30.
  2
SB        26 LT Q   AG   645.   891.   565.   976.      0.  12   1
        90        52       2.0  169   4.1  175 1 3
  1
SB        26 DP     AG   672.   845.  1384.   114.     778 0.8  0.  32   30.
  1
NB        26 AP     AG   829.   716.  1410.   138.     930 0.8  0.  32   30.
  1
NB        26 T+R    AG   832.   719.   715.   846.     834 0.8  0.  44   30.
  2
NB        26 T+R Q  AG   759.   798.   829.   722.      0.  24   2
        90        58       2.0  834   4.1 1193 1 3
  1
NB        26 L      AG   818.   710.   705.   832.      96 0.8  0.  32   30.
  2
NB        26 L Q    AG   747.   787.   817.   711.      0.  12   1
        90        54       2.0   96   4.1  180 1 3
  1
NB        26 DP     AG   712.   843.    13.  1565.     770 0.8  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

Site 1 – 26th & Wilshire
Output Files

```
1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 1 26th & Wilshire (S1EXAM.DAT)                 RUN: Site 1 Existing AM
      DATE: 03/19/2010   TIME: 08:31:52.74


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)         *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*---------------------------------------*---------------------------------------------------------
       1. EB        Wil AP    *    -15.0     139.0     583.0     699.0 *     819.    47. AG   1111.   3.3    .0 44.0
       2. EB        Wil T+R   *    584.0     699.0     715.0     824.0 *     181.    46. AG   1071.   3.3    .0 44.0
       3. EB        Wil T+R Q *    672.0     783.0    -500.4    -348.0 *    1629.   226. AG     71. 100.0    .0 24.0 1.34  82.8
       4. EB        Wil LT    *    569.0     717.0     698.0     843.0 *     180.    46. AG     40.   3.3    .0 32.0
       5. EB        Wil LT Q  *    654.0     800.0     643.5     789.8 *      15.   226. AG     34. 100.0    .0 12.0  .65    .7
       6. EB        Wil DP    *    715.0     824.0    1421.0    1528.0 *     997.    45. AG   1198.   3.3    .0 44.0
       7. WB        Wil AP    *   1393.0    1557.0     810.0     982.0 *     819.   225. AG   1302.   3.3    .0 44.0
       8. WB        Wil T+R   *    806.0     986.0     684.0     868.0 *     170.   226. AG   1181.   3.3    .0 56.0
       9. WB        Wil T+R Q *    717.0     900.0     868.0    1047.5 *     211.    46. AG    103. 100.0    .0 36.0  .99  10.7
      10. WB        Wil LT    *    824.0     966.0     707.0     850.0 *     165.   225. AG    121.   3.3    .0 32.0
      11. WB        Wil LT Q  *    737.0     880.0    1187.5    1330.5 *     637.    45. AG     31. 100.0    .0 12.0 1.81  32.4
      12. WB        Wil DP    *    687.0     864.0     -35.0     163.0 *    1006.   226. AG   1248.   3.3    .0 44.0
      13. SB        26 AP     *    553.0     971.0      -6.0    1547.0 *     803.   316. AG    723.   3.3    .0 32.0
      14. SB        26 T+R    *    549.0     968.0     670.0     841.0 *     175.   136. AG    591.   3.3    .0 44.0
      15. SB        26 T+R Q  *    633.0     880.0     570.0     946.1 *      91.   316. AG     68. 100.0    .0 24.0  .71   4.6
      16. SB        26 LT     *    563.0     978.0     679.0     856.0 *     168.   136. AG    132.   3.3    .0 32.0
      17. SB        26 LT Q   *    645.0     891.0     585.1     954.6 *      87.   317. AG     31. 100.0    .0 12.0  .99   4.4
      18. SB        26 LT     *    672.0     845.0    1384.0     114.0 *    1020.   136. AG    688.   3.3    .0 32.0
      19. NB        26 AP     *    829.0     716.0    1410.0     138.0 *     820.   135. AG    563.   3.3    .0 32.0
      20. NB        26 T+R    *    832.0     719.0     715.0     846.0 *     173.   317. AG    485.   3.3    .0 44.0
      21. NB        26 T+R Q  *    759.0     798.0     810.1     742.5 *      75.   137. AG     70. 100.0    .0 24.0  .60   3.8
      22. NB        26 L      *    818.0     710.0     705.0     832.0 *     166.   317. AG     78.   3.3    .0 32.0
      23. NB        26 L Q    *    747.0     787.0     773.7     758.0 *      39.   137. AG     32. 100.0    .0 12.0  .85   2.0
      24. NB        26 DP     *    712.0     843.0      13.0    1565.0 *    1005.   316. AG    565.   3.3    .0 32.0
1
                                                                                                                PAGE  2
      JOB: Site 1 26th & Wilshire (S1EXAM.DAT)                 RUN: Site 1 Existing AM
      DATE: 03/19/2010   TIME: 08:31:52.74

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R Q *      90       58       2.0      1071       1287      20.50      1        3
       5. EB        Wil LT Q  *      90       55       2.0        40        180      20.50      1        3
       9. WB        Wil T+R Q *      90       56       2.0      1181       1190      20.50      1        3
      11. WB        Wil LT Q  *      90       50       2.0       121        168      20.50      1        3
      15. SB        26 T+R Q  *      90       56       2.0       591       1242      20.50      1        3
      17. SB        26 LT Q   *      90       50       2.0       132        336      20.50      1        3
      21. NB        26 T+R Q  *      90       57       2.0       485       1245      20.50      1        3
      23. NB        26 L Q    *      90       53       2.0        78        252      20.50      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       967.0      615.0       5.0    *
      2. SE 164 S             *       874.0      710.0       5.0    *
      3. SE 82 S              *       816.0      771.0       5.0    *
      4. SE CNR               *       768.0      826.0       5.0    *
      5. SE 82 E              *       819.0      886.0       5.0    *
      6. SE 164 E             *       877.0      944.0       5.0    *
      7. SE MID E             *       996.0     1059.0       5.0    *
      8. NE MID E             *       916.0     1134.0       5.0    *
      9. NE 164 E             *       800.0     1020.0       5.0    *
     10. NE 82 E              *       741.0      962.0       5.0    *
     11. NE CNR               *       680.0      915.0       5.0    *
     12. NE 82 N              *       628.0      964.0       5.0    *
     13. NE 164 N             *       570.0     1023.0       5.0    *
     14. NE MID N             *       454.0     1143.0       5.0    *
     15. NW MID N             *       391.0     1100.0       5.0    *
     16. NW 164 N             *       514.0      974.0       5.0    *
     17. NW 82 N              *       571.0      914.0       5.0    *
     18. NW CNR               *       621.0      855.0       5.0    *
     19. NW 82 W              *       570.0      797.0       5.0    *
     20. NW 164 W             *       512.0      740.0       5.0    *
     21. NW MID W             *       412.0      643.0       5.0    *
     22. SW MID W             *       484.0      558.0       5.0    *
     23. SW 164 W             *       589.0      658.0       5.0    *
     24. SW 82 W              *       649.0      715.0       5.0    *
     25. SW CNR               *       707.0      765.0       5.0    *
     26. SW 82 S              *       763.0      714.0       5.0    *
     27. SW 164 S             *       820.0      656.0       5.0    *
     28. SW MID S             *       919.0      554.0       5.0    *
1
                                                                                                                PAGE  3
      JOB: Site 1 26th & Wilshire (S1EXAM.DAT)                 RUN: Site 1 Existing AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

  WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .2    .4    .2    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .3    .0    .0
   5.  *    .0    .0    .2    .4    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .3    .1    .0
  10.  *    .0    .0    .2    .2    .4    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .3    .2    .1    .0
  15.  *    .0    .0    .1    .2    .5    .3    .3    .0    .0    .0    .0    .0    .0    .0    .1    .1    .3    .2    .1    .0
  20.  *    .0    .0    .1    .3    .5    .4    .3    .0    .0    .0    .0    .0    .0    .0    .1    .1    .3    .2    .1    .0
  25.  *    .0    .0    .1    .4    .5    .4    .3    .0    .0    .0    .0    .0    .0    .0    .1    .1    .3    .2    .1    .0
  30.  *    .0    .0    .1    .4    .3    .3    .3    .0    .0    .0    .0    .0    .0    .0    .1    .1    .3    .2    .0    .0
  35.  *    .0    .0    .1    .2    .3    .3    .3    .1    .1    .2    .1    .0    .0    .0    .1    .1    .3    .3    .0    .0
  40.  *    .0    .0    .0    .2    .3    .3    .2    .1    .1    .3    .1    .0    .0    .0    .1    .1    .3    .2    .1    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .1    .2    .4    .3    .0    .0    .0    .1    .1    .3    .3    .1    .2
  50.  *    .0    .0    .0    .1    .1    .1    .1    .1    .3    .5    .5    .0    .0    .0    .1    .1    .3    .5    .3    .2
  55.  *    .0    .0    .0    .1    .1    .1    .1    .3    .5    .6    .5    .0    .0    .0    .1    .1    .3    .5    .3    .3
  60.  *    .0    .0    .0    .0    .0    .0    .0    .3    .5    .6    .6    .1    .0    .0    .1    .1    .4    .4    .3    .2
  65.  *    .0    .0    .0    .0    .0    .0    .0    .3    .5    .8    .6    .2    .0    .0    .1    .1    .4    .4    .3    .1
  70.  *    .0    .0    .0    .0    .0    .0    .0    .3    .7    .8    .5    .2    .0    .0    .1    .1    .4    .4    .2    .1
  75.  *    .0    .0    .0    .0    .0    .0    .0    .3    .6    .7    .5    .1    .0    .0    .1    .1    .4    .5    .1    .3
  80.  *    .0    .0    .0    .0    .0    .0    .0    .3    .6    .7    .5    .1    .0    .0    .1    .2    .4    .5    .1    .3
  85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .6    .5    .1    .0    .0    .1    .2    .4    .3    .1    .3
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .4    .1    .1    .0    .1    .1    .4    .3    .1    .3
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .4    .1    .1    .0    .1    .1    .4    .2    .2    .3
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .4    .2    .1    .0    .1    .1    .3    .2    .3    .2
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .4    .2    .1    .0    .1    .2    .3    .1    .3    .2
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .3    .2    .1    .0    .1    .2    .3    .2    .3    .2
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .3    .2    .1    .0    .1    .2    .3    .2    .3    .2
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .3    .2    .1    .0    .1    .2    .3    .2    .3    .2
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .3    .2    .1    .0    .1    .2    .2    .2    .3    .2
 130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .2    .1    .0    .0    .1    .2    .2    .2    .3    .2
 135.  *    .1    .1    .0    .1    .0    .0    .0    .2    .5    .5    .2    .0    .0    .1    .0    .2    .2    .3    .3    .2
 140.  *    .1    .1    .1    .1    .0    .0    .0    .2    .5    .5    .2    .0    .1    .1    .0    .1    .1    .2    .3    .3
 145.  *    .1    .2    .2    .2    .0    .0    .0    .2    .5    .5    .2    .1    .1    .1    .0    .0    .1    .2    .3    .3
 150.  *    .2    .2    .2    .3    .0    .0    .0    .2    .5    .5    .2    .1    .2    .1    .0    .0    .1    .3    .3    .3
 155.  *    .2    .2    .1    .3    .0    .0    .0    .2    .5    .5    .2    .1    .2    .1    .0    .0    .0    .3    .2    .3
 160.  *    .2    .2    .1    .4    .0    .0    .0    .2    .5    .5    .2    .1    .2    .1    .0    .0    .2    .3    .2    .3
 165.  *    .2    .2    .1    .4    .0    .0    .0    .2    .6    .5    .2    .1    .2    .2    .0    .0    .2    .3    .2    .3
 170.  *    .2    .2    .1    .4    .0    .0    .0    .2    .6    .5    .2    .2    .2    .2    .0    .0    .2    .3    .2    .3
 175.  *    .2    .2    .3    .3    .0    .0    .0    .2    .5    .5    .3    .3    .2    .2    .0    .0    .2    .2    .2    .3
 180.  *    .1    .2    .2    .3    .0    .0    .0    .2    .5    .5    .3    .4    .2    .2    .0    .0    .2    .2    .2    .3
 185.  *    .1    .1    .2    .2    .0    .0    .0    .2    .6    .4    .5    .4    .2    .2    .0    .1    .2    .2    .2    .3
 190.  *    .1    .1    .2    .2    .1    .0    .0    .2    .6    .4    .3    .4    .2    .1    .0    .1    .2    .2    .3    .3
 195.  *    .1    .1    .2    .2    .1    .0    .0    .3    .6    .4    .3    .4    .2    .1    .0    .1    .2    .2    .4    .4
 200.  *    .1    .1    .2    .2    .1    .0    .0    .3    .5    .5    .3    .4    .2    .1    .0    .1    .2    .2    .4    .4
 205.  *    .1    .1    .1    .1    .1    .0    .0    .3    .4    .5    .3    .4    .2    .1    .0    .1    .2    .3    .4    .4
1
                                                                                                                 PAGE  4
      JOB: Site 1 26th & Wilshire (S1EXAM.DAT)                 RUN: Site 1 Existing AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .2    .1    .0    .0    .0    .3    .5    .5    .3    .4    .2    .1    .0    .0    .2    .3    .4    .4
 215.  *    .1    .1    .3    .1    .1    .0    .0    .4    .6    .5    .3    .4    .1    .1    .0    .0    .2    .3    .4    .4
 220.  *    .1    .1    .3    .2    .1    .2    .1    .3    .5    .4    .3    .3    .1    .1    .0    .0    .1    .2    .4    .4
 225.  *    .1    .1    .4    .2    .2    .2    .2    .3    .5    .4    .3    .2    .1    .1    .0    .0    .0    .2    .2    .2
 230.  *    .1    .1    .4    .5    .3    .3    .3    .1    .4    .3    .3    .2    .1    .1    .0    .0    .0    .2    .2    .2
 235.  *    .1    .2    .4    .5    .3    .3    .2    .1    .2    .2    .3    .2    .1    .1    .0    .0    .0    .1    .1    .1
 240.  *    .1    .2    .4    .3    .3    .3    .3    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .4    .3    .3    .3    .3    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
 250.  *    .1    .1    .4    .3    .2    .4    .4    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
 255.  *    .1    .1    .4    .3    .2    .4    .3    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
 260.  *    .1    .1    .4    .3    .1    .3    .3    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0
 265.  *    .1    .1    .4    .4    .1    .3    .3    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .0    .0    .0
 270.  *    .1    .1    .4    .3    .3    .3    .3    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .0    .0    .0
 275.  *    .2    .1    .3    .2    .3    .4    .2    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .0    .0    .0
 280.  *    .2    .1    .3    .2    .3    .4    .2    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .0    .0    .0
 285.  *    .2    .1    .3    .1    .3    .4    .2    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .0    .0    .0
 290.  *    .2    .1    .3    .1    .3    .3    .2    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .0    .0    .0
 295.  *    .2    .1    .2    .1    .3    .3    .2    .0    .0    .0    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0
 300.  *    .1    .1    .2    .2    .3    .3    .2    .0    .0    .0    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0
 305.  *    .1    .1    .2    .2    .3    .3    .2    .0    .0    .0    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0
 310.  *    .0    .1    .2    .3    .4    .4    .2    .0    .0    .0    .1    .2    .2    .1    .0    .1    .0    .0    .0    .0
 315.  *    .0    .1    .0    .3    .4    .4    .2    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .1    .0    .0
 320.  *    .0    .0    .0    .3    .4    .4    .2    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .2    .0    .0
 325.  *    .0    .0    .2    .3    .4    .4    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0
 330.  *    .0    .1    .2    .3    .4    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0
 335.  *    .0    .1    .2    .3    .4    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .3    .3    .0    .0
 340.  *    .0    .1    .2    .3    .4    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .3    .0    .0
 345.  *    .0    .1    .2    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .3    .0    .0
 350.  *    .0    .1    .2    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .3    .0    .0
 355.  *    .0    .0    .2    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .3    .0    .0
 360.  *    .0    .0    .2    .4    .2    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .3    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .2    .2    .4    .5    .5    .4    .4    .4    .7    .8    .6    .4    .2    .2    .1    .2    .4    .5    .4    .4
 DEGR. *  150   145   225   230    15    20   250   215    70    65    60   180   150   165     0    80    60    50   195   195

1
                                                                                                                 PAGE  5
      JOB: Site 1 26th & Wilshire (S1EXAM.DAT)                 RUN: Site 1 Existing AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .4    .4    .4    .3    .4    .2    .1
   5.  *    .0    .4    .4    .3    .5    .4    .1    .1
  10.  *    .0    .4    .4    .2    .5    .4    .1    .1
  15.  *    .0    .4    .4    .3    .5    .4    .1    .1
  20.  *    .0    .4    .4    .3    .3    .4    .1    .1
  25.  *    .0    .4    .3    .4    .3    .3    .1    .1
  30.  *    .0    .4    .3    .4    .3    .3    .1    .1
  35.  *    .0    .3    .4    .3    .4    .3    .1    .1
  40.  *    .1    .3    .3    .3    .2    .2    .1    .1
  45.  *    .1    .2    .3    .1    .2    .2    .1    .1
  50.  *    .1    .1    .0    .1    .2    .2    .1    .1
  55.  *    .1    .1    .0    .0    .2    .2    .1    .1
  60.  *    .3    .0    .0    .0    .2    .2    .1    .1
  65.  *    .3    .0    .0    .0    .2    .1    .1    .1
  70.  *    .3    .0    .0    .0    .2    .1    .1    .1
  75.  *    .3    .0    .0    .0    .2    .1    .1    .1
  80.  *    .3    .0    .0    .0    .2    .1    .1    .1
  85.  *    .3    .0    .0    .0    .2    .1    .1    .1
  90.  *    .3    .0    .0    .0    .2    .1    .1    .1
  95.  *    .3    .0    .0    .0    .2    .1    .1    .1
 100.  *    .3    .0    .0    .0    .2    .1    .1    .1
 105.  *    .3    .0    .0    .0    .2    .1    .1    .1
 110.  *    .3    .0    .0    .0    .1    .1    .1    .1
 115.  *    .3    .0    .0    .0    .1    .1    .1    .1
 120.  *    .3    .0    .0    .0    .1    .1    .1    .1
 125.  *    .3    .0    .0    .0    .1    .1    .1    .1
 130.  *    .3    .0    .0    .0    .1    .1    .1    .1
 135.  *    .3    .0    .0    .0    .1    .1    .1    .1
 140.  *    .3    .0    .0    .0    .0    .1    .1    .1
 145.  *    .3    .0    .0    .0    .0    .0    .0    .0
 150.  *    .3    .0    .0    .0    .0    .0    .0    .0
 155.  *    .3    .0    .0    .0    .0    .0    .0    .0
 160.  *    .3    .0    .0    .0    .0    .0    .0    .0
 165.  *    .3    .0    .0    .0    .0    .0    .0    .0
 170.  *    .3    .0    .0    .0    .0    .0    .0    .0
 175.  *    .3    .0    .0    .0    .0    .0    .0    .0
 180.  *    .3    .0    .0    .0    .0    .0    .0    .0
 185.  *    .3    .0    .0    .0    .0    .0    .0    .0
 190.  *    .3    .0    .0    .0    .0    .0    .0    .0
 195.  *    .4    .0    .0    .0    .0    .0    .0    .0
 200.  *    .4    .0    .0    .0    .0    .0    .0    .0
 205.  *    .4    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                              PAGE  6
      JOB: Site 1 26th & Wilshire (S1EXAM.DAT)                 RUN: Site 1 Existing AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .4    .0    .0    .0    .0    .0    .0    .0
 215.  *    .4    .1    .1    .1    .1    .0    .0    .0
 220.  *    .3    .2    .2    .2    .1    .0    .0    .0
 225.  *    .2    .3    .3    .3    .3    .1    .0    .0
 230.  *    .2    .3    .4    .4    .4    .1    .0    .0
 235.  *    .1    .4    .4    .4    .5    .1    .1    .0
 240.  *    .0    .4    .4    .4    .5    .1    .1    .0
 245.  *    .0    .4    .5    .5    .5    .2    .1    .0
 250.  *    .0    .4    .4    .5    .4    .1    .1    .0
 255.  *    .0    .4    .4    .5    .4    .1    .1    .0
 260.  *    .0    .4    .4    .5    .4    .1    .1    .0
 265.  *    .0    .4    .4    .4    .4    .1    .1    .0
 270.  *    .0    .4    .4    .4    .4    .1    .1    .0
 275.  *    .0    .4    .4    .4    .3    .1    .1    .0
 280.  *    .0    .4    .4    .4    .3    .1    .1    .0
 285.  *    .0    .4    .4    .4    .3    .1    .1    .0
 290.  *    .0    .4    .4    .4    .3    .1    .0    .0
 295.  *    .0    .4    .4    .4    .3    .1    .0    .0
 300.  *    .0    .4    .4    .4    .3    .0    .0    .0
 305.  *    .0    .4    .4    .4    .3    .0    .0    .0
 310.  *    .0    .4    .4    .4    .2    .0    .0    .0
 315.  *    .0    .4    .4    .4    .2    .0    .0    .1
 320.  *    .0    .4    .4    .4    .2    .0    .1    .1
 325.  *    .0    .4    .4    .4    .2    .1    .1    .1
 330.  *    .0    .4    .4    .4    .2    .1    .1    .1
 335.  *    .0    .4    .4    .4    .2    .1    .2    .1
 340.  *    .0    .4    .4    .4    .2    .1    .2    .1
 345.  *    .0    .4    .4    .4    .2    .1    .2    .1
 350.  *    .0    .4    .4    .4    .2    .2    .3    .1
 355.  *    .0    .4    .5    .4    .2    .3    .3    .1
 360.  *    .0    .4    .4    .4    .3    .4    .2    .1
 ------*------------------------------------------------
 MAX   *    .4    .4    .5    .5    .5    .4    .3    .1
 DEGR. *  195     0   245   245     5     0   350     0

 THE HIGHEST CONCENTRATION IS     .80 PPM AT   65 DEGREES FROM REC10.
 THE 2ND HIGHEST CONCENTRATION IS     .70 PPM AT   70 DEGREES FROM REC9 .
 THE 3RD HIGHEST CONCENTRATION IS     .60 PPM AT   60 DEGREES FROM REC11.
```

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1                        CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 1 26th & Wilshire (S1EXPM.DAT)                  RUN: Site 1 Existing PM
      DATE: 03/19/2010   TIME: 08:32:40.36


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*-------------------------------------------------------------
       1. EB        Wil AP    *    -15.0     139.0     583.0     699.0 *     819.    47. AG   1229.   3.3    .0 44.0
       2. EB        Wil T+R   *    584.0     699.0     715.0     824.0 *     181.    46. AG   1142.   3.3    .0 44.0
       3. EB        Wil T+R Q *    672.0     783.0    -880.4    -714.6 *    2157.   226. AG     72. 100.0    .0 24.0 1.48 109.6
       4. EB        Wil LT    *    569.0     717.0     698.0     843.0 *     180.    46. AG     87.   3.3    .0 32.0
       5. EB        Wil LT Q  *    654.0     800.0     435.3     586.8 *     305.   226. AG     33. 100.0    .0 12.0 1.36  15.5
       6. EB        Wil DP    *    715.0     824.0    1421.0    1528.0 *     997.    45. AG   1326.   3.3    .0 44.0
       7. WB        Wil AP    *   1393.0    1557.0     810.0     982.0 *     819.   225. AG   1384.   3.3    .0 44.0
       8. WB        Wil T+R   *    806.0     986.0     684.0     868.0 *     170.   226. AG   1181.   3.3    .0 56.0
       9. WB        Wil T+R Q *    717.0     900.0     930.9    1108.9 *     299.    46. AG    104. 100.0    .0 36.0 1.02  15.2
      10. WB        Wil LT    *    824.0     966.0     707.0     850.0 *     165.   225. AG    127.   3.3    .0 32.0
      11. WB        Wil LT Q  *    737.0     880.0    1241.3    1384.3 *     713.    45. AG     32. 100.0    .0 12.0 1.92  36.2
      12. WB        Wil DP    *    687.0     864.0     -35.0     163.0 *    1006.   226. AG   1479.   3.3    .0 44.0
      13. SB        26 AP     *    553.0     971.0      -6.0    1547.0 *     803.   316. AG    694.   3.3    .0 32.0
      14. SB        26 T+R    *    549.0     968.0     670.0     841.0 *     175.   136. AG    555.   3.3    .0 44.0
      15. SB        26 T+R Q  *    633.0     880.0     574.5     941.4 *      85.   316. AG     68. 100.0    .0 24.0  .67   4.3
      16. SB        26 LT     *    563.0     978.0     679.0     856.0 *     168.   136. AG    139.   3.3    .0 32.0
      17. SB        26 LT Q   *    645.0     891.0     309.2    1247.8 *     490.   317. AG     31. 100.0    .0 12.0 1.39  24.9
      18. SB        26 DP     *    672.0     845.0    1384.0     114.0 *    1020.   136. AG    656.   3.3    .0 32.0
      19. NB        26 AP     *    829.0     716.0    1410.0     138.0 *     820.   135. AG    727.   3.3    .0 32.0
      20. NB        26 T+R    *    832.0     719.0     715.0     846.0 *     173.   317. AG    616.   3.3    .0 44.0
      21. NB        26 T+R Q  *    759.0     798.0     829.1     721.9 *     103.   137. AG     70. 100.0    .0 24.0  .77   5.3
      22. NB        26 L      *    818.0     710.0     705.0     832.0 *     166.   317. AG    111.   3.3    .0 32.0
      23. NB        26 L Q    *    747.0     787.0     778.4     752.9 *      46.   137. AG     32. 100.0    .0 12.0  .82   2.4
      24. NB        26 DP     *    712.0     843.0      13.0    1565.0 *    1005.   316. AG    700.   3.3    .0 32.0
1
                                                                                                               PAGE  2
      JOB: Site 1 26th & Wilshire (S1EXPM.DAT)                  RUN: Site 1 Existing PM
      DATE: 03/19/2010   TIME: 08:32:40.36

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R Q *     90       59       2.0       1142       1285      20.50      1        3
       5. EB        Wil LT Q  *     90       54       2.0         87        182      20.50      1        3
       9. WB        Wil T+R Q *     90       57       2.0       1181       1196      20.50      1        3
      11. WB        Wil LT Q  *     90       52       2.0        127        176      20.50      1        3
      15. SB        26 T+R Q  *     90       56       2.0        555       1236      20.50      1        3
      17. SB        26 LT Q   *     90       50       2.0        139        252      20.50      1        3
      21. NB        26 T+R Q  *     90       57       2.0        616       1239      20.50      1        3
      23. NB        26 L Q    *     90       52       2.0        111        358      20.50      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-----------------------------------*
      1. SE MID S             *       967.0      615.0       5.0    *
      2. SE 164 S             *       874.0      710.0       5.0    *
      3. SE 82 S              *       816.0      771.0       5.0    *
      4. SE CNR               *       768.0      826.0       5.0    *
      5. SE 82 E              *       819.0      886.0       5.0    *
      6. SE 164 E             *       877.0      944.0       5.0    *
      7. SE MID E             *       996.0     1059.0       5.0    *
      8. NE MID E             *       916.0     1134.0       5.0    *
      9. NE 164 E             *       800.0     1020.0       5.0    *
     10. NE 82 E              *       741.0      962.0       5.0    *
     11. NE CNR               *       680.0      915.0       5.0    *
     12. NE 82 N              *       628.0      964.0       5.0    *
     13. NE 164 N             *       570.0     1023.0       5.0    *
     14. NE MID N             *       454.0     1143.0       5.0    *
     15. NW MID N             *       391.0     1100.0       5.0    *
     16. NW 164 N             *       514.0      974.0       5.0    *
     17. NW 82 N              *       571.0      914.0       5.0    *
     18. NW CNR               *       621.0      855.0       5.0    *
     19. NW 82 W              *       570.0      797.0       5.0    *
     20. NW 164 W             *       512.0      740.0       5.0    *
     21. NW MID W             *       412.0      643.0       5.0    *
     22. SW MID W             *       484.0      558.0       5.0    *
     23. SW 164 W             *       589.0      658.0       5.0    *
     24. SW 82 W              *       649.0      715.0       5.0    *
     25. SW CNR               *       707.0      765.0       5.0    *
     26. SW 82 S              *       763.0      714.0       5.0    *
     27. SW 164 S             *       820.0      656.0       5.0    *
     28. SW MID S             *       919.0      554.0       5.0    *
1
                                                                                                               PAGE  3
      JOB: Site 1 26th & Wilshire (S1EXPM.DAT)                  RUN: Site 1 Existing PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

  WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-----------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .1    .2    .4    .5    .5    .2    .0    .0    .0    .0    .0    .0    .0    .3    .3    .4    .4    .0    .0
   5.  *    .0    .0    .2    .4    .5    .4    .3    .0    .0    .0    .0    .0    .0    .0    .2    .2    .3    .3    .0    .0
  10.  *    .0    .0    .2    .3    .6    .5    .3    .0    .0    .0    .0    .0    .0    .0    .1    .2    .3    .2    .1    .0
  15.  *    .0    .0    .2    .4    .6    .5    .3    .0    .0    .0    .0    .0    .0    .0    .1    .2    .3    .2    .1    .0
  20.  *    .0    .0    .3    .5    .5    .5    .3    .0    .0    .0    .0    .0    .0    .0    .1    .2    .4    .2    .1    .0
  25.  *    .0    .0    .2    .5    .5    .5    .3    .0    .0    .0    .0    .0    .0    .0    .1    .1    .4    .2    .1    .0
  30.  *    .0    .0    .1    .4    .5    .4    .3    .0    .0    .1    .0    .0    .0    .0    .1    .1    .3    .2    .0    .0
  35.  *    .0    .0    .1    .4    .4    .3    .3    .1    .2    .2    .1    .0    .0    .0    .1    .1    .3    .3    .1    .0
  40.  *    .0    .0    .0    .3    .3    .3    .3    .1    .2    .4    .2    .0    .0    .0    .1    .1    .3    .2    .1    .2
  45.  *    .0    .0    .0    .1    .3    .3    .1    .1    .3    .4    .4    .0    .0    .0    .1    .1    .3    .4    .2    .2
  50.  *    .0    .0    .0    .1    .1    .1    .1    .2    .5    .6    .5    .0    .0    .0    .1    .1    .3    .6    .3    .3
  55.  *    .0    .0    .0    .1    .1    .1    .1    .3    .6    .6    .6    .1    .0    .0    .1    .1    .4    .6    .3    .3
  60.  *    .0    .0    .0    .0    .1    .1    .0    .3    .7    .8    .6    .2    .0    .0    .1    .1    .5    .5    .3    .4
  65.  *    .0    .0    .0    .0    .0    .0    .0    .4    .8    .8    .6    .2    .0    .0    .1    .1    .4    .4    .3    .2
  70.  *    .0    .0    .0    .0    .0    .0    .0    .4    .8    .8    .5    .3    .0    .0    .1    .1    .5    .5    .2    .2
  75.  *    .0    .0    .0    .0    .0    .0    .0    .4    .8    .8    .5    .2    .0    .0    .1    .3    .5    .5    .2    .4
  80.  *    .0    .0    .0    .0    .0    .0    .0    .4    .8    .7    .5    .2    .1    .0    .1    .3    .4    .5    .2    .4
  85.  *    .0    .0    .0    .0    .0    .0    .0    .3    .7    .6    .5    .1    .1    .0    .2    .3    .4    .3    .2    .4
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .6    .6    .4    .1    .1    .0    .2    .2    .4    .3    .3    .4
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .4    .1    .1    .0    .3    .3    .4    .3    .3    .4
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .4    .2    .1    .0    .3    .3    .3    .1    .3    .3
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .4    .2    .1    .0    .3    .3    .3    .1    .3    .2
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .3    .2    .1    .1    .3    .2    .3    .2    .3    .2
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .3    .2    .1    .1    .3    .2    .3    .2    .3    .2
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .3    .2    .1    .0    .2    .2    .3    .2    .3    .2
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .5    .5    .3    .2    .1    .0    .1    .2    .2    .2    .3    .2
 130.  *    .1    .1    .0    .0    .0    .0    .0    .3    .5    .5    .2    .1    .0    .1    .1    .2    .3    .3    .3    .2
 135.  *    .1    .1    .1    .1    .0    .0    .0    .3    .5    .5    .2    .0    .1    .1    .0    .1    .3    .3    .3    .3
 140.  *    .1    .1    .1    .2    .0    .0    .0    .3    .5    .5    .2    .1    .1    .1    .0    .1    .2    .2    .3    .3
 145.  *    .1    .1    .2    .2    .0    .0    .0    .3    .5    .5    .2    .1    .1    .2    .0    .0    .1    .2    .3    .3
 150.  *    .2    .2    .3    .4    .0    .0    .0    .4    .5    .5    .2    .1    .1    .2    .0    .0    .1    .3    .3    .3
 155.  *    .2    .2    .4    .4    .0    .0    .0    .4    .5    .5    .3    .1    .2    .2    .0    .0    .1    .3    .3    .3
 160.  *    .2    .2    .4    .4    .0    .0    .0    .4    .5    .5    .2    .1    .3    .2    .0    .0    .2    .3    .2    .3
 165.  *    .2    .2    .3    .3    .0    .0    .0    .4    .6    .5    .2    .2    .3    .2    .0    .0    .2    .3    .2    .3
 170.  *    .2    .2    .4    .3    .0    .0    .0    .5    .6    .5    .3    .3    .3    .3    .0    .0    .2    .3    .2    .3
 175.  *    .1    .1    .3    .3    .0    .0    .0    .5    .6    .5    .3    .3    .3    .3    .0    .0    .2    .3    .3    .4
 180.  *    .1    .1    .3    .3    .1    .0    .0    .5    .5    .5    .4    .4    .2    .3    .0    .0    .2    .3    .3    .4
 185.  *    .1    .1    .3    .2    .1    .0    .0    .5    .6    .5    .5    .4    .3    .2    .0    .1    .2    .2    .4    .4
 190.  *    .1    .1    .3    .2    .1    .0    .0    .6    .6    .4    .4    .4    .3    .2    .0    .1    .2    .3    .4    .4
 195.  *    .1    .1    .3    .2    .1    .0    .0    .7    .6    .4    .3    .4    .3    .2    .0    .1    .2    .3    .4    .4
 200.  *    .1    .1    .3    .2    .1    .0    .0    .7    .6    .6    .3    .4    .3    .2    .0    .1    .2    .3    .4    .4
 205.  *    .1    .1    .3    .2    .1    .0    .0    .6    .6    .5    .3    .4    .3    .2    .0    .1    .2    .4    .4    .4
1
                                                                                                                 PAGE  4
      JOB: Site 1 26th & Wilshire (S1EXPM.DAT)                  RUN: Site 1 Existing PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-----------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .3    .2    .0    .0    .0    .6    .6    .5    .4    .4    .2    .2    .0    .1    .2    .4    .4    .4
 215.  *    .1    .1    .3    .2    .1    .1    .1    .6    .6    .5    .4    .4    .2    .2    .0    .0    .2    .4    .4    .4
 220.  *    .1    .1    .3    .2    .1    .2    .2    .5    .5    .4    .3    .4    .2    .2    .0    .0    .1    .3    .4    .4
 225.  *    .1    .1    .4    .3    .3    .3    .2    .5    .5    .4    .3    .2    .2    .2    .0    .0    .0    .2    .2    .2
 230.  *    .1    .1    .4    .6    .3    .3    .3    .3    .4    .3    .3    .2    .2    .2    .0    .0    .0    .2    .2    .2
 235.  *    .1    .2    .4    .6    .3    .3    .4    .1    .2    .2    .3    .2    .2    .2    .0    .0    .0    .1    .1    .1
 240.  *    .1    .2    .5    .4    .3    .4    .3    .1    .0    .0    .2    .2    .1    .2    .0    .0    .0    .0    .0    .0
 245.  *    .1    .2    .5    .4    .3    .4    .3    .0    .0    .0    .2    .2    .1    .2    .0    .0    .0    .0    .0    .0
 250.  *    .1    .2    .5    .4    .2    .4    .5    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0
 255.  *    .1    .2    .5    .5    .3    .4    .5    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0
 260.  *    .1    .2    .5    .4    .2    .4    .5    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0
 265.  *    .1    .2    .5    .4    .2    .4    .5    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0
 270.  *    .1    .2    .5    .3    .3    .4    .4    .0    .0    .0    .3    .2    .3    .3    .0    .0    .0    .0    .0    .0
 275.  *    .1    .1    .4    .3    .3    .4    .4    .0    .0    .0    .3    .2    .3    .3    .0    .0    .0    .0    .0    .0
 280.  *    .1    .1    .4    .3    .3    .4    .4    .0    .0    .0    .3    .2    .3    .3    .0    .0    .0    .0    .0    .0
 285.  *    .2    .1    .3    .3    .3    .4    .3    .0    .0    .0    .3    .2    .3    .3    .0    .0    .0    .0    .0    .0
 290.  *    .2    .1    .3    .2    .3    .3    .3    .0    .0    .0    .3    .2    .3    .3    .0    .0    .0    .0    .0    .0
 295.  *    .1    .2    .2    .3    .3    .3    .3    .0    .0    .0    .2    .3    .3    .3    .0    .0    .0    .0    .0    .0
 300.  *    .1    .2    .2    .2    .3    .3    .3    .0    .0    .0    .2    .3    .3    .3    .0    .0    .0    .0    .0    .0
 305.  *    .1    .2    .2    .2    .4    .3    .3    .0    .0    .0    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0
 310.  *    .1    .2    .2    .3    .4    .4    .3    .0    .0    .0    .1    .1    .1    .1    .0    .1    .0    .0    .0    .0
 315.  *    .0    .1    .1    .3    .4    .4    .3    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .1    .0    .0
 320.  *    .0    .1    .2    .4    .4    .4    .2    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .2    .0    .0
 325.  *    .0    .0    .2    .3    .4    .4    .2    .0    .0    .0    .0    .0    .0    .0    .1    .2    .3    .3    .0    .0
 330.  *    .0    .1    .2    .3    .4    .4    .2    .0    .0    .0    .0    .0    .0    .0    .2    .3    .4    .4    .0    .0
 335.  *    .0    .1    .2    .3    .4    .4    .2    .0    .0    .0    .0    .0    .0    .0    .2    .3    .4    .5    .0    .0
 340.  *    .0    .1    .2    .3    .4    .4    .2    .0    .0    .0    .0    .0    .0    .0    .2    .3    .3    .5    .0    .0
 345.  *    .0    .1    .2    .3    .3    .4    .2    .0    .0    .0    .0    .0    .0    .0    .2    .3    .4    .5    .0    .0
 350.  *    .0    .1    .2    .3    .3    .4    .2    .0    .0    .0    .0    .0    .0    .0    .3    .3    .4    .5    .0    .0
 355.  *    .0    .1    .2    .3    .3    .4    .2    .0    .0    .0    .0    .0    .0    .0    .3    .3    .4    .4    .0    .0
 360.  *    .0    .1    .2    .4    .5    .5    .2    .0    .0    .0    .0    .0    .0    .0    .3    .3    .4    .4    .0    .0
 ------*-----------------------------------------------------------------------------------------------------------------------
 MAX   *    .2    .2    .5    .6    .6    .5    .5    .7    .8    .8    .6    .4    .3    .3    .3    .3    .5    .6    .4    .4
 DEGR. *   150   150   240   230    10     0   250   195    65    60    55   180   160   170     0     0    60    50   185    60

1
                                                                                                                 PAGE  5
      JOB: Site 1 26th & Wilshire (S1EXPM.DAT)                  RUN: Site 1 Existing PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .4    .5    .4    .3    .4    .3    .2
   5.  *    .0    .4    .4    .4    .5    .4    .3    .1
  10.  *    .0    .5    .4    .3    .5    .4    .3    .1
  15.  *    .0    .5    .4    .3    .5    .4    .1    .1
  20.  *    .0    .4    .4    .3    .3    .4    .1    .1
  25.  *    .0    .4    .5    .4    .3    .4    .1    .1
  30.  *    .0    .4    .3    .4    .4    .3    .1    .1
  35.  *    .0    .4    .4    .3    .4    .3    .1    .1
  40.  *    .1    .3    .4    .3    .4    .2    .1    .1
  45.  *    .1    .2    .3    .2    .2    .2    .1    .1
  50.  *    .1    .1    .1    .1    .2    .2    .1    .1
  55.  *    .2    .1    .0    .0    .2    .2    .1    .1
  60.  *    .3    .0    .0    .0    .2    .2    .1    .1
  65.  *    .3    .0    .0    .0    .2    .2    .1    .1
  70.  *    .3    .0    .0    .0    .2    .2    .1    .1
  75.  *    .4    .0    .0    .0    .2    .2    .1    .1
  80.  *    .4    .0    .0    .0    .2    .2    .2    .1
  85.  *    .4    .0    .0    .0    .2    .2    .2    .2
  90.  *    .4    .0    .0    .0    .2    .1    .2    .2
  95.  *    .4    .0    .0    .0    .2    .1    .2    .2
 100.  *    .3    .0    .0    .0    .2    .1    .2    .2
 105.  *    .3    .0    .0    .0    .2    .1    .2    .2
 110.  *    .3    .0    .0    .0    .2    .2    .2    .2
 115.  *    .3    .0    .0    .0    .2    .2    .2    .2
 120.  *    .3    .0    .0    .0    .1    .2    .2    .2
 125.  *    .3    .0    .0    .0    .1    .2    .2    .2
 130.  *    .3    .0    .0    .0    .1    .2    .1    .1
 135.  *    .3    .0    .0    .0    .1    .1    .1    .1
 140.  *    .3    .0    .0    .0    .0    .1    .1    .1
 145.  *    .3    .0    .0    .0    .0    .0    .0    .0
 150.  *    .3    .0    .0    .0    .0    .0    .0    .0
 155.  *    .3    .0    .0    .0    .0    .0    .0    .0
 160.  *    .3    .0    .0    .0    .0    .0    .0    .0
 165.  *    .3    .0    .0    .0    .0    .0    .0    .0
 170.  *    .3    .0    .0    .0    .0    .0    .0    .0
 175.  *    .4    .0    .0    .0    .0    .0    .0    .0
 180.  *    .4    .0    .0    .0    .0    .0    .0    .0
 185.  *    .4    .0    .0    .0    .0    .0    .0    .0
 190.  *    .4    .0    .0    .0    .0    .0    .0    .0
 195.  *    .4    .0    .0    .0    .0    .0    .0    .0
 200.  *    .4    .0    .0    .0    .0    .0    .0    .0
 205.  *    .4    .0    .0    .0    .0    .0    .0    .0
1                                                                                                                               PAGE  6
      JOB: Site 1 26th & Wilshire (S1EXPM.DAT)                 RUN: Site 1 Existing PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .4    .0    .0    .0    .0    .0    .0    .0
 215.  *    .4    .1    .1    .1    .1    .0    .0    .0
 220.  *    .4    .2    .2    .2    .1    .0    .0    .0
 225.  *    .2    .3    .3    .3    .3    .1    .0    .0
 230.  *    .2    .4    .4    .4    .4    .1    .0    .0
 235.  *    .1    .4    .5    .4    .5    .1    .1    .0
 240.  *    .0    .5    .5    .4    .5    .2    .1    .0
 245.  *    .0    .5    .5    .5    .5    .3    .1    .0
 250.  *    .0    .5    .5    .5    .4    .3    .1    .0
 255.  *    .0    .4    .5    .5    .4    .2    .1    .0
 260.  *    .0    .4    .4    .5    .4    .2    .1    .0
 265.  *    .0    .4    .4    .4    .4    .2    .1    .0
 270.  *    .0    .4    .4    .4    .4    .2    .1    .0
 275.  *    .0    .4    .4    .4    .3    .2    .1    .0
 280.  *    .0    .4    .4    .4    .3    .2    .1    .0
 285.  *    .0    .4    .4    .4    .3    .2    .1    .0
 290.  *    .0    .4    .4    .4    .3    .2    .1    .0
 295.  *    .0    .4    .4    .4    .3    .1    .0    .0
 300.  *    .0    .4    .4    .4    .3    .1    .0    .0
 305.  *    .0    .4    .4    .4    .3    .0    .0    .0
 310.  *    .0    .4    .4    .4    .2    .0    .0    .0
 315.  *    .0    .4    .4    .4    .2    .0    .0    .1
 320.  *    .0    .4    .4    .4    .2    .0    .1    .1
 325.  *    .0    .4    .4    .4    .2    .1    .1    .1
 330.  *    .0    .4    .4    .4    .3    .1    .2    .1
 335.  *    .0    .4    .4    .4    .3    .1    .2    .1
 340.  *    .0    .4    .4    .4    .2    .1    .2    .1
 345.  *    .0    .4    .4    .4    .2    .1    .3    .1
 350.  *    .0    .4    .4    .4    .2    .2    .3    .2
 355.  *    .0    .4    .5    .4    .2    .4    .3    .2
 360.  *    .0    .4    .5    .4    .3    .4    .3    .2
 ------*------------------------------------------------
 MAX   *    .4    .5    .5    .5    .5    .4    .3    .2
 DEGR. *   75    10     0   245     5     0     0     0

 THE HIGHEST CONCENTRATION IS     .80 PPM AT   65 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .80 PPM AT   60 DEGREES FROM REC10.
 THE 3RD HIGHEST CONCENTRATION IS     .70 PPM AT  195 DEGREES FROM REC8 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                   PAGE  1

      JOB: Site 1 26th & Wilshire (S1NBAM.DAT)                  RUN: Site 1 No Build AM
      DATE: 03/19/2010   TIME: 08:37:14.44


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*-----------------------------------------------------------
       1. EB        Wil AP    *    -15.0     139.0     583.0     699.0 *     819.    47. AG   1288.    .8    .0 44.0
       2. EB        Wil T+R   *    584.0     699.0     715.0     824.0 *     181.    46. AG   1248.    .8    .0 44.0
       3. EB        Wil T+R Q *    672.0     783.0   -3512.7   -3254.0 *    5815.   226. AG     14. 100.0    .0 24.0 7.17 295.4
       4. EB        Wil LT    *    569.0     717.0     698.0     843.0 *     180.    46. AG     40.    .8    .0 32.0
       5. EB        Wil LT Q  *    654.0     800.0     643.5     789.8 *      15.   226. AG      7. 100.0    .0 12.0  .65    .7
       6. EB        Wil DP    *    715.0     824.0    1421.0    1528.0 *     997.    45. AG   1363.    .8    .0 44.0
       7. WB        Wil AP    *   1393.0    1557.0     810.0     982.0 *     819.   225. AG   1617.    .8    .0 44.0
       8. WB        Wil T+R   *    806.0     986.0     684.0     868.0 *     170.   226. AG   1496.    .8    .0 56.0
       9. WB        Wil T+R Q *    717.0     900.0    4109.1    4213.2 *    4742.    46. AG     21. 100.0    .0 36.0 7.90 240.9
      10. WB        Wil LT    *    824.0     966.0     707.0     850.0 *     165.   225. AG    121.    .8    .0 32.0
      11. WB        Wil LT Q  *    737.0     880.0    1195.3    1338.3 *     648.    45. AG      6. 100.0    .0 12.0 1.83  32.9
      12. WB        Wil DP    *    687.0     864.0     -35.0     163.0 *    1006.   226. AG   1515.    .8    .0 44.0
      13. SB        26 AP     *    553.0     971.0      -6.0    1547.0 *     803.   316. AG    817.    .8    .0 32.0
      14. SB        26 T+R    *    549.0     968.0     670.0     841.0 *     175.   136. AG    715.    .8    .0 44.0
      15. SB        26 T+R Q  *    633.0     880.0   -1458.9    3073.9 *    3031.   316. AG     14. 100.0    .0 24.0 4.46 154.0
      16. SB        26 LT     *    563.0     978.0     679.0     856.0 *     168.   136. AG    102.    .8    .0 32.0
      17. SB        26 LT Q   *    645.0     891.0     355.3    1198.8 *     423.   317. AG      6. 100.0    .0 12.0 1.50  21.5
      18. SB        26 DP     *    672.0     845.0    1384.0     114.0 *    1020.   136. AG    812.    .8    .0 32.0
      19. NB        26 AP     *    829.0     716.0    1410.0     138.0 *     820.   135. AG    707.    .8    .0 32.0
      20. NB        26 T+R    *    832.0     719.0     715.0     846.0 *     173.   317. AG    629.    .8    .0 44.0
      21. NB        26 T+R Q  *    759.0     798.0    2493.7   -1085.4 *    2561.   137. AG     14. 100.0    .0 24.0 3.88 130.1
      22. NB        26 L      *    818.0     710.0     705.0     832.0 *     166.   317. AG     78.    .8    .0 32.0
      23. NB        26 L Q    *    747.0     787.0     887.8     634.2 *     208.   137. AG      6. 100.0    .0 12.0 1.22  10.6
      24. NB        26 DP     *    712.0     843.0      13.0    1565.0 *    1005.   316. AG    739.    .8    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 1 26th & Wilshire (S1NBAM.DAT)                  RUN: Site 1 No Build AM
      DATE: 03/19/2010   TIME: 08:37:14.44

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*-------------------------------------------------------------------------------
       3. EB        Wil T+R Q *      90       59       2.0      1248        290       4.10      1        3
       5. EB        Wil LT Q  *      90       55       2.0        40        182       4.10      1        3
       9. WB        Wil T+R Q *      90       56       2.0      1496        190       4.10      1        3
      11. WB        Wil LT Q  *      90       51       2.0       121        170       4.10      1        3
      15. SB        26 T+R Q  *      90       56       2.0       715        242       4.10      1        3
      17. SB        26 LT Q   *      90       49       2.0       102        166       4.10      1        3
      21. NB        26 T+R Q  *      90       56       2.0       629        245       4.10      1        3
      23. NB        26 L Q    *      90       52       2.0        78        172       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)         *
         RECEPTOR             *      X          Y          Z      *
     -------------------------*-------------------------------------*
      1. SE MID S             *       967.0      615.0        5.0   *
      2. SE 164 S             *       874.0      710.0        5.0   *
      3. SE 82 S              *       816.0      771.0        5.0   *
      4. SE CNR               *       768.0      826.0        5.0   *
      5. SE 82 E              *       819.0      886.0        5.0   *
      6. SE 164 E             *       877.0      944.0        5.0   *
      7. SE MID E             *       996.0     1059.0        5.0   *
      8. NE MID E             *       916.0     1134.0        5.0   *
      9. NE 164 E             *       800.0     1020.0        5.0   *
     10. NE 82 E              *       741.0      962.0        5.0   *
     11. NE CNR               *       680.0      915.0        5.0   *
     12. NE 82 N              *       628.0      964.0        5.0   *
     13. NE 164 N             *       570.0     1023.0        5.0   *
     14. NE MID N             *       454.0     1143.0        5.0   *
     15. NW MID N             *       391.0     1100.0        5.0   *
     16. NW 164 N             *       514.0      974.0        5.0   *
     17. NW 82 N              *       571.0      914.0        5.0   *
     18. NW CNR               *       621.0      855.0        5.0   *
     19. NW 82 W              *       570.0      797.0        5.0   *
     20. NW 164 W             *       512.0      740.0        5.0   *
     21. NW MID W             *       412.0      643.0        5.0   *
     22. SW MID W             *       484.0      558.0        5.0   *
     23. SW 164 W             *       589.0      658.0        5.0   *
     24. SW 82 W              *       649.0      715.0        5.0   *
     25. SW CNR               *       707.0      765.0        5.0   *
     26. SW 82 S              *       763.0      714.0        5.0   *
     27. SW 164 S             *       820.0      656.0        5.0   *
     28. SW MID S             *       919.0      554.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 1 26th & Wilshire (S1NBAM.DAT)                  RUN: Site 1 No Build AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 140.  *    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 145.  *    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 155.  *    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 160.  *    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 165.  *    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 180.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE  4
      JOB: Site 1 26th & Wilshire (S1NBAM.DAT)                  RUN: Site 1 No Build AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 215.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .1    .1    .1    .0    .2    .2    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .1
 DEGR. *  150   145   140   145    30    30     0    60    60    40    45     0     0     0   110   105   320    45   210   210

1
                                                                                                                PAGE  5
      JOB: Site 1 26th & Wilshire (S1NBAM.DAT)                  RUN: Site 1 No Build AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0
 180.  *    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  6
      JOB: Site 1 26th & Wilshire (S1NBAM.DAT)                 RUN: Site 1 No Build AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .1    .1    .0    .0    .0    .0    .0
 240.  *    .0    .1    .1    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .1    .1    .1    .0    .0    .0    .0    .0
 DEGR. *  210   235   235     0     0     0     0     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT   60 DEGREES FROM REC8 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   60 DEGREES FROM REC9 .
 THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT  150 DEGREES FROM REC1 .
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 1 26th & Wilshire (S1NBPM.DAT)                  RUN: Site 1 No Build PM
      DATE: 03/19/2010   TIME: 08:36:37.97


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)           *   LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2      *    (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*-----------------------------------------*---------------------------------------------------------
       1. EB        Wil AP    *     -15.0     139.0     583.0     699.0 *     819.   47. AG   1495.    .8    .0 44.0
       2. EB        Wil T+R   *     584.0     699.0     715.0     824.0 *     181.   46. AG   1408.    .8    .0 44.0
       3. EB        Wil T+R Q *     672.0     783.0   -4071.5   -3793.1 *    6591.  226. AG     14. 100.0    .0 24.0 7.57 334.8
       4. EB        Wil LT    *     569.0     717.0     698.0     843.0 *     180.   46. AG     87.    .8    .0 32.0
       5. EB        Wil LT Q  *     654.0     800.0     420.3     572.1 *     326.  226. AG      7. 100.0    .0 12.0 1.40  16.6
       6. EB        Wil DP    *     715.0     824.0    1421.0    1528.0 *     997.   45. AG   1726.    .8    .0 44.0
       7. WB        Wil AP    *    1393.0    1557.0     810.0     982.0 *     819.  225. AG   1697.    .8    .0 44.0
       8. WB        Wil T+R   *     806.0     986.0     684.0     868.0 *     170.  226. AG   1570.    .8    .0 56.0
       9. WB        Wil T+R Q *     717.0     900.0    4284.0    4384.0 *    4986.   46. AG     21. 100.0    .0 36.0 8.05 253.3
      10. WB        Wil LT    *     824.0     966.0     707.0     850.0 *     165.  225. AG    127.    .8    .0 32.0
      11. WB        Wil LT Q  *     737.0     880.0    1248.2    1391.2 *     723.   45. AG      6. 100.0    .0 12.0 1.95  36.7
      12. WB        Wil DP    *     687.0     864.0     -35.0     163.0 *    1006.  226. AG   1707.    .8    .0 44.0
      13. SB        26 AP     *     553.0     971.0      -6.0    1547.0 *     803.  316. AG    830.    .8    .0 32.0
      14. SB        26 T+R    *     549.0     968.0     670.0     841.0 *     175.  136. AG    661.    .8    .0 44.0
      15. SB        26 T+R Q  *     633.0     880.0   -1291.2    2898.1 *    2788.  316. AG     14. 100.0    .0 24.0 4.34 141.7
      16. SB        26 LT     *     563.0     978.0     679.0     856.0 *     168.  136. AG    169.    .8    .0 32.0
      17. SB        26 LT Q   *     645.0     891.0    -144.8    1730.1 *    1152.  317. AG      6. 100.0    .0 12.0 2.52  58.5
      18. SB        26 DP     *     672.0     845.0    1384.0     114.0 *    1020.  136. AG    762.    .8    .0 32.0
      19. NB        26 AP     *     829.0     716.0    1410.0     138.0 *     820.  135. AG    921.    .8    .0 32.0
      20. NB        26 T+R    *     832.0     719.0     715.0     846.0 *     173.  317. AG    810.    .8    .0 44.0
      21. NB        26 T+R Q  *     759.0     798.0    3184.9   -1835.9 *    3581.  137. AG     14. 100.0    .0 24.0 5.26 181.9
      22. NB        26 L      *     818.0     710.0     705.0     832.0 *     166.  317. AG    111.    .8    .0 32.0
      23. NB        26 L Q    *     747.0     787.0    1113.9     388.7 *     541.  137. AG      6. 100.0    .0 12.0 1.68  27.5
      24. NB        26 DP     *     712.0     843.0      13.0    1565.0 *    1005.  316. AG    748.    .8    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 1 26th & Wilshire (S1NBPM.DAT)                  RUN: Site 1 No Build PM
      DATE: 03/19/2010   TIME: 08:36:37.97

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R Q *     90       57       2.0      1408       289       4.10      1         3
       5. EB        Wil LT Q  *     90       55       2.0        87       182       4.10      1         3
       9. WB        Wil T+R Q *     90       56       2.0      1570       196       4.10      1         3
      11. WB        Wil LT Q  *     90       51       2.0       127       169       4.10      1         3
      15. SB        26 T+R Q  *     90       57       2.0       661       236       4.10      1         3
      17. SB        26 LT Q   *     90       51       2.0       169       174       4.10      1         3
      21. NB        26 T+R Q  *     90       57       2.0       810       239       4.10      1         3
      23. NB        26 L Q    *     90       52       2.0       111       177       4.10      1         3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       967.0      615.0        5.0   *
      2. SE 164 S             *       874.0      710.0        5.0   *
      3. SE 82 S              *       816.0      771.0        5.0   *
      4. SE CNR               *       768.0      826.0        5.0   *
      5. SE 82 E              *       819.0      886.0        5.0   *
      6. SE 164 E             *       877.0      944.0        5.0   *
      7. SE MID E             *       996.0     1059.0        5.0   *
      8. NE MID E             *       916.0     1134.0        5.0   *
      9. NE 164 E             *       800.0     1020.0        5.0   *
     10. NE 82 E              *       741.0      962.0        5.0   *
     11. NE CNR               *       680.0      915.0        5.0   *
     12. NE 82 N              *       628.0      964.0        5.0   *
     13. NE 164 N             *       570.0     1023.0        5.0   *
     14. NE MID N             *       454.0     1143.0        5.0   *
     15. NW MID N             *       391.0     1100.0        5.0   *
     16. NW 164 N             *       514.0      974.0        5.0   *
     17. NW 82 N              *       571.0      914.0        5.0   *
     18. NW CNR               *       621.0      855.0        5.0   *
     19. NW 82 W              *       570.0      797.0        5.0   *
     20. NW 164 W             *       512.0      740.0        5.0   *
     21. NW MID W             *       412.0      643.0        5.0   *
     22. SW MID W             *       484.0      558.0        5.0   *
     23. SW 164 W             *       589.0      658.0        5.0   *
     24. SW 82 W              *       649.0      715.0        5.0   *
     25. SW CNR               *       707.0      765.0        5.0   *
     26. SW 82 S              *       763.0      714.0        5.0   *
     27. SW 164 S             *       820.0      656.0        5.0   *
     28. SW MID S             *       919.0      554.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 1 26th & Wilshire (S1NBPM.DAT)                  RUN: Site 1 No Build PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .0    .1    .1    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 140.  *    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 160.  *    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 165.  *    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 170.  *    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 180.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 200.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 205.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
1
                                                                                                                 PAGE  4
      JOB: Site 1 26th & Wilshire (S1NBPM.DAT)                  RUN: Site 1 No Build PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 215.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 220.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .1    .1    .1    .1    .2    .2    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .1
 DEGR. *  145   140   140    20     5     5    10    55    55    40    45     0     0     0   105   100   320    45   195   195

1
                                                                                                                 PAGE  5
      JOB: Site 1 26th & Wilshire (S1NBPM.DAT)                  RUN: Site 1 No Build PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .1    .0    .0    .0    .0    .0    .0    .0
  65.  *    .1    .0    .0    .0    .0    .0    .0    .0
  70.  *    .1    .0    .0    .0    .0    .0    .0    .0
  75.  *    .1    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0
 180.  *    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1                                                                                                PAGE  6
      JOB: Site 1 26th & Wilshire (S1NBPM.DAT)                  RUN: Site 1 No Build PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .1    .0    .0    .0    .0    .0    .0    .0
 DEGR. *   60     0     0     0     0     0     0     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT   55 DEGREES FROM REC8 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   55 DEGREES FROM REC9 .
 THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT  145 DEGREES FROM REC1 .
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 1 26th & Wilshire (S1B3AM.DAT)                 RUN: Site 1 Build Alt3 AM
      DATE: 03/19/2010   TIME: 08:42:35.42


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *    -15.0     139.0     583.0     699.0 *     819.    47. AG   1275.    .8    .0 44.0
       2. EB        Wil T+R   *    584.0     699.0     715.0     824.0 *     181.    46. AG   1235.    .8    .0 44.0
       3. EB        Wil T+R Q *    672.0     783.0   -3467.3   -3210.2 *    5752.   226. AG     14. 100.0    .0 24.0 7.17 292.2
       4. EB        Wil LT    *    569.0     717.0     698.0     843.0 *     180.    46. AG     40.    .8    .0 32.0
       5. EB        Wil LT Q  *    654.0     800.0     643.5     789.8 *      15.   226. AG      7. 100.0    .0 12.0  .65    .7
       6. EB        Wil DP    *    715.0     824.0    1421.0    1528.0 *     997.    45. AG   1352.    .8    .0 44.0
       7. WB        Wil AP    *   1393.0    1557.0     810.0     982.0 *     819.   225. AG   1613.    .8    .0 44.0
       8. WB        Wil T+R   *    806.0     986.0     684.0     868.0 *     170.   226. AG   1492.    .8    .0 56.0
       9. WB        Wil T+R Q *    717.0     900.0    4101.4    4205.7 *    4731.    46. AG     21. 100.0    .0 36.0 7.89 240.3
      10. WB        Wil LT    *    824.0     966.0     707.0     850.0 *     165.   225. AG    121.    .8    .0 32.0
      11. WB        Wil LT Q  *    737.0     880.0    1195.3    1338.3 *     648.    45. AG      6. 100.0    .0 12.0 1.83  32.9
      12. WB        Wil DP    *    687.0     864.0     -35.0     163.0 *    1006.   226. AG   1491.    .8    .0 44.0
      13. SB        26 AP     *    553.0     971.0      -6.0    1547.0 *     803.   316. AG    822.    .8    .0 32.0
      14. SB        26 T+R    *    549.0     968.0     670.0     841.0 *     175.   136. AG    714.    .8    .0 44.0
      15. SB        26 T+R Q  *    633.0     880.0   -1544.0    3163.2 *    3155.   316. AG     14. 100.0    .0 24.0 5.17 160.3
      16. SB        26 LT     *    563.0     978.0     679.0     856.0 *     168.   136. AG    108.    .8    .0 32.0
      17. SB        26 LT Q   *    645.0     891.0     388.3    1163.8 *     375.   317. AG      6. 100.0    .0 12.0 1.37  19.0
      18. SB        26 DP     *    672.0     845.0    1384.0     114.0 *    1020.   136. AG    808.    .8    .0 32.0
      19. NB        26 AP     *    829.0     716.0    1410.0     138.0 *     820.   135. AG    669.    .8    .0 32.0
      20. NB        26 T+R    *    832.0     719.0     715.0     846.0 *     173.   317. AG    591.    .8    .0 44.0
      21. NB        26 T+R Q  *    759.0     798.0    2461.3   -1050.3 *    2513.   137. AG     14. 100.0    .0 24.0 4.40 127.6
      22. NB        26 L      *    818.0     710.0     705.0     832.0 *     166.   317. AG     78.    .8    .0 32.0
      23. NB        26 L Q    *    747.0     787.0     887.8     634.2 *     208.   137. AG      6. 100.0    .0 12.0 1.22  10.6
      24. NB        26 DP     *    712.0     843.0      13.0    1565.0 *    1005.   316. AG    725.    .8    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 1 26th & Wilshire (S1B3AM.DAT)                 RUN: Site 1 Build Alt3 AM
      DATE: 03/19/2010   TIME: 08:42:35.42

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE    SIGNAL    ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R Q *      90       59       2.0      1235        288       4.10      1        3
       5. EB        Wil LT Q  *      90       55       2.0        40        182       4.10      1        3
       9. WB        Wil T+R Q *      90       56       2.0      1492        190       4.10      1        3
      11. WB        Wil LT Q  *      90       51       2.0       121        170       4.10      1        3
      15. SB        26 T+R Q  *      90       56       2.0       714        208       4.10      1        3
      17. SB        26 LT Q   *      90       50       2.0       108        198       4.10      1        3
      21. NB        26 T+R Q  *      90       57       2.0       591        210       4.10      1        3
      23. NB        26 L Q    *      90       52       2.0        78        172       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*-------------------------------------*
      1. SE MID S             *       967.0      615.0        5.0   *
      2. SE 164 S             *       874.0      710.0        5.0   *
      3. SE 82 S              *       816.0      771.0        5.0   *
      4. SE CNR               *       768.0      826.0        5.0   *
      5. SE 82 E              *       819.0      886.0        5.0   *
      6. SE 164 E             *       877.0      944.0        5.0   *
      7. SE MID E             *       996.0     1059.0        5.0   *
      8. NE MID E             *       916.0     1134.0        5.0   *
      9. NE 164 E             *       800.0     1020.0        5.0   *
     10. NE 82 E              *       741.0      962.0        5.0   *
     11. NE CNR               *       680.0      915.0        5.0   *
     12. NE 82 N              *       628.0      964.0        5.0   *
     13. NE 164 N             *       570.0     1023.0        5.0   *
     14. NE MID N             *       454.0     1143.0        5.0   *
     15. NW MID N             *       391.0     1100.0        5.0   *
     16. NW 164 N             *       514.0      974.0        5.0   *
     17. NW 82 N              *       571.0      914.0        5.0   *
     18. NW CNR               *       621.0      855.0        5.0   *
     19. NW 82 W              *       570.0      797.0        5.0   *
     20. NW 164 W             *       512.0      740.0        5.0   *
     21. NW MID W             *       412.0      643.0        5.0   *
     22. SW MID W             *       484.0      558.0        5.0   *
     23. SW 164 W             *       589.0      658.0        5.0   *
     24. SW 82 W              *       649.0      715.0        5.0   *
     25. SW CNR               *       707.0      765.0        5.0   *
     26. SW 82 S              *       763.0      714.0        5.0   *
     27. SW 164 S             *       820.0      656.0        5.0   *
     28. SW MID S             *       919.0      554.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 1 26th & Wilshire (S1B3AM.DAT)                 RUN: Site 1 Build Alt3 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 140.  *    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 145.  *    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 160.  *    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 165.  *    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 170.  *    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 180.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE  4
      JOB: Site 1 26th & Wilshire (S1B3AM.DAT)                  RUN: Site 1 Build Alt3 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 215.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .1    .1    .1    .0    .2    .2    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .1
 DEGR. *  150   145   140   145    30    30     0    60    60    40    45     0     0     0   110   105   320    45   210   210

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                                                                                                                PAGE  5
      JOB: Site 1 26th & Wilshire (S1B3AM.DAT)                  RUN: Site 1 Build Alt3 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0
 180.  *    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  6
      JOB: Site 1 26th & Wilshire (S1B3AM.DAT)                  RUN: Site 1 Build Alt3 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .1    .1    .0    .0    .0    .0    .0
 240.  *    .0    .1    .1    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .0    .1    .1    .0    .0    .0    .0    .0
 DEGR. *    0   235   235     0     0     0     0     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT   60 DEGREES FROM REC8 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   60 DEGREES FROM REC9 .
 THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT  150 DEGREES FROM REC1 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 1 26th & Wilshire (S1B3PM.DAT)                  RUN: Site 1 Build Alt3 PM
      DATE: 03/19/2010   TIME: 08:42:55.91


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*---------------------------------------------------------
       1. EB        Wil AP    *    -15.0     139.0     583.0     699.0 *     819.   47. AG    1509.    .8    .0 44.0
       2. EB        Wil T+R   *    584.0     699.0     715.0     824.0 *     181.   46. AG    1422.    .8    .0 44.0
       3. EB        Wil T+R Q *    672.0     783.0   -4133.7   -3853.1 *    6677.  226. AG      14. 100.0    .0 24.0 7.73 339.2
       4. EB        Wil LT    *    569.0     717.0     698.0     843.0 *     180.   46. AG      87.    .8    .0 32.0
       5. EB        Wil LT Q  *    654.0     800.0     435.7     587.1 *     305.  226. AG       6. 100.0    .0 12.0 1.36  15.5
       6. EB        Wil DP    *    715.0     824.0    1421.0    1528.0 *     997.   45. AG    1766.    .8    .0 44.0
       7. WB        Wil AP    *   1393.0    1557.0     810.0     982.0 *     819.  225. AG    1713.    .8    .0 44.0
       8. WB        Wil T+R   *    806.0     986.0     684.0     868.0 *     170.  226. AG    1586.    .8    .0 56.0
       9. WB        Wil T+R Q *    717.0     900.0    4322.5    4421.6 *    5040.   46. AG      21. 100.0    .0 36.0 8.12 256.0
      10. WB        Wil LT    *    824.0     966.0     707.0     850.0 *     165.  225. AG     127.    .8    .0 32.0
      11. WB        Wil LT Q  *    737.0     880.0    1248.2    1391.2 *     723.   45. AG       6. 100.0    .0 12.0 1.95  36.7
      12. WB        Wil DP    *    687.0     864.0     -35.0     163.0 *    1006.  226. AG    1728.    .8    .0 44.0
      13. SB        26 AP     *    553.0     971.0      -6.0    1547.0 *     803.  316. AG     852.    .8    .0 32.0
      14. SB        26 T+R    *    549.0     968.0     670.0     841.0 *     175.  136. AG     680.    .8    .0 44.0
      15. SB        26 T+R Q  *    633.0     880.0   -1458.6    3073.6 *    3031.  316. AG      14. 100.0    .0 24.0 5.31 154.0
      16. SB        26 LT     *    563.0     978.0     679.0     856.0 *     168.  136. AG     169.    .8    .0 32.0
      17. SB        26 LT Q   *    645.0     891.0    -160.0    1746.3 *    1175.  317. AG       6. 100.0    .0 12.0 2.60  59.7
      18. SB        26 DP     *    672.0     845.0    1384.0     114.0 *    1020.  136. AG     765.    .8    .0 32.0
      19. NB        26 AP     *    829.0     716.0    1410.0     138.0 *     820.  135. AG     974.    .8    .0 32.0
      20. NB        26 T+R    *    832.0     719.0     715.0     846.0 *     173.  317. AG     863.    .8    .0 44.0
      21. NB        26 T+R Q  *    759.0     798.0    3485.9   -2162.6 *    4025.  137. AG      14. 100.0    .0 24.0 6.84 204.5
      22. NB        26 L      *    818.0     710.0     705.0     832.0 *     166.  317. AG     111.    .8    .0 32.0
      23. NB        26 L Q    *    747.0     787.0    1113.9     388.7 *     541.  137. AG       6. 100.0    .0 12.0 1.68  27.5
      24. NB        26 DP     *    712.0     843.0      13.0    1565.0 *    1005.  316. AG     793.    .8    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 1 26th & Wilshire (S1B3PM.DAT)                  RUN: Site 1 Build Alt3 PM
      DATE: 03/19/2010   TIME: 08:42:55.91

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R Q *      90       57       2.0      1422        287       4.10      1        3
       5. EB        Wil LT Q  *      90       53       2.0        87        175       4.10      1        3
       9. WB        Wil T+R Q *      90       56       2.0      1586        196       4.10      1        3
      11. WB        Wil LT Q  *      90       51       2.0       127        169       4.10      1        3
      15. SB        26 T+R Q  *      90       57       2.0       680        200       4.10      1        3
      17. SB        26 LT Q   *      90       52       2.0       169        174       4.10      1        3
      21. NB        26 T+R Q  *      90       58       2.0       863        204       4.10      1        3
      23. NB        26 L Q    *      90       52       2.0       111        177       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       967.0      615.0        5.0   *
      2. SE 164 S             *       874.0      710.0        5.0   *
      3. SE 82 S              *       816.0      771.0        5.0   *
      4. SE CNR               *       768.0      826.0        5.0   *
      5. SE 82 E              *       819.0      886.0        5.0   *
      6. SE 164 E             *       877.0      944.0        5.0   *
      7. SE MID E             *       996.0     1059.0        5.0   *
      8. NE MID E             *       916.0     1134.0        5.0   *
      9. NE 164 E             *       800.0     1020.0        5.0   *
     10. NE 82 E              *       741.0      962.0        5.0   *
     11. NE CNR               *       680.0      915.0        5.0   *
     12. NE 82 N              *       628.0      964.0        5.0   *
     13. NE 164 N             *       570.0     1023.0        5.0   *
     14. NE MID N             *       454.0     1143.0        5.0   *
     15. NW MID N             *       391.0     1100.0        5.0   *
     16. NW 164 N             *       514.0      974.0        5.0   *
     17. NW 82 N              *       571.0      914.0        5.0   *
     18. NW CNR               *       621.0      855.0        5.0   *
     19. NW 82 W              *       570.0      797.0        5.0   *
     20. NW 164 W             *       512.0      740.0        5.0   *
     21. NW MID W             *       412.0      643.0        5.0   *
     22. SW MID W             *       484.0      558.0        5.0   *
     23. SW 164 W             *       589.0      658.0        5.0   *
     24. SW 82 W              *       649.0      715.0        5.0   *
     25. SW CNR               *       707.0      765.0        5.0   *
     26. SW 82 S              *       763.0      714.0        5.0   *
     27. SW 164 S             *       820.0      656.0        5.0   *
     28. SW MID S             *       919.0      554.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 1 26th & Wilshire (S1B3PM.DAT)                  RUN: Site 1 Build Alt3 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 140.  *    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 160.  *    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 165.  *    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 170.  *    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 180.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 200.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 205.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
1
                                                                                                                     PAGE  4
      JOB: Site 1 26th & Wilshire (S1B3PM.DAT)                 RUN: Site 1 Build Alt3 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 215.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 220.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 ------*-------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .1    .1    .1    .1    .2    .2    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .1
 DEGR. *   145   140   140    15     5     5    10    55    55    40    45     0     0     0   105   100   320    45   195   195

1
                                                                                                                     PAGE  5
      JOB: Site 1 26th & Wilshire (S1B3PM.DAT)                 RUN: Site 1 Build Alt3 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .1    .0    .0    .0    .0    .0    .0    .0
  65.  *    .1    .0    .0    .0    .0    .0    .0    .0
  70.  *    .1    .0    .0    .0    .0    .0    .0    .0
  75.  *    .1    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0
 180.  *    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1                                                                                                                             PAGE  6
      JOB: Site 1 26th & Wilshire (S1B3PM.DAT)                 RUN: Site 1 Build Alt3 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .1    .0    .0    .0    .0    .0    .0    .0
 DEGR. *   60     0     0     0     0     0     0     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT   55 DEGREES FROM REC8 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   55 DEGREES FROM REC9 .
 THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT  145 DEGREES FROM REC1 .
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 1 26th & Wilshire (S1B5AM.DAT)                  RUN: Site 1 Build Alt5 AM
      DATE: 03/19/2010   TIME: 08:43:23.32


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)           *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2      *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*-----------------------------------------*----------------------------------------------------------
        1. EB        Wil AP    *     -15.0     139.0     583.0     699.0 *     819.    47. AG   1254.    .8    .0 44.0
        2. EB        Wil T+R   *     584.0     699.0     715.0     824.0 *     181.    46. AG   1214.    .8    .0 44.0
        3. EB        Wil T+R Q *     672.0     783.0   -3390.4   -3136.0 *    5645.   226. AG     14. 100.0    .0 24.0 7.06 286.7
        4. EB        Wil LT    *     569.0     717.0     698.0     843.0 *     180.    46. AG     40.    .8    .0 32.0
        5. EB        Wil LT Q  *     654.0     800.0     643.5     789.8 *      15.   226. AG      7. 100.0    .0 12.0  .65    .7
        6. EB        Wil DP    *     715.0     824.0    1421.0    1528.0 *     997.    45. AG   1331.    .8    .0 44.0
        7. WB        Wil AP    *    1393.0    1557.0     810.0     982.0 *     819.   225. AG   1560.    .8    .0 44.0
        8. WB        Wil T+R   *     806.0     986.0     684.0     868.0 *     170.   226. AG   1439.    .8    .0 56.0
        9. WB        Wil T+R Q *     717.0     900.0    3962.8    4070.3 *    4537.    46. AG     21. 100.0    .0 36.0 7.60 230.5
       10. WB        Wil LT    *     824.0     966.0     707.0     850.0 *     165.   225. AG    121.    .8    .0 32.0
       11. WB        Wil LT Q  *     737.0     880.0    1187.5    1330.5 *     637.    45. AG      6. 100.0    .0 12.0 1.81  32.4
       12. WB        Wil DP    *     687.0     864.0     -35.0     163.0 *    1006.   226. AG   1550.    .8    .0 44.0
       13. SB        26 AP     *     553.0     971.0      -6.0    1547.0 *     803.   316. AG    823.    .8    .0 32.0
       14. SB        26 T+R    *     549.0     968.0     670.0     841.0 *     175.   136. AG    715.    .8    .0 44.0
       15. SB        26 T+R Q  *     633.0     880.0   -1575.6    3196.3 *    3200.   316. AG     14. 100.0    .0 24.0 5.49 162.6
       16. SB        26 LT     *     563.0     978.0     679.0     856.0 *     168.   136. AG    108.    .8    .0 32.0
       17. SB        26 LT Q   *     645.0     891.0     388.3    1163.8 *     375.   317. AG      6. 100.0    .0 12.0 1.37  19.0
       18. SB        26 DP     *     672.0     845.0    1384.0     114.0 *    1020.   136. AG    812.    .8    .0 32.0
       19. NB        26 AP     *     829.0     716.0    1410.0     138.0 *     820.   135. AG    669.    .8    .0 32.0
       20. NB        26 T+R    *     832.0     719.0     715.0     846.0 *     173.   317. AG    591.    .8    .0 44.0
       21. NB        26 T+R Q  *     759.0     798.0    2484.1   -1075.0 *    2546.   137. AG     14. 100.0    .0 24.0 4.61 129.4
       22. NB        26 L      *     818.0     710.0     705.0     832.0 *     166.   317. AG     78.    .8    .0 32.0
       23. NB        26 L Q    *     747.0     787.0     887.8     634.2 *     208.   137. AG      6. 100.0    .0 12.0 1.22  10.6
       24. NB        26 DP     *     712.0     843.0      13.0    1565.0 *    1005.   316. AG    707.    .8    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 1 26th & Wilshire (S1B5AM.DAT)                  RUN: Site 1 Build Alt5 AM
      DATE: 03/19/2010   TIME: 08:43:23.32

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE    SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC    TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*---------------------------------------------------------------------------------
        3. EB        Wil T+R Q *       90       59       2.0      1214        289       4.10      1        3
        5. EB        Wil LT Q  *       90       55       2.0        40        182       4.10      1        3
        9. WB        Wil T+R Q *       90       56       2.0      1439        190       4.10      1        3
       11. WB        Wil LT Q  *       90       50       2.0       121        170       4.10      1        3
       15. SB        26 T+R Q  *       90       56       2.0       715        196       4.10      1        3
       17. SB        26 LT Q   *       90       50       2.0       108        198       4.10      1        3
       21. NB        26 T+R Q  *       90       57       2.0       591        199       4.10      1        3
       23. NB        26 L Q    *       90       52       2.0        78        172       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)         *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*------------------------------------*
      1. SE MID S             *        967.0      615.0        5.0  *
      2. SE 164 S             *        874.0      710.0        5.0  *
      3. SE 82 S              *        816.0      771.0        5.0  *
      4. SE CNR               *        768.0      826.0        5.0  *
      5. SE 82 E              *        819.0      886.0        5.0  *
      6. SE 164 E             *        877.0      944.0        5.0  *
      7. SE MID E             *        996.0     1059.0        5.0  *
      8. NE MID E             *        916.0     1134.0        5.0  *
      9. NE 164 E             *        800.0     1020.0        5.0  *
     10. NE 82 E              *        741.0      962.0        5.0  *
     11. NE CNR               *        680.0      915.0        5.0  *
     12. NE 82 N              *        628.0      964.0        5.0  *
     13. NE 164 N             *        570.0     1023.0        5.0  *
     14. NE MID N             *        454.0     1143.0        5.0  *
     15. NW MID N             *        391.0     1100.0        5.0  *
     16. NW 164 N             *        514.0      974.0        5.0  *
     17. NW 82 N              *        571.0      914.0        5.0  *
     18. NW CNR               *        621.0      855.0        5.0  *
     19. NW 82 W              *        570.0      797.0        5.0  *
     20. NW 164 W             *        512.0      740.0        5.0  *
     21. NW MID W             *        412.0      643.0        5.0  *
     22. SW MID W             *        484.0      558.0        5.0  *
     23. SW 164 W             *        589.0      658.0        5.0  *
     24. SW 82 W              *        649.0      715.0        5.0  *
     25. SW CNR               *        707.0      765.0        5.0  *
     26. SW 82 S              *        763.0      714.0        5.0  *
     27. SW 164 S             *        820.0      656.0        5.0  *
     28. SW MID S             *        919.0      554.0        5.0  *
1
                                                                                                                 PAGE  3
      JOB: Site 1 26th & Wilshire (S1B5AM.DAT)                  RUN: Site 1 Build Alt5 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND   * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 140.  *    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 145.  *    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 160.  *    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 165.  *    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 170.  *    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 180.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
1
                                                                                                                 PAGE  4
      JOB: Site 1 26th & Wilshire (S1B5AM.DAT)                  RUN: Site 1 Build Alt5 AM

 WIND   * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 215.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 220.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .1
 DEGR. *  150   145   140   145     0     0     0    60    60    40    45     0     0     0   110   105   320    50   205   205

1
                                                                                                                 PAGE  5
      JOB: Site 1 26th & Wilshire (S1B5AM.DAT)                  RUN: Site 1 Build Alt5 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND   * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0
 180.  *    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
      JOB: Site 1 26th & Wilshire (S1B5AM.DAT)                  RUN: Site 1 Build Alt5 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .1    .1    .0    .0    .0    .0    .0
 240.  *    .0    .1    .1    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .1    .1    .1    .0    .0    .0    .0    .0
 DEGR. *  205   235   235     0     0     0     0     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT   60 DEGREES FROM REC8 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   60 DEGREES FROM REC9 .
 THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT  150 DEGREES FROM REC1 .
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 1 26th & Wilshire (S1B5PM.DAT)                  RUN: Site 1 Build Alt5 PM
      DATE: 03/19/2010   TIME: 08:43:42.60


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *    -15.0     139.0     583.0     699.0 *     819.   47. AG    1492.    .8    .0 44.0
       2. EB        Wil T+R   *    584.0     699.0     715.0     824.0 *     181.   46. AG    1405.    .8    .0 44.0
       3. EB        Wil T+R Q *    672.0     783.0   -4056.1   -3778.3 *    6570.  226. AG      14. 100.0    .0 24.0 7.55 333.7
       4. EB        Wil LT    *    569.0     717.0     698.0     843.0 *     180.   46. AG      87.    .8    .0 32.0
       5. EB        Wil LT Q  *    654.0     800.0     421.0     572.8 *     325.  226. AG       6. 100.0    .0 12.0 1.40  16.5
       6. EB        Wil DP    *    715.0     824.0    1421.0    1528.0 *     997.   45. AG    1722.    .8    .0 44.0
       7. WB        Wil AP    *   1393.0    1557.0     810.0     982.0 *     819.  225. AG    1720.    .8    .0 44.0
       8. WB        Wil T+R   *    806.0     986.0     684.0     868.0 *     170.  226. AG    1593.    .8    .0 56.0
       9. WB        Wil T+R Q *    717.0     900.0    4325.9    4425.0 *    5045.   46. AG      20. 100.0    .0 36.0 7.93 256.3
      10. WB        Wil LT    *    824.0     966.0     707.0     850.0 *     165.  225. AG     127.    .8    .0 32.0
      11. WB        Wil LT Q  *    737.0     880.0    1247.7    1390.7 *     722.   45. AG       6. 100.0    .0 12.0 1.95  36.7
      12. WB        Wil DP    *    687.0     864.0     -35.0     163.0 *    1006.  226. AG    1718.    .8    .0 44.0
      13. SB        26 AP     *    553.0     971.0      -6.0    1547.0 *     803.  316. AG     846.    .8    .0 32.0
      14. SB        26 T+R    *    549.0     968.0     670.0     841.0 *     175.  136. AG     677.    .8    .0 44.0
      15. SB        26 T+R Q  *    633.0     880.0   -1467.6    3083.0 *    3044.  316. AG      14. 100.0    .0 24.0 5.54 154.6
      16. SB        26 LT     *    563.0     978.0     679.0     856.0 *     168.  136. AG     169.    .8    .0 32.0
      17. SB        26 LT Q   *    645.0     891.0    -152.7    1738.5 *    1164.  317. AG       6. 100.0    .0 12.0 2.56  59.1
      18. SB        26 DP     *    672.0     845.0    1384.0     114.0 *    1020.  136. AG     778.    .8    .0 32.0
      19. NB        26 AP     *    829.0     716.0    1410.0     138.0 *     820.  135. AG     930.    .8    .0 32.0
      20. NB        26 T+R    *    832.0     719.0     715.0     846.0 *     173.  317. AG     834.    .8    .0 44.0
      21. NB        26 T+R Q  *    759.0     798.0    3408.0   -2078.0 *    3910.  137. AG      14. 100.0    .0 24.0 6.95 198.6
      22. NB        26 L      *    818.0     710.0     705.0     832.0 *     166.  317. AG      96.    .8    .0 32.0
      23. NB        26 L Q    *    747.0     787.0    1019.5     491.2 *     402.  137. AG       7. 100.0    .0 12.0 1.50  20.4
      24. NB        26 DP     *    712.0     843.0      13.0    1565.0 *    1005.  316. AG     770.    .8    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 1 26th & Wilshire (S1B5PM.DAT)                  RUN: Site 1 Build Alt5 PM
      DATE: 03/19/2010   TIME: 08:43:42.60

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R Q *      90       57       2.0      1405        289       4.10      1        3
       5. EB        Wil LT Q  *      90       53       2.0        87        171       4.10      1        3
       9. WB        Wil T+R Q *      90       55       2.0      1593        196       4.10      1        3
      11. WB        Wil LT Q  *      90       50       2.0       127        164       4.10      1        3
      15. SB        26 T+R Q  *      90       57       2.0       677        190       4.10      1        3
      17. SB        26 LT Q   *      90       52       2.0       169        175       4.10      1        3
      21. NB        26 T+R Q  *      90       58       2.0       834        193       4.10      1        3
      23. NB        26 L Q    *      90       54       2.0        96        180       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       967.0      615.0        5.0   *
      2. SE 164 S             *       874.0      710.0        5.0   *
      3. SE 82 S              *       816.0      771.0        5.0   *
      4. SE CNR               *       768.0      826.0        5.0   *
      5. SE 82 E              *       819.0      886.0        5.0   *
      6. SE 164 E             *       877.0      944.0        5.0   *
      7. SE MID E             *       996.0     1059.0        5.0   *
      8. NE MID E             *       916.0     1134.0        5.0   *
      9. NE 164 E             *       800.0     1020.0        5.0   *
     10. NE 82 E              *       741.0      962.0        5.0   *
     11. NE CNR               *       680.0      915.0        5.0   *
     12. NE 82 N              *       628.0      964.0        5.0   *
     13. NE 164 N             *       570.0     1023.0        5.0   *
     14. NE MID N             *       454.0     1143.0        5.0   *
     15. NW MID N             *       391.0     1100.0        5.0   *
     16. NW 164 N             *       514.0      974.0        5.0   *
     17. NW 82 N              *       571.0      914.0        5.0   *
     18. NW CNR               *       621.0      855.0        5.0   *
     19. NW 82 W              *       570.0      797.0        5.0   *
     20. NW 164 W             *       512.0      740.0        5.0   *
     21. NW MID W             *       412.0      643.0        5.0   *
     22. SW MID W             *       484.0      558.0        5.0   *
     23. SW 164 W             *       589.0      658.0        5.0   *
     24. SW 82 W              *       649.0      715.0        5.0   *
     25. SW CNR               *       707.0      765.0        5.0   *
     26. SW 82 S              *       763.0      714.0        5.0   *
     27. SW 164 S             *       820.0      656.0        5.0   *
     28. SW MID S             *       919.0      554.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 1 26th & Wilshire (S1B5PM.DAT)                  RUN: Site 1 Build Alt5 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .0    .1    .1    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 140.  *    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 160.  *    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 165.  *    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 170.  *    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 180.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 200.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 205.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
1
                                                                                                                     PAGE  4
      JOB: Site 1 26th & Wilshire (S1B5PM.DAT)                  RUN: Site 1 Build Alt5 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 215.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 220.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 ------*-------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .1    .1    .1    .1    .2    .2    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .1
 DEGR. *  145   140   140    20     5     5    10    55    55    40    45     0     0     0   105   100   320    50   195   195

1
                                                                                                                     PAGE  5
      JOB: Site 1 26th & Wilshire (S1B5PM.DAT)                  RUN: Site 1 Build Alt5 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*-------------------------------------------------
  0.  *    .0    .0    .0    .0    .0    .0    .0    .0
  5.  *    .0    .0    .0    .0    .0    .0    .0    .0
 10.  *    .0    .0    .0    .0    .0    .0    .0    .0
 15.  *    .0    .0    .0    .0    .0    .0    .0    .0
 20.  *    .0    .0    .0    .0    .0    .0    .0    .0
 25.  *    .0    .0    .0    .0    .0    .0    .0    .0
 30.  *    .0    .0    .0    .0    .0    .0    .0    .0
 35.  *    .0    .0    .0    .0    .0    .0    .0    .0
 40.  *    .0    .0    .0    .0    .0    .0    .0    .0
 45.  *    .0    .0    .0    .0    .0    .0    .0    .0
 50.  *    .0    .0    .0    .0    .0    .0    .0    .0
 55.  *    .0    .0    .0    .0    .0    .0    .0    .0
 60.  *    .1    .0    .0    .0    .0    .0    .0    .0
 65.  *    .1    .0    .0    .0    .0    .0    .0    .0
 70.  *    .1    .0    .0    .0    .0    .0    .0    .0
 75.  *    .1    .0    .0    .0    .0    .0    .0    .0
 80.  *    .0    .0    .0    .0    .0    .0    .0    .0
 85.  *    .0    .0    .0    .0    .0    .0    .0    .0
 90.  *    .0    .0    .0    .0    .0    .0    .0    .0
 95.  *    .0    .0    .0    .0    .0    .0    .0    .0
100.  *    .0    .0    .0    .0    .0    .0    .0    .0
105.  *    .0    .0    .0    .0    .0    .0    .0    .0
110.  *    .0    .0    .0    .0    .0    .0    .0    .0
115.  *    .0    .0    .0    .0    .0    .0    .0    .0
120.  *    .0    .0    .0    .0    .0    .0    .0    .0
125.  *    .0    .0    .0    .0    .0    .0    .0    .0
130.  *    .0    .0    .0    .0    .0    .0    .0    .0
135.  *    .0    .0    .0    .0    .0    .0    .0    .0
140.  *    .0    .0    .0    .0    .0    .0    .0    .0
145.  *    .0    .0    .0    .0    .0    .0    .0    .0
150.  *    .0    .0    .0    .0    .0    .0    .0    .0
155.  *    .0    .0    .0    .0    .0    .0    .0    .0
160.  *    .0    .0    .0    .0    .0    .0    .0    .0
165.  *    .0    .0    .0    .0    .0    .0    .0    .0
170.  *    .0    .0    .0    .0    .0    .0    .0    .0
175.  *    .0    .0    .0    .0    .0    .0    .0    .0
180.  *    .0    .0    .0    .0    .0    .0    .0    .0
185.  *    .0    .0    .0    .0    .0    .0    .0    .0
190.  *    .0    .0    .0    .0    .0    .0    .0    .0
195.  *    .1    .0    .0    .0    .0    .0    .0    .0
200.  *    .1    .0    .0    .0    .0    .0    .0    .0
205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1                                                                                                              PAGE  6
     JOB: Site 1 26th & Wilshire (S1B5PM.DAT)                 RUN: Site 1 Build Alt5 PM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*-------------------------------------------------
210.  *    .1    .0    .0    .0    .0    .0    .0    .0
215.  *    .1    .0    .0    .0    .0    .0    .0    .0
220.  *    .0    .0    .0    .0    .0    .0    .0    .0
225.  *    .0    .0    .0    .0    .0    .0    .0    .0
230.  *    .0    .0    .0    .0    .0    .0    .0    .0
235.  *    .0    .0    .0    .0    .0    .0    .0    .0
240.  *    .0    .0    .0    .0    .0    .0    .0    .0
245.  *    .0    .0    .0    .0    .0    .0    .0    .0
250.  *    .0    .0    .0    .0    .0    .0    .0    .0
255.  *    .0    .0    .0    .0    .0    .0    .0    .0
260.  *    .0    .0    .0    .0    .0    .0    .0    .0
265.  *    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .0    .0    .0    .0    .0
360.  *    .0    .0    .0    .0    .0    .0    .0    .0
------*-------------------------------------------------
MAX   *    .1    .0    .0    .0    .0    .0    .0    .0
DEGR. *   60     0     0     0     0     0     0     0

THE HIGHEST CONCENTRATION IS     .20 PPM AT   55 DEGREES FROM REC8 .
THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   55 DEGREES FROM REC9 .
THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT  145 DEGREES FROM REC1 .
```

Site 2 – Veterans & Wilshire
Input Files

```
Site 2 Veteran & Wilshire (S2EXAM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 Existing AM                       27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    4350 3.3   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    4350 3.3   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3824 3.3   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        56       2.0 3824   11.1  999 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     526 3.3   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       118       2.0  526   11.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3918 3.3   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    2511 3.3   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    2443 3.3   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        82       2.0 2443   11.1 1009 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      68 3.3   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       142       2.0   68   11.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    2828 3.3   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    2828 3.3   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     992 3.5   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     842 3.5   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       111       2.0  842   20.5  964 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     150 3.5   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150       106       2.0  150   20.5  955 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1188 3.5   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1188 3.5   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.     440 3.5   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     235 3.5   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       120       2.0  235   20.5  829 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     205 3.5   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        90       2.0  205   20.5  834 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     359 3.5   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2EXPM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 Existing PM                       27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    2564 3.3   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    2564 3.3   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    2293 3.3   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        60       2.0 2293   20.5  999 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     271 3.3   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       126       2.0  271   20.5 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    2453 3.3   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    2853 3.3   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    2778 3.3   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        77       2.0 2778   20.5 1010 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      75 3.3   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   75   20.5 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3732 3.3   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3732 3.3   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1155 3.5   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     957 3.5   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       107       2.0  957   20.5  860 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     198 3.5   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150       102       2.0  198   20.5  927 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.     984 3.5   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.     984 3.5   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1132 3.5   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     422 3.5   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       116       2.0  422   20.5  817 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     710 3.5   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        94       2.0  710   20.5  808 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     535 3.5   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2NBAM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 NO BUILD AM                        27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5619 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5619 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4678 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        57       2.0 4678   4.1  983 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     941 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       118       2.0  941   4.1  995 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4869 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3164 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3147 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        82       2.0 3147   4.1 1084 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      17 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   17   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3437 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3437 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     946 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     814 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       111       2.0  814   4.1  875 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150       106       2.0  132   4.1  955 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1787 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1787 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1155 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     833 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       120       2.0  833   4.1  852 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     322 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        90       2.0  322   4.1  834 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     791 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2NBPM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 NO BUILD PM                       27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3358 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3358 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3073 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        68       2.0 3073   4.1  982 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     285 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       126       2.0  285   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3305 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4295 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4276 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        85       2.0 4276   4.1  982 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      19 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   19   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    4969 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    4969 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1351 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1028 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150        97       2.0 1028   4.1  790 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     323 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150        95       2.0  323   4.1  955 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1719 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1719 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1987 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     858 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       109       2.0  858   4.1  810 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1129 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        87       2.0 1129   4.1  804 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     968 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B1AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 BUILD ALT1 AM                     27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5595 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5595 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4672 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.   48   4
       150        59       2.0 4672   4.1  981 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     923 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.   24   2
       150       118       2.0  923   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4826 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3179 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3160 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.   48   4
       150        84       2.0 3160   4.1  997 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      19 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   19   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3487 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3487 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     959 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     827 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       109       2.0  827   4.1  877 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150       104       2.0  132   4.1  885 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1751 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1751 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1151 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     820 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       120       2.0  820   4.1  858 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     331 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        90       2.0  331   4.1  834 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     817 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B1PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 BUILD ALT1 PM                     27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3430 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3430 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3138 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        65       2.0 3138   4.1  984 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     292 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       128       2.0  292   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3339 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4302 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4286 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        82       2.0 4286   4.1  979 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      16 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   16   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    4930 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    4930 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1373 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1090 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       100       2.0 1090   4.1  782 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     283 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150        95       2.0  283   4.1  885 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1841 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1841 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1997 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     894 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       109       2.0  800   4.1  858 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1103 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        90       2.0 1103   4.1  800 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     992 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B2AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 BUILD ALT2 AM                     27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5509 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5509 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4596 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        57       2.0 4596   4.1  969 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     913 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       118       2.0  913   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4761 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3138 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3121 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        82       2.0 3121   4.1  995 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      17 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   17   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3409 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3409 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     947 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     815 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       111       2.0  815   4.1  888 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150       106       2.0  132   4.1  967 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1755 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1755 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1085 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     767 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       120       2.0  767   4.1  852 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     318 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        90       2.0  318   4.1  837 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     751 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B2PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.        5.0
SE 164 S                  942.      686.        5.0
SE 82 S                   892.      756.        5.0
SE CNR                    869.      821.        5.0
SE 82 E                   925.      853.        5.0
SE 164 E                 1005.      880.        5.0
SE MID E                 1219.      947.        5.0
NE MID E                 1144.     1099.        5.0
NE 164 E                  918.     1026.        5.0
NE 82 E                   838.     1000.        5.0
NE CNR                    759.      983.        5.0
NE 82 N                   716.     1047.        5.0
NE 164 N                  676.     1120.        5.0
NE MID N                  595.     1269.        5.0
NW MID N                  464.     1209.        5.0
NW 164 N                  546.     1079.        5.0
NW 82 N                   589.     1010.        5.0
NW CNR                    611.      945.        5.0
NW 82 W                   552.      910.        5.0
NW 164 W                  475.      884.        5.0
NW MID W                  273.      815.        5.0
SW MID W                  305.      649.        5.0
SW 164 W                  565.      737.        5.0
SW 82 W                   645.      764.        5.0
SW CNR                    718.      779.        5.0
SW 82 S                   774.      718.        5.0
SW 164 S                  824.      646.        5.0
SW MID S                  957.      459.        5.0
Site 2 BUILD ALT2 PM                     27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3358 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3358 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3074 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        70       2.0 3074   4.1  971 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     284 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       131       2.0  284   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3319 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4364 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4346 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        82       2.0 4346   4.1  981 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      18 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   18   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    5006 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    5006 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1384 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1053 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150        95       2.0 1053   4.1  784 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     331 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150        93       2.0  331   4.1  929 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1795 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1795 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    2004 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     886 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       109       2.0  886   4.1  812 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1118 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        89       2.0 1118   4.1  797 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     990 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B3AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 BUILD ALT3 AM                     27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5495 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5495 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4593 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        57       2.0 4593   4.1  969 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     902 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       118       2.0  902   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4799 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3158 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3142 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        82       2.0 3142   4.1  995 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      16 0.8   0  44   30.
```

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  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   16   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3429 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3429 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     932 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     800 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       108       2.0  800   4.1  885 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150       106       2.0  132   4.1  959 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1754 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1754 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1134 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     795 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       120       2.0  795   4.1  853 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     339 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        90       2.0  339   4.1  859 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     737 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B3PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 BUILD ALT3 PM                     27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3401 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3401 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3112 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150         68       2.0 3112   4.1  977 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     289 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150        127       2.0  289   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3325 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4274 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4256 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150         83       2.0 4256   4.1  982 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      18 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   18   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    4918 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    4918 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1362 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1091 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       100       2.0 1091   4.1  776 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     271 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150        95       2.0  271   4.1  933 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1792 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1792 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1983 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     912 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       109       2.0  912   4.1  800 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1074 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        88       2.0 1074   4.1  804 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     985 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
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```
Site 2 Veteran & Wilshire (S2B4AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 BUILD ALT4 AM                     27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5553 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5553 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4635 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150         57       2.0 4635   4.1  968 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     918 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150        118       2.0  918   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4832 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3177 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3161 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150         82       2.0 3161   4.1  994 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      16 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   16   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    3438 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    3438 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.     949 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.     817 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       111       2.0  817   4.1  859 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150       106       2.0  132   4.1  955 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1787 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1787 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1182 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     853 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       120       2.0  853   4.1  834 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.     329 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        90       2.0  329   4.1  834 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     807 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B4PM.DAT)  60.0321.0.0000.000280.30480000     1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 BUILD ALT4 PM                     27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3310 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3310 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3031 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        68       2.0 3031   4.1  969 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     279 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       126       2.0  279   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3239 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4265 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4246 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        85       2.0 4246   4.1  984 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      19 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   19   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    5001 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    5001 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1387 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1067 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       100       2.0 1067   4.1  782 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     320 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150        95       2.0  320   4.1  928 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1703 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1703 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1982 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     871 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       111       2.0  871   4.1  806 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1111 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        87       2.0 1111   4.1  804 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     999 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B5AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 BUILD ALT5 AM                     27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    5547 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    5547 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    4619 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        57       2.0 4619   4.1  966 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     928 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       118       2.0  928   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    4794 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    3154 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    3137 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        81       2.0 3137   4.1  994 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      17 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   17   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.     3424 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.     3424 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.      931 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.      799 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150       111       2.0  799   4.1  887 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.      132 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150       106       2.0  132   4.1  955 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.     1771 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.     1771 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.     1108 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.      777 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       120       2.0  777   4.1  834 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.      331 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        90       2.0  331   4.1  834 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.      748 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 2 Veteran & Wilshire (S2B5PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                 1066.      492.       5.0
SE 164 S                  942.      686.       5.0
SE 82 S                   892.      756.       5.0
SE CNR                    869.      821.       5.0
SE 82 E                   925.      853.       5.0
SE 164 E                 1005.      880.       5.0
SE MID E                 1219.      947.       5.0
NE MID E                 1144.     1099.       5.0
NE 164 E                  918.     1026.       5.0
NE 82 E                   838.     1000.       5.0
NE CNR                    759.      983.       5.0
NE 82 N                   716.     1047.       5.0
NE 164 N                  676.     1120.       5.0
NE MID N                  595.     1269.       5.0
NW MID N                  464.     1209.       5.0
NW 164 N                  546.     1079.       5.0
NW 82 N                   589.     1010.       5.0
NW CNR                    611.      945.       5.0
NW 82 W                   552.      910.       5.0
NW 164 W                  475.      884.       5.0
NW MID W                  273.      815.       5.0
SW MID W                  305.      649.       5.0
SW 164 W                  565.      737.       5.0
SW 82 W                   645.      764.       5.0
SW CNR                    718.      779.       5.0
SW 82 S                   774.      718.       5.0
SW 164 S                  824.      646.       5.0
SW MID S                  957.      459.       5.0
Site 2 BUILD ALT5 PM                     27  1   0
  1
EB        Wil AP    AG  -172.   469.    78.   601.    3396 0.8   0  68   30.
  1
EB        Wil AP    AG    78.   601.   276.   684.    3396 0.8   0  68   30.
  1
EB        Wil T+R   AG   276.   684.   778.   856.    3109 0.8   0  68   30.
  2
EB        Wil T+R Q AG   678.   822.   304.   693.      0.  48   4
       150        71       2.0 3109   4.1  969 1 3
  1
EB        Wil LT    AG   259.   724.   761.   889.     287 0.8   0  44   30.
  2
EB        Wil LT Q  AG   659.   855.   296.   736.      0.  24   2
       150       132       2.0  287   4.1 1084 1 3
  1
EB        Wil DP    AG   782.   851.  1703.  1145.    3318 0.8   0  68   30.
  1
WB        Wil AP    AG  1025.  1019.  1677.  1228.    4322 0.8   0  68   30.
  1
WB        Wil T+R   AG  1025.  1019.   717.   920.    4305 0.8   0  68   30.
  2
WB        Wil T+R Q AG   798.   946.  1023.  1018.      0.  48   4
       150        82       2.0 4305   4.1  981 1 3
  1
WB        Wil LT    AG  1040.   975.   742.   883.      17 0.8   0  44   30.
```

```
  2
WB        Wil LT Q  AG   824.   908.  1030.   971.      0.  24   2
       150       143       2.0   17   4.1 1084 1 3
  1
WB        Wil DP    AG   715.   922.   201.   748.    4984 0.8   0  68   30.
  1
WB        Wil DP    AG   201.   748.  -199.   546.    4984 0.8   0  68   30.
  1
NB        Vet AP    AG   967.   583.  1327.    75.    1370 0.9   0  32   30.
  1
NB        Vet T+LT  AG   960.   579.   781.   840.    1075 0.9   0  56   30.
  2
NB        Vet T+LT QAG   820.   783.   957.   583.      0.  36   3
       150        97       2.0 1075   4.1  795 1 3
  1
NB        Vet RT    AG   964.   622.   813.   839.     295 0.9   0  32   30.
  2
NB        Vet RT Q  AG   847.   791.   953.   637.      0.  12   1
       150        92       2.0  295   4.1  929 1 3
  1
NB        Vet DP    AG   798.   836.   611.  1170.    1793 0.9   0  44   30.
  1
NB        Vet DP    AG   611.  1170.   214.  1729.    1793 0.9   0  44   30.
  1
SB        Vet AP    AG   544.  1188.   172.  1701.    1986 0.9   0  44   30.
  1
SB        Vet T+LT  AG   550.  1188.   730.   898.     876 0.9   0  56   30.
  2
SB        Vet T+LT QAG   679.   981.   556.  1179.      0.  36   3
       150       108       2.0  876   4.1  812 1 3
  1
SB        Vet RT    AG   521.  1169.   695.   888.    1110 0.9   0  44   30.
  2
SB        Vet RT Q  AG   643.   972.   527.  1159.      0.  24   2
       150        90       2.0 1110   4.1  794 1 3
  1
SB        Vet DP    AG   703.   889.  1292.    46.     979 0.9   0  44   30.
1.0   04 1000.   0Y  5  0 72
```

Site 2 – Veterans & Wilshire
Output Files

```
1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2EXAM.DAT)               RUN: Site 2 Existing AM
      DATE: 03/19/2010   TIME: 09:05:18.18


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =    .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *   -172.0     469.0      78.0     601.0 *     283.   62. AG    4350.   3.3   .0 68.0
       2. EB        Wil AP    *     78.0     601.0     276.0     684.0 *     215.   67. AG    4350.   3.3   .0 68.0
       3. EB        Wil T+R   *    276.0     684.0     778.0     856.0 *     531.   71. AG    3824.   3.3   .0 68.0
       4. EB        Wil T+R Q *    678.0     822.0   -3100.5    -481.3 *    3997.  251. AG      44. 100.0   .0 48.0 1.60 203.0
       5. EB        Wil LT    *    259.0     724.0     761.0     889.0 *     528.   72. AG     526.   3.3   .0 44.0
       6. EB        Wil LT Q  *    659.0     855.0    -158.3     587.1 *     860.  252. AG      47. 100.0   .0 24.0 1.30  43.7
       7. EB        Wil DP    *    782.0     851.0    1703.0    1145.0 *     967.   72. AG    3918.   3.3   .0 68.0
       8. WB        Wil AP    *   1025.0    1019.0    1677.0    1228.0 *     685.   72. AG    2511.   3.3   .0 68.0
       9. WB        Wil T+R   *   1025.0    1019.0     717.0     920.0 *     324.  252. AG    2443.   3.3   .0 68.0
      10. WB        Wil T+R Q *    798.0     946.0    2882.1    1612.9 *    2188.   72. AG      65. 100.0   .0 48.0 1.42 111.2
      11. WB        Wil LT    *   1040.0     975.0     742.0     883.0 *     312.  253. AG      68.   3.3   .0 44.0
      12. WB        Wil LT Q  *    824.0     908.0     935.8     942.2 *     117.   73. AG      56. 100.0   .0 24.0 1.21   5.9
      13. WB        Wil DP    *    715.0     922.0     201.0     748.0 *     543.  251. AG    2828.   3.3   .0 68.0
      14. WB        Wil DP    *    201.0     748.0    -199.0     546.0 *     448.  243. AG    2828.   3.3   .0 68.0
      15. NB        Vet AP    *    967.0     583.0    1327.0      75.0 *     623.  145. AG     992.   3.5   .0 32.0
      16. NB        Vet T+LT  *    960.0     579.0     781.0     840.0 *     316.  326. AG     842.   3.5   .0 56.0
      17. NB        Vet T+LT Q*    820.0     783.0    1279.0     113.0 *     812.  146. AG     122. 100.0   .0 36.0 1.25  41.3
      18. NB        Vet RT    *    964.0     622.0     813.0     839.0 *     264.  325. AG     150.   3.5   .0 32.0
      19. NB        Vet RT Q  *    847.0     791.0     896.3     719.4 *      87.  145. AG      39. 100.0   .0 12.0  .59   4.4
      20. NB        Vet DP    *    798.0     836.0     611.0    1170.0 *     383.  331. AG    1188.   3.5   .0 44.0
      21. NB        Vet DP    *    611.0    1170.0     214.0    1729.0 *     686.  325. AG    1188.   3.5   .0 44.0
      22. SB        Vet AP    *    544.0    1188.0     172.0    1701.0 *     634.  324. AG     440.   3.5   .0 44.0
      23. SB        Vet T+LT  *    550.0    1188.0     730.0     898.0 *     341.  148. AG     235.   3.5   .0 56.0
      24. SB        Vet T+LT Q*    679.0     981.0     652.0    1024.5 *      51.  328. AG     132. 100.0   .0 36.0  .55   2.6
      25. SB        Vet RT    *    521.0    1169.0     695.0     888.0 *     331.  148. AG     205.   3.5   .0 44.0
      26. SB        Vet RT Q  *    643.0     972.0     616.5    1014.7 *      50.  328. AG      66. 100.0   .0 24.0  .33   2.6
      27. SB        Vet DP    *    703.0     889.0    1292.0      46.0 *    1028.  145. AG     359.   3.5   .0 44.0
1
                                                                                                                 PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2EXAM.DAT)               RUN: Site 2 Existing AM
      DATE: 03/19/2010   TIME: 09:05:18.18

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *     150       56       2.0      3824        999      11.10      1        3
       6. EB        Wil LT Q  *     150      118       2.0       526       1084      11.10      1        3
      10. WB        Wil T+R Q *     150       82       2.0      2443       1009      11.10      1        3
      12. WB        Wil LT Q  *     150      142       2.0        68       1084      11.10      1        3
      17. NB        Vet T+LT Q*     150      111       2.0       842        964      20.50      1        3
      19. NB        Vet RT Q  *     150      106       2.0       150        955      20.50      1        3
      24. SB        Vet T+LT Q*     150      120       2.0       235        829      20.50      1        3
      26. SB        Vet RT Q  *     150       90       2.0       205        834      20.50      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       1066.0      492.0        5.0  *
      2. SE 164 S             *        942.0      686.0        5.0  *
      3. SE 82 S              *        892.0      756.0        5.0  *
      4. SE CNR               *        869.0      821.0        5.0  *
      5. SE 82 E              *        925.0      853.0        5.0  *
      6. SE 164 E             *       1005.0      880.0        5.0  *
      7. SE MID E             *       1219.0      947.0        5.0  *
      8. NE MID E             *       1144.0     1099.0        5.0  *
      9. NE 164 E             *        918.0     1026.0        5.0  *
     10. NE 82 E              *        838.0     1000.0        5.0  *
     11. NE CNR               *        759.0      983.0        5.0  *
     12. NE 82 N              *        716.0     1047.0        5.0  *
     13. NE 164 N             *        676.0     1120.0        5.0  *
     14. NE MID N             *        595.0     1269.0        5.0  *
     15. NW MID N             *        464.0     1209.0        5.0  *
     16. NW 164 N             *        546.0     1079.0        5.0  *
     17. NW 82 N              *        589.0     1010.0        5.0  *
     18. NW CNR               *        611.0      945.0        5.0  *
     19. NW 82 W              *        552.0      910.0        5.0  *
     20. NW 164 W             *        475.0      884.0        5.0  *
     21. NW MID W             *        273.0      815.0        5.0  *
     22. SW MID W             *        305.0      649.0        5.0  *
     23. SW 164 W             *        565.0      737.0        5.0  *
     24. SW 82 W              *        645.0      764.0        5.0  *
     25. SW CNR               *        718.0      779.0        5.0  *
     26. SW 82 S              *        774.0      718.0        5.0  *
     27. SW 164 S             *        824.0      646.0        5.0  *
     28. SW MID S             *        957.0      459.0        5.0  *
1
                                                                                                                 PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2EXAM.DAT)               RUN: Site 2 Existing AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

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                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *   .1    .2    .4    .6    .5    .5    .5    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .1    .0    .0
   5.  *   .1    .1    .4    .6    .5    .5    .5    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .1    .0    .0
  10.  *   .1    .1    .4    .6    .6    .7    .6    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .1    .0    .0
  15.  *   .1    .1    .4    .6    .6    .6    .6    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .3    .0    .0
  20.  *   .1    .1    .4    .6    .6    .6    .6    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .3    .0    .0
  25.  *   .1    .2    .3    .5    .6    .6    .6    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .3    .0    .0
  30.  *   .1    .2    .3    .6    .7    .6    .6    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .3    .0    .0
  35.  *   .1    .3    .4    .6    .7    .6    .6    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .3    .0    .0
  40.  *   .1    .3    .4    .7    .7    .7    .7    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .3    .1    .0
  45.  *   .0    .3    .4    .6    .7    .7    .7    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .3    .1    .0
  50.  *   .0    .2    .4    .6    .7    .7    .7    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .3    .1    .0
  55.  *   .0    .2    .4    .6    .7    .8    .7    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1    .3    .1    .1
  60.  *   .0    .1    .4    .6    .7    .8    .7    .2    .2    .3    .1    .0    .0    .0    .1    .1    .1    .2    .2    .1
  65.  *   .0    .1    .2    .6    .7    .7    .7    .3    .3    .3    .3    .0    .0    .0    .1    .1    .2    .4    .3    .2
  70.  *   .0    .0    .1    .4    .6    .7    .5    .4    .5    .5    .4    .1    .0    .0    .1    .1    .4    .6    .4    .5
  75.  *   .0    .0    .1    .2    .3    .4    .3    .6    .6    .6    .6    .2    .0    .0    .1    .1    .4    .5    .6    .5
  80.  *   .0    .0    .0    .1    .2    .3    .2    .6    .7    .6    .6    .3    .1    .0    .1    .2    .6    .6    .5    .6
  85.  *   .0    .0    .0    .1    .2    .2    .1    .6    .9    .9    .7    .3    .3    .0    .1    .3    .7    .6    .7    .7
  90.  *   .0    .0    .0    .0    .1    .1    .1    .8    .9    .9    .7    .4    .3    .0    .1    .4    .7    .6    .7    .6
  95.  *   .0    .0    .0    .0    .1    .1    .1    .7    .7    .8    .7    .4    .3    .0    .1    .3    .7    .6    .6    .5
 100.  *   .0    .0    .0    .0    .0    .0    .0    .7    .7    .7    .7    .3    .3    .1    .1    .4    .6    .6    .5    .5
 105.  *   .0    .0    .0    .0    .0    .0    .0    .7    .7    .7    .7    .3    .2    .1    .1    .4    .6    .5    .5    .6
 110.  *   .0    .0    .0    .0    .0    .0    .0    .7    .7    .7    .6    .3    .3    .1    .1    .4    .5    .5    .5    .7
 115.  *   .0    .0    .0    .0    .0    .0    .0    .7    .6    .7    .6    .3    .3    .1    .1    .4    .5    .5    .6    .7
 120.  *   .0    .0    .0    .0    .0    .0    .0    .7    .6    .7    .6    .3    .3    .1    .1    .4    .6    .5    .6    .7
 125.  *   .0    .0    .0    .0    .0    .0    .0    .7    .6    .6    .6    .3    .3    .1    .2    .4    .6    .5    .6    .8
 130.  *   .0    .0    .1    .0    .0    .0    .0    .6    .6    .7    .5    .3    .2    .1    .2    .3    .5    .4    .6    .8
 135.  *   .1    .1    .1    .1    .0    .0    .0    .6    .6    .7    .6    .3    .2    .1    .1    .4    .4    .4    .7    .8
 140.  *   .2    .1    .2    .1    .0    .0    .0    .6    .6    .7    .6    .3    .3    .1    .1    .3    .4    .5    .6    .6
 145.  *   .3    .3    .2    .2    .1    .0    .0    .6    .6    .8    .5    .4    .4    .2    .1    .3    .3    .5    .7    .6
 150.  *   .4    .4    .3    .2    .1    .0    .0    .6    .6    .8    .5    .4    .4    .2    .2    .3    .3    .5    .7    .7
 155.  *   .4    .4    .4    .2    .1    .0    .0    .6    .7    .8    .6    .4    .4    .2    .2    .2    .2    .4    .7    .7
 160.  *   .5    .4    .5    .3    .1    .1    .0    .6    .7    .8    .5    .5    .4    .2    .2    .2    .2    .4    .7    .7
 165.  *   .5    .4    .5    .4    .2    .1    .0    .6    .7    .8    .6    .4    .4    .3    .2    .2    .2    .4    .7    .7
 170.  *   .5    .4    .6    .5    .2    .1    .0    .6    .7    .8    .6    .5    .4    .3    .2    .2    .2    .4    .7    .7
 175.  *   .5    .4    .5    .5    .2    .1    .0    .6    .7    .8    .6    .4    .5    .3    .2    .2    .2    .4    .7    .7
 180.  *   .5    .4    .5    .5    .2    .1    .0    .7    .8    .8    .4    .5    .5    .3    .2    .2    .2    .5    .6    .6
 185.  *   .5    .4    .5    .5    .2    .1    .1    .7    .8    .7    .4    .3    .4    .3    .2    .2    .2    .6    .7    .7
 190.  *   .4    .4    .5    .4    .2    .1    .1    .7    .8    .6    .4    .3    .4    .3    .2    .2    .2    .6    .7    .7
 195.  *   .4    .4    .5    .4    .1    .1    .1    .7    .8    .6    .5    .4    .4    .3    .1    .2    .2    .6    .7    .7
 200.  *   .4    .4    .5    .4    .1    .1    .1    .7    .8    .6    .6    .4    .4    .3    .1    .2    .2    .6    .7    .7
 205.  *   .4    .4    .5    .3    .1    .1    .1    .8    .8    .6    .6    .4    .3    .2    .0    .2    .2    .6    .7    .7
1
                                                                                                                   PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2EXAM.DAT)               RUN: Site 2 Existing AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *   .4    .4    .5    .3    .1    .1    .1    .8    .8    .6    .6    .4    .3    .1    .0    .2    .2    .7    .7    .7
 215.  *   .4    .4    .5    .3    .1    .1    .1    .7    .7    .6    .5    .4    .3    .1    .0    .2    .2    .7    .7    .7
 220.  *   .4    .4    .5    .3    .1    .1    .1    .7    .7    .7    .7    .5    .3    .1    .0    .1    .2    .7    .7    .7
 225.  *   .4    .4    .5    .2    .1    .1    .1    .8    .7    .8    .7    .5    .3    .1    .0    .1    .2    .6    .6    .7
 230.  *   .4    .4    .5    .2    .1    .2    .2    .9    .8    .8    .8    .6    .2    .1    .0    .0    .1    .6    .8    .7
 235.  *   .4    .4    .5    .2    .1    .2    .1    .7    .8    .8    .7    .6    .1    .1    .0    .0    .2    .7    .8    .9
 240.  *   .4    .4    .5    .3    .3    .3    .1    .7    .7    .7    .7    .5    .1    .1    .0    .0    .1    .5    .8    .7
 245.  *   .4    .4    .5    .4    .3    .3    .3    .8    .6    .7    .7    .3    .1    .1    .0    .0    .0    .3    .6    .6
 250.  *   .4    .4    .5    .4    .5    .4    .4    .6    .6    .7    .4    .2    .1    .1    .0    .0    .0    .2    .5    .4
 255.  *   .4    .4    .7    .4    .6    .6    .5    .3    .3    .3    .3    .2    .1    .1    .0    .0    .0    .1    .2    .3
 260.  *   .4    .4    .7    .7    .7    .7    .6    .3    .2    .3    .3    .2    .1    .1    .0    .0    .0    .1    .1    .1
 265.  *   .4    .5    .7    .8    .7    .6    .7    .1    .1    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .1
 270.  *   .4    .5    .9    .7    .6    .6    .7    .0    .0    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .1
 275.  *   .4    .5    .8    .4    .6    .8    .7    .0    .0    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0
 280.  *   .4    .6    .7    .5    .6    .7    .7    .0    .0    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0
 285.  *   .4    .6    .7    .6    .8    .6    .8    .0    .0    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0
 290.  *   .6    .6    .7    .5    .7    .7    .7    .0    .0    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0
 295.  *   .6    .6    .5    .5    .6    .7    .6    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0
 300.  *   .6    .6    .6    .6    .6    .7    .6    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0
 305.  *   .6    .5    .6    .7    .7    .6    .6    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0
 310.  *   .6    .4    .7    .5    .6    .6    .6    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0
 315.  *   .4    .4    .4    .5    .6    .6    .6    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0
 320.  *   .4    .2    .3    .5    .6    .5    .5    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0
 325.  *   .2    .2    .3    .5    .6    .5    .5    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0
 330.  *   .2    .2    .4    .5    .6    .6    .5    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0
 335.  *   .2    .2    .3    .4    .7    .6    .6    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
 340.  *   .2    .2    .3    .5    .7    .6    .6    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 345.  *   .1    .2    .3    .6    .7    .6    .6    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 350.  *   .1    .2    .3    .6    .7    .6    .6    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 355.  *   .1    .2    .4    .6    .6    .6    .5    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .1    .0    .0
 360.  *   .1    .2    .4    .6    .5    .5    .5    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .1    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *   .6    .6    .9    .8    .8    .8    .8    .9    .9    .9    .8    .6    .5    .3    .2    .4    .7    .7    .8    .9
 DEGR. *  290   280   270   265   285    55   285   230    85    85   230   230   175   165   125    90    85   210   240   235

1
                                                                                                                   PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2EXAM.DAT)               RUN: Site 2 Existing AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
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 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .6    .6    .5    .6    .4    .4    .3
   5.  *    .0    .6    .6    .5    .5    .3    .5    .3
  10.  *    .0    .6    .6    .5    .5    .3    .5    .3
  15.  *    .0    .7    .7    .6    .5    .2    .5    .3
  20.  *    .0    .7    .7    .6    .5    .3    .4    .3
  25.  *    .0    .7    .7    .7    .6    .6    .4    .3
  30.  *    .0    .7    .6    .7    .7    .6    .4    .3
  35.  *    .0    .7    .6    .6    .6    .6    .5    .3
  40.  *    .0    .7    .7    .7    .6    .5    .6    .3
  45.  *    .0    .8    .7    .7    .6    .6    .6    .4
  50.  *    .0    .8    .8    .7    .7    .7    .6    .3
  55.  *    .1    .8    .8    .7    .7    .7    .5    .3
  60.  *    .1    .8    .9    .8    .6    .7    .4    .3
  65.  *    .2    .7    .6    .6    .6    .5    .4    .3
  70.  *    .4    .6    .5    .5    .4    .4    .3    .2
  75.  *    .6    .5    .3    .3    .2    .4    .3    .3
  80.  *    .5    .3    .2    .2    .3    .3    .3    .3
  85.  *    .6    .1    .3    .3    .2    .3    .3    .3
  90.  *    .7    .1    .1    .2    .2    .3    .3    .3
  95.  *    .7    .1    .1    .1    .2    .3    .3    .3
 100.  *    .7    .1    .1    .1    .2    .3    .3    .3
 105.  *    .8    .1    .1    .1    .3    .3    .2    .3
 110.  *    .8    .0    .1    .1    .3    .3    .2    .3
 115.  *    .8    .0    .1    .1    .3    .3    .2    .3
 120.  *    .7    .0    .1    .1    .2    .2    .2    .3
 125.  *    .7    .0    .1    .1    .2    .2    .2    .3
 130.  *    .7    .0    .1    .1    .2    .2    .2    .3
 135.  *    .7    .0    .0    .1    .2    .2    .2    .2
 140.  *    .6    .0    .0    .1    .2    .2    .2    .1
 145.  *    .7    .0    .0    .0    .1    .1    .1    .1
 150.  *    .7    .0    .0    .0    .1    .1    .1    .1
 155.  *    .7    .0    .0    .0    .0    .0    .0    .0
 160.  *    .7    .0    .0    .0    .0    .0    .0    .0
 165.  *    .6    .0    .0    .0    .0    .0    .0    .0
 170.  *    .7    .0    .0    .0    .0    .0    .0    .0
 175.  *    .7    .0    .0    .0    .0    .0    .0    .0
 180.  *    .6    .0    .0    .0    .0    .0    .0    .0
 185.  *    .6    .0    .0    .0    .0    .0    .0    .0
 190.  *    .6    .0    .0    .0    .0    .0    .0    .0
 195.  *    .7    .0    .0    .0    .0    .0    .0    .0
 200.  *    .7    .0    .0    .0    .0    .0    .0    .0
 205.  *    .7    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                           PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2EXAM.DAT)              RUN: Site 2 Existing AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .8    .0    .0    .0    .0    .0    .0    .0
 215.  *    .9    .0    .0    .0    .0    .0    .0    .0
 220.  *    .7    .0    .0    .0    .0    .0    .0    .0
 225.  *    .8    .0    .0    .0    .0    .0    .0    .0
 230.  *    .8    .0    .0    .0    .0    .0    .0    .0
 235.  *    .8    .2    .1    .1    .0    .0    .0    .0
 240.  *    .7    .3    .2    .2    .1    .0    .0    .0
 245.  *    .4    .4    .4    .3    .2    .0    .0    .0
 250.  *    .3    .5    .4    .5    .3    .0    .0    .0
 255.  *    .2    .6    .6    .5    .4    .2    .0    .0
 260.  *    .2    .8    .9   1.0    .6    .2    .0    .0
 265.  *    .0    .9   1.0    .8    .7    .2    .0    .0
 270.  *    .0    .9    .9    .9    .7    .2    .1    .0
 275.  *    .0    .8    .8    .7    .7    .4    .1    .0
 280.  *    .0    .8    .7    .7    .7    .4    .1    .0
 285.  *    .0    .8    .7    .7    .7    .4    .2    .0
 290.  *    .0    .8    .7    .7    .7    .4    .2    .0
 295.  *    .0    .7    .7    .7    .6    .4    .2    .1
 300.  *    .0    .7    .7    .7    .6    .3    .2    .1
 305.  *    .0    .7    .7    .7    .6    .3    .2    .1
 310.  *    .0    .8    .6    .6    .5    .3    .2    .1
 315.  *    .0    .8    .6    .6    .5    .3    .2    .1
 320.  *    .0    .7    .6    .6    .4    .3    .2    .1
 325.  *    .0    .7    .6    .6    .4    .3    .2    .2
 330.  *    .0    .7    .6    .6    .4    .3    .1    .1
 335.  *    .0    .7    .6    .6    .4    .3    .1    .1
 340.  *    .0    .7    .7    .6    .4    .4    .1    .2
 345.  *    .0    .6    .6    .6    .4    .2    .2    .3
 350.  *    .0    .6    .6    .6    .5    .2    .3    .3
 355.  *    .0    .6    .6    .5    .5    .4    .3    .3
 360.  *    .0    .6    .6    .5    .6    .4    .4    .3
 ------*------------------------------------------------
 MAX   *    .9    .9   1.0   1.0    .7    .7    .6    .4
 DEGR. *   215   265   265   260    30    50    40    45

 THE HIGHEST CONCENTRATION IS    1.00 PPM AT  265 DEGREES FROM REC23.
 THE 2ND HIGHEST CONCENTRATION IS    1.00 PPM AT  260 DEGREES FROM REC24.
 THE 3RD HIGHEST CONCENTRATION IS     .90 PPM AT  270 DEGREES FROM REC3 .
```

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1                        CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2EXPM.DAT)              RUN: Site 2 Existing PM
      DATE: 03/21/2010   TIME: 22:19:57.08


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)           *    LENGTH  BRG TYPE   VPH     EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2      *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*-----------------------------------------*---------------------------------------------------------
       1. EB        Wil AP    *    -172.0     469.0      78.0     601.0 *     283.   62. AG   2564.   3.3    .0 68.0
       2. EB        Wil AP    *      78.0     601.0     276.0     684.0 *     215.   67. AG   2564.   3.3    .0 68.0
       3. EB        Wil T+R   *     276.0     684.0     778.0     856.0 *     531.   71. AG   2293.   3.3    .0 68.0
       4. EB        Wil T+R Q *     678.0     822.0     380.6     719.4 *     315.  251. AG     88. 100.0    .0 48.0 1.00  16.0
       5. EB        Wil LT    *     259.0     724.0     761.0     889.0 *     528.   72. AG    271.   3.3    .0 44.0
       6. EB        Wil LT Q  *     659.0     855.0     534.7     814.3 *     131.  252. AG     92. 100.0    .0 24.0  .94   6.6
       7. EB        Wil DP    *     782.0     851.0    1703.0    1145.0 *     967.   72. AG   2453.   3.3    .0 68.0
       8. WB        Wil AP    *    1025.0    1019.0    1677.0    1228.0 *     685.   72. AG   2853.   3.3    .0 68.0
       9. WB        Wil T+R   *    1025.0    1019.0     717.0     920.0 *     324.  252. AG   2778.   3.3    .0 68.0
      10. WB        Wil T+R Q *     798.0     946.0    3381.7    1772.8 *    2713.   72. AG    113. 100.0    .0 48.0 1.50 137.8
      11. WB        Wil LT    *    1040.0     975.0     742.0     883.0 *     312.  253. AG     75.   3.3    .0 44.0
      12. WB        Wil LT Q  *     824.0     908.0    1040.1     974.1 *     226.   73. AG    105. 100.0    .0 24.0 1.76  11.5
      13. WB        Wil DP    *     715.0     922.0     201.0     748.0 *     543.  251. AG   3732.   3.3    .0 68.0
      14. WB        Wil DP    *     201.0     748.0    -199.0     546.0 *     448.  243. AG   3732.   3.3    .0 68.0
      15. NB        Vet AP    *     967.0     583.0    1327.0      75.0 *     623.  145. AG   1155.   3.5    .0 32.0
      16. NB        Vet T+LT  *     960.0     579.0     781.0     840.0 *     316.  326. AG    957.   3.5    .0 56.0
      17. NB        Vet T+LT Q*     820.0     783.0    1518.2    -236.3 *    1235.  146. AG    118. 100.0    .0 36.0 1.43  62.8
      18. NB        Vet RT    *     964.0     622.0     813.0     839.0 *     264.  325. AG    198.   3.5    .0 32.0
      19. NB        Vet RT Q  *     847.0     791.0     911.0     698.1 *     113.  145. AG     37. 100.0    .0 12.0  .73   5.7
      20. NB        Vet DP    *     798.0     836.0     611.0    1170.0 *     383.  331. AG    984.   3.5    .0 44.0
      21. NB        Vet DP    *     611.0    1170.0     214.0    1729.0 *     686.  325. AG    984.   3.5    .0 44.0
      22. SB        Vet AP    *     544.0    1188.0     172.0    1701.0 *     634.  324. AG   1132.   3.5    .0 44.0
      23. SB        Vet T+LT  *     550.0    1188.0     730.0     898.0 *     341.  148. AG    422.   3.5    .0 56.0
      24. SB        Vet T+LT Q*     679.0     981.0     621.2    1074.1 *     110.  328. AG    128. 100.0    .0 36.0  .86   5.6
      25. SB        Vet RT    *     521.0    1169.0     695.0     888.0 *     331.  148. AG    710.   3.5    .0 44.0
      26. SB        Vet RT Q  *     643.0     972.0     103.3    1842.1 *    1024.  328. AG     69. 100.0    .0 24.0 1.27  52.0
      27. SB        Vet DP    *     703.0     889.0    1292.0      46.0 *    1028.  145. AG    535.   3.5    .0 44.0
1
                                                                                                                 PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2EXPM.DAT)              RUN: Site 2 Existing PM
      DATE: 03/21/2010   TIME: 22:19:57.08

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL    ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *     150        60       2.0      2293        999      20.50      1        3
       6. EB        Wil LT Q  *     150       126       2.0       271       1084      20.50      1        3
      10. WB        Wil T+R Q *     150        77       2.0      2778       1010      20.50      1        3
      12. WB        Wil LT Q  *     150       143       2.0        75       1084      20.50      1        3
      17. NB        Vet T+LT Q*     150       107       2.0       957        860      20.50      1        3
      19. NB        Vet RT Q  *     150       102       2.0       198        927      20.50      1        3
      24. SB        Vet T+LT Q*     150       116       2.0       422        817      20.50      1        3
      26. SB        Vet RT Q  *     150        94       2.0       710        808      20.50      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       1066.0      492.0        5.0  *
      2. SE 164 S             *        942.0      686.0        5.0  *
      3. SE 82 S              *        892.0      756.0        5.0  *
      4. SE CNR               *        869.0      821.0        5.0  *
      5. SE 82 E              *        925.0      853.0        5.0  *
      6. SE 164 E             *       1005.0      880.0        5.0  *
      7. SE MID E             *       1219.0      947.0        5.0  *
      8. NE MID E             *       1144.0     1099.0        5.0  *
      9. NE 164 E             *        918.0     1026.0        5.0  *
     10. NE 82 E              *        838.0     1000.0        5.0  *
     11. NE CNR               *        759.0      983.0        5.0  *
     12. NE 82 N              *        716.0     1047.0        5.0  *
     13. NE 164 N             *        676.0     1120.0        5.0  *
     14. NE MID N             *        595.0     1269.0        5.0  *
     15. NW MID N             *        464.0     1209.0        5.0  *
     16. NW 164 N             *        546.0     1079.0        5.0  *
     17. NW 82 N              *        589.0     1010.0        5.0  *
     18. NW CNR               *        611.0      945.0        5.0  *
     19. NW 82 W              *        552.0      910.0        5.0  *
     20. NW 164 W             *        475.0      884.0        5.0  *
     21. NW MID W             *        273.0      815.0        5.0  *
     22. SW MID W             *        305.0      649.0        5.0  *
     23. SW 164 W             *        565.0      737.0        5.0  *
     24. SW 82 W              *        645.0      764.0        5.0  *
     25. SW CNR               *        718.0      779.0        5.0  *
     26. SW 82 S              *        774.0      718.0        5.0  *
     27. SW 164 S             *        824.0      646.0        5.0  *
     28. SW MID S             *        957.0      459.0        5.0  *
1
                                                                                                                 PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2EXPM.DAT)              RUN: Site 2 Existing PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

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              concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
  0.  *    .1    .4    .4    .5    .5    .5    .4    .0    .0    .0    .0    .0    .0    .0    .4    .4    .3    .4    .1    .1
  5.  *    .1    .4    .4    .5    .5    .6    .4    .0    .0    .0    .0    .0    .0    .0    .4    .4    .3    .4    .1    .1
 10.  *    .1    .3    .4    .5    .5    .6    .4    .0    .0    .0    .0    .0    .0    .0    .4    .3    .4    .4    .1    .1
 15.  *    .1    .2    .4    .5    .5    .5    .4    .0    .0    .0    .0    .0    .0    .0    .4    .3    .4    .4    .1    .1
 20.  *    .1    .2    .4    .5    .5    .5    .4    .0    .0    .0    .0    .0    .0    .0    .4    .3    .4    .4    .2    .1
 25.  *    .1    .3    .4    .5    .6    .7    .5    .0    .0    .0    .0    .0    .0    .0    .3    .3    .4    .4    .2    .1
 30.  *    .1    .3    .4    .5    .8    .6    .6    .0    .0    .0    .0    .0    .0    .0    .3    .3    .4    .4    .2    .1
 35.  *    .1    .3    .3    .6    .8    .6    .6    .0    .0    .0    .0    .0    .0    .0    .3    .3    .5    .4    .2    .1
 40.  *    .1    .3    .3    .7    .7    .6    .6    .0    .0    .0    .0    .0    .0    .0    .3    .3    .5    .4    .2    .1
 45.  *    .1    .3    .3    .7    .7    .6    .6    .0    .0    .0    .0    .0    .0    .0    .3    .3    .5    .4    .2    .1
 50.  *    .1    .3    .3    .7    .7    .6    .6    .1    .0    .0    .0    .0    .0    .0    .3    .3    .5    .4    .1    .2
 55.  *    .1    .2    .3    .7    .6    .6    .6    .2    .1    .2    .1    .0    .0    .0    .3    .3    .5    .3    .2    .2
 60.  *    .0    .2    .3    .6    .6    .6    .6    .2    .3    .3    .2    .0    .0    .0    .3    .3    .5    .3    .3    .3
 65.  *    .0    .1    .2    .4    .6    .6    .6    .4    .4    .4    .4    .1    .0    .0    .3    .3    .6    .4    .4    .4
 70.  *    .0    .0    .2    .4    .5    .5    .3    .6    .6    .6    .5    .1    .1    .0    .3    .4    .6    .6    .6    .4
 75.  *    .0    .0    .0    .2    .3    .3    .3    .7    .8    .8    .7    .2    .1    .0    .3    .4    .7    .6    .8    .8
 80.  *    .0    .0    .0    .1    .3    .3    .1    .9    .9    .9    .8    .3    .1    .1    .4    .4    .8    .7    .8    .7
 85.  *    .0    .0    .0    .1    .1    .1    .1    .9    .9   1.0   1.0    .4    .2    .1    .4    .6   1.0    .9    .7    .7
 90.  *    .0    .0    .0    .0    .1    .1    .1    .9    .9   1.0   1.0    .5    .2    .1    .4    .6   1.0    .8    .7    .7
 95.  *    .0    .0    .0    .0    .0    .0    .0    .9    .8   1.0    .8    .5    .3    .1    .4    .7    .9    .7    .7    .7
100.  *    .0    .0    .0    .0    .0    .0    .0    .9    .9    .9    .8    .5    .3    .2    .4    .7   1.0    .7    .7    .6
105.  *    .0    .0    .0    .0    .0    .0    .0    .8    .9    .9    .8    .5    .3    .2    .4    .9   1.0    .5    .6    .7
110.  *    .0    .0    .0    .0    .0    .0    .0    .8   1.0    .9    .8    .5    .3    .1    .3    .9    .8    .6    .5    .8
115.  *    .0    .0    .0    .0    .0    .0    .0    .7    .8    .8    .7    .5    .3    .1    .3    .9    .7    .6    .7    .8
120.  *    .0    .0    .0    .0    .0    .0    .0    .7    .8    .8    .7    .4    .4    .1    .3    .7    .7    .6    .7    .8
125.  *    .0    .0    .0    .0    .0    .0    .0    .7    .8    .8    .7    .4    .4    .1    .2    .6    .5    .5    .8    .8
130.  *    .1    .1    .1    .0    .0    .0    .0    .7    .8    .8    .6    .4    .4    .1    .4    .7    .4    .5    .7    .7
135.  *    .2    .1    .1    .1    .0    .0    .0    .7    .8    .8    .6    .5    .3    .2    .5    .6    .4    .5    .7    .7
140.  *    .3    .3    .2    .1    .0    .0    .0    .7    .7    .7    .6    .4    .4    .1    .5    .5    .5    .5    .7    .7
145.  *    .4    .3    .2    .2    .1    .0    .0    .7    .7    .8    .5    .4    .3    .1    .5    .4    .5    .5    .7    .5
150.  *    .4    .4    .4    .2    .1    .0    .0    .7    .9    .9    .6    .4    .3    .2    .3    .5    .5    .5    .6    .5
155.  *    .5    .4    .5    .3    .1    .1    .0    .7    .9    .9    .5    .4    .3    .2    .2    .5    .4    .7    .6    .5
160.  *    .6    .4    .6    .4    .2    .1    .0    .7    .9    .9    .6    .3    .3    .3    .2    .2    .3    .6    .7    .6
165.  *    .6    .5    .6    .5    .2    .1    .0    .7    .9    .9    .5    .3    .4    .2    .1    .2    .5    .6    .7    .6
170.  *    .6    .4    .5    .5    .2    .1    .0    .7    .9    .9    .5    .4    .3    .4    .1    .3    .5    .6    .6    .5
175.  *    .5    .4    .5    .5    .2    .1    .1    .8    .9    .9    .5    .4    .3    .4    .1    .3    .5    .6    .6    .5
180.  *    .5    .4    .5    .5    .2    .1    .1    .7    .8    .8    .4    .4    .4    .3    .1    .3    .5    .6    .6    .5
185.  *    .4    .4    .5    .4    .1    .1    .1    .8    .8    .8    .4    .3    .5    .3    .1    .3    .5    .6    .6    .5
190.  *    .4    .4    .5    .4    .1    .1    .1    .8    .9    .8    .4    .3    .5    .3    .1    .3    .4    .6    .6    .5
195.  *    .4    .4    .5    .4    .1    .1    .1    .8    .9    .7    .5    .4    .6    .3    .1    .2    .4    .6    .6    .6
200.  *    .4    .4    .5    .4    .1    .1    .1    .8    .9    .7    .5    .6    .7    .3    .1    .2    .4    .6    .6    .6
205.  *    .4    .4    .5    .3    .1    .1    .1    .8    .8    .7    .6    .6    .7    .3    .1    .1    .4    .6    .6    .6
1
                                                                                                                   PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2EXPM.DAT)               RUN: Site 2 Existing PM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
210.  *    .4    .4    .5    .3    .1    .1    .1    .8    .8    .6    .6    .6    .6    .3    .0    .1    .4    .6    .6    .6
215.  *    .4    .4    .5    .3    .1    .1    .1    .9    .8    .6    .7    .6    .5    .3    .1    .1    .3    .6    .6    .5
220.  *    .4    .4    .5    .3    .1    .1    .1    .9    .9    .8    .7    .7    .4    .2    .1    .1    .3    .6    .6    .5
225.  *    .4    .4    .5    .2    .1    .1    .1   1.0    .8    .8    .7    .7    .4    .2    .0    .2    .2    .6    .7    .5
230.  *    .4    .4    .5    .2    .1    .1    .1   1.0    .8    .7    .8    .5    .4    .3    .0    .2    .3    .6    .6    .7
235.  *    .4    .4    .5    .2    .1    .1    .1   1.0    .9    .8    .7    .6    .4    .3    .0    .1    .2    .6    .7    .6
240.  *    .4    .4    .5    .2    .1    .2    .1    .9    .8    .7    .7    .5    .3    .3    .0    .0    .2    .4    .6    .5
245.  *    .4    .4    .5    .2    .2    .2    .1    .8    .7    .6    .5    .5    .2    .3    .0    .0    .2    .4    .5    .5
250.  *    .4    .4    .5    .3    .3    .2    .2    .6    .4    .4    .4    .5    .2    .3    .0    .0    .0    .3    .4    .4
255.  *    .4    .4    .5    .4    .4    .4    .3    .5    .4    .3    .3    .4    .2    .3    .0    .0    .0    .1    .4    .3
260.  *    .4    .4    .6    .5    .5    .4    .6    .3    .2    .3    .3    .4    .2    .3    .0    .0    .0    .1    .2    .2
265.  *    .4    .4    .8    .6    .5    .5    .7    .2    .2    .3    .3    .4    .2    .3    .0    .0    .0    .0    .1    .1
270.  *    .4    .4    .8    .6    .5    .6    .7    .0    .2    .1    .2    .4    .2    .3    .0    .0    .0    .0    .1    .1
275.  *    .4    .6    .7    .6    .4    .6    .6    .0    .0    .1    .3    .4    .2    .3    .0    .0    .0    .0    .0    .0
280.  *    .4    .7    .7    .4    .4    .7    .6    .0    .0    .2    .4    .4    .2    .3    .0    .0    .0    .0    .0    .0
285.  *    .4    .7    .7    .3    .5    .7    .6    .0    .0    .2    .4    .3    .2    .3    .0    .0    .0    .0    .0    .0
290.  *    .4    .8    .6    .4    .5    .6    .6    .0    .0    .2    .4    .3    .2    .3    .0    .0    .0    .0    .0    .0
295.  *    .6    .7    .5    .5    .6    .6    .5    .0    .0    .2    .4    .3    .2    .3    .0    .0    .0    .0    .0    .0
300.  *    .6    .6    .5    .6    .5    .6    .5    .0    .0    .1    .4    .3    .2    .3    .0    .0    .0    .0    .0    .0
305.  *    .6    .6    .5    .5    .6    .5    .4    .0    .0    .1    .3    .2    .4    .3    .0    .0    .0    .0    .0    .0
310.  *    .4    .5    .6    .6    .6    .5    .4    .0    .0    .1    .3    .2    .4    .3    .0    .0    .0    .0    .0    .0
315.  *    .4    .3    .6    .5    .6    .5    .4    .0    .0    .1    .3    .2    .4    .2    .1    .1    .1    .0    .0    .0
320.  *    .4    .3    .4    .5    .5    .5    .4    .0    .0    .0    .2    .3    .4    .2    .1    .1    .1    .1    .0    .0
325.  *    .3    .4    .4    .5    .5    .5    .4    .0    .0    .0    .2    .3    .2    .1    .2    .3    .3    .1    .0    .0
330.  *    .1    .2    .2    .5    .5    .5    .4    .0    .0    .0    .1    .1    .1    .0    .3    .4    .4    .1    .0    .0
335.  *    .1    .2    .3    .5    .5    .5    .4    .0    .0    .0    .0    .0    .0    .0    .3    .4    .4    .2    .1    .0
340.  *    .1    .3    .4    .5    .5    .5    .4    .0    .0    .0    .0    .0    .0    .0    .3    .5    .5    .3    .1    .0
345.  *    .0    .4    .4    .5    .5    .5    .4    .0    .0    .0    .0    .0    .0    .0    .4    .6    .4    .3    .1    .1
350.  *    .0    .4    .4    .5    .5    .5    .4    .0    .0    .0    .0    .0    .0    .0    .4    .6    .4    .3    .1    .1
355.  *    .1    .4    .4    .5    .5    .5    .4    .0    .0    .0    .0    .0    .0    .0    .4    .5    .3    .4    .1    .1
360.  *    .1    .4    .4    .5    .5    .5    .4    .0    .0    .0    .0    .0    .0    .0    .4    .4    .3    .4    .1    .1
------*------------------------------------------------------------------------------------------------------------------------
MAX   *    .6    .8    .8    .7    .8    .7    .7   1.0   1.0   1.0   1.0    .7    .7    .4    .5    .9   1.0    .9    .8    .8
DEGR. *   160   290   265    40    30    25   265   225   110    85    85   220   200   170   135   105    85    85   125   110

1
                                                                                                                   PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2EXPM.DAT)               RUN: Site 2 Existing PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .4    .8    .8    .5    .3    .5    .3
   5.  *    .0    .4    .7    .8    .5    .3    .6    .4
  10.  *    .0    .4    .7    .6    .4    .4    .7    .4
  15.  *    .0    .4    .7    .5    .4    .5    .8    .4
  20.  *    .0    .4    .7    .5    .4    .6    .8    .5
  25.  *    .0    .4    .7    .6    .4    .6    .6    .5
  30.  *    .0    .4    .6    .5    .5    .6    .5    .4
  35.  *    .0    .6    .6    .5    .5    .6    .6    .4
  40.  *    .0    .6    .8    .5    .5    .6    .6    .4
  45.  *    .0    .6    .9    .6    .5    .6    .6    .4
  50.  *    .1    .6    .8    .7    .8    .6    .6    .4
  55.  *    .1    .7    .7    .8    .8    .6    .5    .4
  60.  *    .2    .7    .7    .8    .7    .6    .5    .3
  65.  *    .3    .7    .7    .7    .6    .5    .4    .3
  70.  *    .4    .5    .4    .3    .5    .5    .3    .3
  75.  *    .6    .4    .3    .3    .3    .3    .3    .3
  80.  *    .8    .2    .3    .2    .3    .3    .3    .3
  85.  *    .9    .1    .1    .2    .3    .3    .3    .4
  90.  *    .7    .0    .1    .1    .2    .4    .4    .4
  95.  *    .7    .1    .1    .1    .2    .4    .4    .4
 100.  *    .7    .1    .1    .1    .2    .4    .4    .4
 105.  *    .7    .1    .1    .1    .3    .4    .4    .4
 110.  *    .7    .1    .1    .1    .3    .4    .3    .4
 115.  *    .7    .1    .1    .1    .4    .4    .3    .4
 120.  *    .7    .0    .1    .1    .4    .4    .3    .4
 125.  *    .7    .0    .1    .1    .3    .3    .4    .4
 130.  *    .6    .0    .1    .1    .3    .3    .4    .4
 135.  *    .4    .0    .1    .1    .2    .3    .4    .3
 140.  *    .4    .0    .0    .1    .2    .3    .3    .3
 145.  *    .4    .0    .0    .1    .1    .1    .1    .1
 150.  *    .4    .0    .0    .0    .1    .1    .1    .1
 155.  *    .5    .0    .0    .0    .0    .1    .1    .1
 160.  *    .5    .0    .0    .0    .0    .0    .0    .0
 165.  *    .5    .0    .0    .0    .0    .0    .0    .0
 170.  *    .4    .0    .0    .0    .0    .0    .0    .0
 175.  *    .4    .0    .0    .0    .0    .0    .0    .0
 180.  *    .4    .0    .0    .0    .0    .0    .0    .0
 185.  *    .4    .0    .0    .0    .0    .0    .0    .0
 190.  *    .4    .0    .0    .0    .0    .0    .0    .0
 195.  *    .4    .0    .0    .0    .0    .0    .0    .0
 200.  *    .5    .0    .0    .0    .0    .0    .0    .0
 205.  *    .6    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                         PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2EXPM.DAT)              RUN: Site 2 Existing PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .6    .0    .0    .0    .0    .0    .0    .0
 215.  *    .5    .0    .0    .0    .0    .0    .0    .0
 220.  *    .6    .0    .0    .0    .0    .0    .0    .0
 225.  *    .7    .0    .0    .0    .0    .0    .0    .0
 230.  *    .7    .0    .0    .0    .0    .0    .0    .0
 235.  *    .7    .1    .0    .0    .0    .0    .0    .0
 240.  *    .5    .1    .1    .1    .0    .0    .0    .0
 245.  *    .4    .2    .1    .2    .2    .0    .0    .0
 250.  *    .4    .4    .3    .3    .2    .0    .0    .0
 255.  *    .2    .4    .4    .4    .4    .0    .0    .0
 260.  *    .2    .4    .4    .6    .6    .0    .0    .0
 265.  *    .2    .4    .7    .7    .6    .2    .0    .0
 270.  *    .0    .5    .7    .7    .5    .3    .0    .0
 275.  *    .0    .4    .7    .8    .7    .3    .0    .0
 280.  *    .0    .4    .6    .8    .7    .3    .2    .0
 285.  *    .0    .4    .8    .8    .7    .3    .3    .0
 290.  *    .0    .4    .6    .8    .7    .3    .3    .0
 295.  *    .0    .4    .6    .7    .7    .3    .3    .0
 300.  *    .0    .4    .6    .7    .7    .4    .3    .1
 305.  *    .0    .5    .6    .7    .6    .4    .3    .1
 310.  *    .0    .5    .6    .7    .6    .4    .3    .1
 315.  *    .0    .4    .6    .7    .6    .3    .2    .1
 320.  *    .0    .4    .6    .7    .7    .2    .2    .1
 325.  *    .0    .3    .6    .7    .6    .3    .3    .1
 330.  *    .0    .4    .6    .8    .5    .3    .3    .1
 335.  *    .0    .5    .6    .8    .4    .3    .2    .2
 340.  *    .0    .4    .7    .8    .5    .3    .1    .4
 345.  *    .0    .4    .8    .8    .5    .3    .2    .4
 350.  *    .0    .4    .8    .8    .4    .4    .3    .3
 355.  *    .0    .4    .8    .9    .3    .4    .4    .3
 360.  *    .0    .4    .8    .8    .5    .3    .5    .3
 ------*------------------------------------------------
 MAX   *    .9    .7    .9    .9    .8    .6    .8    .5
 DEGR. *   85    55    45   355    50    20    15    20

 THE HIGHEST CONCENTRATION IS    1.00 PPM AT  225 DEGREES FROM REC8 .
 THE 2ND HIGHEST CONCENTRATION IS    1.00 PPM AT  110 DEGREES FROM REC9 .
 THE 3RD HIGHEST CONCENTRATION IS    1.00 PPM AT   85 DEGREES FROM REC10.
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2NBAM.DAT)               RUN: Site 2 NO BUILD AM
      DATE: 03/19/2010   TIME: 09:06:00.03


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)           *   LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2      *    (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*-----------------------------------------*---------------------------------------------------------
       1. EB        Wil AP    *    -172.0     469.0      78.0     601.0 *     283.   62. AG    5619.    .8    .0 68.0
       2. EB        Wil AP    *      78.0     601.0     276.0     684.0 *     215.   67. AG    5619.    .8    .0 68.0
       3. EB        Wil T+R   *     276.0     684.0     778.0     856.0 *     531.   71. AG    4678.    .8    .0 68.0
       4. EB        Wil T+R Q *     678.0     822.0   -5342.0   -1254.4 *    6368.  251. AG      17. 100.0    .0 48.0 2.01 323.5
       5. EB        Wil LT    *     259.0     724.0     761.0     889.0 *     528.   72. AG     941.    .8    .0 44.0
       6. EB        Wil LT Q  *     659.0     855.0   -2454.5    -165.7 *    3277.  252. AG      17. 100.0    .0 24.0 2.54 166.4
       7. EB        Wil DP    *     782.0     851.0    1703.0    1145.0 *     967.   72. AG    4869.    .8    .0 68.0
       8. WB        Wil AP    *    1025.0    1019.0    1677.0    1228.0 *     685.   72. AG    3164.    .8    .0 68.0
       9. WB        Wil T+R   *    1025.0    1019.0     717.0     920.0 *     324.  252. AG    3147.    .8    .0 68.0
      10. WB        Wil T+R Q *     798.0     946.0    8794.2    3504.8 *    8396.   72. AG      24. 100.0    .0 48.0 **** 426.5
      11. WB        Wil LT    *    1040.0     975.0     742.0     883.0 *     312.  253. AG      17.    .8    .0 44.0
      12. WB        Wil LT Q  *     824.0     908.0     933.5     941.5 *     114.   73. AG      21. 100.0    .0 24.0 8.00   5.8
      13. WB        Wil DP    *     715.0     922.0     201.0     748.0 *     543.  251. AG    3437.    .8    .0 68.0
      14. WB        Wil DP    *     201.0     748.0    -199.0     546.0 *     448.  243. AG    3437.    .8    .0 68.0
      15. NB        Vet AP    *     967.0     583.0    1327.0      75.0 *     623.  145. AG     946.    .9    .0 32.0
      16. NB        Vet T+LT  *     960.0     579.0     781.0     840.0 *     316.  326. AG     814.    .9    .0 56.0
      17. NB        Vet T+LT Q*     820.0     783.0    1337.8      27.1 *     916.  146. AG      24. 100.0    .0 36.0 1.33  46.5
      18. NB        Vet RT    *     964.0     622.0     813.0     839.0 *     264.  325. AG     132.    .9    .0 32.0
      19. NB        Vet RT Q  *     847.0     791.0     890.4     728.0 *      77.  145. AG       8. 100.0    .0 12.0  .52   3.9
      20. NB        Vet DP    *     798.0     836.0     611.0    1170.0 *     383.  331. AG    1787.    .9    .0 44.0
      21. NB        Vet DP    *     611.0    1170.0     214.0    1729.0 *     686.  325. AG    1787.    .9    .0 44.0
      22. SB        Vet AP    *     544.0    1188.0     172.0    1701.0 *     634.  324. AG    1155.    .9    .0 44.0
      23. SB        Vet T+LT  *     550.0    1188.0     730.0     898.0 *     341.  148. AG     833.    .9    .0 56.0
      24. SB        Vet T+LT Q*     679.0     981.0    -150.8    2316.8 *    1573.  328. AG      26. 100.0    .0 36.0 1.88  79.9
      25. SB        Vet RT    *     521.0    1169.0     695.0     888.0 *     331.  148. AG     322.    .9    .0 44.0
      26. SB        Vet RT Q  *     643.0     972.0     601.2    1039.3 *      79.  328. AG      13. 100.0    .0 24.0  .52   4.0
      27. SB        Vet DP    *     703.0     889.0    1292.0      46.0 *    1028.  145. AG     791.    .9    .0 44.0
1
                                                                                                                 PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2NBAM.DAT)               RUN: Site 2 NO BUILD AM
      DATE: 03/19/2010   TIME: 09:06:00.03

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *      150       57       2.0      4678        983       4.10     1        3
       6. EB        Wil LT Q  *      150      118       2.0       941        995       4.10     1        3
      10. WB        Wil T+R Q *      150       82       2.0      3147         84       4.10     1        3
      12. WB        Wil LT Q  *      150      143       2.0        17         84       4.10     1        3
      17. NB        Vet T+LT Q*      150      111       2.0       814        875       4.10     1        3
      19. NB        Vet RT Q  *      150      106       2.0       132        955       4.10     1        3
      24. SB        Vet T+LT Q*      150      120       2.0       833        852       4.10     1        3
      26. SB        Vet RT Q  *      150       90       2.0       322        834       4.10     1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       1066.0      492.0        5.0   *
      2. SE 164 S             *        942.0      686.0        5.0   *
      3. SE 82 S              *        892.0      756.0        5.0   *
      4. SE CNR               *        869.0      821.0        5.0   *
      5. SE 82 E              *        925.0      853.0        5.0   *
      6. SE 164 E             *       1005.0      880.0        5.0   *
      7. SE MID E             *       1219.0      947.0        5.0   *
      8. NE MID E             *       1144.0     1099.0        5.0   *
      9. NE 164 E             *        918.0     1026.0        5.0   *
     10. NE 82 E              *        838.0     1000.0        5.0   *
     11. NE CNR               *        759.0      983.0        5.0   *
     12. NE 82 N              *        716.0     1047.0        5.0   *
     13. NE 164 N             *        676.0     1120.0        5.0   *
     14. NE MID N             *        595.0     1269.0        5.0   *
     15. NW MID N             *        464.0     1209.0        5.0   *
     16. NW 164 N             *        546.0     1079.0        5.0   *
     17. NW 82 N              *        589.0     1010.0        5.0   *
     18. NW CNR               *        611.0      945.0        5.0   *
     19. NW 82 W              *        552.0      910.0        5.0   *
     20. NW 164 W             *        475.0      884.0        5.0   *
     21. NW MID W             *        273.0      815.0        5.0   *
     22. SW MID W             *        305.0      649.0        5.0   *
     23. SW 164 W             *        565.0      737.0        5.0   *
     24. SW 82 W              *        645.0      764.0        5.0   *
     25. SW CNR               *        718.0      779.0        5.0   *
     26. SW 82 S              *        774.0      718.0        5.0   *
     27. SW 164 S             *        824.0      646.0        5.0   *
     28. SW MID S             *        957.0      459.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2NBAM.DAT)               RUN: Site 2 NO BUILD AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

```
               concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   5.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  10.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  15.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  20.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
  25.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .2    .2    .1    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1
  75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  80.  *    .0    .0    .0    .0    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  85.  *    .0    .0    .0    .0    .0    .1    .0    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .4    .3    .3    .0    .0    .0    .0    .0    .0    .1    .2    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .0    .0    .0    .1    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .1    .0    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
 120.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
 125.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
 130.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .2
 135.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .2    .2
 140.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 145.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 150.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 155.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 160.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 165.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 170.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 175.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 180.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 185.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 190.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 195.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 200.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 205.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .2    .2    .2
1
                                                                                                                         PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2NBAM.DAT)               RUN: Site 2 NO BUILD AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1
 215.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .1
 220.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 225.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 230.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 235.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 240.  *    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .1    .1    .1    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .1    .1    .1    .0    .0    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 255.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 260.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .1    .1    .1    .1    .2    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0    .0    .0    .0
 295.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0
 300.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0
 305.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .2    .0    .0    .0    .0    .0    .0
 310.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
 315.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0
 320.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 340.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 345.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 350.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 355.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 360.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .2    .2    .2    .2    .3    .4    .3    .3    .2    .1    .2    .1    .1    .1    .2    .2    .2
 DEGR. *   150   150     0   280    50    50    50    95    90    85    90   285   160   305     0     0     0   205    90   115

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                                                                                                                         PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2NBAM.DAT)               RUN: Site 2 NO BUILD AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .1    .1    .1    .1    .0    .0    .0
  5.  *    .0    .1    .1    .1    .1    .0    .0    .0
 10.  *    .0    .1    .1    .1    .1    .0    .0    .0
 15.  *    .0    .1    .1    .1    .1    .0    .0    .0
 20.  *    .0    .1    .1    .1    .1    .0    .0    .0
 25.  *    .0    .1    .1    .1    .1    .1    .0    .0
 30.  *    .0    .1    .1    .1    .1    .1    .0    .0
 35.  *    .0    .2    .1    .1    .1    .1    .0    .0
 40.  *    .0    .2    .1    .1    .2    .1    .0    .0
 45.  *    .0    .2    .1    .1    .2    .1    .0    .0
 50.  *    .0    .2    .1    .1    .1    .1    .0    .0
 55.  *    .0    .2    .1    .2    .1    .1    .0    .0
 60.  *    .0    .1    .1    .2    .1    .1    .0    .0
 65.  *    .1    .1    .2    .2    .1    .0    .0    .0
 70.  *    .1    .1    .2    .2    .1    .0    .0    .0
 75.  *    .1    .1    .1    .1    .1    .0    .0    .0
 80.  *    .1    .1    .0    .0    .0    .0    .0    .0
 85.  *    .1    .0    .0    .0    .0    .0    .0    .0
 90.  *    .1    .0    .0    .0    .0    .0    .0    .0
 95.  *    .2    .0    .0    .0    .0    .0    .0    .0
100.  *    .2    .0    .0    .0    .0    .0    .0    .0
105.  *    .2    .0    .0    .0    .0    .0    .0    .0
110.  *    .2    .0    .0    .0    .0    .0    .0    .0
115.  *    .2    .0    .0    .0    .0    .0    .0    .0
120.  *    .2    .0    .0    .0    .0    .0    .0    .0
125.  *    .2    .0    .0    .0    .0    .0    .0    .0
130.  *    .2    .0    .0    .0    .0    .0    .0    .0
135.  *    .2    .0    .0    .0    .0    .0    .0    .0
140.  *    .2    .0    .0    .0    .0    .0    .0    .0
145.  *    .2    .0    .0    .0    .0    .0    .0    .0
150.  *    .2    .0    .0    .0    .0    .0    .0    .0
155.  *    .1    .0    .0    .0    .0    .0    .0    .0
160.  *    .1    .0    .0    .0    .0    .0    .0    .0
165.  *    .1    .0    .0    .0    .0    .0    .0    .0
170.  *    .1    .0    .0    .0    .0    .0    .0    .0
175.  *    .1    .0    .0    .0    .0    .0    .0    .0
180.  *    .1    .0    .0    .0    .0    .0    .0    .0
185.  *    .1    .0    .0    .0    .0    .0    .0    .0
190.  *    .1    .0    .0    .0    .0    .0    .0    .0
195.  *    .1    .0    .0    .0    .0    .0    .0    .0
200.  *    .2    .0    .0    .0    .0    .0    .0    .0
205.  *    .2    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                          PAGE  6
     JOB: Site 2 Veteran & Wilshire (S2NBAM.DAT)              RUN: Site 2 NO BUILD AM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .2    .0    .0    .0    .0    .0    .0    .0
215.  *    .2    .0    .0    .0    .0    .0    .0    .0
220.  *    .1    .0    .0    .0    .0    .0    .0    .0
225.  *    .1    .0    .0    .0    .0    .0    .0    .0
230.  *    .2    .0    .0    .0    .0    .0    .0    .0
235.  *    .2    .0    .0    .0    .0    .0    .0    .0
240.  *    .2    .0    .0    .0    .0    .0    .0    .0
245.  *    .1    .1    .0    .1    .0    .0    .0    .0
250.  *    .0    .1    .1    .1    .1    .0    .0    .0
255.  *    .0    .2    .2    .2    .1    .0    .0    .0
260.  *    .0    .2    .2    .2    .2    .0    .0    .0
265.  *    .0    .2    .2    .2    .2    .0    .0    .0
270.  *    .0    .2    .2    .2    .2    .0    .0    .0
275.  *    .0    .2    .2    .2    .1    .0    .0    .0
280.  *    .0    .2    .2    .2    .1    .1    .0    .0
285.  *    .0    .2    .2    .2    .1    .1    .0    .0
290.  *    .0    .2    .1    .1    .1    .1    .0    .0
295.  *    .0    .1    .1    .1    .1    .1    .0    .0
300.  *    .0    .1    .1    .1    .1    .1    .0    .0
305.  *    .0    .1    .1    .1    .1    .1    .0    .0
310.  *    .0    .1    .1    .1    .1    .1    .0    .0
315.  *    .0    .1    .1    .1    .1    .0    .0    .0
320.  *    .0    .2    .1    .1    .1    .0    .0    .0
325.  *    .0    .1    .1    .1    .1    .0    .0    .0
330.  *    .0    .1    .1    .1    .1    .0    .0    .0
335.  *    .0    .1    .1    .1    .1    .0    .0    .0
340.  *    .0    .1    .1    .1    .1    .0    .0    .0
345.  *    .0    .1    .1    .1    .1    .0    .0    .0
350.  *    .0    .1    .1    .1    .1    .0    .0    .0
355.  *    .0    .1    .1    .1    .1    .0    .0    .0
360.  *    .0    .1    .1    .1    .1    .0    .0    .0
------*------------------------------------------------
MAX   *    .2    .2    .2    .2    .2    .1    .0    .0
DEGR. *   95    35    65    55    40    25     0     0

THE HIGHEST CONCENTRATION IS     .40 PPM AT   90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   95 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT   85 DEGREES FROM REC10.
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1                        CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2NBPM.DAT)              RUN: Site 2 NO BUILD PM
      DATE: 03/19/2010   TIME: 09:06:18.82


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2    *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*--------------------------------------*--------------------------------------------------------------
        1. EB        Wil AP    *   -172.0     469.0      78.0     601.0 *     283.    62. AG  3358.    .8    .0 68.0
        2. EB        Wil AP    *     78.0     601.0     276.0     684.0 *     215.    67. AG  3358.    .8    .0 68.0
        3. EB        Wil T+R   *    276.0     684.0     778.0     856.0 *     531.    71. AG  3073.    .8    .0 68.0
        4. EB        Wil T+R Q *    678.0     822.0   -2149.1    -153.1 *    2991.   251. AG    20. 100.0    .0 48.0 1.51 151.9
        5. EB        Wil LT    *    259.0     724.0     761.0     889.0 *     528.    72. AG   285.    .8    .0 44.0
        6. EB        Wil LT Q  *    659.0     855.0    -858.8     357.4 *    1597.   252. AG    18. 100.0    .0 24.0 ****  81.1
        7. EB        Wil DP    *    782.0     851.0    1703.0    1145.0 *     967.    72. AG  3305.    .8    .0 68.0
        8. WB        Wil AP    *   1025.0    1019.0    1677.0    1228.0 *     685.    72. AG  4295.    .8    .0 68.0
        9. WB        Wil T+R   *   1025.0    1019.0     717.0     920.0 *     324.   252. AG  4276.    .8    .0 68.0
       10. WB        Wil T+R Q *    798.0     946.0    7799.9    3186.6 *    7352.    72. AG    25. 100.0    .0 48.0 2.68 373.5
       11. WB        Wil LT    *   1040.0     975.0     742.0     883.0 *     312.   253. AG    19.    .8    .0 44.0
       12. WB        Wil LT Q  *    824.0     908.0     948.3     946.0 *     130.    73. AG    21. 100.0    .0 24.0 9.00   6.6
       13. WB        Wil DP    *    715.0     922.0     201.0     748.0 *     543.   251. AG  4969.    .8    .0 68.0
       14. WB        Wil DP    *    201.0     748.0    -199.0     546.0 *     448.   243. AG  4969.    .8    .0 68.0
       15. NB        Vet AP    *    967.0     583.0    1327.0      75.0 *     623.   145. AG  1351.    .9    .0 32.0
       16. NB        Vet T+LT  *    960.0     579.0     781.0     840.0 *     316.   326. AG  1028.    .9    .0 56.0
       17. NB        Vet T+LT Q*    820.0     783.0    1448.3    -134.3 *    1112.   146. AG    21. 100.0    .0 36.0 1.33  56.5
       18. NB        Vet RT    *    964.0     622.0     813.0     839.0 *     264.   325. AG   323.    .9    .0 32.0
       19. NB        Vet RT Q  *    847.0     791.0     990.5     582.6 *     253.   145. AG     7. 100.0    .0 12.0 1.00  12.9
       20. NB        Vet DP    *    798.0     836.0     611.0    1170.0 *     383.   331. AG  1719.    .9    .0 44.0
       21. NB        Vet DP    *    611.0    1170.0     214.0    1729.0 *     686.   325. AG  1719.    .9    .0 44.0
       22. SB        Vet AP    *    544.0    1188.0     172.0    1701.0 *     634.   324. AG  1987.    .9    .0 44.0
       23. SB        Vet T+LT  *    550.0    1188.0     730.0     898.0 *     341.   148. AG   858.    .9    .0 56.0
       24. SB        Vet T+LT Q*    679.0     981.0      85.1    1937.0 *    1125.   328. AG    24. 100.0    .0 36.0 1.44  57.2
       25. SB        Vet RT    *    521.0    1169.0     695.0     888.0 *     331.   148. AG  1129.    .9    .0 44.0
       26. SB        Vet RT Q  *    643.0     972.0    -866.6    3405.5 *    2864.   328. AG    13. 100.0    .0 24.0 1.78 145.5
       27. SB        Vet DP    *    703.0     889.0    1292.0      46.0 *    1028.   145. AG   968.    .9    .0 44.0
1
                                                                                                                   PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2NBPM.DAT)              RUN: Site 2 NO BUILD PM
      DATE: 03/19/2010   TIME: 09:06:18.82

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*---------------------------------------------------------------------------------
        4. EB        Wil T+R Q *     150      68       2.0       3073        982       4.10      1        3
        6. EB        Wil LT Q  *     150     126       2.0        285         84       4.10      1        3
       10. WB        Wil T+R Q *     150      85       2.0       4276        982       4.10      1        3
       12. WB        Wil LT Q  *     150     143       2.0         19         84       4.10      1        3
       17. NB        Vet T+LT Q*     150      97       2.0       1028        790       4.10      1        3
       19. NB        Vet RT Q  *     150      95       2.0        323        955       4.10      1        3
       24. SB        Vet T+LT Q*     150     109       2.0        858        810       4.10      1        3
       26. SB        Vet RT Q  *     150      87       2.0       1129        804       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)           *
         RECEPTOR             *      X           Y          Z        *
     -------------------------*--------------------------------------*
      1. SE MID S             *      1066.0      492.0       5.0    *
      2. SE 164 S             *       942.0      686.0       5.0    *
      3. SE 82 S              *       892.0      756.0       5.0    *
      4. SE CNR               *       869.0      821.0       5.0    *
      5. SE 82 E              *       925.0      853.0       5.0    *
      6. SE 164 E             *      1005.0      880.0       5.0    *
      7. SE MID E             *      1219.0      947.0       5.0    *
      8. NE MID E             *      1144.0     1099.0       5.0    *
      9. NE 164 E             *       918.0     1026.0       5.0    *
     10. NE 82 E              *       838.0     1000.0       5.0    *
     11. NE CNR               *       759.0      983.0       5.0    *
     12. NE 82 N              *       716.0     1047.0       5.0    *
     13. NE 164 N             *       676.0     1120.0       5.0    *
     14. NE MID N             *       595.0     1269.0       5.0    *
     15. NW MID N             *       464.0     1209.0       5.0    *
     16. NW 164 N             *       546.0     1079.0       5.0    *
     17. NW 82 N              *       589.0     1010.0       5.0    *
     18. NW CNR               *       611.0      945.0       5.0    *
     19. NW 82 W              *       552.0      910.0       5.0    *
     20. NW 164 W             *       475.0      884.0       5.0    *
     21. NW MID W             *       273.0      815.0       5.0    *
     22. SW MID W             *       305.0      649.0       5.0    *
     23. SW 164 W             *       565.0      737.0       5.0    *
     24. SW 82 W              *       645.0      764.0       5.0    *
     25. SW CNR               *       718.0      779.0       5.0    *
     26. SW 82 S              *       774.0      718.0       5.0    *
     27. SW 164 S             *       824.0      646.0       5.0    *
     28. SW MID S             *       957.0      459.0       5.0    *
1
                                                                                                                   PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2NBPM.DAT)              RUN: Site 2 NO BUILD PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

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              concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  75.  *    .0    .0    .0    .0    .1    .1    .1    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  80.  *    .0    .0    .0    .0    .1    .1    .0    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .2    .1    .1
  85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .2    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 150.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .1    .0    .0    .0    .1    .1    .1    .1
 165.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 170.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 175.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 180.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 185.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 190.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 195.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 200.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
 205.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
1
                                                                                                                          PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2NBPM.DAT)              RUN: Site 2 NO BUILD PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
 215.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
 220.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
 225.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
 230.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .1    .0    .0    .0    .0    .0    .1    .2    .1
 235.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .0    .1    .2    .1
 240.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .1    .0    .0    .0    .0    .0    .1    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 255.  *    .1    .0    .0    .0    .0    .1    .1    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 260.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 265.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .1    .1    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .1    .1    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0
 315.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .1    .1    .2    .2    .2    .3    .3    .2    .2    .1    .0    .1    .2    .2    .2    .2    .1
 DEGR. *  150   155   150     0     0    40    30    65    75    75    75   300   160     0     0   340   340    80   230    65

1
                                                                                                                          PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2NBPM.DAT)              RUN: Site 2 NO BUILD PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .3    .2    .2    .1    .0    .0    .0
   5.  *    .0    .3    .2    .1    .1    .0    .0    .0
  10.  *    .0    .3    .3    .1    .1    .0    .0    .0
  15.  *    .0    .3    .3    .1    .1    .0    .0    .0
  20.  *    .0    .3    .2    .1    .1    .0    .0    .0
  25.  *    .0    .3    .2    .1    .1    .0    .0    .0
  30.  *    .0    .3    .2    .1    .1    .0    .0    .0
  35.  *    .0    .3    .2    .1    .0    .0    .0    .0
  40.  *    .0    .3    .2    .1    .0    .0    .0    .0
  45.  *    .0    .3    .1    .1    .0    .0    .0    .0
  50.  *    .0    .2    .1    .1    .1    .0    .0    .0
  55.  *    .0    .2    .1    .1    .1    .0    .0    .0
  60.  *    .1    .2    .1    .1    .1    .0    .0    .0
  65.  *    .1    .1    .1    .0    .1    .0    .0    .0
  70.  *    .1    .1    .0    .0    .1    .0    .0    .0
  75.  *    .1    .1    .0    .0    .0    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .2    .0    .0    .0    .0    .0    .0    .0
  90.  *    .2    .0    .0    .0    .0    .0    .0    .0
  95.  *    .2    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2NBPM.DAT)               RUN: Site 2 NO BUILD PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .2    .1    .2    .0    .0    .0    .0
 255.  *    .0    .2    .2    .2    .1    .0    .0    .0
 260.  *    .0    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .3    .2    .2    .2    .0    .0    .0
 275.  *    .0    .3    .2    .2    .2    .0    .0    .0
 280.  *    .0    .3    .2    .3    .3    .0    .0    .0
 285.  *    .0    .3    .3    .3    .2    .0    .0    .0
 290.  *    .0    .3    .3    .3    .2    .0    .0    .0
 295.  *    .0    .2    .3    .3    .2    .0    .0    .0
 300.  *    .0    .2    .3    .3    .2    .0    .0    .0
 305.  *    .0    .2    .3    .3    .2    .0    .0    .0
 310.  *    .0    .1    .3    .3    .2    .0    .0    .0
 315.  *    .0    .1    .3    .2    .2    .0    .0    .0
 320.  *    .0    .1    .2    .2    .2    .0    .0    .0
 325.  *    .0    .1    .2    .2    .2    .0    .0    .0
 330.  *    .0    .1    .2    .2    .1    .0    .0    .0
 335.  *    .0    .2    .2    .2    .1    .0    .0    .0
 340.  *    .0    .3    .2    .2    .1    .0    .0    .0
 345.  *    .0    .3    .2    .2    .1    .0    .0    .0
 350.  *    .0    .3    .2    .2    .1    .0    .0    .0
 355.  *    .0    .3    .2    .2    .1    .0    .0    .0
 360.  *    .0    .3    .2    .2    .1    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .2    .3    .3    .3    .3    .0    .0    .0
 DEGR. *   85     0    10   280   280     0     0     0

 THE HIGHEST CONCENTRATION IS      .30 PPM AT   75 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   75 DEGREES FROM REC10.
 THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT    0 DEGREES FROM REC22.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT)               RUN: Site 2 BUILD ALT1 AM
      DATE: 03/19/2010   TIME: 09:06:37.27


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI) (FT) (FT)        (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *   -172.0     469.0      78.0     601.0 *     283.    62. AG   5595.    .8    .0 68.0
       2. EB        Wil AP    *     78.0     601.0     276.0     684.0 *     215.    67. AG   5595.    .8    .0 68.0
       3. EB        Wil T+R   *    276.0     684.0     778.0     856.0 *     531.    71. AG   4672.    .8    .0 68.0
       4. EB        Wil T+R Q *    678.0     822.0   -5486.7   -1304.3 *    6521.   251. AG     17. 100.0    .0 48.0 2.06 331.3
       5. EB        Wil LT    *    259.0     724.0     761.0     889.0 *     528.    72. AG    923.    .8    .0 44.0
       6. EB        Wil LT Q  *    659.0     855.0   -4349.7    -787.0 *    5271.   252. AG     17. 100.0    .0 24.0 **** 267.8
       7. EB        Wil DP    *    782.0     851.0    1703.0    1145.0 *     967.    72. AG   4826.    .8    .0 68.0
       8. WB        Wil AP    *   1025.0    1019.0    1677.0    1228.0 *     685.    72. AG   3179.    .8    .0 68.0
       9. WB        Wil T+R   *   1025.0    1019.0     717.0     920.0 *     324.   252. AG   3160.    .8    .0 68.0
      10. WB        Wil T+R Q *    798.0     946.0    4867.3    2248.2 *    4273.    72. AG     25. 100.0    .0 48.0 1.92 217.0
      11. WB        Wil LT    *   1040.0     975.0     742.0     883.0 *     312.   253. AG     19.    .8    .0 44.0
      12. WB        Wil LT Q  *    824.0     908.0     948.3     946.0 *     130.    73. AG     21. 100.0    .0 24.0 9.00   6.6
      13. WB        Wil DP    *    715.0     922.0     201.0     748.0 *     543.   251. AG   3487.    .8    .0 68.0
      14. WB        Wil DP    *    201.0     748.0    -199.0     546.0 *     448.   243. AG   3487.    .8    .0 68.0
      15. NB        Vet AP    *    967.0     583.0    1327.0      75.0 *     623.   145. AG    959.    .9    .0 32.0
      16. NB        Vet T+LT  *    960.0     579.0     781.0     840.0 *     316.   326. AG    827.    .9    .0 56.0
      17. NB        Vet T+LT Q*    820.0     783.0    1292.3      93.6 *     836.   146. AG     24. 100.0    .0 36.0 1.27  42.5
      18. NB        Vet RT    *    964.0     622.0     813.0     839.0 *     264.   325. AG    132.    .9    .0 32.0
      19. NB        Vet RT Q  *    847.0     791.0     889.6     729.2 *      75.   145. AG      8. 100.0    .0 12.0  .53   3.8
      20. NB        Vet DP    *    798.0     836.0     611.0    1170.0 *     383.   331. AG   1751.    .9    .0 44.0
      21. NB        Vet DP    *    611.0    1170.0     214.0    1729.0 *     686.   325. AG   1751.    .9    .0 44.0
      22. SB        Vet AP    *    544.0    1188.0     172.0    1701.0 *     634.   324. AG   1151.    .9    .0 44.0
      23. SB        Vet T+LT  *    550.0    1188.0     730.0     898.0 *     341.   148. AG    820.    .9    .0 56.0
      24. SB        Vet T+LT Q*    679.0     981.0    -122.4    2271.1 *    1519.   328. AG     26. 100.0    .0 36.0 1.84  77.2
      25. SB        Vet RT    *    521.0    1169.0     695.0     888.0 *     331.   148. AG    331.    .9    .0 44.0
      26. SB        Vet RT Q  *    643.0     972.0     600.2    1041.0 *      81.   328. AG     13. 100.0    .0 24.0  .53   4.1
      27. SB        Vet DP    *    703.0     889.0    1292.0      46.0 *    1028.   145. AG    817.    .9    .0 44.0
1
                                                                                                                 PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT)               RUN: Site 2 BUILD ALT1 AM
      DATE: 03/19/2010   TIME: 09:06:37.27

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)     (SEC)     (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *     150       59       2.0      4672        981       4.10      1         3
       6. EB        Wil LT Q  *     150      118       2.0       923         84       4.10      1         3
      10. WB        Wil T+R Q *     150       84       2.0      3160        997       4.10      1         3
      12. WB        Wil LT Q  *     150      143       2.0        19         84       4.10      1         3
      17. NB        Vet T+LT Q*     150      109       2.0       827        877       4.10      1         3
      19. NB        Vet RT Q  *     150      104       2.0       132        885       4.10      1         3
      24. SB        Vet T+LT Q*     150      120       2.0       820        858       4.10      1         3
      26. SB        Vet RT Q  *     150       90       2.0       331        834       4.10      1         3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *      1066.0      492.0         5.0   *
      2. SE 164 S             *       942.0      686.0         5.0   *
      3. SE 82 S              *       892.0      756.0         5.0   *
      4. SE CNR               *       869.0      821.0         5.0   *
      5. SE 82 E              *       925.0      853.0         5.0   *
      6. SE 164 E             *      1005.0      880.0         5.0   *
      7. SE MID E             *      1219.0      947.0         5.0   *
      8. NE MID E             *      1144.0     1099.0         5.0   *
      9. NE 164 E             *       918.0     1026.0         5.0   *
     10. NE 82 E              *       838.0     1000.0         5.0   *
     11. NE CNR               *       759.0      983.0         5.0   *
     12. NE 82 N              *       716.0     1047.0         5.0   *
     13. NE 164 N             *       676.0     1120.0         5.0   *
     14. NE MID N             *       595.0     1269.0         5.0   *
     15. NW MID N             *       464.0     1209.0         5.0   *
     16. NW 164 N             *       546.0     1079.0         5.0   *
     17. NW 82 N              *       589.0     1010.0         5.0   *
     18. NW CNR               *       611.0      945.0         5.0   *
     19. NW 82 W              *       552.0      910.0         5.0   *
     20. NW 164 W             *       475.0      884.0         5.0   *
     21. NW MID W             *       273.0      815.0         5.0   *
     22. SW MID W             *       305.0      649.0         5.0   *
     23. SW 164 W             *       565.0      737.0         5.0   *
     24. SW 82 W              *       645.0      764.0         5.0   *
     25. SW CNR               *       718.0      779.0         5.0   *
     26. SW 82 S              *       774.0      718.0         5.0   *
     27. SW 164 S             *       824.0      646.0         5.0   *
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     28. SW MID S             *       957.0      459.0        5.0   *
1
                                                                                                                            PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT)               RUN: Site 2 BUILD ALT1 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
    0.  *   .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
    5.  *   .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   10.  *   .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   15.  *   .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   20.  *   .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
   25.  *   .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   30.  *   .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   35.  *   .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   40.  *   .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   45.  *   .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   50.  *   .0    .0    .1    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   55.  *   .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   60.  *   .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   65.  *   .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   70.  *   .0    .0    .0    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1
   75.  *   .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
   80.  *   .0    .0    .0    .0    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
   85.  *   .0    .0    .0    .0    .0    .1    .0    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
   90.  *   .0    .0    .0    .0    .0    .0    .0    .2    .4    .3    .3    .0    .0    .0    .0    .0    .0    .1    .1    .1
   95.  *   .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .0    .0    .0    .1    .1    .1
  100.  *   .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .1    .0    .0    .1    .1
  105.  *   .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
  110.  *   .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
  115.  *   .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .2
  120.  *   .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
  125.  *   .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
  130.  *   .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .2
  135.  *   .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .2    .2
  140.  *   .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
  145.  *   .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
  150.  *   .1    .1    .1    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
  155.  *   .1    .1    .1    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
  160.  *   .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .0    .1    .0    .0    .0    .0    .1    .2    .2
  165.  *   .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
  170.  *   .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
  175.  *   .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
  180.  *   .1    .1    .1    .1    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
  185.  *   .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
  190.  *   .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
  195.  *   .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
  200.  *   .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
  205.  *   .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .2    .2    .2
1
                                                                                                                            PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT)               RUN: Site 2 BUILD ALT1 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
  210.  *   .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1
  215.  *   .1    .1    .1    .0    .0    .0    .0    .3    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .1
  220.  *   .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  225.  *   .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  230.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  235.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  240.  *   .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  245.  *   .1    .1    .1    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  250.  *   .1    .1    .1    .0    .0    .1    .1    .1    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  255.  *   .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
  260.  *   .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  265.  *   .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  270.  *   .1    .1    .1    .1    .2    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  275.  *   .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  280.  *   .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  285.  *   .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0
  290.  *   .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0    .0    .0    .0
  295.  *   .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0    .0    .0    .0
  300.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0
  305.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
  310.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0
  315.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0
  320.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
  325.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  330.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  335.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
```

```
 340.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 345.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 350.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 355.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 360.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 ------*-----------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .2    .2    .2    .2    .3    .4    .3    .3    .2    .1    .1    .1    .1    .1    .2    .2    .2
 DEGR. *  150   150     0   280    50    50    55    95    90    85    90   285   160   305     0     0     0   205   135   115

1
                                                                                                                   PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT)               RUN: Site 2 BUILD ALT1 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .1    .0    .0    .0
   5.  *    .0    .1    .1    .1    .1    .0    .0    .0
  10.  *    .0    .1    .1    .1    .1    .0    .0    .0
  15.  *    .0    .1    .1    .1    .1    .0    .0    .0
  20.  *    .0    .1    .1    .1    .1    .0    .0    .0
  25.  *    .0    .1    .1    .1    .1    .1    .0    .0
  30.  *    .0    .2    .1    .1    .1    .1    .0    .0
  35.  *    .0    .2    .1    .1    .1    .1    .0    .0
  40.  *    .0    .2    .1    .1    .2    .1    .0    .0
  45.  *    .0    .2    .1    .1    .2    .1    .0    .0
  50.  *    .0    .2    .1    .1    .1    .1    .0    .0
  55.  *    .0    .2    .1    .2    .1    .1    .0    .0
  60.  *    .0    .1    .1    .2    .1    .1    .0    .0
  65.  *    .1    .1    .2    .2    .1    .0    .0    .0
  70.  *    .1    .1    .2    .2    .1    .0    .0    .0
  75.  *    .1    .1    .1    .1    .1    .0    .0    .0
  80.  *    .1    .1    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .2    .0    .0    .0    .0    .0    .0    .0
 100.  *    .2    .0    .0    .0    .0    .0    .0    .0
 105.  *    .2    .0    .0    .0    .0    .0    .0    .0
 110.  *    .2    .0    .0    .0    .0    .0    .0    .0
 115.  *    .2    .0    .0    .0    .0    .0    .0    .0
 120.  *    .2    .0    .0    .0    .0    .0    .0    .0
 125.  *    .2    .0    .0    .0    .0    .0    .0    .0
 130.  *    .2    .0    .0    .0    .0    .0    .0    .0
 135.  *    .2    .0    .0    .0    .0    .0    .0    .0
 140.  *    .2    .0    .0    .0    .0    .0    .0    .0
 145.  *    .2    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .2    .0    .0    .0    .0    .0    .0    .0
 205.  *    .2    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                   PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2B1AM.DAT)               RUN: Site 2 BUILD ALT1 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .0    .1    .0    .0    .0    .0
 250.  *    .0    .2    .1    .1    .1    .0    .0    .0
 255.  *    .0    .2    .2    .2    .1    .0    .0    .0
 260.  *    .0    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .2    .2    .2    .2    .0    .0    .0
 275.  *    .0    .2    .2    .2    .1    .0    .0    .0
 280.  *    .0    .2    .2    .2    .1    .1    .0    .0
 285.  *    .0    .2    .2    .2    .1    .1    .0    .0
```

```
290.  *    .0    .2    .2    .2    .1    .1    .0    .0
295.  *    .0    .2    .1    .1    .1    .1    .0    .0
300.  *    .0    .1    .1    .1    .1    .1    .0    .0
305.  *    .0    .1    .1    .1    .1    .1    .0    .0
310.  *    .0    .1    .1    .1    .1    .1    .0    .0
315.  *    .0    .1    .1    .1    .1    .0    .0    .0
320.  *    .0    .2    .1    .1    .1    .0    .0    .0
325.  *    .0    .1    .1    .1    .1    .0    .0    .0
330.  *    .0    .1    .1    .1    .1    .0    .0    .0
335.  *    .0    .1    .1    .1    .1    .0    .0    .0
340.  *    .0    .1    .1    .1    .1    .0    .0    .0
345.  *    .0    .1    .1    .1    .1    .0    .0    .0
350.  *    .0    .1    .1    .1    .1    .0    .0    .0
355.  *    .0    .1    .1    .1    .1    .0    .0    .0
360.  *    .0    .1    .1    .1    .1    .0    .0    .0
------*-------------------------------------------------
MAX   *    .2    .2    .2    .2    .2    .1    .0    .0
DEGR. *   95    30    65    55    40    25     0     0

THE HIGHEST CONCENTRATION IS     .40 PPM AT   90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   95 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT   85 DEGREES FROM REC10.
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT)               RUN: Site 2 BUILD ALT1 PM
      DATE: 03/21/2010   TIME: 22:20:17.29


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *   -172.0     469.0      78.0     601.0 *     283.    62. AG   3430.    .8    .0 68.0
       2. EB        Wil AP    *     78.0     601.0     276.0     684.0 *     215.    67. AG   3430.    .8    .0 68.0
       3. EB        Wil T+R   *    276.0     684.0     778.0     856.0 *     531.    71. AG   3138.    .8    .0 68.0
       4. EB        Wil T+R Q *    678.0     822.0   -2096.1    -134.8 *    2934.   251. AG     19. 100.0    .0 48.0 1.48 149.1
       5. EB        Wil LT    *    259.0     724.0     761.0     889.0 *     528.    72. AG    292.    .8    .0 44.0
       6. EB        Wil LT Q  *    659.0     855.0    -925.3     335.6 *    1667.   252. AG     19. 100.0    .0 24.0 ****  84.7
       7. EB        Wil DP    *    782.0     851.0    1703.0    1145.0 *     967.    72. AG   3339.    .8    .0 68.0
       8. WB        Wil AP    *   1025.0    1019.0    1677.0    1228.0 *     685.    72. AG   4302.    .8    .0 68.0
       9. WB        Wil T+R   *   1025.0    1019.0     717.0     920.0 *     324.   252. AG   4286.    .8    .0 68.0
      10. WB        Wil T+R Q *    798.0     946.0    7629.1    3132.0 *    7172.    72. AG     24. 100.0    .0 48.0 2.57 364.4
      11. WB        Wil LT    *   1040.0     975.0     742.0     883.0 *     312.   253. AG     16.    .8    .0 44.0
      12. WB        Wil LT Q  *    824.0     908.0     933.5     941.5 *     114.    73. AG     21. 100.0    .0 24.0 8.00   5.8
      13. WB        Wil DP    *    715.0     922.0     201.0     748.0 *     543.   251. AG   4930.    .8    .0 68.0
      14. WB        Wil DP    *    201.0     748.0    -199.0     546.0 *     448.   243. AG   4930.    .8    .0 68.0
      15. NB        Vet AP    *    967.0     583.0    1327.0      75.0 *     623.   145. AG   1373.    .9    .0 32.0
      16. NB        Vet T+LT  *    960.0     579.0     781.0     840.0 *     316.   326. AG   1090.    .9    .0 56.0
      17. NB        Vet T+LT Q*    820.0     783.0    1686.5    -482.0 *    1533.   146. AG     22. 100.0    .0 36.0 1.52  77.9
      18. NB        Vet RT    *    964.0     622.0     813.0     839.0 *     264.   325. AG    283.    .9    .0 32.0
      19. NB        Vet RT Q  *    847.0     791.0     959.2     628.0 *     198.   145. AG      7. 100.0    .0 12.0  .94  10.1
      20. NB        Vet DP    *    798.0     836.0     611.0    1170.0 *     383.   331. AG   1841.    .9    .0 44.0
      21. NB        Vet DP    *    611.0    1170.0     214.0    1729.0 *     686.   325. AG   1841.    .9    .0 44.0
      22. SB        Vet AP    *    544.0    1188.0     172.0    1701.0 *     634.   324. AG   1997.    .9    .0 44.0
      23. SB        Vet T+LT  *    550.0    1188.0     730.0     898.0 *     341.   148. AG    894.    .9    .0 56.0
      24. SB        Vet T+LT Q*    679.0     981.0     262.7    1651.2 *     789.   328. AG     24. 100.0    .0 36.0 1.26  40.1
      25. SB        Vet RT    *    521.0    1169.0     695.0     888.0 *     331.   148. AG   1103.    .9    .0 44.0
      26. SB        Vet RT Q  *    643.0     972.0    -894.5    3450.6 *    2917.   328. AG     13. 100.0    .0 24.0 1.85 148.2
      27. SB        Vet DP    *    703.0     889.0    1292.0      46.0 *    1028.   145. AG    992.    .9    .0 44.0
1
                                                                                                                PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT)               RUN: Site 2 BUILD ALT1 PM
      DATE: 03/21/2010   TIME: 22:20:17.29

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *     150       65       2.0      3138        984       4.10     1        3
       6. EB        Wil LT Q  *     150      128       2.0       292         84       4.10     1        3
      10. WB        Wil T+R Q *     150       82       2.0      4286        979       4.10     1        3
      12. WB        Wil LT Q  *     150      143       2.0        16         84       4.10     1        3
      17. NB        Vet T+LT Q*     150      100       2.0      1090        782       4.10     1        3
      19. NB        Vet RT Q  *     150       95       2.0       283        885       4.10     1        3
      24. SB        Vet T+LT Q*     150      109       2.0       800        858       4.10     1        3
      26. SB        Vet RT Q  *     150       90       2.0      1103        800       4.10     1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *      1066.0      492.0        5.0   *
      2. SE 164 S             *       942.0      686.0        5.0   *
      3. SE 82 S              *       892.0      756.0        5.0   *
      4. SE CNR               *       869.0      821.0        5.0   *
      5. SE 82 E              *       925.0      853.0        5.0   *
      6. SE 164 E             *      1005.0      880.0        5.0   *
      7. SE MID E             *      1219.0      947.0        5.0   *
      8. NE MID E             *      1144.0     1099.0        5.0   *
      9. NE 164 E             *       918.0     1026.0        5.0   *
     10. NE 82 E              *       838.0     1000.0        5.0   *
     11. NE CNR               *       759.0      983.0        5.0   *
     12. NE 82 N              *       716.0     1047.0        5.0   *
     13. NE 164 N             *       676.0     1120.0        5.0   *
     14. NE MID N             *       595.0     1269.0        5.0   *
     15. NW MID N             *       464.0     1209.0        5.0   *
     16. NW 164 N             *       546.0     1079.0        5.0   *
     17. NW 82 N              *       589.0     1010.0        5.0   *
     18. NW CNR               *       611.0      945.0        5.0   *
     19. NW 82 W              *       552.0      910.0        5.0   *
     20. NW 164 W             *       475.0      884.0        5.0   *
     21. NW MID W             *       273.0      815.0        5.0   *
     22. SW MID W             *       305.0      649.0        5.0   *
     23. SW 164 W             *       565.0      737.0        5.0   *
     24. SW 82 W              *       645.0      764.0        5.0   *
     25. SW CNR               *       718.0      779.0        5.0   *
     26. SW 82 S              *       774.0      718.0        5.0   *
     27. SW 164 S             *       824.0      646.0        5.0   *
     28. SW MID S             *       957.0      459.0        5.0   *
1
                                                                                                                PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT)               RUN: Site 2 BUILD ALT1 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

```
               concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
  0.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  5.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
 10.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 15.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 20.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 25.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 30.  *   .0    .0    .0    .1    .1    .1    .2    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 35.  *   .0    .0    .0    .1    .1    .1    .2    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 40.  *   .0    .0    .0    .1    .1    .2    .2    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 45.  *   .0    .0    .0    .1    .1    .2    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 50.  *   .0    .0    .0    .1    .1    .2    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 55.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 60.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 65.  *   .0    .0    .0    .1    .1    .1    .1    .1    .0     .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
 70.  *   .0    .0    .0    .1    .1    .1    .1    .2    .2     .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 75.  *   .0    .0    .0    .0    .1    .1    .1    .2    .3     .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 80.  *   .0    .0    .0    .0    .1    .1    .0    .2    .3     .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 85.  *   .0    .0    .0    .0    .0    .0    .0    .2    .3     .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 90.  *   .0    .0    .0    .0    .0    .0    .0    .2    .3     .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 95.  *   .0    .0    .0    .0    .0    .0    .0    .2    .3     .2    .2    .0    .0    .0    .0    .0    .0    .2    .1    .1
100.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2     .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
105.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2     .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
110.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2     .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
115.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2     .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
120.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2     .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
125.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2     .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
130.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2     .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
135.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2     .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
140.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2     .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
145.  *   .1    .0    .0    .0    .0    .0    .0    .2    .2     .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
150.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2     .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
155.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2     .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
160.  *   .1    .1    .1    .1    .0    .0    .0    .2    .2     .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
165.  *   .1    .1    .1    .1    .0    .0    .0    .2    .2     .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
170.  *   .1    .1    .1    .1    .0    .0    .0    .2    .2     .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
175.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2     .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
180.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2     .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
185.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2     .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
190.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2     .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
195.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2     .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
200.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2     .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
205.  *   .1    .0    .1    .0    .0    .0    .0    .2    .2     .2    .1    .2    .1    .0    .0    .0    .1    .1    .1    .1
1
                                                                                                                      PAGE  4
     JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT)               RUN: Site 2 BUILD ALT1 PM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
210.  *   .1    .0    .1    .0    .0    .0    .0    .2    .2     .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
215.  *   .1    .0    .0    .0    .0    .0    .0    .2    .2     .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
220.  *   .1    .0    .1    .0    .0    .0    .0    .2    .2     .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
225.  *   .1    .0    .1    .0    .0    .0    .0    .2    .2     .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
230.  *   .1    .0    .0    .0    .0    .0    .0    .2    .2     .1    .1    .1    .0    .0    .0    .0    .0    .1    .2    .1
235.  *   .1    .0    .0    .0    .0    .0    .0    .2    .2     .2    .1    .1    .0    .0    .0    .0    .0    .1    .2    .1
240.  *   .1    .0    .0    .0    .0    .0    .0    .2    .1     .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
245.  *   .1    .0    .0    .0    .0    .0    .0    .2    .1     .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
250.  *   .1    .0    .0    .0    .0    .0    .1    .1    .1     .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
255.  *   .1    .0    .0    .0    .0    .1    .1    .0    .1     .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
260.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
265.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
270.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
275.  *   .1    .0    .0    .0    .1    .1    .1    .0    .0     .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
280.  *   .1    .1    .0    .0    .1    .1    .1    .0    .0     .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
285.  *   .1    .1    .0    .0    .1    .1    .1    .0    .0     .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
290.  *   .1    .1    .0    .0    .1    .1    .1    .0    .0     .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0
295.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0     .0    .1    .1    .0    .1    .0    .0    .0    .0    .0    .0
300.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0     .0    .1    .2    .0    .1    .0    .0    .0    .0    .0    .0
305.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0     .0    .1    .2    .0    .1    .0    .0    .0    .0    .0    .0
310.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0     .0    .2    .2    .0    .1    .0    .0    .0    .0    .0    .0
315.  *   .1    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
320.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
325.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
330.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
335.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
340.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
345.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
350.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
355.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
360.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0     .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
------*------------------------------------------------------------------------------------------------------------------------
MAX   *   .1    .1    .1    .1    .1    .2    .2    .2    .3     .3    .2    .2    .1    .1    .1    .2    .2    .2    .2    .1
DEGR. *  145   150   150     0     0    40    30    70    75     75    75   205   160   295     0   345   345    95   230    65

1
                                                                                                                      PAGE  5
     JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT)               RUN: Site 2 BUILD ALT1 PM

      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .2    .2    .2    .1    .0    .0    .0
   5.  *    .0    .2    .2    .1    .1    .0    .0    .0
  10.  *    .0    .2    .2    .1    .1    .0    .0    .0
  15.  *    .0    .3    .2    .1    .1    .0    .0    .0
  20.  *    .0    .3    .2    .1    .1    .0    .0    .0
  25.  *    .0    .3    .2    .1    .1    .0    .0    .0
  30.  *    .0    .3    .2    .1    .1    .0    .0    .0
  35.  *    .0    .3    .2    .1    .0    .0    .0    .0
  40.  *    .0    .3    .1    .1    .0    .0    .0    .0
  45.  *    .0    .3    .1    .1    .0    .0    .0    .0
  50.  *    .0    .2    .1    .1    .1    .0    .0    .0
  55.  *    .0    .2    .1    .1    .1    .0    .0    .0
  60.  *    .1    .2    .1    .1    .1    .0    .0    .0
  65.  *    .1    .1    .1    .0    .1    .0    .0    .0
  70.  *    .1    .1    .0    .0    .1    .0    .0    .0
  75.  *    .1    .1    .0    .0    .0    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .2    .0    .0    .0    .0    .0    .0    .0
  90.  *    .2    .0    .0    .0    .0    .0    .0    .0
  95.  *    .2    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2B1PM.DAT)              RUN: Site 2 BUILD ALT1 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .2    .0    .1    .0    .0    .0    .0
 255.  *    .0    .2    .2    .2    .2    .0    .0    .0
 260.  *    .0    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .3    .2    .2    .2    .0    .0    .0
 275.  *    .0    .3    .2    .2    .2    .0    .0    .0
 280.  *    .0    .3    .2    .3    .2    .0    .0    .0
 285.  *    .0    .3    .3    .3    .2    .0    .0    .0
 290.  *    .0    .2    .3    .3    .2    .0    .0    .0
 295.  *    .0    .2    .3    .3    .2    .0    .0    .0
 300.  *    .0    .2    .3    .3    .2    .0    .0    .0
 305.  *    .0    .2    .3    .2    .2    .0    .0    .0
 310.  *    .0    .1    .2    .2    .2    .0    .0    .0
 315.  *    .0    .0    .2    .2    .2    .0    .0    .0
 320.  *    .0    .0    .2    .2    .2    .0    .0    .0
 325.  *    .0    .0    .2    .2    .1    .0    .0    .0
 330.  *    .0    .0    .2    .2    .1    .0    .0    .0
 335.  *    .0    .1    .2    .2    .1    .0    .0    .0
 340.  *    .0    .2    .2    .2    .1    .0    .0    .0
 345.  *    .0    .2    .2    .2    .1    .0    .0    .0
 350.  *    .0    .2    .2    .2    .1    .0    .0    .0
 355.  *    .0    .2    .2    .2    .1    .0    .0    .0
 360.  *    .0    .2    .2    .2    .1    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .2    .3    .3    .3    .2    .0    .0    .0
 DEGR. *   85    15   285   280   255     0     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   75 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   75 DEGREES FROM REC10.
 THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT   15 DEGREES FROM REC22.
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1                        CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2B2AM.DAT)              RUN: Site 2 BUILD ALT2 AM
      DATE: 03/19/2010   TIME: 13:25:51.13


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*-------------------------------------------------------------
       1. EB        Wil AP    *   -172.0     469.0      78.0     601.0 *     283.    62. AG   5509.    .8    .0 68.0
       2. EB        Wil AP    *     78.0     601.0     276.0     684.0 *     215.    67. AG   5509.    .8    .0 68.0
       3. EB        Wil T+R   *    276.0     684.0     778.0     856.0 *     531.    71. AG   4596.    .8    .0 68.0
       4. EB        Wil T+R Q *    678.0     822.0   -5231.7   -1216.4 *    6251.   251. AG     17. 100.0    .0 48.0 2.00 317.6
       5. EB        Wil LT    *    259.0     724.0     761.0     889.0 *     528.    72. AG    913.    .8    .0 44.0
       6. EB        Wil LT Q  *    659.0     855.0   -4293.8    -768.7 *    5212.   252. AG     17. 100.0    .0 24.0 **** 264.8
       7. EB        Wil DP    *    782.0     851.0    1703.0    1145.0 *     967.    72. AG   4761.    .8    .0 68.0
       8. WB        Wil AP    *   1025.0    1019.0    1677.0    1228.0 *     685.    72. AG   3138.    .8    .0 68.0
       9. WB        Wil T+R   *   1025.0    1019.0     717.0     920.0 *     324.   252. AG   3121.    .8    .0 68.0
      10. WB        Wil T+R Q *    798.0     946.0    4643.8    2176.7 *    4038.    72. AG     24. 100.0    .0 48.0 1.84 205.1
      11. WB        Wil LT    *   1040.0     975.0     742.0     883.0 *     312.   253. AG     17.    .8    .0 44.0
      12. WB        Wil LT Q  *    824.0     908.0     933.5     941.5 *     114.    73. AG     21. 100.0    .0 24.0 8.00   5.8
      13. WB        Wil DP    *    715.0     922.0     201.0     748.0 *     543.   251. AG   3409.    .8    .0 68.0
      14. WB        Wil DP    *    201.0     748.0    -199.0     546.0 *     448.   243. AG   3409.    .8    .0 68.0
      15. NB        Vet AP    *    967.0     583.0    1327.0      75.0 *     623.   145. AG    947.    .9    .0 32.0
      16. NB        Vet T+LT  *    960.0     579.0     781.0     840.0 *     316.   326. AG    815.    .9    .0 56.0
      17. NB        Vet T+LT Q*    820.0     783.0    1320.7      52.0 *     886.   146. AG     24. 100.0    .0 36.0 1.31  45.0
      18. NB        Vet RT    *    964.0     622.0     813.0     839.0 *     264.   325. AG    132.    .9    .0 32.0
      19. NB        Vet RT Q  *    847.0     791.0     890.4     728.0 *      77.   145. AG      8. 100.0    .0 12.0  .51   3.9
      20. NB        Vet DP    *    798.0     836.0     611.0    1170.0 *     383.   331. AG   1755.    .9    .0 44.0
      21. NB        Vet DP    *    611.0    1170.0     214.0    1729.0 *     686.   325. AG   1755.    .9    .0 44.0
      22. SB        Vet AP    *    544.0    1188.0     172.0    1701.0 *     634.   324. AG   1085.    .9    .0 44.0
      23. SB        Vet T+LT  *    550.0    1188.0     730.0     898.0 *     341.   148. AG    767.    .9    .0 56.0
      24. SB        Vet T+LT Q*    679.0     981.0     -24.3    2113.1 *    1333.   328. AG     26. 100.0    .0 36.0 1.73  67.7
      25. SB        Vet RT    *    521.0    1169.0     695.0     888.0 *     331.   148. AG    318.    .9    .0 44.0
      26. SB        Vet RT Q  *    643.0     972.0     601.8    1038.5 *      78.   328. AG     13. 100.0    .0 24.0  .51   4.0
      27. SB        Vet DP    *    703.0     889.0    1292.0      46.0 *    1028.   145. AG    751.    .9    .0 44.0
1
                                                                                                            PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2B2AM.DAT)              RUN: Site 2 BUILD ALT2 AM
      DATE: 03/19/2010   TIME: 13:25:51.13

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION  IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE  EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)     (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *     150       57       2.0      4596        969       4.10      1        3
       6. EB        Wil LT Q  *     150      118       2.0       913         84       4.10      1        3
      10. WB        Wil T+R Q *     150       82       2.0      3121        995       4.10      1        3
      12. WB        Wil LT Q  *     150      143       2.0        17         84       4.10      1        3
      17. NB        Vet T+LT Q*     150      111       2.0       815        888       4.10      1        3
      19. NB        Vet RT Q  *     150      106       2.0       132        967       4.10      1        3
      24. SB        Vet T+LT Q*     150      120       2.0       767        852       4.10      1        3
      26. SB        Vet RT Q  *     150       90       2.0       318        837       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)           *
         RECEPTOR             *      X           Y          Z        *
     -------------------------*--------------------------------------*
      1. SE MID S             *      1066.0      492.0       5.0   *
      2. SE 164 S             *       942.0      686.0       5.0   *
      3. SE 82 S              *       892.0      756.0       5.0   *
      4. SE CNR               *       869.0      821.0       5.0   *
      5. SE 82 E              *       925.0      853.0       5.0   *
      6. SE 164 E             *      1005.0      880.0       5.0   *
      7. SE MID E             *      1219.0      947.0       5.0   *
      8. NE MID E             *      1144.0     1099.0       5.0   *
      9. NE 164 E             *       918.0     1026.0       5.0   *
     10. NE 82 E              *       838.0     1000.0       5.0   *
     11. NE CNR               *       759.0      983.0       5.0   *
     12. NE 82 N              *       716.0     1047.0       5.0   *
     13. NE 164 N             *       676.0     1120.0       5.0   *
     14. NE MID N             *       595.0     1269.0       5.0   *
     15. NW MID N             *       464.0     1209.0       5.0   *
     16. NW 164 N             *       546.0     1079.0       5.0   *
     17. NW 82 N              *       589.0     1010.0       5.0   *
     18. NW CNR               *       611.0      945.0       5.0   *
     19. NW 82 W              *       552.0      910.0       5.0   *
     20. NW 164 W             *       475.0      884.0       5.0   *
     21. NW MID W             *       273.0      815.0       5.0   *
     22. SW MID W             *       305.0      649.0       5.0   *
     23. SW 164 W             *       565.0      737.0       5.0   *
     24. SW 82 W              *       645.0      764.0       5.0   *
     25. SW CNR               *       718.0      779.0       5.0   *
     26. SW 82 S              *       774.0      718.0       5.0   *
     27. SW 164 S             *       824.0      646.0       5.0   *
     28. SW MID S             *       957.0      459.0       5.0   *
1
                                                                                                            PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2B2AM.DAT)              RUN: Site 2 BUILD ALT2 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

```
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   5.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  10.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  15.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  20.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
  25.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .1    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1
  75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  80.  *    .0    .0    .0    .0    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  85.  *    .0    .0    .0    .0    .0    .1    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .3    .3    .0    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .0    .0    .0    .1    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .1    .0    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
 120.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
 125.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 145.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 150.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 155.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 160.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .0    .1    .0    .0    .0    .0    .1    .2    .2
 165.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 170.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 175.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 180.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .1    .2
 185.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
 190.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
 195.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
 200.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
 205.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .2    .2
1
                                                                                                                         PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2B2AM.DAT)               RUN: Site 2 BUILD ALT2 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .2    .1
 215.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .1
 220.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 225.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 230.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 235.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 240.  *    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .1    .1    .1    .0    .0    .0    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .1    .1    .1    .0    .0    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 255.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 260.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .1    .1    .1    .1    .2    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0    .0    .0    .0
 295.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0    .0    .0    .0
 300.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0
 305.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
 310.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0
 315.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0
 320.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 340.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 345.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 350.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 355.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 360.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .2    .2    .2    .2    .3    .3    .3    .3    .2    .1    .1    .1    .1    .1    .1    .2    .2
 DEGR. *   150   150     0   285    50    50    55    95    85    90    90   285   160   305     0     0     0    90   140   115

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                                                                                                                         PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2B2AM.DAT)               RUN: Site 2 BUILD ALT2 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .1    .0    .0    .0
   5.  *    .0    .1    .1    .1    .1    .0    .0    .0
  10.  *    .0    .1    .1    .1    .1    .0    .0    .0
  15.  *    .0    .1    .1    .1    .1    .0    .0    .0
  20.  *    .0    .1    .1    .1    .1    .0    .0    .0
  25.  *    .0    .1    .1    .1    .1    .0    .0    .0
  30.  *    .0    .1    .1    .1    .1    .1    .0    .0
  35.  *    .0    .2    .1    .1    .1    .1    .0    .0
  40.  *    .0    .2    .1    .1    .1    .1    .0    .0
  45.  *    .0    .2    .1    .1    .2    .1    .0    .0
  50.  *    .0    .2    .1    .1    .1    .1    .0    .0
  55.  *    .0    .2    .1    .2    .1    .1    .0    .0
  60.  *    .0    .1    .1    .2    .1    .1    .0    .0
  65.  *    .1    .1    .2    .2    .1    .0    .0    .0
  70.  *    .1    .1    .2    .2    .1    .0    .0    .0
  75.  *    .1    .1    .1    .1    .1    .0    .0    .0
  80.  *    .1    .1    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .1    .0    .0    .0    .0    .0    .0    .0
 100.  *    .2    .0    .0    .0    .0    .0    .0    .0
 105.  *    .2    .0    .0    .0    .0    .0    .0    .0
 110.  *    .2    .0    .0    .0    .0    .0    .0    .0
 115.  *    .2    .0    .0    .0    .0    .0    .0    .0
 120.  *    .2    .0    .0    .0    .0    .0    .0    .0
 125.  *    .2    .0    .0    .0    .0    .0    .0    .0
 130.  *    .2    .0    .0    .0    .0    .0    .0    .0
 135.  *    .2    .0    .0    .0    .0    .0    .0    .0
 140.  *    .2    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .2    .0    .0    .0    .0    .0    .0    .0
 205.  *    .2    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                     PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2B2AM.DAT)              RUN: Site 2 BUILD ALT2 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .0    .1    .0    .0    .0    .0
 250.  *    .0    .1    .1    .1    .1    .0    .0    .0
 255.  *    .0    .2    .2    .2    .1    .0    .0    .0
 260.  *    .0    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .2    .2    .2    .2    .0    .0    .0
 275.  *    .0    .2    .2    .2    .1    .0    .0    .0
 280.  *    .0    .2    .2    .2    .1    .1    .0    .0
 285.  *    .0    .2    .2    .2    .1    .1    .0    .0
 290.  *    .0    .2    .1    .1    .1    .1    .0    .0
 295.  *    .0    .1    .1    .1    .1    .1    .0    .0
 300.  *    .0    .1    .1    .1    .1    .1    .0    .0
 305.  *    .0    .1    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .2    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .1    .0    .0    .0
 340.  *    .0    .1    .1    .1    .1    .0    .0    .0
 345.  *    .0    .1    .1    .1    .1    .0    .0    .0
 350.  *    .0    .1    .1    .1    .1    .0    .0    .0
 355.  *    .0    .1    .1    .1    .1    .0    .0    .0
 360.  *    .0    .1    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .2    .2    .2    .2    .2    .1    .0    .0
 DEGR. *  100    35    65    55    45    30     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   95 DEGREES FROM REC8 .
 THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   85 DEGREES FROM REC9 .
 THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT   90 DEGREES FROM REC10.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2B2PM.DAT)               RUN: Site 2 BUILD ALT2 PM
      DATE: 03/21/2010   TIME: 22:20:39.42


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *   -172.0     469.0      78.0     601.0 *    283.     62. AG   3358.    .8    .0 68.0
       2. EB        Wil AP    *     78.0     601.0     276.0     684.0 *    215.     67. AG   3358.    .8    .0 68.0
       3. EB        Wil T+R   *    276.0     684.0     778.0     856.0 *    531.     71. AG   3074.    .8    .0 68.0
       4. EB        Wil T+R Q *    678.0     822.0   -2336.8    -217.9 *   3189.    251. AG     21. 100.0    .0 48.0 1.56 162.0
       5. EB        Wil LT    *    259.0     724.0     761.0     889.0 *    528.     72. AG    284.    .8    .0 44.0
       6. EB        Wil LT Q  *    659.0     855.0    -925.0     335.7 *   1667.    252. AG     19. 100.0    .0 24.0 ****  84.7
       7. EB        Wil DP    *    782.0     851.0    1703.0    1145.0 *    967.     72. AG   3319.    .8    .0 68.0
       8. WB        Wil AP    *   1025.0    1019.0    1677.0    1228.0 *    685.     72. AG   4364.    .8    .0 68.0
       9. WB        Wil T+R   *   1025.0    1019.0     717.0     920.0 *    324.    252. AG   4346.    .8    .0 68.0
      10. WB        Wil T+R Q *    798.0     946.0    7769.9    3177.0 *   7320.     72. AG     24. 100.0    .0 48.0 2.60 371.9
      11. WB        Wil LT    *   1040.0     975.0     742.0     883.0 *    312.    253. AG     18.    .8    .0 44.0
      12. WB        Wil LT Q  *    824.0     908.0     948.3     946.0 *    130.     73. AG     21. 100.0    .0 24.0 9.00   6.6
      13. WB        Wil DP    *    715.0     922.0     201.0     748.0 *    543.    251. AG   5006.    .8    .0 68.0
      14. WB        Wil DP    *    201.0     748.0    -199.0     546.0 *    448.    243. AG   5006.    .8    .0 68.0
      15. NB        Vet AP    *    967.0     583.0    1327.0      75.0 *    623.    145. AG   1384.    .9    .0 32.0
      16. NB        Vet T+LT  *    960.0     579.0     781.0     840.0 *    316.    326. AG   1053.    .9    .0 56.0
      17. NB        Vet T+LT Q*    820.0     783.0    1455.0    -144.1 *   1124.    146. AG     21. 100.0    .0 36.0 1.32  57.1
      18. NB        Vet RT    *    964.0     622.0     813.0     839.0 *    264.    325. AG    331.    .9    .0 32.0
      19. NB        Vet RT Q  *    847.0     791.0    1009.6     554.8 *    287.    145. AG      7. 100.0    .0 12.0 1.01  14.6
      20. NB        Vet DP    *    798.0     836.0     611.0    1170.0 *    383.    331. AG   1795.    .9    .0 44.0
      21. NB        Vet DP    *    611.0    1170.0     214.0    1729.0 *    686.    325. AG   1795.    .9    .0 44.0
      22. SB        Vet AP    *    544.0    1188.0     172.0    1701.0 *    634.    324. AG   2004.    .9    .0 44.0
      23. SB        Vet T+LT  *    550.0    1188.0     730.0     898.0 *    341.    148. AG    886.    .9    .0 56.0
      24. SB        Vet T+LT Q*    679.0     981.0      39.2    2010.9 *   1212.    328. AG     24. 100.0    .0 36.0 1.48  61.6
      25. SB        Vet RT    *    521.0    1169.0     695.0     888.0 *    331.    148. AG   1118.    .9    .0 44.0
      26. SB        Vet RT Q  *    643.0     972.0    -916.4    3485.8 *   2958.    328. AG     13. 100.0    .0 24.0 1.85 150.3
      27. SB        Vet DP    *    703.0     889.0    1292.0      46.0 *   1028.    145. AG    990.    .9    .0 44.0
1
                                                                                                                 PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2B2PM.DAT)               RUN: Site 2 BUILD ALT2 PM
      DATE: 03/21/2010   TIME: 22:20:39.42

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE    SIGNAL    ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *      150      70       2.0      3074        971       4.10      1        3
       6. EB        Wil LT Q  *      150     131       2.0       284         84       4.10      1        3
      10. WB        Wil T+R Q *      150      82       2.0      4346        981       4.10      1        3
      12. WB        Wil LT Q  *      150     143       2.0        18         84       4.10      1        3
      17. NB        Vet T+LT Q*      150      95       2.0      1053        784       4.10      1        3
      19. NB        Vet RT Q  *      150      93       2.0       331        929       4.10      1        3
      24. SB        Vet T+LT Q*      150     109       2.0       886        812       4.10      1        3
      26. SB        Vet RT Q  *      150      89       2.0      1118        797       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *      1066.0      492.0        5.0   *
      2. SE 164 S             *       942.0      686.0        5.0   *
      3. SE 82 S              *       892.0      756.0        5.0   *
      4. SE CNR               *       869.0      821.0        5.0   *
      5. SE 82 E              *       925.0      853.0        5.0   *
      6. SE 164 E             *      1005.0      880.0        5.0   *
      7. SE MID E             *      1219.0      947.0        5.0   *
      8. NE MID E             *      1144.0     1099.0        5.0   *
      9. NE 164 E             *       918.0     1026.0        5.0   *
     10. NE 82 E              *       838.0     1000.0        5.0   *
     11. NE CNR               *       759.0      983.0        5.0   *
     12. NE 82 N              *       716.0     1047.0        5.0   *
     13. NE 164 N             *       676.0     1120.0        5.0   *
     14. NE MID N             *       595.0     1269.0        5.0   *
     15. NW MID N             *       464.0     1209.0        5.0   *
     16. NW 164 N             *       546.0     1079.0        5.0   *
     17. NW 82 N              *       589.0     1010.0        5.0   *
     18. NW CNR               *       611.0      945.0        5.0   *
     19. NW 82 W              *       552.0      910.0        5.0   *
     20. NW 164 W             *       475.0      884.0        5.0   *
     21. NW MID W             *       273.0      815.0        5.0   *
     22. SW MID W             *       305.0      649.0        5.0   *
     23. SW 164 W             *       565.0      737.0        5.0   *
     24. SW 82 W              *       645.0      764.0        5.0   *
     25. SW CNR               *       718.0      779.0        5.0   *
     26. SW 82 S              *       774.0      718.0        5.0   *
     27. SW 164 S             *       824.0      646.0        5.0   *
     28. SW MID S             *       957.0      459.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2B2PM.DAT)               RUN: Site 2 BUILD ALT2 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

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                    concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*---------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  75.  *    .0    .0    .0    .0    .1    .1    .1    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  80.  *    .0    .0    .0    .0    .1    .1    .0    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .2    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 150.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 165.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 170.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 175.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 180.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 185.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 190.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 195.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 200.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 205.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .2    .0    .0    .0    .0    .1    .1    .1    .1
1
                                                                                                                             PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2B2PM.DAT)               RUN: Site 2 BUILD ALT2 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*---------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
 215.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
 220.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
 225.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
 230.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .1    .0    .0    .0    .0    .0    .1    .2    .1
 235.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .0    .1    .2    .1
 240.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .1    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 255.  *    .1    .0    .0    .0    .0    .1    .1    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 260.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 265.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
 310.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0
 315.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0
 340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 ------*---------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .1    .1    .2    .2    .2    .3    .3    .2    .2    .1    .1    .2    .2    .2    .2    .2    .1
 DEGR. *   150   155   150     0     0    35    25    70    75    75    75   205   160   305   340   340   340    95   230    65

1
                                                                                                                             PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2B2PM.DAT)               RUN: Site 2 BUILD ALT2 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .3    .3    .2    .1    .0    .0    .0
   5.  *    .0    .3    .3    .1    .1    .0    .0    .0
  10.  *    .0    .3    .3    .1    .1    .0    .0    .0
  15.  *    .0    .3    .3    .1    .1    .0    .0    .0
  20.  *    .0    .3    .3    .1    .1    .0    .0    .0
  25.  *    .0    .3    .2    .1    .1    .0    .0    .0
  30.  *    .0    .3    .2    .1    .1    .0    .0    .0
  35.  *    .0    .3    .2    .1    .0    .0    .0    .0
  40.  *    .0    .3    .2    .1    .0    .0    .0    .0
  45.  *    .0    .3    .1    .1    .0    .0    .0    .0
  50.  *    .0    .2    .1    .1    .1    .0    .0    .0
  55.  *    .0    .2    .1    .1    .1    .0    .0    .0
  60.  *    .1    .2    .1    .1    .1    .0    .0    .0
  65.  *    .1    .1    .1    .0    .1    .0    .0    .0
  70.  *    .1    .1    .0    .0    .1    .0    .0    .0
  75.  *    .1    .1    .0    .0    .0    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .2    .0    .0    .0    .0    .0    .0    .0
  90.  *    .2    .0    .0    .0    .0    .0    .0    .0
  95.  *    .2    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2B2PM.DAT)               RUN: Site 2 BUILD ALT2 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .2    .1    .2    .0    .0    .0    .0
 255.  *    .0    .2    .2    .2    .1    .0    .0    .0
 260.  *    .0    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .3    .2    .2    .2    .0    .0    .0
 275.  *    .0    .3    .2    .2    .2    .0    .0    .0
 280.  *    .0    .3    .2    .3    .3    .0    .0    .0
 285.  *    .0    .3    .3    .3    .2    .0    .0    .0
 290.  *    .0    .3    .3    .3    .2    .0    .0    .0
 295.  *    .0    .2    .3    .3    .2    .0    .0    .0
 300.  *    .0    .2    .3    .3    .2    .0    .0    .0
 305.  *    .0    .2    .3    .3    .2    .0    .0    .0
 310.  *    .0    .1    .3    .3    .2    .0    .0    .0
 315.  *    .0    .1    .3    .3    .2    .0    .0    .0
 320.  *    .0    .1    .3    .3    .2    .0    .0    .0
 325.  *    .0    .1    .3    .3    .2    .0    .0    .0
 330.  *    .0    .1    .3    .3    .2    .0    .0    .0
 335.  *    .0    .2    .3    .3    .1    .0    .0    .0
 340.  *    .0    .3    .3    .3    .1    .0    .0    .0
 345.  *    .0    .3    .3    .3    .1    .0    .0    .0
 350.  *    .0    .3    .3    .2    .1    .0    .0    .0
 355.  *    .0    .3    .3    .2    .1    .0    .0    .0
 360.  *    .0    .3    .3    .2    .1    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .2    .3    .3    .3    .3    .0    .0    .0
 DEGR. *   85     0     0   280   280     0     0     0

 THE HIGHEST CONCENTRATION IS      .30 PPM AT   75 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   75 DEGREES FROM REC10.
 THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT    0 DEGREES FROM REC22.
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2B3AM.DAT)               RUN: Site 2 BUILD ALT3 AM
      DATE: 03/21/2010   TIME: 21:46:22.13


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)      (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *   -172.0     469.0      78.0     601.0 *     283.    62. AG   5495.    .8    .0 68.0
       2. EB        Wil AP    *     78.0     601.0     276.0     684.0 *     215.    67. AG   5495.    .8    .0 68.0
       3. EB        Wil T+R   *    276.0     684.0     778.0     856.0 *     531.    71. AG   4593.    .8    .0 68.0
       4. EB        Wil T+R Q *    678.0     822.0   -5221.9   -1213.0 *    6241.   251. AG     17. 100.0    .0 48.0 2.00 317.0
       5. EB        Wil LT    *    259.0     724.0     761.0     889.0 *     528.    72. AG    902.    .8    .0 44.0
       6. EB        Wil LT Q  *    659.0     855.0   -4238.0    -750.3 *    5153.   252. AG     17. 100.0    .0 24.0 **** 261.8
       7. EB        Wil DP    *    782.0     851.0    1703.0    1145.0 *     967.    72. AG   4799.    .8    .0 68.0
       8. WB        Wil AP    *   1025.0    1019.0    1677.0    1228.0 *     685.    72. AG   3158.    .8    .0 68.0
       9. WB        Wil T+R   *   1025.0    1019.0     717.0     920.0 *     324.   252. AG   3142.    .8    .0 68.0
      10. WB        Wil T+R Q *    798.0     946.0    4693.9    2192.7 *    4091.    72. AG     24. 100.0    .0 48.0 1.85 207.8
      11. WB        Wil LT    *   1040.0     975.0     742.0     883.0 *     312.   253. AG     16.    .8    .0 44.0
      12. WB        Wil LT Q  *    824.0     908.0     933.5     941.5 *     114.    73. AG     21. 100.0    .0 24.0 8.00   5.8
      13. WB        Wil DP    *    715.0     922.0     201.0     748.0 *     543.   251. AG   3429.    .8    .0 68.0
      14. WB        Wil DP    *    201.0     748.0    -199.0     546.0 *     448.   243. AG   3429.    .8    .0 68.0
      15. NB        Vet AP    *    967.0     583.0    1327.0      75.0 *     623.   145. AG    932.    .9    .0 32.0
      16. NB        Vet T+LT  *    960.0     579.0     781.0     840.0 *     316.   326. AG    800.    .9    .0 56.0
      17. NB        Vet T+LT Q*    820.0     783.0    1191.3     241.0 *     657.   146. AG     24. 100.0    .0 36.0 1.19  33.4
      18. NB        Vet RT    *    964.0     622.0     813.0     839.0 *     264.   325. AG    132.    .9    .0 32.0
      19. NB        Vet RT Q  *    847.0     791.0     890.4     728.0 *      77.   145. AG      8. 100.0    .0 12.0  .52   3.9
      20. NB        Vet DP    *    798.0     836.0     611.0    1170.0 *     383.   331. AG   1754.    .9    .0 44.0
      21. NB        Vet DP    *    611.0    1170.0     214.0    1729.0 *     686.   325. AG   1754.    .9    .0 44.0
      22. SB        Vet AP    *    544.0    1188.0     172.0    1701.0 *     634.   324. AG   1134.    .9    .0 44.0
      23. SB        Vet T+LT  *    550.0    1188.0     730.0     898.0 *     341.   148. AG    795.    .9    .0 56.0
      24. SB        Vet T+LT Q*    679.0     981.0     -81.8    2205.7 *    1442.   328. AG     26. 100.0    .0 36.0 1.80  73.2
      25. SB        Vet RT    *    521.0    1169.0     695.0     888.0 *     331.   148. AG    339.    .9    .0 44.0
      26. SB        Vet RT Q  *    643.0     972.0     599.2    1042.7 *      83.   328. AG     13. 100.0    .0 24.0  .53   4.2
      27. SB        Vet DP    *    703.0     889.0    1292.0      46.0 *    1028.   145. AG    737.    .9    .0 44.0
1
                                                                                                                 PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2B3AM.DAT)               RUN: Site 2 BUILD ALT3 AM
      DATE: 03/21/2010   TIME: 21:46:22.13

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION  IDLE    SIGNAL  ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE  EM FAC    TYPE    RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)   (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *     150       57       2.0      4593         969       4.10      1        3
       6. EB        Wil LT Q  *     150      118       2.0       902          84       4.10      1        3
      10. WB        Wil T+R Q *     150       82       2.0      3142         995       4.10      1        3
      12. WB        Wil LT Q  *     150      143       2.0        16          84       4.10      1        3
      17. NB        Vet T+LT Q*     150      108       2.0       800         885       4.10      1        3
      19. NB        Vet RT Q  *     150      106       2.0       132         959       4.10      1        3
      24. SB        Vet T+LT Q*     150      120       2.0       795         853       4.10      1        3
      26. SB        Vet RT Q  *     150       90       2.0       339         859       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*------------------------------------*
      1. SE MID S             *      1066.0      492.0        5.0   *
      2. SE 164 S             *       942.0      686.0        5.0   *
      3. SE 82 S              *       892.0      756.0        5.0   *
      4. SE CNR               *       869.0      821.0        5.0   *
      5. SE 82 E              *       925.0      853.0        5.0   *
      6. SE 164 E             *      1005.0      880.0        5.0   *
      7. SE MID E             *      1219.0      947.0        5.0   *
      8. NE MID E             *      1144.0     1099.0        5.0   *
      9. NE 164 E             *       918.0     1026.0        5.0   *
     10. NE 82 E              *       838.0     1000.0        5.0   *
     11. NE CNR               *       759.0      983.0        5.0   *
     12. NE 82 N              *       716.0     1047.0        5.0   *
     13. NE 164 N             *       676.0     1120.0        5.0   *
     14. NE MID N             *       595.0     1269.0        5.0   *
     15. NW MID N             *       464.0     1209.0        5.0   *
     16. NW 164 N             *       546.0     1079.0        5.0   *
     17. NW 82 N              *       589.0     1010.0        5.0   *
     18. NW CNR               *       611.0      945.0        5.0   *
     19. NW 82 W              *       552.0      910.0        5.0   *
     20. NW 164 W             *       475.0      884.0        5.0   *
     21. NW MID W             *       273.0      815.0        5.0   *
     22. SW MID W             *       305.0      649.0        5.0   *
     23. SW 164 W             *       565.0      737.0        5.0   *
     24. SW 82 W              *       645.0      764.0        5.0   *
     25. SW CNR               *       718.0      779.0        5.0   *
     26. SW 82 S              *       774.0      718.0        5.0   *
     27. SW 164 S             *       824.0      646.0        5.0   *
     28. SW MID S             *       957.0      459.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2B3AM.DAT)               RUN: Site 2 BUILD ALT3 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

```
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
    0.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
    5.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   10.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   15.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   20.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
   25.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   30.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   35.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   40.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   45.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   50.  *    .0    .0    .1    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   55.  *    .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   60.  *    .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   65.  *    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1
   75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
   80.  *    .0    .0    .0    .0    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
   85.  *    .0    .0    .0    .0    .0    .1    .0    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
   90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .4    .3    .3    .0    .0    .0    .0    .0    .0    .1    .1    .1
   95.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .0    .0    .0    .1    .1    .1
  100.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .1    .0    .0    .1    .1
  105.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
  110.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
  115.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
  120.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
  125.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .1
  130.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  135.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  140.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
  145.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
  150.  *    .0    .0    .1    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
  155.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
  160.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .0    .1    .0    .0    .0    .0    .1    .2    .2
  165.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
  170.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
  175.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
  180.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .1    .2
  185.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
  190.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
  195.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
  200.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
  205.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .2    .2
1
                                                                                                                 PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2B3AM.DAT)              RUN: Site 2 BUILD ALT3 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
  210.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .2    .1
  215.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .1
  220.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  225.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  230.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  235.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  240.  *    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  245.  *    .1    .1    .1    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  250.  *    .1    .1    .1    .0    .0    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  255.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
  260.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  265.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  270.  *    .1    .1    .1    .1    .2    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  275.  *    .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  280.  *    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  285.  *    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0
  290.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0    .0    .0    .0
  295.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0    .0    .0    .0
  300.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0
  305.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
  310.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0
  315.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0
  320.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
  325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  340.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  345.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  350.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  355.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  360.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX    *    .1    .1    .1    .2    .2    .2    .2    .3    .4    .3    .3    .2    .1    .1    .1    .1    .1    .1    .2    .2
 DEGR.  *  155   155     0   280    50    50    55    95    90    85    90   285   160   305     0     0     0    90   140   115

1
                                                                                                                 PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2B3AM.DAT)              RUN: Site 2 BUILD ALT3 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .1    .0    .0    .0
   5.  *    .0    .1    .1    .1    .1    .0    .0    .0
  10.  *    .0    .1    .1    .1    .1    .0    .0    .0
  15.  *    .0    .1    .1    .1    .1    .0    .0    .0
  20.  *    .0    .1    .1    .1    .1    .0    .0    .0
  25.  *    .0    .1    .1    .1    .1    .1    .0    .0
  30.  *    .0    .1    .1    .1    .1    .1    .0    .0
  35.  *    .0    .2    .1    .1    .1    .1    .0    .0
  40.  *    .0    .2    .1    .1    .1    .1    .0    .0
  45.  *    .0    .2    .1    .1    .2    .1    .0    .0
  50.  *    .0    .2    .1    .1    .1    .1    .0    .0
  55.  *    .0    .2    .1    .2    .1    .1    .0    .0
  60.  *    .0    .1    .1    .2    .1    .1    .0    .0
  65.  *    .1    .1    .2    .2    .1    .0    .0    .0
  70.  *    .1    .1    .2    .2    .1    .0    .0    .0
  75.  *    .1    .1    .1    .1    .1    .0    .0    .0
  80.  *    .1    .1    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .1    .0    .0    .0    .0    .0    .0    .0
 100.  *    .2    .0    .0    .0    .0    .0    .0    .0
 105.  *    .2    .0    .0    .0    .0    .0    .0    .0
 110.  *    .2    .0    .0    .0    .0    .0    .0    .0
 115.  *    .2    .0    .0    .0    .0    .0    .0    .0
 120.  *    .2    .0    .0    .0    .0    .0    .0    .0
 125.  *    .2    .0    .0    .0    .0    .0    .0    .0
 130.  *    .2    .0    .0    .0    .0    .0    .0    .0
 135.  *    .2    .0    .0    .0    .0    .0    .0    .0
 140.  *    .2    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .2    .0    .0    .0    .0    .0    .0    .0
 205.  *    .2    .0    .0    .0    .0    .0    .0    .0
1                                                                                                                 PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2B3AM.DAT)              RUN: Site 2 BUILD ALT3 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .0    .1    .0    .0    .0    .0
 250.  *    .0    .1    .1    .1    .1    .0    .0    .0
 255.  *    .0    .2    .2    .2    .1    .0    .0    .0
 260.  *    .0    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .2    .2    .2    .2    .0    .0    .0
 275.  *    .0    .2    .2    .2    .1    .0    .0    .0
 280.  *    .0    .2    .2    .2    .1    .1    .0    .0
 285.  *    .0    .2    .2    .2    .1    .1    .0    .0
 290.  *    .0    .2    .1    .1    .1    .1    .0    .0
 295.  *    .0    .1    .1    .1    .1    .1    .0    .0
 300.  *    .0    .1    .1    .1    .1    .1    .0    .0
 305.  *    .0    .1    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .2    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .1    .0    .0    .0
 340.  *    .0    .1    .1    .1    .1    .0    .0    .0
 345.  *    .0    .1    .1    .1    .1    .0    .0    .0
 350.  *    .0    .1    .1    .1    .1    .0    .0    .0
 355.  *    .0    .1    .1    .1    .1    .0    .0    .0
 360.  *    .0    .1    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .2    .2    .2    .2    .2    .1    .0    .0
 DEGR. *  100    35    65    55    45    25     0     0

 THE HIGHEST CONCENTRATION IS     .40 PPM AT   90 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   95 DEGREES FROM REC8 .
 THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT   85 DEGREES FROM REC10.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT)               RUN: Site 2 BUILD ALT3 PM
      DATE: 03/21/2010   TIME: 22:20:55.63


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *   -172.0     469.0      78.0     601.0 *     283.    62. AG   3401.    .8    .0 68.0
       2. EB        Wil AP    *     78.0     601.0     276.0     684.0 *     215.    67. AG   3401.    .8    .0 68.0
       3. EB        Wil T+R   *    276.0     684.0     778.0     856.0 *     531.    71. AG   3112.    .8    .0 68.0
       4. EB        Wil T+R Q *    678.0     822.0   -2266.6    -193.6 *    3115.   251. AG     20. 100.0    .0 48.0 1.53 158.2
       5. EB        Wil LT    *    259.0     724.0     761.0     889.0 *     528.    72. AG    289.    .8    .0 44.0
       6. EB        Wil LT Q  *    659.0     855.0    -901.6     343.4 *    1642.   252. AG     19. 100.0    .0 24.0 ****  83.4
       7. EB        Wil DP    *    782.0     851.0    1703.0    1145.0 *     967.    72. AG   3325.    .8    .0 68.0
       8. WB        Wil AP    *   1025.0    1019.0    1677.0    1228.0 *     685.    72. AG   4274.    .8    .0 68.0
       9. WB        Wil T+R   *   1025.0    1019.0     717.0     920.0 *     324.   252. AG   4256.    .8    .0 68.0
      10. WB        Wil T+R Q *    798.0     946.0    7612.8    3126.7 *    7155.    72. AG     24. 100.0    .0 48.0 2.58 363.5
      11. WB        Wil LT    *   1040.0     975.0     742.0     883.0 *     312.   253. AG     18.    .8    .0 44.0
      12. WB        Wil LT Q  *    824.0     908.0     948.3     946.0 *     130.    73. AG     21. 100.0    .0 24.0 9.00   6.6
      13. WB        Wil DP    *    715.0     922.0     201.0     748.0 *     543.   251. AG   4918.    .8    .0 68.0
      14. WB        Wil DP    *    201.0     748.0    -199.0     546.0 *     448.   243. AG   4918.    .8    .0 68.0
      15. NB        Vet AP    *    967.0     583.0    1327.0      75.0 *     623.   145. AG   1362.    .9    .0 32.0
      16. NB        Vet T+LT  *    960.0     579.0     781.0     840.0 *     316.   326. AG   1091.    .9    .0 56.0
      17. NB        Vet T+LT Q*    820.0     783.0    1697.9    -498.6 *    1553.   146. AG     22. 100.0    .0 36.0 1.53  78.9
      18. NB        Vet RT    *    964.0     622.0     813.0     839.0 *     264.   325. AG    271.    .9    .0 32.0
      19. NB        Vet RT Q  *    847.0     791.0     938.2     658.5 *     161.   145. AG      7. 100.0    .0 12.0  .85   8.2
      20. NB        Vet DP    *    798.0     836.0     611.0    1170.0 *     383.   331. AG   1792.    .9    .0 44.0
      21. NB        Vet DP    *    611.0    1170.0     214.0    1729.0 *     686.   325. AG   1792.    .9    .0 44.0
      22. SB        Vet AP    *    544.0    1188.0     172.0    1701.0 *     634.   324. AG   1983.    .9    .0 44.0
      23. SB        Vet T+LT  *    550.0    1188.0     730.0     898.0 *     341.   148. AG    912.    .9    .0 56.0
      24. SB        Vet T+LT Q*    679.0     981.0     -28.0    2119.1 *    1340.   328. AG     24. 100.0    .0 36.0 1.54  68.1
      25. SB        Vet RT    *    521.0    1169.0     695.0     888.0 *     331.   148. AG   1074.    .9    .0 44.0
      26. SB        Vet RT Q  *    643.0     972.0    -749.2    3216.4 *    2641.   328. AG     13. 100.0    .0 24.0 1.73 134.2
      27. SB        Vet DP    *    703.0     889.0    1292.0      46.0 *    1028.   145. AG    985.    .9    .0 44.0
1
                                                                                                                 PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT)               RUN: Site 2 BUILD ALT3 PM
      DATE: 03/21/2010   TIME: 22:20:55.63

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL    ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE      RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *     150        68      2.0      3112         977      4.10      1        3
       6. EB        Wil LT Q  *     150       127      2.0       289          84      4.10      1        3
      10. WB        Wil T+R Q *     150        83      2.0      4256         982      4.10      1        3
      12. WB        Wil LT Q  *     150       143      2.0        18          84      4.10      1        3
      17. NB        Vet T+LT Q*     150       100      2.0      1091         776      4.10      1        3
      19. NB        Vet RT Q  *     150        95      2.0       271         933      4.10      1        3
      24. SB        Vet T+LT Q*     150       109      2.0       912         800      4.10      1        3
      26. SB        Vet RT Q  *     150        88      2.0      1074         804      4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *      1066.0      492.0        5.0   *
      2. SE 164 S             *       942.0      686.0        5.0   *
      3. SE 82 S              *       892.0      756.0        5.0   *
      4. SE CNR               *       869.0      821.0        5.0   *
      5. SE 82 E              *       925.0      853.0        5.0   *
      6. SE 164 E             *      1005.0      880.0        5.0   *
      7. SE MID E             *      1219.0      947.0        5.0   *
      8. NE MID E             *      1144.0     1099.0        5.0   *
      9. NE 164 E             *       918.0     1026.0        5.0   *
     10. NE 82 E              *       838.0     1000.0        5.0   *
     11. NE CNR               *       759.0      983.0        5.0   *
     12. NE 82 N              *       716.0     1047.0        5.0   *
     13. NE 164 N             *       676.0     1120.0        5.0   *
     14. NE MID N             *       595.0     1269.0        5.0   *
     15. NW MID N             *       464.0     1209.0        5.0   *
     16. NW 164 N             *       546.0     1079.0        5.0   *
     17. NW 82 N              *       589.0     1010.0        5.0   *
     18. NW CNR               *       611.0      945.0        5.0   *
     19. NW 82 W              *       552.0      910.0        5.0   *
     20. NW 164 W             *       475.0      884.0        5.0   *
     21. NW MID W             *       273.0      815.0        5.0   *
     22. SW MID W             *       305.0      649.0        5.0   *
     23. SW 164 W             *       565.0      737.0        5.0   *
     24. SW 82 W              *       645.0      764.0        5.0   *
     25. SW CNR               *       718.0      779.0        5.0   *
     26. SW 82 S              *       774.0      718.0        5.0   *
     27. SW 164 S             *       824.0      646.0        5.0   *
     28. SW MID S             *       957.0      459.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT)               RUN: Site 2 BUILD ALT3 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

```
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  75.  *    .0    .0    .0    .0    .1    .1    .1    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  80.  *    .0    .0    .0    .0    .1    .1    .0    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .2    .1    .1
  85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .2    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 165.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 170.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 175.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 180.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 185.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 190.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 195.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 200.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 205.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
1
                                                                                                                PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT)               RUN: Site 2 BUILD ALT3 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
 215.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
 220.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
 225.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
 230.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1
 235.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .0    .1    .2    .1
 240.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .1    .0    .0    .0    .0    .0    .1    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 255.  *    .1    .0    .0    .0    .0    .1    .1    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 260.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 265.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .1    .1    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .1    .1    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .1    .1    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
 310.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0
 315.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .1    .1    .2    .2    .2    .3    .3    .2    .2    .1    .1    .1    .2    .2    .2    .2    .1
 DEGR. *  145   150   150     0     0    40    30    70    75    75    75   300   160   305     0   340   340    80   235    65

1
                                                                                                                PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT)               RUN: Site 2 BUILD ALT3 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .3    .2    .2    .1    .0    .0    .0
   5.  *    .0    .3    .2    .1    .1    .0    .0    .0
  10.  *    .0    .3    .3    .1    .1    .0    .0    .0
  15.  *    .0    .3    .3    .1    .1    .0    .0    .0
  20.  *    .0    .3    .2    .1    .1    .0    .0    .0
  25.  *    .0    .3    .2    .1    .1    .0    .0    .0
  30.  *    .0    .3    .2    .1    .1    .0    .0    .0
  35.  *    .0    .3    .2    .1    .0    .0    .0    .0
  40.  *    .0    .3    .2    .1    .0    .0    .0    .0
  45.  *    .0    .3    .1    .1    .0    .0    .0    .0
  50.  *    .0    .2    .1    .1    .1    .0    .0    .0
  55.  *    .0    .2    .1    .1    .1    .0    .0    .0
  60.  *    .1    .2    .1    .1    .1    .0    .0    .0
  65.  *    .1    .1    .1    .0    .1    .0    .0    .0
  70.  *    .1    .1    .0    .0    .1    .0    .0    .0
  75.  *    .1    .1    .0    .0    .0    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .2    .0    .0    .0    .0    .0    .0    .0
  90.  *    .2    .0    .0    .0    .0    .0    .0    .0
  95.  *    .2    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                            PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2B3PM.DAT)               RUN: Site 2 BUILD ALT3 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .1    .2    .1    .2    .0    .0    .0    .0
 255.  *    .0    .2    .2    .2    .2    .0    .0    .0
 260.  *    .0    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .3    .2    .2    .2    .0    .0    .0
 275.  *    .0    .3    .2    .2    .2    .0    .0    .0
 280.  *    .0    .3    .2    .3    .3    .0    .0    .0
 285.  *    .0    .3    .3    .3    .2    .0    .0    .0
 290.  *    .0    .2    .3    .3    .2    .0    .0    .0
 295.  *    .0    .2    .3    .3    .2    .0    .0    .0
 300.  *    .0    .2    .3    .3    .2    .0    .0    .0
 305.  *    .0    .2    .3    .3    .2    .0    .0    .0
 310.  *    .0    .1    .3    .3    .2    .0    .0    .0
 315.  *    .0    .1    .3    .2    .2    .0    .0    .0
 320.  *    .0    .1    .2    .2    .2    .0    .0    .0
 325.  *    .0    .1    .2    .2    .1    .0    .0    .0
 330.  *    .0    .1    .2    .2    .1    .0    .0    .0
 335.  *    .0    .2    .2    .2    .1    .0    .0    .0
 340.  *    .0    .3    .2    .2    .1    .0    .0    .0
 345.  *    .0    .3    .2    .2    .1    .0    .0    .0
 350.  *    .0    .3    .2    .2    .1    .0    .0    .0
 355.  *    .0    .3    .2    .2    .1    .0    .0    .0
 360.  *    .0    .3    .2    .2    .1    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .2    .3    .3    .3    .3    .0    .0    .0
 DEGR. *   85     0    10   280   280     0     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   75 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   75 DEGREES FROM REC10.
 THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT    0 DEGREES FROM REC22.
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1                          CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2B4AM.DAT)              RUN: Site 2 BUILD ALT4 AM
      DATE: 03/21/2010   TIME: 21:46:42.68


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*-------------------------------------------------------------
       1. EB        Wil AP    *  -172.0     469.0      78.0     601.0 *    283.    62. AG  5553.    .8    .0 68.0
       2. EB        Wil AP    *    78.0     601.0     276.0     684.0 *    215.    67. AG  5553.    .8    .0 68.0
       3. EB        Wil T+R   *   276.0     684.0     778.0     856.0 *    531.    71. AG  4635.    .8    .0 68.0
       4. EB        Wil T+R Q *   678.0     822.0   -5319.8   -1246.8 *   6345.   251. AG    17. 100.0    .0 48.0 2.02 322.3
       5. EB        Wil LT    *   259.0     724.0     761.0     889.0 *    528.    72. AG   918.    .8    .0 44.0
       6. EB        Wil LT Q  *   659.0     855.0   -4327.3    -779.6 *   5247.   252. AG    17. 100.0    .0 24.0 **** 266.6
       7. EB        Wil DP    *   782.0     851.0    1703.0    1145.0 *    967.    72. AG  4832.    .8    .0 68.0
       8. WB        Wil AP    *  1025.0    1019.0    1677.0    1228.0 *    685.    72. AG  3177.    .8    .0 68.0
       9. WB        Wil T+R   *  1025.0    1019.0     717.0     920.0 *    324.   252. AG  3161.    .8    .0 68.0
      10. WB        Wil T+R Q *   798.0     946.0    4744.1    2208.7 *   4143.    72. AG    24. 100.0    .0 48.0 1.86 210.5
      11. WB        Wil LT    *  1040.0     975.0     742.0     883.0 *    312.   253. AG    16.    .8    .0 44.0
      12. WB        Wil LT Q  *   824.0     908.0     933.5     941.5 *    114.    73. AG    21. 100.0    .0 24.0 8.00   5.8
      13. WB        Wil DP    *   715.0     922.0     201.0     748.0 *    543.   251. AG  3438.    .8    .0 68.0
      14. WB        Wil DP    *   201.0     748.0    -199.0     546.0 *    448.   243. AG  3438.    .8    .0 68.0
      15. NB        Vet AP    *   967.0     583.0    1327.0      75.0 *    623.   145. AG   949.    .9    .0 32.0
      16. NB        Vet T+LT  *   960.0     579.0     781.0     840.0 *    316.   326. AG   817.    .9    .0 56.0
      17. NB        Vet T+LT Q*   820.0     783.0    1366.7     -15.1 *    967.   146. AG    24. 100.0    .0 36.0 1.36  49.1
      18. NB        Vet RT    *   964.0     622.0     813.0     839.0 *    264.   325. AG   132.    .9    .0 32.0
      19. NB        Vet RT Q  *   847.0     791.0     890.4     728.0 *     77.   145. AG     8. 100.0    .0 12.0  .52   3.9
      20. NB        Vet DP    *   798.0     836.0     611.0    1170.0 *    383.   331. AG  1787.    .9    .0 44.0
      21. NB        Vet DP    *   611.0    1170.0     214.0    1729.0 *    686.   325. AG  1787.    .9    .0 44.0
      22. SB        Vet AP    *   544.0    1188.0     172.0    1701.0 *    634.   324. AG  1182.    .9    .0 44.0
      23. SB        Vet T+LT  *   550.0    1188.0     730.0     898.0 *    341.   148. AG   853.    .9    .0 56.0
      24. SB        Vet T+LT Q*   679.0     981.0    -207.3    2407.7 *   1680.   328. AG    26. 100.0    .0 36.0 1.97  85.3
      25. SB        Vet RT    *   521.0    1169.0     695.0     888.0 *    331.   148. AG   329.    .9    .0 44.0
      26. SB        Vet RT Q  *   643.0     972.0     600.5    1040.6 *     81.   328. AG    13. 100.0    .0 24.0  .53   4.1
      27. SB        Vet DP    *   703.0     889.0    1292.0      46.0 *   1028.   145. AG   807.    .9    .0 44.0
1
                                                                                                                         PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2B4AM.DAT)              RUN: Site 2 BUILD ALT4 AM
      DATE: 03/21/2010   TIME: 21:46:42.68

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *     150       57       2.0      4635        968       4.10      1        3
       6. EB        Wil LT Q  *     150      118       2.0       918         84       4.10      1        3
      10. WB        Wil T+R Q *     150       82       2.0      3161        994       4.10      1        3
      12. WB        Wil LT Q  *     150      143       2.0        16         84       4.10      1        3
      17. NB        Vet T+LT Q*     150      111       2.0       817        859       4.10      1        3
      19. NB        Vet RT Q  *     150      106       2.0       132        955       4.10      1        3
      24. SB        Vet T+LT Q*     150      120       2.0       853        834       4.10      1        3
      26. SB        Vet RT Q  *     150       90       2.0       329        834       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*------------------------------------*
       1. SE MID S            *      1066.0      492.0       5.0   *
       2. SE 164 S            *       942.0      686.0       5.0   *
       3. SE 82 S             *       892.0      756.0       5.0   *
       4. SE CNR              *       869.0      821.0       5.0   *
       5. SE 82 E             *       925.0      853.0       5.0   *
       6. SE 164 E            *      1005.0      880.0       5.0   *
       7. SE MID E            *      1219.0      947.0       5.0   *
       8. NE MID E            *      1144.0     1099.0       5.0   *
       9. NE 164 E            *       918.0     1026.0       5.0   *
      10. NE 82 E             *       838.0     1000.0       5.0   *
      11. NE CNR              *       759.0      983.0       5.0   *
      12. NE 82 N             *       716.0     1047.0       5.0   *
      13. NE 164 N            *       676.0     1120.0       5.0   *
      14. NE MID N            *       595.0     1269.0       5.0   *
      15. NW MID N            *       464.0     1209.0       5.0   *
      16. NW 164 N            *       546.0     1079.0       5.0   *
      17. NW 82 N             *       589.0     1010.0       5.0   *
      18. NW CNR              *       611.0      945.0       5.0   *
      19. NW 82 W             *       552.0      910.0       5.0   *
      20. NW 164 W            *       475.0      884.0       5.0   *
      21. NW MID W            *       273.0      815.0       5.0   *
      22. SW MID W            *       305.0      649.0       5.0   *
      23. SW 164 W            *       565.0      737.0       5.0   *
      24. SW 82 W             *       645.0      764.0       5.0   *
      25. SW CNR              *       718.0      779.0       5.0   *
      26. SW 82 S             *       774.0      718.0       5.0   *
      27. SW 164 S            *       824.0      646.0       5.0   *
      28. SW MID S            *       957.0      459.0       5.0   *
1
                                                                                                                         PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2B4AM.DAT)              RUN: Site 2 BUILD ALT4 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

```
          concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   5.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  10.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  15.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  20.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
  25.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .1    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1
  75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  80.  *    .0    .0    .0    .0    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  85.  *    .0    .0    .0    .0    .0    .1    .0    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .4    .3    .3    .0    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .0    .0    .0    .1    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .1    .0    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
 120.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
 125.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
 130.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .2
 135.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .2    .2
 140.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 145.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 150.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 155.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 160.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 165.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 170.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 175.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 180.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 185.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 190.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 195.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
 200.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
 205.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .2    .2
1
                                                                                                                     PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2B4AM.DAT)               RUN: Site 2 BUILD ALT4 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .2    .1
 215.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .1
 220.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 225.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 230.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 235.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 240.  *    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .1    .1    .1    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .1    .1    .1    .0    .0    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 255.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 260.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .1    .1    .1    .1    .2    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0    .0    .0    .0
 295.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0
 300.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0
 305.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .2    .0    .0    .0    .0    .0    .0
 310.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
 315.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0
 320.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 340.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 345.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 350.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 355.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 360.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .2    .2    .2    .2    .3    .4    .3    .3    .2    .1    .2    .1    .1    .1    .1    .2    .2
 DEGR. *   150   150     0   280    50    50    55    95    90    85    90   285   160   305     0     0     0    90   135   115

1
                                                                                                                     PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2B4AM.DAT)               RUN: Site 2 BUILD ALT4 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .1    .0    .0    .0
   5.  *    .0    .1    .1    .1    .1    .0    .0    .0
  10.  *    .0    .1    .1    .1    .1    .0    .0    .0
  15.  *    .0    .1    .1    .1    .1    .0    .0    .0
  20.  *    .0    .1    .1    .1    .1    .0    .0    .0
  25.  *    .0    .1    .1    .1    .1    .1    .0    .0
  30.  *    .0    .1    .1    .1    .1    .1    .0    .0
  35.  *    .0    .2    .1    .1    .1    .1    .0    .0
  40.  *    .0    .2    .1    .1    .2    .1    .0    .0
  45.  *    .0    .2    .1    .1    .2    .1    .0    .0
  50.  *    .0    .2    .1    .1    .1    .1    .0    .0
  55.  *    .0    .2    .1    .2    .1    .1    .0    .0
  60.  *    .0    .1    .1    .2    .1    .1    .0    .0
  65.  *    .1    .1    .2    .2    .1    .0    .0    .0
  70.  *    .1    .1    .2    .2    .1    .0    .0    .0
  75.  *    .1    .1    .1    .1    .1    .0    .0    .0
  80.  *    .1    .1    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .2    .0    .0    .0    .0    .0    .0    .0
 100.  *    .2    .0    .0    .0    .0    .0    .0    .0
 105.  *    .2    .0    .0    .0    .0    .0    .0    .0
 110.  *    .2    .0    .0    .0    .0    .0    .0    .0
 115.  *    .2    .0    .0    .0    .0    .0    .0    .0
 120.  *    .2    .0    .0    .0    .0    .0    .0    .0
 125.  *    .2    .0    .0    .0    .0    .0    .0    .0
 130.  *    .2    .0    .0    .0    .0    .0    .0    .0
 135.  *    .2    .0    .0    .0    .0    .0    .0    .0
 140.  *    .2    .0    .0    .0    .0    .0    .0    .0
 145.  *    .2    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .2    .0    .0    .0    .0    .0    .0    .0
 205.  *    .2    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2B4AM.DAT)               RUN: Site 2 BUILD ALT4 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .0    .1    .0    .0    .0    .0
 250.  *    .0    .1    .1    .1    .1    .0    .0    .0
 255.  *    .0    .2    .2    .2    .1    .0    .0    .0
 260.  *    .0    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .2    .2    .2    .2    .0    .0    .0
 275.  *    .0    .2    .2    .2    .1    .0    .0    .0
 280.  *    .0    .2    .2    .2    .1    .1    .0    .0
 285.  *    .0    .2    .2    .2    .1    .1    .0    .0
 290.  *    .0    .2    .1    .1    .1    .1    .0    .0
 295.  *    .0    .1    .1    .1    .1    .1    .0    .0
 300.  *    .0    .1    .1    .1    .1    .1    .0    .0
 305.  *    .0    .1    .1    .1    .1    .1    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .2    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .1    .0    .0    .0
 340.  *    .0    .1    .1    .1    .1    .0    .0    .0
 345.  *    .0    .1    .1    .1    .1    .0    .0    .0
 350.  *    .0    .1    .1    .1    .1    .0    .0    .0
 355.  *    .0    .1    .1    .1    .1    .0    .0    .0
 360.  *    .0    .1    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .2    .2    .2    .2    .2    .1    .0    .0
 DEGR. *   95    35    65    55    40    25     0     0

 THE HIGHEST CONCENTRATION IS      .40 PPM AT   90 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   95 DEGREES FROM REC8 .
 THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT   85 DEGREES FROM REC10.
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                   PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2B4PM.DAT)              RUN: Site 2 BUILD ALT4 PM
      DATE: 03/21/2010   TIME: 22:21:18.75


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *   -172.0     469.0      78.0     601.0 *     283.    62. AG   3310.    .8    .0 68.0
       2. EB        Wil AP    *     78.0     601.0     276.0     684.0 *     215.    67. AG   3310.    .8    .0 68.0
       3. EB        Wil T+R   *    276.0     684.0     778.0     856.0 *     531.    71. AG   3031.    .8    .0 68.0
       4. EB        Wil T+R Q *    678.0     822.0   -2106.8    -138.5 *    2946.   251. AG     20. 100.0    .0 48.0 1.50 149.6
       5. EB        Wil LT    *    259.0     724.0     761.0     889.0 *     528.    72. AG    279.    .8    .0 44.0
       6. EB        Wil LT Q  *    659.0     855.0    -824.5     368.7 *    1561.   252. AG     18. 100.0    .0 24.0 ****  79.3
       7. EB        Wil DP    *    782.0     851.0    1703.0    1145.0 *     967.    72. AG   3239.    .8    .0 68.0
       8. WB        Wil AP    *   1025.0    1019.0    1677.0    1228.0 *     685.    72. AG   4265.    .8    .0 68.0
       9. WB        Wil T+R   *   1025.0    1019.0     717.0     920.0 *     324.   252. AG   4246.    .8    .0 68.0
      10. WB        Wil T+R Q *    798.0     946.0    7709.8    3157.8 *    7257.    72. AG     25. 100.0    .0 48.0 2.65 368.7
      11. WB        Wil LT    *   1040.0     975.0     742.0     883.0 *     312.   253. AG     19.    .8    .0 44.0
      12. WB        Wil LT Q  *    824.0     908.0     948.3     946.0 *     130.    73. AG     21. 100.0    .0 24.0 9.00   6.6
      13. WB        Wil DP    *    715.0     922.0     201.0     748.0 *     543.   251. AG   5001.    .8    .0 68.0
      14. WB        Wil DP    *    201.0     748.0    -199.0     546.0 *     448.   243. AG   5001.    .8    .0 68.0
      15. NB        Vet AP    *    967.0     583.0    1327.0      75.0 *     623.   145. AG   1387.    .9    .0 32.0
      16. NB        Vet T+LT  *    960.0     579.0     781.0     840.0 *     316.   326. AG   1067.    .9    .0 56.0
      17. NB        Vet T+LT Q*    820.0     783.0    1638.1    -411.3 *    1448.   146. AG     22. 100.0    .0 36.0 1.49  73.5
      18. NB        Vet RT    *    964.0     622.0     813.0     839.0 *     264.   325. AG    320.    .9    .0 32.0
      19. NB        Vet RT Q  *    847.0     791.0    1018.9     541.3 *     303.   145. AG      7. 100.0    .0 12.0 1.02  15.4
      20. NB        Vet DP    *    798.0     836.0     611.0    1170.0 *     383.   331. AG   1703.    .9    .0 44.0
      21. NB        Vet DP    *    611.0    1170.0     214.0    1729.0 *     686.   325. AG   1703.    .9    .0 44.0
      22. SB        Vet AP    *    544.0    1188.0     172.0    1701.0 *     634.   324. AG   1982.    .9    .0 44.0
      23. SB        Vet T+LT  *    550.0    1188.0     730.0     898.0 *     341.   148. AG    871.    .9    .0 56.0
      24. SB        Vet T+LT Q*    679.0     981.0       2.0    2070.8 *    1283.   328. AG     24. 100.0    .0 36.0 1.54  65.2
      25. SB        Vet RT    *    521.0    1169.0     695.0     888.0 *     331.   148. AG   1111.    .9    .0 44.0
      26. SB        Vet RT Q  *    643.0     972.0    -816.3    3324.5 *    2768.   328. AG     13. 100.0    .0 24.0 1.76 140.6
      27. SB        Vet DP    *    703.0     889.0    1292.0      46.0 *    1028.   145. AG    999.    .9    .0 44.0
1
                                                                                                                 PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2B4PM.DAT)              RUN: Site 2 BUILD ALT4 PM
      DATE: 03/21/2010   TIME: 22:21:18.75

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *     150       68       2.0      3031        969       4.10      1        3
       6. EB        Wil LT Q  *     150      126       2.0       279         84       4.10      1        3
      10. WB        Wil T+R Q *     150       85       2.0      4246        984       4.10      1        3
      12. WB        Wil LT Q  *     150      143       2.0        19         84       4.10      1        3
      17. NB        Vet T+LT Q*     150      100       2.0      1067        782       4.10      1        3
      19. NB        Vet RT Q  *     150       95       2.0       320        928       4.10      1        3
      24. SB        Vet T+LT Q*     150      111       2.0       871        806       4.10      1        3
      26. SB        Vet RT Q  *     150       87       2.0      1111        804       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)         *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*-------------------------------------*
      1. SE MID S             *      1066.0      492.0        5.0   *
      2. SE 164 S             *       942.0      686.0        5.0   *
      3. SE 82 S              *       892.0      756.0        5.0   *
      4. SE CNR               *       869.0      821.0        5.0   *
      5. SE 82 E              *       925.0      853.0        5.0   *
      6. SE 164 E             *      1005.0      880.0        5.0   *
      7. SE MID E             *      1219.0      947.0        5.0   *
      8. NE MID E             *      1144.0     1099.0        5.0   *
      9. NE 164 E             *       918.0     1026.0        5.0   *
     10. NE 82 E              *       838.0     1000.0        5.0   *
     11. NE CNR               *       759.0      983.0        5.0   *
     12. NE 82 N              *       716.0     1047.0        5.0   *
     13. NE 164 N             *       676.0     1120.0        5.0   *
     14. NE MID N             *       595.0     1269.0        5.0   *
     15. NW MID N             *       464.0     1209.0        5.0   *
     16. NW 164 N             *       546.0     1079.0        5.0   *
     17. NW 82 N              *       589.0     1010.0        5.0   *
     18. NW CNR               *       611.0      945.0        5.0   *
     19. NW 82 W              *       552.0      910.0        5.0   *
     20. NW 164 W             *       475.0      884.0        5.0   *
     21. NW MID W             *       273.0      815.0        5.0   *
     22. SW MID W             *       305.0      649.0        5.0   *
     23. SW 164 W             *       565.0      737.0        5.0   *
     24. SW 82 W              *       645.0      764.0        5.0   *
     25. SW CNR               *       718.0      779.0        5.0   *
     26. SW 82 S              *       774.0      718.0        5.0   *
     27. SW 164 S             *       824.0      646.0        5.0   *
     28. SW MID S             *       957.0      459.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2B4PM.DAT)              RUN: Site 2 BUILD ALT4 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

```
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
  15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  75.  *    .0    .0    .0    .0    .1    .1    .1    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  80.  *    .0    .0    .0    .0    .0    .1    .0    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .2    .1    .1
  85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .2    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 150.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .1    .0    .0    .0    .1    .1    .1    .1
 165.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 170.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 175.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 180.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 185.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 190.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 195.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 200.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 205.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
1
                                                                                                                PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2B4PM.DAT)               RUN: Site 2 BUILD ALT4 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
 215.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
 220.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
 225.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
 230.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .1    .0    .0    .0    .0    .0    .1    .2    .1
 235.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .0    .1    .2    .1
 240.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .1    .0    .0    .0    .0    .0    .1    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 255.  *    .1    .0    .0    .0    .0    .1    .1    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 260.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 265.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .1    .1    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .1    .1    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .1    .1    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0
 310.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0
 315.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0
 340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .1    .1    .2    .2    .2    .3    .3    .2    .2    .1    .0    .1    .2    .2    .2    .2    .1
 DEGR. *  150   150   150     0     0    40    35    65    75    75    75   295   160     0     0   340   340    80   230    65

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                                                                                                                PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2B4PM.DAT)               RUN: Site 2 BUILD ALT4 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .3    .2    .2    .1    .0    .0    .0
   5.  *    .0    .3    .2    .1    .1    .0    .0    .0
  10.  *    .0    .3    .3    .1    .1    .0    .0    .0
  15.  *    .0    .3    .3    .1    .1    .0    .0    .0
  20.  *    .0    .3    .2    .1    .1    .0    .0    .0
  25.  *    .0    .3    .2    .1    .1    .0    .0    .0
  30.  *    .0    .3    .2    .1    .0    .0    .0    .0
  35.  *    .0    .3    .2    .1    .0    .0    .0    .0
  40.  *    .0    .3    .2    .1    .0    .0    .0    .0
  45.  *    .0    .3    .1    .1    .0    .0    .0    .0
  50.  *    .0    .2    .1    .1    .1    .0    .0    .0
  55.  *    .0    .2    .1    .1    .1    .0    .0    .0
  60.  *    .1    .2    .1    .1    .1    .0    .0    .0
  65.  *    .1    .1    .1    .0    .1    .0    .0    .0
  70.  *    .1    .1    .0    .0    .1    .0    .0    .0
  75.  *    .1    .1    .0    .0    .0    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .2    .0    .0    .0    .0    .0    .0    .0
  90.  *    .2    .0    .0    .0    .0    .0    .0    .0
  95.  *    .2    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                                PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2B4PM.DAT)              RUN: Site 2 BUILD ALT4 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .2    .1    .2    .0    .0    .0    .0
 255.  *    .0    .2    .2    .2    .1    .0    .0    .0
 260.  *    .0    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .3    .2    .2    .2    .0    .0    .0
 275.  *    .0    .3    .2    .2    .2    .0    .0    .0
 280.  *    .0    .3    .2    .3    .3    .0    .0    .0
 285.  *    .0    .3    .3    .3    .2    .0    .0    .0
 290.  *    .0    .3    .3    .3    .2    .0    .0    .0
 295.  *    .0    .2    .3    .3    .2    .0    .0    .0
 300.  *    .0    .2    .3    .3    .2    .0    .0    .0
 305.  *    .0    .2    .3    .3    .2    .0    .0    .0
 310.  *    .0    .1    .3    .3    .2    .0    .0    .0
 315.  *    .0    .1    .3    .2    .2    .0    .0    .0
 320.  *    .0    .1    .2    .2    .2    .0    .0    .0
 325.  *    .0    .1    .2    .2    .2    .0    .0    .0
 330.  *    .0    .1    .2    .2    .2    .0    .0    .0
 335.  *    .0    .2    .2    .2    .1    .0    .0    .0
 340.  *    .0    .3    .2    .2    .1    .0    .0    .0
 345.  *    .0    .3    .2    .2    .1    .0    .0    .0
 350.  *    .0    .3    .2    .2    .1    .0    .0    .0
 355.  *    .0    .3    .2    .2    .1    .0    .0    .0
 360.  *    .0    .3    .2    .2    .1    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .2    .3    .3    .3    .3    .0    .0    .0
 DEGR. *   85     0    10   280   280     0     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   75 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   75 DEGREES FROM REC10.
 THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT    0 DEGREES FROM REC22.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2B5AM.DAT)              RUN: Site 2 BUILD ALT5 AM
      DATE: 03/21/2010   TIME: 21:57:39.04


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1       Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*---------------------------------------*--------------------------------------------------------------
        1. EB        Wil AP   *  -172.0     469.0      78.0     601.0 *     283.    62. AG  5547.    .8    .0 68.0
        2. EB        Wil AP   *    78.0     601.0     276.0     684.0 *     215.    67. AG  5547.    .8    .0 68.0
        3. EB        Wil T+R  *   276.0     684.0     778.0     856.0 *     531.    71. AG  4619.    .8    .0 68.0
        4. EB        Wil T+R Q *   678.0     822.0   -5290.1   -1236.5 *    6313.   251. AG    17. 100.0    .0 48.0 2.01 320.7
        5. EB        Wil LT   *   259.0     724.0     761.0     889.0 *     528.    72. AG   928.    .8    .0 44.0
        6. EB        Wil LT Q *   659.0     855.0   -4383.2    -797.9 *    5306.   252. AG    17. 100.0    .0 24.0 **** 269.6
        7. EB        Wil DP   *   782.0     851.0    1703.0    1145.0 *     967.    72. AG  4794.    .8    .0 68.0
        8. WB        Wil AP   *  1025.0    1019.0    1677.0    1228.0 *     685.    72. AG  3154.    .8    .0 68.0
        9. WB        Wil T+R  *  1025.0    1019.0     717.0     920.0 *     324.   252. AG  3137.    .8    .0 68.0
       10. WB        Wil T+R Q *   798.0     946.0    4622.4    2169.8 *    4015.    72. AG    24. 100.0    .0 48.0 1.82 204.0
       11. WB        Wil LT   *  1040.0     975.0     742.0     883.0 *     312.   253. AG    17.    .8    .0 44.0
       12. WB        Wil LT Q *   824.0     908.0     933.5     941.5 *     114.    73. AG    21. 100.0    .0 24.0 8.00   5.8
       13. WB        Wil DP   *   715.0     922.0     201.0     748.0 *     543.   251. AG  3424.    .8    .0 68.0
       14. WB        Wil DP   *   201.0     748.0    -199.0     546.0 *     448.   243. AG  3424.    .8    .0 68.0
       15. NB        Vet AP   *   967.0     583.0    1327.0      75.0 *     623.   145. AG   931.    .9    .0 32.0
       16. NB        Vet T+LT *   960.0     579.0     781.0     840.0 *     316.   326. AG   799.    .9    .0 56.0
       17. NB        Vet T+LT Q*   820.0     783.0    1295.9      88.2 *     842.   146. AG    24. 100.0    .0 36.0 1.29  42.8
       18. NB        Vet RT   *   964.0     622.0     813.0     839.0 *     264.   325. AG   132.    .9    .0 32.0
       19. NB        Vet RT Q *   847.0     791.0     890.4     728.0 *      77.   145. AG     8. 100.0    .0 12.0  .52   3.9
       20. NB        Vet DP   *   798.0     836.0     611.0    1170.0 *     383.   331. AG  1771.    .9    .0 44.0
       21. NB        Vet DP   *   611.0    1170.0     214.0    1729.0 *     686.   325. AG  1771.    .9    .0 44.0
       22. SB        Vet AP   *   544.0    1188.0     172.0    1701.0 *     634.   324. AG  1108.    .9    .0 44.0
       23. SB        Vet T+LT *   550.0    1188.0     730.0     898.0 *     341.   148. AG   777.    .9    .0 56.0
       24. SB        Vet T+LT Q*   679.0     981.0     -63.4    2176.2 *    1407.   328. AG    26. 100.0    .0 36.0 1.80  71.5
       25. SB        Vet RT   *   521.0    1169.0     695.0     888.0 *     331.   148. AG   331.    .9    .0 44.0
       26. SB        Vet RT Q *   643.0     972.0     600.2    1041.0 *      81.   328. AG    13. 100.0    .0 24.0  .53   4.1
       27. SB        Vet DP   *   703.0     889.0    1292.0      46.0 *    1028.   145. AG   748.    .9    .0 44.0
1
                                                                                                                PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2B5AM.DAT)              RUN: Site 2 BUILD ALT5 AM
      DATE: 03/21/2010   TIME: 21:57:39.04

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*------------------------------------------------------------------------------
        4. EB        Wil T+R Q *     150       57       2.0      4619        966       4.10      1        3
        6. EB        Wil LT Q *     150      118       2.0       928         84       4.10      1        3
       10. WB        Wil T+R Q *     150       81       2.0      3137        994       4.10      1        3
       12. WB        Wil LT Q *     150      143       2.0        17         84       4.10      1        3
       17. NB        Vet T+LT Q*     150      111       2.0       799        887       4.10      1        3
       19. NB        Vet RT Q *     150      106       2.0       132        955       4.10      1        3
       24. SB        Vet T+LT Q*     150      120       2.0       777        834       4.10      1        3
       26. SB        Vet RT Q *     150       90       2.0       331        834       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X           Y          Z      *
     -------------------------*------------------------------------*
        1. SE MID S           *      1066.0      492.0       5.0   *
        2. SE 164 S           *       942.0      686.0       5.0   *
        3. SE 82 S            *       892.0      756.0       5.0   *
        4. SE CNR             *       869.0      821.0       5.0   *
        5. SE 82 E            *       925.0      853.0       5.0   *
        6. SE 164 E           *      1005.0      880.0       5.0   *
        7. SE MID E           *      1219.0      947.0       5.0   *
        8. NE MID E           *      1144.0     1099.0       5.0   *
        9. NE 164 E           *       918.0     1026.0       5.0   *
       10. NE 82 E            *       838.0     1000.0       5.0   *
       11. NE CNR             *       759.0      983.0       5.0   *
       12. NE 82 N            *       716.0     1047.0       5.0   *
       13. NE 164 N           *       676.0     1120.0       5.0   *
       14. NE MID N           *       595.0     1269.0       5.0   *
       15. NW MID N           *       464.0     1209.0       5.0   *
       16. NW 164 N           *       546.0     1079.0       5.0   *
       17. NW 82 N            *       589.0     1010.0       5.0   *
       18. NW CNR             *       611.0      945.0       5.0   *
       19. NW 82 W            *       552.0      910.0       5.0   *
       20. NW 164 W           *       475.0      884.0       5.0   *
       21. NW MID W           *       273.0      815.0       5.0   *
       22. SW MID W           *       305.0      649.0       5.0   *
       23. SW 164 W           *       565.0      737.0       5.0   *
       24. SW 82 W            *       645.0      764.0       5.0   *
       25. SW CNR             *       718.0      779.0       5.0   *
       26. SW 82 S            *       774.0      718.0       5.0   *
       27. SW 164 S           *       824.0      646.0       5.0   *
       28. SW MID S           *       957.0      459.0       5.0   *
1
                                                                                                                PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2B5AM.DAT)              RUN: Site 2 BUILD ALT5 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

```
            concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   5.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  10.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  15.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  20.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
  25.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .1    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .1    .1    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1
  75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  80.  *    .0    .0    .0    .0    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  85.  *    .0    .0    .0    .0    .0    .1    .0    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .4    .3    .3    .0    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .0    .0    .0    .1    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .1    .0    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .3    .0    .0    .0    .1    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
 120.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
 125.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .1    .0    .0    .1    .1    .2
 130.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .1    .2
 140.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 145.  *    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 150.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 155.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2
 160.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .0    .1    .0    .0    .0    .0    .1    .2    .2
 165.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 170.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 175.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 180.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 185.  *    .1    .1    .1    .1    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2
 190.  *    .1    .1    .1    .0    .0    .0    .0    .3    .3    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
 195.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
 200.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .2    .1
 205.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .2    .2
1
                                                                                                                 PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2B5AM.DAT)               RUN: Site 2 BUILD ALT5 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .2    .1
 215.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .1
 220.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 225.  *    .1    .1    .1    .0    .0    .0    .0    .3    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 230.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 235.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 240.  *    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .1    .1    .1    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .1    .1    .1    .0    .0    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 255.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 260.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .1    .1    .1    .1    .2    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .1    .1    .1    .2    .1    .1    .1    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0    .0    .0    .0
 295.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0
 300.  *    .1    .1    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0
 305.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .2    .0    .0    .0    .0    .0    .0
 310.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0
 315.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0
 320.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 340.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 345.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 350.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 355.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 360.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .2    .2    .2    .2    .3    .4    .3    .3    .2    .1    .2    .1    .1    .1    .1    .2    .2
 DEGR. *   150   150     0   280    50    50    55    95    90    85    90   285   160   305     0     0     0    90   140   115

1
                                                                                                                 PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2B5AM.DAT)               RUN: Site 2 BUILD ALT5 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
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```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .1    .0    .0    .0
   5.  *    .0    .1    .1    .1    .1    .0    .0    .0
  10.  *    .0    .1    .1    .1    .1    .0    .0    .0
  15.  *    .0    .1    .1    .1    .1    .0    .0    .0
  20.  *    .0    .1    .1    .1    .1    .0    .0    .0
  25.  *    .0    .1    .1    .1    .1    .1    .0    .0
  30.  *    .0    .1    .1    .1    .1    .1    .0    .0
  35.  *    .0    .2    .1    .1    .1    .1    .0    .0
  40.  *    .0    .2    .1    .1    .1    .1    .0    .0
  45.  *    .0    .2    .1    .1    .2    .1    .0    .0
  50.  *    .0    .2    .1    .1    .1    .1    .0    .0
  55.  *    .0    .2    .1    .2    .1    .1    .0    .0
  60.  *    .0    .1    .1    .2    .1    .1    .0    .0
  65.  *    .1    .1    .2    .2    .1    .0    .0    .0
  70.  *    .1    .1    .2    .2    .1    .0    .0    .0
  75.  *    .1    .1    .1    .1    .1    .0    .0    .0
  80.  *    .1    .1    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .2    .0    .0    .0    .0    .0    .0    .0
 100.  *    .2    .0    .0    .0    .0    .0    .0    .0
 105.  *    .2    .0    .0    .0    .0    .0    .0    .0
 110.  *    .2    .0    .0    .0    .0    .0    .0    .0
 115.  *    .2    .0    .0    .0    .0    .0    .0    .0
 120.  *    .2    .0    .0    .0    .0    .0    .0    .0
 125.  *    .2    .0    .0    .0    .0    .0    .0    .0
 130.  *    .2    .0    .0    .0    .0    .0    .0    .0
 135.  *    .2    .0    .0    .0    .0    .0    .0    .0
 140.  *    .2    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .2    .0    .0    .0    .0    .0    .0    .0
 205.  *    .2    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                               PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2B5AM.DAT)               RUN: Site 2 BUILD ALT5 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .0    .1    .0    .0    .0    .0
 250.  *    .0    .1    .1    .1    .1    .0    .0    .0
 255.  *    .0    .2    .2    .2    .1    .0    .0    .0
 260.  *    .0    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .2    .2    .2    .2    .0    .0    .0
 275.  *    .0    .2    .2    .2    .1    .0    .0    .0
 280.  *    .0    .2    .2    .2    .1    .1    .0    .0
 285.  *    .0    .2    .2    .2    .1    .1    .0    .0
 290.  *    .0    .2    .1    .1    .1    .1    .0    .0
 295.  *    .0    .1    .1    .1    .1    .1    .0    .0
 300.  *    .0    .1    .1    .1    .1    .1    .0    .0
 305.  *    .0    .1    .1    .1    .1    .1    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .2    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .1    .0    .0    .0
 340.  *    .0    .1    .1    .1    .1    .0    .0    .0
 345.  *    .0    .1    .1    .1    .1    .0    .0    .0
 350.  *    .0    .1    .1    .1    .1    .0    .0    .0
 355.  *    .0    .1    .1    .1    .1    .0    .0    .0
 360.  *    .0    .1    .1    .1    .1    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .2    .2    .2    .2    .2    .1    .0    .0
 DEGR. *   95    35    65    55    45    25     0     0

 THE HIGHEST CONCENTRATION IS     .40 PPM AT   90 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   95 DEGREES FROM REC8 .
 THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT   85 DEGREES FROM REC10.
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                  PAGE  1

      JOB: Site 2 Veteran & Wilshire (S2B5PM.DAT)              RUN: Site 2 BUILD ALT5 PM
      DATE: 03/21/2010   TIME: 22:44:13.37


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1       Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*---------------------------------------*---------------------------------------------------------
       1. EB        Wil AP    *   -172.0     469.0      78.0     601.0 *     283.    62. AG  3396.    .8    .0 68.0
       2. EB        Wil AP    *     78.0     601.0     276.0     684.0 *     215.    67. AG  3396.    .8    .0 68.0
       3. EB        Wil T+R   *    276.0     684.0     778.0     856.0 *     531.    71. AG  3109.    .8    .0 68.0
       4. EB        Wil T+R Q *    678.0     822.0   -2495.9    -272.8 *    3357.   251. AG    21. 100.0    .0 48.0 1.61 170.6
       5. EB        Wil LT    *    259.0     724.0     761.0     889.0 *     528.    72. AG   287.    .8    .0 44.0
       6. EB        Wil LT Q  *    659.0     855.0    -963.1     323.2 *    1707.   252. AG    19. 100.0    .0 24.0 ****  86.7
       7. EB        Wil DP    *    782.0     851.0    1703.0    1145.0 *     967.    72. AG  3318.    .8    .0 68.0
       8. WB        Wil AP    *   1025.0    1019.0    1677.0    1228.0 *     685.    72. AG  4322.    .8    .0 68.0
       9. WB        Wil T+R   *   1025.0    1019.0     717.0     920.0 *     324.   252. AG  4305.    .8    .0 68.0
      10. WB        Wil T+R Q *    798.0     946.0    7669.6    3144.9 *    7215.    72. AG    24. 100.0    .0 48.0 2.57 366.5
      11. WB        Wil LT    *   1040.0     975.0     742.0     883.0 *     312.   253. AG    17.    .8    .0 44.0
      12. WB        Wil LT Q  *    824.0     908.0     933.5     941.5 *     114.    73. AG    21. 100.0    .0 24.0 8.00   5.8
      13. WB        Wil DP    *    715.0     922.0     201.0     748.0 *     543.   251. AG  4984.    .8    .0 68.0
      14. WB        Wil DP    *    201.0     748.0    -199.0     546.0 *     448.   243. AG  4984.    .8    .0 68.0
      15. NB        Vet AP    *    967.0     583.0    1327.0      75.0 *     623.   145. AG  1370.    .9    .0 32.0
      16. NB        Vet T+LT  *    960.0     579.0     781.0     840.0 *     316.   326. AG  1075.    .9    .0 56.0
      17. NB        Vet T+LT Q*    820.0     783.0    1539.2    -266.9 *    1273.   146. AG    21. 100.0    .0 36.0 1.38  64.6
      18. NB        Vet RT    *    964.0     622.0     813.0     839.0 *     264.   325. AG   295.    .9    .0 32.0
      19. NB        Vet RT Q  *    847.0     791.0     947.0     645.7 *     176.   145. AG     7. 100.0    .0 12.0  .88   9.0
      20. NB        Vet DP    *    798.0     836.0     611.0    1170.0 *     383.   331. AG  1793.    .9    .0 44.0
      21. NB        Vet DP    *    611.0    1170.0     214.0    1729.0 *     686.   325. AG  1793.    .9    .0 44.0
      22. SB        Vet AP    *    544.0    1188.0     172.0    1701.0 *     634.   324. AG  1986.    .9    .0 44.0
      23. SB        Vet T+LT  *    550.0    1188.0     730.0     898.0 *     341.   148. AG   876.    .9    .0 56.0
      24. SB        Vet T+LT Q*    679.0     981.0      83.8    1939.2 *    1128.   328. AG    24. 100.0    .0 36.0 1.42  57.3
      25. SB        Vet RT    *    521.0    1169.0     695.0     888.0 *     331.   148. AG  1110.    .9    .0 44.0
      26. SB        Vet RT Q  *    643.0     972.0    -927.5    3503.8 *    2979.   328. AG    13. 100.0    .0 24.0 1.88 151.4
      27. SB        Vet DP    *    703.0     889.0    1292.0      46.0 *    1028.   145. AG   979.    .9    .0 44.0
1
                                                                                                              PAGE  2
      JOB: Site 2 Veteran & Wilshire (S2B5PM.DAT)              RUN: Site 2 BUILD ALT5 PM
      DATE: 03/21/2010   TIME: 22:44:13.37

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       4. EB        Wil T+R Q *     150       71       2.0      3109        969       4.10      1        3
       6. EB        Wil LT Q  *     150      132       2.0       287         84       4.10      1        3
      10. WB        Wil T+R Q *     150       82       2.0      4305        981       4.10      1        3
      12. WB        Wil LT Q  *     150      143       2.0        17         84       4.10      1        3
      17. NB        Vet T+LT Q*     150       97       2.0      1075        795       4.10      1        3
      19. NB        Vet RT Q  *     150       92       2.0       295        929       4.10      1        3
      24. SB        Vet T+LT Q*     150      108       2.0       876        812       4.10      1        3
      26. SB        Vet RT Q  *     150       90       2.0      1110        794       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*------------------------------------*
       1. SE MID S            *      1066.0      492.0       5.0   *
       2. SE 164 S            *       942.0      686.0       5.0   *
       3. SE 82 S             *       892.0      756.0       5.0   *
       4. SE CNR              *       869.0      821.0       5.0   *
       5. SE 82 E             *       925.0      853.0       5.0   *
       6. SE 164 E            *      1005.0      880.0       5.0   *
       7. SE MID E            *      1219.0      947.0       5.0   *
       8. NE MID E            *      1144.0     1099.0       5.0   *
       9. NE 164 E            *       918.0     1026.0       5.0   *
      10. NE 82 E             *       838.0     1000.0       5.0   *
      11. NE CNR              *       759.0      983.0       5.0   *
      12. NE 82 N             *       716.0     1047.0       5.0   *
      13. NE 164 N            *       676.0     1120.0       5.0   *
      14. NE MID N            *       595.0     1269.0       5.0   *
      15. NW MID N            *       464.0     1209.0       5.0   *
      16. NW 164 N            *       546.0     1079.0       5.0   *
      17. NW 82 N             *       589.0     1010.0       5.0   *
      18. NW CNR              *       611.0      945.0       5.0   *
      19. NW 82 W             *       552.0      910.0       5.0   *
      20. NW 164 W            *       475.0      884.0       5.0   *
      21. NW MID W            *       273.0      815.0       5.0   *
      22. SW MID W            *       305.0      649.0       5.0   *
      23. SW 164 W            *       565.0      737.0       5.0   *
      24. SW 82 W             *       645.0      764.0       5.0   *
      25. SW CNR              *       718.0      779.0       5.0   *
      26. SW 82 S             *       774.0      718.0       5.0   *
      27. SW 164 S            *       824.0      646.0       5.0   *
      28. SW MID S            *       957.0      459.0       5.0   *
1
                                                                                                              PAGE  3
      JOB: Site 2 Veteran & Wilshire (S2B5PM.DAT)              RUN: Site 2 BUILD ALT5 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
```

```
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
   5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
  10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  75.  *    .0    .0    .0    .0    .1    .1    .1    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  80.  *    .0    .0    .0    .0    .1    .1    .0    .2    .3    .3    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .2    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 150.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 165.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 170.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 175.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 180.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 185.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 190.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 195.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 200.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1
 205.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
1
                                                                                                                       PAGE  4
      JOB: Site 2 Veteran & Wilshire (S2B5PM.DAT)             RUN: Site 2 BUILD ALT5 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
 215.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
 220.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .1
 225.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1
 230.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .1    .0    .0    .0    .0    .0    .1    .2    .1
 235.  *    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .0    .0    .0    .0    .1    .2    .1
 240.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .1    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 255.  *    .1    .0    .0    .0    .0    .1    .1    .0    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 260.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 265.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .1    .1    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .1    .1    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .0    .1    .0    .0    .0    .0    .0    .0
 310.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0
 315.  *    .1    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
 340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 ------*-------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .1    .1    .1    .1    .2    .2    .2    .3    .3    .2    .2    .1    .1    .2    .2    .2    .2    .2    .1
 DEGR. *  150   150   150     0     0    40    30    70    75    75    75   300   160   305   345   340   340    95   230    65

1
                                                                                                                       PAGE  5
      JOB: Site 2 Veteran & Wilshire (S2B5PM.DAT)             RUN: Site 2 BUILD ALT5 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.
```

```
 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .3    .3    .2    .1    .0    .0    .0
   5.  *    .0    .3    .3    .1    .1    .0    .0    .0
  10.  *    .0    .3    .3    .1    .1    .0    .0    .0
  15.  *    .0    .3    .3    .1    .1    .0    .0    .0
  20.  *    .0    .3    .2    .1    .1    .0    .0    .0
  25.  *    .0    .3    .2    .1    .1    .0    .0    .0
  30.  *    .0    .3    .2    .1    .1    .0    .0    .0
  35.  *    .0    .3    .2    .1    .0    .0    .0    .0
  40.  *    .0    .3    .2    .1    .0    .0    .0    .0
  45.  *    .0    .3    .2    .1    .0    .0    .0    .0
  50.  *    .0    .2    .1    .1    .1    .0    .0    .0
  55.  *    .0    .2    .1    .1    .1    .0    .0    .0
  60.  *    .1    .2    .1    .1    .1    .0    .0    .0
  65.  *    .1    .2    .1    .0    .1    .0    .0    .0
  70.  *    .1    .1    .0    .0    .1    .0    .0    .0
  75.  *    .1    .1    .0    .0    .0    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .2    .0    .0    .0    .0    .0    .0    .0
  90.  *    .2    .0    .0    .0    .0    .0    .0    .0
  95.  *    .2    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
      JOB: Site 2 Veteran & Wilshire (S2B5PM.DAT)              RUN: Site 2 BUILD ALT5 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .2    .1    .2    .0    .0    .0    .0
 255.  *    .0    .2    .2    .2    .2    .0    .0    .0
 260.  *    .0    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .3    .2    .2    .2    .0    .0    .0
 275.  *    .0    .3    .2    .2    .2    .0    .0    .0
 280.  *    .0    .3    .2    .3    .3    .0    .0    .0
 285.  *    .0    .3    .3    .3    .2    .0    .0    .0
 290.  *    .0    .3    .3    .3    .2    .0    .0    .0
 295.  *    .0    .2    .3    .3    .2    .0    .0    .0
 300.  *    .0    .2    .3    .3    .2    .0    .0    .0
 305.  *    .0    .2    .3    .3    .2    .0    .0    .0
 310.  *    .0    .1    .3    .3    .2    .0    .0    .0
 315.  *    .0    .1    .3    .3    .2    .0    .0    .0
 320.  *    .0    .1    .3    .3    .2    .0    .0    .0
 325.  *    .0    .1    .3    .3    .2    .0    .0    .0
 330.  *    .0    .1    .3    .3    .2    .0    .0    .0
 335.  *    .0    .2    .3    .3    .1    .0    .0    .0
 340.  *    .0    .3    .3    .3    .1    .0    .0    .0
 345.  *    .0    .3    .3    .3    .1    .0    .0    .0
 350.  *    .0    .3    .3    .3    .1    .0    .0    .0
 355.  *    .0    .3    .3    .2    .1    .0    .0    .0
 360.  *    .0    .3    .3    .2    .1    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .2    .3    .3    .3    .3    .0    .0    .0
 DEGR. *   85     0     0   280   280     0     0     0

 THE HIGHEST CONCENTRATION IS      .30 PPM AT   75 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .30 PPM AT   75 DEGREES FROM REC10.
 THE 3RD HIGHEST CONCENTRATION IS     .30 PPM AT    0 DEGREES FROM REC22.
```

Site 3 – Glendon & Wilshire
Input Files

```
Site 3 Glendon & Wilshire (S3EXAM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 Existing AM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2246 3.3  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    1981 3.3  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        35       2.0 1981   20.5 1001 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     265 3.3  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       124       2.0  265   20.5 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    1928 3.3  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2442 3.3  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2375 3.3  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        63       2.0 2375   20.5  991 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      67 3.3  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        63       2.0   67   20.5   98 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2168 3.3  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     199 3.5  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       120       2.0  199   20.5 1143 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     757 3.5  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     229 3.5  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     117 3.5  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       120       2.0  117   20.5  806 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     112 3.5  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        96       2.0  112   20.5 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     263 3.5  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     263 3.5  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3EXPM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 Existing PM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    1996 3.3  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    1842 3.3  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 1842   20.5 1008 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     154 3.3  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       124       2.0  154     20.5 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2144 3.3  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2124 3.3  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2044 3.3  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        74       2.0 2044   20.5  994 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      80 3.3  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        74       2.0   80   20.5   50 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2158 3.3  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     367 3.5  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150        99       2.0  367   20.5  566 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     531 3.5  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     797 3.5  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     547 3.5  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150        99       2.0  547   20.5  838 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     250 3.5  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        85       2.0  250   20.5 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     451 3.5  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     451 3.5  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3NBAM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 NO BUILD AM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2967 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2763 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        39       2.0 2763   4.1  992 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     204 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       130       2.0  204   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2497 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3144 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3048 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        62       2.0 3048   4.1  990 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      96 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        62       2.0   96   4.1   54 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2816 0.8  0.   68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     311 0.9  0.   32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       116       2.0  311   4.1 1039 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     898 0.9  0.   32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     540 0.9  0.   32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     336 0.9  0.   44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       116       2.0  336   4.1  731 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     204 0.9  0.   32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        98       2.0  204   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     751 0.9  0.   32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     751 0.9  0.   32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3NBPM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.        5.0
SE 164 S                  638.      508.        5.0
SE 82 S                   611.      586.        5.0
SE CNR                    595.      659.        5.0
SE 82 E                   664.      689.        5.0
SE 164 E                  742.      713.        5.0
SE MID E                  849.      747.        5.0
NE MID E                  793.      878.        5.0
NE 164 E                  674.      839.        5.0
NE 82 E                   595.      813.        5.0
NE CNR                    515.      792.        5.0
NE 82 N                   452.      847.        5.0
NE 164 N                  396.      907.        5.0
NE MID N                  319.      990.        5.0
NW MID N                  190.      983.        5.0
NW 164 N                  267.      900.        5.0
NW 82 N                   323.      841.        5.0
NW CNR                    381.      759.        5.0
NW 82 W                   299.      719.        5.0
NW 164 W                  222.      694.        5.0
NW MID W                  107.      658.        5.0
SW MID W                  213.      548.        5.0
SW 164 W                  367.      595.        5.0
SW 82 W                   447.      619.        5.0
SW CNR                    518.      634.        5.0
SW 82 S                   550.      565.        5.0
SW 164 S                  577.      487.        5.0
SW MID S                  622.      354.        5.0
Site 3 NO BUILD PM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2690 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2457 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2457   4.1 1007 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     233 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       129       2.0  233   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2819 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2887 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2754 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        79       2.0 2754   4.1  991 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     133 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        79        2.0  133   4.1   68 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    3052 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     899 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150        99        2.0  899   4.1  276 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     960 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.    1017 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     713 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150        99        2.0  713   4.1  836 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     304 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        80        2.0  304   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     662 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     662 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B1AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD 1  AM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2885 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2690 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        39        2.0 2690   4.1  994 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     195 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       130        2.0  195   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2465 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3121 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3035 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        62        2.0 3035   4.1  924 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      86 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        62       2.0   86   4.1   54 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2899 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     388 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       116       2.0  388   4.1 1069 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     929 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     593 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     330 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       116       2.0  330   4.1  678 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     263 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        98       2.0  263   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     694 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     694 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B1PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD A1 PM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2704 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2475 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2475   4.1 1007 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     229 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       130       2.0  229   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2819 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2895 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2762 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        78       2.0 2762   4.1  990 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     133 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        78       2.0  133   4.1   68 1 3
  1
WB        Wil DP    AG   483.    742.   -451.    441.    3001 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.    703.    861.   -211.     870 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.    640.    649.    396.      0.  12   1
       150        99       2.0  870   4.1  280 1 3
  1
NB        Gln DP    AG   545.    705.   -160.   1462.     988 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.    915.   -182.   1445.    1004 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.    915.    479.    736.     699 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.    786.    325.    894.      0.  24   2
       150        99       2.0  699   4.1  816 1 3
  1
SB        Gln R     AG   300.    890.    443.    732.     305 0.9  0.  32   30.
  2
SB        Gln R     AG   400.    780.    310.    880.      0.  12   1
       150        81       2.0  305   4.1 1000 1 3
  1
SB        Gln DP    AG   478.    734.    548.    638.     665 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.    638.    840.   -220.     665 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B2AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD 2  AM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2910 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2733 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150         39       2.0 2733   4.1  993 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     177 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150        131       2.0  177   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2513 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3134 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3039 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150         60       2.0 3039   4.1  989 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      95 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        60       2.0   95   4.1   54 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2846 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     382 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       116       2.0  382   4.1 1075 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     951 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     604 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     352 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       116       2.0  352   4.1  681 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     252 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        99       2.0  252   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     720 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     720 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B2PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD A2 PM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2692 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2479 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2479   4.1 1006 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     229 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       130       2.0  229   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2820 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2921 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2789 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        77       2.0 2789   4.1  989 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     132 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        77       2.0  132   4.1   66 1 3
  1
WB         Wil DP    AG   483.   742.  -451.   441.    3052 0.8  0.  68   30.
  1
NB         Gln AP    AG   542.   703.   861.  -211.     888 0.9  0.  32   30.
  2
NB         Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150        99       2.0  888   4.1  268 1 3
  1
NB         Gln DP    AG   545.   705.  -160.  1462.     964 0.9  0.  32   30.
  1
SB         Gln AP    AG   305.   915.  -182.  1445.    1003 0.9  0.  32   30.
  1
SB         Gln T+LT  AG   305.   915.   479.   736.     706 0.9  0.  44   30.
  2
SB         Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150        99       2.0  706   4.1  833 1 3
  1
SB         Gln R     AG   300.   890.   443.   732.     303 0.9  0.  32   30.
  2
SB         Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        83       2.0  303   4.1 1000 1 3
  1
SB         Gln DP    AG   478.   734.   548.   638.     674 0.9  0.  32   30.
  1
SB         Gln DP    AG   548.   638.   840.  -220.     674 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

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Site 3 Glendon & Wilshire (S3B3AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD 3  AM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2883 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2678 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        39       2.0 2678   4.1  994 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     205 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       129       2.0  205   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2652 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3101 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3005 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        62       2.0 3005   4.1  990 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      96 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        62       2.0   96   4.1   54 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2818 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.    861.  -211.     316 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.    649.   396.      0.  12   1
       150       116       2.0  316   4.1 1046 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     885 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     570 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.    479.   736.     340 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.    325.   894.      0.  24   2
       150       116       2.0  340   4.1  727 1 3
  1
SB        Gln R     AG   300.   890.    443.   732.     230 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.    310.   880.      0.  12   1
       150        97       2.0  230   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.    548.   638.     698 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.    840.  -220.     698 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B3PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD A3 PM                       22   1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2689 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2449 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2449   4.1 1007 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     240 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       129       2.0  240   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2786 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2876 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2744 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        79       2.0 2744   4.1  991 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     132 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        79       2.0  132   4.1   68 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2979 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     855 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150        99       2.0  855   4.1  262 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     973 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     998 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     708 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150        99       2.0  708   4.1  808 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     290 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        80       2.0  290   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     680 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     680 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
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Site 3 Glendon & Wilshire (S3B4AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD 4  AM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2883 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2701 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        39       2.0 2701   4.1  994 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     182 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       131       2.0  182   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2517 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3126 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3030 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        60       2.0 3030   4.1  990 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      96 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        60       2.0   96   4.1   53 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2821 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     371 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       116       2.0  371   4.1 1064 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     928 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     583 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     363 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       116       2.0  363   4.1  689 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     220 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        99       2.0  220   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     697 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     697 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 3 Glendon & Wilshire (S3B4PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD A4 PM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2660 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2445 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2445   4.1 1007 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     205 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       131       2.0  205   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2820 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2950 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2818 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        77       2.0 2818   4.1  990 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     132 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        77       2.0  132   4.1   66 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    3022 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     880 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150        99       2.0  880   4.1  282 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.    1010 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.    1034 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     727 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150        99       2.0  727   4.1  794 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     307 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        82       2.0  307   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     672 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     672 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

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Site 3 Glendon & Wilshire (S3B5AM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.       5.0
SE 164 S                  638.      508.       5.0
SE 82 S                   611.      586.       5.0
SE CNR                    595.      659.       5.0
SE 82 E                   664.      689.       5.0
SE 164 E                  742.      713.       5.0
SE MID E                  849.      747.       5.0
NE MID E                  793.      878.       5.0
NE 164 E                  674.      839.       5.0
NE 82 E                   595.      813.       5.0
NE CNR                    515.      792.       5.0
NE 82 N                   452.      847.       5.0
NE 164 N                  396.      907.       5.0
NE MID N                  319.      990.       5.0
NW MID N                  190.      983.       5.0
NW 164 N                  267.      900.       5.0
NW 82 N                   323.      841.       5.0
NW CNR                    381.      759.       5.0
NW 82 W                   299.      719.       5.0
NW 164 W                  222.      694.       5.0
NW MID W                  107.      658.       5.0
SW MID W                  213.      548.       5.0
SW 164 W                  367.      595.       5.0
SW 82 W                   447.      619.       5.0
SW CNR                    518.      634.       5.0
SW 82 S                   550.      565.       5.0
SW 164 S                  577.      487.       5.0
SW MID S                  622.      354.       5.0
Site 3 BUILD 5  AM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2901 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2690 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150         45       2.0 2690   4.1  992 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     211 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       137       2.0  211   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2446 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    3128 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    3032 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        60       2.0 3032   4.1  989 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.      96 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        60       2.0   96   4.1   53 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2795 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     374 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150       110       2.0  374   4.1 1141 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.     975 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.     574 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     367 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150       110       2.0  367   4.1  733 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     207 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        99       2.0  207   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     761 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     761 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
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Site 3 Glendon & Wilshire (S3B5PM.DAT)  60.0321.0.0000.000280.30480000    1
1
SE MID S                  685.      365.        5.0
SE 164 S                  638.      508.        5.0
SE 82 S                   611.      586.        5.0
SE CNR                    595.      659.        5.0
SE 82 E                   664.      689.        5.0
SE 164 E                  742.      713.        5.0
SE MID E                  849.      747.        5.0
NE MID E                  793.      878.        5.0
NE 164 E                  674.      839.        5.0
NE 82 E                   595.      813.        5.0
NE CNR                    515.      792.        5.0
NE 82 N                   452.      847.        5.0
NE 164 N                  396.      907.        5.0
NE MID N                  319.      990.        5.0
NW MID N                  190.      983.        5.0
NW 164 N                  267.      900.        5.0
NW 82 N                   323.      841.        5.0
NW CNR                    381.      759.        5.0
NW 82 W                   299.      719.        5.0
NW 164 W                  222.      694.        5.0
NW MID W                  107.      658.        5.0
SW MID W                  213.      548.        5.0
SW 164 W                  367.      595.        5.0
SW 82 W                   447.      619.        5.0
SW CNR                    518.      634.        5.0
SW 82 S                   550.      565.        5.0
SW 164 S                  577.      487.        5.0
SW MID S                  622.      354.        5.0
Site 3 BUILD A5 PM                       22  1   0
  1
EB        Wil AP    AG   323.   617.  -426.   376.    2699 0.8  0.  68   30.
  1
EB        Wil T+R   AG   323.   616.   531.   681.    2469 0.8  0.  68   30.
  2
EB        Wil T+R   AG   475.   663.   329.   618.      0.  48   4
       150        56       2.0 2469   4.1 1007 1 3
  1
EB        Wil LT    AG   315.   650.   513.   712.     230 0.8  0.  44   30.
  2
EB        Wil LT    AG   444.   690.   317.   651.      0.  24   2
       150       130       2.0  230   4.1 1084 1 3
  1
EB        Wil DP    AG   532.   683.  1471.   989.    2814 0.8  0.  68   30.
  1
WB        Wil AP    AG   756.   830.  1454.  1051.    2904 0.8  0.  68   30.
  1
WB        Wil T+R   AG   756.   829.   484.   742.    2772 0.8  0.  68   30.
  2
WB        Wil T+R   AG   540.   760.   753.   828.      0.  48   4
       150        78       2.0 2772   4.1  989 1 3
  1
WB        Wil LT    AG   767.   790.   513.   706.     132 0.8  0.  32   30.
  2
WB        Wil LT    AG   566.   723.   763.   788.      0.  12   1
```

```
       150        78       2.0  132   4.1   68 1 3
  1
WB        Wil DP    AG   483.   742.  -451.   441.    2979 0.8  0.  68   30.
  1
NB        Gln AP    AG   542.   703.   861.  -211.     881 0.9  0.  32   30.
  2
NB        Gln AP    AG   564.   640.   649.   396.      0.  12   1
       150        99       2.0  881   4.1  285 1 3
  1
NB        Gln DP    AG   545.   705.  -160.  1462.    1031 0.9  0.  32   30.
  1
SB        Gln AP    AG   305.   915.  -182.  1445.    1010 0.9  0.  32   30.
  1
SB        Gln T+LT  AG   305.   915.   479.   736.     705 0.9  0.  44   30.
  2
SB        Gln T+LT  AG   430.   786.   325.   894.      0.  24   2
       150        99       2.0  705   4.1  804 1 3
  1
SB        Gln R     AG   300.   890.   443.   732.     305 0.9  0.  32   30.
  2
SB        Gln R     AG   400.   780.   310.   880.      0.  12   1
       150        81       2.0  305   4.1 1000 1 3
  1
SB        Gln DP    AG   478.   734.   548.   638.     670 0.9  0.  32   30.
  1
SB        Gln DP    AG   548.   638.   840.  -220.     670 0.9  0.  32   30.
1.0   04 1000.   0Y  5  0 72
```

Site 3 – Glendon & Wilshire Output Files

```
1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                   PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT)              RUN: Site 3 Existing AM
      DATE: 03/22/2010   TIME: 09:10:02.31


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*--------------------------------------*-------------------------------------------------------------
       1. EB        Wil AP    *    323.0     617.0    -426.0     376.0 *     787.   252. AG   2246.   3.3    .0 68.0
       2. EB        Wil T+R   *    323.0     616.0     531.0     681.0 *     218.    73. AG   1981.   3.3    .0 68.0
       3. EB        Wil T+R   *    475.0     663.0     384.5     635.1 *      95.   253. AG     51. 100.0    .0 48.0  .67   4.8
       4. EB        Wil LT    *    315.0     650.0     513.0     712.0 *     207.    73. AG    265.   3.3    .0 44.0
       5. EB        Wil LT    *    444.0     690.0     342.0     658.7 *     107.   253. AG     91. 100.0    .0 24.0  .84   5.4
       6. EB        Wil DP    *    532.0     683.0    1471.0     989.0 *     988.    72. AG   1928.   3.3    .0 68.0
       7. WB        Wil AP    *    756.0     830.0    1454.0    1051.0 *     732.    72. AG   2442.   3.3    .0 68.0
       8. WB        Wil T+R   *    756.0     829.0     484.0     742.0 *     286.   252. AG   2375.   3.3    .0 68.0
       9. WB        Wil T+R   *    540.0     760.0    1274.1     994.4 *     771.    72. AG     92. 100.0    .0 48.0 1.08  39.1
      10. WB        Wil LT    *    767.0     790.0     513.0     706.0 *     268.   252. AG     67.   3.3    .0 32.0
      11. WB        Wil LT    *    566.0     723.0     751.9     784.3 *     196.    72. AG     23. 100.0    .0 12.0 1.24   9.9
      12. WB        Wil DP    *    483.0     742.0    -451.0     441.0 *     981.   252. AG   2168.   3.3    .0 68.0
      13. NB        Gln AP    *    542.0     703.0     861.0    -211.0 *     968.   161. AG    199.   3.5    .0 32.0
      14. NB        Gln AP    *    564.0     640.0     632.8     442.4 *     209.   161. AG     44. 100.0    .0 12.0 1.01  10.6
      15. NB        Gln DP    *    545.0     705.0    -160.0    1462.0 *    1034.   317. AG    757.   3.5    .0 32.0
      16. SB        Gln AP    *    305.0     915.0    -182.0    1445.0 *     720.   317. AG    229.   3.5    .0 32.0
      17. SB        Gln T+LT  *    305.0     915.0     479.0     736.0 *     250.   136. AG    117.   3.5    .0 44.0
      18. SB        Gln T+LT  *    430.0     786.0     403.5     813.3 *      38.   316. AG     88. 100.0    .0 24.0  .42   1.9
      19. SB        Gln R     *    300.0     890.0     443.0     732.0 *     213.   138. AG    112.   3.5    .0 32.0
      20. SB        Gln R     *    400.0     780.0     360.7     823.7 *      59.   318. AG     35. 100.0    .0 12.0  .34   3.0
      21. SB        Gln DP    *    478.0     734.0     548.0     638.0 *     119.   144. AG    263.   3.5    .0 32.0
      22. SB        Gln DP    *    548.0     638.0     840.0    -220.0 *     906.   161. AG    263.   3.5    .0 32.0
1
                                                                                                               PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT)              RUN: Site 3 Existing AM
      DATE: 03/22/2010   TIME: 09:10:02.31

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)     (SEC)     (VPH)      (VPH)    (gm/hr)
      ------------------------*------------------------------------------------------------------------------
       3. EB        Wil T+R   *     150       35       2.0      1981       1001      20.50      1        3
       5. EB        Wil LT    *     150      124       2.0       265       1084      20.50      1        3
       9. WB        Wil T+R   *     150       63       2.0      2375        991      20.50      1        3
      11. WB        Wil LT    *     150       63       2.0        67         98      20.50      1        3
      14. NB        Gln AP    *     150      120       2.0       199       1143      20.50      1        3
      18. SB        Gln T+LT  *     150      120       2.0       117        806      20.50      1        3
      20. SB        Gln R     *     150       96       2.0       112       1000      20.50      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-----------------------------------*
      1. SE MID S             *       685.0      365.0        5.0   *
      2. SE 164 S             *       638.0      508.0        5.0   *
      3. SE 82 S              *       611.0      586.0        5.0   *
      4. SE CNR               *       595.0      659.0        5.0   *
      5. SE 82 E              *       664.0      689.0        5.0   *
      6. SE 164 E             *       742.0      713.0        5.0   *
      7. SE MID E             *       849.0      747.0        5.0   *
      8. NE MID E             *       793.0      878.0        5.0   *
      9. NE 164 E             *       674.0      839.0        5.0   *
     10. NE 82 E              *       595.0      813.0        5.0   *
     11. NE CNR               *       515.0      792.0        5.0   *
     12. NE 82 N              *       452.0      847.0        5.0   *
     13. NE 164 N             *       396.0      907.0        5.0   *
     14. NE MID N             *       319.0      990.0        5.0   *
     15. NW MID N             *       190.0      983.0        5.0   *
     16. NW 164 N             *       267.0      900.0        5.0   *
     17. NW 82 N              *       323.0      841.0        5.0   *
     18. NW CNR               *       381.0      759.0        5.0   *
     19. NW 82 W              *       299.0      719.0        5.0   *
     20. NW 164 W             *       222.0      694.0        5.0   *
     21. NW MID W             *       107.0      658.0        5.0   *
     22. SW MID W             *       213.0      548.0        5.0   *
     23. SW 164 W             *       367.0      595.0        5.0   *
     24. SW 82 W              *       447.0      619.0        5.0   *
     25. SW CNR               *       518.0      634.0        5.0   *
     26. SW 82 S              *       550.0      565.0        5.0   *
     27. SW 164 S             *       577.0      487.0        5.0   *
     28. SW MID S             *       622.0      354.0        5.0   *
1
                                                                                                               PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT)              RUN: Site 3 Existing AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .3    .3    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0
   5.  *    .0    .3    .3    .4    .4    .5    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0
  10.  *    .0    .2    .3    .4    .4    .5    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0
  15.  *    .0    .2    .3    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0
  20.  *    .0    .2    .3    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0
  25.  *    .0    .2    .3    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0
  30.  *    .0    .3    .2    .4    .5    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0
  35.  *    .0    .3    .3    .4    .5    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0
  40.  *    .0    .3    .3    .5    .6    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0
  45.  *    .0    .3    .3    .5    .5    .5    .5    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0
  50.  *    .0    .3    .3    .6    .5    .5    .5    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1
  55.  *    .0    .1    .3    .5    .5    .5    .5    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
  60.  *    .0    .0    .3    .5    .5    .5    .5    .3    .3    .3    .2    .0    .0    .0    .0    .0    .0    .2    .1    .1
  65.  *    .0    .0    .1    .4    .5    .5    .5    .3    .4    .4    .3    .0    .0    .0    .0    .0    .0    .3    .3    .3
  70.  *    .0    .0    .1    .4    .5    .5    .3    .5    .5    .5    .5    .0    .0    .0    .0    .0    .0    .3    .4    .4
  75.  *    .0    .0    .0    .2    .2    .2    .2    .7    .7    .7    .7    .2    .0    .0    .0    .0    .1    .5    .6    .5
  80.  *    .0    .0    .0    .1    .2    .2    .1    .8    .8    .8    .8    .2    .0    .0    .0    .0    .2    .6    .5    .6
  85.  *    .0    .0    .0    .1    .1    .1    .1    .9    .9    .9    .8    .3    .2    .0    .0    .1    .2    .5    .6    .6
  90.  *    .0    .0    .0    .0    .1    .1    .1    .9    .9    .9    .8    .4    .2    .0    .0    .1    .4    .4    .6    .6
  95.  *    .0    .0    .0    .0    .1    .0    .0    .9    .9    .9    .7    .4    .3    .2    .1    .1    .3    .4    .6    .5
 100.  *    .0    .0    .0    .0    .0    .0    .0    .7    .8    .8    .7    .3    .3    .1    .1    .2    .3    .5    .6    .5
 105.  *    .0    .0    .0    .0    .0    .0    .0    .7    .7    .7    .7    .3    .3    .1    .1    .3    .3    .4    .5    .5
 110.  *    .0    .0    .0    .0    .0    .0    .0    .7    .7    .7    .7    .3    .3    .1    .1    .2    .3    .4    .5    .4
 115.  *    .0    .0    .0    .0    .0    .0    .0    .7    .6    .7    .6    .3    .3    .1    .0    .1    .2    .3    .4    .4
 120.  *    .0    .0    .0    .0    .0    .0    .0    .7    .6    .7    .5    .3    .3    .1    .0    .0    .1    .3    .4    .3
 125.  *    .0    .0    .0    .0    .0    .0    .0    .7    .6    .7    .5    .3    .3    .2    .0    .0    .1    .3    .4    .4
 130.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .5    .3    .2    .1    .0    .0    .1    .3    .4    .3
 135.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .5    .3    .1    .1    .0    .0    .1    .4    .4    .3
 140.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .4    .2    .2    .1    .0    .1    .1    .4    .4    .3
 145.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .4    .2    .2    .1    .0    .1    .2    .4    .4    .3
 150.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .4    .2    .1    .1    .0    .1    .2    .5    .3    .3
 155.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .4    .2    .1    .1    .0    .1    .3    .5    .3    .3
 160.  *    .0    .0    .0    .0    .0    .0    .0    .7    .6    .6    .3    .2    .2    .1    .0    .1    .3    .5    .3    .3
 165.  *    .0    .0    .1    .0    .0    .0    .0    .7    .6    .6    .3    .4    .2    .1    .0    .1    .2    .5    .4    .3
 170.  *    .0    .0    .1    .1    .0    .0    .0    .6    .6    .6    .4    .3    .2    .2    .0    .1    .1    .4    .3    .3
 175.  *    .0    .0    .1    .1    .0    .0    .0    .6    .6    .6    .4    .3    .2    .2    .0    .1    .1    .4    .3    .3
 180.  *    .0    .0    .1    .1    .0    .0    .0    .6    .6    .6    .4    .3    .2    .2    .0    .1    .1    .4    .3    .3
 185.  *    .0    .1    .1    .1    .0    .0    .0    .6    .6    .6    .4    .3    .2    .2    .1    .1    .1    .4    .3    .3
 190.  *    .0    .1    .1    .1    .0    .0    .0    .6    .6    .6    .4    .3    .2    .2    .1    .2    .2    .4    .3    .3
 195.  *    .0    .1    .1    .1    .0    .0    .0    .6    .6    .6    .4    .5    .2    .2    .1    .2    .2    .4    .3    .3
 200.  *    .0    .1    .1    .1    .0    .0    .0    .7    .7    .7    .5    .5    .2    .2    .1    .2    .2    .4    .3    .3
 205.  *    .0    .1    .1    .1    .0    .0    .0    .7    .7    .7    .5    .4    .3    .2    .1    .2    .2    .4    .3    .3
1
                                                                                                                 PAGE  4
      JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT)              RUN: Site 3 Existing AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .1    .1    .1    .0    .0    .0    .7    .7    .7    .5    .3    .3    .3    .1    .2    .2    .3    .4    .4
 215.  *    .0    .1    .1    .1    .0    .0    .0    .7    .7    .7    .6    .4    .3    .2    .1    .2    .2    .3    .4    .4
 220.  *    .0    .1    .1    .1    .0    .0    .0    .7    .7    .6    .5    .4    .3    .2    .0    .2    .2    .3    .4    .4
 225.  *    .0    .1    .1    .1    .0    .0    .0    .8    .7    .7    .7    .4    .3    .2    .0    .2    .2    .3    .4    .4
 230.  *    .0    .1    .1    .1    .0    .0    .0    .8    .7    .7    .7    .4    .3    .1    .0    .1    .2    .4    .4    .4
 235.  *    .0    .1    .1    .0    .0    .1    .1    .7    .8    .8    .6    .4    .2    .1    .0    .1    .2    .4    .4    .4
 240.  *    .0    .1    .1    .0    .1    .1    .1    .7    .7    .5    .5    .4    .2    .1    .0    .0    .1    .4    .4    .4
 245.  *    .0    .1    .1    .2    .2    .1    .1    .7    .7    .6    .5    .2    .1    .1    .0    .0    .1    .3    .4    .4
 250.  *    .0    .1    .1    .2    .4    .3    .2    .6    .6    .6    .5    .2    .1    .1    .0    .0    .0    .3    .4    .4
 255.  *    .0    .1    .2    .3    .5    .5    .3    .5    .4    .4    .4    .1    .1    .1    .0    .0    .0    .2    .3    .3
 260.  *    .0    .1    .2    .4    .5    .5    .3    .4    .3    .2    .2    .1    .1    .1    .0    .0    .0    .1    .2    .2
 265.  *    .0    .2    .3    .4    .5    .3    .6    .3    .1    .2    .2    .1    .1    .1    .0    .0    .0    .1    .1    .1
 270.  *    .0    .2    .3    .5    .4    .4    .6    .0    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1
 275.  *    .0    .3    .4    .4    .4    .4    .5    .0    .1    .0    .2    .1    .1    .1    .0    .0    .0    .0    .1    .1
 280.  *    .0    .3    .3    .4    .4    .5    .4    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 285.  *    .0    .2    .3    .3    .4    .4    .4    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 290.  *    .0    .2    .3    .3    .3    .4    .4    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 295.  *    .0    .2    .3    .3    .4    .4    .4    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 300.  *    .0    .3    .3    .3    .4    .4    .4    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 305.  *    .0    .3    .3    .4    .4    .4    .4    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 310.  *    .0    .3    .3    .4    .4    .4    .5    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 315.  *    .0    .2    .2    .4    .4    .4    .4    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 320.  *    .0    .1    .1    .4    .4    .4    .4    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 325.  *    .0    .1    .1    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .1    .2    .5    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .1    .2    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0
 340.  *    .0    .1    .2    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 345.  *    .0    .2    .3    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 350.  *    .0    .3    .3    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0
 355.  *    .0    .3    .3    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0
 360.  *    .0    .3    .3    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .0    .3    .4    .6    .6    .5    .6    .9    .9    .9    .8    .5    .3    .3    .1    .3    .4    .6    .6    .6
 DEGR. *     0     0   275    50    40     5   265    85    85    85    80   195    95   210    95   105    90    80    75    80

1
                                                                                                                 PAGE  5
      JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT)              RUN: Site 3 Existing AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .3    .4    .5    .2    .2    .2    .1
```

```
   5.  *    .0    .3    .4    .4    .3    .3    .4    .0
  10.  *    .0    .3    .4    .4    .4    .3    .4    .0
  15.  *    .0    .3    .5    .5    .4    .4    .4    .0
  20.  *    .0    .3    .5    .5    .4    .4    .3    .1
  25.  *    .0    .4    .5    .4    .4    .4    .3    .1
  30.  *    .0    .4    .5    .5    .4    .4    .3    .1
  35.  *    .0    .4    .5    .5    .4    .4    .3    .0
  40.  *    .0    .4    .6    .6    .5    .3    .4    .0
  45.  *    .0    .4    .7    .6    .5    .4    .4    .0
  50.  *    .1    .5    .6    .6    .5    .4    .4    .0
  55.  *    .1    .6    .7    .7    .5    .4    .2    .0
  60.  *    .1    .6    .7    .7    .4    .4    .1    .0
  65.  *    .2    .5    .7    .6    .4    .2    .1    .0
  70.  *    .3    .5    .5    .5    .4    .2    .1    .0
  75.  *    .4    .4    .5    .3    .2    .1    .1    .0
  80.  *    .5    .2    .2    .2    .1    .1    .1    .0
  85.  *    .4    .1    .1    .2    .1    .1    .1    .0
  90.  *    .3    .1    .1    .0    .0    .1    .1    .0
  95.  *    .4    .1    .1    .0    .0    .1    .1    .0
 100.  *    .4    .0    .0    .0    .1    .1    .1    .0
 105.  *    .4    .0    .0    .0    .1    .1    .1    .0
 110.  *    .4    .0    .0    .0    .1    .1    .1    .0
 115.  *    .3    .0    .0    .0    .1    .1    .1    .0
 120.  *    .3    .0    .0    .0    .1    .1    .1    .0
 125.  *    .3    .0    .0    .0    .1    .1    .0    .0
 130.  *    .3    .0    .0    .0    .1    .1    .0    .0
 135.  *    .3    .0    .0    .0    .1    .1    .0    .0
 140.  *    .3    .0    .0    .0    .1    .1    .0    .0
 145.  *    .3    .0    .0    .0    .1    .1    .0    .0
 150.  *    .3    .0    .0    .0    .0    .0    .0    .0
 155.  *    .3    .0    .0    .0    .0    .0    .0    .0
 160.  *    .3    .0    .0    .0    .0    .0    .0    .0
 165.  *    .3    .0    .0    .0    .0    .0    .0    .0
 170.  *    .3    .0    .0    .0    .0    .0    .0    .0
 175.  *    .3    .0    .0    .0    .0    .0    .0    .0
 180.  *    .3    .0    .0    .0    .0    .0    .0    .0
 185.  *    .3    .0    .0    .0    .0    .0    .0    .0
 190.  *    .3    .0    .0    .0    .0    .0    .0    .0
 195.  *    .3    .0    .0    .0    .0    .0    .0    .0
 200.  *    .3    .0    .0    .0    .0    .0    .0    .0
 205.  *    .3    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
      JOB: Site 3 Glendon & Wilshire (S3EXAM.DAT)               RUN: Site 3 Existing AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .4    .0    .0    .0    .0    .0    .0    .0
 215.  *    .4    .0    .0    .0    .0    .0    .0    .0
 220.  *    .4    .0    .0    .0    .0    .0    .0    .0
 225.  *    .4    .1    .0    .0    .0    .0    .0    .0
 230.  *    .4    .1    .0    .0    .0    .0    .0    .0
 235.  *    .4    .1    .1    .1    .0    .0    .0    .0
 240.  *    .4    .2    .1    .2    .0    .0    .0    .0
 245.  *    .4    .2    .3    .2    .2    .0    .0    .0
 250.  *    .4    .3    .3    .2    .2    .0    .0    .0
 255.  *    .2    .4    .4    .5    .3    .1    .0    .0
 260.  *    .2    .5    .5    .5    .5    .1    .0    .0
 265.  *    .1    .5    .5    .5    .5    .2    .1    .0
 270.  *    .1    .5    .5    .5    .5    .2    .1    .0
 275.  *    .1    .4    .4    .5    .6    .2    .2    .0
 280.  *    .0    .4    .4    .5    .5    .3    .2    .0
 285.  *    .0    .4    .4    .5    .5    .3    .2    .0
 290.  *    .0    .4    .3    .5    .5    .2    .2    .0
 295.  *    .0    .4    .3    .5    .5    .2    .1    .0
 300.  *    .0    .4    .3    .5    .5    .2    .1    .0
 305.  *    .0    .3    .4    .5    .5    .3    .1    .0
 310.  *    .0    .3    .4    .5    .5    .2    .2    .0
 315.  *    .0    .3    .4    .5    .3    .2    .2    .0
 320.  *    .0    .3    .3    .5    .3    .2    .2    .0
 325.  *    .0    .3    .3    .5    .3    .2    .1    .0
 330.  *    .0    .3    .3    .5    .4    .2    .1    .0
 335.  *    .0    .3    .4    .5    .4    .1    .1    .0
 340.  *    .0    .3    .4    .5    .5    .1    .0    .0
 345.  *    .0    .3    .4    .5    .4    .2    .0    .0
 350.  *    .0    .3    .4    .5    .3    .1    .0    .0
 355.  *    .0    .3    .4    .5    .3    .2    .2    .1
 360.  *    .0    .3    .4    .5    .2    .2    .2    .1
 ------*------------------------------------------------
 MAX   *    .5    .6    .7    .7    .6    .4    .4    .1
 DEGR. *   80    55    45    55   275    15     5     0

 THE HIGHEST CONCENTRATION IS     .90 PPM AT   85 DEGREES FROM REC8 .
 THE 2ND HIGHEST CONCENTRATION IS     .90 PPM AT   85 DEGREES FROM REC9 .
 THE 3RD HIGHEST CONCENTRATION IS     .90 PPM AT   85 DEGREES FROM REC10.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT)               RUN: Site 3 Existing PM
      DATE: 03/22/2010   TIME: 09:47:43.86


       SITE & METEOROLOGICAL VARIABLES
       --------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W   V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *    323.0     617.0    -426.0     376.0 *     787.   252. AG   1996.   3.3    .0 68.0
       2. EB        Wil T+R   *    323.0     616.0     531.0     681.0 *     218.    73. AG   1842.   3.3    .0 68.0
       3. EB        Wil T+R   *    475.0     663.0     340.4     621.5 *     141.   253. AG     82. 100.0    .0 48.0  .76   7.2
       4. EB        Wil LT    *    315.0     650.0     513.0     712.0 *     207.    73. AG    154.   3.3    .0 44.0
       5. EB        Wil LT    *    444.0     690.0     365.9     666.0 *      82.   253. AG      1. 100.0    .0 24.0 1.04   4.2
       6. EB        Wil DP    *    532.0     683.0    1471.0     989.0 *     988.    72. AG   2144.   3.3    .0 68.0
       7. WB        Wil AP    *    756.0     830.0    1454.0    1051.0 *     732.    72. AG   2124.   3.3    .0 68.0
       8. WB        Wil T+R   *    756.0     829.0     484.0     742.0 *     286.   252. AG   2044.   3.3    .0 68.0
       9. WB        Wil T+R   *    540.0     760.0    1164.2     959.3 *     655.    72. AG    109. 100.0    .0 48.0 1.07  33.3
      10. WB        Wil LT    *    767.0     790.0     513.0     706.0 *     268.   252. AG     80.   3.3    .0 32.0
      11. WB        Wil LT    *    566.0     723.0    1196.3     931.0 *     664.    72. AG     27. 100.0    .0 12.0 3.33  33.7
      12. WB        Wil DP    *    483.0     742.0    -451.0     441.0 *     981.   252. AG   2158.   3.3    .0 68.0
      13. NB        Gln AP    *    542.0     703.0     861.0    -211.0 *     968.   161. AG    367.   3.5    .0 32.0
      14. NB        Gln AP    *    564.0     640.0    1288.8   -1440.6 *    2203.   161. AG     36. 100.0    .0 12.0 2.07 111.9
      15. NB        Gln DP    *    545.0     705.0    -160.0    1462.0 *    1034.   317. AG    531.   3.5    .0 32.0
      16. SB        Gln AP    *    305.0     915.0    -182.0    1445.0 *     720.   317. AG    797.   3.5    .0 32.0
      17. SB        Gln T+LT  *    305.0     915.0     479.0     736.0 *     250.   136. AG    547.   3.5    .0 44.0
      18. SB        Gln T+LT  *    430.0     786.0     194.3    1028.4 *     338.   316. AG     73. 100.0    .0 24.0 1.04  17.2
      19. SB        Gln R     *    300.0     890.0     443.0     732.0 *     213.   138. AG    250.   3.5    .0 32.0
      20. SB        Gln R     *    400.0     780.0     322.3     866.4 *     116.   318. AG     31. 100.0    .0 12.0  .62   5.9
      21. SB        Gln DP    *    478.0     734.0     548.0     638.0 *     119.   144. AG    451.   3.5    .0 32.0
      22. SB        Gln DP    *    548.0     638.0     840.0    -220.0 *     906.   161. AG    451.   3.5    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT)               RUN: Site 3 Existing PM
      DATE: 03/22/2010   TIME: 09:47:43.86

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R   *    150      56       2.0      1842      1008      20.50      1        3
       5. EB        Wil LT    *    150     124       2.0       154       510        .20      4        1
       9. WB        Wil T+R   *    150      74       2.0      2044       994      20.50      1        3
      11. WB        Wil LT    *    150      74       2.0        80        50      20.50      1        3
      14. NB        Gln AP    *    150      99       2.0       367       566      20.50      1        3
      18. SB        Gln T+LT  *    150      99       2.0       547       838      20.50      1        3
      20. SB        Gln R     *    150      85       2.0       250      1000      20.50      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       685.0      365.0        5.0    *
      2. SE 164 S             *       638.0      508.0        5.0    *
      3. SE 82 S              *       611.0      586.0        5.0    *
      4. SE CNR               *       595.0      659.0        5.0    *
      5. SE 82 E              *       664.0      689.0        5.0    *
      6. SE 164 E             *       742.0      713.0        5.0    *
      7. SE MID E             *       849.0      747.0        5.0    *
      8. NE MID E             *       793.0      878.0        5.0    *
      9. NE 164 E             *       674.0      839.0        5.0    *
     10. NE 82 E              *       595.0      813.0        5.0    *
     11. NE CNR               *       515.0      792.0        5.0    *
     12. NE 82 N              *       452.0      847.0        5.0    *
     13. NE 164 N             *       396.0      907.0        5.0    *
     14. NE MID N             *       319.0      990.0        5.0    *
     15. NW MID N             *       190.0      983.0        5.0    *
     16. NW 164 N             *       267.0      900.0        5.0    *
     17. NW 82 N              *       323.0      841.0        5.0    *
     18. NW CNR               *       381.0      759.0        5.0    *
     19. NW 82 W              *       299.0      719.0        5.0    *
     20. NW 164 W             *       222.0      694.0        5.0    *
     21. NW MID W             *       107.0      658.0        5.0    *
     22. SW MID W             *       213.0      548.0        5.0    *
     23. SW 164 W             *       367.0      595.0        5.0    *
     24. SW 82 W              *       447.0      619.0        5.0    *
     25. SW CNR               *       518.0      634.0        5.0    *
     26. SW 82 S              *       550.0      565.0        5.0    *
     27. SW 164 S             *       577.0      487.0        5.0    *
     28. SW MID S             *       622.0      354.0        5.0    *
1
                                                                                                                 PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT)               RUN: Site 3 Existing PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .1    .2    .3    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .2    .3    .3    .2    .1    .0
   5.  *    .1    .2    .3    .4    .5    .4    .4    .0    .0    .0    .0    .0    .0    .0    .2    .3    .3    .2    .1    .0
  10.  *    .1    .2    .3    .4    .5    .5    .5    .0    .0    .0    .0    .0    .0    .0    .2    .3    .3    .2    .1    .0
  15.  *    .1    .2    .3    .4    .5    .5    .5    .0    .0    .0    .0    .0    .0    .0    .2    .3    .3    .2    .1    .0
  20.  *    .1    .2    .3    .5    .5    .5    .5    .0    .0    .0    .0    .0    .0    .0    .2    .3    .3    .2    .1    .0
  25.  *    .1    .2    .3    .5    .5    .5    .5    .0    .0    .0    .0    .0    .0    .0    .2    .3    .3    .1    .1    .1
  30.  *    .0    .2    .2    .5    .6    .5    .5    .0    .0    .0    .0    .0    .0    .0    .2    .3    .3    .1    .1    .1
  35.  *    .0    .3    .2    .5    .7    .6    .6    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .1    .0
  40.  *    .0    .3    .3    .6    .6    .6    .6    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .1    .0
  45.  *    .0    .3    .3    .7    .6    .6    .5    .0    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .1    .0
  50.  *    .0    .1    .3    .6    .6    .6    .5    .1    .0    .0    .0    .0    .0    .0    .3    .3    .3    .1    .1    .1
  55.  *    .0    .1    .3    .5    .5    .5    .5    .2    .1    .2    .1    .0    .0    .0    .3    .3    .3    .1    .1    .1
  60.  *    .0    .0    .3    .5    .5    .5    .5    .2    .3    .3    .2    .0    .0    .0    .3    .2    .3    .2    .2    .1
  65.  *    .0    .0    .1    .5    .5    .5    .5    .3    .4    .4    .4    .0    .0    .0    .3    .2    .3    .3    .2    .3
  70.  *    .0    .0    .1    .4    .5    .5    .4    .4    .5    .6    .4    .0    .0    .0    .3    .2    .3    .3    .5    .3
  75.  *    .0    .0    .0    .2    .2    .2    .2    .7    .7    .7    .7    .2    .0    .0    .3    .2    .5    .6    .5    .4
  80.  *    .0    .0    .0    .1    .2    .2    .2    .7    .8    .8    .8    .2    .0    .0    .3    .2    .5    .6    .5    .5
  85.  *    .0    .0    .0    .1    .1    .1    .1    .8    .8    .8    .8    .3    .2    .0    .3    .3    .7    .5    .6    .5
  90.  *    .0    .0    .0    .0    .1    .1    .1    .8    .9    .9    .9    .5    .3    .0    .3    .3    .6    .4    .6    .6
  95.  *    .0    .0    .0    .0    .1    .1    .0    .8    .8    .8    .8    .5    .3    .1    .4    .4    .7    .4    .4    .6
 100.  *    .0    .0    .0    .0    .0    .0    .0    .8    .8    .8    .7    .4    .2    .1    .4    .5    .7    .4    .5    .5
 105.  *    .0    .0    .0    .0    .0    .0    .0    .8    .8    .7    .6    .4    .2    .1    .4    .5    .6    .4    .5    .5
 110.  *    .0    .0    .0    .0    .0    .0    .0    .8    .8    .7    .6    .4    .3    .1    .4    .5    .6    .4    .5    .5
 115.  *    .0    .0    .0    .0    .0    .0    .0    .7    .7    .7    .6    .3    .3    .1    .4    .4    .6    .3    .4    .4
 120.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .7    .6    .3    .3    .1    .2    .2    .2    .3    .4    .4
 125.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .5    .3    .3    .1    .2    .1    .3    .3    .4    .3
 130.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .5    .3    .3    .1    .1    .1    .3    .3    .4    .3
 135.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .5    .3    .2    .0    .1    .1    .2    .4    .4    .3
 140.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .5    .3    .1    .0    .1    .1    .1    .4    .4    .3
 145.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .4    .2    .1    .2    .0    .1    .2    .4    .4    .3
 150.  *    .0    .0    .0    .0    .0    .0    .0    .6    .6    .6    .4    .2    .1    .2    .0    .1    .3    .4    .4    .3
 155.  *    .1    .1    .1    .1    .0    .0    .0    .6    .6    .6    .4    .2    .1    .2    .0    .1    .3    .4    .4    .3
 160.  *    .1    .1    .1    .1    .0    .0    .0    .6    .6    .6    .4    .2    .3    .2    .0    .1    .3    .4    .3    .3
 165.  *    .2    .1    .1    .1    .0    .0    .0    .6    .6    .6    .4    .2    .3    .2    .0    .1    .2    .4    .3    .3
 170.  *    .2    .2    .2    .1    .0    .0    .0    .6    .6    .6    .3    .3    .3    .3    .0    .1    .1    .4    .3    .3
 175.  *    .2    .2    .2    .1    .0    .0    .0    .6    .6    .6    .3    .3    .3    .3    .0    .1    .1    .4    .3    .3
 180.  *    .2    .2    .2    .1    .0    .0    .0    .6    .6    .6    .3    .3    .3    .3    .0    .1    .1    .4    .3    .3
 185.  *    .2    .2    .2    .1    .0    .0    .0    .6    .6    .6    .3    .4    .3    .3    .0    .1    .1    .4    .3    .3
 190.  *    .2    .2    .1    .1    .0    .0    .0    .6    .6    .6    .3    .4    .3    .3    .0    .1    .1    .4    .3    .3
 195.  *    .2    .1    .1    .1    .0    .0    .0    .6    .6    .6    .3    .4    .3    .3    .1    .1    .2    .4    .3    .3
 200.  *    .1    .1    .1    .1    .0    .0    .0    .6    .6    .6    .5    .5    .3    .3    .1    .2    .2    .3    .3    .3
 205.  *    .1    .1    .1    .1    .0    .0    .0    .7    .6    .6    .5    .3    .3    .3    .1    .2    .2    .3    .3    .3
1
                                                                                                                 PAGE  4
      JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT)               RUN: Site 3 Existing PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .1    .0    .0    .0    .8    .7    .7    .4    .3    .4    .3    .1    .2    .2    .3    .4    .4
 215.  *    .1    .1    .1    .1    .0    .0    .0    .8    .7    .6    .4    .3    .4    .3    .1    .2    .2    .3    .4    .4
 220.  *    .1    .1    .1    .1    .0    .0    .0    .8    .8    .6    .4    .4    .4    .3    .0    .2    .2    .3    .4    .4
 225.  *    .1    .1    .1    .0    .0    .0    .0    .7    .8    .8    .5    .4    .4    .3    .0    .1    .2    .3    .4    .4
 230.  *    .1    .1    .1    .0    .0    .0    .0    .8    .6    .7    .6    .4    .4    .2    .0    .1    .2    .4    .4    .4
 235.  *    .1    .1    .1    .0    .1    .1    .1    .8    .7    .7    .4    .4    .3    .2    .0    .1    .2    .4    .4    .4
 240.  *    .1    .1    .1    .0    .1    .1    .1    .9    .7    .6    .4    .4    .3    .2    .0    .0    .1    .4    .4    .4
 245.  *    .1    .1    .1    .1    .1    .1    .1    .7    .6    .6    .4    .3    .2    .2    .0    .0    .1    .3    .4    .4
 250.  *    .1    .1    .1    .3    .4    .3    .2    .5    .5    .6    .4    .3    .2    .2    .0    .0    .0    .3    .4    .4
 255.  *    .1    .1    .2    .4    .6    .4    .3    .5    .4    .3    .2    .2    .2    .2    .0    .0    .0    .2    .3    .3
 260.  *    .1    .1    .2    .5    .6    .3    .4    .4    .3    .2    .1    .2    .2    .2    .0    .0    .0    .1    .2    .2
 265.  *    .1    .1    .3    .5    .5    .4    .6    .2    .2    .2    .2    .2    .2    .3    .0    .0    .0    .1    .1    .1
 270.  *    .1    .2    .3    .4    .4    .4    .6    .0    .1    .2    .1    .2    .2    .3    .0    .0    .0    .0    .1    .1
 275.  *    .1    .3    .5    .4    .4    .6    .5    .0    .0    .1    .2    .2    .2    .3    .0    .0    .0    .0    .1    .1
 280.  *    .1    .3    .4    .4    .3    .5    .5    .0    .0    .1    .2    .2    .2    .3    .0    .0    .0    .0    .0    .0
 285.  *    .1    .2    .4    .3    .4    .5    .5    .0    .0    .1    .2    .2    .2    .3    .0    .0    .0    .0    .0    .0
 290.  *    .1    .2    .4    .3    .3    .4    .6    .0    .0    .1    .2    .2    .2    .3    .0    .0    .0    .0    .0    .0
 295.  *    .1    .2    .4    .3    .4    .4    .5    .0    .0    .1    .2    .2    .3    .2    .0    .0    .0    .0    .0    .0
 300.  *    .1    .3    .3    .4    .4    .4    .5    .0    .0    .0    .2    .2    .3    .2    .0    .0    .0    .0    .0    .0
 305.  *    .2    .3    .3    .5    .4    .4    .5    .0    .0    .0    .2    .2    .3    .2    .0    .0    .0    .0    .0    .0
 310.  *    .2    .3    .3    .5    .4    .4    .6    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0
 315.  *    .2    .1    .2    .5    .4    .4    .4    .0    .0    .0    .1    .1    .1    .1    .0    .0    .1    .1    .0    .0
 320.  *    .2    .1    .0    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
 325.  *    .2    .1    .1    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
 330.  *    .2    .1    .2    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
 335.  *    .1    .0    .2    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .1    .2    .3    .2    .0    .0
 340.  *    .1    .1    .3    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .1    .3    .3    .2    .0    .0
 345.  *    .0    .2    .3    .4    .5    .4    .4    .0    .0    .0    .0    .0    .0    .0    .1    .3    .2    .2    .0    .0
 350.  *    .0    .3    .3    .4    .5    .5    .4    .0    .0    .0    .0    .0    .0    .0    .1    .3    .2    .2    .1    .0
 355.  *    .1    .3    .3    .4    .5    .4    .4    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .1    .0
 360.  *    .1    .2    .3    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .2    .3    .3    .2    .1    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .2    .3    .5    .7    .7    .6    .6    .9    .9    .9    .9    .5    .4    .3    .4    .5    .7    .6    .6    .6
 DEGR. *  165    35   275    45    35    35    35   240    90    90    90    90   210   170    95   100    85    75    85    90

1
                                                                                                                 PAGE  5
      JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT)               RUN: Site 3 Existing PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .3    .6    .5    .3    .3    .4    .2
```

```
   5.  *    .0    .3    .5    .5    .5    .4    .4    .3
  10.  *    .0    .3    .5    .5    .5    .4    .4    .3
  15.  *    .0    .3    .5    .5    .4    .4    .4    .3
  20.  *    .0    .3    .6    .6    .4    .4    .4    .3
  25.  *    .0    .3    .6    .5    .4    .5    .4    .4
  30.  *    .0    .3    .6    .6    .4    .5    .4    .4
  35.  *    .0    .3    .6    .6    .6    .4    .4    .3
  40.  *    .0    .3    .8    .6    .6    .4    .4    .2
  45.  *    .0    .3    .7    .6    .5    .5    .5    .2
  50.  *    .1    .4    .8    .6    .6    .4    .4    .1
  55.  *    .1    .6    .7    .8    .7    .4    .3    .2
  60.  *    .1    .7    .7    .8    .5    .5    .3    .2
  65.  *    .2    .6    .6    .6    .4    .3    .2    .2
  70.  *    .3    .6    .5    .4    .4    .3    .2    .2
  75.  *    .5    .4    .5    .3    .2    .2    .2    .2
  80.  *    .5    .2    .3    .2    .1    .2    .2    .2
  85.  *    .5    .1    .2    .2    .1    .2    .2    .2
  90.  *    .3    .1    .1    .0    .0    .2    .2    .2
  95.  *    .3    .0    .0    .0    .0    .2    .2    .2
 100.  *    .4    .0    .0    .0    .0    .2    .2    .2
 105.  *    .4    .0    .0    .0    .0    .2    .2    .2
 110.  *    .4    .0    .0    .0    .1    .2    .2    .2
 115.  *    .3    .0    .0    .0    .1    .2    .2    .2
 120.  *    .3    .0    .0    .0    .1    .2    .2    .2
 125.  *    .3    .0    .0    .0    .1    .2    .2    .2
 130.  *    .3    .0    .0    .0    .2    .2    .2    .2
 135.  *    .3    .0    .0    .0    .2    .2    .2    .2
 140.  *    .3    .0    .0    .0    .2    .2    .2    .2
 145.  *    .3    .0    .0    .0    .2    .2    .2    .2
 150.  *    .3    .0    .0    .0    .2    .2    .2    .2
 155.  *    .3    .0    .0    .0    .2    .2    .2    .2
 160.  *    .3    .0    .0    .0    .1    .2    .2    .2
 165.  *    .3    .0    .0    .0    .0    .2    .2    .2
 170.  *    .3    .0    .0    .0    .0    .0    .0    .0
 175.  *    .3    .0    .0    .0    .0    .0    .0    .0
 180.  *    .3    .0    .0    .0    .0    .0    .0    .0
 185.  *    .3    .0    .0    .0    .0    .0    .0    .0
 190.  *    .3    .0    .0    .0    .0    .0    .0    .0
 195.  *    .3    .0    .0    .0    .0    .0    .0    .0
 200.  *    .3    .0    .0    .0    .0    .0    .0    .0
 205.  *    .3    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  6
      JOB: Site 3 Glendon & Wilshire (S3EXPM.DAT)               RUN: Site 3 Existing PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .4    .0    .0    .0    .0    .0    .0    .0
 215.  *    .4    .0    .0    .0    .0    .0    .0    .0
 220.  *    .4    .0    .0    .0    .0    .0    .0    .0
 225.  *    .4    .1    .0    .0    .0    .0    .0    .0
 230.  *    .4    .1    .0    .0    .0    .0    .0    .0
 235.  *    .4    .1    .1    .0    .0    .0    .0    .0
 240.  *    .4    .1    .1    .2    .0    .0    .0    .0
 245.  *    .4    .2    .2    .2    .2    .0    .0    .0
 250.  *    .3    .3    .3    .3    .3    .0    .0    .0
 255.  *    .2    .4    .4    .4    .4    .1    .0    .0
 260.  *    .2    .4    .4    .5    .5    .1    .0    .0
 265.  *    .1    .4    .4    .6    .6    .2    .0    .0
 270.  *    .1    .4    .4    .6    .6    .2    .1    .0
 275.  *    .1    .4    .4    .6    .6    .2    .2    .0
 280.  *    .0    .4    .4    .6    .5    .2    .2    .0
 285.  *    .0    .4    .4    .6    .5    .3    .2    .0
 290.  *    .0    .4    .4    .6    .5    .3    .1    .0
 295.  *    .0    .3    .4    .6    .4    .3    .1    .0
 300.  *    .0    .3    .4    .6    .4    .3    .1    .0
 305.  *    .0    .3    .4    .6    .4    .3    .1    .0
 310.  *    .0    .3    .5    .5    .4    .3    .3    .0
 315.  *    .0    .3    .4    .5    .5    .3    .3    .0
 320.  *    .0    .3    .4    .5    .4    .3    .3    .0
 325.  *    .0    .3    .5    .5    .4    .2    .1    .0
 330.  *    .0    .3    .5    .6    .4    .2    .1    .0
 335.  *    .0    .3    .5    .6    .4    .1    .0    .0
 340.  *    .0    .3    .5    .6    .3    .1    .0    .0
 345.  *    .0    .3    .5    .6    .3    .1    .0    .1
 350.  *    .0    .3    .6    .6    .4    .1    .1    .2
 355.  *    .0    .3    .6    .5    .4    .2    .1    .2
 360.  *    .0    .3    .6    .5    .3    .3    .4    .2
 ------*------------------------------------------------
 MAX   *    .5    .7    .8    .8    .7    .5    .5    .4
 DEGR. *   75    60    40    60    55    25    45    25

 THE HIGHEST CONCENTRATION IS     .90 PPM AT  240 DEGREES FROM REC8 .
 THE 2ND HIGHEST CONCENTRATION IS     .90 PPM AT   90 DEGREES FROM REC9 .
 THE 3RD HIGHEST CONCENTRATION IS     .90 PPM AT   90 DEGREES FROM REC10.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT)               RUN: Site 3 NO BUILD AM
      DATE: 03/22/2010   TIME: 10:01:38.62


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *    323.0     617.0    -426.0     376.0 *     787.   252. AG   2967.    .8    .0 68.0
       2. EB        Wil T+R   *    323.0     616.0     531.0     681.0 *     218.    73. AG   2763.    .8    .0 68.0
       3. EB        Wil T+R   *    475.0     663.0     242.0     591.2 *     244.   253. AG     11. 100.0    .0 48.0  .98  12.4
       4. EB        Wil LT    *    315.0     650.0     513.0     712.0 *     207.    73. AG    204.    .8    .0 44.0
       5. EB        Wil LT    *    444.0     690.0    -678.9     345.2 *    1175.   253. AG     19. 100.0    .0 24.0 ****  59.7
       6. EB        Wil DP    *    532.0     683.0    1471.0     989.0 *     988.    72. AG   2497.    .8    .0 68.0
       7. WB        Wil AP    *    756.0     830.0    1454.0    1051.0 *     732.    72. AG   3144.    .8    .0 68.0
       8. WB        Wil T+R   *    756.0     829.0     484.0     742.0 *     286.   252. AG   3048.    .8    .0 68.0
       9. WB        Wil T+R   *    540.0     760.0    2886.6    1509.1 *    2463.    72. AG     18. 100.0    .0 48.0 1.38 125.1
      10. WB        Wil LT    *    767.0     790.0     513.0     706.0 *     268.   252. AG     96.    .8    .0 32.0
      11. WB        Wil LT    *    566.0     723.0    1295.5     963.7 *     768.    72. AG      5. 100.0    .0 12.0 3.20  39.0
      12. WB        Wil DP    *    483.0     742.0    -451.0     441.0 *     981.   252. AG   2816.    .8    .0 68.0
      13. NB        Gln AP    *    542.0     703.0     861.0    -211.0 *     968.   161. AG    311.    .9    .0 32.0
      14. NB        Gln AP    *    564.0     640.0    1803.0   -2916.8 *    3766.   161. AG      9. 100.0    .0 12.0 **** 191.3
      15. NB        Gln DP    *    545.0     705.0    -160.0    1462.0 *    1034.   317. AG    898.    .9    .0 32.0
      16. SB        Gln AP    *    305.0     915.0    -182.0    1445.0 *     720.   317. AG    540.    .9    .0 32.0
      17. SB        Gln T+LT  *    305.0     915.0     479.0     736.0 *     250.   136. AG    336.    .9    .0 44.0
      18. SB        Gln T+LT  *    430.0     786.0     157.5    1066.2 *     391.   316. AG     17. 100.0    .0 24.0 1.15  19.9
      19. SB        Gln R     *    300.0     890.0     443.0     732.0 *     213.   138. AG    204.    .9    .0 32.0
      20. SB        Gln R     *    400.0     780.0     326.9     861.3 *     109.   318. AG      7. 100.0    .0 12.0  .40   5.6
      21. SB        Gln DP    *    478.0     734.0     548.0     638.0 *     119.   144. AG    751.    .9    .0 32.0
      22. SB        Gln DP    *    548.0     638.0     840.0    -220.0 *     906.   161. AG    751.    .9    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT)               RUN: Site 3 NO BUILD AM
      DATE: 03/22/2010   TIME: 10:01:38.62

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R   *     150       39       2.0      2763        992       4.10      1        3
       5. EB        Wil LT    *     150      130       2.0       204         84       4.10      1        3
       9. WB        Wil T+R   *     150       62       2.0      3048        990       4.10      1        3
      11. WB        Wil LT    *     150       62       2.0        96         54       4.10      1        3
      14. NB        Gln AP    *     150      116       2.0       311         39       4.10      1        3
      18. SB        Gln T+LT  *     150      116       2.0       336        731       4.10      1        3
      20. SB        Gln R     *     150       98       2.0       204       1600       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       685.0      365.0        5.0   *
      2. SE 164 S             *       638.0      508.0        5.0   *
      3. SE 82 S              *       611.0      586.0        5.0   *
      4. SE CNR               *       595.0      659.0        5.0   *
      5. SE 82 E              *       664.0      689.0        5.0   *
      6. SE 164 E             *       742.0      713.0        5.0   *
      7. SE MID E             *       849.0      747.0        5.0   *
      8. NE MID E             *       793.0      878.0        5.0   *
      9. NE 164 E             *       674.0      839.0        5.0   *
     10. NE 82 E              *       595.0      813.0        5.0   *
     11. NE CNR               *       515.0      792.0        5.0   *
     12. NE 82 N              *       452.0      847.0        5.0   *
     13. NE 164 N             *       396.0      907.0        5.0   *
     14. NE MID N             *       319.0      990.0        5.0   *
     15. NW MID N             *       190.0      983.0        5.0   *
     16. NW 164 N             *       267.0      900.0        5.0   *
     17. NW 82 N              *       323.0      841.0        5.0   *
     18. NW CNR               *       381.0      759.0        5.0   *
     19. NW 82 W              *       299.0      719.0        5.0   *
     20. NW 164 W             *       222.0      694.0        5.0   *
     21. NW MID W             *       107.0      658.0        5.0   *
     22. SW MID W             *       213.0      548.0        5.0   *
     23. SW 164 W             *       367.0      595.0        5.0   *
     24. SW 82 W              *       447.0      619.0        5.0   *
     25. SW CNR               *       518.0      634.0        5.0   *
     26. SW 82 S              *       550.0      565.0        5.0   *
     27. SW 164 S             *       577.0      487.0        5.0   *
     28. SW MID S             *       622.0      354.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT)               RUN: Site 3 NO BUILD AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
  0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 80.  *    .0    .0    .0    .0    .1    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
140.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
150.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
155.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
160.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
165.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
170.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
175.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
180.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
190.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                   PAGE  4
     JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT)               RUN: Site 3 NO BUILD AM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
225.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
245.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
250.  *    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
255.  *    .0    .0    .0    .0    .0    .1    .1    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
------*------------------------------------------------------------------------------------------------------------------------
MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
DEGR. *     0     0     0     0     0     0     0    70    85    70    70     0     0     0     0     0     0   105    70    70

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                                                                                                                   PAGE  5
     JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT)               RUN: Site 3 NO BUILD AM

      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
   5.  *    .0    .1    .1    .1    .0    .0    .0    .0
  10.  *    .0    .1    .1    .1    .0    .0    .0    .0
  15.  *    .0    .1    .1    .1    .0    .0    .0    .0
  20.  *    .0    .1    .1    .1    .0    .0    .0    .0
  25.  *    .0    .1    .1    .1    .0    .0    .0    .0
  30.  *    .0    .1    .1    .1    .0    .0    .0    .0
  35.  *    .0    .1    .1    .1    .0    .0    .0    .0
  40.  *    .0    .1    .1    .1    .1    .0    .0    .0
  45.  *    .0    .1    .1    .1    .1    .0    .0    .0
  50.  *    .0    .1    .1    .1    .1    .0    .0    .0
  55.  *    .0    .1    .1    .1    .1    .0    .0    .0
  60.  *    .0    .1    .1    .1    .1    .0    .0    .0
  65.  *    .1    .1    .1    .2    .1    .0    .0    .0
  70.  *    .1    .1    .1    .0    .1    .0    .0    .0
  75.  *    .1    .1    .1    .0    .0    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .1    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                          PAGE  6
      JOB: Site 3 Glendon & Wilshire (S3NBAM.DAT)               RUN: Site 3 NO BUILD AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .1    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .1    .0    .0    .0    .0    .0
 250.  *    .1    .1    .1    .0    .0    .0    .0    .0
 255.  *    .1    .1    .1    .1    .0    .0    .0    .0
 260.  *    .1    .1    .1    .2    .1    .0    .0    .0
 265.  *    .0    .1    .1    .1    .1    .0    .0    .0
 270.  *    .0    .1    .1    .1    .1    .0    .0    .0
 275.  *    .0    .1    .1    .1    .1    .0    .0    .0
 280.  *    .0    .1    .1    .1    .1    .0    .0    .0
 285.  *    .0    .1    .1    .1    .1    .0    .0    .0
 290.  *    .0    .1    .0    .1    .1    .0    .0    .0
 295.  *    .0    .1    .0    .1    .1    .0    .0    .0
 300.  *    .0    .1    .0    .1    .1    .0    .0    .0
 305.  *    .0    .1    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .1    .0    .0    .0
 340.  *    .0    .1    .1    .1    .1    .0    .0    .0
 345.  *    .0    .1    .1    .1    .1    .0    .0    .0
 350.  *    .0    .1    .1    .1    .1    .0    .0    .0
 355.  *    .0    .1    .1    .1    .1    .0    .0    .0
 360.  *    .0    .1    .1    .1    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .1    .1    .1    .2    .1    .0    .0    .0
 DEGR. *   65     0     0    65    40     0     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   85 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC8 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC10.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT)               RUN: Site 3 NO BUILD PM
      DATE: 03/22/2010   TIME: 10:12:07.35


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *    323.0     617.0    -426.0     376.0 *     787.  252. AG    2690.    .8    .0 68.0
       2. EB        Wil T+R   *    323.0     616.0     531.0     681.0 *     218.   73. AG    2457.    .8    .0 68.0
       3. EB        Wil T+R   *    475.0     663.0   -6884.3   -1605.3 *    7701.  253. AG      16. 100.0    .0 48.0 **** 391.2
       4. EB        Wil LT    *    315.0     650.0     513.0     712.0 *     207.   73. AG     233.    .8    .0 44.0
       5. EB        Wil LT    *    444.0     690.0    -822.3     301.1 *    1325.  253. AG      19. 100.0    .0 24.0 ****  67.3
       6. EB        Wil DP    *    532.0     683.0    1471.0     989.0 *     988.   72. AG    2819.    .8    .0 68.0
       7. WB        Wil AP    *    756.0     830.0    1454.0    1051.0 *     732.   72. AG    2887.    .8    .0 68.0
       8. WB        Wil T+R   *    756.0     829.0     484.0     742.0 *     286.  252. AG    2754.    .8    .0 68.0
       9. WB        Wil T+R   *    540.0     760.0    3281.3    1635.2 *    2878.   72. AG      23. 100.0    .0 48.0 1.56 146.2
      10. WB        Wil LT    *    767.0     790.0     513.0     706.0 *     268.  252. AG     133.    .8    .0 32.0
      11. WB        Wil LT    *    566.0     723.0    1696.4    1096.0 *    1190.   72. AG       6. 100.0    .0 12.0 4.43  60.5
      12. WB        Wil DP    *    483.0     742.0    -451.0     441.0 *     981.  252. AG    3052.    .8    .0 68.0
      13. NB        Gln AP    *    542.0     703.0     861.0    -211.0 *     968.  161. AG     899.    .9    .0 32.0
      14. NB        Gln AP    *    564.0     640.0    3512.4   -7823.7 *    8963.  161. AG       7. 100.0    .0 12.0 **** 455.3
      15. NB        Gln DP    *    545.0     705.0    -160.0    1462.0 *    1034.  317. AG     960.    .9    .0 32.0
      16. SB        Gln AP    *    305.0     915.0    -182.0    1445.0 *     720.  317. AG    1017.    .9    .0 32.0
      17. SB        Gln T+LT  *    305.0     915.0     479.0     736.0 *     250.  136. AG     713.    .9    .0 44.0
      18. SB        Gln T+LT  *    430.0     786.0    -430.9    1671.5 *    1235.  316. AG      15. 100.0    .0 24.0 1.36  62.7
      19. SB        Gln R     *    300.0     890.0     443.0     732.0 *     213.  138. AG     304.    .9    .0 32.0
      20. SB        Gln R     *    400.0     780.0     311.0     878.8 *     133.  318. AG       6. 100.0    .0 12.0  .43   6.8
      21. SB        Gln DP    *    478.0     734.0     548.0     638.0 *     119.  144. AG     662.    .9    .0 32.0
      22. SB        Gln DP    *    548.0     638.0     840.0    -220.0 *     906.  161. AG     662.    .9    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT)               RUN: Site 3 NO BUILD PM
      DATE: 03/22/2010   TIME: 10:12:07.35

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*-------------------------------------------------------------------------------
       3. EB        Wil T+R   *    150        56       2.0      2457          7       4.10      1        3
       5. EB        Wil LT    *    150       129       2.0       233         84       4.10      1        3
       9. WB        Wil T+R   *    150        79       2.0      2754        991       4.10      1        3
      11. WB        Wil LT    *    150        79       2.0       133         68       4.10      1        3
      14. NB        Gln AP    *    150        99       2.0       899        276       4.10      1        3
      18. SB        Gln T+LT  *    150        99       2.0       713        836       4.10      1        3
      20. SB        Gln R     *    150        80       2.0       304       1600       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
       1. SE MID S            *       685.0      365.0        5.0   *
       2. SE 164 S            *       638.0      508.0        5.0   *
       3. SE 82 S             *       611.0      586.0        5.0   *
       4. SE CNR              *       595.0      659.0        5.0   *
       5. SE 82 E             *       664.0      689.0        5.0   *
       6. SE 164 E            *       742.0      713.0        5.0   *
       7. SE MID E            *       849.0      747.0        5.0   *
       8. NE MID E            *       793.0      878.0        5.0   *
       9. NE 164 E            *       674.0      839.0        5.0   *
      10. NE 82 E             *       595.0      813.0        5.0   *
      11. NE CNR              *       515.0      792.0        5.0   *
      12. NE 82 N             *       452.0      847.0        5.0   *
      13. NE 164 N            *       396.0      907.0        5.0   *
      14. NE MID N            *       319.0      990.0        5.0   *
      15. NW MID N            *       190.0      983.0        5.0   *
      16. NW 164 N            *       267.0      900.0        5.0   *
      17. NW 82 N             *       323.0      841.0        5.0   *
      18. NW CNR              *       381.0      759.0        5.0   *
      19. NW 82 W             *       299.0      719.0        5.0   *
      20. NW 164 W            *       222.0      694.0        5.0   *
      21. NW MID W            *       107.0      658.0        5.0   *
      22. SW MID W            *       213.0      548.0        5.0   *
      23. SW 164 W            *       367.0      595.0        5.0   *
      24. SW 82 W             *       447.0      619.0        5.0   *
      25. SW CNR              *       518.0      634.0        5.0   *
      26. SW 82 S             *       550.0      565.0        5.0   *
      27. SW 164 S            *       577.0      487.0        5.0   *
      28. SW MID S            *       622.0      354.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT)               RUN: Site 3 NO BUILD PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*-------------------------------------------------------------------------------------------------------------------------
  0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 65.  *    .0    .0    .0    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
 70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 80.  *    .0    .0    .0    .0    .1    .1    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
140.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
150.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
155.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
160.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
165.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
170.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
175.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
180.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
185.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
190.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                   PAGE  4
      JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT)               RUN: Site 3 NO BUILD PM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*-------------------------------------------------------------------------------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
225.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
245.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
250.  *    .0    .0    .0    .0    .0    .1    .1    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
255.  *    .0    .0    .0    .0    .1    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
------*-------------------------------------------------------------------------------------------------------------------------
MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
DEGR. *     0     0     0     0     0     0     0    65    90    70    75     0     0     0     0     0     0   100    70    65

1
                                                                                                                   PAGE  5
      JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT)               RUN: Site 3 NO BUILD PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
   5.  *    .0    .1    .1    .1    .0    .0    .0    .0
  10.  *    .0    .1    .1    .1    .0    .0    .0    .0
  15.  *    .0    .1    .1    .1    .0    .0    .0    .0
  20.  *    .0    .2    .2    .1    .0    .0    .0    .0
  25.  *    .0    .2    .2    .1    .0    .0    .0    .0
  30.  *    .0    .2    .2    .1    .0    .0    .0    .0
  35.  *    .0    .2    .2    .1    .1    .0    .0    .0
  40.  *    .0    .2    .2    .1    .1    .0    .0    .0
  45.  *    .0    .2    .2    .1    .1    .0    .0    .0
  50.  *    .0    .2    .2    .1    .1    .0    .0    .0
  55.  *    .0    .2    .1    .1    .1    .0    .0    .0
  60.  *    .0    .2    .1    .2    .1    .0    .0    .0
  65.  *    .1    .2    .1    .1    .1    .0    .0    .0
  70.  *    .1    .1    .1    .1    .1    .0    .0    .0
  75.  *    .1    .0    .1    .0    .1    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .1    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                      PAGE  6
      JOB: Site 3 Glendon & Wilshire (S3NBPM.DAT)               RUN: Site 3 NO BUILD PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .0    .0    .0    .0    .0    .0
 250.  *    .1    .2    .2    .1    .0    .0    .0    .0
 255.  *    .1    .2    .2    .1    .1    .0    .0    .0
 260.  *    .1    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .2    .2    .2    .2    .0    .0    .0
 275.  *    .0    .2    .2    .2    .2    .0    .0    .0
 280.  *    .0    .2    .2    .2    .1    .0    .0    .0
 285.  *    .0    .2    .2    .2    .1    .0    .0    .0
 290.  *    .0    .2    .1    .2    .1    .0    .0    .0
 295.  *    .0    .2    .1    .2    .1    .0    .0    .0
 300.  *    .0    .2    .1    .2    .1    .0    .0    .0
 305.  *    .0    .2    .1    .2    .1    .0    .0    .0
 310.  *    .0    .1    .0    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .1    .0    .0    .0
 340.  *    .0    .1    .1    .1    .1    .0    .0    .0
 345.  *    .0    .1    .1    .1    .1    .0    .0    .0
 350.  *    .0    .1    .1    .1    .1    .0    .0    .0
 355.  *    .0    .1    .1    .1    .0    .0    .0    .0
 360.  *    .0    .1    .1    .1    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .1    .2    .2    .2    .2    .0    .0    .0
 DEGR. *   65    20    20    60   260     0     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   90 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   65 DEGREES FROM REC8 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC10.
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3B1AM.DAT)              RUN: Site 3 BUILD 1  AM
      DATE: 03/22/2010   TIME: 10:42:44.83


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2    *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*---------------------------------------*-----------------------------------------------------------
       1. EB        Wil AP    *   323.0     617.0    -426.0     376.0 *    787.   252. AG  2885.    .8    .0 68.0
       2. EB        Wil T+R   *   323.0     616.0     531.0     681.0 *    218.    73. AG  2690.    .8    .0 68.0
       3. EB        Wil T+R   *   475.0     663.0     274.5     601.2 *    210.   253. AG    11. 100.0    .0 48.0  .95  10.7
       4. EB        Wil LT    *   315.0     650.0     513.0     712.0 *    207.    73. AG   195.    .8    .0 44.0
       5. EB        Wil LT    *   444.0     690.0    -620.2     363.2 *   1113.   253. AG    19. 100.0    .0 24.0 ****  56.6
       6. EB        Wil DP    *   532.0     683.0    1471.0     989.0 *    988.    72. AG  2465.    .8    .0 68.0
       7. WB        Wil AP    *   756.0     830.0    1454.0    1051.0 *    732.    72. AG  3121.    .8    .0 68.0
       8. WB        Wil T+R   *   756.0     829.0     484.0     742.0 *    286.   252. AG  3035.    .8    .0 68.0
       9. WB        Wil T+R   *   540.0     760.0    3199.2    1609.0 *   2791.    72. AG    18. 100.0    .0 48.0 1.47 141.8
      10. WB        Wil LT    *   767.0     790.0     513.0     706.0 *    268.   252. AG    86.    .8    .0 32.0
      11. WB        Wil LT    *   566.0     723.0    1190.3     929.0 *    657.    72. AG     5. 100.0    .0 12.0 2.87  33.4
      12. WB        Wil DP    *   483.0     742.0    -451.0     441.0 *    981.   252. AG  2899.    .8    .0 68.0
      13. NB        Gln AP    *   542.0     703.0     861.0    -211.0 *    968.   161. AG   388.    .9    .0 32.0
      14. NB        Gln AP    *   564.0     640.0    2032.8   -3576.4 *   4465.   161. AG     9. 100.0    .0 12.0 **** 226.8
      15. NB        Gln DP    *   545.0     705.0    -160.0    1462.0 *   1034.   317. AG   929.    .9    .0 32.0
      16. SB        Gln AP    *   305.0     915.0    -182.0    1445.0 *    720.   317. AG   593.    .9    .0 32.0
      17. SB        Gln T+LT  *   305.0     915.0     479.0     736.0 *    250.   136. AG   330.    .9    .0 44.0
      18. SB        Gln T+LT  *   430.0     786.0     103.0    1122.4 *    469.   316. AG    17. 100.0    .0 24.0 1.22  23.8
      19. SB        Gln R     *   300.0     890.0     443.0     732.0 *    213.   138. AG   263.    .9    .0 32.0
      20. SB        Gln R     *   400.0     780.0     305.7     884.8 *    141.   318. AG     7. 100.0    .0 12.0  .51   7.2
      21. SB        Gln DP    *   478.0     734.0     548.0     638.0 *    119.   144. AG   694.    .9    .0 32.0
      22. SB        Gln DP    *   548.0     638.0     840.0    -220.0 *    906.   161. AG   694.    .9    .0 32.0
1
                                                                                                                PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3B1AM.DAT)              RUN: Site 3 BUILD 1  AM
      DATE: 03/22/2010   TIME: 10:42:44.83

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*------------------------------------------------------------------------------
       3. EB        Wil T+R   *     150      39       2.0       2690        994       4.10      1        3
       5. EB        Wil LT    *     150     130       2.0        195         84       4.10      1        3
       9. WB        Wil T+R   *     150      62       2.0       3035        924       4.10      1        3
      11. WB        Wil LT    *     150      62       2.0         86         54       4.10      1        3
      14. NB        Gln AP    *     150     116       2.0        388         69       4.10      1        3
      18. SB        Gln T+LT  *     150     116       2.0        330        678       4.10      1        3
      20. SB        Gln R     *     150      98       2.0        263       1600       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y           Z       *
     -------------------------*-------------------------------------*
      1. SE MID S             *       685.0      365.0        5.0   *
      2. SE 164 S             *       638.0      508.0        5.0   *
      3. SE 82 S              *       611.0      586.0        5.0   *
      4. SE CNR               *       595.0      659.0        5.0   *
      5. SE 82 E              *       664.0      689.0        5.0   *
      6. SE 164 E             *       742.0      713.0        5.0   *
      7. SE MID E             *       849.0      747.0        5.0   *
      8. NE MID E             *       793.0      878.0        5.0   *
      9. NE 164 E             *       674.0      839.0        5.0   *
     10. NE 82 E              *       595.0      813.0        5.0   *
     11. NE CNR               *       515.0      792.0        5.0   *
     12. NE 82 N              *       452.0      847.0        5.0   *
     13. NE 164 N             *       396.0      907.0        5.0   *
     14. NE MID N             *       319.0      990.0        5.0   *
     15. NW MID N             *       190.0      983.0        5.0   *
     16. NW 164 N             *       267.0      900.0        5.0   *
     17. NW 82 N              *       323.0      841.0        5.0   *
     18. NW CNR               *       381.0      759.0        5.0   *
     19. NW 82 W              *       299.0      719.0        5.0   *
     20. NW 164 W             *       222.0      694.0        5.0   *
     21. NW MID W             *       107.0      658.0        5.0   *
     22. SW MID W             *       213.0      548.0        5.0   *
     23. SW 164 W             *       367.0      595.0        5.0   *
     24. SW 82 W              *       447.0      619.0        5.0   *
     25. SW CNR               *       518.0      634.0        5.0   *
     26. SW 82 S              *       550.0      565.0        5.0   *
     27. SW 164 S             *       577.0      487.0        5.0   *
     28. SW MID S             *       622.0      354.0        5.0   *
1
                                                                                                                PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3B1AM.DAT)              RUN: Site 3 BUILD 1  AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  80.  *    .0    .0    .0    .0    .1    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 155.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 160.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 165.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 170.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 175.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 190.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                PAGE  4
      JOB: Site 3 Glendon & Wilshire (S3B1AM.DAT)               RUN: Site 3 BUILD 1  AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 225.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 255.  *    .0    .0    .0    .0    .0    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 DEGR. *     0     0     0     0     0     0     0    70    85    70    70     0     0     0     0     0     0   105    70    70

1
                                                                                                                PAGE  5
      JOB: Site 3 Glendon & Wilshire (S3B1AM.DAT)               RUN: Site 3 BUILD 1  AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
  5.  *    .0    .1    .1    .1    .0    .0    .0    .0
 10.  *    .0    .1    .1    .1    .0    .0    .0    .0
 15.  *    .0    .1    .1    .1    .0    .0    .0    .0
 20.  *    .0    .1    .1    .1    .0    .0    .0    .0
 25.  *    .0    .1    .1    .1    .0    .0    .0    .0
 30.  *    .0    .1    .1    .1    .0    .0    .0    .0
 35.  *    .0    .1    .1    .1    .0    .0    .0    .0
 40.  *    .0    .1    .1    .1    .1    .0    .0    .0
 45.  *    .0    .1    .1    .1    .1    .0    .0    .0
 50.  *    .0    .1    .1    .1    .1    .0    .0    .0
 55.  *    .0    .1    .1    .1    .1    .0    .0    .0
 60.  *    .0    .1    .1    .1    .1    .0    .0    .0
 65.  *    .1    .1    .1    .1    .1    .0    .0    .0
 70.  *    .1    .1    .1    .0    .1    .0    .0    .0
 75.  *    .1    .1    .1    .0    .0    .0    .0    .0
 80.  *    .1    .0    .0    .0    .0    .0    .0    .0
 85.  *    .1    .0    .0    .0    .0    .0    .0    .0
 90.  *    .1    .0    .0    .0    .0    .0    .0    .0
 95.  *    .1    .0    .0    .0    .0    .0    .0    .0
100.  *    .1    .0    .0    .0    .0    .0    .0    .0
105.  *    .1    .0    .0    .0    .0    .0    .0    .0
110.  *    .1    .0    .0    .0    .0    .0    .0    .0
115.  *    .1    .0    .0    .0    .0    .0    .0    .0
120.  *    .1    .0    .0    .0    .0    .0    .0    .0
125.  *    .1    .0    .0    .0    .0    .0    .0    .0
130.  *    .1    .0    .0    .0    .0    .0    .0    .0
135.  *    .1    .0    .0    .0    .0    .0    .0    .0
140.  *    .1    .0    .0    .0    .0    .0    .0    .0
145.  *    .1    .0    .0    .0    .0    .0    .0    .0
150.  *    .1    .0    .0    .0    .0    .0    .0    .0
155.  *    .1    .0    .0    .0    .0    .0    .0    .0
160.  *    .1    .0    .0    .0    .0    .0    .0    .0
165.  *    .1    .0    .0    .0    .0    .0    .0    .0
170.  *    .1    .0    .0    .0    .0    .0    .0    .0
175.  *    .1    .0    .0    .0    .0    .0    .0    .0
180.  *    .1    .0    .0    .0    .0    .0    .0    .0
185.  *    .1    .0    .0    .0    .0    .0    .0    .0
190.  *    .1    .0    .0    .0    .0    .0    .0    .0
195.  *    .1    .0    .0    .0    .0    .0    .0    .0
200.  *    .1    .0    .0    .0    .0    .0    .0    .0
205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                                PAGE  6
     JOB: Site 3 Glendon & Wilshire (S3B1AM.DAT)              RUN: Site 3 BUILD 1  AM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .1    .0    .0    .0    .0    .0    .0    .0
215.  *    .1    .0    .0    .0    .0    .0    .0    .0
220.  *    .1    .0    .0    .0    .0    .0    .0    .0
225.  *    .1    .0    .0    .0    .0    .0    .0    .0
230.  *    .1    .0    .0    .0    .0    .0    .0    .0
235.  *    .1    .0    .0    .0    .0    .0    .0    .0
240.  *    .1    .1    .0    .0    .0    .0    .0    .0
245.  *    .1    .1    .1    .0    .0    .0    .0    .0
250.  *    .1    .1    .1    .0    .0    .0    .0    .0
255.  *    .1    .1    .1    .1    .0    .0    .0    .0
260.  *    .1    .1    .1    .1    .1    .0    .0    .0
265.  *    .0    .1    .1    .1    .1    .0    .0    .0
270.  *    .0    .1    .1    .1    .1    .0    .0    .0
275.  *    .0    .1    .1    .1    .1    .0    .0    .0
280.  *    .0    .1    .1    .1    .1    .0    .0    .0
285.  *    .0    .1    .1    .1    .1    .0    .0    .0
290.  *    .0    .1    .0    .1    .1    .0    .0    .0
295.  *    .0    .1    .0    .1    .1    .0    .0    .0
300.  *    .0    .1    .0    .1    .1    .0    .0    .0
305.  *    .0    .1    .1    .1    .1    .0    .0    .0
310.  *    .0    .1    .1    .1    .1    .0    .0    .0
315.  *    .0    .1    .1    .1    .1    .0    .0    .0
320.  *    .0    .1    .1    .1    .1    .0    .0    .0
325.  *    .0    .1    .1    .1    .1    .0    .0    .0
330.  *    .0    .1    .1    .1    .1    .0    .0    .0
335.  *    .0    .1    .1    .1    .1    .0    .0    .0
340.  *    .0    .1    .1    .1    .1    .0    .0    .0
345.  *    .0    .1    .1    .1    .1    .0    .0    .0
350.  *    .0    .1    .1    .1    .1    .0    .0    .0
355.  *    .0    .1    .1    .1    .1    .0    .0    .0
360.  *    .0    .1    .1    .1    .0    .0    .0    .0
------*------------------------------------------------
MAX   *    .1    .1    .1    .1    .1    .0    .0    .0
DEGR. *   65     0     0     0    40     0     0     0

THE HIGHEST CONCENTRATION IS     .30 PPM AT   85 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC10.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT)              RUN: Site 3 BUILD A1 PM
      DATE: 03/22/2010   TIME: 10:51:05.37


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2    *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*---------------------------------------*--------------------------------------------------------------
       1. EB        Wil AP    *   323.0     617.0    -426.0     376.0 *     787.   252. AG  2704.    .8    .0 68.0
       2. EB        Wil T+R   *   323.0     616.0     531.0     681.0 *     218.    73. AG  2475.    .8    .0 68.0
       3. EB        Wil T+R   *   475.0     663.0   -6932.5   -1620.1 *    7751.   253. AG    16. 100.0    .0 48.0 **** 393.8
       4. EB        Wil LT    *   315.0     650.0     513.0     712.0 *     207.    73. AG   229.    .8    .0 44.0
       5. EB        Wil LT    *   444.0     690.0    -819.9     301.9 *    1322.   253. AG    19. 100.0    .0 24.0 ****  67.2
       6. EB        Wil DP    *   532.0     683.0    1471.0     989.0 *     988.    72. AG  2819.    .8    .0 68.0
       7. WB        Wil AP    *   756.0     830.0    1454.0    1051.0 *     732.    72. AG  2895.    .8    .0 68.0
       8. WB        Wil T+R   *   756.0     829.0     484.0     742.0 *     286.   252. AG  2762.    .8    .0 68.0
       9. WB        Wil T+R   *   540.0     760.0    3240.5    1622.1 *    2835.    72. AG    23. 100.0    .0 48.0 1.54 144.0
      10. WB        Wil LT    *   767.0     790.0     513.0     706.0 *     268.   252. AG   133.    .8    .0 32.0
      11. WB        Wil LT    *   566.0     723.0    1695.7    1095.7 *    1190.    72. AG     6. 100.0    .0 12.0 4.43  60.4
      12. WB        Wil DP    *   483.0     742.0    -451.0     441.0 *     981.   252. AG  3001.    .8    .0 68.0
      13. NB        Gln AP    *   542.0     703.0     861.0    -211.0 *     968.   161. AG   870.    .9    .0 32.0
      14. NB        Gln AP    *   564.0     640.0    3404.2   -7513.1 *    8634.   161. AG     7. 100.0    .0 12.0 **** 438.6
      15. NB        Gln DP    *   545.0     705.0    -160.0    1462.0 *    1034.   317. AG   988.    .9    .0 32.0
      16. SB        Gln AP    *   305.0     915.0    -182.0    1445.0 *     720.   317. AG  1004.    .9    .0 32.0
      17. SB        Gln T+LT  *   305.0     915.0     479.0     736.0 *     250.   136. AG   699.    .9    .0 44.0
      18. SB        Gln T+LT  *   430.0     786.0    -420.8    1661.1 *    1220.   316. AG    15. 100.0    .0 24.0 1.37  62.0
      19. SB        Gln R     *   300.0     890.0     443.0     732.0 *     213.   138. AG   305.    .9    .0 32.0
      20. SB        Gln R     *   400.0     780.0     309.6     880.4 *     135.   318. AG     6. 100.0    .0 12.0  .44   6.9
      21. SB        Gln DP    *   478.0     734.0     548.0     638.0 *     119.   144. AG   665.    .9    .0 32.0
      22. SB        Gln DP    *   548.0     638.0     840.0    -220.0 *     906.   161. AG   665.    .9    .0 32.0
1
                                                                                                                PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT)              RUN: Site 3 BUILD A1 PM
      DATE: 03/22/2010   TIME: 10:51:05.37

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)     (SEC)     (VPH)      (VPH)    (gm/hr)
      ------------------------*----------------------------------------------------------------------------------
       3. EB        Wil T+R   *     150       56       2.0       2475         7       4.10      1        3
       5. EB        Wil LT    *     150      130       2.0        229        84       4.10      1        3
       9. WB        Wil T+R   *     150       78       2.0       2762       990       4.10      1        3
      11. WB        Wil LT    *     150       78       2.0        133        68       4.10      1        3
      14. NB        Gln AP    *     150       99       2.0        870       280       4.10      1        3
      18. SB        Gln T+LT  *     150       99       2.0        699       816       4.10      1        3
      20. SB        Gln R     *     150       81       2.0        305      1600       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)           *
         RECEPTOR             *      X           Y           Z       *
     -------------------------*--------------------------------------*
      1. SE MID S             *       685.0      365.0        5.0    *
      2. SE 164 S             *       638.0      508.0        5.0    *
      3. SE 82 S              *       611.0      586.0        5.0    *
      4. SE CNR               *       595.0      659.0        5.0    *
      5. SE 82 E              *       664.0      689.0        5.0    *
      6. SE 164 E             *       742.0      713.0        5.0    *
      7. SE MID E             *       849.0      747.0        5.0    *
      8. NE MID E             *       793.0      878.0        5.0    *
      9. NE 164 E             *       674.0      839.0        5.0    *
     10. NE 82 E              *       595.0      813.0        5.0    *
     11. NE CNR               *       515.0      792.0        5.0    *
     12. NE 82 N              *       452.0      847.0        5.0    *
     13. NE 164 N             *       396.0      907.0        5.0    *
     14. NE MID N             *       319.0      990.0        5.0    *
     15. NW MID N             *       190.0      983.0        5.0    *
     16. NW 164 N             *       267.0      900.0        5.0    *
     17. NW 82 N              *       323.0      841.0        5.0    *
     18. NW CNR               *       381.0      759.0        5.0    *
     19. NW 82 W              *       299.0      719.0        5.0    *
     20. NW 164 W             *       222.0      694.0        5.0    *
     21. NW MID W             *       107.0      658.0        5.0    *
     22. SW MID W             *       213.0      548.0        5.0    *
     23. SW 164 W             *       367.0      595.0        5.0    *
     24. SW 82 W              *       447.0      619.0        5.0    *
     25. SW CNR               *       518.0      634.0        5.0    *
     26. SW 82 S              *       550.0      565.0        5.0    *
     27. SW 164 S             *       577.0      487.0        5.0    *
     28. SW MID S             *       622.0      354.0        5.0    *
1
                                                                                                                PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT)              RUN: Site 3 BUILD A1 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  80.  *    .0    .0    .0    .0    .1    .1    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 155.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 160.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 165.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 170.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 175.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 190.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                PAGE  4
      JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT)              RUN: Site 3 BUILD A1 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 225.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .0    .0    .0    .0    .0    .1    .1    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 255.  *    .0    .0    .0    .0    .1    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 DEGR. *     0     0     0     0     0     0     0    70    90    70    75     0     0     0     0     0     0   100    70    65

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                                                                                                                PAGE  5
      JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT)              RUN: Site 3 BUILD A1 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
  5.  *    .0    .1    .1    .1    .0    .0    .0    .0
 10.  *    .0    .1    .1    .1    .0    .0    .0    .0
 15.  *    .0    .1    .1    .1    .0    .0    .0    .0
 20.  *    .0    .2    .2    .1    .0    .0    .0    .0
 25.  *    .0    .2    .2    .1    .0    .0    .0    .0
 30.  *    .0    .2    .2    .1    .0    .0    .0    .0
 35.  *    .0    .2    .2    .1    .1    .0    .0    .0
 40.  *    .0    .2    .2    .1    .1    .0    .0    .0
 45.  *    .0    .2    .2    .1    .1    .0    .0    .0
 50.  *    .0    .2    .2    .1    .1    .0    .0    .0
 55.  *    .0    .2    .1    .1    .1    .0    .0    .0
 60.  *    .0    .2    .1    .2    .1    .0    .0    .0
 65.  *    .1    .2    .1    .1    .1    .0    .0    .0
 70.  *    .1    .1    .1    .1    .1    .0    .0    .0
 75.  *    .1    .0    .1    .0    .1    .0    .0    .0
 80.  *    .1    .0    .0    .0    .0    .0    .0    .0
 85.  *    .1    .0    .0    .0    .0    .0    .0    .0
 90.  *    .1    .0    .0    .0    .0    .0    .0    .0
 95.  *    .1    .0    .0    .0    .0    .0    .0    .0
100.  *    .1    .0    .0    .0    .0    .0    .0    .0
105.  *    .1    .0    .0    .0    .0    .0    .0    .0
110.  *    .1    .0    .0    .0    .0    .0    .0    .0
115.  *    .1    .0    .0    .0    .0    .0    .0    .0
120.  *    .1    .0    .0    .0    .0    .0    .0    .0
125.  *    .1    .0    .0    .0    .0    .0    .0    .0
130.  *    .1    .0    .0    .0    .0    .0    .0    .0
135.  *    .1    .0    .0    .0    .0    .0    .0    .0
140.  *    .1    .0    .0    .0    .0    .0    .0    .0
145.  *    .1    .0    .0    .0    .0    .0    .0    .0
150.  *    .1    .0    .0    .0    .0    .0    .0    .0
155.  *    .1    .0    .0    .0    .0    .0    .0    .0
160.  *    .1    .0    .0    .0    .0    .0    .0    .0
165.  *    .1    .0    .0    .0    .0    .0    .0    .0
170.  *    .1    .0    .0    .0    .0    .0    .0    .0
175.  *    .1    .0    .0    .0    .0    .0    .0    .0
180.  *    .1    .0    .0    .0    .0    .0    .0    .0
185.  *    .1    .0    .0    .0    .0    .0    .0    .0
190.  *    .1    .0    .0    .0    .0    .0    .0    .0
195.  *    .1    .0    .0    .0    .0    .0    .0    .0
200.  *    .1    .0    .0    .0    .0    .0    .0    .0
205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                                 PAGE  6
     JOB: Site 3 Glendon & Wilshire (S3B1PM.DAT)               RUN: Site 3 BUILD A1 PM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .1    .0    .0    .0    .0    .0    .0    .0
215.  *    .1    .0    .0    .0    .0    .0    .0    .0
220.  *    .1    .0    .0    .0    .0    .0    .0    .0
225.  *    .1    .0    .0    .0    .0    .0    .0    .0
230.  *    .1    .0    .0    .0    .0    .0    .0    .0
235.  *    .1    .0    .0    .0    .0    .0    .0    .0
240.  *    .1    .0    .0    .0    .0    .0    .0    .0
245.  *    .1    .1    .0    .0    .0    .0    .0    .0
250.  *    .1    .2    .2    .1    .0    .0    .0    .0
255.  *    .1    .2    .2    .1    .1    .0    .0    .0
260.  *    .1    .2    .2    .2    .2    .0    .0    .0
265.  *    .0    .2    .2    .2    .2    .0    .0    .0
270.  *    .0    .2    .2    .2    .2    .0    .0    .0
275.  *    .0    .2    .2    .2    .2    .0    .0    .0
280.  *    .0    .2    .2    .2    .1    .0    .0    .0
285.  *    .0    .2    .2    .2    .1    .0    .0    .0
290.  *    .0    .2    .1    .2    .1    .0    .0    .0
295.  *    .0    .2    .1    .2    .1    .0    .0    .0
300.  *    .0    .2    .1    .2    .1    .0    .0    .0
305.  *    .0    .2    .1    .2    .1    .0    .0    .0
310.  *    .0    .1    .0    .1    .1    .0    .0    .0
315.  *    .0    .1    .1    .1    .1    .0    .0    .0
320.  *    .0    .1    .1    .1    .1    .0    .0    .0
325.  *    .0    .1    .1    .1    .1    .0    .0    .0
330.  *    .0    .1    .1    .1    .1    .0    .0    .0
335.  *    .0    .1    .1    .1    .1    .0    .0    .0
340.  *    .0    .1    .1    .1    .1    .0    .0    .0
345.  *    .0    .1    .1    .1    .1    .0    .0    .0
350.  *    .0    .1    .1    .1    .1    .0    .0    .0
355.  *    .0    .1    .1    .1    .0    .0    .0    .0
360.  *    .0    .1    .1    .1    .0    .0    .0    .0
------*------------------------------------------------
MAX   *    .1    .2    .2    .2    .2    .0    .0    .0
DEGR. *   65    20    20    60   260     0     0     0

THE HIGHEST CONCENTRATION IS     .30 PPM AT   90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC10.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT)               RUN: Site 3 BUILD 2  AM
      DATE: 03/22/2010   TIME: 11:01:39.59


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG  TYPE  VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *    323.0     617.0    -426.0     376.0 *     787.   252. AG   2910.    .8    .0 68.0
       2. EB        Wil T+R   *    323.0     616.0     531.0     681.0 *     218.    73. AG   2733.    .8    .0 68.0
       3. EB        Wil T+R   *    475.0     663.0     255.9     595.5 *     229.   253. AG     11. 100.0    .0 48.0  .96  11.6
       4. EB        Wil LT    *    315.0     650.0     513.0     712.0 *     207.    73. AG    177.    .8    .0 44.0
       5. EB        Wil LT    *    444.0     690.0    -514.9     395.5 *    1003.   253. AG     19. 100.0    .0 24.0 ****  51.0
       6. EB        Wil DP    *    532.0     683.0    1471.0     989.0 *     988.    72. AG   2513.    .8    .0 68.0
       7. WB        Wil AP    *    756.0     830.0    1454.0    1051.0 *     732.    72. AG   3134.    .8    .0 68.0
       8. WB        Wil T+R   *    756.0     829.0     484.0     742.0 *     286.   252. AG   3039.    .8    .0 68.0
       9. WB        Wil T+R   *    540.0     760.0    2725.4    1457.7 *    2294.    72. AG     18. 100.0    .0 48.0 1.34 116.5
      10. WB        Wil LT    *    767.0     790.0     513.0     706.0 *     268.   252. AG     95.    .8    .0 32.0
      11. WB        Wil LT    *    566.0     723.0    1284.0     959.9 *     756.    72. AG      4. 100.0    .0 12.0 3.17  38.4
      12. WB        Wil DP    *    483.0     742.0    -451.0     441.0 *     981.   252. AG   2846.    .8    .0 68.0
      13. NB        Gln AP    *    542.0     703.0     861.0    -211.0 *     968.   161. AG    382.    .9    .0 32.0
      14. NB        Gln AP    *    564.0     640.0    1991.2   -3456.8 *    4338.   161. AG      9. 100.0    .0 12.0 **** 220.4
      15. NB        Gln DP    *    545.0     705.0    -160.0    1462.0 *    1034.   317. AG    951.    .9    .0 32.0
      16. SB        Gln AP    *    305.0     915.0    -182.0    1445.0 *     720.   317. AG    604.    .9    .0 32.0
      17. SB        Gln T+LT  *    305.0     915.0     479.0     736.0 *     250.   136. AG    352.    .9    .0 44.0
      18. SB        Gln T+LT  *    430.0     786.0      26.5    1201.1 *     579.   316. AG     17. 100.0    .0 24.0 1.29  29.4
      19. SB        Gln R     *    300.0     890.0     443.0     732.0 *     213.   138. AG    252.    .9    .0 32.0
      20. SB        Gln R     *    400.0     780.0     308.7     881.4 *     136.   318. AG      7. 100.0    .0 12.0  .50   6.9
      21. SB        Gln DP    *    478.0     734.0     548.0     638.0 *     119.   144. AG    720.    .9    .0 32.0
      22. SB        Gln DP    *    548.0     638.0     840.0    -220.0 *     906.   161. AG    720.    .9    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT)               RUN: Site 3 BUILD 2  AM
      DATE: 03/22/2010   TIME: 11:01:39.59

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R   *    150        39       2.0      2733        993       4.10      1        3
       5. EB        Wil LT    *    150       131       2.0       177         84       4.10      1        3
       9. WB        Wil T+R   *    150        60       2.0      3039        989       4.10      1        3
      11. WB        Wil LT    *    150        60       2.0        95         54       4.10      1        3
      14. NB        Gln AP    *    150       116       2.0       382         75       4.10      1        3
      18. SB        Gln T+LT  *    150       116       2.0       352        681       4.10      1        3
      20. SB        Gln R     *    150        99       2.0       252       1600       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       685.0      365.0        5.0   *
      2. SE 164 S             *       638.0      508.0        5.0   *
      3. SE 82 S              *       611.0      586.0        5.0   *
      4. SE CNR               *       595.0      659.0        5.0   *
      5. SE 82 E              *       664.0      689.0        5.0   *
      6. SE 164 E             *       742.0      713.0        5.0   *
      7. SE MID E             *       849.0      747.0        5.0   *
      8. NE MID E             *       793.0      878.0        5.0   *
      9. NE 164 E             *       674.0      839.0        5.0   *
     10. NE 82 E              *       595.0      813.0        5.0   *
     11. NE CNR               *       515.0      792.0        5.0   *
     12. NE 82 N              *       452.0      847.0        5.0   *
     13. NE 164 N             *       396.0      907.0        5.0   *
     14. NE MID N             *       319.0      990.0        5.0   *
     15. NW MID N             *       190.0      983.0        5.0   *
     16. NW 164 N             *       267.0      900.0        5.0   *
     17. NW 82 N              *       323.0      841.0        5.0   *
     18. NW CNR               *       381.0      759.0        5.0   *
     19. NW 82 W              *       299.0      719.0        5.0   *
     20. NW 164 W             *       222.0      694.0        5.0   *
     21. NW MID W             *       107.0      658.0        5.0   *
     22. SW MID W             *       213.0      548.0        5.0   *
     23. SW 164 W             *       367.0      595.0        5.0   *
     24. SW 82 W              *       447.0      619.0        5.0   *
     25. SW CNR               *       518.0      634.0        5.0   *
     26. SW 82 S              *       550.0      565.0        5.0   *
     27. SW 164 S             *       577.0      487.0        5.0   *
     28. SW MID S             *       622.0      354.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT)               RUN: Site 3 BUILD 2  AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
  0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 80.  *    .0    .0    .0    .0    .1    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
135.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
140.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
145.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
150.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
155.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
160.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
165.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
170.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
175.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
180.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
190.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                     PAGE  4
     JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT)              RUN: Site 3 BUILD 2  AM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
225.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
245.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
250.  *    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
255.  *    .0    .0    .0    .0    .0    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
------*------------------------------------------------------------------------------------------------------------------------
MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
DEGR. *    0     0     0     0     0     0     0    70    85    70    75     0     0     0     0     0     0   105    70    70

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                                                                                                                     PAGE  5
     JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT)              RUN: Site 3 BUILD 2  AM

      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
   5.  *    .0    .1    .1    .1    .0    .0    .0    .0
  10.  *    .0    .1    .1    .1    .0    .0    .0    .0
  15.  *    .0    .1    .1    .1    .0    .0    .0    .0
  20.  *    .0    .1    .1    .1    .0    .0    .0    .0
  25.  *    .0    .1    .1    .1    .0    .0    .0    .0
  30.  *    .0    .1    .1    .1    .0    .0    .0    .0
  35.  *    .0    .1    .1    .1    .0    .0    .0    .0
  40.  *    .0    .1    .1    .1    .1    .0    .0    .0
  45.  *    .0    .1    .1    .1    .1    .0    .0    .0
  50.  *    .0    .1    .1    .1    .1    .0    .0    .0
  55.  *    .0    .1    .1    .1    .1    .0    .0    .0
  60.  *    .0    .1    .1    .1    .1    .0    .0    .0
  65.  *    .1    .1    .1    .2    .1    .0    .0    .0
  70.  *    .1    .1    .1    .0    .1    .0    .0    .0
  75.  *    .1    .1    .1    .0    .0    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .1    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE  6
      JOB: Site 3 Glendon & Wilshire (S3B2AM.DAT)               RUN: Site 3 BUILD 2  AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .1    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .1    .0    .0    .0    .0    .0
 250.  *    .1    .1    .1    .0    .0    .0    .0    .0
 255.  *    .1    .1    .1    .1    .0    .0    .0    .0
 260.  *    .1    .1    .1    .2    .1    .0    .0    .0
 265.  *    .0    .1    .1    .1    .1    .0    .0    .0
 270.  *    .0    .1    .1    .1    .1    .0    .0    .0
 275.  *    .0    .1    .1    .1    .1    .0    .0    .0
 280.  *    .0    .1    .1    .1    .1    .0    .0    .0
 285.  *    .0    .1    .1    .1    .1    .0    .0    .0
 290.  *    .0    .1    .0    .1    .1    .0    .0    .0
 295.  *    .0    .1    .0    .1    .1    .0    .0    .0
 300.  *    .0    .1    .0    .1    .1    .0    .0    .0
 305.  *    .0    .1    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .1    .0    .0    .0
 340.  *    .0    .1    .1    .1    .1    .0    .0    .0
 345.  *    .0    .1    .1    .1    .1    .0    .0    .0
 350.  *    .0    .1    .1    .1    .1    .0    .0    .0
 355.  *    .0    .1    .1    .1    .1    .0    .0    .0
 360.  *    .0    .1    .1    .1    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .1    .1    .1    .2    .1    .0    .0    .0
 DEGR. *   65     0     0    65    40     0     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   85 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC8 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC10.
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT)               RUN: Site 3 BUILD A2 PM
      DATE: 03/22/2010   TIME: 11:09:09.87


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M      AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *   LENGTH  BRG TYPE   VPH    EF     H   W   V/C QUEUE
                              *   X1        Y1        X2        Y2     *    (FT)  (DEG)            (G/MI) (FT) (FT)      (VEH)
      ------------------------*----------------------------------------*------------------------------------------------------
       1. EB        Wil AP    *    323.0     617.0    -426.0     376.0 *     787.  252. AG    2692.    .8   .0 68.0
       2. EB        Wil T+R   *    323.0     616.0     531.0     681.0 *     218.   73. AG    2479.    .8   .0 68.0
       3. EB        Wil T+R   *    475.0     663.0   -7179.1   -1696.1 *    8009.  253. AG      16. 100.0   .0 48.0 **** 406.9
       4. EB        Wil LT    *    315.0     650.0     513.0     712.0 *     207.   73. AG     229.    .8   .0 44.0
       5. EB        Wil LT    *    444.0     690.0    -819.9     301.9 *    1322.  253. AG      19. 100.0   .0 24.0 ****  67.2
       6. EB        Wil DP    *    532.0     683.0    1471.0     989.0 *     988.   72. AG    2820.    .8   .0 68.0
       7. WB        Wil AP    *    756.0     830.0    1454.0    1051.0 *     732.   72. AG    2921.    .8   .0 68.0
       8. WB        Wil T+R   *    756.0     829.0     484.0     742.0 *     286.  252. AG    2789.    .8   .0 68.0
       9. WB        Wil T+R   *    540.0     760.0    3249.6    1625.0 *    2844.   72. AG      23. 100.0   .0 48.0 1.54 144.5
      10. WB        Wil LT    *    767.0     790.0     513.0     706.0 *     268.  252. AG     132.    .8   .0 32.0
      11. WB        Wil LT    *    566.0     723.0    1684.4    1092.0 *    1178.   72. AG       6. 100.0   .0 12.0 4.40  59.8
      12. WB        Wil DP    *    483.0     742.0    -451.0     441.0 *     981.  252. AG    3052.    .8   .0 68.0
      13. NB        Gln AP    *    542.0     703.0     861.0    -211.0 *     968.  161. AG     888.    .9   .0 32.0
      14. NB        Gln AP    *    564.0     640.0    3485.4   -7746.2 *    8881.  161. AG       7. 100.0   .0 12.0 **** 451.1
      15. NB        Gln DP    *    545.0     705.0    -160.0    1462.0 *    1034.  317. AG     964.    .9   .0 32.0
      16. SB        Gln AP    *    305.0     915.0    -182.0    1445.0 *     720.  317. AG    1003.    .9   .0 32.0
      17. SB        Gln T+LT  *    305.0     915.0     479.0     736.0 *     250.  136. AG     706.    .9   .0 44.0
      18. SB        Gln T+LT  *    430.0     786.0    -408.5    1648.5 *    1203.  316. AG      15. 100.0   .0 24.0 1.35  61.1
      19. SB        Gln R     *    300.0     890.0     443.0     732.0 *     213.  138. AG     303.    .9   .0 32.0
      20. SB        Gln R     *    400.0     780.0     308.0     882.2 *     138.  318. AG       6. 100.0   .0 12.0  .45   7.0
      21. SB        Gln DP    *    478.0     734.0     548.0     638.0 *     119.  144. AG     674.    .9   .0 32.0
      22. SB        Gln DP    *    548.0     638.0     840.0    -220.0 *     906.  161. AG     674.    .9   .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT)               RUN: Site 3 BUILD A2 PM
      DATE: 03/22/2010   TIME: 11:09:09.87

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R   *    150        56       2.0      2479          6       4.10      1       3
       5. EB        Wil LT    *    150       130       2.0       229         84       4.10      1       3
       9. WB        Wil T+R   *    150        77       2.0      2789        989       4.10      1       3
      11. WB        Wil LT    *    150        77       2.0       132         66       4.10      1       3
      14. NB        Gln AP    *    150        99       2.0       888        268       4.10      1       3
      18. SB        Gln T+LT  *    150        99       2.0       706        833       4.10      1       3
      20. SB        Gln R     *    150        83       2.0       303       1600       4.10      1       3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*------------------------------------*
      1. SE MID S             *       685.0      365.0        5.0   *
      2. SE 164 S             *       638.0      508.0        5.0   *
      3. SE 82 S              *       611.0      586.0        5.0   *
      4. SE CNR               *       595.0      659.0        5.0   *
      5. SE 82 E              *       664.0      689.0        5.0   *
      6. SE 164 E             *       742.0      713.0        5.0   *
      7. SE MID E             *       849.0      747.0        5.0   *
      8. NE MID E             *       793.0      878.0        5.0   *
      9. NE 164 E             *       674.0      839.0        5.0   *
     10. NE 82 E              *       595.0      813.0        5.0   *
     11. NE CNR               *       515.0      792.0        5.0   *
     12. NE 82 N              *       452.0      847.0        5.0   *
     13. NE 164 N             *       396.0      907.0        5.0   *
     14. NE MID N             *       319.0      990.0        5.0   *
     15. NW MID N             *       190.0      983.0        5.0   *
     16. NW 164 N             *       267.0      900.0        5.0   *
     17. NW 82 N              *       323.0      841.0        5.0   *
     18. NW CNR               *       381.0      759.0        5.0   *
     19. NW 82 W              *       299.0      719.0        5.0   *
     20. NW 164 W             *       222.0      694.0        5.0   *
     21. NW MID W             *       107.0      658.0        5.0   *
     22. SW MID W             *       213.0      548.0        5.0   *
     23. SW 164 W             *       367.0      595.0        5.0   *
     24. SW 82 W              *       447.0      619.0        5.0   *
     25. SW CNR               *       518.0      634.0        5.0   *
     26. SW 82 S              *       550.0      565.0        5.0   *
     27. SW 164 S             *       577.0      487.0        5.0   *
     28. SW MID S             *       622.0      354.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT)               RUN: Site 3 BUILD A2 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  80.  *    .0    .0    .0    .0    .1    .1    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 155.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 160.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 165.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 170.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 175.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 190.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                PAGE  4
      JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT)              RUN: Site 3 BUILD A2 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 225.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .0    .0    .0    .0    .0    .1    .1    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 255.  *    .0    .0    .0    .0    .1    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 DEGR. *     0     0     0     0     0     0     0    70    90    70    75     0     0     0     0     0     0   100    70    65

1
                                                                                                                PAGE  5
      JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT)              RUN: Site 3 BUILD A2 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
  5.  *    .0    .1    .1    .1    .0    .0    .0    .0
 10.  *    .0    .1    .1    .1    .0    .0    .0    .0
 15.  *    .0    .1    .1    .1    .0    .0    .0    .0
 20.  *    .0    .2    .2    .1    .0    .0    .0    .0
 25.  *    .0    .2    .2    .1    .0    .0    .0    .0
 30.  *    .0    .2    .2    .1    .0    .0    .0    .0
 35.  *    .0    .2    .2    .1    .1    .0    .0    .0
 40.  *    .0    .2    .2    .1    .1    .0    .0    .0
 45.  *    .0    .2    .2    .1    .1    .0    .0    .0
 50.  *    .0    .2    .2    .1    .1    .0    .0    .0
 55.  *    .0    .2    .1    .1    .1    .0    .0    .0
 60.  *    .0    .2    .1    .2    .1    .0    .0    .0
 65.  *    .1    .2    .1    .1    .1    .0    .0    .0
 70.  *    .1    .1    .1    .1    .1    .0    .0    .0
 75.  *    .1    .0    .1    .0    .1    .0    .0    .0
 80.  *    .1    .0    .0    .0    .0    .0    .0    .0
 85.  *    .1    .0    .0    .0    .0    .0    .0    .0
 90.  *    .1    .0    .0    .0    .0    .0    .0    .0
 95.  *    .1    .0    .0    .0    .0    .0    .0    .0
100.  *    .1    .0    .0    .0    .0    .0    .0    .0
105.  *    .1    .0    .0    .0    .0    .0    .0    .0
110.  *    .1    .0    .0    .0    .0    .0    .0    .0
115.  *    .1    .0    .0    .0    .0    .0    .0    .0
120.  *    .1    .0    .0    .0    .0    .0    .0    .0
125.  *    .1    .0    .0    .0    .0    .0    .0    .0
130.  *    .1    .0    .0    .0    .0    .0    .0    .0
135.  *    .1    .0    .0    .0    .0    .0    .0    .0
140.  *    .1    .0    .0    .0    .0    .0    .0    .0
145.  *    .1    .0    .0    .0    .0    .0    .0    .0
150.  *    .1    .0    .0    .0    .0    .0    .0    .0
155.  *    .1    .0    .0    .0    .0    .0    .0    .0
160.  *    .1    .0    .0    .0    .0    .0    .0    .0
165.  *    .1    .0    .0    .0    .0    .0    .0    .0
170.  *    .1    .0    .0    .0    .0    .0    .0    .0
175.  *    .1    .0    .0    .0    .0    .0    .0    .0
180.  *    .1    .0    .0    .0    .0    .0    .0    .0
185.  *    .1    .0    .0    .0    .0    .0    .0    .0
190.  *    .1    .0    .0    .0    .0    .0    .0    .0
195.  *    .1    .0    .0    .0    .0    .0    .0    .0
200.  *    .1    .0    .0    .0    .0    .0    .0    .0
205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE  6
     JOB: Site 3 Glendon & Wilshire (S3B2PM.DAT)              RUN: Site 3 BUILD A2 PM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .1    .0    .0    .0    .0    .0    .0    .0
215.  *    .1    .0    .0    .0    .0    .0    .0    .0
220.  *    .1    .0    .0    .0    .0    .0    .0    .0
225.  *    .1    .0    .0    .0    .0    .0    .0    .0
230.  *    .1    .0    .0    .0    .0    .0    .0    .0
235.  *    .1    .0    .0    .0    .0    .0    .0    .0
240.  *    .1    .0    .0    .0    .0    .0    .0    .0
245.  *    .1    .1    .0    .0    .0    .0    .0    .0
250.  *    .1    .2    .2    .1    .0    .0    .0    .0
255.  *    .1    .2    .2    .1    .1    .0    .0    .0
260.  *    .1    .2    .2    .2    .2    .0    .0    .0
265.  *    .0    .2    .2    .2    .2    .0    .0    .0
270.  *    .0    .2    .2    .2    .2    .0    .0    .0
275.  *    .0    .2    .2    .2    .2    .0    .0    .0
280.  *    .0    .2    .2    .2    .1    .0    .0    .0
285.  *    .0    .2    .2    .2    .1    .0    .0    .0
290.  *    .0    .2    .1    .2    .1    .0    .0    .0
295.  *    .0    .2    .1    .2    .1    .0    .0    .0
300.  *    .0    .2    .1    .2    .1    .0    .0    .0
305.  *    .0    .2    .1    .2    .1    .0    .0    .0
310.  *    .0    .1    .0    .1    .1    .0    .0    .0
315.  *    .0    .1    .1    .1    .1    .0    .0    .0
320.  *    .0    .1    .1    .1    .1    .0    .0    .0
325.  *    .0    .1    .1    .1    .1    .0    .0    .0
330.  *    .0    .1    .1    .1    .1    .0    .0    .0
335.  *    .0    .1    .1    .1    .1    .0    .0    .0
340.  *    .0    .1    .1    .1    .1    .0    .0    .0
345.  *    .0    .1    .1    .1    .1    .0    .0    .0
350.  *    .0    .1    .1    .1    .1    .0    .0    .0
355.  *    .0    .1    .1    .1    .0    .0    .0    .0
360.  *    .0    .1    .1    .1    .0    .0    .0    .0
------*------------------------------------------------
MAX   *    .1    .2    .2    .2    .2    .0    .0    .0
DEGR. *   65    20    20    60   260     0     0     0

THE HIGHEST CONCENTRATION IS     .30 PPM AT   90 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC10.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT)              RUN: Site 3 BUILD 3  AM
      DATE: 03/22/2010   TIME: 11:19:24.60


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*-------------------------------------------------------------
        1. EB        Wil AP    *    323.0     617.0    -426.0     376.0 *     787.   252. AG  2883.    .8    .0 68.0
        2. EB        Wil T+R   *    323.0     616.0     531.0     681.0 *     218.    73. AG  2678.    .8    .0 68.0
        3. EB        Wil T+R   *    475.0     663.0     278.8     602.5 *     205.   253. AG    11. 100.0    .0 48.0  .94  10.4
        4. EB        Wil LT    *    315.0     650.0     513.0     712.0 *     207.    73. AG   205.    .8    .0 44.0
        5. EB        Wil LT    *    444.0     690.0    -659.3     351.2 *    1154.   253. AG    19. 100.0    .0 24.0 ****  58.6
        6. EB        Wil DP    *    532.0     683.0    1471.0     989.0 *     988.    72. AG  2652.    .8    .0 68.0
        7. WB        Wil AP    *    756.0     830.0    1454.0    1051.0 *     732.    72. AG  3101.    .8    .0 68.0
        8. WB        Wil T+R   *    756.0     829.0     484.0     742.0 *     286.   252. AG  3005.    .8    .0 68.0
        9. WB        Wil T+R   *    540.0     760.0    2777.7    1474.4 *    2349.    72. AG    18. 100.0    .0 48.0 1.36 119.3
       10. WB        Wil LT    *    767.0     790.0     513.0     706.0 *     268.   252. AG    96.    .8    .0 32.0
       11. WB        Wil LT    *    566.0     723.0    1295.5     963.7 *     768.    72. AG     5. 100.0    .0 12.0 3.20  39.0
       12. WB        Wil DP    *    483.0     742.0    -451.0     441.0 *     981.   252. AG  2818.    .8    .0 68.0
       13. NB        Gln AP    *    542.0     703.0     861.0    -211.0 *     968.   161. AG   316.    .9    .0 32.0
       14. NB        Gln AP    *    564.0     640.0    1794.0   -2890.9 *    3739.   161. AG     9. 100.0    .0 12.0 **** 189.9
       15. NB        Gln DP    *    545.0     705.0    -160.0    1462.0 *    1034.   317. AG   885.    .9    .0 32.0
       16. SB        Gln AP    *    305.0     915.0    -182.0    1445.0 *     720.   317. AG   570.    .9    .0 32.0
       17. SB        Gln T+LT  *    305.0     915.0     479.0     736.0 *     250.   136. AG   340.    .9    .0 44.0
       18. SB        Gln T+LT  *    430.0     786.0     135.4    1089.1 *     423.   316. AG    17. 100.0    .0 24.0 1.17  21.5
       19. SB        Gln R     *    300.0     890.0     443.0     732.0 *     213.   138. AG   230.    .9    .0 32.0
       20. SB        Gln R     *    400.0     780.0     318.4     870.7 *     122.   318. AG     7. 100.0    .0 12.0  .44   6.2
       21. SB        Gln DP    *    478.0     734.0     548.0     638.0 *     119.   144. AG   698.    .9    .0 32.0
       22. SB        Gln DP    *    548.0     638.0     840.0    -220.0 *     906.   161. AG   698.    .9    .0 32.0
1
                                                                                                                PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT)              RUN: Site 3 BUILD 3  AM
      DATE: 03/22/2010   TIME: 11:19:24.60

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL    ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE      RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
        3. EB        Wil T+R   *     150       39       2.0      2678         994       4.10      1        3
        5. EB        Wil LT    *     150      129       2.0       205          84       4.10      1        3
        9. WB        Wil T+R   *     150       62       2.0      3005         990       4.10      1        3
       11. WB        Wil LT    *     150       62       2.0        96          54       4.10      1        3
       14. NB        Gln AP    *     150      116       2.0       316          46       4.10      1        3
       18. SB        Gln T+LT  *     150      116       2.0       340         727       4.10      1        3
       20. SB        Gln R     *     150       97       2.0       230        1600       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-----------------------------------*
       1. SE MID S            *       685.0      365.0       5.0   *
       2. SE 164 S            *       638.0      508.0       5.0   *
       3. SE 82 S             *       611.0      586.0       5.0   *
       4. SE CNR              *       595.0      659.0       5.0   *
       5. SE 82 E             *       664.0      689.0       5.0   *
       6. SE 164 E            *       742.0      713.0       5.0   *
       7. SE MID E            *       849.0      747.0       5.0   *
       8. NE MID E            *       793.0      878.0       5.0   *
       9. NE 164 E            *       674.0      839.0       5.0   *
      10. NE 82 E             *       595.0      813.0       5.0   *
      11. NE CNR              *       515.0      792.0       5.0   *
      12. NE 82 N             *       452.0      847.0       5.0   *
      13. NE 164 N            *       396.0      907.0       5.0   *
      14. NE MID N            *       319.0      990.0       5.0   *
      15. NW MID N            *       190.0      983.0       5.0   *
      16. NW 164 N            *       267.0      900.0       5.0   *
      17. NW 82 N             *       323.0      841.0       5.0   *
      18. NW CNR              *       381.0      759.0       5.0   *
      19. NW 82 W             *       299.0      719.0       5.0   *
      20. NW 164 W            *       222.0      694.0       5.0   *
      21. NW MID W            *       107.0      658.0       5.0   *
      22. SW MID W            *       213.0      548.0       5.0   *
      23. SW 164 W            *       367.0      595.0       5.0   *
      24. SW 82 W             *       447.0      619.0       5.0   *
      25. SW CNR              *       518.0      634.0       5.0   *
      26. SW 82 S             *       550.0      565.0       5.0   *
      27. SW 164 S            *       577.0      487.0       5.0   *
      28. SW MID S            *       622.0      354.0       5.0   *
1
                                                                                                                PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT)              RUN: Site 3 BUILD 3  AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
  0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 80.  *    .0    .0    .0    .0    .1    .1    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
140.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
150.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
155.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
160.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
165.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
170.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
175.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
180.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
190.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                    PAGE  4
      JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT)              RUN: Site 3 BUILD 3  AM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
225.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
245.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
250.  *    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
255.  *    .0    .0    .0    .0    .1    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
------*------------------------------------------------------------------------------------------------------------------------
MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
DEGR. *     0     0     0     0     0     0     0    70    85    70    70     0     0     0     0     0     0   105    70    70

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                                                                                                                    PAGE  5
      JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT)              RUN: Site 3 BUILD 3  AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
  5.  *    .0    .1    .1    .1    .0    .0    .0    .0
 10.  *    .0    .1    .1    .1    .0    .0    .0    .0
 15.  *    .0    .1    .1    .1    .0    .0    .0    .0
 20.  *    .0    .1    .1    .1    .0    .0    .0    .0
 25.  *    .0    .1    .1    .1    .0    .0    .0    .0
 30.  *    .0    .1    .1    .1    .0    .0    .0    .0
 35.  *    .0    .1    .1    .1    .0    .0    .0    .0
 40.  *    .0    .1    .1    .1    .1    .0    .0    .0
 45.  *    .0    .1    .1    .1    .1    .0    .0    .0
 50.  *    .0    .1    .1    .1    .1    .0    .0    .0
 55.  *    .0    .1    .1    .1    .1    .0    .0    .0
 60.  *    .0    .1    .1    .2    .1    .0    .0    .0
 65.  *    .1    .1    .1    .2    .1    .0    .0    .0
 70.  *    .1    .1    .1    .1    .1    .0    .0    .0
 75.  *    .1    .1    .1    .0    .1    .0    .0    .0
 80.  *    .1    .0    .0    .0    .0    .0    .0    .0
 85.  *    .1    .0    .0    .0    .0    .0    .0    .0
 90.  *    .1    .0    .0    .0    .0    .0    .0    .0
 95.  *    .1    .0    .0    .0    .0    .0    .0    .0
100.  *    .1    .0    .0    .0    .0    .0    .0    .0
105.  *    .1    .0    .0    .0    .0    .0    .0    .0
110.  *    .1    .0    .0    .0    .0    .0    .0    .0
115.  *    .1    .0    .0    .0    .0    .0    .0    .0
120.  *    .1    .0    .0    .0    .0    .0    .0    .0
125.  *    .1    .0    .0    .0    .0    .0    .0    .0
130.  *    .1    .0    .0    .0    .0    .0    .0    .0
135.  *    .1    .0    .0    .0    .0    .0    .0    .0
140.  *    .1    .0    .0    .0    .0    .0    .0    .0
145.  *    .1    .0    .0    .0    .0    .0    .0    .0
150.  *    .1    .0    .0    .0    .0    .0    .0    .0
155.  *    .1    .0    .0    .0    .0    .0    .0    .0
160.  *    .1    .0    .0    .0    .0    .0    .0    .0
165.  *    .1    .0    .0    .0    .0    .0    .0    .0
170.  *    .1    .0    .0    .0    .0    .0    .0    .0
175.  *    .1    .0    .0    .0    .0    .0    .0    .0
180.  *    .1    .0    .0    .0    .0    .0    .0    .0
185.  *    .1    .0    .0    .0    .0    .0    .0    .0
190.  *    .1    .0    .0    .0    .0    .0    .0    .0
195.  *    .1    .0    .0    .0    .0    .0    .0    .0
200.  *    .1    .0    .0    .0    .0    .0    .0    .0
205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                               PAGE  6
      JOB: Site 3 Glendon & Wilshire (S3B3AM.DAT)               RUN: Site 3 BUILD 3  AM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .1    .0    .0    .0    .0    .0    .0    .0
215.  *    .1    .0    .0    .0    .0    .0    .0    .0
220.  *    .1    .0    .0    .0    .0    .0    .0    .0
225.  *    .1    .0    .0    .0    .0    .0    .0    .0
230.  *    .1    .0    .0    .0    .0    .0    .0    .0
235.  *    .1    .0    .0    .0    .0    .0    .0    .0
240.  *    .1    .1    .0    .0    .0    .0    .0    .0
245.  *    .1    .1    .1    .0    .0    .0    .0    .0
250.  *    .1    .1    .1    .0    .0    .0    .0    .0
255.  *    .1    .1    .1    .1    .0    .0    .0    .0
260.  *    .1    .1    .1    .1    .1    .0    .0    .0
265.  *    .0    .1    .1    .1    .1    .0    .0    .0
270.  *    .0    .1    .1    .1    .1    .0    .0    .0
275.  *    .0    .1    .1    .1    .1    .0    .0    .0
280.  *    .0    .1    .1    .1    .1    .0    .0    .0
285.  *    .0    .1    .1    .1    .1    .0    .0    .0
290.  *    .0    .1    .0    .1    .1    .0    .0    .0
295.  *    .0    .1    .0    .1    .1    .0    .0    .0
300.  *    .0    .1    .0    .1    .1    .0    .0    .0
305.  *    .0    .1    .1    .1    .1    .0    .0    .0
310.  *    .0    .1    .1    .1    .1    .0    .0    .0
315.  *    .0    .1    .1    .1    .1    .0    .0    .0
320.  *    .0    .1    .1    .1    .1    .0    .0    .0
325.  *    .0    .1    .1    .1    .1    .0    .0    .0
330.  *    .0    .1    .1    .1    .1    .0    .0    .0
335.  *    .0    .1    .1    .1    .1    .0    .0    .0
340.  *    .0    .1    .1    .1    .1    .0    .0    .0
345.  *    .0    .1    .1    .1    .1    .0    .0    .0
350.  *    .0    .1    .1    .1    .1    .0    .0    .0
355.  *    .0    .1    .1    .1    .1    .0    .0    .0
360.  *    .0    .1    .1    .1    .0    .0    .0    .0
------*------------------------------------------------
MAX   *    .1    .1    .1    .2    .1    .0    .0    .0
DEGR. *   65     0     0    60    40     0     0     0

THE HIGHEST CONCENTRATION IS      .30 PPM AT   85 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS      .20 PPM AT   70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS      .20 PPM AT   70 DEGREES FROM REC10.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT)               RUN: Site 3 BUILD A3 PM
      DATE: 03/22/2010   TIME: 12:13:22.02


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *    323.0     617.0    -426.0     376.0 *     787.   252. AG   2689.    .8    .0 68.0
       2. EB        Wil T+R   *    323.0     616.0     531.0     681.0 *     218.    73. AG   2449.    .8    .0 68.0
       3. EB        Wil T+R   *    475.0     663.0   -6860.2   -1597.9 *    7676.   253. AG     16. 100.0    .0 48.0 **** 389.9
       4. EB        Wil LT    *    315.0     650.0     513.0     712.0 *     207.    73. AG    240.    .8    .0 44.0
       5. EB        Wil LT    *    444.0     690.0    -868.9     286.8 *    1373.   253. AG     19. 100.0    .0 24.0 ****  69.8
       6. EB        Wil DP    *    532.0     683.0    1471.0     989.0 *     988.    72. AG   2786.    .8    .0 68.0
       7. WB        Wil AP    *    756.0     830.0    1454.0    1051.0 *     732.    72. AG   2876.    .8    .0 68.0
       8. WB        Wil T+R   *    756.0     829.0     484.0     742.0 *     286.   252. AG   2744.    .8    .0 68.0
       9. WB        Wil T+R   *    540.0     760.0    3261.3    1628.8 *    2857.    72. AG     23. 100.0    .0 48.0 1.55 145.1
      10. WB        Wil LT    *    767.0     790.0     513.0     706.0 *     268.   252. AG    132.    .8    .0 32.0
      11. WB        Wil LT    *    566.0     723.0    1685.8    1092.5 *    1179.    72. AG      6. 100.0    .0 12.0 4.40  59.9
      12. WB        Wil DP    *    483.0     742.0    -451.0     441.0 *     981.   252. AG   2979.    .8    .0 68.0
      13. NB        Gln AP    *    542.0     703.0     861.0    -211.0 *     968.   161. AG    855.    .9    .0 32.0
      14. NB        Gln AP    *    564.0     640.0    3371.0   -7417.9 *    8533.   161. AG      7. 100.0    .0 12.0 **** 433.5
      15. NB        Gln DP    *    545.0     705.0    -160.0    1462.0 *    1034.   317. AG    973.    .9    .0 32.0
      16. SB        Gln AP    *    305.0     915.0    -182.0    1445.0 *     720.   317. AG    998.    .9    .0 32.0
      17. SB        Gln T+LT  *    305.0     915.0     479.0     736.0 *     250.   136. AG    708.    .9    .0 44.0
      18. SB        Gln T+LT  *    430.0     786.0    -472.1    1713.8 *    1294.   316. AG     15. 100.0    .0 24.0 1.40  65.7
      19. SB        Gln R     *    300.0     890.0     443.0     732.0 *     213.   138. AG    290.    .9    .0 32.0
      20. SB        Gln R     *    400.0     780.0     315.1     874.3 *     127.   318. AG      6. 100.0    .0 12.0  .41   6.4
      21. SB        Gln DP    *    478.0     734.0     548.0     638.0 *     119.   144. AG    680.    .9    .0 32.0
      22. SB        Gln DP    *    548.0     638.0     840.0    -220.0 *     906.   161. AG    680.    .9    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT)               RUN: Site 3 BUILD A3 PM
      DATE: 03/22/2010   TIME: 12:13:22.02

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL    ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE      RATE
                              *     (SEC)   (SEC)     (SEC)     (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R   *     150       56       2.0       2449         7       4.10      1        3
       5. EB        Wil LT    *     150      129       2.0        240        84       4.10      1        3
       9. WB        Wil T+R   *     150       79       2.0       2744       991       4.10      1        3
      11. WB        Wil LT    *     150       79       2.0        132        68       4.10      1        3
      14. NB        Gln AP    *     150       99       2.0        855       262       4.10      1        3
      18. SB        Gln T+LT  *     150       99       2.0        708       808       4.10      1        3
      20. SB        Gln R     *     150       80       2.0        290      1600       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)           *
         RECEPTOR             *      X          Y          Z         *
     -------------------------*--------------------------------------*
      1. SE MID S             *       685.0      365.0        5.0   *
      2. SE 164 S             *       638.0      508.0        5.0   *
      3. SE 82 S              *       611.0      586.0        5.0   *
      4. SE CNR               *       595.0      659.0        5.0   *
      5. SE 82 E              *       664.0      689.0        5.0   *
      6. SE 164 E             *       742.0      713.0        5.0   *
      7. SE MID E             *       849.0      747.0        5.0   *
      8. NE MID E             *       793.0      878.0        5.0   *
      9. NE 164 E             *       674.0      839.0        5.0   *
     10. NE 82 E              *       595.0      813.0        5.0   *
     11. NE CNR               *       515.0      792.0        5.0   *
     12. NE 82 N              *       452.0      847.0        5.0   *
     13. NE 164 N             *       396.0      907.0        5.0   *
     14. NE MID N             *       319.0      990.0        5.0   *
     15. NW MID N             *       190.0      983.0        5.0   *
     16. NW 164 N             *       267.0      900.0        5.0   *
     17. NW 82 N              *       323.0      841.0        5.0   *
     18. NW CNR               *       381.0      759.0        5.0   *
     19. NW 82 W              *       299.0      719.0        5.0   *
     20. NW 164 W             *       222.0      694.0        5.0   *
     21. NW MID W             *       107.0      658.0        5.0   *
     22. SW MID W             *       213.0      548.0        5.0   *
     23. SW 164 W             *       367.0      595.0        5.0   *
     24. SW 82 W              *       447.0      619.0        5.0   *
     25. SW CNR               *       518.0      634.0        5.0   *
     26. SW 82 S              *       550.0      565.0        5.0   *
     27. SW 164 S             *       577.0      487.0        5.0   *
     28. SW MID S             *       622.0      354.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT)               RUN: Site 3 BUILD A3 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
  0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 65.  *    .0    .0    .0    .1    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
 70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 80.  *    .0    .0    .0    .0    .1    .1    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
140.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
150.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
155.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
160.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
165.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
170.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
175.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
180.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
185.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
190.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                     PAGE  4
     JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT)              RUN: Site 3 BUILD A3 PM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
225.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
245.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
250.  *    .0    .0    .0    .0    .0    .1    .1    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
255.  *    .0    .0    .0    .0    .1    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
------*------------------------------------------------------------------------------------------------------------------------
MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
DEGR. *     0     0     0     0     0     0     0    65    90    70    75     0     0     0     0     0     0   105    70    65

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                                                                                                                     PAGE  5
     JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT)              RUN: Site 3 BUILD A3 PM

      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
   5.  *    .0    .1    .1    .1    .0    .0    .0    .0
  10.  *    .0    .1    .1    .1    .0    .0    .0    .0
  15.  *    .0    .1    .1    .1    .0    .0    .0    .0
  20.  *    .0    .2    .2    .1    .0    .0    .0    .0
  25.  *    .0    .2    .2    .1    .0    .0    .0    .0
  30.  *    .0    .2    .2    .1    .0    .0    .0    .0
  35.  *    .0    .2    .2    .1    .1    .0    .0    .0
  40.  *    .0    .2    .2    .1    .1    .0    .0    .0
  45.  *    .0    .2    .2    .1    .1    .0    .0    .0
  50.  *    .0    .2    .2    .1    .1    .0    .0    .0
  55.  *    .0    .2    .1    .1    .1    .0    .0    .0
  60.  *    .0    .2    .1    .2    .1    .0    .0    .0
  65.  *    .1    .2    .1    .1    .1    .0    .0    .0
  70.  *    .1    .1    .1    .1    .1    .0    .0    .0
  75.  *    .1    .0    .1    .0    .1    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .1    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE  6
      JOB: Site 3 Glendon & Wilshire (S3B3PM.DAT)              RUN: Site 3 BUILD A3 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .0    .0    .0    .0    .0    .0
 250.  *    .1    .2    .2    .1    .0    .0    .0    .0
 255.  *    .1    .2    .2    .1    .1    .0    .0    .0
 260.  *    .1    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .2    .2    .2    .2    .0    .0    .0
 275.  *    .0    .2    .2    .2    .2    .0    .0    .0
 280.  *    .0    .2    .2    .2    .1    .0    .0    .0
 285.  *    .0    .2    .2    .2    .1    .0    .0    .0
 290.  *    .0    .2    .1    .2    .1    .0    .0    .0
 295.  *    .0    .2    .1    .2    .1    .0    .0    .0
 300.  *    .0    .2    .1    .2    .1    .0    .0    .0
 305.  *    .0    .2    .1    .2    .1    .0    .0    .0
 310.  *    .0    .1    .0    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .1    .0    .0    .0
 340.  *    .0    .1    .1    .1    .1    .0    .0    .0
 345.  *    .0    .1    .1    .1    .1    .0    .0    .0
 350.  *    .0    .1    .1    .1    .1    .0    .0    .0
 355.  *    .0    .1    .1    .1    .0    .0    .0    .0
 360.  *    .0    .1    .1    .1    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .1    .2    .2    .2    .2    .0    .0    .0
 DEGR. *   65    20    20    60   260     0     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   90 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   65 DEGREES FROM REC8 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC10.
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT)             RUN: Site 3 BUILD 4  AM
      DATE: 03/22/2010   TIME: 11:38:57.92


       SITE & METEOROLOGICAL VARIABLES
       --------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)         *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *     323.0     617.0    -426.0     376.0 *      787.  252. AG    2883.     .8     .0 68.0
       2. EB        Wil T+R   *     323.0     616.0     531.0     681.0 *      218.   73. AG    2701.     .8     .0 68.0
       3. EB        Wil T+R   *     475.0     663.0     270.0     599.8 *      214.  253. AG      11. 100.0     .0 48.0  .95  10.9
       4. EB        Wil LT    *     315.0     650.0     513.0     712.0 *      207.   73. AG     182.     .8     .0 44.0
       5. EB        Wil LT    *     444.0     690.0    -550.2     384.7 *     1040.  253. AG      19. 100.0     .0 24.0 ****  52.8
       6. EB        Wil DP    *     532.0     683.0    1471.0     989.0 *      988.   72. AG    2517.     .8     .0 68.0
       7. WB        Wil AP    *     756.0     830.0    1454.0    1051.0 *      732.   72. AG    3126.     .8     .0 68.0
       8. WB        Wil T+R   *     756.0     829.0     484.0     742.0 *      286.  252. AG    3030.     .8     .0 68.0
       9. WB        Wil T+R   *     540.0     760.0    2705.6    1451.4 *     2273.   72. AG      18. 100.0     .0 48.0 1.34 115.5
      10. WB        Wil LT    *     767.0     790.0     513.0     706.0 *      268.  252. AG      96.     .8     .0 32.0
      11. WB        Wil LT    *     566.0     723.0    1294.5     963.4 *      767.   72. AG       4. 100.0     .0 12.0 3.20  39.0
      12. WB        Wil DP    *     483.0     742.0    -451.0     441.0 *      981.  252. AG    2821.     .8     .0 68.0
      13. NB        Gln AP    *     542.0     703.0     861.0    -211.0 *      968.  161. AG     371.     .9     .0 32.0
      14. NB        Gln AP    *     564.0     640.0    1976.7   -3415.2 *     4294.  161. AG       9. 100.0     .0 12.0 **** 218.1
      15. NB        Gln DP    *     545.0     705.0    -160.0    1462.0 *     1034.  317. AG     928.     .9     .0 32.0
      16. SB        Gln AP    *     305.0     915.0    -182.0    1445.0 *      720.  317. AG     583.     .9     .0 32.0
      17. SB        Gln T+LT  *     305.0     915.0     479.0     736.0 *      250.  136. AG     363.     .9     .0 44.0
      18. SB        Gln T+LT  *     430.0     786.0      -4.5    1232.9 *      623.  316. AG      17. 100.0     .0 24.0 1.32  31.7
      19. SB        Gln R     *     300.0     890.0     443.0     732.0 *      213.  138. AG     220.     .9     .0 32.0
      20. SB        Gln R     *     400.0     780.0     320.3     868.5 *      119.  318. AG       7. 100.0     .0 12.0  .44   6.1
      21. SB        Gln DP    *     478.0     734.0     548.0     638.0 *      119.  144. AG     697.     .9     .0 32.0
      22. SB        Gln DP    *     548.0     638.0     840.0    -220.0 *      906.  161. AG     697.     .9     .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT)             RUN: Site 3 BUILD 4  AM
      DATE: 03/22/2010   TIME: 11:38:57.92

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)     (SEC)     (VPH)      (VPH)   (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R   *     150        39       2.0      2701        994      4.10      1        3
       5. EB        Wil LT    *     150       131       2.0       182         84      4.10      1        3
       9. WB        Wil T+R   *     150        60       2.0      3030        990      4.10      1        3
      11. WB        Wil LT    *     150        60       2.0        96         53      4.10      1        3
      14. NB        Gln AP    *     150       116       2.0       371         64      4.10      1        3
      18. SB        Gln T+LT  *     150       116       2.0       363        689      4.10      1        3
      20. SB        Gln R     *     150        99       2.0       220       1600      4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)         *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*-------------------------------------*
      1. SE MID S             *       685.0      365.0       5.0    *
      2. SE 164 S             *       638.0      508.0       5.0    *
      3. SE 82 S              *       611.0      586.0       5.0    *
      4. SE CNR               *       595.0      659.0       5.0    *
      5. SE 82 E              *       664.0      689.0       5.0    *
      6. SE 164 E             *       742.0      713.0       5.0    *
      7. SE MID E             *       849.0      747.0       5.0    *
      8. NE MID E             *       793.0      878.0       5.0    *
      9. NE 164 E             *       674.0      839.0       5.0    *
     10. NE 82 E              *       595.0      813.0       5.0    *
     11. NE CNR               *       515.0      792.0       5.0    *
     12. NE 82 N              *       452.0      847.0       5.0    *
     13. NE 164 N             *       396.0      907.0       5.0    *
     14. NE MID N             *       319.0      990.0       5.0    *
     15. NW MID N             *       190.0      983.0       5.0    *
     16. NW 164 N             *       267.0      900.0       5.0    *
     17. NW 82 N              *       323.0      841.0       5.0    *
     18. NW CNR               *       381.0      759.0       5.0    *
     19. NW 82 W              *       299.0      719.0       5.0    *
     20. NW 164 W             *       222.0      694.0       5.0    *
     21. NW MID W             *       107.0      658.0       5.0    *
     22. SW MID W             *       213.0      548.0       5.0    *
     23. SW 164 W             *       367.0      595.0       5.0    *
     24. SW 82 W              *       447.0      619.0       5.0    *
     25. SW CNR               *       518.0      634.0       5.0    *
     26. SW 82 S              *       550.0      565.0       5.0    *
     27. SW 164 S             *       577.0      487.0       5.0    *
     28. SW MID S             *       622.0      354.0       5.0    *
1
                                                                                                                 PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT)             RUN: Site 3 BUILD 4  AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
  0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 80.  *    .0    .0    .0    .0    .1    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
135.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
140.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
145.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
150.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
155.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
160.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
165.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
170.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
175.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
180.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
190.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                        PAGE  4
     JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT)              RUN: Site 3 BUILD 4  AM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
225.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
245.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
250.  *    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
255.  *    .0    .0    .0    .0    .0    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
------*------------------------------------------------------------------------------------------------------------------------
MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
DEGR. *    0     0     0     0     0     0     0    70    85    70    75     0     0     0     0     0     0   105    70    70

1
                                                                                                                        PAGE  5
     JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT)              RUN: Site 3 BUILD 4  AM

      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
  5.  *    .0    .1    .1    .1    .0    .0    .0    .0
 10.  *    .0    .1    .1    .1    .0    .0    .0    .0
 15.  *    .0    .1    .1    .1    .0    .0    .0    .0
 20.  *    .0    .1    .1    .1    .0    .0    .0    .0
 25.  *    .0    .1    .1    .1    .0    .0    .0    .0
 30.  *    .0    .1    .1    .1    .0    .0    .0    .0
 35.  *    .0    .1    .1    .1    .0    .0    .0    .0
 40.  *    .0    .1    .1    .1    .1    .0    .0    .0
 45.  *    .0    .1    .1    .1    .1    .0    .0    .0
 50.  *    .0    .1    .1    .1    .1    .0    .0    .0
 55.  *    .0    .1    .1    .1    .1    .0    .0    .0
 60.  *    .0    .1    .1    .1    .1    .0    .0    .0
 65.  *    .1    .1    .1    .2    .1    .0    .0    .0
 70.  *    .1    .1    .1    .0    .1    .0    .0    .0
 75.  *    .1    .1    .1    .0    .0    .0    .0    .0
 80.  *    .1    .0    .0    .0    .0    .0    .0    .0
 85.  *    .1    .0    .0    .0    .0    .0    .0    .0
 90.  *    .1    .0    .0    .0    .0    .0    .0    .0
 95.  *    .1    .0    .0    .0    .0    .0    .0    .0
100.  *    .1    .0    .0    .0    .0    .0    .0    .0
105.  *    .1    .0    .0    .0    .0    .0    .0    .0
110.  *    .1    .0    .0    .0    .0    .0    .0    .0
115.  *    .1    .0    .0    .0    .0    .0    .0    .0
120.  *    .1    .0    .0    .0    .0    .0    .0    .0
125.  *    .1    .0    .0    .0    .0    .0    .0    .0
130.  *    .1    .0    .0    .0    .0    .0    .0    .0
135.  *    .1    .0    .0    .0    .0    .0    .0    .0
140.  *    .1    .0    .0    .0    .0    .0    .0    .0
145.  *    .1    .0    .0    .0    .0    .0    .0    .0
150.  *    .1    .0    .0    .0    .0    .0    .0    .0
155.  *    .1    .0    .0    .0    .0    .0    .0    .0
160.  *    .1    .0    .0    .0    .0    .0    .0    .0
165.  *    .1    .0    .0    .0    .0    .0    .0    .0
170.  *    .1    .0    .0    .0    .0    .0    .0    .0
175.  *    .1    .0    .0    .0    .0    .0    .0    .0
180.  *    .1    .0    .0    .0    .0    .0    .0    .0
185.  *    .1    .0    .0    .0    .0    .0    .0    .0
190.  *    .1    .0    .0    .0    .0    .0    .0    .0
195.  *    .1    .0    .0    .0    .0    .0    .0    .0
200.  *    .1    .0    .0    .0    .0    .0    .0    .0
205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                            PAGE  6
     JOB: Site 3 Glendon & Wilshire (S3B4AM.DAT)              RUN: Site 3 BUILD 4  AM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .1    .0    .0    .0    .0    .0    .0    .0
215.  *    .1    .0    .0    .0    .0    .0    .0    .0
220.  *    .1    .0    .0    .0    .0    .0    .0    .0
225.  *    .1    .0    .0    .0    .0    .0    .0    .0
230.  *    .1    .0    .0    .0    .0    .0    .0    .0
235.  *    .1    .0    .0    .0    .0    .0    .0    .0
240.  *    .1    .1    .0    .0    .0    .0    .0    .0
245.  *    .1    .1    .1    .0    .0    .0    .0    .0
250.  *    .1    .1    .1    .0    .0    .0    .0    .0
255.  *    .1    .1    .1    .1    .0    .0    .0    .0
260.  *    .1    .1    .1    .1    .1    .0    .0    .0
265.  *    .0    .1    .1    .1    .1    .0    .0    .0
270.  *    .0    .1    .1    .1    .1    .0    .0    .0
275.  *    .0    .1    .1    .1    .1    .0    .0    .0
280.  *    .0    .1    .1    .1    .1    .0    .0    .0
285.  *    .0    .1    .1    .1    .1    .0    .0    .0
290.  *    .0    .1    .0    .1    .1    .0    .0    .0
295.  *    .0    .1    .0    .1    .1    .0    .0    .0
300.  *    .0    .1    .0    .1    .1    .0    .0    .0
305.  *    .0    .1    .1    .1    .1    .0    .0    .0
310.  *    .0    .1    .1    .1    .1    .0    .0    .0
315.  *    .0    .1    .1    .1    .1    .0    .0    .0
320.  *    .0    .1    .1    .1    .1    .0    .0    .0
325.  *    .0    .1    .1    .1    .1    .0    .0    .0
330.  *    .0    .1    .1    .1    .1    .0    .0    .0
335.  *    .0    .1    .1    .1    .1    .0    .0    .0
340.  *    .0    .1    .1    .1    .1    .0    .0    .0
345.  *    .0    .1    .1    .1    .1    .0    .0    .0
350.  *    .0    .1    .1    .1    .1    .0    .0    .0
355.  *    .0    .1    .1    .1    .1    .0    .0    .0
360.  *    .0    .1    .1    .1    .0    .0    .0    .0
------*------------------------------------------------
MAX   *    .1    .1    .1    .2    .1    .0    .0    .0
DEGR. *   65     0     0    65    40     0     0     0

THE HIGHEST CONCENTRATION IS     .30 PPM AT   85 DEGREES FROM REC9 .
THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC8 .
THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC10.
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1                          CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3B4PM.DAT)              RUN: Site 3 BUILD A4 PM
      DATE: 03/22/2010   TIME: 11:53:49.19


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*--------------------------------------------------------------
       1. EB        Wil AP    *   323.0     617.0    -426.0     376.0 *     787.   252. AG   2660.    .8    .0 68.0
       2. EB        Wil T+R   *   323.0     616.0     531.0     681.0 *     218.    73. AG   2445.    .8    .0 68.0
       3. EB        Wil T+R   *   475.0     663.0   -6848.2   -1594.2 *    7663.   253. AG     16. 100.0    .0 48.0 **** 389.3
       4. EB        Wil LT    *   315.0     650.0     513.0     712.0 *     207.    73. AG    205.    .8    .0 44.0
       5. EB        Wil LT    *   444.0     690.0    -679.4     345.0 *    1175.   253. AG     19. 100.0    .0 24.0 ****  59.7
       6. EB        Wil DP    *   532.0     683.0    1471.0     989.0 *     988.    72. AG   2820.    .8    .0 68.0
       7. WB        Wil AP    *   756.0     830.0    1454.0    1051.0 *     732.    72. AG   2950.    .8    .0 68.0
       8. WB        Wil T+R   *   756.0     829.0     484.0     742.0 *     286.   252. AG   2818.    .8    .0 68.0
       9. WB        Wil T+R   *   540.0     760.0    3310.0    1644.3 *    2908.    72. AG     23. 100.0    .0 48.0 1.55 147.7
      10. WB        Wil LT    *   767.0     790.0     513.0     706.0 *     268.   252. AG    132.    .8    .0 32.0
      11. WB        Wil LT    *   566.0     723.0    1684.4    1092.0 *    1178.    72. AG      6. 100.0    .0 12.0 4.40  59.8
      12. WB        Wil DP    *   483.0     742.0    -451.0     441.0 *     981.   252. AG   3022.    .8    .0 68.0
      13. NB        Gln AP    *   542.0     703.0     861.0    -211.0 *     968.   161. AG    880.    .9    .0 32.0
      14. NB        Gln AP    *   564.0     640.0    3436.0   -7604.3 *    8730.   161. AG      7. 100.0    .0 12.0 **** 443.5
      15. NB        Gln DP    *   545.0     705.0    -160.0    1462.0 *    1034.   317. AG   1010.    .9    .0 32.0
      16. SB        Gln AP    *   305.0     915.0    -182.0    1445.0 *     720.   317. AG   1034.    .9    .0 32.0
      17. SB        Gln T+LT  *   305.0     915.0     479.0     736.0 *     250.   136. AG    727.    .9    .0 44.0
      18. SB        Gln T+LT  *   430.0     786.0    -574.2    1818.9 *    1441.   316. AG     15. 100.0    .0 24.0 1.46  73.2
      19. SB        Gln R     *   300.0     890.0     443.0     732.0 *     213.   138. AG    307.    .9    .0 32.0
      20. SB        Gln R     *   400.0     780.0     307.9     882.3 *     138.   318. AG      6. 100.0    .0 12.0  .45   7.0
      21. SB        Gln DP    *   478.0     734.0     548.0     638.0 *     119.   144. AG    672.    .9    .0 32.0
      22. SB        Gln DP    *   548.0     638.0     840.0    -220.0 *     906.   161. AG    672.    .9    .0 32.0
1
                                                                                                                           PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3B4PM.DAT)              RUN: Site 3 BUILD A4 PM
      DATE: 03/22/2010   TIME: 11:53:49.19

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Wil T+R   *     150       56       2.0      2445          7       4.10      1        3
       5. EB        Wil LT    *     150      131       2.0       205         84       4.10      1        3
       9. WB        Wil T+R   *     150       77       2.0      2818        990       4.10      1        3
      11. WB        Wil LT    *     150       77       2.0       132         66       4.10      1        3
      14. NB        Gln AP    *     150       99       2.0       880        282       4.10      1        3
      18. SB        Gln T+LT  *     150       99       2.0       727        794       4.10      1        3
      20. SB        Gln R     *     150       82       2.0       307       1600       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)         *
         RECEPTOR             *      X          Y          Z      *
     -------------------------*-----------------------------------*
      1. SE MID S             *       685.0      365.0       5.0   *
      2. SE 164 S             *       638.0      508.0       5.0   *
      3. SE 82 S              *       611.0      586.0       5.0   *
      4. SE CNR               *       595.0      659.0       5.0   *
      5. SE 82 E              *       664.0      689.0       5.0   *
      6. SE 164 E             *       742.0      713.0       5.0   *
      7. SE MID E             *       849.0      747.0       5.0   *
      8. NE MID E             *       793.0      878.0       5.0   *
      9. NE 164 E             *       674.0      839.0       5.0   *
     10. NE 82 E              *       595.0      813.0       5.0   *
     11. NE CNR               *       515.0      792.0       5.0   *
     12. NE 82 N              *       452.0      847.0       5.0   *
     13. NE 164 N             *       396.0      907.0       5.0   *
     14. NE MID N             *       319.0      990.0       5.0   *
     15. NW MID N             *       190.0      983.0       5.0   *
     16. NW 164 N             *       267.0      900.0       5.0   *
     17. NW 82 N              *       323.0      841.0       5.0   *
     18. NW CNR               *       381.0      759.0       5.0   *
     19. NW 82 W              *       299.0      719.0       5.0   *
     20. NW 164 W             *       222.0      694.0       5.0   *
     21. NW MID W             *       107.0      658.0       5.0   *
     22. SW MID W             *       213.0      548.0       5.0   *
     23. SW 164 W             *       367.0      595.0       5.0   *
     24. SW 82 W              *       447.0      619.0       5.0   *
     25. SW CNR               *       518.0      634.0       5.0   *
     26. SW 82 S              *       550.0      565.0       5.0   *
     27. SW 164 S             *       577.0      487.0       5.0   *
     28. SW MID S             *       622.0      354.0       5.0   *
1
                                                                                                                           PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3B4PM.DAT)              RUN: Site 3 BUILD A4 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  80.  *    .0    .0    .0    .0    .1    .1    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 155.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 160.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 165.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 170.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 175.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 190.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                       PAGE  4
      JOB: Site 3 Glendon & Wilshire (S3B4PM.DAT)              RUN: Site 3 BUILD A4 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 225.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .0    .0    .0    .0    .0    .1    .1    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 255.  *    .0    .0    .0    .0    .1    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 ------*-------------------------------------------------------------------------------------------------------------------------
 MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 DEGR. *    0     0     0     0     0     0     0    70    90    70    75     0     0     0     0     0     0   100    70    65

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                                                                                                                       PAGE  5
      JOB: Site 3 Glendon & Wilshire (S3B4PM.DAT)              RUN: Site 3 BUILD A4 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
   5.  *    .0    .1    .1    .1    .0    .0    .0    .0
  10.  *    .0    .1    .1    .1    .0    .0    .0    .0
  15.  *    .0    .1    .1    .1    .0    .0    .0    .0
  20.  *    .0    .2    .2    .1    .0    .0    .0    .0
  25.  *    .0    .2    .2    .1    .0    .0    .0    .0
  30.  *    .0    .2    .2    .1    .0    .0    .0    .0
  35.  *    .0    .2    .2    .1    .1    .0    .0    .0
  40.  *    .0    .2    .2    .1    .1    .0    .0    .0
  45.  *    .0    .2    .2    .1    .1    .0    .0    .0
  50.  *    .0    .2    .2    .1    .1    .0    .0    .0
  55.  *    .0    .2    .1    .1    .1    .0    .0    .0
  60.  *    .0    .2    .1    .2    .1    .0    .0    .0
  65.  *    .1    .2    .1    .1    .1    .0    .0    .0
  70.  *    .1    .1    .1    .1    .1    .0    .0    .0
  75.  *    .1    .0    .1    .0    .1    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .1    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE  6
      JOB: Site 3 Glendon & Wilshire (S3B4PM.DAT)              RUN: Site 3 BUILD A4 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .0    .0    .0    .0    .0    .0
 250.  *    .1    .2    .2    .1    .0    .0    .0    .0
 255.  *    .1    .2    .2    .1    .1    .0    .0    .0
 260.  *    .1    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .2    .2    .2    .2    .0    .0    .0
 275.  *    .0    .2    .2    .2    .2    .0    .0    .0
 280.  *    .0    .2    .2    .2    .1    .0    .0    .0
 285.  *    .0    .2    .1    .2    .1    .0    .0    .0
 290.  *    .0    .2    .1    .2    .1    .0    .0    .0
 295.  *    .0    .2    .1    .2    .1    .0    .0    .0
 300.  *    .0    .2    .1    .2    .1    .0    .0    .0
 305.  *    .0    .2    .1    .2    .1    .0    .0    .0
 310.  *    .0    .1    .0    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .1    .0    .0    .0
 340.  *    .0    .1    .1    .1    .1    .0    .0    .0
 345.  *    .0    .1    .1    .1    .1    .0    .0    .0
 350.  *    .0    .1    .1    .1    .1    .0    .0    .0
 355.  *    .0    .1    .1    .1    .0    .0    .0    .0
 360.  *    .0    .1    .1    .1    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .1    .2    .2    .2    .2    .0    .0    .0
 DEGR. *   65    20    20    60   260     0     0     0

 THE HIGHEST CONCENTRATION IS      .30 PPM AT   90 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS      .20 PPM AT   70 DEGREES FROM REC8 .
 THE 3RD HIGHEST CONCENTRATION IS      .20 PPM AT   70 DEGREES FROM REC10.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT)               RUN: Site 3 BUILD 5  AM
      DATE: 03/22/2010   TIME: 11:45:12.84


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE  VPH    EF       H   W    V/C QUEUE
                              *   X1         Y1       X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Wil AP    *    323.0     617.0    -426.0     376.0 *     787.   252. AG   2901.    .8    .0 68.0
       2. EB        Wil T+R   *    323.0     616.0     531.0     681.0 *     218.    73. AG   2690.    .8    .0 68.0
       3. EB        Wil T+R   *    475.0     663.0     148.6     562.4 *     342.   253. AG     13. 100.0    .0 48.0 1.01  17.4
       4. EB        Wil LT    *    315.0     650.0     513.0     712.0 *     207.    73. AG    211.    .8    .0 44.0
       5. EB        Wil LT    *    444.0     690.0    -792.4     310.3 *    1293.   253. AG     20. 100.0    .0 24.0 ****  65.7
       6. EB        Wil DP    *    532.0     683.0    1471.0     989.0 *     988.    72. AG   2446.    .8    .0 68.0
       7. WB        Wil AP    *    756.0     830.0    1454.0    1051.0 *     732.    72. AG   3128.    .8    .0 68.0
       8. WB        Wil T+R   *    756.0     829.0     484.0     742.0 *     286.   252. AG   3032.    .8    .0 68.0
       9. WB        Wil T+R   *    540.0     760.0    2715.5    1454.5 *    2284.    72. AG     18. 100.0    .0 48.0 1.34 116.0
      10. WB        Wil LT    *    767.0     790.0     513.0     706.0 *     268.   252. AG     96.    .8    .0 32.0
      11. WB        Wil LT    *    566.0     723.0    1294.5     963.4 *     767.    72. AG      4. 100.0    .0 12.0 3.20  39.0
      12. WB        Wil DP    *    483.0     742.0    -451.0     441.0 *     981.   252. AG   2795.    .8    .0 68.0
      13. NB        Gln AP    *    542.0     703.0     861.0    -211.0 *     968.   161. AG    374.    .9    .0 32.0
      14. NB        Gln AP    *    564.0     640.0    1847.0   -3043.1 *    3900.   161. AG      8. 100.0    .0 12.0 **** 198.1
      15. NB        Gln DP    *    545.0     705.0    -160.0    1462.0 *    1034.   317. AG    975.    .9    .0 32.0
      16. SB        Gln AP    *    305.0     915.0    -182.0    1445.0 *     720.   317. AG    574.    .9    .0 32.0
      17. SB        Gln T+LT  *    305.0     915.0     479.0     736.0 *     250.   136. AG    367.    .9    .0 44.0
      18. SB        Gln T+LT  *    430.0     786.0     251.4     969.7 *     256.   316. AG     16. 100.0    .0 24.0 1.05  13.0
      19. SB        Gln R     *    300.0     890.0     443.0     732.0 *     213.   138. AG    207.    .9    .0 32.0
      20. SB        Gln R     *    400.0     780.0     325.0     863.3 *     112.   318. AG      7. 100.0    .0 12.0  .41   5.7
      21. SB        Gln DP    *    478.0     734.0     548.0     638.0 *     119.   144. AG    761.    .9    .0 32.0
      22. SB        Gln DP    *    548.0     638.0     840.0    -220.0 *     906.   161. AG    761.    .9    .0 32.0
1
                                                                                                                 PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT)               RUN: Site 3 BUILD 5  AM
      DATE: 03/22/2010   TIME: 11:45:12.84

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*---------------------------------------------------------------------------------
       3. EB        Wil T+R   *     150       45       2.0      2690        992       4.10      1        3
       5. EB        Wil LT    *     150      137       2.0       211         84       4.10      1        3
       9. WB        Wil T+R   *     150       60       2.0      3032        989       4.10      1        3
      11. WB        Wil LT    *     150       60       2.0        96         53       4.10      1        3
      14. NB        Gln AP    *     150      110       2.0       374        141       4.10      1        3
      18. SB        Gln T+LT  *     150      110       2.0       367        733       4.10      1        3
      20. SB        Gln R     *     150       99       2.0       207       1600       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*-------------------------------------*
      1. SE MID S             *       685.0      365.0        5.0   *
      2. SE 164 S             *       638.0      508.0        5.0   *
      3. SE 82 S              *       611.0      586.0        5.0   *
      4. SE CNR               *       595.0      659.0        5.0   *
      5. SE 82 E              *       664.0      689.0        5.0   *
      6. SE 164 E             *       742.0      713.0        5.0   *
      7. SE MID E             *       849.0      747.0        5.0   *
      8. NE MID E             *       793.0      878.0        5.0   *
      9. NE 164 E             *       674.0      839.0        5.0   *
     10. NE 82 E              *       595.0      813.0        5.0   *
     11. NE CNR               *       515.0      792.0        5.0   *
     12. NE 82 N              *       452.0      847.0        5.0   *
     13. NE 164 N             *       396.0      907.0        5.0   *
     14. NE MID N             *       319.0      990.0        5.0   *
     15. NW MID N             *       190.0      983.0        5.0   *
     16. NW 164 N             *       267.0      900.0        5.0   *
     17. NW 82 N              *       323.0      841.0        5.0   *
     18. NW CNR               *       381.0      759.0        5.0   *
     19. NW 82 W              *       299.0      719.0        5.0   *
     20. NW 164 W             *       222.0      694.0        5.0   *
     21. NW MID W             *       107.0      658.0        5.0   *
     22. SW MID W             *       213.0      548.0        5.0   *
     23. SW 164 W             *       367.0      595.0        5.0   *
     24. SW 82 W              *       447.0      619.0        5.0   *
     25. SW CNR               *       518.0      634.0        5.0   *
     26. SW 82 S              *       550.0      565.0        5.0   *
     27. SW 164 S             *       577.0      487.0        5.0   *
     28. SW MID S             *       622.0      354.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT)               RUN: Site 3 BUILD 5  AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
   5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
  75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  80.  *    .0    .0    .0    .0    .1    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 155.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 160.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 165.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 170.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 175.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 190.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                      PAGE  4
      JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT)               RUN: Site 3 BUILD 5  AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
 225.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 245.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 250.  *    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
 255.  *    .0    .0    .0    .0    .0    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
 265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
 DEGR. *     0     0     0     0     0     0     0    70    85    70    75     0     0     0     0     0     0   105    70    70

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                                                                                                                      PAGE  5
      JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT)               RUN: Site 3 BUILD 5  AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
   5.  *    .0    .1    .1    .1    .0    .0    .0    .0
  10.  *    .0    .1    .1    .1    .0    .0    .0    .0
  15.  *    .0    .1    .1    .1    .0    .0    .0    .0
  20.  *    .0    .1    .1    .1    .0    .0    .0    .0
  25.  *    .0    .1    .1    .1    .0    .0    .0    .0
  30.  *    .0    .1    .1    .1    .0    .0    .0    .0
  35.  *    .0    .1    .1    .1    .0    .0    .0    .0
  40.  *    .0    .1    .1    .1    .1    .0    .0    .0
  45.  *    .0    .2    .1    .1    .1    .0    .0    .0
  50.  *    .0    .2    .1    .1    .1    .0    .0    .0
  55.  *    .0    .2    .1    .1    .1    .0    .0    .0
  60.  *    .0    .1    .1    .1    .1    .0    .0    .0
  65.  *    .1    .1    .1    .1    .1    .0    .0    .0
  70.  *    .1    .1    .1    .0    .1    .0    .0    .0
  75.  *    .1    .1    .1    .0    .0    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .1    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
      JOB: Site 3 Glendon & Wilshire (S3B5AM.DAT)              RUN: Site 3 BUILD 5  AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .1    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .1    .0    .0    .0    .0    .0
 250.  *    .1    .1    .1    .0    .0    .0    .0    .0
 255.  *    .1    .1    .1    .1    .0    .0    .0    .0
 260.  *    .1    .1    .1    .2    .1    .0    .0    .0
 265.  *    .0    .1    .1    .1    .1    .0    .0    .0
 270.  *    .0    .1    .1    .2    .1    .0    .0    .0
 275.  *    .0    .1    .1    .2    .1    .0    .0    .0
 280.  *    .0    .1    .1    .1    .1    .0    .0    .0
 285.  *    .0    .1    .1    .1    .1    .0    .0    .0
 290.  *    .0    .1    .0    .1    .1    .0    .0    .0
 295.  *    .0    .1    .0    .1    .1    .0    .0    .0
 300.  *    .0    .1    .0    .1    .1    .0    .0    .0
 305.  *    .0    .1    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .1    .0    .0    .0
 340.  *    .0    .1    .1    .1    .1    .0    .0    .0
 345.  *    .0    .1    .1    .1    .1    .0    .0    .0
 350.  *    .0    .1    .1    .1    .1    .0    .0    .0
 355.  *    .0    .1    .1    .1    .1    .0    .0    .0
 360.  *    .0    .1    .1    .1    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .1    .2    .1    .2    .1    .0    .0    .0
 DEGR. *   65    45     0   260    40     0     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   85 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC8 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC10.
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1                        CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT)              RUN: Site 3 BUILD A5 PM
      DATE: 03/22/2010   TIME: 12:01:57.15


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*--------------------------------------*-------------------------------------------------------------
       1. EB        Wil AP    *    323.0     617.0    -426.0     376.0 *     787.   252. AG   2699.    .8    .0 68.0
       2. EB        Wil T+R   *    323.0     616.0     531.0     681.0 *     218.    73. AG   2469.    .8    .0 68.0
       3. EB        Wil T+R   *    475.0     663.0   -6920.5   -1616.4 *    7739.   253. AG     16. 100.0    .0 48.0 **** 393.1
       4. EB        Wil LT    *    315.0     650.0     513.0     712.0 *     207.    73. AG    230.    .8    .0 44.0
       5. EB        Wil LT    *    444.0     690.0    -831.6     298.3 *    1334.   253. AG     19. 100.0    .0 24.0 ****  67.8
       6. EB        Wil DP    *    532.0     683.0    1471.0     989.0 *     988.    72. AG   2814.    .8    .0 68.0
       7. WB        Wil AP    *    756.0     830.0    1454.0    1051.0 *     732.    72. AG   2904.    .8    .0 68.0
       8. WB        Wil T+R   *    756.0     829.0     484.0     742.0 *     286.   252. AG   2772.    .8    .0 68.0
       9. WB        Wil T+R   *    540.0     760.0    3270.5    1631.7 *    2866.    72. AG     23. 100.0    .0 48.0 1.55 145.6
      10. WB        Wil LT    *    767.0     790.0     513.0     706.0 *     268.   252. AG    132.    .8    .0 32.0
      11. WB        Wil LT    *    566.0     723.0    1685.1    1092.2 *    1178.    72. AG      6. 100.0    .0 12.0 4.40  59.9
      12. WB        Wil DP    *    483.0     742.0    -451.0     441.0 *     981.   252. AG   2979.    .8    .0 68.0
      13. NB        Gln AP    *    542.0     703.0     861.0    -211.0 *     968.   161. AG    881.    .9    .0 32.0
      14. NB        Gln AP    *    564.0     640.0    3435.5   -7602.9 *    8729.   161. AG      7. 100.0    .0 12.0 9.90 443.4
      15. NB        Gln DP    *    545.0     705.0    -160.0    1462.0 *    1034.   317. AG   1031.    .9    .0 32.0
      16. SB        Gln AP    *    305.0     915.0    -182.0    1445.0 *     720.   317. AG   1010.    .9    .0 32.0
      17. SB        Gln T+LT  *    305.0     915.0     479.0     736.0 *     250.   136. AG    705.    .9    .0 44.0
      18. SB        Gln T+LT  *    430.0     786.0    -471.2    1712.9 *    1293.   316. AG     15. 100.0    .0 24.0 1.40  65.7
      19. SB        Gln R     *    300.0     890.0     443.0     732.0 *     213.   138. AG    305.    .9    .0 32.0
      20. SB        Gln R     *    400.0     780.0     309.6     880.4 *     135.   318. AG      6. 100.0    .0 12.0  .44   6.9
      21. SB        Gln DP    *    478.0     734.0     548.0     638.0 *     119.   144. AG    670.    .9    .0 32.0
      22. SB        Gln DP    *    548.0     638.0     840.0    -220.0 *     906.   161. AG    670.    .9    .0 32.0
1
                                                                                                               PAGE  2
      JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT)              RUN: Site 3 BUILD A5 PM
      DATE: 03/22/2010   TIME: 12:01:57.15

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL    ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE      RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*------------------------------------------------------------------------------
       3. EB        Wil T+R   *     150       56       2.0       2469          7       4.10     1        3
       5. EB        Wil LT    *     150      130       2.0        230         84       4.10     1        3
       9. WB        Wil T+R   *     150       78       2.0       2772        989       4.10     1        3
      11. WB        Wil LT    *     150       78       2.0        132         68       4.10     1        3
      14. NB        Gln AP    *     150       99       2.0        881        285       4.10     1        3
      18. SB        Gln T+LT  *     150       99       2.0        705        804       4.10     1        3
      20. SB        Gln R     *     150       81       2.0        305       1600       4.10     1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       685.0      365.0        5.0   *
      2. SE 164 S             *       638.0      508.0        5.0   *
      3. SE 82 S              *       611.0      586.0        5.0   *
      4. SE CNR               *       595.0      659.0        5.0   *
      5. SE 82 E              *       664.0      689.0        5.0   *
      6. SE 164 E             *       742.0      713.0        5.0   *
      7. SE MID E             *       849.0      747.0        5.0   *
      8. NE MID E             *       793.0      878.0        5.0   *
      9. NE 164 E             *       674.0      839.0        5.0   *
     10. NE 82 E              *       595.0      813.0        5.0   *
     11. NE CNR               *       515.0      792.0        5.0   *
     12. NE 82 N              *       452.0      847.0        5.0   *
     13. NE 164 N             *       396.0      907.0        5.0   *
     14. NE MID N             *       319.0      990.0        5.0   *
     15. NW MID N             *       190.0      983.0        5.0   *
     16. NW 164 N             *       267.0      900.0        5.0   *
     17. NW 82 N              *       323.0      841.0        5.0   *
     18. NW CNR               *       381.0      759.0        5.0   *
     19. NW 82 W              *       299.0      719.0        5.0   *
     20. NW 164 W             *       222.0      694.0        5.0   *
     21. NW MID W             *       107.0      658.0        5.0   *
     22. SW MID W             *       213.0      548.0        5.0   *
     23. SW 164 W             *       367.0      595.0        5.0   *
     24. SW 82 W              *       447.0      619.0        5.0   *
     25. SW CNR               *       518.0      634.0        5.0   *
     26. SW 82 S              *       550.0      565.0        5.0   *
     27. SW 164 S             *       577.0      487.0        5.0   *
     28. SW MID S             *       622.0      354.0        5.0   *
1
                                                                                                               PAGE  3
      JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT)              RUN: Site 3 BUILD A5 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
```

```
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
  0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
  5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 10.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 15.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 20.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 25.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 65.  *    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1
 70.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1
 75.  *    .0    .0    .0    .1    .1    .1    .1    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 80.  *    .0    .0    .0    .0    .1    .1    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 85.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 90.  *    .0    .0    .0    .0    .0    .0    .0    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
 95.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1
105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
130.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
135.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
140.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
145.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
150.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
155.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
160.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
165.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
170.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
175.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
180.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
185.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
190.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
195.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
200.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
205.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
1
                                                                                                                     PAGE  4
      JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT)               RUN: Site 3 BUILD A5 PM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
215.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
220.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1
225.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
230.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
235.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
240.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
245.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
250.  *    .0    .0    .0    .0    .0    .1    .1    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
255.  *    .0    .0    .0    .0    .1    .1    .1    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1
260.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1
265.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
------*------------------------------------------------------------------------------------------------------------------------
MAX   *    .0    .0    .0    .1    .1    .1    .1    .2    .3    .2    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1
DEGR. *     0     0     0     0     0     0     0    70    90    70    75     0     0     0     0     0     0   105    70    65

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                                                                                                                     PAGE  5
      JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT)               RUN: Site 3 BUILD A5 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .1    .1    .1    .0    .0    .0    .0
```

```
   5.  *    .0    .1    .1    .1    .0    .0    .0    .0
  10.  *    .0    .1    .1    .1    .0    .0    .0    .0
  15.  *    .0    .1    .1    .1    .0    .0    .0    .0
  20.  *    .0    .2    .2    .1    .0    .0    .0    .0
  25.  *    .0    .2    .2    .1    .0    .0    .0    .0
  30.  *    .0    .2    .2    .1    .0    .0    .0    .0
  35.  *    .0    .2    .2    .1    .1    .0    .0    .0
  40.  *    .0    .2    .2    .1    .1    .0    .0    .0
  45.  *    .0    .2    .2    .1    .1    .0    .0    .0
  50.  *    .0    .2    .2    .1    .1    .0    .0    .0
  55.  *    .0    .2    .1    .1    .1    .0    .0    .0
  60.  *    .0    .2    .1    .2    .1    .0    .0    .0
  65.  *    .1    .2    .1    .1    .1    .0    .0    .0
  70.  *    .1    .1    .1    .1    .1    .0    .0    .0
  75.  *    .1    .0    .1    .0    .1    .0    .0    .0
  80.  *    .1    .0    .0    .0    .0    .0    .0    .0
  85.  *    .1    .0    .0    .0    .0    .0    .0    .0
  90.  *    .1    .0    .0    .0    .0    .0    .0    .0
  95.  *    .1    .0    .0    .0    .0    .0    .0    .0
 100.  *    .1    .0    .0    .0    .0    .0    .0    .0
 105.  *    .1    .0    .0    .0    .0    .0    .0    .0
 110.  *    .1    .0    .0    .0    .0    .0    .0    .0
 115.  *    .1    .0    .0    .0    .0    .0    .0    .0
 120.  *    .1    .0    .0    .0    .0    .0    .0    .0
 125.  *    .1    .0    .0    .0    .0    .0    .0    .0
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0
 150.  *    .1    .0    .0    .0    .0    .0    .0    .0
 155.  *    .1    .0    .0    .0    .0    .0    .0    .0
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                        PAGE  6
      JOB: Site 3 Glendon & Wilshire (S3B5PM.DAT)               RUN: Site 3 BUILD A5 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .1    .0    .0    .0    .0    .0    .0
 250.  *    .1    .2    .2    .1    .0    .0    .0    .0
 255.  *    .1    .2    .2    .1    .1    .0    .0    .0
 260.  *    .1    .2    .2    .2    .2    .0    .0    .0
 265.  *    .0    .2    .2    .2    .2    .0    .0    .0
 270.  *    .0    .2    .2    .2    .2    .0    .0    .0
 275.  *    .0    .2    .2    .2    .2    .0    .0    .0
 280.  *    .0    .2    .2    .2    .1    .0    .0    .0
 285.  *    .0    .2    .2    .2    .1    .0    .0    .0
 290.  *    .0    .2    .1    .2    .1    .0    .0    .0
 295.  *    .0    .2    .1    .2    .1    .0    .0    .0
 300.  *    .0    .2    .1    .2    .1    .0    .0    .0
 305.  *    .0    .2    .1    .2    .1    .0    .0    .0
 310.  *    .0    .1    .0    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .1    .0    .0    .0
 340.  *    .0    .1    .1    .1    .1    .0    .0    .0
 345.  *    .0    .1    .1    .1    .1    .0    .0    .0
 350.  *    .0    .1    .1    .1    .1    .0    .0    .0
 355.  *    .0    .1    .1    .1    .0    .0    .0    .0
 360.  *    .0    .1    .1    .1    .0    .0    .0    .0
 ------*------------------------------------------------
 MAX   *    .1    .2    .2    .2    .2    .0    .0    .0
 DEGR. *   65    20    20    60   260     0     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   90 DEGREES FROM REC9 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC8 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   70 DEGREES FROM REC10.
```

Site 4 – Beverly & La Cienega Input Files

```
Site 4 Bev & La Cien (S4EXAM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Existing AM                       33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     699 3.3   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     699 3.3   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     699 3.3   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     565 3.3   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  565   20.5 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      53 3.3   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   53   20.5 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      81 3.3   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   81   20.5 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     837 3.3   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1325 3.3   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1055 3.3   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        68       2.0 1055   20.5 1556 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     270 3.3   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  270   20.5 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1331 3.3   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1331 3.3   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1331 3.3   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1331 3.3   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1116 3.3   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.     815 3.3   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        79       2.0  815   20.5 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     202 3.3   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        71       2.0  202   20.5 1353 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 3.3   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        72       2.0   99   20.5  165 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.     965 3.3   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1513 3.3   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1443 3.3   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1443   20.5 1448 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      70 3.3   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        75       2.0   70   20.5  264 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1520 3.3   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4EXPM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Existing PM                       33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1694 3.3   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1694 3.3   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1694 3.3   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1324 3.3   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        70       2.0 1324   20.5 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.     104 3.3   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        63       2.0  104   20.5 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     266 3.3   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       110       2.0  266   20.5 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    1846 3.3   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1139 3.3   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     881 3.3   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  881   20.5 1510 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     258 3.3   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  258   20.5 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.     945 3.3   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.     945 3.3   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.     945 3.3   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.     945 3.3   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1787 3.3   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1271 3.3   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        80       2.0 1271   20.5 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     427 3.3   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        72       2.0  427   20.5 1117 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      89 3.3   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        73       2.0   89   20.5  210 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1669 3.3   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1144 3.3   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1049 3.3   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1049   20.5 1451 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      95 3.3   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        73       2.0   95   20.5  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1304 3.3   0  56   30.
1.0   04 1000.   0Y  5  0 72
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```
Site 4 Bev & La Cien (S4NBAM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 No Build AM                       33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     727 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     727 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     727 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     582 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  582   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      63 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   63   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      82 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   82   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     925 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1616 0.8   0  44   30.
```

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  1
WB        Bev T+R   AG   683.   690.   443.   689.    1242 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        68        2.0 1242   04.1 1565 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     374 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110        2.0  374   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1503 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1503 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1503 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1503 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1534 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1111 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        76        2.0 1111   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     324 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        68        2.0  324   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69        2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1248 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2181 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2162 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80        2.0 2162   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      19 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        78        2.0   19   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2382 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4NBPM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 No Build PM                       33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1848 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1848 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1848 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1625 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        70       2.0 1625   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      57 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        63       2.0   57   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     166 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       110       2.0  166   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2075 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1213 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.      763 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  763   04.1 1583 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.      450 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  450   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.     1281 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.     1281 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.     1281 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.     1281 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.     2649 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.     1806 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1806   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.      438 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  438   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      405 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        68       2.0  405   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.     1973 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.     1517 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.     1505 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1505   04.1 1468 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.       12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.     1898 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4M1AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 MOS 1 AM                          33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     754 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     754 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     754 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     612 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  612   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      59 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        63       2.0   59   04.1 1324 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      83 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   83   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     960 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1591 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1229 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        68       2.0 1229   04.1 1572 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     362 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  362   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1513 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1513 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1513 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1513 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1534 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1144 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        76       2.0 1144   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     329 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        68       2.0  329   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        70       2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1259 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2228 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2209 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        79       2.0 2209   04.1 1477 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      19 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   19   04.1  167 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2413 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4M1PM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 MOS 1 PM                          33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1828 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1828 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1828 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1618 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        70       2.0 1618   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      53 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        63       2.0   53   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     157 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       110       2.0  157   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2103 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1235 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.      771 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.       0.  24   2
       120        70       2.0  771   04.1 1547 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.      464 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.       0.  24   2
       120       110       2.0  464   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.     1222 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.     1222 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.     1222 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.     1222 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.     2714 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.     1849 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.       0.  24   2
       120        75       2.0 1849   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.      473 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.       0.  12   1
       120        67       2.0  473   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      392 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.       0.  12   1
       120        68       2.0  392   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.     2063 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.     1532 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.     1520 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.       0.  36   3
       120        80       2.0 1520   04.1 1467 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.       12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.       0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.     1921 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4M2AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 MOS 2 AM                          33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     742 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     742 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     742 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     594 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  594  04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      66 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   66  04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      82 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   82  04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     936 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1619 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1269 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        68       2.0 1269   04.1 1565 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     350 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  350   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1530 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1530 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1530 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1530 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1551 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1129 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        76       2.0 1129   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     323 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        68       2.0  323   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1265 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2176 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2157 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 2157   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      19 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        78       2.0   19   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2357 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4M2PM.DAT)      60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 MOS 2 PM                          33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1835 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1835 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1835 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1599 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        70       2.0 1599   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.     105 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        63       2.0  105   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     131 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       110       2.0  131   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2064 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1250 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     786 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  786   04.1 1548 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     464 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  464   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1248 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1248 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1248 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1248 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2679 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1820 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1820   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     453 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  453   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     406 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        68       2.0  406   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    2008 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1499 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1487 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1487   04.1 1468 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1943 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B1AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 1 AM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     734 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     734 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     734 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     588 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  588   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      64 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   64   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      82 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   82   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     942 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1596 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1223 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        68       2.0 1223   04.1 1573 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     373 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  373   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1508 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1508 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1508 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1508 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1570 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1137 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        76       2.0 1137   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     334 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        68       2.0  334   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1249 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2170 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2150 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 2150   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      20 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        78       2.0   20   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2371 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B1PM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 1 PM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1849 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1849 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1849 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1604 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        70       2.0 1604   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      54 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        63       2.0   54   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     191 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       110       2.0  191   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2094 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1210 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     749 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  749   04.1 1583 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     461 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  461   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1256 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1256 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1256 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1256 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2656 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1785 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1785   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     478 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  478   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     393 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0  393   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1977 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1537 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1525 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1525   04.1 1468 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1925 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B2AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 2 AM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     740 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     740 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     740 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     581 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  581   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      76 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   76   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      83 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   83   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     935 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1595 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1225 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.       0.  24   2
       120        68       2.0 1225   04.1 1574 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     370 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.       0.  24   2
       120       110       2.0  370   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1511 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1511 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1511 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1511 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1586 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1152 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.       0.  24   2
       120        76       2.0 1152   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     335 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.       0.  12   1
       120        68       2.0  335   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.       0.  12   1
       120        69       2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1263 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2128 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2109 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.       0.  36   3
       120        80       2.0 2109   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      19 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.       0.  12   1
       120        78       2.0   19   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2340 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B2PM.DAT)      60.0321.0.0000.000280.30480000   1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 2 PM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1802 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1802 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1802 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1617 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        70       2.0 1617   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      58 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        63       2.0   58   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     127 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       110       2.0  127   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2068 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1211 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     760 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  760   04.1 1546 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     451 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  451   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1216 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1216 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1216 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1216 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2227 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1814 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1814   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     439 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  439   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     401 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0  401   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1998 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1536 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1524 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1524   04.1 1468 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1921 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B3AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 3 AM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     746 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     746 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     746 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     597 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  597   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      67 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   67   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      82 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   82   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     941 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1594 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1219 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        68        2.0 1219   04.1 1564 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     375 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110        2.0  375   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1480 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1480 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1480 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1480 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1568 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1145 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        76        2.0 1145   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     324 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        68        2.0  324   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69        2.0   99   04.1  155 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1282 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2151 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2131 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80        2.0 2131   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      20 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        78        2.0   20   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2356 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B3PM.DAT)      60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 3 PM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1841 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1841 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1841 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1599 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        70       2.0 1599   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.     105 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        63       2.0  105   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     137 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       110       2.0  137   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2076 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1239 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     788 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        70       2.0  788   04.1 1548 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     451 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  451   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1241 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1241 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1241 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1241 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2670 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1806 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        75       2.0 1806   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     465 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        67       2.0  465   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     399 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0  399   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    2000 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1517 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1505 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 1505   04.1 1469 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        77       2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1950 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B4AM.DAT)      60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 4 AM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     726 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     726 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     726 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     581 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  581   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      62 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   62   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      83 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   83   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     933 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1587 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1220 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120        68       2.0 1220   04.1 1573 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     367 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120       110       2.0  367   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1507 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1507 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1507 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1507 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1558 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1127 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120        76       2.0 1127   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     332 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120        68       2.0  332   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120        69       2.0   99   04.1   99 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1239 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2153 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2133 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120        80       2.0 2133   04.1 1476 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      20 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120        78       2.0   20   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2345 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B4PM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 4 PM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1853 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1853 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1853 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1610 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        70       2.0 1610   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      54 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        63       2.0   54   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     189 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       110       2.0  189   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2090 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1239 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.     781 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120         70        2.0  781   04.1 1583 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     458 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120        110        2.0  458   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1288 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1288 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1288 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1288 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    2624 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1767 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120         75        2.0 1767   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     468 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120         67        2.0  468   04.1 1113 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.     389 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120         69        2.0  389   04.1  153 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1957 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    1510 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    1498 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120         80        2.0 1498   04.1 1465 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      12 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120         77        2.0   12   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    1891 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B5AM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 5 AM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.     740 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.     740 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.     740 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.     594 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        69       2.0  594   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      64 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        62       2.0   64   04.1 1325 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.      82 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       112       2.0   82   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.     933 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1594 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.    1240 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.      0.  24   2
       120         68       2.0 1240   04.1 1574 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.     354 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.      0.  24   2
       120        110       2.0  354   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.    1527 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.    1527 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.    1527 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.    1527 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.    1552 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.    1134 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.      0.  24   2
       120         76       2.0 1134   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.     319 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.      0.  12   1
       120         68       2.0  319   04.1 1352 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      99 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.      0.  12   1
       120         69       2.0   99   04.1   99 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.    1245 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.    2130 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.    2110 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.      0.  36   3
       120         80       2.0 2110   04.1 1475 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.      20 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.      0.  12   1
       120         78       2.0   20   04.1  171 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.    2311 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 4 Bev & La Cien (S4B5PM.DAT)       60.0321.0.0000.000280.30480000    1
1
SE MID S                  492.      301.       5.0
SE 164 S                  488.      448.       5.0
SE 82 S                   486.      530.       5.0
SE CNR                    491.      605.       5.0
SE 82 E                   564.      612.       5.0
SE 164 E                  646.      612.       5.0
SE MID E                  775.      615.       5.0
NE MID E                  767.      715.       5.0
NE 164 E                  637.      714.       5.0
NE 82 E                   555.      714.       5.0
NE CNR                    474.      717.       5.0
NE 82 N                   473.      796.       5.0
NE 164 N                  472.      877.       5.0
NE MID N                  474.      999.       5.0
NW MID N                  372.      996.       5.0
NW 164 N                  367.      884.       5.0
NW 82 N                   367.      803.       5.0
NW CNR                    365.      726.       5.0
NW 82 W                   287.      721.       5.0
NW 164 W                  206.      720.       5.0
NW MID W                   62.      720.       5.0
SW MID W                   56.      606.       5.0
SW 164 W                  209.      606.       5.0
SW 82 W                   289.      606.       5.0
SW CNR                    361.      601.       5.0
SW 82 S                   376.      526.       5.0
SW 164 S                  380.      445.       5.0
SW MID S                  385.      307.       5.0
Site 4 Build 5 PM                        33  1   0
  1
EB        Bev AP    AG  -543.   891.  -185.   701.    1813 0.8   0  44   30.
  1
EB        Bev AP    AG  -185.   701.   -55.   655.    1813 0.8   0  44   30.
  1
EB        Bev AP    AG   -55.   655.   123.   646.    1813 0.8   0  44   30.
  1
EB        Bev THRU  AG   124.   641.   417.   641.    1594 0.8   0  44   30.
  2
EB        Bev THR Q AG   354.   641.   135.   641.      0.  24   2
       120        70       2.0 1594   04.1 1584 1 3
  1
EB        Bev RT    AG   126.   624.   402.   626.      55 0.8   0  32   30.
  2
EB        Bev RT Q  AG   354.   625.   139.   624.      0.  12   1
       120        63       2.0   55   04.1 1048 1 3
  1
EB        Bev LT    AG   124.   663.   413.   664.     164 0.8   0  44   30.
  2
EB        Bev LT Q  AG   353.   664.   134.   663.      0.  24   2
       120       110       2.0  164   04.1 1536 1 3
  1
EB        Bev DP    AG   418.   641.  1427.   656.    2070 0.8   0  44   30.
  1
WB        Bev AP    AG   683.   689.  1428.   687.    1216 0.8   0  44   30.
```

```
  1
WB        Bev T+R   AG   683.   690.   443.   689.      760 0.8   0  44   30.
  2
WB        Bev T+R Q AG   495.   689.   683.   690.       0.  24   2
       120        70       2.0  760   04.1 1583 1 3
  1
WB        Bev LT    AG   685.   667.   445.   665.      456 0.8   0  44   30.
  2
WB        Bev LT Q  AG   499.   666.   679.   667.       0.  24   2
       120       110       2.0  456   04.1 1536 1 3
  1
WB        Bev DP    AG   442.   689.    75.   687.     1265 0.8   0  44   30.
  1
WB        Bev DP    AG    75.   687.   -43.   699.     1265 0.8   0  44   30.
  1
WB        Bev DP    AG   -43.   699.  -189.   746.     1265 0.8   0  44   30.
  1
WB        Bev DP    AG  -189.   746.  -533.   933.     1265 0.8   0  44   30.
  1
NB        Cin AP    AG   461.   300.   483.  -335.     2653 0.8   0  56   30.
  1
NB        Cin THRU  AG   456.   301.   445.   652.     1811 0.8   0  44   30.
  2
NB        Cin THR Q AG   447.   590.   455.   314.       0.  24   2
       120        77       2.0 1811   04.1 1584 1 3
  1
NB        Cin RT    AG   474.   302.   463.   648.      448 0.8   0  32   30.
  2
NB        Cin RT Q  AG   465.   591.   473.   322.       0.  12   1
       120        69       2.0  448   04.1 1114 1 3
  1
NB        Cin LT    AG   438.   301.   430.   652.      394 0.8   0  32   30.
  2
NB        Cin LT Q  AG   431.   589.   437.   316.       0.  12   1
       120        70       2.0  394   04.1  156 1 3
  1
NB        Cin DP    AG   445.   652.   431.  1659.     1976 0.8   0  44   30.
  1
SB        Cin AP    AG   406.  1039.   398.  1660.     1544 0.8   0  44   30.
  1
SB        Cin T+R   AG   401.  1038.   404.   661.     1516 0.8   0  56   30.
  2
SB        Cin T+R Q AG   403.   736.   401.   999.       0.  36   3
       120        80       2.0 1516   04.1 1469 1 3
  1
SB        Cin LT    AG   422.  1036.   424.   666.       28 0.8   0  32   30.
  2
SB        Cin LT Q  AG   424.   735.   422.   991.       0.  12   1
       120        76       2.0   28   04.1  168 1 3
  1
SB        Cin DP    AG   404.   662.   437.  -338.     1915 0.8   0  56   30.
1.0   04 1000.   0Y  5  0 72
```

Site 4 – Beverly & La Cienega
Output Files

```
1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 4 Bev & La Cien (S4EXAM.DAT)                   RUN: Site 4 Existing AM
      DATE: 03/19/2010   TIME: 15:03:19.87


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*-----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.  118. AG    699.   3.3    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.  109. AG    699.   3.3    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.   93. AG    699.   3.3    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.   90. AG    565.   3.3    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0     247.6     641.0 *     106.  270. AG     63. 100.0    .0 24.0  .45   5.4
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.   90. AG     53.   3.3    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     336.0     624.9 *      18.  270. AG     28. 100.0    .0 12.0  .09    .9
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.   90. AG     81.   3.3    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     319.0     663.8 *      34.  270. AG    103. 100.0    .0 24.0  .78   1.7
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.   89. AG    837.   3.3    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.   90. AG   1325.   3.3    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.  270. AG   1055.   3.3    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     707.4     690.1 *     212.   90. AG     62. 100.0    .0 24.0  .85  10.8
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.  270. AG    270.   3.3    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    1236.6     670.1 *     738.   90. AG    101. 100.0    .0 24.0 1.78  37.5
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.  270. AG   1331.   3.3    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.  276. AG   1331.   3.3    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.  288. AG   1331.   3.3    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.  299. AG   1331.   3.3    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.  178. AG   1116.   3.3    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.  358. AG    815.   3.3    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     452.6     398.4 *     192.  178. AG     72. 100.0    .0 24.0  .83   9.7
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.  358. AG    202.   3.3    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     467.3     512.6 *      78.  178. AG     33. 100.0    .0 12.0  .40   4.0
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.  359. AG     99.   3.3    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     441.7     103.6 *     485.  179. AG     33. 100.0    .0 12.0 1.65  24.7
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.  359. AG    965.   3.3    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.  359. AG   1513.   3.3    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.  180. AG   1443.   3.3    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     397.0    1521.3 *     785.  360. AG    110. 100.0    .0 36.0 1.11  39.9
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.  180. AG     70.   3.3    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     423.7     772.9 *      38.  360. AG     34. 100.0    .0 12.0  .78   1.9
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.  178. AG   1520.   3.3    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4EXAM.DAT)                   RUN: Site 4 Existing AM
      DATE: 03/19/2010   TIME: 15:03:19.87

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       69       2.0        565       1584      20.50      1        3
       7. EB        Bev RT Q  *     120       62       2.0         53       1325      20.50      1        3
       9. EB        Bev LT Q  *     120      112       2.0         81       1536      20.50      1        3
      13. WB        Bev T+R Q *     120       68       2.0       1055       1556      20.50      1        3
      15. WB        Bev LT Q  *     120      110       2.0        270       1536      20.50      1        3
      22. NB        Cin THR Q *     120       79       2.0        815       1584      20.50      1        3
      24. NB        Cin RT Q  *     120       71       2.0        202       1353      20.50      1        3
      26. NB        Cin LT Q  *     120       72       2.0         99        165      20.50      1        3
      30. SB        Cin T+R Q *     120       80       2.0       1443       1448      20.50      1        3
      32. SB        Cin LT Q  *     120       75       2.0         70        264      20.50      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
                                                                                                                 PAGE  3
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      JOB: Site 4 Bev & La Cien (S4EXAM.DAT)                  RUN: Site 4 Existing AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .2    .1    .2    .5    .5    .5    .4    .0    .0    .0    .2    .2    .3    .3    .5    .5    .5    .3    .1    .0
   5.  *    .0    .1    .1    .4    .5    .5    .4    .0    .0    .0    .2    .2    .2    .2    .6    .5    .5    .4    .1    .0
  10.  *    .0    .0    .1    .4    .5    .4    .4    .0    .0    .0    .1    .1    .1    .0    .8    .7    .8    .6    .1    .1
  15.  *    .0    .1    .1    .4    .5    .4    .4    .0    .0    .0    .0    .0    .0    .0    .8    .7    .7    .7    .1    .1
  20.  *    .0    .1    .1    .4    .5    .4    .4    .0    .0    .0    .0    .0    .0    .0    .7    .8    .7    .7    .1    .1
  25.  *    .0    .1    .1    .4    .5    .4    .4    .0    .0    .0    .0    .0    .0    .0    .7    .7    .7    .6    .3    .1
  30.  *    .0    .1    .2    .4    .5    .4    .4    .0    .0    .0    .0    .0    .0    .0    .7    .7    .7    .6    .3    .1
  35.  *    .1    .1    .2    .5    .5    .5    .4    .0    .0    .0    .0    .0    .0    .0    .7    .6    .6    .6    .3    .1
  40.  *    .1    .1    .1    .5    .5    .4    .4    .0    .0    .0    .0    .0    .0    .0    .7    .6    .6    .6    .2    .1
  45.  *    .1    .1    .1    .5    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .7    .6    .6    .6    .2    .1
  50.  *    .0    .1    .1    .5    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .5    .5    .5    .4    .2    .1
  55.  *    .0    .1    .1    .5    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .5    .5    .5    .4    .2    .1
  60.  *    .0    .1    .1    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .5    .5    .5    .4    .2    .1
  65.  *    .0    .1    .1    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .5    .5    .5    .4    .2    .1
  70.  *    .0    .1    .1    .3    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .5    .5    .5    .4    .2    .1
  75.  *    .0    .0    .1    .4    .4    .4    .4    .1    .1    .0    .0    .0    .0    .0    .5    .5    .5    .3    .2    .1
  80.  *    .0    .0    .1    .4    .4    .4    .4    .2    .2    .2    .1    .0    .0    .0    .5    .5    .5    .3    .2    .1
  85.  *    .0    .0    .1    .2    .4    .3    .3    .2    .2    .4    .3    .0    .0    .0    .6    .5    .5    .4    .3    .2
  90.  *    .0    .0    .0    .2    .2    .2    .2    .3    .3    .4    .4    .0    .0    .0    .6    .5    .5    .5    .3    .2
  95.  *    .0    .0    .0    .1    .2    .2    .2    .4    .5    .5    .5    .1    .0    .0    .6    .5    .6    .5    .3    .2
 100.  *    .0    .0    .0    .0    .0    .0    .0    .5    .6    .7    .7    .1    .0    .0    .5    .5    .6    .5    .3    .2
 105.  *    .0    .0    .0    .0    .0    .0    .0    .5    .6    .7    .6    .1    .0    .0    .5    .6    .6    .7    .3    .3
 110.  *    .0    .0    .0    .0    .0    .0    .0    .5    .6    .7    .6    .1    .1    .0    .5    .6    .6    .5    .2    .2
 115.  *    .0    .0    .0    .0    .0    .0    .0    .5    .7    .6    .6    .1    .1    .0    .5    .6    .6    .5    .1    .2
 120.  *    .0    .0    .0    .0    .0    .0    .0    .5    .7    .6    .6    .2    .1    .0    .7    .6    .6    .3    .1    .3
 125.  *    .0    .0    .0    .0    .0    .0    .0    .5    .7    .6    .5    .2    .1    .1    .7    .6    .6    .2    .2    .3
 130.  *    .0    .0    .0    .0    .0    .0    .0    .5    .6    .6    .5    .2    .1    .1    .8    .7    .6    .2    .3    .2
 135.  *    .0    .0    .0    .0    .0    .0    .0    .5    .6    .6    .5    .2    .1    .1    .8    .7    .7    .2    .3    .3
 140.  *    .0    .0    .0    .0    .0    .0    .0    .5    .6    .6    .3    .2    .1    .1    .8    .7    .5    .3    .3    .3
 145.  *    .0    .0    .0    .0    .0    .0    .0    .4    .6    .5    .3    .2    .1    .1    .7    .6    .4    .3    .4    .3
 150.  *    .0    .0    .0    .0    .0    .0    .0    .4    .5    .5    .3    .2    .1    .1    .7    .6    .4    .3    .4    .2
 155.  *    .0    .0    .0    .0    .0    .0    .0    .4    .5    .5    .2    .2    .1    .0    .7    .5    .4    .4    .4    .2
 160.  *    .0    .0    .0    .0    .0    .0    .0    .4    .5    .5    .2    .1    .1    .0    .7    .5    .3    .4    .3    .1
 165.  *    .1    .0    .0    .0    .0    .0    .0    .4    .6    .5    .1    .1    .0    .0    .7    .5    .3    .4    .3    .1
 170.  *    .1    .0    .0    .0    .0    .0    .0    .4    .5    .5    .1    .0    .0    .0    .5    .5    .4    .3    .3    .1
 175.  *    .1    .1    .0    .0    .0    .0    .0    .3    .5    .5    .3    .1    .1    .1    .6    .3    .3    .2    .2    .1
 180.  *    .3    .2    .1    .2    .0    .0    .0    .3    .5    .5    .4    .2    .2    .1    .4    .3    .3    .2    .2    .1
 185.  *    .3    .2    .3    .3    .0    .0    .0    .4    .5    .5    .4    .2    .2    .2    .3    .3    .3    .3    .2    .1
 190.  *    .3    .3    .3    .3    .0    .0    .0    .4    .5    .6    .5    .2    .2    .3    .2    .0    .1    .3    .2    .1
 195.  *    .3    .2    .4    .3    .1    .0    .0    .4    .5    .6    .5    .2    .4    .3    .2    .0    .1    .3    .2    .1
 200.  *    .3    .2    .4    .4    .1    .0    .0    .4    .5    .6    .4    .2    .3    .4    .0    .0    .1    .3    .2    .1
 205.  *    .3    .4    .5    .6    .1    .0    .0    .4    .5    .7    .3    .3    .3    .4    .0    .0    .1    .3    .1    .1
1
                                                                                                                         PAGE  4
      JOB: Site 4 Bev & La Cien (S4EXAM.DAT)                  RUN: Site 4 Existing AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .2    .4    .5    .5    .2    .0    .0    .4    .5    .7    .3    .2    .3    .4    .0    .0    .1    .3    .1    .1
 215.  *    .2    .4    .5    .5    .2    .0    .0    .4    .6    .6    .3    .3    .4    .4    .0    .0    .1    .3    .1    .1
 220.  *    .2    .3    .5    .4    .2    .0    .0    .4    .6    .5    .4    .4    .4    .4    .0    .0    .1    .3    .1    .1
 225.  *    .2    .3    .4    .4    .2    .0    .0    .5    .6    .5    .4    .4    .4    .4    .0    .0    .1    .3    .1    .1
 230.  *    .2    .3    .4    .3    .2    .0    .0    .5    .6    .5    .4    .4    .4    .4    .0    .0    .1    .2    .1    .1
 235.  *    .2    .3    .5    .3    .2    .0    .0    .5    .6    .4    .4    .4    .4    .4    .0    .0    .1    .1    .2    .1
 240.  *    .2    .3    .5    .3    .2    .0    .0    .6    .6    .3    .4    .4    .4    .4    .0    .0    .1    .1    .2    .1
 245.  *    .2    .4    .5    .3    .2    .0    .0    .5    .6    .2    .3    .5    .4    .4    .0    .0    .0    .1    .2    .1
 250.  *    .2    .4    .5    .3    .2    .0    .0    .6    .5    .3    .3    .5    .4    .4    .0    .0    .0    .1    .2    .1
 255.  *    .2    .4    .5    .3    .1    .0    .0    .5    .5    .3    .3    .4    .4    .4    .0    .0    .0    .1    .1    .1
 260.  *    .2    .4    .5    .2    .1    .0    .0    .4    .3    .3    .3    .4    .4    .4    .0    .0    .0    .1    .1    .1
 265.  *    .2    .4    .5    .2    .1    .0    .1    .4    .3    .2    .3    .4    .4    .4    .0    .0    .0    .1    .1    .1
 270.  *    .2    .4    .5    .2    .0    .1    .2    .4    .2    .2    .3    .4    .4    .4    .0    .0    .0    .1    .1    .1
 275.  *    .1    .4    .5    .2    .1    .1    .2    .2    .2    .3    .4    .4    .4    .4    .0    .0    .0    .1    .1    .0
 280.  *    .1    .4    .5    .2    .2    .2    .2    .1    .2    .2    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0
 285.  *    .2    .4    .5    .3    .2    .2    .4    .0    .1    .2    .3    .4    .4    .4    .0    .0    .0    .0    .0    .0
 290.  *    .2    .4    .5    .3    .2    .2    .4    .1    .1    .2    .3    .4    .4    .4    .0    .0    .0    .0    .0    .0
 295.  *    .2    .4    .5    .4    .2    .2    .4    .1    .1    .2    .3    .4    .4    .4    .0    .0    .0    .0    .0    .0
 300.  *    .2    .4    .5    .4    .2    .5    .4    .1    .1    .2    .3    .4    .4    .3    .0    .0    .0    .0    .0    .0
 305.  *    .2    .4    .4    .3    .2    .6    .5    .1    .1    .2    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0
 310.  *    .2    .4    .4    .3    .4    .6    .5    .1    .1    .2    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0
 315.  *    .2    .4    .4    .3    .5    .6    .6    .1    .1    .2    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0
 320.  *    .2    .4    .4    .3    .6    .6    .5    .1    .1    .2    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0
 325.  *    .3    .4    .4    .4    .6    .6    .5    .1    .1    .1    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0
 330.  *    .4    .4    .5    .4    .6    .6    .5    .0    .1    .1    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0
 335.  *    .3    .5    .5    .4    .6    .6    .4    .0    .1    .1    .4    .4    .4    .4    .0    .0    .0    .0    .0    .0
 340.  *    .3    .4    .4    .5    .6    .6    .4    .0    .1    .1    .4    .4    .5    .4    .1    .0    .0    .0    .0    .0
 345.  *    .4    .3    .4    .5    .6    .6    .4    .0    .1    .1    .4    .4    .4    .4    .1    .1    .1    .1    .0    .0
 350.  *    .4    .3    .3    .5    .6    .5    .4    .0    .0    .1    .4    .4    .4    .4    .3    .1    .2    .1    .0    .0
 355.  *    .3    .2    .2    .4    .6    .5    .4    .0    .0    .1    .3    .3    .3    .3    .3    .4    .3    .3    .0    .0
 360.  *    .2    .1    .2    .5    .5    .5    .4    .0    .0    .0    .2    .2    .3    .3    .5    .5    .5    .3    .1    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .4    .5    .5    .6    .6    .6    .6    .6    .7    .7    .7    .5    .5    .4    .8    .8    .8    .7    .4    .3
 DEGR. *   330   335   205   205   320   305   315   240   115   205   100   245   340   200    10    20    10    15   145   105

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                                                                                                                         PAGE  5
      JOB: Site 4 Bev & La Cien (S4EXAM.DAT)                  RUN: Site 4 Existing AM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .2    .2    .4    .5    .3    .3    .3
   5.  *    .0    .1    .2    .4    .4    .4    .3    .3
  10.  *    .0    .1    .3    .4    .5    .5    .3    .4
  15.  *    .0    .1    .3    .4    .5    .5    .3    .3
  20.  *    .0    .1    .3    .5    .5    .3    .3    .3
  25.  *    .0    .3    .3    .6    .5    .2    .3    .5
  30.  *    .1    .3    .3    .6    .5    .2    .3    .5
  35.  *    .1    .3    .3    .6    .3    .2    .3    .5
  40.  *    .1    .3    .4    .6    .2    .2    .4    .5
  45.  *    .1    .3    .4    .6    .1    .3    .5    .4
  50.  *    .1    .2    .4    .5    .1    .4    .4    .3
  55.  *    .1    .2    .4    .4    .2    .4    .4    .2
  60.  *    .1    .1    .3    .2    .3    .3    .4    .2
  65.  *    .1    .1    .3    .3    .4    .3    .3    .1
  70.  *    .1    .1    .3    .3    .4    .3    .3    .1
  75.  *    .1    .1    .3    .2    .3    .3    .2    .1
  80.  *    .1    .1    .2    .3    .3    .4    .3    .2
  85.  *    .1    .1    .2    .3    .3    .4    .3    .2
  90.  *    .2    .1    .1    .2    .3    .3    .3    .2
  95.  *    .2    .0    .1    .2    .2    .3    .3    .2
 100.  *    .2    .0    .0    .1    .1    .2    .2    .2
 105.  *    .2    .0    .0    .1    .2    .2    .2    .1
 110.  *    .2    .0    .0    .2    .2    .2    .2    .2
 115.  *    .1    .0    .0    .2    .2    .2    .3    .3
 120.  *    .1    .0    .0    .2    .2    .3    .3    .3
 125.  *    .1    .0    .0    .2    .2    .3    .2    .3
 130.  *    .1    .0    .1    .2    .2    .3    .2    .3
 135.  *    .1    .0    .1    .1    .2    .3    .2    .3
 140.  *    .1    .0    .1    .1    .3    .3    .3    .3
 145.  *    .1    .0    .1    .1    .3    .4    .3    .3
 150.  *    .2    .0    .1    .1    .3    .4    .3    .3
 155.  *    .2    .0    .1    .1    .3    .3    .3    .3
 160.  *    .2    .0    .0    .1    .2    .2    .3    .3
 165.  *    .1    .0    .0    .1    .2    .2    .3    .3
 170.  *    .1    .0    .0    .1    .2    .2    .3    .3
 175.  *    .1    .0    .0    .0    .1    .2    .2    .2
 180.  *    .1    .0    .0    .0    .1    .2    .2    .2
 185.  *    .1    .0    .0    .0    .1    .1    .1    .1
 190.  *    .1    .0    .0    .0    .0    .1    .1    .1
 195.  *    .1    .0    .0    .0    .0    .1    .1    .1
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  6
      JOB: Site 4 Bev & La Cien (S4EXAM.DAT)                    RUN: Site 4 Existing AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .0    .0    .0    .0    .0    .0    .0
 250.  *    .1    .0    .0    .0    .0    .0    .0    .0
 255.  *    .1    .0    .0    .0    .0    .0    .0    .0
 260.  *    .1    .0    .0    .0    .0    .0    .0    .0
 265.  *    .2    .0    .0    .0    .0    .0    .0    .0
 270.  *    .2    .0    .0    .0    .0    .0    .0    .0
 275.  *    .2    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .1    .0    .0    .0
 285.  *    .0    .0    .0    .1    .1    .0    .0    .0
 290.  *    .0    .0    .0    .1    .3    .0    .0    .0
 295.  *    .0    .0    .0    .2    .3    .0    .0    .0
 300.  *    .0    .0    .0    .3    .3    .0    .0    .0
 305.  *    .0    .1    .2    .3    .3    .0    .0    .0
 310.  *    .0    .1    .2    .3    .3    .0    .0    .0
 315.  *    .0    .1    .2    .3    .3    .0    .0    .0
 320.  *    .0    .2    .2    .3    .4    .0    .0    .0
 325.  *    .0    .2    .2    .3    .4    .1    .0    .0
 330.  *    .0    .2    .2    .3    .3    .1    .0    .0
 335.  *    .0    .2    .2    .3    .3    .1    .0    .0
 340.  *    .0    .2    .1    .3    .3    .0    .0    .1
 345.  *    .0    .2    .1    .3    .3    .1    .1    .1
 350.  *    .0    .2    .2    .3    .4    .2    .2    .1
 355.  *    .0    .2    .2    .3    .5    .3    .2    .2
 360.  *    .0    .2    .2    .4    .5    .3    .3    .3
 ------*------------------------------------------------
 MAX   *    .2    .3    .4    .6    .5    .5    .5    .5
 DEGR. *   90    25    40    25     0    10    45    25

 THE HIGHEST CONCENTRATION IS     .80 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .80 PPM AT   20 DEGREES FROM REC16.
 THE 3RD HIGHEST CONCENTRATION IS     .80 PPM AT   10 DEGREES FROM REC17.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 4 Bev & La Cien (S4EXPM.DAT)                    RUN: Site 4 Existing PM
      DATE: 03/19/2010   TIME: 15:14:27.10


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH     EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG   1694.   3.3    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG   1694.   3.3    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG   1694.   3.3    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG   1324.   3.3    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0    -571.4     641.0 *     925.   270. AG     64. 100.0    .0 24.0 1.09  47.0
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG    104.   3.3    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     318.2     624.8 *      36.   270. AG     29. 100.0    .0 12.0  .23   1.8
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG    266.   3.3    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0    -362.6     660.7 *     716.   270. AG    101. 100.0    .0 24.0 1.75  36.4
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG   1846.   3.3    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1139.   3.3    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG    881.   3.3    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     663.4     689.9 *     168.    90. AG     64. 100.0    .0 24.0  .76   8.6
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    258.   3.3    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    1170.6     669.7 *     672.    90. AG    101. 100.0    .0 24.0 1.70  34.1
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG    945.   3.3    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG    945.   3.3    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG    945.   3.3    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG    945.   3.3    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   1787.   3.3    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1271.   3.3    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     504.8   -1403.4 *    1994.   178. AG     73. 100.0    .0 24.0 1.34 101.3
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    427.   3.3    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     478.3     143.1 *     448.   178. AG     33. 100.0    .0 12.0 1.04  22.8
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG     89.   3.3    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     435.9     365.4 *     224.   179. AG     33. 100.0    .0 12.0 1.19  11.4
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   1669.   3.3    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   1144.   3.3    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   1049.   3.3    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     401.8     898.7 *     163.   360. AG    110. 100.0    .0 36.0  .80   8.3
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     95.   3.3    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     420.5    1177.5 *     443.   360. AG     33. 100.0    .0 12.0 1.58  22.5
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   1304.   3.3    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4EXPM.DAT)                    RUN: Site 4 Existing PM
      DATE: 03/19/2010   TIME: 15:14:27.10

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       70        2.0      1324        1584       20.50      1        3
       7. EB        Bev RT Q  *     120       63        2.0       104        1048       20.50      1        3
       9. EB        Bev LT Q  *     120      110        2.0       266        1536       20.50      1        3
      13. WB        Bev T+R Q *     120       70        2.0       881        1510       20.50      1        3
      15. WB        Bev LT Q  *     120      110        2.0       258        1536       20.50      1        3
      22. NB        Cin THR Q *     120       80        2.0      1271        1584       20.50      1        3
      24. NB        Cin RT Q  *     120       72        2.0       427        1117       20.50      1        3
      26. NB        Cin LT Q  *     120       73        2.0        89         210       20.50      1        3
      30. SB        Cin T+R Q *     120       80        2.0      1049        1451       20.50      1        3
      32. SB        Cin LT Q  *     120       73        2.0        95         168       20.50      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
                                                                                                                 PAGE  3
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      JOB: Site 4 Bev & La Cien (S4EXPM.DAT)                  RUN: Site 4 Existing PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .4    .2    .2    .4    .5    .5    .5    .0    .0    .0    .2    .2    .2    .1    .2    .3    .3    .3    .0    .0
   5.  *    .2    .2    .2    .4    .5    .5    .5    .0    .0    .0    .1    .1    .1    .1    .3    .3    .3    .4    .0    .0
  10.  *    .0    .1    .2    .4    .5    .4    .5    .0    .0    .0    .1    .1    .1    .1    .3    .3    .3    .4    .0    .0
  15.  *    .0    .2    .2    .4    .5    .4    .5    .0    .0    .0    .1    .1    .1    .0    .3    .3    .4    .4    .1    .0
  20.  *    .0    .2    .2    .4    .5    .4    .5    .0    .0    .0    .0    .0    .0    .0    .3    .2    .4    .6    .1    .0
  25.  *    .0    .2    .2    .4    .5    .4    .5    .0    .0    .0    .0    .0    .0    .0    .3    .2    .5    .6    .1    .0
  30.  *    .0    .2    .2    .4    .5    .4    .5    .0    .0    .0    .0    .0    .0    .0    .3    .3    .6    .6    .2    .0
  35.  *    .1    .2    .2    .5    .5    .4    .5    .0    .0    .0    .0    .0    .0    .0    .4    .3    .6    .5    .2    .0
  40.  *    .1    .2    .2    .5    .5    .5    .5    .0    .0    .0    .0    .0    .0    .0    .4    .2    .5    .5    .2    .0
  45.  *    .0    .2    .2    .5    .5    .5    .5    .0    .0    .0    .0    .0    .0    .0    .3    .3    .5    .5    .2    .0
  50.  *    .0    .2    .2    .5    .5    .5    .5    .0    .0    .0    .0    .0    .0    .0    .2    .3    .5    .4    .2    .1
  55.  *    .0    .2    .2    .5    .4    .5    .5    .0    .0    .0    .0    .0    .0    .0    .2    .3    .5    .4    .2    .1
  60.  *    .0    .2    .2    .5    .4    .5    .5    .0    .0    .0    .0    .0    .0    .0    .2    .3    .5    .4    .2    .1
  65.  *    .0    .2    .2    .4    .6    .5    .5    .0    .0    .0    .0    .0    .0    .0    .2    .3    .5    .4    .2    .1
  70.  *    .0    .2    .2    .4    .6    .6    .6    .0    .0    .0    .0    .0    .0    .0    .2    .4    .5    .4    .2    .1
  75.  *    .0    .0    .2    .4    .6    .6    .6    .1    .0    .0    .0    .0    .0    .0    .2    .4    .5    .3    .2    .1
  80.  *    .0    .0    .2    .4    .6    .5    .5    .1    .2    .1    .1    .0    .0    .0    .2    .4    .5    .3    .2    .1
  85.  *    .0    .0    .1    .3    .5    .4    .4    .2    .3    .5    .4    .0    .0    .0    .2    .4    .5    .4    .3    .1
  90.  *    .0    .0    .0    .3    .3    .3    .3    .3    .3    .5    .4    .0    .0    .0    .2    .5    .5    .5    .3    .3
  95.  *    .0    .0    .0    .2    .2    .2    .2    .5    .5    .6    .5    .1    .0    .0    .2    .5    .6    .5    .4    .3
 100.  *    .0    .0    .0    .1    .1    .1    .1    .5    .5    .6    .5    .2    .0    .0    .2    .5    .7    .6    .3    .4
 105.  *    .0    .0    .0    .0    .1    .1    .1    .5    .5    .7    .6    .2    .0    .0    .2    .5    .7    .6    .3    .4
 110.  *    .0    .0    .0    .0    .0    .0    .0    .5    .5    .6    .6    .2    .1    .0    .2    .6    .7    .5    .3    .3
 115.  *    .0    .0    .0    .0    .0    .0    .0    .5    .6    .6    .6    .2    .2    .0    .2    .7    .7    .5    .2    .3
 120.  *    .0    .0    .0    .0    .0    .0    .0    .5    .6    .6    .6    .2    .2    .0    .2    .7    .7    .5    .3    .4
 125.  *    .0    .0    .0    .0    .0    .0    .0    .5    .6    .6    .5    .3    .2    .0    .3    .7    .7    .4    .3    .5
 130.  *    .0    .0    .0    .0    .0    .0    .0    .4    .5    .6    .5    .3    .2    .1    .4    .7    .7    .4    .3    .5
 135.  *    .0    .0    .0    .0    .0    .0    .0    .4    .5    .6    .5    .3    .2    .1    .4    .6    .7    .3    .4    .5
 140.  *    .0    .0    .0    .0    .0    .0    .0    .4    .5    .6    .4    .3    .1    .1    .4    .6    .6    .4    .5    .6
 145.  *    .0    .0    .0    .0    .0    .0    .0    .4    .5    .6    .4    .3    .1    .1    .3    .5    .5    .5    .6    .6
 150.  *    .0    .0    .0    .0    .0    .0    .0    .4    .5    .6    .4    .3    .1    .1    .4    .5    .4    .5    .6    .6
 155.  *    .0    .0    .0    .0    .0    .0    .0    .4    .6    .6    .3    .3    .1    .0    .5    .5    .5    .5    .7    .6
 160.  *    .1    .0    .0    .0    .0    .0    .0    .4    .6    .6    .3    .2    .1    .0    .4    .6    .4    .6    .7    .6
 165.  *    .2    .1    .1    .0    .0    .0    .0    .4    .6    .6    .3    .2    .0    .0    .4    .5    .4    .5    .7    .6
 170.  *    .2    .2    .1    .1    .0    .0    .0    .4    .6    .6    .4    .2    .2    .1    .5    .5    .4    .4    .7    .5
 175.  *    .3    .3    .3    .1    .0    .0    .0    .4    .6    .6    .4    .3    .2    .2    .4    .4    .3    .4    .6    .5
 180.  *    .5    .6    .7    .6    .1    .0    .0    .4    .6    .7    .6    .5    .3    .2    .3    .4    .3    .4    .5    .5
 185.  *    .7    .7    .7    .6    .1    .0    .0    .4    .7    .7    .6    .5    .4    .4    .2    .2    .2    .5    .5    .5
 190.  *    .7    .7    .7    .6    .2    .1    .0    .4    .7    .7    .6    .5    .4    .3    .2    .0    .1    .3    .5    .5
 195.  *    .7    .7    .6    .6    .1    .1    .0    .4    .7    .8    .6    .4    .4    .4    .0    .1    .1    .4    .5    .5
 200.  *    .7    .7    .6    .6    .2    .1    .0    .4    .7    .8    .6    .3    .4    .4    .0    .1    .1    .4    .5    .5
 205.  *    .6    .6    .6    .6    .2    .1    .0    .4    .7    .9    .5    .3    .4    .5    .1    .1    .1    .4    .5    .5
1
                                                                                                                          PAGE  4
      JOB: Site 4 Bev & La Cien (S4EXPM.DAT)                  RUN: Site 4 Existing PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .6    .6    .6    .6    .2    .1    .0    .4    .7    .9    .6    .2    .4    .5    .1    .1    .2    .4    .5    .5
 215.  *    .6    .6    .6    .6    .3    .1    .0    .4    .7    .9    .5    .3    .5    .5    .1    .1    .2    .5    .5    .5
 220.  *    .6    .6    .6    .5    .3    .1    .0    .4    .7    .7    .4    .4    .6    .6    .1    .1    .2    .5    .5    .5
 225.  *    .6    .6    .6    .4    .3    .1    .0    .4    .6    .5    .5    .5    .6    .6    .1    .1    .2    .5    .5    .4
 230.  *    .6    .6    .6    .4    .2    .1    .0    .4    .6    .5    .5    .6    .6    .4    .1    .1    .2    .5    .5    .5
 235.  *    .6    .6    .6    .3    .2    .1    .0    .4    .6    .5    .6    .6    .6    .4    .1    .1    .2    .5    .5    .5
 240.  *    .6    .5    .5    .3    .2    .1    .0    .4    .6    .5    .6    .6    .6    .3    .0    .1    .2    .5    .5    .5
 245.  *    .5    .5    .5    .3    .2    .0    .0    .4    .6    .4    .7    .7    .6    .3    .0    .1    .2    .5    .4    .5
 250.  *    .5    .5    .5    .3    .2    .0    .0    .5    .5    .5    .7    .7    .6    .3    .0    .1    .2    .4    .4    .5
 255.  *    .5    .5    .5    .3    .1    .0    .1    .5    .7    .6    .8    .7    .6    .3    .0    .0    .2    .4    .4    .5
 260.  *    .5    .5    .5    .3    .1    .1    .1    .6    .6    .6    .7    .6    .5    .3    .0    .0    .1    .4    .4    .4
 265.  *    .5    .5    .5    .5    .3    .2    .1    .6    .5    .6    .6    .6    .5    .3    .0    .0    .0    .3    .3    .3
 270.  *    .6    .5    .5    .5    .3    .3    .4    .4    .3    .4    .6    .5    .5    .3    .0    .0    .0    .3    .3    .2
 275.  *    .6    .5    .7    .5    .4    .4    .4    .0    .3    .3    .6    .5    .4    .3    .0    .0    .0    .1    .1    .1
 280.  *    .6    .5    .7    .6    .5    .5    .4    .0    .1    .2    .5    .5    .4    .3    .0    .0    .0    .0    .0    .0
 285.  *    .5    .6    .7    .6    .4    .4    .5    .0    .1    .2    .4    .5    .4    .3    .0    .0    .0    .0    .0    .0
 290.  *    .5    .7    .7    .6    .3    .3    .5    .0    .1    .2    .4    .5    .4    .2    .0    .0    .0    .0    .0    .0
 295.  *    .5    .7    .8    .6    .2    .3    .5    .0    .1    .2    .4    .5    .4    .2    .0    .0    .0    .0    .0    .0
 300.  *    .5    .7    .8    .5    .4    .5    .5    .0    .2    .2    .4    .5    .3    .2    .0    .0    .0    .0    .0    .0
 305.  *    .5    .8    .8    .3    .4    .5    .4    .0    .1    .2    .5    .5    .3    .2    .0    .0    .0    .0    .0    .0
 310.  *    .6    .7    .7    .4    .5    .6    .4    .0    .1    .2    .5    .6    .4    .2    .0    .0    .0    .0    .0    .0
 315.  *    .7    .7    .6    .4    .5    .7    .4    .0    .1    .2    .5    .6    .4    .3    .0    .0    .0    .0    .0    .0
 320.  *    .6    .7    .5    .6    .6    .6    .5    .0    .1    .2    .6    .5    .4    .3    .0    .0    .0    .0    .0    .0
 325.  *    .6    .6    .5    .5    .6    .6    .5    .0    .1    .1    .6    .5    .4    .3    .0    .0    .0    .0    .0    .0
 330.  *    .6    .6    .4    .5    .7    .6    .5    .0    .1    .1    .6    .5    .4    .3    .0    .0    .0    .0    .0    .0
 335.  *    .6    .6    .7    .5    .6    .6    .5    .0    .1    .1    .5    .5    .3    .3    .0    .0    .0    .0    .0    .0
 340.  *    .6    .5    .7    .6    .6    .5    .5    .0    .0    .1    .6    .5    .3    .3    .0    .0    .0    .0    .0    .0
 345.  *    .6    .5    .5    .5    .6    .5    .5    .0    .0    .1    .6    .4    .4    .3    .0    .0    .0    .0    .0    .0
 350.  *    .4    .5    .5    .5    .6    .5    .5    .0    .0    .1    .3    .2    .3    .3    .0    .0    .0    .0    .0    .0
 355.  *    .5    .5    .2    .3    .5    .5    .5    .0    .0    .1    .2    .2    .2    .3    .1    .0    .1    .2    .0    .0
 360.  *    .4    .2    .2    .4    .5    .5    .5    .0    .0    .0    .2    .2    .2    .1    .2    .3    .3    .3    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .7    .8    .8    .6    .7    .7    .6    .6    .7    .9    .8    .7    .6    .6    .5    .7    .7    .6    .7    .6
 DEGR. *   185   305   295   180   330   315    70   260   185   205   255   245   220   220   155   115   100    20   155   140

1
                                                                                                                          PAGE  5
      JOB: Site 4 Bev & La Cien (S4EXPM.DAT)                  RUN: Site 4 Existing PM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .4    .4    .4    .5    .3    .2    .2
  5.  *    .0    .4    .5    .4    .4    .4    .3    .3
 10.  *    .0    .4    .5    .5    .4    .4    .3    .4
 15.  *    .0    .4    .5    .7    .4    .3    .3    .4
 20.  *    .0    .4    .5    .6    .4    .2    .5    .4
 25.  *    .0    .4    .5    .6    .5    .3    .4    .4
 30.  *    .0    .4    .5    .5    .5    .4    .4    .4
 35.  *    .0    .4    .6    .5    .3    .4    .5    .4
 40.  *    .0    .5    .7    .5    .3    .3    .6    .5
 45.  *    .0    .6    .7    .5    .4    .4    .5    .5
 50.  *    .0    .6    .7    .4    .4    .5    .5    .4
 55.  *    .0    .6    .6    .4    .5    .5    .5    .3
 60.  *    .0    .7    .4    .2    .4    .5    .5    .3
 65.  *    .0    .7    .3    .4    .4    .5    .5    .3
 70.  *    .0    .7    .4    .4    .4    .5    .5    .3
 75.  *    .0    .5    .5    .3    .5    .5    .3    .3
 80.  *    .0    .4    .5    .3    .5    .5    .3    .3
 85.  *    .1    .5    .4    .4    .5    .5    .3    .3
 90.  *    .3    .5    .3    .3    .4    .3    .3    .2
 95.  *    .4    .2    .2    .3    .4    .3    .3    .3
100.  *    .4    .0    .0    .2    .4    .3    .3    .3
105.  *    .4    .0    .0    .1    .3    .3    .3    .3
110.  *    .5    .0    .0    .2    .3    .3    .3    .3
115.  *    .5    .0    .0    .2    .3    .3    .3    .3
120.  *    .5    .0    .0    .2    .3    .3    .3    .3
125.  *    .5    .0    .0    .2    .3    .3    .3    .3
130.  *    .5    .0    .1    .2    .3    .3    .3    .3
135.  *    .4    .0    .1    .2    .3    .4    .4    .4
140.  *    .5    .0    .1    .2    .3    .4    .4    .4
145.  *    .5    .0    .1    .2    .3    .4    .4    .4
150.  *    .5    .0    .1    .2    .3    .4    .5    .4
155.  *    .5    .0    .1    .2    .4    .4    .4    .4
160.  *    .5    .0    .1    .2    .4    .5    .4    .4
165.  *    .5    .0    .1    .2    .4    .4    .4    .4
170.  *    .5    .0    .0    .1    .3    .4    .4    .4
175.  *    .5    .0    .0    .1    .2    .4    .4    .4
180.  *    .5    .0    .0    .0    .2    .2    .4    .4
185.  *    .5    .0    .0    .0    .1    .2    .2    .2
190.  *    .5    .0    .0    .0    .0    .1    .1    .1
195.  *    .5    .0    .0    .0    .0    .0    .1    .1
200.  *    .5    .0    .0    .0    .0    .0    .0    .0
205.  *    .5    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
     JOB: Site 4 Bev & La Cien (S4EXPM.DAT)                   RUN: Site 4 Existing PM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .5    .0    .0    .0    .0    .0    .0    .0
215.  *    .5    .0    .0    .0    .0    .0    .0    .0
220.  *    .5    .0    .0    .0    .0    .0    .0    .0
225.  *    .5    .0    .0    .0    .0    .0    .0    .0
230.  *    .5    .0    .0    .0    .0    .0    .0    .0
235.  *    .5    .0    .0    .0    .0    .0    .0    .0
240.  *    .5    .0    .0    .0    .0    .0    .0    .0
245.  *    .5    .0    .0    .0    .0    .0    .0    .0
250.  *    .4    .0    .0    .0    .0    .0    .0    .0
255.  *    .5    .0    .0    .0    .0    .0    .0    .0
260.  *    .5    .1    .1    .1    .1    .0    .0    .0
265.  *    .3    .2    .2    .2    .2    .0    .0    .0
270.  *    .2    .2    .3    .3    .3    .0    .0    .0
275.  *    .1    .3    .4    .4    .3    .2    .0    .0
280.  *    .0    .4    .6    .5    .5    .2    .0    .0
285.  *    .0    .6    .6    .5    .5    .2    .0    .0
290.  *    .0    .6    .6    .5    .5    .2    .1    .0
295.  *    .0    .6    .6    .5    .5    .2    .2    .0
300.  *    .0    .6    .6    .5    .5    .2    .2    .0
305.  *    .0    .5    .5    .5    .6    .3    .2    .0
310.  *    .0    .5    .5    .6    .5    .3    .2    .1
315.  *    .0    .5    .5    .6    .5    .3    .2    .1
320.  *    .0    .5    .5    .6    .4    .3    .1    .1
325.  *    .0    .4    .4    .5    .4    .3    .1    .1
330.  *    .0    .4    .4    .4    .3    .3    .1    .0
335.  *    .0    .4    .4    .4    .3    .3    .1    .0
340.  *    .0    .4    .4    .4    .3    .2    .1    .0
345.  *    .0    .4    .5    .5    .3    .2    .1    .1
350.  *    .0    .4    .5    .5    .3    .2    .1    .1
355.  *    .0    .4    .4    .5    .4    .4    .1    .1
360.  *    .0    .4    .4    .4    .5    .3    .2    .2
------*------------------------------------------------
MAX   *    .5    .7    .7    .7    .6    .5    .6    .5
DEGR. *  110    60    40    15   305    50    40    40

THE HIGHEST CONCENTRATION IS     .90 PPM AT  205 DEGREES FROM REC10.
THE 2ND HIGHEST CONCENTRATION IS     .80 PPM AT  305 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS     .80 PPM AT  295 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                   PAGE  1

      JOB: Site 4 Bev & La Cien (S4NBAM.DAT)                   RUN: Site 4 No Build AM
      DATE: 03/19/2010   TIME: 15:35:27.86


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1         Y1        X2         Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.  118. AG     727.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.  109. AG     727.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.   93. AG     727.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.   90. AG     582.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0     244.2     641.0 *     110.  270. AG      13. 100.0    .0 24.0  .47    5.6
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.   90. AG      63.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     332.6     624.9 *      21.  270. AG       6. 100.0    .0 12.0  .11    1.1
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.   90. AG      82.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     317.0     663.8 *      36.  270. AG      21. 100.0    .0 24.0  .80    1.8
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.   89. AG     925.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.   90. AG    1616.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.  270. AG    1242.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     837.6     690.8 *     343.   90. AG      12. 100.0    .0 24.0  .99   17.4
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.  270. AG     374.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    1808.8     673.3 *    1310.   90. AG      20. 100.0    .0 24.0 2.46   66.5
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.  270. AG    1503.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.  276. AG    1503.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.  288. AG    1503.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.  299. AG    1503.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.  178. AG    1534.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.  358. AG    1111.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     465.1     -33.5 *     624.  178. AG      14. 100.0    .0 24.0 1.05   31.7
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.  358. AG     324.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     468.6     470.6 *     120.  178. AG       6. 100.0    .0 12.0  .60    6.1
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.  359. AG      99.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     441.6     105.3 *     484.  179. AG       6. 100.0    .0 12.0 1.65   24.6
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.  359. AG    1248.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.  359. AG    2181.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.  180. AG    2162.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     378.5    3953.7 *    3218.  360. AG      22. 100.0    .0 36.0 1.63  163.5
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.  180. AG      19.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     423.9     743.1 *       8.  360. AG       7. 100.0    .0 12.0  .35     .4
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.  178. AG    2382.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4NBAM.DAT)                   RUN: Site 4 No Build AM
      DATE: 03/19/2010   TIME: 15:35:27.86

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*-------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       69        2.0       582       1584       4.10      1         3
       7. EB        Bev RT Q  *     120       62        2.0        63       1325       4.10      1         3
       9. EB        Bev LT Q  *     120      112        2.0        82       1536       4.10      1         3
      13. WB        Bev T+R Q *     120       68        2.0      1242       1565       4.10      1         3
      15. WB        Bev LT Q  *     120      110        2.0       374       1536       4.10      1         3
      22. NB        Cin THR Q *     120       76        2.0      1111       1584       4.10      1         3
      24. NB        Cin RT Q  *     120       68        2.0       324       1352       4.10      1         3
      26. NB        Cin LT Q  *     120       69        2.0        99        155       4.10      1         3
      30. SB        Cin T+R Q *     120       80        2.0      2162       1476       4.10      1         3
      32. SB        Cin LT Q  *     120       78        2.0        19        171       4.10      1         3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
                                                                                                                 PAGE  3
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      JOB: Site 4 Bev & La Cien (S4NBAM.DAT)                    RUN: Site 4 No Build AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .1    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                      PAGE  4
      JOB: Site 4 Bev & La Cien (S4NBAM.DAT)                    RUN: Site 4 No Build AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .0    .2    .2    .2    .2    .0    .0
 DEGR. *   180     0     0     0     0     0     0    90   105   105   345   345   345     0     5    15    10    10     0     0

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                                                                                                                      PAGE  5
      JOB: Site 4 Bev & La Cien (S4NBAM.DAT)                    RUN: Site 4 No Build AM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .1    .1
   5.  *    .0    .0    .0    .0    .0    .1    .1    .1
  10.  *    .0    .0    .0    .0    .0    .1    .1    .1
  15.  *    .0    .0    .0    .0    .0    .1    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .1    .1    .1
  55.  *    .0    .0    .0    .0    .0    .1    .1    .1
  60.  *    .0    .0    .0    .0    .0    .1    .1    .1
  65.  *    .0    .0    .0    .0    .0    .1    .1    .1
  70.  *    .0    .0    .0    .0    .0    .1    .1    .1
  75.  *    .0    .0    .0    .0    .0    .1    .1    .1
  80.  *    .0    .0    .0    .0    .0    .1    .1    .1
  85.  *    .0    .0    .0    .0    .0    .1    .1    .1
  90.  *    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .1    .1    .1
 100.  *    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .1    .1    .1    .1
 125.  *    .0    .0    .0    .0    .1    .1    .1    .1
 130.  *    .0    .0    .0    .0    .1    .1    .1    .1
 135.  *    .0    .0    .0    .0    .1    .1    .1    .1
 140.  *    .0    .0    .0    .0    .1    .1    .1    .1
 145.  *    .0    .0    .0    .0    .1    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .1    .1    .1    .1
 175.  *    .0    .0    .0    .0    .1    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .1    .1
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
      JOB: Site 4 Bev & La Cien (S4NBAM.DAT)                    RUN: Site 4 No Build AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .1
 360.  *    .0    .0    .0    .0    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *    0     0     0     0   120     5     0     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT    5 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   15 DEGREES FROM REC16.
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC17.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 4 Bev & La Cien (S4NBPM.DAT)                    RUN: Site 4 No Build PM
      DATE: 03/19/2010   TIME: 15:47:05.53


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *    X1       Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG   1848.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG   1848.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG   1848.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG   1625.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0   -2134.8     641.0 *    2489.   270. AG     13. 100.0    .0 24.0 1.34 126.4
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG     57.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     334.4     624.9 *      20.   270. AG      6. 100.0    .0 12.0  .12   1.0
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG    166.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     187.6     663.2 *     165.   270. AG     20. 100.0    .0 24.0 1.09   8.4
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG   2075.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1213.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG    763.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     640.8     689.8 *     146.    90. AG     13. 100.0    .0 24.0  .63   7.4
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    450.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    2227.0     675.6 *    1728.    90. AG     20. 100.0    .0 24.0 2.96  87.8
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG   1281.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG   1281.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG   1281.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG   1281.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   2649.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1806.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     566.4   -3530.3 *    4122.   178. AG     14. 100.0    .0 24.0 1.67 209.4
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    438.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     472.0     357.3 *     234.   178. AG      6. 100.0    .0 12.0  .96  11.9
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG    405.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     514.3   -3200.7 *    3791.   179. AG      6. 100.0    .0 12.0 6.64 192.6
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   1973.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   1517.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   1505.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     395.9    1671.7 *     936.   360. AG     22. 100.0    .0 36.0 1.14  47.5
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     12.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     424.0     740.1 *       5.   360. AG      7. 100.0    .0 12.0  .22    .3
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   1898.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4NBPM.DAT)                    RUN: Site 4 No Build PM
      DATE: 03/19/2010   TIME: 15:47:05.53

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       70       2.0      1625       1584       4.10      1        3
       7. EB        Bev RT Q  *     120       63       2.0        57       1048       4.10      1        3
       9. EB        Bev LT Q  *     120      110       2.0       166       1536       4.10      1        3
      13. WB        Bev T+R Q *     120       70       2.0       763       1583       4.10      1        3
      15. WB        Bev LT Q  *     120      110       2.0       450       1536       4.10      1        3
      22. NB        Cin THR Q *     120       75       2.0      1806       1584       4.10      1        3
      24. NB        Cin RT Q  *     120       67       2.0       438       1113       4.10      1        3
      26. NB        Cin LT Q  *     120       68       2.0       405        153       4.10      1        3
      30. SB        Cin T+R Q *     120       80       2.0      1505       1468       4.10      1        3
      32. SB        Cin LT Q  *     120       77       2.0        12        168       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
                                                                                                                 PAGE  3
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      JOB: Site 4 Bev & La Cien (S4NBPM.DAT)                  RUN: Site 4 No Build PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  40.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE   4
      JOB: Site 4 Bev & La Cien (S4NBPM.DAT)                  RUN: Site 4 No Build PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 330.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 335.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 340.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0
 DEGR. *  170     0     0    45    30    35    30   105   100   100     0     0     0   190   150     0     0     0     0     0

1
                                                                                                                 PAGE   5
      JOB: Site 4 Bev & La Cien (S4NBPM.DAT)                  RUN: Site 4 No Build PM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .0    .0    .0    .0    .0    .0    .1
  5.  *    .0    .0    .0    .0    .0    .0    .1    .1
 10.  *    .0    .0    .0    .0    .0    .0    .1    .1
 15.  *    .0    .0    .0    .0    .0    .1    .1    .1
 20.  *    .0    .0    .0    .0    .0    .1    .1    .1
 25.  *    .0    .0    .0    .0    .0    .1    .1    .1
 30.  *    .0    .0    .0    .0    .0    .1    .1    .1
 35.  *    .0    .0    .0    .0    .0    .1    .1    .1
 40.  *    .0    .0    .0    .0    .0    .1    .1    .1
 45.  *    .0    .0    .0    .0    .0    .1    .1    .1
 50.  *    .0    .0    .0    .0    .0    .0    .1    .1
 55.  *    .0    .0    .0    .0    .0    .0    .0    .0
 60.  *    .0    .0    .0    .0    .0    .0    .0    .0
 65.  *    .0    .0    .0    .0    .0    .0    .0    .0
 70.  *    .0    .0    .0    .0    .0    .0    .0    .0
 75.  *    .0    .0    .0    .0    .0    .0    .0    .0
 80.  *    .0    .0    .0    .0    .0    .0    .0    .0
 85.  *    .0    .0    .0    .0    .0    .0    .0    .0
 90.  *    .0    .0    .0    .0    .0    .0    .0    .0
 95.  *    .0    .0    .0    .0    .0    .0    .0    .0
100.  *    .0    .0    .0    .0    .0    .0    .0    .0
105.  *    .0    .0    .0    .0    .0    .0    .0    .0
110.  *    .0    .0    .0    .0    .0    .0    .0    .0
115.  *    .0    .0    .0    .0    .0    .0    .0    .0
120.  *    .0    .0    .0    .0    .0    .0    .0    .0
125.  *    .0    .0    .0    .0    .0    .0    .0    .1
130.  *    .0    .0    .0    .0    .0    .1    .1    .1
135.  *    .0    .0    .0    .0    .0    .1    .1    .1
140.  *    .0    .0    .0    .0    .0    .1    .1    .1
145.  *    .0    .0    .0    .0    .0    .1    .1    .1
150.  *    .0    .0    .0    .0    .1    .1    .1    .1
155.  *    .0    .0    .0    .0    .1    .1    .1    .1
160.  *    .0    .0    .0    .0    .1    .1    .1    .1
165.  *    .0    .0    .0    .0    .1    .1    .1    .1
170.  *    .0    .0    .0    .0    .0    .1    .1    .1
175.  *    .0    .0    .0    .0    .0    .1    .1    .1
180.  *    .0    .0    .0    .0    .0    .1    .1    .1
185.  *    .0    .0    .0    .0    .0    .0    .0    .0
190.  *    .0    .0    .0    .0    .0    .0    .0    .0
195.  *    .0    .0    .0    .0    .0    .0    .0    .0
200.  *    .0    .0    .0    .0    .0    .0    .0    .0
205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                       PAGE  6
     JOB: Site 4 Bev & La Cien (S4NBPM.DAT)                   RUN: Site 4 No Build PM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .0
215.  *    .0    .0    .0    .0    .0    .0    .0    .0
220.  *    .0    .0    .0    .0    .0    .0    .0    .0
225.  *    .0    .0    .0    .0    .0    .0    .0    .0
230.  *    .0    .0    .0    .0    .0    .0    .0    .0
235.  *    .0    .0    .0    .0    .0    .0    .0    .0
240.  *    .0    .0    .0    .0    .0    .0    .0    .0
245.  *    .0    .0    .0    .0    .0    .0    .0    .0
250.  *    .0    .0    .0    .0    .0    .0    .0    .0
255.  *    .0    .0    .0    .0    .0    .0    .0    .0
260.  *    .0    .0    .0    .0    .0    .0    .0    .0
265.  *    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .0    .0    .0    .0    .0
360.  *    .0    .0    .0    .0    .0    .0    .0    .1
------*------------------------------------------------
MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
DEGR. *    0     0     0     0   150    15     5     0

THE HIGHEST CONCENTRATION IS     .20 PPM AT  150 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS     .10 PPM AT  170 DEGREES FROM REC1 .
THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT   45 DEGREES FROM REC4 .
```

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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                      PAGE  1

      JOB: Site 4 Bev & La Cien (S4M1AM.DAT)                    RUN: Site 4 MOS 1 AM
      DATE: 03/22/2010   TIME: 10:08:05.46


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.  118. AG      754.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.  109. AG      754.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.   93. AG      754.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.   90. AG      612.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0     238.5     641.0 *     115.  270. AG       13. 100.0    .0 24.0  .49   5.9
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.   90. AG       59.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     333.7     624.9 *      20.  270. AG        6. 100.0    .0 12.0  .10   1.0
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.   90. AG       83.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     317.0     663.8 *      36.  270. AG       21. 100.0    .0 24.0  .80   1.8
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.   89. AG      960.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.   90. AG     1591.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.  270. AG     1229.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     819.0     690.7 *     324.   90. AG       12. 100.0    .0 24.0  .98  16.5
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.  270. AG      362.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    1742.8     672.9 *    1244.   90. AG       20. 100.0    .0 24.0 2.38  63.2
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.  270. AG     1513.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.  276. AG     1513.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.  288. AG     1513.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.  299. AG     1513.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.  178. AG     1534.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.  358. AG     1144.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     470.2    -211.4 *     802.  178. AG       14. 100.0    .0 24.0 1.09  40.7
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.  358. AG      329.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     468.6     468.7 *     122.  178. AG        6. 100.0    .0 12.0  .61   6.2
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.  359. AG       99.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     441.9      94.4 *     495.  179. AG        6. 100.0    .0 12.0 1.68  25.1
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.  359. AG     1259.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.  359. AG     2228.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.  180. AG     2209.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     378.3    3987.4 *    3252.  360. AG       22. 100.0    .0 36.0 1.62 165.2
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.  180. AG       19.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     423.9     743.0 *       8.  360. AG        7. 100.0    .0 12.0  .35    .4
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.  178. AG     2413.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4M1AM.DAT)                    RUN: Site 4 MOS 1 AM
      DATE: 03/22/2010   TIME: 10:08:05.46

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL    ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       69       2.0       612       1584       4.10      1        3
       7. EB        Bev RT Q  *     120       63       2.0        59       1324       4.10      1        3
       9. EB        Bev LT Q  *     120      112       2.0        83       1536       4.10      1        3
      13. WB        Bev T+R Q *     120       68       2.0      1229       1572       4.10      1        3
      15. WB        Bev LT Q  *     120      110       2.0       362       1536       4.10      1        3
      22. NB        Cin THR Q *     120       76       2.0      1144       1584       4.10      1        3
      24. NB        Cin RT Q  *     120       68       2.0       329       1352       4.10      1        3
      26. NB        Cin LT Q  *     120       70       2.0        99        155       4.10      1        3
      30. SB        Cin T+R Q *     120       79       2.0      2209       1477       4.10      1        3
      32. SB        Cin LT Q  *     120       77       2.0        19        167       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
                                                                                                                 PAGE  3
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      JOB: Site 4 Bev & La Cien (S4M1AM.DAT)                    RUN: Site 4 MOS 1 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-----------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .1    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  4
      JOB: Site 4 Bev & La Cien (S4M1AM.DAT)                    RUN: Site 4 MOS 1 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-----------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 ------*-----------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .1    .0    .2    .2    .2    .2    .0    .0
 DEGR. *   180     0     0     0     0     0     0    95   105   105     0     0   345     0     5    15    10    10     0     0

1
                                                                                                                 PAGE  5
      JOB: Site 4 Bev & La Cien (S4M1AM.DAT)                    RUN: Site 4 MOS 1 AM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .0    .0    .0    .0    .0    .1    .1
  5.  *    .0    .0    .0    .0    .0    .1    .1    .1
 10.  *    .0    .0    .0    .0    .0    .1    .1    .1
 15.  *    .0    .0    .0    .0    .0    .1    .1    .1
 20.  *    .0    .0    .0    .0    .0    .1    .1    .1
 25.  *    .0    .0    .0    .0    .0    .1    .1    .1
 30.  *    .0    .0    .0    .0    .0    .1    .1    .1
 35.  *    .0    .0    .0    .0    .0    .1    .1    .1
 40.  *    .0    .0    .0    .0    .0    .1    .1    .1
 45.  *    .0    .0    .0    .0    .0    .1    .1    .1
 50.  *    .0    .0    .0    .0    .0    .1    .1    .1
 55.  *    .0    .0    .0    .0    .0    .1    .1    .1
 60.  *    .0    .0    .0    .0    .0    .1    .1    .1
 65.  *    .0    .0    .0    .0    .0    .1    .1    .1
 70.  *    .0    .0    .0    .0    .0    .1    .1    .1
 75.  *    .0    .0    .0    .0    .0    .1    .1    .1
 80.  *    .0    .0    .0    .0    .0    .1    .1    .1
 85.  *    .0    .0    .0    .0    .0    .1    .1    .1
 90.  *    .0    .0    .0    .0    .0    .1    .1    .1
 95.  *    .0    .0    .0    .0    .0    .1    .1    .1
100.  *    .0    .0    .0    .0    .0    .1    .1    .1
105.  *    .0    .0    .0    .0    .0    .1    .1    .1
110.  *    .0    .0    .0    .0    .0    .1    .1    .1
115.  *    .0    .0    .0    .0    .0    .1    .1    .1
120.  *    .0    .0    .0    .0    .1    .1    .1    .1
125.  *    .0    .0    .0    .0    .1    .1    .1    .1
130.  *    .0    .0    .0    .0    .1    .1    .1    .1
135.  *    .0    .0    .0    .0    .1    .1    .1    .1
140.  *    .0    .0    .0    .0    .1    .1    .1    .1
145.  *    .0    .0    .0    .0    .1    .1    .1    .1
150.  *    .0    .0    .0    .0    .1    .1    .1    .1
155.  *    .0    .0    .0    .0    .1    .1    .1    .1
160.  *    .0    .0    .0    .0    .1    .1    .1    .1
165.  *    .0    .0    .0    .0    .1    .1    .1    .1
170.  *    .0    .0    .0    .0    .1    .1    .1    .1
175.  *    .0    .0    .0    .0    .1    .1    .1    .1
180.  *    .0    .0    .0    .0    .0    .1    .1    .1
185.  *    .0    .0    .0    .0    .0    .1    .1    .1
190.  *    .0    .0    .0    .0    .0    .0    .0    .0
195.  *    .0    .0    .0    .0    .0    .0    .0    .0
200.  *    .0    .0    .0    .0    .0    .0    .0    .0
205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                       PAGE  6
     JOB: Site 4 Bev & La Cien (S4M1AM.DAT)                   RUN: Site 4 MOS 1 AM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .0
215.  *    .0    .0    .0    .0    .0    .0    .0    .0
220.  *    .0    .0    .0    .0    .0    .0    .0    .0
225.  *    .0    .0    .0    .0    .0    .0    .0    .0
230.  *    .0    .0    .0    .0    .0    .0    .0    .0
235.  *    .0    .0    .0    .0    .0    .0    .0    .0
240.  *    .0    .0    .0    .0    .0    .0    .0    .0
245.  *    .0    .0    .0    .0    .0    .0    .0    .0
250.  *    .0    .0    .0    .0    .0    .0    .0    .0
255.  *    .0    .0    .0    .0    .0    .0    .0    .0
260.  *    .0    .0    .0    .0    .0    .0    .0    .0
265.  *    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .0    .0    .0    .0    .1
360.  *    .0    .0    .0    .0    .0    .0    .1    .1
------*------------------------------------------------
MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
DEGR. *    0     0     0     0   120     5     0     0

THE HIGHEST CONCENTRATION IS     .20 PPM AT    5 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   15 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC17.
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1                        CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 4 Bev & La Cien (S4M1PM.DAT)                    RUN: Site 4 MOS 1 PM
      DATE: 03/19/2010   TIME: 16:22:52.29


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*---------------------------------------*-----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG   1828.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG   1828.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG   1828.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG   1618.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0   -2103.5     641.0 *    2458.   270. AG     13. 100.0    .0 24.0 1.33 124.8
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG     53.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     335.7     624.9 *      18.   270. AG      6. 100.0    .0 12.0  .11    .9
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG    157.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     242.7     663.5 *     110.   270. AG     20. 100.0    .0 24.0 1.03   5.6
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG   2103.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1235.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG    771.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     642.4     689.8 *     147.    90. AG     13. 100.0    .0 24.0  .65   7.5
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    464.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    2304.0     676.0 *    1805.    90. AG     20. 100.0    .0 24.0 3.05  91.7
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG   1222.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG   1222.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG   1222.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG   1222.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   2714.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1849.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     572.8   -3749.9 *    4342.   178. AG     14. 100.0    .0 24.0 1.71 220.6
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    473.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     478.9     122.8 *     468.   178. AG      6. 100.0    .0 12.0 1.04  23.8
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG    392.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     511.2   -3059.8 *    3650.   179. AG      6. 100.0    .0 12.0 6.43 185.4
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   2063.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   1532.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   1520.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     395.5    1724.3 *     988.   360. AG     22. 100.0    .0 36.0 1.15  50.2
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     12.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     424.0     740.1 *       5.   360. AG      7. 100.0    .0 12.0  .22    .3
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   1921.    .8    .0 56.0
1
                                                                                                                       PAGE  2
      JOB: Site 4 Bev & La Cien (S4M1PM.DAT)                    RUN: Site 4 MOS 1 PM
      DATE: 03/19/2010   TIME: 16:22:52.29

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE    SIGNAL    ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC    TYPE      RATE
                              *     (SEC)   (SEC)     (SEC)     (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       70       2.0      1618       1584       4.10      1         3
       7. EB        Bev RT Q  *     120       63       2.0        53       1048       4.10      1         3
       9. EB        Bev LT Q  *     120      110       2.0       157       1536       4.10      1         3
      13. WB        Bev T+R Q *     120       70       2.0       771       1547       4.10      1         3
      15. WB        Bev LT Q  *     120      110       2.0       464       1536       4.10      1         3
      22. NB        Cin THR Q *     120       75       2.0      1849       1584       4.10      1         3
      24. NB        Cin RT Q  *     120       67       2.0       473       1113       4.10      1         3
      26. NB        Cin LT Q  *     120       68       2.0       392        153       4.10      1         3
      30. SB        Cin T+R Q *     120       80       2.0      1520       1467       4.10      1         3
      32. SB        Cin LT Q  *     120       77       2.0        12        168       4.10      1         3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *       X          Y          Z       *
     -------------------------*-------------------------------------*
       1. SE MID S            *       492.0      301.0        5.0   *
       2. SE 164 S            *       488.0      448.0        5.0   *
       3. SE 82 S             *       486.0      530.0        5.0   *
       4. SE CNR              *       491.0      605.0        5.0   *
       5. SE 82 E             *       564.0      612.0        5.0   *
       6. SE 164 E            *       646.0      612.0        5.0   *
       7. SE MID E            *       775.0      615.0        5.0   *
       8. NE MID E            *       767.0      715.0        5.0   *
       9. NE 164 E            *       637.0      714.0        5.0   *
      10. NE 82 E             *       555.0      714.0        5.0   *
      11. NE CNR              *       474.0      717.0        5.0   *
      12. NE 82 N             *       473.0      796.0        5.0   *
      13. NE 164 N            *       472.0      877.0        5.0   *
      14. NE MID N            *       474.0      999.0        5.0   *
      15. NW MID N            *       372.0      996.0        5.0   *
      16. NW 164 N            *       367.0      884.0        5.0   *
      17. NW 82 N             *       367.0      803.0        5.0   *
      18. NW CNR              *       365.0      726.0        5.0   *
      19. NW 82 W             *       287.0      721.0        5.0   *
      20. NW 164 W            *       206.0      720.0        5.0   *
      21. NW MID W            *        62.0      720.0        5.0   *
      22. SW MID W            *        56.0      606.0        5.0   *
      23. SW 164 W            *       209.0      606.0        5.0   *
      24. SW 82 W             *       289.0      606.0        5.0   *
      25. SW CNR              *       361.0      601.0        5.0   *
      26. SW 82 S             *       376.0      526.0        5.0   *
      27. SW 164 S            *       380.0      445.0        5.0   *
      28. SW MID S            *       385.0      307.0        5.0   *
1
                                                                                                                       PAGE  3
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      JOB: Site 4 Bev & La Cien (S4M1PM.DAT)                    RUN: Site 4 MOS 1 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  40.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
1
                                                                                                                     PAGE  4
      JOB: Site 4 Bev & La Cien (S4M1PM.DAT)                    RUN: Site 4 MOS 1 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 330.  *    .1    .0    .0    .0    .1    .0    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 335.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 340.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
 ------*-------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0
 DEGR. *  170     0     0    45     0    35    30   105   100   100     0     0     0   190   150     0     0     0     0     0

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                                                                                                                     PAGE  5
      JOB: Site 4 Bev & La Cien (S4M1PM.DAT)                    RUN: Site 4 MOS 1 PM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .1
   5.  *    .0    .0    .0    .0    .0    .0    .1    .1
  10.  *    .0    .0    .0    .0    .0    .0    .1    .1
  15.  *    .0    .0    .0    .0    .0    .1    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .0    .1    .1
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .1    .1
 130.  *    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .0    .1    .1    .1
 175.  *    .0    .0    .0    .0    .0    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                           PAGE  6
     JOB: Site 4 Bev & La Cien (S4M1PM.DAT)                   RUN: Site 4 MOS 1 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *    0     0     0     0   150    15     5     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT  150 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .10 PPM AT  170 DEGREES FROM REC1 .
 THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT   45 DEGREES FROM REC4 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 4 Bev & La Cien (S4M2AM.DAT)                   RUN: Site 4 MOS 2 AM
      DATE: 03/22/2010   TIME: 10:09:25.71


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2    *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG    742.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG    742.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG    742.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG    594.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0     241.9     641.0 *     112.   270. AG     13. 100.0    .0 24.0  .48    5.7
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG     66.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     331.6     624.9 *      22.   270. AG      6. 100.0    .0 12.0  .11    1.1
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG     82.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     317.0     663.8 *      36.   270. AG     21. 100.0    .0 24.0  .80    1.8
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG    936.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1619.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG   1269.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     932.7     691.3 *     438.    90. AG     12. 100.0    .0 24.0 1.01   22.2
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    350.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    1676.8     672.5 *    1178.    90. AG     20. 100.0    .0 24.0 2.30   59.8
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG   1530.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG   1530.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG   1530.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG   1530.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   1551.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1129.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     467.8    -127.7 *     718.   178. AG     14. 100.0    .0 24.0 1.07   36.5
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    323.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     468.6     471.0 *     120.   178. AG      6. 100.0    .0 12.0  .60    6.1
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG     99.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     441.6     105.3 *     484.   179. AG      6. 100.0    .0 12.0 1.65   24.6
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   1265.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   2176.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   2157.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     378.6    3943.2 *    3207.   360. AG     22. 100.0    .0 36.0 1.63  162.9
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     19.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     423.9     743.1 *       8.   360. AG      7. 100.0    .0 12.0  .35     .4
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   2357.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4M2AM.DAT)                   RUN: Site 4 MOS 2 AM
      DATE: 03/22/2010   TIME: 10:09:25.71

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)     (SEC)     (VPH)      (VPH)    (gm/hr)
      ------------------------*---------------------------------------------------------------------------------

       5. EB        Bev THR Q *     120       69        2.0       594       1584       4.10      1         3
       7. EB        Bev RT Q  *     120       62        2.0        66       1325       4.10      1         3
       9. EB        Bev LT Q  *     120      112        2.0        82       1536       4.10      1         3
      13. WB        Bev T+R Q *     120       68        2.0      1269       1565       4.10      1         3
      15. WB        Bev LT Q  *     120      110        2.0       350       1536       4.10      1         3
      22. NB        Cin THR Q *     120       76        2.0      1129       1584       4.10      1         3
      24. NB        Cin RT Q  *     120       68        2.0       323       1352       4.10      1         3
      26. NB        Cin LT Q  *     120       69        2.0        99        155       4.10      1         3
      30. SB        Cin T+R Q *     120       80        2.0      2157       1476       4.10      1         3
      32. SB        Cin LT Q  *     120       78        2.0        19        171       4.10      1         3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
                                                                                                                 PAGE  3
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     JOB: Site 4 Bev & La Cien (S4M2AM.DAT)                    RUN: Site 4 MOS 2 AM

      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
  0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0
 10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0
 15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0
 20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
 25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
 30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
 35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
 40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
 45.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
 50.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
 55.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
 60.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 65.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 70.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 75.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 80.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 85.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 90.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
130.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
170.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
175.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .1    .0    .0
180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE   4
     JOB: Site 4 Bev & La Cien (S4M2AM.DAT)                    RUN: Site 4 MOS 2 AM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
215.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
220.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
------*------------------------------------------------------------------------------------------------------------------------
MAX   *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .0    .2    .2    .2    .2    .0    .0
DEGR. *  180     0     0     0     0     0     0    90   105   105   345   345   345     0     5    15    10    10     0     0

1
                                                                                                                PAGE   5
     JOB: Site 4 Bev & La Cien (S4M2AM.DAT)                    RUN: Site 4 MOS 2 AM

      MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .1    .1
   5.  *    .0    .0    .0    .0    .0    .1    .1    .1
  10.  *    .0    .0    .0    .0    .0    .1    .1    .1
  15.  *    .0    .0    .0    .0    .0    .1    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .1    .1    .1
  55.  *    .0    .0    .0    .0    .0    .1    .1    .1
  60.  *    .0    .0    .0    .0    .0    .1    .1    .1
  65.  *    .0    .0    .0    .0    .0    .1    .1    .1
  70.  *    .0    .0    .0    .0    .0    .1    .1    .1
  75.  *    .0    .0    .0    .0    .0    .1    .1    .1
  80.  *    .0    .0    .0    .0    .0    .1    .1    .1
  85.  *    .0    .0    .0    .0    .0    .1    .1    .1
  90.  *    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .1    .1    .1
 100.  *    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .1    .1    .1    .1
 130.  *    .0    .0    .0    .0    .1    .1    .1    .1
 135.  *    .0    .0    .0    .0    .1    .1    .1    .1
 140.  *    .0    .0    .0    .0    .1    .1    .1    .1
 145.  *    .0    .0    .0    .0    .1    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .1    .1    .1    .1
 175.  *    .0    .0    .0    .0    .1    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .1    .1
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                         PAGE  6
     JOB: Site 4 Bev & La Cien (S4M2AM.DAT)                   RUN: Site 4 MOS 2 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .1
 360.  *    .0    .0    .0    .0    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *     0     0     0     0   125     5     0     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT    5 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   15 DEGREES FROM REC16.
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC17.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 4 Bev & La Cien (S4M2PM.DAT)                    RUN: Site 4 MOS 2 PM
      DATE: 03/22/2010   TIME: 10:32:21.70


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =    .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH     EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*-----------------------------------------------------------
       1. EB        Bev AP    *    -543.0     891.0    -185.0     701.0 *     405.  118. AG    1835.    .8   .0 44.0
       2. EB        Bev AP    *    -185.0     701.0     -55.0     655.0 *     138.  109. AG    1835.    .8   .0 44.0
       3. EB        Bev AP    *     -55.0     655.0     123.0     646.0 *     178.   93. AG    1835.    .8   .0 44.0
       4. EB        Bev THRU  *     124.0     641.0     417.0     641.0 *     293.   90. AG    1599.    .8   .0 44.0
       5. EB        Bev THR Q *     354.0     641.0   -1999.3     641.0 *    2353.  270. AG      13. 100.0   .0 24.0 1.32 119.5
       6. EB        Bev RT    *     126.0     624.0     402.0     626.0 *     276.   90. AG     105.    .8   .0 32.0
       7. EB        Bev RT Q  *     354.0     625.0     317.8     624.8 *      36.  270. AG       6. 100.0   .0 12.0  .23   1.8
       8. EB        Bev LT    *     124.0     663.0     413.0     664.0 *     289.   90. AG     131.    .8   .0 44.0
       9. EB        Bev LT Q  *     353.0     664.0     296.6     663.7 *      56.  270. AG      20. 100.0   .0 24.0  .86   2.9
      10. EB        Bev DP    *     418.0     641.0    1427.0     656.0 *    1009.   89. AG    2064.    .8   .0 44.0
      11. WB        Bev AP    *     683.0     689.0    1428.0     687.0 *     745.   90. AG    1250.    .8   .0 44.0
      12. WB        Bev T+R   *     683.0     690.0     443.0     689.0 *     240.  270. AG     786.    .8   .0 44.0
      13. WB        Bev T+R Q *     495.0     689.0     645.4     689.8 *     150.   90. AG      13. 100.0   .0 24.0  .66   7.6
      14. WB        Bev LT    *     685.0     667.0     445.0     665.0 *     240.  270. AG     464.    .8   .0 44.0
      15. WB        Bev LT Q  *     499.0     666.0    2304.0     676.0 *    1805.   90. AG      20. 100.0   .0 24.0 3.05  91.7
      16. WB        Bev DP    *     442.0     689.0      75.0     687.0 *     367.  270. AG    1248.    .8   .0 44.0
      17. WB        Bev DP    *      75.0     687.0     -43.0     699.0 *     119.  276. AG    1248.    .8   .0 44.0
      18. WB        Bev DP    *     -43.0     699.0    -189.0     746.0 *     153.  288. AG    1248.    .8   .0 44.0
      19. WB        Bev DP    *    -189.0     746.0    -533.0     933.0 *     392.  299. AG    1248.    .8   .0 44.0
      20. NB        Cin AP    *     461.0     300.0     483.0    -335.0 *     635.  178. AG    2679.    .8   .0 56.0
      21. NB        Cin THRU  *     456.0     301.0     445.0     652.0 *     351.  358. AG    1820.    .8   .0 44.0
      22. NB        Cin THR Q *     447.0     590.0     568.6   -3603.5 *    4195.  178. AG      14. 100.0   .0 24.0 1.68 213.1
      23. NB        Cin RT    *     474.0     302.0     463.0     648.0 *     346.  358. AG     453.    .8   .0 32.0
      24. NB        Cin RT Q  *     465.0     591.0     473.0     323.5 *     268.  178. AG       6. 100.0   .0 12.0 1.00  13.6
      25. NB        Cin LT    *     438.0     301.0     430.0     652.0 *     351.  359. AG     406.    .8   .0 32.0
      26. NB        Cin LT Q  *     431.0     589.0     514.5   -3211.5 *    3801.  179. AG       6. 100.0   .0 12.0 6.66 193.1
      27. NB        Cin DP    *     445.0     652.0     431.0    1659.0 *    1007.  359. AG    2008.    .8   .0 44.0
      28. SB        Cin AP    *     406.0    1039.0     398.0    1660.0 *     621.  359. AG    1499.    .8   .0 44.0
      29. SB        Cin T+R   *     401.0    1038.0     404.0     661.0 *     377.  180. AG    1487.    .8   .0 56.0
      30. SB        Cin T+R Q *     403.0     736.0     396.4    1608.6 *     873.  360. AG      22. 100.0   .0 36.0 1.13  44.3
      31. SB        Cin LT    *     422.0    1036.0     424.0     666.0 *     370.  180. AG      12.    .8   .0 32.0
      32. SB        Cin LT Q  *     424.0     735.0     424.0     740.1 *       5.  360. AG       7. 100.0   .0 12.0  .22    .3
      33. SB        Cin DP    *     404.0     662.0     437.0    -338.0 *    1001.  178. AG    1943.    .8   .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4M2PM.DAT)                    RUN: Site 4 MOS 2 PM
      DATE: 03/22/2010   TIME: 10:32:21.70

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)       (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       70       2.0      1599       1584       4.10      1        3
       7. EB        Bev RT Q  *     120       63       2.0       105       1048       4.10      1        3
       9. EB        Bev LT Q  *     120      110       2.0       131       1536       4.10      1        3
      13. WB        Bev T+R Q *     120       70       2.0       786       1548       4.10      1        3
      15. WB        Bev LT Q  *     120      110       2.0       464       1536       4.10      1        3
      22. NB        Cin THR Q *     120       75       2.0      1820       1584       4.10      1        3
      24. NB        Cin RT Q  *     120       67       2.0       453       1113       4.10      1        3
      26. NB        Cin LT Q  *     120       68       2.0       406        153       4.10      1        3
      30. SB        Cin T+R Q *     120       80       2.0      1487       1468       4.10      1        3
      32. SB        Cin LT Q  *     120       77       2.0        12        168       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
                                                                                                                 PAGE  3
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     JOB: Site 4 Bev & La Cien (S4M2PM.DAT)                    RUN: Site 4 MOS 2 PM

      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
  0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
  5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 35.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 40.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 90.  *    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 95.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
100.  *    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
115.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
120.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
125.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
170.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
175.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0
195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE  4
     JOB: Site 4 Bev & La Cien (S4M2PM.DAT)                    RUN: Site 4 MOS 2 PM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
210.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
215.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
220.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
225.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
230.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
235.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
240.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
245.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .0    .1    .0    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
330.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
335.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
340.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
------*------------------------------------------------------------------------------------------------------------------------
MAX   *    .1    .0    .0    .1    .1    .1    .1    .2    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0
DEGR. *   170     0     0    45    35    35    35   105   100   100     0     0     0   190   150     0     0     0     0     0

1
                                                                                                                PAGE  5
     JOB: Site 4 Bev & La Cien (S4M2PM.DAT)                    RUN: Site 4 MOS 2 PM

      MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .1
   5.  *    .0    .0    .0    .0    .0    .0    .1    .1
  10.  *    .0    .0    .0    .0    .0    .0    .1    .1
  15.  *    .0    .0    .0    .0    .0    .1    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .1    .1    .1
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .1
  90.  *    .0    .0    .0    .0    .0    .0    .0    .1
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .1    .1    .1
 130.  *    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .1    .1    .1    .1
 175.  *    .0    .0    .0    .0    .0    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  6
      JOB: Site 4 Bev & La Cien (S4M2PM.DAT)                     RUN: Site 4 MOS 2 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *     0     0     0     0   150    15     5     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT  105 DEGREES FROM REC8 .
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  150 DEGREES FROM REC15.
 THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT  170 DEGREES FROM REC1 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 4 Bev & La Cien (S4B1AM.DAT)                    RUN: Site 4 Build 1 AM
      DATE: 03/22/2010   TIME: 10:43:00.54


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG    734.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG    734.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG    734.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG    588.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0     243.1     641.0 *     111.   270. AG     13. 100.0    .0 24.0  .47   5.6
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG     64.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     332.3     624.9 *      22.   270. AG      6. 100.0    .0 12.0  .11   1.1
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG     82.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     317.0     663.8 *      36.   270. AG     21. 100.0    .0 24.0  .80   1.8
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG    942.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1596.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG   1223.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     811.4     690.7 *     316.    90. AG     12. 100.0    .0 24.0  .97  16.1
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    373.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    1797.8     673.2 *    1299.    90. AG     20. 100.0    .0 24.0 2.45  66.0
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG   1508.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG   1508.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG   1508.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG   1508.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   1570.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1137.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     469.0    -169.6 *     760.   178. AG     14. 100.0    .0 24.0 1.08  38.6
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    334.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     468.7     466.9 *     124.   178. AG      6. 100.0    .0 12.0  .62   6.3
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG     99.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     441.6     105.3 *     484.   179. AG      6. 100.0    .0 12.0 1.65  24.6
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   1249.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   2170.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   2150.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     378.9    3911.6 *    3176.   360. AG     22. 100.0    .0 36.0 1.62 161.3
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     20.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     423.9     743.5 *       9.   360. AG      7. 100.0    .0 12.0  .37    .4
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   2371.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4B1AM.DAT)                    RUN: Site 4 Build 1 AM
      DATE: 03/22/2010   TIME: 10:43:00.54

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*---------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120        69       2.0       588       1584       4.10      1        3
       7. EB        Bev RT Q  *     120        62       2.0        64       1325       4.10      1        3
       9. EB        Bev LT Q  *     120       112       2.0        82       1536       4.10      1        3
      13. WB        Bev T+R Q *     120        68       2.0      1223       1573       4.10      1        3
      15. WB        Bev LT Q  *     120       110       2.0       373       1536       4.10      1        3
      22. NB        Cin THR Q *     120        76       2.0      1137       1584       4.10      1        3
      24. NB        Cin RT Q  *     120        68       2.0       334       1352       4.10      1        3
      26. NB        Cin LT Q  *     120        69       2.0        99        155       4.10      1        3
      30. SB        Cin T+R Q *     120        80       2.0      2150       1476       4.10      1        3
      32. SB        Cin LT Q  *     120        78       2.0        20        171       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)         *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
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      JOB: Site 4 Bev & La Cien (S4B1AM.DAT)                    RUN: Site 4 Build 1 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*----------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .1    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                      PAGE   4
      JOB: Site 4 Bev & La Cien (S4B1AM.DAT)                    RUN: Site 4 Build 1 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*----------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 ------*----------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .0    .2    .2    .2    .2    .0    .0
 DEGR. *  180     0     0     0     0     0     0    95   105   105   345   345   345     0     5    15    10    10     0     0

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                                                                                                                      PAGE   5
      JOB: Site 4 Bev & La Cien (S4B1AM.DAT)                    RUN: Site 4 Build 1 AM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .1    .1
   5.  *    .0    .0    .0    .0    .0    .1    .1    .1
  10.  *    .0    .0    .0    .0    .0    .1    .1    .1
  15.  *    .0    .0    .0    .0    .0    .1    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .1    .1    .1
  55.  *    .0    .0    .0    .0    .0    .1    .1    .1
  60.  *    .0    .0    .0    .0    .0    .1    .1    .1
  65.  *    .0    .0    .0    .0    .0    .1    .1    .1
  70.  *    .0    .0    .0    .0    .0    .1    .1    .1
  75.  *    .0    .0    .0    .0    .0    .1    .1    .1
  80.  *    .0    .0    .0    .0    .0    .1    .1    .1
  85.  *    .0    .0    .0    .0    .0    .1    .1    .1
  90.  *    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .1    .1    .1
 100.  *    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .1    .1    .1    .1
 125.  *    .0    .0    .0    .0    .1    .1    .1    .1
 130.  *    .0    .0    .0    .0    .1    .1    .1    .1
 135.  *    .0    .0    .0    .0    .1    .1    .1    .1
 140.  *    .0    .0    .0    .0    .1    .1    .1    .1
 145.  *    .0    .0    .0    .0    .1    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .1    .1    .1    .1
 175.  *    .0    .0    .0    .0    .1    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .1    .1
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
     JOB: Site 4 Bev & La Cien (S4B1AM.DAT)                    RUN: Site 4 Build 1 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .1
 360.  *    .0    .0    .0    .0    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *    0     0     0     0   120     5     0     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT    5 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   15 DEGREES FROM REC16.
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC17.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 4 Bev & La Cien (S4B1PM.DAT)                    RUN: Site 4 Build 1 PM
      DATE: 03/22/2010   TIME: 10:51:31.95


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =    .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)           *   LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2      *    (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*-----------------------------------------*---------------------------------------------------------
       1. EB        Bev AP    *    -543.0     891.0    -185.0     701.0 *     405.   118. AG   1849.    .8    .0 44.0
       2. EB        Bev AP    *    -185.0     701.0     -55.0     655.0 *     138.   109. AG   1849.    .8    .0 44.0
       3. EB        Bev AP    *     -55.0     655.0     123.0     646.0 *     178.    93. AG   1849.    .8    .0 44.0
       4. EB        Bev THRU  *     124.0     641.0     417.0     641.0 *     293.    90. AG   1604.    .8    .0 44.0
       5. EB        Bev THR Q *     354.0     641.0   -2030.6     641.0 *    2385.   270. AG     13. 100.0    .0 24.0 1.32 121.1
       6. EB        Bev RT    *     126.0     624.0     402.0     626.0 *     276.    90. AG     54.    .8    .0 32.0
       7. EB        Bev RT Q  *     354.0     625.0     335.4     624.9 *      19.   270. AG      6. 100.0    .0 12.0  .12     .9
       8. EB        Bev LT    *     124.0     663.0     413.0     664.0 *     289.    90. AG    191.    .8    .0 44.0
       9. EB        Bev LT Q  *     353.0     664.0      55.6     662.6 *     297.   270. AG     20. 100.0    .0 24.0 1.25  15.1
      10. EB        Bev DP    *     418.0     641.0    1427.0     656.0 *    1009.    89. AG   2094.    .8    .0 44.0
      11. WB        Bev AP    *     683.0     689.0    1428.0     687.0 *     745.    90. AG   1210.    .8    .0 44.0
      12. WB        Bev T+R   *     683.0     690.0     443.0     689.0 *     240.   270. AG    749.    .8    .0 44.0
      13. WB        Bev T+R Q *     495.0     689.0     638.2     689.8 *     143.    90. AG     13. 100.0    .0 24.0  .62   7.3
      14. WB        Bev LT    *     685.0     667.0     445.0     665.0 *     240.   270. AG    461.    .8    .0 44.0
      15. WB        Bev LT Q  *     499.0     666.0    2282.0     675.9 *    1783.    90. AG     20. 100.0    .0 24.0 3.03  90.6
      16. WB        Bev DP    *     442.0     689.0      75.0     687.0 *     367.   270. AG   1256.    .8    .0 44.0
      17. WB        Bev DP    *      75.0     687.0     -43.0     699.0 *     119.   276. AG   1256.    .8    .0 44.0
      18. WB        Bev DP    *     -43.0     699.0    -189.0     746.0 *     153.   288. AG   1256.    .8    .0 44.0
      19. WB        Bev DP    *    -189.0     746.0    -533.0     933.0 *     392.   299. AG   1256.    .8    .0 44.0
      20. NB        Cin AP    *     461.0     300.0     483.0    -335.0 *     635.   178. AG   2656.    .8    .0 56.0
      21. NB        Cin THRU  *     456.0     301.0     445.0     652.0 *     351.   358. AG   1785.    .8    .0 44.0
      22. NB        Cin THR Q *     447.0     590.0     563.1   -3415.3 *    4007.   178. AG     14. 100.0    .0 24.0 1.65 203.6
      23. NB        Cin RT    *     474.0     302.0     463.0     648.0 *     346.   358. AG    478.    .8    .0 32.0
      24. NB        Cin RT Q  *     465.0     591.0     480.5      70.6 *     521.   178. AG      6. 100.0    .0 12.0 1.05  26.4
      25. NB        Cin LT    *     438.0     301.0     430.0     652.0 *     351.   359. AG    393.    .8    .0 32.0
      26. NB        Cin LT Q  *     431.0     589.0     512.0   -3096.6 *    3686.   179. AG      6. 100.0    .0 12.0 6.66 187.3
      27. NB        Cin DP    *     445.0     652.0     431.0    1659.0 *    1007.   359. AG   1977.    .8    .0 44.0
      28. SB        Cin AP    *     406.0    1039.0     398.0    1660.0 *     621.   359. AG   1537.    .8    .0 44.0
      29. SB        Cin T+R   *     401.0    1038.0     404.0     661.0 *     377.   180. AG   1525.    .8    .0 56.0
      30. SB        Cin T+R Q *     403.0     736.0     395.3    1745.3 *    1009.   360. AG     22. 100.0    .0 36.0 1.15  51.3
      31. SB        Cin LT    *     422.0    1036.0     424.0     666.0 *     370.   180. AG     12.    .8    .0 32.0
      32. SB        Cin LT Q  *     424.0     735.0     424.0     740.1 *       5.   360. AG      7. 100.0    .0 12.0  .22     .3
      33. SB        Cin DP    *     404.0     662.0     437.0    -338.0 *    1001.   178. AG   1925.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4B1PM.DAT)                    RUN: Site 4 Build 1 PM
      DATE: 03/22/2010   TIME: 10:51:31.95

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*---------------------------------------------------------------------------------

       5. EB        Bev THR Q *      120       70       2.0      1604       1584       4.10      1        3
       7. EB        Bev RT Q  *      120       63       2.0        54       1048       4.10      1        3
       9. EB        Bev LT Q  *      120      110       2.0       191       1536       4.10      1        3
      13. WB        Bev T+R Q *      120       70       2.0       749       1583       4.10      1        3
      15. WB        Bev LT Q  *      120      110       2.0       461       1536       4.10      1        3
      22. NB        Cin THR Q *      120       75       2.0      1785       1584       4.10      1        3
      24. NB        Cin RT Q  *      120       67       2.0       478       1113       4.10      1        3
      26. NB        Cin LT Q  *      120       69       2.0       393        153       4.10      1        3
      30. SB        Cin T+R Q *      120       80       2.0      1525       1468       4.10      1        3
      32. SB        Cin LT Q  *      120       77       2.0        12        168       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)           *
         RECEPTOR             *      X          Y           Z        *
     -------------------------*--------------------------------------*
      1. SE MID S             *       492.0      301.0       5.0    *
      2. SE 164 S             *       488.0      448.0       5.0    *
      3. SE 82 S              *       486.0      530.0       5.0    *
      4. SE CNR               *       491.0      605.0       5.0    *
      5. SE 82 E              *       564.0      612.0       5.0    *
      6. SE 164 E             *       646.0      612.0       5.0    *
      7. SE MID E             *       775.0      615.0       5.0    *
      8. NE MID E             *       767.0      715.0       5.0    *
      9. NE 164 E             *       637.0      714.0       5.0    *
     10. NE 82 E              *       555.0      714.0       5.0    *
     11. NE CNR               *       474.0      717.0       5.0    *
     12. NE 82 N              *       473.0      796.0       5.0    *
     13. NE 164 N             *       472.0      877.0       5.0    *
     14. NE MID N             *       474.0      999.0       5.0    *
     15. NW MID N             *       372.0      996.0       5.0    *
     16. NW 164 N             *       367.0      884.0       5.0    *
     17. NW 82 N              *       367.0      803.0       5.0    *
     18. NW CNR               *       365.0      726.0       5.0    *
     19. NW 82 W              *       287.0      721.0       5.0    *
     20. NW 164 W             *       206.0      720.0       5.0    *
     21. NW MID W             *        62.0      720.0       5.0    *
     22. SW MID W             *        56.0      606.0       5.0    *
     23. SW 164 W             *       209.0      606.0       5.0    *
     24. SW 82 W              *       289.0      606.0       5.0    *
     25. SW CNR               *       361.0      601.0       5.0    *
     26. SW 82 S              *       376.0      526.0       5.0    *
     27. SW 164 S             *       380.0      445.0       5.0    *
     28. SW MID S             *       385.0      307.0       5.0    *
1
                                                                                                                 PAGE  3
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      JOB: Site 4 Bev & La Cien (S4B1PM.DAT)                    RUN: Site 4 Build 1 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  40.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
1
                                                                                                                           PAGE  4
      JOB: Site 4 Bev & La Cien (S4B1PM.DAT)                    RUN: Site 4 Build 1 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 335.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 340.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
 ------*-------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0
 DEGR. *   170     0     0    45    30    35    30   105   100   100     0     0     0   190   150     0     0     0     0     0

1
                                                                                                                           PAGE  5
      JOB: Site 4 Bev & La Cien (S4B1PM.DAT)                    RUN: Site 4 Build 1 PM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .1
   5.  *    .0    .0    .0    .0    .0    .0    .1    .1
  10.  *    .0    .0    .0    .0    .0    .0    .1    .1
  15.  *    .0    .0    .0    .0    .0    .1    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .0    .1    .1
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .1    .1
 130.  *    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .1    .1    .1    .1
 175.  *    .0    .0    .0    .0    .0    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  6
      JOB: Site 4 Bev & La Cien (S4B1PM.DAT)                   RUN: Site 4 Build 1 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *    0     0     0     0   150    15     5     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT  150 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .10 PPM AT  170 DEGREES FROM REC1 .
 THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT   45 DEGREES FROM REC4 .
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1                        CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 4 Bev & La Cien (S4B2AM.DAT)                    RUN: Site 4 Build 2 AM
      DATE: 03/22/2010   TIME: 10:59:39.09


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)        (VEH)
      ------------------------*----------------------------------------*-------------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG    740.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG    740.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG    740.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG    581.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0     244.6     641.0 *     109.   270. AG     13. 100.0    .0 24.0  .47    5.6
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG     76.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     328.2     624.9 *      26.   270. AG      6. 100.0    .0 12.0  .13    1.3
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG     83.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     317.0     663.8 *      36.   270. AG     21. 100.0    .0 24.0  .80    1.8
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG    935.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1595.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG   1225.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     813.4     690.7 *     318.    90. AG     12. 100.0    .0 24.0  .97   16.2
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    370.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    1786.8     673.2 *    1288.    90. AG     20. 100.0    .0 24.0 2.43   65.4
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG   1511.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG   1511.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG   1511.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG   1511.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   1586.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1152.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     471.4    -253.3 *     844.   178. AG     14. 100.0    .0 24.0 1.09   42.9
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    335.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     468.7     466.5 *     125.   178. AG      6. 100.0    .0 12.0  .62    6.3
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG     99.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     441.6     105.3 *     484.   179. AG      6. 100.0    .0 12.0 1.65   24.6
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   1263.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   2128.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   2109.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     379.9    3775.0 *    3039.   360. AG     22. 100.0    .0 36.0 1.59  154.4
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     19.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     423.9     743.1 *       8.   360. AG      7. 100.0    .0 12.0  .35     .4
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   2340.    .8    .0 56.0
1
                                                                                                                    PAGE  2
      JOB: Site 4 Bev & La Cien (S4B2AM.DAT)                    RUN: Site 4 Build 2 AM
      DATE: 03/22/2010   TIME: 10:59:39.09

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       69       2.0        581        1584       4.10      1        3
       7. EB        Bev RT Q  *     120       62       2.0         76        1325       4.10      1        3
       9. EB        Bev LT Q  *     120      112       2.0         83        1536       4.10      1        3
      13. WB        Bev T+R Q *     120       68       2.0       1225        1574       4.10      1        3
      15. WB        Bev LT Q  *     120      110       2.0        370        1536       4.10      1        3
      22. NB        Cin THR Q *     120       76       2.0       1152        1584       4.10      1        3
      24. NB        Cin RT Q  *     120       68       2.0        335        1352       4.10      1        3
      26. NB        Cin LT Q  *     120       69       2.0         99         155       4.10      1        3
      30. SB        Cin T+R Q *     120       80       2.0       2109        1476       4.10      1        3
      32. SB        Cin LT Q  *     120       78       2.0         19         171       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)           *
         RECEPTOR             *       X           Y          Z       *
     -------------------------*--------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0    *
      2. SE 164 S             *       488.0      448.0        5.0    *
      3. SE 82 S              *       486.0      530.0        5.0    *
      4. SE CNR               *       491.0      605.0        5.0    *
      5. SE 82 E              *       564.0      612.0        5.0    *
      6. SE 164 E             *       646.0      612.0        5.0    *
      7. SE MID E             *       775.0      615.0        5.0    *
      8. NE MID E             *       767.0      715.0        5.0    *
      9. NE 164 E             *       637.0      714.0        5.0    *
     10. NE 82 E              *       555.0      714.0        5.0    *
     11. NE CNR               *       474.0      717.0        5.0    *
     12. NE 82 N              *       473.0      796.0        5.0    *
     13. NE 164 N             *       472.0      877.0        5.0    *
     14. NE MID N             *       474.0      999.0        5.0    *
     15. NW MID N             *       372.0      996.0        5.0    *
     16. NW 164 N             *       367.0      884.0        5.0    *
     17. NW 82 N              *       367.0      803.0        5.0    *
     18. NW CNR               *       365.0      726.0        5.0    *
     19. NW 82 W              *       287.0      721.0        5.0    *
     20. NW 164 W             *       206.0      720.0        5.0    *
     21. NW MID W             *        62.0      720.0        5.0    *
     22. SW MID W             *        56.0      606.0        5.0    *
     23. SW 164 W             *       209.0      606.0        5.0    *
     24. SW 82 W              *       289.0      606.0        5.0    *
     25. SW CNR               *       361.0      601.0        5.0    *
     26. SW 82 S              *       376.0      526.0        5.0    *
     27. SW 164 S             *       380.0      445.0        5.0    *
     28. SW MID S             *       385.0      307.0        5.0    *
1
                                                                                                                    PAGE  3
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      JOB: Site 4 Bev & La Cien (S4B2AM.DAT)                 RUN: Site 4 Build 2 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-----------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .1    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  4
      JOB: Site 4 Bev & La Cien (S4B2AM.DAT)                 RUN: Site 4 Build 2 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-----------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 ------*-----------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .0    .2    .2    .2    .2    .0    .0
 DEGR. *   180     0     0     0     0     0     0    95   105   105   345   345   345     0    10    15    10    10     0     0

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                                                                                                                 PAGE  5
      JOB: Site 4 Bev & La Cien (S4B2AM.DAT)                 RUN: Site 4 Build 2 AM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .1    .1
   5.  *    .0    .0    .0    .0    .0    .1    .1    .1
  10.  *    .0    .0    .0    .0    .0    .1    .1    .1
  15.  *    .0    .0    .0    .0    .0    .1    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .1    .1    .1
  55.  *    .0    .0    .0    .0    .0    .1    .1    .1
  60.  *    .0    .0    .0    .0    .0    .1    .1    .1
  65.  *    .0    .0    .0    .0    .0    .1    .1    .1
  70.  *    .0    .0    .0    .0    .0    .1    .1    .1
  75.  *    .0    .0    .0    .0    .0    .1    .1    .1
  80.  *    .0    .0    .0    .0    .0    .1    .1    .1
  85.  *    .0    .0    .0    .0    .0    .1    .1    .1
  90.  *    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .1    .1    .1
 100.  *    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .1    .1    .1    .1
 130.  *    .0    .0    .0    .0    .1    .1    .1    .1
 135.  *    .0    .0    .0    .0    .1    .1    .1    .1
 140.  *    .0    .0    .0    .0    .1    .1    .1    .1
 145.  *    .0    .0    .0    .0    .1    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .1    .1    .1    .1
 175.  *    .0    .0    .0    .0    .1    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .1    .1
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                                PAGE  6
     JOB: Site 4 Bev & La Cien (S4B2AM.DAT)                    RUN: Site 4 Build 2 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .1
 360.  *    .0    .0    .0    .0    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *     0     0     0     0   125     5     0     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   15 DEGREES FROM REC16.
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC17.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 4 Bev & La Cien (S4B2PM.DAT)                    RUN: Site 4 Build 2 PM
      DATE: 03/22/2010   TIME: 11:14:27.12


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG   1802.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG   1802.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG   1802.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG   1617.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0   -2093.1     641.0 *    2447.   270. AG     13. 100.0    .0 24.0 1.33 124.3
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG     58.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     334.0     624.9 *      20.   270. AG      6. 100.0    .0 12.0  .13   1.0
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG    127.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     300.7     663.8 *      52.   270. AG     20. 100.0    .0 24.0  .83   2.7
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG   2068.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1211.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG    760.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     640.4     689.8 *     145.    90. AG     13. 100.0    .0 24.0  .64   7.4
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    451.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    2227.0     675.6 *    1728.    90. AG     20. 100.0    .0 24.0 2.96  87.8
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG   1216.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG   1216.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG   1216.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG   1216.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   2227.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1814.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     567.6   -3572.2 *    4164.   178. AG     14. 100.0    .0 24.0 1.68 211.5
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    439.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     472.0     355.3 *     236.   178. AG      6. 100.0    .0 12.0  .97  12.0
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG    401.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     513.9   -3183.4 *    3773.   179. AG      6. 100.0    .0 12.0 6.80 191.7
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   1998.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   1536.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   1524.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     395.3    1745.3 *    1009.   360. AG     22. 100.0    .0 36.0 1.15  51.3
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     12.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     424.0     740.1 *       5.   360. AG      7. 100.0    .0 12.0  .22    .3
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   1921.    .8    .0 56.0
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                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4B2PM.DAT)                    RUN: Site 4 Build 2 PM
      DATE: 03/22/2010   TIME: 11:14:27.12

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       70       2.0      1617       1584       4.10     1        3
       7. EB        Bev RT Q  *     120       63       2.0        58       1048       4.10     1        3
       9. EB        Bev LT Q  *     120      110       2.0       127       1536       4.10     1        3
      13. WB        Bev T+R Q *     120       70       2.0       760       1546       4.10     1        3
      15. WB        Bev LT Q  *     120      110       2.0       451       1536       4.10     1        3
      22. NB        Cin THR Q *     120       75       2.0      1814       1584       4.10     1        3
      24. NB        Cin RT Q  *     120       67       2.0       439       1113       4.10     1        3
      26. NB        Cin LT Q  *     120       69       2.0       401        153       4.10     1        3
      30. SB        Cin T+R Q *     120       80       2.0      1524       1468       4.10     1        3
      32. SB        Cin LT Q  *     120       77       2.0        12        168       4.10     1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)           *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
                                                                                                                 PAGE  3
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      JOB: Site 4 Bev & La Cien (S4B2PM.DAT)                    RUN: Site 4 Build 2 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  40.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  4
      JOB: Site 4 Bev & La Cien (S4B2PM.DAT)                    RUN: Site 4 Build 2 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 330.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 335.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 340.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0
 DEGR. *   175     0     0    45    35    35    35   105   100   100     0     0     0   190   150     0     0     0     0     0

1
                                                                                                                 PAGE  5
      JOB: Site 4 Bev & La Cien (S4B2PM.DAT)                    RUN: Site 4 Build 2 PM

       MODEL RESULTS
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      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .1
   5.  *    .0    .0    .0    .0    .0    .0    .1    .1
  10.  *    .0    .0    .0    .0    .0    .0    .1    .1
  15.  *    .0    .0    .0    .0    .0    .1    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .0    .1    .1
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .1    .1
 130.  *    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .0    .1    .1    .1
 175.  *    .0    .0    .0    .0    .0    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                                PAGE  6
     JOB: Site 4 Bev & La Cien (S4B2PM.DAT)                  RUN: Site 4 Build 2 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *    0     0     0     0   150    15     5     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT  150 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .10 PPM AT  175 DEGREES FROM REC1 .
 THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT   45 DEGREES FROM REC4 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 4 Bev & La Cien (S4B3AM.DAT)                    RUN: Site 4 Build 3 AM
      DATE: 03/22/2010   TIME: 11:26:49.93


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*--------------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG    746.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG    746.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG    746.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG    597.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0     241.6     641.0 *     112.   270. AG     13. 100.0    .0 24.0  .48    5.7
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG     67.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     331.3     624.9 *      23.   270. AG      6. 100.0    .0 12.0  .11    1.2
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG     82.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     317.0     663.8 *      36.   270. AG     21. 100.0    .0 24.0  .80    1.8
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG    941.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1594.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG   1219.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     813.5     690.7 *     319.    90. AG     12. 100.0    .0 24.0  .97   16.2
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    375.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    1808.8     673.3 *    1310.    90. AG     20. 100.0    .0 24.0 2.46   66.5
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG   1480.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG   1480.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG   1480.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG   1480.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   1568.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1145.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     470.2    -211.4 *     802.   178. AG     14. 100.0    .0 24.0 1.09   40.7
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    324.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     468.6     470.6 *     120.   178. AG      6. 100.0    .0 12.0  .60    6.1
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG     99.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     441.6     105.3 *     484.   179. AG      6. 100.0    .0 12.0 1.65   24.6
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   1282.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   2151.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   2131.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     379.3    3848.6 *    3113.   360. AG     22. 100.0    .0 36.0 1.61  158.1
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     20.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     423.9     743.5 *       9.   360. AG      7. 100.0    .0 12.0  .37     .4
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   2356.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4B3AM.DAT)                    RUN: Site 4 Build 3 AM
      DATE: 03/22/2010   TIME: 11:26:49.93

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)     (SEC)     (VPH)      (VPH)    (gm/hr)
      ------------------------*---------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       69        2.0       597       1584       4.10      1        3
       7. EB        Bev RT Q  *     120       62        2.0        67       1325       4.10      1        3
       9. EB        Bev LT Q  *     120      112        2.0        82       1536       4.10      1        3
      13. WB        Bev T+R Q *     120       68        2.0      1219       1564       4.10      1        3
      15. WB        Bev LT Q  *     120      110        2.0       375       1536       4.10      1        3
      22. NB        Cin THR Q *     120       76        2.0      1145       1584       4.10      1        3
      24. NB        Cin RT Q  *     120       68        2.0       324       1352       4.10      1        3
      26. NB        Cin LT Q  *     120       69        2.0        99        155       4.10      1        3
      30. SB        Cin T+R Q *     120       80        2.0      2131       1476       4.10      1        3
      32. SB        Cin LT Q  *     120       78        2.0        20        171       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *         COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
                                                                                                                 PAGE  3
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      JOB: Site 4 Bev & La Cien (S4B3AM.DAT)                    RUN: Site 4 Build 3 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .1    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                        PAGE   4
      JOB: Site 4 Bev & La Cien (S4B3AM.DAT)                    RUN: Site 4 Build 3 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .0    .2    .2    .2    .2    .0    .0
 DEGR. *  180     0     0     0     0     0     0    95   105   105   345   345   345     0    10    15    10    10     0     0

1
                                                                                                                        PAGE   5
      JOB: Site 4 Bev & La Cien (S4B3AM.DAT)                    RUN: Site 4 Build 3 AM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .1    .1
   5.  *    .0    .0    .0    .0    .0    .1    .1    .1
  10.  *    .0    .0    .0    .0    .0    .1    .1    .1
  15.  *    .0    .0    .0    .0    .0    .1    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .1    .1    .1
  55.  *    .0    .0    .0    .0    .0    .1    .1    .1
  60.  *    .0    .0    .0    .0    .0    .1    .1    .1
  65.  *    .0    .0    .0    .0    .0    .1    .1    .1
  70.  *    .0    .0    .0    .0    .0    .1    .1    .1
  75.  *    .0    .0    .0    .0    .0    .1    .1    .1
  80.  *    .0    .0    .0    .0    .0    .1    .1    .1
  85.  *    .0    .0    .0    .0    .0    .1    .1    .1
  90.  *    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .1    .1    .1
 100.  *    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .1    .1    .1    .1
 130.  *    .0    .0    .0    .0    .1    .1    .1    .1
 135.  *    .0    .0    .0    .0    .1    .1    .1    .1
 140.  *    .0    .0    .0    .0    .1    .1    .1    .1
 145.  *    .0    .0    .0    .0    .1    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .1    .1    .1    .1
 175.  *    .0    .0    .0    .0    .1    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .1    .1
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                            PAGE  6
     JOB: Site 4 Bev & La Cien (S4B3AM.DAT)                    RUN: Site 4 Build 3 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .1
 360.  *    .0    .0    .0    .0    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *    0     0     0     0   125     5     0     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   15 DEGREES FROM REC16.
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC17.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 4 Bev & La Cien (S4B3PM.DAT)                    RUN: Site 4 Build 3 PM
      DATE: 03/22/2010   TIME: 11:41:44.23


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG   1841.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG   1841.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG   1841.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG   1599.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0   -1999.3     641.0 *    2353.   270. AG     13. 100.0    .0 24.0 1.32 119.5
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG    105.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     317.8     624.8 *      36.   270. AG      6. 100.0    .0 12.0  .23   1.8
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG    137.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     289.7     663.7 *      63.   270. AG     20. 100.0    .0 24.0  .89   3.2
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG   2076.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1239.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG    788.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     645.8     689.8 *     151.    90. AG     13. 100.0    .0 24.0  .66   7.7
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    451.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    2227.0     675.6 *    1728.    90. AG     20. 100.0    .0 24.0 2.96  87.8
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG   1241.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG   1241.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG   1241.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG   1241.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   2670.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1806.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     566.4   -3530.3 *    4122.   178. AG     14. 100.0    .0 24.0 1.67 209.4
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    465.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     476.4     206.2 *     385.   178. AG      6. 100.0    .0 12.0 1.02  19.6
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG    399.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     513.4   -3161.7 *    3752.   179. AG      6. 100.0    .0 12.0 6.76 190.6
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   2000.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   1517.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   1505.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     395.9    1671.7 *     936.   360. AG     22. 100.0    .0 36.0 1.14  47.5
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     12.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     424.0     740.1 *       5.   360. AG      7. 100.0    .0 12.0  .22    .3
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   1950.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4B3PM.DAT)                    RUN: Site 4 Build 3 PM
      DATE: 03/22/2010   TIME: 11:41:44.23

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*-------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       70       2.0      1599       1584       4.10      1        3
       7. EB        Bev RT Q  *     120       63       2.0       105       1048       4.10      1        3
       9. EB        Bev LT Q  *     120      110       2.0       137       1536       4.10      1        3
      13. WB        Bev T+R Q *     120       70       2.0       788       1548       4.10      1        3
      15. WB        Bev LT Q  *     120      110       2.0       451       1536       4.10      1        3
      22. NB        Cin THR Q *     120       75       2.0      1806       1584       4.10      1        3
      24. NB        Cin RT Q  *     120       67       2.0       465       1113       4.10      1        3
      26. NB        Cin LT Q  *     120       69       2.0       399        153       4.10      1        3
      30. SB        Cin T+R Q *     120       80       2.0      1505       1469       4.10      1        3
      32. SB        Cin LT Q  *     120       77       2.0        12        168       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
                                                                                                                 PAGE  3
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      JOB: Site 4 Bev & La Cien (S4B3PM.DAT)                    RUN: Site 4 Build 3 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  40.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
1
                                                                                                                   PAGE  4
      JOB: Site 4 Bev & La Cien (S4B3PM.DAT)                    RUN: Site 4 Build 3 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 330.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 335.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 340.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
 ------*-------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0
 DEGR. *  170     0     0    45    30    35    30   105   100   100     0     0     0   190   150     0     0     0     0     0

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                                                                                                                   PAGE  5
      JOB: Site 4 Bev & La Cien (S4B3PM.DAT)                    RUN: Site 4 Build 3 PM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .0    .0    .0    .0    .0    .0    .1
  5.  *    .0    .0    .0    .0    .0    .0    .1    .1
 10.  *    .0    .0    .0    .0    .0    .0    .1    .1
 15.  *    .0    .0    .0    .0    .0    .1    .1    .1
 20.  *    .0    .0    .0    .0    .0    .1    .1    .1
 25.  *    .0    .0    .0    .0    .0    .1    .1    .1
 30.  *    .0    .0    .0    .0    .0    .1    .1    .1
 35.  *    .0    .0    .0    .0    .0    .1    .1    .1
 40.  *    .0    .0    .0    .0    .0    .1    .1    .1
 45.  *    .0    .0    .0    .0    .0    .1    .1    .1
 50.  *    .0    .0    .0    .0    .0    .1    .1    .1
 55.  *    .0    .0    .0    .0    .0    .0    .0    .0
 60.  *    .0    .0    .0    .0    .0    .0    .0    .0
 65.  *    .0    .0    .0    .0    .0    .0    .0    .0
 70.  *    .0    .0    .0    .0    .0    .0    .0    .0
 75.  *    .0    .0    .0    .0    .0    .0    .0    .0
 80.  *    .0    .0    .0    .0    .0    .0    .0    .0
 85.  *    .0    .0    .0    .0    .0    .0    .0    .1
 90.  *    .0    .0    .0    .0    .0    .0    .0    .1
 95.  *    .0    .0    .0    .0    .0    .0    .0    .0
100.  *    .0    .0    .0    .0    .0    .0    .0    .0
105.  *    .0    .0    .0    .0    .0    .0    .0    .0
110.  *    .0    .0    .0    .0    .0    .0    .0    .0
115.  *    .0    .0    .0    .0    .0    .0    .0    .0
120.  *    .0    .0    .0    .0    .0    .0    .0    .0
125.  *    .0    .0    .0    .0    .0    .1    .1    .1
130.  *    .0    .0    .0    .0    .0    .1    .1    .1
135.  *    .0    .0    .0    .0    .0    .1    .1    .1
140.  *    .0    .0    .0    .0    .0    .1    .1    .1
145.  *    .0    .0    .0    .0    .0    .1    .1    .1
150.  *    .0    .0    .0    .0    .1    .1    .1    .1
155.  *    .0    .0    .0    .0    .1    .1    .1    .1
160.  *    .0    .0    .0    .0    .1    .1    .1    .1
165.  *    .0    .0    .0    .0    .1    .1    .1    .1
170.  *    .0    .0    .0    .0    .1    .1    .1    .1
175.  *    .0    .0    .0    .0    .0    .1    .1    .1
180.  *    .0    .0    .0    .0    .0    .1    .1    .1
185.  *    .0    .0    .0    .0    .0    .0    .0    .0
190.  *    .0    .0    .0    .0    .0    .0    .0    .0
195.  *    .0    .0    .0    .0    .0    .0    .0    .0
200.  *    .0    .0    .0    .0    .0    .0    .0    .0
205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                        PAGE  6
     JOB: Site 4 Bev & La Cien (S4B3PM.DAT)                 RUN: Site 4 Build 3 PM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .0
215.  *    .0    .0    .0    .0    .0    .0    .0    .0
220.  *    .0    .0    .0    .0    .0    .0    .0    .0
225.  *    .0    .0    .0    .0    .0    .0    .0    .0
230.  *    .0    .0    .0    .0    .0    .0    .0    .0
235.  *    .0    .0    .0    .0    .0    .0    .0    .0
240.  *    .0    .0    .0    .0    .0    .0    .0    .0
245.  *    .0    .0    .0    .0    .0    .0    .0    .0
250.  *    .0    .0    .0    .0    .0    .0    .0    .0
255.  *    .0    .0    .0    .0    .0    .0    .0    .0
260.  *    .0    .0    .0    .0    .0    .0    .0    .0
265.  *    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .0    .0    .0    .0    .0
360.  *    .0    .0    .0    .0    .0    .0    .0    .1
------*------------------------------------------------
MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
DEGR. *    0     0     0     0   150    15     5     0

THE HIGHEST CONCENTRATION IS     .20 PPM AT  150 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS     .10 PPM AT  170 DEGREES FROM REC1 .
THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT   45 DEGREES FROM REC4 .
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1                        CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 4 Bev & La Cien (S4B4AM.DAT)                    RUN: Site 4 Build 4 AM
      DATE: 03/22/2010   TIME: 11:50:02.46


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =    .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*-----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG    726.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG    726.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG    726.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG    581.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0     244.6     641.0 *     109.   270. AG     13. 100.0    .0 24.0  .47   5.6
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG     62.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     333.0     624.9 *      21.   270. AG      6. 100.0    .0 12.0  .10   1.1
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG     83.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     317.0     663.8 *      36.   270. AG     21. 100.0    .0 24.0  .80   1.8
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG    933.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1587.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG   1220.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     809.5     690.7 *     314.    90. AG     12. 100.0    .0 24.0  .97  16.0
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    367.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    1764.8     673.0 *    1266.    90. AG     20. 100.0    .0 24.0 2.41  64.3
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG   1507.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG   1507.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG   1507.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG   1507.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   1558.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1127.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     467.5    -117.2 *     708.   178. AG     14. 100.0    .0 24.0 1.07  35.9
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    332.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     468.7     467.6 *     123.   178. AG      6. 100.0    .0 12.0  .61   6.3
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG     99.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     446.7    -127.3 *     717.   179. AG      6. 100.0    .0 12.0 2.61  36.4
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   1239.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   2153.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   2133.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     379.3    3859.1 *    3123.   360. AG     22. 100.0    .0 36.0 1.61 158.7
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     20.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     423.9     743.5 *       9.   360. AG      7. 100.0    .0 12.0  .37    .4
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   2345.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4B4AM.DAT)                    RUN: Site 4 Build 4 AM
      DATE: 03/22/2010   TIME: 11:50:02.46

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL    ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*---------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       69       2.0       581       1584       4.10      1        3
       7. EB        Bev RT Q  *     120       62       2.0        62       1325       4.10      1        3
       9. EB        Bev LT Q  *     120      112       2.0        83       1536       4.10      1        3
      13. WB        Bev T+R Q *     120       68       2.0      1220       1573       4.10      1        3
      15. WB        Bev LT Q  *     120      110       2.0       367       1536       4.10      1        3
      22. NB        Cin THR Q *     120       76       2.0      1127       1584       4.10      1        3
      24. NB        Cin RT Q  *     120       68       2.0       332       1352       4.10      1        3
      26. NB        Cin LT Q  *     120       69       2.0        99         99       4.10      1        3
      30. SB        Cin T+R Q *     120       80       2.0      2133       1476       4.10      1        3
      32. SB        Cin LT Q  *     120       78       2.0        20        171       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *        492.0      301.0        5.0  *
      2. SE 164 S             *        488.0      448.0        5.0  *
      3. SE 82 S              *        486.0      530.0        5.0  *
      4. SE CNR               *        491.0      605.0        5.0  *
      5. SE 82 E              *        564.0      612.0        5.0  *
      6. SE 164 E             *        646.0      612.0        5.0  *
      7. SE MID E             *        775.0      615.0        5.0  *
      8. NE MID E             *        767.0      715.0        5.0  *
      9. NE 164 E             *        637.0      714.0        5.0  *
     10. NE 82 E              *        555.0      714.0        5.0  *
     11. NE CNR               *        474.0      717.0        5.0  *
     12. NE 82 N              *        473.0      796.0        5.0  *
     13. NE 164 N             *        472.0      877.0        5.0  *
     14. NE MID N             *        474.0      999.0        5.0  *
     15. NW MID N             *        372.0      996.0        5.0  *
     16. NW 164 N             *        367.0      884.0        5.0  *
     17. NW 82 N              *        367.0      803.0        5.0  *
     18. NW CNR               *        365.0      726.0        5.0  *
     19. NW 82 W              *        287.0      721.0        5.0  *
     20. NW 164 W             *        206.0      720.0        5.0  *
     21. NW MID W             *         62.0      720.0        5.0  *
     22. SW MID W             *         56.0      606.0        5.0  *
     23. SW 164 W             *        209.0      606.0        5.0  *
     24. SW 82 W              *        289.0      606.0        5.0  *
     25. SW CNR               *        361.0      601.0        5.0  *
     26. SW 82 S              *        376.0      526.0        5.0  *
     27. SW 164 S             *        380.0      445.0        5.0  *
     28. SW MID S             *        385.0      307.0        5.0  *
1
                                                                                                                 PAGE  3
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      JOB: Site 4 Bev & La Cien (S4B4AM.DAT)                    RUN: Site 4 Build 4 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .1    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                      PAGE   4
      JOB: Site 4 Bev & La Cien (S4B4AM.DAT)                    RUN: Site 4 Build 4 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .0    .2    .2    .2    .2    .0    .0
 DEGR. *  180     0     0     0     0     0     0    95   105   105   345   345   345     0    10    15    10    10     0     0

1
                                                                                                                      PAGE   5
      JOB: Site 4 Bev & La Cien (S4B4AM.DAT)                    RUN: Site 4 Build 4 AM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .0    .0    .0    .0    .0    .1    .1
  5.  *    .0    .0    .0    .0    .0    .1    .1    .1
 10.  *    .0    .0    .0    .0    .0    .1    .1    .1
 15.  *    .0    .0    .0    .0    .0    .1    .1    .1
 20.  *    .0    .0    .0    .0    .0    .1    .1    .1
 25.  *    .0    .0    .0    .0    .0    .1    .1    .1
 30.  *    .0    .0    .0    .0    .0    .1    .1    .1
 35.  *    .0    .0    .0    .0    .0    .1    .1    .1
 40.  *    .0    .0    .0    .0    .0    .1    .1    .1
 45.  *    .0    .0    .0    .0    .0    .1    .1    .1
 50.  *    .0    .0    .0    .0    .0    .1    .1    .1
 55.  *    .0    .0    .0    .0    .0    .1    .1    .1
 60.  *    .0    .0    .0    .0    .0    .1    .1    .1
 65.  *    .0    .0    .0    .0    .0    .1    .1    .1
 70.  *    .0    .0    .0    .0    .0    .1    .1    .1
 75.  *    .0    .0    .0    .0    .0    .1    .1    .1
 80.  *    .0    .0    .0    .0    .0    .1    .1    .1
 85.  *    .0    .0    .0    .0    .0    .1    .1    .1
 90.  *    .0    .0    .0    .0    .0    .1    .1    .1
 95.  *    .0    .0    .0    .0    .0    .1    .1    .1
100.  *    .0    .0    .0    .0    .0    .1    .1    .1
105.  *    .0    .0    .0    .0    .0    .1    .1    .1
110.  *    .0    .0    .0    .0    .0    .1    .1    .1
115.  *    .0    .0    .0    .0    .0    .1    .1    .1
120.  *    .0    .0    .0    .0    .0    .1    .1    .1
125.  *    .0    .0    .0    .0    .1    .1    .1    .1
130.  *    .0    .0    .0    .0    .1    .1    .1    .1
135.  *    .0    .0    .0    .0    .1    .1    .1    .1
140.  *    .0    .0    .0    .0    .1    .1    .1    .1
145.  *    .0    .0    .0    .0    .1    .1    .1    .1
150.  *    .0    .0    .0    .0    .1    .1    .1    .1
155.  *    .0    .0    .0    .0    .1    .1    .1    .1
160.  *    .0    .0    .0    .0    .1    .1    .1    .1
165.  *    .0    .0    .0    .0    .1    .1    .1    .1
170.  *    .0    .0    .0    .0    .1    .1    .1    .1
175.  *    .0    .0    .0    .0    .1    .1    .1    .1
180.  *    .0    .0    .0    .0    .0    .1    .1    .1
185.  *    .0    .0    .0    .0    .0    .0    .1    .1
190.  *    .0    .0    .0    .0    .0    .0    .0    .0
195.  *    .0    .0    .0    .0    .0    .0    .0    .0
200.  *    .0    .0    .0    .0    .0    .0    .0    .0
205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE  6
     JOB: Site 4 Bev & La Cien (S4B4AM.DAT)                    RUN: Site 4 Build 4 AM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .0    .0    .0    .0    .0    .0    .0    .0
215.  *    .0    .0    .0    .0    .0    .0    .0    .0
220.  *    .0    .0    .0    .0    .0    .0    .0    .0
225.  *    .0    .0    .0    .0    .0    .0    .0    .0
230.  *    .0    .0    .0    .0    .0    .0    .0    .0
235.  *    .0    .0    .0    .0    .0    .0    .0    .0
240.  *    .0    .0    .0    .0    .0    .0    .0    .0
245.  *    .0    .0    .0    .0    .0    .0    .0    .0
250.  *    .0    .0    .0    .0    .0    .0    .0    .0
255.  *    .0    .0    .0    .0    .0    .0    .0    .0
260.  *    .0    .0    .0    .0    .0    .0    .0    .0
265.  *    .0    .0    .0    .0    .0    .0    .0    .0
270.  *    .0    .0    .0    .0    .0    .0    .0    .0
275.  *    .0    .0    .0    .0    .0    .0    .0    .0
280.  *    .0    .0    .0    .0    .0    .0    .0    .0
285.  *    .0    .0    .0    .0    .0    .0    .0    .0
290.  *    .0    .0    .0    .0    .0    .0    .0    .0
295.  *    .0    .0    .0    .0    .0    .0    .0    .0
300.  *    .0    .0    .0    .0    .0    .0    .0    .0
305.  *    .0    .0    .0    .0    .0    .0    .0    .0
310.  *    .0    .0    .0    .0    .0    .0    .0    .0
315.  *    .0    .0    .0    .0    .0    .0    .0    .0
320.  *    .0    .0    .0    .0    .0    .0    .0    .0
325.  *    .0    .0    .0    .0    .0    .0    .0    .0
330.  *    .0    .0    .0    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .0    .0    .0    .0    .1
360.  *    .0    .0    .0    .0    .0    .0    .1    .1
------*------------------------------------------------
MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
DEGR. *    0     0     0     0   125     5     0     0

THE HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC15.
THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   15 DEGREES FROM REC16.
THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC17.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 4 Bev & La Cien (S4B4PM.DAT)                    RUN: Site 4 Build 4 PM
      DATE: 03/22/2010   TIME: 11:56:42.98


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *          LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2      *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*---------------------------------------*-----------------------------------------------------------
       1. EB         Bev AP    *  -543.0     891.0    -185.0     701.0 *     405.   118. AG  1853.    .8    .0 44.0
       2. EB         Bev AP    *  -185.0     701.0     -55.0     655.0 *     138.   109. AG  1853.    .8    .0 44.0
       3. EB         Bev AP    *   -55.0     655.0     123.0     646.0 *     178.    93. AG  1853.    .8    .0 44.0
       4. EB         Bev THRU  *   124.0     641.0     417.0     641.0 *     293.    90. AG  1610.    .8    .0 44.0
       5. EB         Bev THR Q *   354.0     641.0   -2061.8     641.0 *    2416.   270. AG    13. 100.0    .0 24.0 1.33 122.7
       6. EB         Bev RT    *   126.0     624.0     402.0     626.0 *     276.    90. AG    54.    .8    .0 32.0
       7. EB         Bev RT Q  *   354.0     625.0     335.4     624.9 *      19.   270. AG     6. 100.0    .0 12.0  .12    .9
       8. EB         Bev LT    *   124.0     663.0     413.0     664.0 *     289.    90. AG   189.    .8    .0 44.0
       9. EB         Bev LT Q  *   353.0     664.0      66.6     662.7 *     286.   270. AG    20. 100.0    .0 24.0 1.24  14.5
      10. EB         Bev DP    *   418.0     641.0    1427.0     656.0 *    1009.    89. AG  2090.    .8    .0 44.0
      11. WB         Bev AP    *   683.0     689.0    1428.0     687.0 *     745.    90. AG  1239.    .8    .0 44.0
      12. WB         Bev T+R   *   683.0     690.0     443.0     689.0 *     240.   270. AG   781.    .8    .0 44.0
      13. WB         Bev T+R Q *   495.0     689.0     644.3     689.8 *     149.    90. AG    13. 100.0    .0 24.0  .64   7.6
      14. WB         Bev LT    *   685.0     667.0     445.0     665.0 *     240.   270. AG   458.    .8    .0 44.0
      15. WB         Bev LT Q  *   499.0     666.0    2271.0     675.8 *    1772.    90. AG    20. 100.0    .0 24.0 3.01  90.0
      16. WB         Bev DP    *   442.0     689.0      75.0     687.0 *     367.   270. AG  1288.    .8    .0 44.0
      17. WB         Bev DP    *    75.0     687.0     -43.0     699.0 *     119.   276. AG  1288.    .8    .0 44.0
      18. WB         Bev DP    *   -43.0     699.0    -189.0     746.0 *     153.   288. AG  1288.    .8    .0 44.0
      19. WB         Bev DP    *  -189.0     746.0    -533.0     933.0 *     392.   299. AG  1288.    .8    .0 44.0
      20. NB         Cin AP    *   461.0     300.0     483.0    -335.0 *     635.   178. AG  2624.    .8    .0 56.0
      21. NB         Cin THRU  *   456.0     301.0     445.0     652.0 *     351.   358. AG  1767.    .8    .0 44.0
      22. NB         Cin THR Q *   447.0     590.0     560.4   -3321.2 *    3913.   178. AG    14. 100.0    .0 24.0 1.63 198.8
      23. NB         Cin RT    *   474.0     302.0     463.0     648.0 *     346.   358. AG   468.    .8    .0 32.0
      24. NB         Cin RT Q  *   465.0     591.0     477.4     174.9 *     416.   178. AG     6. 100.0    .0 12.0 1.03  21.1
      25. NB         Cin LT    *   438.0     301.0     430.0     652.0 *     351.   359. AG   389.    .8    .0 32.0
      26. NB         Cin LT Q  *   431.0     589.0     511.0   -3053.2 *    3643.   179. AG     6. 100.0    .0 12.0 6.59 185.1
      27. NB         Cin DP    *   445.0     652.0     431.0    1659.0 *    1007.   359. AG  1957.    .8    .0 44.0
      28. SB         Cin AP    *   406.0    1039.0     398.0    1660.0 *     621.   359. AG  1510.    .8    .0 44.0
      29. SB         Cin T+R   *   401.0    1038.0     404.0     661.0 *     377.   180. AG  1498.    .8    .0 56.0
      30. SB         Cin T+R Q *   403.0     736.0     396.0    1660.7 *     925.   360. AG    22. 100.0    .0 36.0 1.14  47.0
      31. SB         Cin LT    *   422.0    1036.0     424.0     666.0 *     370.   180. AG    12.    .8    .0 32.0
      32. SB         Cin LT Q  *   424.0     735.0     424.0     740.1 *       5.   360. AG     7. 100.0    .0 12.0  .22    .3
      33. SB         Cin DP    *   404.0     662.0     437.0    -338.0 *    1001.   178. AG  1891.    .8    .0 56.0
1
                                                                                                                       PAGE  2
      JOB: Site 4 Bev & La Cien (S4B4PM.DAT)                    RUN: Site 4 Build 4 PM
      DATE: 03/22/2010   TIME: 11:56:42.98

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE  EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)     (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       5. EB         Bev THR Q *     120       70       2.0      1610       1584       4.10      1        3
       7. EB         Bev RT Q  *     120       63       2.0        54       1048       4.10      1        3
       9. EB         Bev LT Q  *     120      110       2.0       189       1536       4.10      1        3
      13. WB         Bev T+R Q *     120       70       2.0       781       1583       4.10      1        3
      15. WB         Bev LT Q  *     120      110       2.0       458       1536       4.10      1        3
      22. NB         Cin THR Q *     120       75       2.0      1767       1584       4.10      1        3
      24. NB         Cin RT Q  *     120       67       2.0       468       1113       4.10      1        3
      26. NB         Cin LT Q  *     120       69       2.0       389        153       4.10      1        3
      30. SB         Cin T+R Q *     120       80       2.0      1498       1465       4.10      1        3
      32. SB         Cin LT Q  *     120       77       2.0        12        168       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-----------------------------------*
      1. SE MID S             *       492.0      301.0       5.0   *
      2. SE 164 S             *       488.0      448.0       5.0   *
      3. SE 82 S              *       486.0      530.0       5.0   *
      4. SE CNR               *       491.0      605.0       5.0   *
      5. SE 82 E              *       564.0      612.0       5.0   *
      6. SE 164 E             *       646.0      612.0       5.0   *
      7. SE MID E             *       775.0      615.0       5.0   *
      8. NE MID E             *       767.0      715.0       5.0   *
      9. NE 164 E             *       637.0      714.0       5.0   *
     10. NE 82 E              *       555.0      714.0       5.0   *
     11. NE CNR               *       474.0      717.0       5.0   *
     12. NE 82 N              *       473.0      796.0       5.0   *
     13. NE 164 N             *       472.0      877.0       5.0   *
     14. NE MID N             *       474.0      999.0       5.0   *
     15. NW MID N             *       372.0      996.0       5.0   *
     16. NW 164 N             *       367.0      884.0       5.0   *
     17. NW 82 N              *       367.0      803.0       5.0   *
     18. NW CNR               *       365.0      726.0       5.0   *
     19. NW 82 W              *       287.0      721.0       5.0   *
     20. NW 164 W             *       206.0      720.0       5.0   *
     21. NW MID W             *        62.0      720.0       5.0   *
     22. SW MID W             *        56.0      606.0       5.0   *
     23. SW 164 W             *       209.0      606.0       5.0   *
     24. SW 82 W              *       289.0      606.0       5.0   *
     25. SW CNR               *       361.0      601.0       5.0   *
     26. SW 82 S              *       376.0      526.0       5.0   *
     27. SW 164 S             *       380.0      445.0       5.0   *
     28. SW MID S             *       385.0      307.0       5.0   *
1
                                                                                                                       PAGE  3
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      JOB: Site 4 Bev & La Cien (S4B4PM.DAT)                RUN: Site 4 Build 4 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .1    .0    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  40.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
1
                                                                                                                     PAGE  4
      JOB: Site 4 Bev & La Cien (S4B4PM.DAT)                RUN: Site 4 Build 4 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 340.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .1    .1    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0
 DEGR. *  170     0     0    45    30    35    30   105   100   100     0     0   190   190   150     0     0     0     0     0

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                                                                                                                     PAGE  5
      JOB: Site 4 Bev & La Cien (S4B4PM.DAT)                RUN: Site 4 Build 4 PM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .1
   5.  *    .0    .0    .0    .0    .0    .0    .1    .1
  10.  *    .0    .0    .0    .0    .0    .0    .1    .1
  15.  *    .0    .0    .0    .0    .0    .0    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .0    .0    .1
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .0    .1    .1    .1
 175.  *    .0    .0    .0    .0    .0    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  6
      JOB: Site 4 Bev & La Cien (S4B4PM.DAT)                    RUN: Site 4 Build 4 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *     0     0     0     0   150    20     5     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT  150 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .10 PPM AT  170 DEGREES FROM REC1 .
 THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT   45 DEGREES FROM REC4 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                   PAGE  1

      JOB: Site 4 Bev & La Cien (S4B5AM.DAT)                   RUN: Site 4 Build 5 AM
      DATE: 03/22/2010   TIME: 12:16:54.14


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH     EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)        (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG    740.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG    740.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG    740.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG    594.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0     241.9     641.0 *     112.   270. AG     13. 100.0    .0 24.0  .48   5.7
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG     64.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     332.3     624.9 *      22.   270. AG      6. 100.0    .0 12.0  .11   1.1
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG     82.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     317.0     663.8 *      36.   270. AG     21. 100.0    .0 24.0  .80   1.8
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG    933.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1594.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG   1240.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     830.1     690.8 *     335.    90. AG     12. 100.0    .0 24.0  .99  17.0
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    354.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    1698.8     672.7 *    1200.    90. AG     20. 100.0    .0 24.0 2.33  60.9
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG   1527.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG   1527.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG   1527.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG   1527.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   1552.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1134.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     468.7    -159.1 *     749.   178. AG     14. 100.0    .0 24.0 1.08  38.1
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    319.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     468.5     472.4 *     119.   178. AG      6. 100.0    .0 12.0  .59   6.0
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG     99.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     446.7    -127.3 *     717.   179. AG      6. 100.0    .0 12.0 2.61  36.4
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   1245.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   2130.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   2110.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     379.9    3775.0 *    3039.   360. AG     22. 100.0    .0 36.0 1.59 154.4
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     20.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     423.9     743.5 *       9.   360. AG      7. 100.0    .0 12.0  .37    .4
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   2311.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 4 Bev & La Cien (S4B5AM.DAT)                   RUN: Site 4 Build 5 AM
      DATE: 03/22/2010   TIME: 12:16:54.14

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       69       2.0       594          1584     4.10      1        3
       7. EB        Bev RT Q  *     120       62       2.0        64          1325     4.10      1        3
       9. EB        Bev LT Q  *     120      112       2.0        82          1536     4.10      1        3
      13. WB        Bev T+R Q *     120       68       2.0      1240          1574     4.10      1        3
      15. WB        Bev LT Q  *     120      110       2.0       354          1536     4.10      1        3
      22. NB        Cin THR Q *     120       76       2.0      1134          1584     4.10      1        3
      24. NB        Cin RT Q  *     120       68       2.0       319          1352     4.10      1        3
      26. NB        Cin LT Q  *     120       69       2.0        99            99     4.10      1        3
      30. SB        Cin T+R Q *     120       80       2.0      2110          1475     4.10      1        3
      32. SB        Cin LT Q  *     120       78       2.0        20           171     4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       492.0      301.0        5.0   *
      2. SE 164 S             *       488.0      448.0        5.0   *
      3. SE 82 S              *       486.0      530.0        5.0   *
      4. SE CNR               *       491.0      605.0        5.0   *
      5. SE 82 E              *       564.0      612.0        5.0   *
      6. SE 164 E             *       646.0      612.0        5.0   *
      7. SE MID E             *       775.0      615.0        5.0   *
      8. NE MID E             *       767.0      715.0        5.0   *
      9. NE 164 E             *       637.0      714.0        5.0   *
     10. NE 82 E              *       555.0      714.0        5.0   *
     11. NE CNR               *       474.0      717.0        5.0   *
     12. NE 82 N              *       473.0      796.0        5.0   *
     13. NE 164 N             *       472.0      877.0        5.0   *
     14. NE MID N             *       474.0      999.0        5.0   *
     15. NW MID N             *       372.0      996.0        5.0   *
     16. NW 164 N             *       367.0      884.0        5.0   *
     17. NW 82 N              *       367.0      803.0        5.0   *
     18. NW CNR               *       365.0      726.0        5.0   *
     19. NW 82 W              *       287.0      721.0        5.0   *
     20. NW 164 W             *       206.0      720.0        5.0   *
     21. NW MID W             *        62.0      720.0        5.0   *
     22. SW MID W             *        56.0      606.0        5.0   *
     23. SW 164 W             *       209.0      606.0        5.0   *
     24. SW 82 W              *       289.0      606.0        5.0   *
     25. SW CNR               *       361.0      601.0        5.0   *
     26. SW 82 S              *       376.0      526.0        5.0   *
     27. SW 164 S             *       380.0      445.0        5.0   *
     28. SW MID S             *       385.0      307.0        5.0   *
1
                                                                                                                 PAGE  3
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      JOB: Site 4 Bev & La Cien (S4B5AM.DAT)                    RUN: Site 4 Build 5 AM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  45.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0
  50.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .1    .1    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 170.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .1    .0    .0
 175.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .1    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE   4
      JOB: Site 4 Bev & La Cien (S4B5AM.DAT)                    RUN: Site 4 Build 5 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .0    .2    .2    .2    .2    .0    .0
 DEGR. *  180     0     0     0     0     0     0    95   105   105   345   345   345     0    10    15    10    10     0     0

1
                                                                                                                PAGE   5
      JOB: Site 4 Bev & La Cien (S4B5AM.DAT)                    RUN: Site 4 Build 5 AM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .1    .1
   5.  *    .0    .0    .0    .0    .0    .0    .1    .1
  10.  *    .0    .0    .0    .0    .0    .1    .1    .1
  15.  *    .0    .0    .0    .0    .0    .1    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .1    .1    .1
  55.  *    .0    .0    .0    .0    .0    .1    .1    .1
  60.  *    .0    .0    .0    .0    .0    .1    .1    .1
  65.  *    .0    .0    .0    .0    .0    .1    .1    .1
  70.  *    .0    .0    .0    .0    .0    .1    .1    .1
  75.  *    .0    .0    .0    .0    .0    .1    .1    .1
  80.  *    .0    .0    .0    .0    .0    .1    .1    .1
  85.  *    .0    .0    .0    .0    .0    .1    .1    .1
  90.  *    .0    .0    .0    .0    .0    .1    .1    .1
  95.  *    .0    .0    .0    .0    .0    .1    .1    .1
 100.  *    .0    .0    .0    .0    .0    .1    .1    .1
 105.  *    .0    .0    .0    .0    .0    .1    .1    .1
 110.  *    .0    .0    .0    .0    .0    .1    .1    .1
 115.  *    .0    .0    .0    .0    .0    .1    .1    .1
 120.  *    .0    .0    .0    .0    .0    .1    .1    .1
 125.  *    .0    .0    .0    .0    .1    .1    .1    .1
 130.  *    .0    .0    .0    .0    .1    .1    .1    .1
 135.  *    .0    .0    .0    .0    .1    .1    .1    .1
 140.  *    .0    .0    .0    .0    .1    .1    .1    .1
 145.  *    .0    .0    .0    .0    .1    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .1    .1    .1    .1
 175.  *    .0    .0    .0    .0    .1    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .1    .1
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE  6
      JOB: Site 4 Bev & La Cien (S4B5AM.DAT)                   RUN: Site 4 Build 5 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .1
 360.  *    .0    .0    .0    .0    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *    0     0     0     0   125    10     0     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT   15 DEGREES FROM REC16.
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT   10 DEGREES FROM REC17.
```

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1                        CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 4 Bev & La Cien (S4B5PM.DAT)                    RUN: Site 4 Build 5 PM
      DATE: 03/22/2010   TIME: 12:17:08.91


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)        (VEH)
      ------------------------*----------------------------------------*-------------------------------------------------------------
       1. EB        Bev AP    *   -543.0     891.0    -185.0     701.0 *     405.   118. AG   1813.    .8    .0 44.0
       2. EB        Bev AP    *   -185.0     701.0     -55.0     655.0 *     138.   109. AG   1813.    .8    .0 44.0
       3. EB        Bev AP    *    -55.0     655.0     123.0     646.0 *     178.    93. AG   1813.    .8    .0 44.0
       4. EB        Bev THRU  *    124.0     641.0     417.0     641.0 *     293.    90. AG   1594.    .8    .0 44.0
       5. EB        Bev THR Q *    354.0     641.0   -1978.4     641.0 *    2332.   270. AG     13. 100.0    .0 24.0 1.31 118.5
       6. EB        Bev RT    *    126.0     624.0     402.0     626.0 *     276.    90. AG     55.    .8    .0 32.0
       7. EB        Bev RT Q  *    354.0     625.0     335.1     624.9 *      19.   270. AG      6. 100.0    .0 12.0  .12   1.0
       8. EB        Bev LT    *    124.0     663.0     413.0     664.0 *     289.    90. AG    164.    .8    .0 44.0
       9. EB        Bev LT Q  *    353.0     664.0     198.7     663.3 *     154.   270. AG     20. 100.0    .0 24.0 1.08   7.8
      10. EB        Bev DP    *    418.0     641.0    1427.0     656.0 *    1009.    89. AG   2070.    .8    .0 44.0
      11. WB        Bev AP    *    683.0     689.0    1428.0     687.0 *     745.    90. AG   1216.    .8    .0 44.0
      12. WB        Bev T+R   *    683.0     690.0     443.0     689.0 *     240.   270. AG    760.    .8    .0 44.0
      13. WB        Bev T+R Q *    495.0     689.0     640.4     689.8 *     145.    90. AG     13. 100.0    .0 24.0  .63   7.4
      14. WB        Bev LT    *    685.0     667.0     445.0     665.0 *     240.   270. AG    456.    .8    .0 44.0
      15. WB        Bev LT Q  *    499.0     666.0    2260.0     675.8 *    1761.    90. AG     20. 100.0    .0 24.0 3.00  89.5
      16. WB        Bev DP    *    442.0     689.0      75.0     687.0 *     367.   270. AG   1265.    .8    .0 44.0
      17. WB        Bev DP    *     75.0     687.0     -43.0     699.0 *     119.   276. AG   1265.    .8    .0 44.0
      18. WB        Bev DP    *    -43.0     699.0    -189.0     746.0 *     153.   288. AG   1265.    .8    .0 44.0
      19. WB        Bev DP    *   -189.0     746.0    -533.0     933.0 *     392.   299. AG   1265.    .8    .0 44.0
      20. NB        Cin AP    *    461.0     300.0     483.0    -335.0 *     635.   178. AG   2653.    .8    .0 56.0
      21. NB        Cin THRU  *    456.0     301.0     445.0     652.0 *     351.   358. AG   1811.    .8    .0 44.0
      22. NB        Cin THR Q *    447.0     590.0     575.2   -3831.7 *    4424.   178. AG     14. 100.0    .0 24.0 1.76 224.7
      23. NB        Cin RT    *    474.0     302.0     463.0     648.0 *     346.   358. AG    448.    .8    .0 32.0
      24. NB        Cin RT Q  *    465.0     591.0     476.6     199.5 *     392.   178. AG      6. 100.0    .0 12.0 1.03  19.9
      25. NB        Cin LT    *    438.0     301.0     430.0     652.0 *     351.   359. AG    394.    .8    .0 32.0
      26. NB        Cin LT Q  *    431.0     589.0     512.3   -3109.6 *    3699.   179. AG      6. 100.0    .0 12.0 6.68 187.9
      27. NB        Cin DP    *    445.0     652.0     431.0    1659.0 *    1007.   359. AG   1976.    .8    .0 44.0
      28. SB        Cin AP    *    406.0    1039.0     398.0    1660.0 *     621.   359. AG   1544.    .8    .0 44.0
      29. SB        Cin T+R   *    401.0    1038.0     404.0     661.0 *     377.   180. AG   1516.    .8    .0 56.0
      30. SB        Cin T+R Q *    403.0     736.0     395.6    1713.7 *     978.   360. AG     22. 100.0    .0 36.0 1.15  49.7
      31. SB        Cin LT    *    422.0    1036.0     424.0     666.0 *     370.   180. AG     28.    .8    .0 32.0
      32. SB        Cin LT Q  *    424.0     735.0     423.9     746.6 *      12.   360. AG      7. 100.0    .0 12.0  .51    .6
      33. SB        Cin DP    *    404.0     662.0     437.0    -338.0 *    1001.   178. AG   1915.    .8    .0 56.0
1
                                                                                                                       PAGE  2
      JOB: Site 4 Bev & La Cien (S4B5PM.DAT)                    RUN: Site 4 Build 5 PM
      DATE: 03/22/2010   TIME: 12:17:08.91

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)      (SEC)     (VPH)      (VPH)    (gm/hr)
      ------------------------*----------------------------------------------------------------------------
       5. EB        Bev THR Q *     120       70       2.0      1594       1584       4.10      1        3
       7. EB        Bev RT Q  *     120       63       2.0        55       1048       4.10      1        3
       9. EB        Bev LT Q  *     120      110       2.0       164       1536       4.10      1        3
      13. WB        Bev T+R Q *     120       70       2.0       760       1583       4.10      1        3
      15. WB        Bev LT Q  *     120      110       2.0       456       1536       4.10      1        3
      22. NB        Cin THR Q *     120       77       2.0      1811       1584       4.10      1        3
      24. NB        Cin RT Q  *     120       69       2.0       448       1114       4.10      1        3
      26. NB        Cin LT Q  *     120       70       2.0       394        156       4.10      1        3
      30. SB        Cin T+R Q *     120       80       2.0      1516       1469       4.10      1        3
      32. SB        Cin LT Q  *     120       76       2.0        28        168       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)           *
         RECEPTOR             *       X           Y          Z       *
     -------------------------*--------------------------------------*
       1. SE MID S            *       492.0       301.0        5.0   *
       2. SE 164 S            *       488.0       448.0        5.0   *
       3. SE 82 S             *       486.0       530.0        5.0   *
       4. SE CNR              *       491.0       605.0        5.0   *
       5. SE 82 E             *       564.0       612.0        5.0   *
       6. SE 164 E            *       646.0       612.0        5.0   *
       7. SE MID E            *       775.0       615.0        5.0   *
       8. NE MID E            *       767.0       715.0        5.0   *
       9. NE 164 E            *       637.0       714.0        5.0   *
      10. NE 82 E             *       555.0       714.0        5.0   *
      11. NE CNR              *       474.0       717.0        5.0   *
      12. NE 82 N             *       473.0       796.0        5.0   *
      13. NE 164 N            *       472.0       877.0        5.0   *
      14. NE MID N            *       474.0       999.0        5.0   *
      15. NW MID N            *       372.0       996.0        5.0   *
      16. NW 164 N            *       367.0       884.0        5.0   *
      17. NW 82 N             *       367.0       803.0        5.0   *
      18. NW CNR              *       365.0       726.0        5.0   *
      19. NW 82 W             *       287.0       721.0        5.0   *
      20. NW 164 W            *       206.0       720.0        5.0   *
      21. NW MID W            *        62.0       720.0        5.0   *
      22. SW MID W            *        56.0       606.0        5.0   *
      23. SW 164 W            *       209.0       606.0        5.0   *
      24. SW 82 W             *       289.0       606.0        5.0   *
      25. SW CNR              *       361.0       601.0        5.0   *
      26. SW 82 S             *       376.0       526.0        5.0   *
      27. SW 164 S            *       380.0       445.0        5.0   *
      28. SW MID S            *       385.0       307.0        5.0   *
1
                                                                                                                       PAGE  3
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      JOB: Site 4 Bev & La Cien (S4B5PM.DAT)                    RUN: Site 4 Build 5 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  40.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 130.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 135.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 140.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0
 145.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0
 150.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 155.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 160.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .1    .0    .0    .0    .0
 165.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
1
                                                                                                                   PAGE  4
      JOB: Site 4 Bev & La Cien (S4B5PM.DAT)                    RUN: Site 4 Build 5 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 330.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 335.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 340.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .1    .1    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .0    .0    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .0    .0
 DEGR. *  170     0     0    45    30    35    35   105   100   100     0     0     0   190   150     0     0     0     0     0

1
                                                                                                                   PAGE  5
      JOB: Site 4 Bev & La Cien (S4B5PM.DAT)                    RUN: Site 4 Build 5 PM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .1
   5.  *    .0    .0    .0    .0    .0    .0    .1    .1
  10.  *    .0    .0    .0    .0    .0    .0    .1    .1
  15.  *    .0    .0    .0    .0    .0    .1    .1    .1
  20.  *    .0    .0    .0    .0    .0    .1    .1    .1
  25.  *    .0    .0    .0    .0    .0    .1    .1    .1
  30.  *    .0    .0    .0    .0    .0    .1    .1    .1
  35.  *    .0    .0    .0    .0    .0    .1    .1    .1
  40.  *    .0    .0    .0    .0    .0    .1    .1    .1
  45.  *    .0    .0    .0    .0    .0    .1    .1    .1
  50.  *    .0    .0    .0    .0    .0    .0    .1    .1
  55.  *    .0    .0    .0    .0    .0    .0    .0    .0
  60.  *    .0    .0    .0    .0    .0    .0    .0    .0
  65.  *    .0    .0    .0    .0    .0    .0    .0    .0
  70.  *    .0    .0    .0    .0    .0    .0    .0    .0
  75.  *    .0    .0    .0    .0    .0    .0    .0    .0
  80.  *    .0    .0    .0    .0    .0    .0    .0    .0
  85.  *    .0    .0    .0    .0    .0    .0    .0    .0
  90.  *    .0    .0    .0    .0    .0    .0    .0    .0
  95.  *    .0    .0    .0    .0    .0    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .0
 105.  *    .0    .0    .0    .0    .0    .0    .0    .0
 110.  *    .0    .0    .0    .0    .0    .0    .0    .0
 115.  *    .0    .0    .0    .0    .0    .0    .0    .0
 120.  *    .0    .0    .0    .0    .0    .0    .0    .0
 125.  *    .0    .0    .0    .0    .0    .0    .1    .1
 130.  *    .0    .0    .0    .0    .0    .1    .1    .1
 135.  *    .0    .0    .0    .0    .0    .1    .1    .1
 140.  *    .0    .0    .0    .0    .0    .1    .1    .1
 145.  *    .0    .0    .0    .0    .0    .1    .1    .1
 150.  *    .0    .0    .0    .0    .1    .1    .1    .1
 155.  *    .0    .0    .0    .0    .1    .1    .1    .1
 160.  *    .0    .0    .0    .0    .1    .1    .1    .1
 165.  *    .0    .0    .0    .0    .1    .1    .1    .1
 170.  *    .0    .0    .0    .0    .0    .1    .1    .1
 175.  *    .0    .0    .0    .0    .0    .1    .1    .1
 180.  *    .0    .0    .0    .0    .0    .1    .1    .1
 185.  *    .0    .0    .0    .0    .0    .0    .0    .0
 190.  *    .0    .0    .0    .0    .0    .0    .0    .0
 195.  *    .0    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1                                                                                                                PAGE  6
      JOB: Site 4 Bev & La Cien (S4B5PM.DAT)                    RUN: Site 4 Build 5 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .0    .0    .0    .0    .0    .0    .0    .0
 215.  *    .0    .0    .0    .0    .0    .0    .0    .0
 220.  *    .0    .0    .0    .0    .0    .0    .0    .0
 225.  *    .0    .0    .0    .0    .0    .0    .0    .0
 230.  *    .0    .0    .0    .0    .0    .0    .0    .0
 235.  *    .0    .0    .0    .0    .0    .0    .0    .0
 240.  *    .0    .0    .0    .0    .0    .0    .0    .0
 245.  *    .0    .0    .0    .0    .0    .0    .0    .0
 250.  *    .0    .0    .0    .0    .0    .0    .0    .0
 255.  *    .0    .0    .0    .0    .0    .0    .0    .0
 260.  *    .0    .0    .0    .0    .0    .0    .0    .0
 265.  *    .0    .0    .0    .0    .0    .0    .0    .0
 270.  *    .0    .0    .0    .0    .0    .0    .0    .0
 275.  *    .0    .0    .0    .0    .0    .0    .0    .0
 280.  *    .0    .0    .0    .0    .0    .0    .0    .0
 285.  *    .0    .0    .0    .0    .0    .0    .0    .0
 290.  *    .0    .0    .0    .0    .0    .0    .0    .0
 295.  *    .0    .0    .0    .0    .0    .0    .0    .0
 300.  *    .0    .0    .0    .0    .0    .0    .0    .0
 305.  *    .0    .0    .0    .0    .0    .0    .0    .0
 310.  *    .0    .0    .0    .0    .0    .0    .0    .0
 315.  *    .0    .0    .0    .0    .0    .0    .0    .0
 320.  *    .0    .0    .0    .0    .0    .0    .0    .0
 325.  *    .0    .0    .0    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .1
 ------*------------------------------------------------
 MAX   *    .0    .0    .0    .0    .1    .1    .1    .1
 DEGR. *    0     0     0     0   150    15     5     0

 THE HIGHEST CONCENTRATION IS     .20 PPM AT  150 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .10 PPM AT  170 DEGREES FROM REC1 .
 THE 3RD HIGHEST CONCENTRATION IS     .10 PPM AT   45 DEGREES FROM REC4 .
```

Site 5 – La Brea & Olympic
Input Files

```
Site 5 Olymp & La Brea (S5EXAM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Existing AM                       33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1183 3.3  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1183 3.3  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        65       2.0 1183   20.5 1108 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1220 3.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1542 3.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1542 3.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        54       2.0 1542   20.5 1103 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1679 3.3  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    1463 3.3  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    1463 3.3  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    1463 3.3  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1346 3.3  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1346 3.3  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1346   20.5 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     117 3.3  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     117 3.3  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        86       2.0  117   20.5 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    1452 3.3  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    1452 3.3  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    1452 3.3  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    1655 3.3  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    1536 3.3  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    1536 3.3  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        69       2.0 1536   20.5 1403 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     119 3.3  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     119 3.3  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        58       2.0  119   20.5  208 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    1492 3.3  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    1492 3.3  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    1492 3.3  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    1492 3.3  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    1492 3.3  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    1492 3.3  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5EXPM.DAT)    60.0321.0.0000.000280.30480000   1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Existing PM                       33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1745 3.3  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1745 3.3  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        65       2.0 1745   20.5 1154 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1744 3.3  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1171 3.3  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1171 3.3  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        54       2.0 1171   20.5 1094 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1167 3.3  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    1547 3.3  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    1547 3.3  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    1547 3.3  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1494 3.3  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1494 3.3  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1494   20.5 1422 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      53 3.3  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      53 3.3  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        90       2.0   53   20.5 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    1699 3.3  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    1699 3.3  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    1699 3.3  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    1845 3.3  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    1705 3.3  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    1705 3.3  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        65       2.0 1705   20.5 1411 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     140 3.3  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     140 3.3  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        53       2.0  140   20.5  180 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    1698 3.3  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    1698 3.3  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    1698 3.3  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    1698 3.3  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    1698 3.3  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    1698 3.3  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5NBAM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 No Build AM                       33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1574 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1574 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        66       2.0 1574   04.1 1112 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1611 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    2014 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    2014 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        54       2.0 2014   04.1 1105 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2122 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2059 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2059 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2059 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1961 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1961 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        69       2.0 1961   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      98 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      98 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        88       2.0   98   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2119 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2322 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2165 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2165 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        66       2.0 2165   04.1 1408 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     157 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     157 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        54       2.0  157   04.1  190 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2117 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2117 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2117 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2117 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2117 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2117 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5NBPM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 No Build PM                       33   1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2302 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2302 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        66       2.0 2302   04.1 1115 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2212 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1456 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1456 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        56       2.0 1456   04.1 1100 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1502 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2217 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2217 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2217 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2174 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2174 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 2174   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      43 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      43 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   43   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2520 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2520 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2520 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2660 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2472 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2472 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        61       2.0 2472   04.1 1412 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     188 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     188 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51       2.0  188   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2401 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2401 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2401 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2401 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2401 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2401 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5M1AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 MOS 1 AM                          33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1576 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1576 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        66       2.0 1576   04.1 1111 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1595 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1928 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1928 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        54       2.0 1928   04.1 1106 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2087 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2062 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2062 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2062 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1961 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1961 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1961   04.1 1422 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     101 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     101 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        88       2.0  101   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2113 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2113 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2113 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2347 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2200 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2200 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        66       2.0 2200   04.1 1404 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     147 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     147 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        54       2.0  147   04.1  191 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2118 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2118 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2118 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2118 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2118 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2118 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5M1PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 MOS 1 PM                          33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2330 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2330 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        65       2.0 2330   04.1 1113 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2181 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1459 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1459 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        56       2.0 1459   04.1 1098 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1529 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2190 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2190 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2190 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2143 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2143 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        64       2.0 2143   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      47 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      47 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   47   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2562 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2562 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2562 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2702 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2515 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2515 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        60       2.0 2515   04.1 1411 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     187 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     187 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51       2.0  187   04.1  161 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2409 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2409 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2409 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2409 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2409 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2409 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5M2AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 MOS 2 AM                          33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1580 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1580 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        64       2.0 1580   04.1 1110 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1583 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1900 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1900 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        52       2.0 1900   04.1 1103 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2025 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2071 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2071 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2071 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1950 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1950 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1950   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     121 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     121 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        89       2.0  121   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2119 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2342 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2204 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2204 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        67       2.0 2204   04.1 1409 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     138 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     138 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        58       2.0  138   04.1  196 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2166 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2166 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2166 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2166 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2166 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2166 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5M2PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 MOS 2 PM                           33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2286 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2286 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        68       2.0 2286   04.1 1117 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2151 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1487 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1487 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        57       2.0 1487   04.1 1101 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1533 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2206 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2206 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2206 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2161 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2161 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        64       2.0 2161   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      45 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      45 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   45   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2567 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2567 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2567 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2684 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2495 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2495 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        59       2.0 2495   04.1 1412 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     189 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     189 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        50       2.0  189   04.1  158 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2412 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2412 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2412 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2412 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2412 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2412 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B1AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Build 1 AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1590 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1590 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        66       2.0 1590   04.1 1112 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1612 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1948 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1948 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        55       2.0 1948   04.1 1106 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2060 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2040 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2040 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2040 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1944 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1944 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1944   04.1 1422 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      96 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      96 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        88       2.0   96   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2107 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2107 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2107 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2343 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2185 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2185 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        66       2.0 2185   04.1 1408 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     158 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     158 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        54       2.0  158   04.1  189 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2142 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2142 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2142 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2142 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2142 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2142 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B1PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Build 1 PM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2260 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2260 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        65       2.0 2260   04.1 1115 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2168 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1438 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1438 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        56       2.0 1438   04.1 1099 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1541 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2204 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2204 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2204 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2163 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2163 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 2163   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      41 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      41 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   41   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2518 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2518 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2518 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2672 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2483 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2483 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        60       2.0 2483   04.1 1409 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     189 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     189 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51       2.0  189   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2347 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0  72
```

```
Site 5 Olymp & La Brea (S5B2AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Build 2 AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1548 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1548 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        66       2.0 1548   04.1 1111 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1564 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1925 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1925 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        54       2.0 1925   04.1 1105 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2025 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2059 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2059 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2059 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1959 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1959 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1959   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     100 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     100 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        88       2.0  100   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2119 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2119 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2326 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2184 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2184 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        67       2.0 2184   04.1 1409 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     142 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     142 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        55       2.0  142   04.1  191 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2150 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2150 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2150 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2150 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2150 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2150 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B2PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Build 2 PM                        33   1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2284 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2284 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        67       2.0 2284   04.1 1117 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2172 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1465 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1465 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        56       2.0 1465   04.1 1100 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1487 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2140 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2140 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2140 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2098 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2098 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 2098   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      42 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      42 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   42   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2479 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2479 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2479 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2654 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2470 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2470 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        61       2.0 2470   04.1 1414 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     184 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     184 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51       2.0  184   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2405 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2405 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2405 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2405 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2405 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2405 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B3AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Build 3 AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1555 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1555 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.   48   4
       101        67       2.0 1555   04.1 1111 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1559 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1904 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1904 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.   48   4
       101        54       2.0 1904   04.1 1104 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2050 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2016 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2016 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2016 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1911 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1911 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       101        69       2.0 1911   04.1 1424 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     105 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     105 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       101        88       2.0  105   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2084 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2084 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2084 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2342 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2195 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2195 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       101        68       2.0 2195   04.1 1406 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     147 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     147 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       101        57       2.0  147   04.1  197 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2124 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2124 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2124 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2124 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2124 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2124 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B3PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Build 3 PM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2253 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2253 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48    4
       100        68       2.0 2253   04.1 1121 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2174 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1458 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1458 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48    4
       100        56       2.0 1458   04.1 1101 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1491 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2233 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2233 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2233 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2192 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2192 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 2192   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      41 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      41 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92       2.0   41   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2555 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2555 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2555 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2623 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2428 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2428 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        60       2.0 2428   04.1 1411 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     195 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     195 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        50       2.0  195   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2347 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2347 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B4AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Build 4 AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1578 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1578 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        62       2.0 1578   04.1 1106 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1606 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1912 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1912 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        50       2.0 1912   04.1 1101 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2025 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2060 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2060 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2060 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1957 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1957 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 1957   04.1 1422 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.     103 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.     103 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        90       2.0  103   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2099 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2099 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2099 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2294 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2148 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2148 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        68       2.0 2148   04.1 1409 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     146 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     146 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        60       2.0  146   04.1  202 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2114 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2114 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2114 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2114 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2114 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2114 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B4PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Build 4 PM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2244 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2244 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        67       2.0 2244   04.1 1116 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2159 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1464 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1464 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        56       2.0 1464   04.1 1101 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1507 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2251 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2251 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2251 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2208 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2208 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68        2.0 2208   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      43 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      43 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        92        2.0   43   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2548 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2548 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2548 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2648 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2466 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2466 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        61        2.0 2466   04.1 1413 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     182 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     182 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51        2.0  182   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2393 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2393 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2393 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2393 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2393 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2393 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B5AM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Build 5 AM                        33  1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    1549 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    1549 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        66       2.0 1549   04.1 1111 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    1559 0.9  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1904 0.9  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1904 0.9  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        54       2.0 1904   04.1 1106 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    2022 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2042 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2042 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2042 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    1944 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    1944 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        69       2.0 1944   04.1 1424 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      98 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      98 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        88       2.0   98   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2105 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2105 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2105 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2303 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2153 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2153 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        66       2.0 2153   04.1 1408 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     150 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     150 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        54       2.0  150   04.1  190 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2112 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2112 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2112 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2112 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2112 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2112 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

```
Site 5 Olymp & La Brea (S5B5PM.DAT)     60.0321.0.0000.000280.30480000    1
1
SE MID S                  873.      736.       5.0
SE 164 S                  771.      827.       5.0
SE 82 S                   719.      893.       5.0
SE CNR                    695.      985.       5.0
SE 82 E                   784.      990.       5.0
SE 164 E                  866.      989.       5.0
SE MID E                  986.      986.       5.0
NE MID E                  977.     1089.       5.0
NE 164 E                  844.     1094.       5.0
NE 82 E                   762.     1096.       5.0
NE CNR                    680.     1105.       5.0
NE 82 N                   683.     1199.       5.0
NE 164 N                  707.     1278.       5.0
NE MID N                  748.     1407.       5.0
NW MID N                  646.     1421.       5.0
NW 164 N                  592.     1268.       5.0
NW 82 N                   569.     1188.       5.0
NW CNR                    550.     1110.       5.0
NW 82 W                   462.     1106.       5.0
NW 164 W                  380.     1107.       5.0
NW MID W                  226.     1111.       5.0
SW MID W                  220.     1007.       5.0
SW 164 W                  395.     1000.       5.0
SW 82 W                   478.      998.       5.0
SW CNR                    560.      994.       5.0
SW 82 S                   594.      911.       5.0
SW 164 S                  626.      834.       5.0
SW MID S                  709.      731.       5.0
Site 5 Build 5 PM                        33   1   0
  1
EB        Oly AP    AG   354.  1033.  -378.  1053.    2222 0.8  0.  56   30.
  1
EB        Oly AP    AG   353.  1037.   623.  1030.    2222 0.8  0.  68   30.
  2
EB        Oly AP Q  AG   544.  1032.   368.  1037.      0.  48   4
       100        67       2.0 2222   04.1 1117 1 3
  1
EB        Oly DP    AG   624.  1024.  1617.  1000.    2166 0.8  0.  56   30.
  1
WB        Oly AP    AG   891.  1065.  1622.  1047.    1455 0.8  0.  56   30.
  1
WB        Oly AP    AG   890.  1060.   630.  1066.    1455 0.8  0.  68   30.
  2
WB        Oly AP Q  AG   695.  1064.   862.  1060.      0.  48   4
       100        56       2.0 1455   04.1 1101 1 3
  1
WB        Oly DP    AG   628.  1073.  -378.  1100.    1515 0.8  0.  56   30.
  1
NB        Brea AP   AG  1230.   261.  1042.   547.    2226 0.8  0.  56   30.
  1
NB        Brea AP   AG  1042.   547.   981.   616.    2226 0.8  0.  56   30.
  1
NB        Brea AP   AG   981.   616.   795.   761.    2226 0.8  0.  56   30.
  1
```

```
NB        Brea T+R  AG   795.   760.   706.   856.    2196 0.8  0.  56   30.
  1
NB        Brea T+R  AG   706.   856.   653.   980.    2196 0.8  0.  56   30.
  2
NB        Brea T+R QAG   657.   972.   703.   863.      0.  36   3
       100        68       2.0 2196   04.1 1423 1 3
  1
NB        Brea LT   AG   777.   742.   686.   845.      30 0.8  0.  32   30.
  1
NB        Brea LT   AG   686.   845.   625.   981.      30 0.8  0.  32   30.
  2
NB        Brea LT Q AG   628.   973.   681.   855.      0.  12   1
       100        93       2.0   30   04.1 1490 1 3
  1
NB        Brea DP   AG   653.   978.   638.  1130.    2530 0.8  0.  56   30.
  1
NB        Brea DP   AG   638.  1130.   658.  1238.    2530 0.8  0.  56   30.
  1
NB        Brea DP   AG   658.  1238.   933.  2002.    2530 0.8  0.  56   30.
  1
SB        Brea AP   AG   644.  1336.   884.  2016.    2640 0.8  0.  56   30.
  1
SB        Brea T+R  AG   644.  1337.   606.  1228.    2446 0.8  0.  56   30.
  1
SB        Brea T+R  AG   606.  1228.   588.  1103.    2446 0.8  0.  56   30.
  2
SB        Brea T+R QAG   590.  1120.   605.  1224.      0.  36   3
       100        60       2.0 2446   04.1 1410 1 3
  1
SB        Brea LT   AG   665.  1326.   629.  1221.     194 0.8  0.  32   30.
  1
SB        Brea LT   AG   629.  1221.   612.  1105.     194 0.8  0.  32   30.
  2
SB        Brea LT Q AG   614.  1118.   629.  1219.      0.  12   1
       100        51       2.0  194   04.1  176 1 3
  1
SB        Brea DP   AG   588.  1102.   600.   989.    2332 0.8  0.  56   30.
  1
SB        Brea DP   AG   600.   989.   650.   854.    2332 0.8  0.  56   30.
  1
SB        Brea DP   AG   650.   854.   723.   758.    2332 0.8  0.  56   30.
  1
SB        Brea DP   AG   723.   758.   938.   583.    2332 0.8  0.  56   30.
  1
SB        Brea DP   AG   938.   583.  1029.   479.    2332 0.8  0.  56   30.
  1
SB        Brea DP   AG  1029.   479.  1184.   227.    2332 0.8  0.  56   30.
1.0   04 1000.   0Y  5  0 72
```

Site 5 – La Brea & Olympic
Output Files

```
1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5EXAM.DAT)                  RUN: Site 5 Existing AM
      DATE: 03/19/2010   TIME: 10:04:28.84


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1         Y1       X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   1183.   3.3    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   1183.   3.3    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0     415.4    1035.7 *     129.   272. AG    143. 100.0    .0 48.0  .86   6.5
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   1220.   3.9    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   1542.   3.9    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   1542.   3.9    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0     824.0    1060.9 *     129.    91. AG    119. 100.0    .0 48.0  .83   6.6
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   1679.   3.3    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   1463.   3.3    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   1463.   3.3    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   1463.   3.3    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   1346.   3.3    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   1346.   3.3    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0     955.7     264.3 *     768.   157. AG    112. 100.0    .0 36.0 1.13  39.0
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG    117.   3.3    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG    117.   3.3    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     655.6     911.6 *      67.   156. AG     47. 100.0    .0 12.0  .79   3.4
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   1452.   3.3    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   1452.   3.3    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   1452.   3.3    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   1655.   3.3    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   1536.   3.3    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   1536.   3.3    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0     824.2    2743.7 *    1640.     8. AG    114. 100.0    .0 36.0 1.35  83.3
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    119.   3.3    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    119.   3.3    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     687.0    1609.7 *     497.     8. AG     32. 100.0    .0 12.0 1.51  25.3
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   1492.   3.3    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   1492.   3.3    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   1492.   3.3    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   1492.   3.3    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   1492.   3.3    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   1492.   3.3    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5EXAM.DAT)                  RUN: Site 5 Existing AM
      DATE: 03/19/2010   TIME: 10:04:28.84

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       65       2.0      1183       1108      20.50      1        3
       7. WB        Oly AP Q  *     100       54       2.0      1542       1103      20.50      1        3
      14. NB        Brea T+R Q*     100       68       2.0      1346       1423      20.50      1        3
      17. NB        Brea LT Q *     100       86       2.0       117       1490      20.50      1        3
      24. SB        Brea T+R Q*     100       69       2.0      1536       1403      20.50      1        3
      27. SB        Brea LT Q *     100       58       2.0       119        208      20.50      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0       5.0    *
      2. SE 164 S             *       771.0      827.0       5.0    *
      3. SE 82 S              *       719.0      893.0       5.0    *
      4. SE CNR               *       695.0      985.0       5.0    *
      5. SE 82 E              *       784.0      990.0       5.0    *
      6. SE 164 E             *       866.0      989.0       5.0    *
      7. SE MID E             *       986.0      986.0       5.0    *
      8. NE MID E             *       977.0     1089.0       5.0    *
      9. NE 164 E             *       844.0     1094.0       5.0    *
     10. NE 82 E              *       762.0     1096.0       5.0    *
     11. NE CNR               *       680.0     1105.0       5.0    *
     12. NE 82 N              *       683.0     1199.0       5.0    *
     13. NE 164 N             *       707.0     1278.0       5.0    *
     14. NE MID N             *       748.0     1407.0       5.0    *
     15. NW MID N             *       646.0     1421.0       5.0    *
     16. NW 164 N             *       592.0     1268.0       5.0    *
     17. NW 82 N              *       569.0     1188.0       5.0    *
     18. NW CNR               *       550.0     1110.0       5.0    *
     19. NW 82 W              *       462.0     1106.0       5.0    *
     20. NW 164 W             *       380.0     1107.0       5.0    *
     21. NW MID W             *       226.0     1111.0       5.0    *
     22. SW MID W             *       220.0     1007.0       5.0    *
     23. SW 164 W             *       395.0     1000.0       5.0    *
     24. SW 82 W              *       478.0      998.0       5.0    *
     25. SW CNR               *       560.0      994.0       5.0    *
     26. SW 82 S              *       594.0      911.0       5.0    *
     27. SW 164 S             *       626.0      834.0       5.0    *
     28. SW MID S             *       709.0      731.0       5.0    *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5EXAM.DAT)                  RUN: Site 5 Existing AM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .3    .4    .5    .6    .4    .3    .0    .1    .3    .5    .6    .5    .4   1.0    .4    .2    .2    .0    .0
   5.  *    .0    .2    .4    .5    .6    .3    .3    .0    .0    .2    .4    .5    .4    .5   1.0    .7    .3    .2    .1    .0
  10.  *    .0    .1    .4    .5    .4    .2    .2    .0    .0    .0    .3    .4    .4    .4   1.1    .8    .7    .4    .1    .1
  15.  *    .0    .0    .3    .4    .4    .2    .2    .0    .0    .0    .2    .4    .4    .3   1.0    .9    .7    .6    .1    .1
  20.  *    .0    .0    .3    .4    .4    .3    .2    .0    .0    .0    .1    .2    .3    .3   1.0   1.0    .9    .7    .2    .1
  25.  *    .0    .0    .3    .4    .3    .2    .2    .0    .0    .0    .0    .1    .1    .2    .9   1.1    .9    .7    .3    .1
  30.  *    .0    .0    .3    .4    .3    .2    .2    .0    .0    .0    .0    .1    .1    .1    .8   1.0   1.0    .7    .3    .1
  35.  *    .0    .0    .3    .4    .4    .3    .3    .0    .0    .0    .0    .0    .1    .1    .7   1.1    .9    .5    .4    .1
  40.  *    .0    .0    .1    .4    .4    .3    .3    .0    .0    .0    .0    .0    .0    .1    .7   1.0    .8    .7    .3    .1
  45.  *    .0    .0    .1    .5    .3    .3    .3    .0    .0    .0    .0    .0    .0    .0    .6   1.0    .7    .6    .2    .1
  50.  *    .0    .1    .1    .5    .3    .3    .3    .0    .0    .0    .0    .0    .0    .0    .5   1.0    .7    .6    .1    .1
  55.  *    .0    .2    .2    .4    .4    .3    .3    .0    .0    .0    .0    .0    .0    .0    .5    .9    .7    .4    .1    .1
  60.  *    .0    .2    .2    .4    .4    .3    .3    .0    .0    .0    .0    .0    .0    .0    .5    .8    .5    .4    .2    .1
  65.  *    .0    .0    .2    .4    .4    .3    .3    .1    .0    .0    .0    .0    .0    .0    .5    .7    .5    .4    .2    .1
  70.  *    .0    .0    .2    .5    .3    .3    .3    .1    .0    .0    .0    .0    .0    .0    .5    .7    .5    .4    .2    .2
  75.  *    .0    .0    .2    .4    .3    .3    .3    .1    .1    .1    .0    .0    .0    .0    .5    .7    .5    .2    .3    .2
  80.  *    .0    .0    .1    .3    .3    .3    .3    .2    .2    .2    .1    .0    .0    .0    .4    .7    .5    .2    .2    .2
  85.  *    .0    .0    .0    .3    .3    .3    .3    .2    .2    .2    .3    .0    .0    .0    .4    .7    .6    .4    .2    .1
  90.  *    .0    .0    .0    .3    .3    .3    .3    .3    .3    .4    .3    .0    .0    .0    .4    .7    .6    .6    .4    .2
  95.  *    .0    .0    .0    .1    .3    .2    .2    .4    .4    .5    .4    .0    .0    .0    .4    .7    .6    .8    .5    .3
 100.  *    .0    .0    .0    .1    .1    .1    .1    .4    .4    .5    .6    .1    .0    .0    .4    .7    .7    .7    .5    .4
 105.  *    .0    .0    .0    .1    .1    .1    .1    .4    .4    .6    .6    .1    .0    .0    .4    .7    .7    .7    .5    .6
 110.  *    .0    .0    .0    .0    .1    .1    .1    .4    .4    .6    .7    .1    .0    .0    .4    .7    .9    .6    .5    .5
 115.  *    .1    .0    .0    .0    .0    .0    .0    .4    .3    .6    .6    .2    .1    .0    .4    .6    .8    .6    .6    .5
 120.  *    .1    .0    .0    .0    .0    .0    .0    .4    .3    .6    .6    .1    .1    .0    .4    .7    .8    .6    .5    .6
 125.  *    .1    .1    .0    .0    .0    .0    .0    .4    .3    .6    .6    .2    .1    .0    .5    .7    .9    .6    .5    .6
 130.  *    .2    .2    .0    .0    .0    .0    .0    .3    .3    .6    .6    .3    .0    .0    .5    .7    .8    .6    .5    .6
 135.  *    .2    .2    .3    .0    .0    .0    .0    .3    .4    .6    .6    .3    .0    .0    .5    .8    .9    .6    .6    .6
 140.  *    .2    .2    .3    .0    .0    .0    .0    .3    .3    .6    .6    .3    .0    .0    .5    .9    .9    .5    .6    .6
 145.  *    .2    .4    .5    .1    .0    .0    .0    .3    .3    .6    .5    .3    .0    .0    .5   1.1    .8    .6    .6    .6
 150.  *    .2    .4    .4    .1    .0    .0    .0    .3    .3    .6    .6    .2    .0    .0    .5   1.2    .7    .6    .6    .4
 155.  *    .3    .4    .6    .2    .0    .0    .0    .3    .3    .6    .6    .3    .1    .0    .5   1.0    .7    .6    .6    .4
 160.  *    .3    .5    .7    .4    .1    .0    .0    .3    .3    .7    .6    .3    .3    .0    .6    .9    .9    .6    .6    .4
 165.  *    .4    .5    .8    .4    .1    .0    .0    .3    .3    .7    .6    .3    .3    .0    .8    .9    .6    .5    .6    .4
 170.  *    .4    .5    .8    .4    .1    .1    .0    .3    .4    .7    .6    .3    .3    .1    .8    .8    .6    .5    .6    .3
 175.  *    .4    .5    .7    .5    .1    .1    .0    .3    .4    .7    .7    .3    .3    .1   1.0    .8    .6    .5    .6    .3
 180.  *    .4    .5    .8    .5    .1    .1    .0    .3    .4    .7    .6    .4    .3    .1   1.1    .7    .4    .4    .6    .3
 185.  *    .5    .5    .8    .4    .1    .1    .0    .3    .4    .7    .5    .4    .1    .2   1.0    .6    .4    .4    .5    .3
 190.  *    .5    .5    .7    .4    .1    .1    .1    .4    .4    .7    .5    .4    .1    .1   1.1    .6    .3    .5    .5    .3
 195.  *    .4    .5    .7    .4    .1    .1    .1    .4    .5    .7    .5    .3    .1    .1   1.0    .6    .3    .5    .5    .3
 200.  *    .4    .5    .7    .5    .1    .1    .1    .4    .5    .7    .5    .2    .2    .2   1.0    .5    .2    .5    .5    .2
 205.  *    .4    .5    .7    .5    .1    .1    .1    .4    .5    .7    .4    .2    .2    .3    .8    .6    .2    .5    .5    .2
1
                                                                                                                 PAGE  4
      JOB: Site 5 Olymp & La Brea (S5EXAM.DAT)                 RUN: Site 5 Existing AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .4    .4    .6    .5    .1    .1    .1    .4    .6    .7    .4    .2    .3    .3    .8    .3    .2    .5    .5    .3
 215.  *    .4    .3    .6    .5    .1    .1    .1    .4    .6    .7    .2    .3    .3    .3    .7    .3    .2    .5    .4    .3
 220.  *    .4    .4    .5    .5    .1    .1    .1    .4    .6    .7    .3    .4    .5    .3    .6    .2    .2    .5    .4    .3
 225.  *    .4    .4    .5    .4    .1    .1    .1    .4    .7    .6    .3    .5    .6    .3    .6    .1    .2    .5    .4    .3
 230.  *    .3    .4    .5    .4    .2    .1    .1    .4    .7    .6    .6    .6    .5    .3    .5    .1    .2    .5    .4    .3
 235.  *    .3    .4    .5    .4    .2    .1    .1    .4    .6    .7    .6    .6    .6    .4    .5    .1    .1    .5    .3    .3
 240.  *    .3    .4    .4    .4    .2    .1    .1    .4    .6    .7    .6    .6    .4    .4    .4    .1    .1    .5    .2    .3
 245.  *    .3    .4    .5    .4    .2    .1    .1    .4    .6    .7    .6    .5    .5    .4    .4    .1    .1    .4    .4    .4
 250.  *    .4    .4    .5    .3    .1    .1    .1    .5    .6    .7    .6    .5    .5    .4    .4    .1    .1    .4    .4    .4
 255.  *    .4    .4    .5    .4    .1    .2    .2    .5    .7    .7    .7    .5    .4    .4    .4    .0    .1    .4    .4    .4
 260.  *    .4    .4    .5    .4    .2    .2    .1    .5    .6    .7    .7    .5    .4    .4    .4    .0    .1    .4    .4    .4
 265.  *    .4    .4    .5    .5    .2    .1    .1    .6    .5    .6    .5    .5    .4    .3    .4    .0    .1    .2    .4    .4
 270.  *    .4    .4    .5    .4    .3    .2    .2    .5    .5    .5    .3    .4    .4    .3    .4    .0    .0    .2    .3    .3
 275.  *    .4    .4    .5    .4    .3    .3    .5    .3    .4    .3    .4    .4    .4    .3    .4    .0    .0    .2    .2    .2
 280.  *    .4    .4    .6    .6    .4    .5    .5    .2    .3    .3    .4    .5    .4    .4    .4    .0    .0    .1    .2    .2
 285.  *    .4    .3    .8    .6    .5    .5    .4    .1    .3    .3    .4    .5    .4    .4    .4    .0    .0    .1    .1    .1
 290.  *    .3    .4    .9    .6    .5    .5    .4    .2    .2    .2    .3    .3    .4    .4    .4    .0    .0    .0    .1    .1
 295.  *    .3    .6    .9    .6    .6    .4    .4    .1    .1    .1    .3    .4    .4    .4    .4    .0    .0    .0    .1    .1
 300.  *    .3    .7    .9    .6    .6    .5    .4    .1    .1    .1    .4    .4    .4    .4    .4    .0    .0    .0    .0    .0
 305.  *    .3    .6    .9    .4    .4    .6    .5    .1    .1    .1    .5    .4    .4    .3    .4    .0    .0    .0    .0    .0
 310.  *    .3    .4    .9    .4    .5    .6    .5    .1    .1    .1    .5    .4    .4    .3    .4    .0    .0    .0    .0    .0
 315.  *    .2    .4    .7    .5    .6    .6    .4    .1    .1    .1    .5    .4    .4    .3    .4    .0    .0    .0    .0    .0
 320.  *    .2    .4    .5    .5    .6    .5    .4    .1    .1    .1    .4    .5    .4    .4    .5    .0    .0    .0    .0    .0
 325.  *    .1    .4    .6    .4    .6    .5    .4    .1    .1    .1    .4    .5    .5    .5    .5    .0    .0    .0    .0    .0
 330.  *    .1    .3    .5    .4    .5    .5    .4    .1    .1    .1    .3    .5    .5    .5    .5    .0    .0    .0    .0    .0
 335.  *    .1    .2    .5    .4    .5    .4    .3    .1    .1    .1    .3    .5    .5    .5    .6    .1    .0    .0    .0    .0
 340.  *    .1    .1    .5    .4    .5    .4    .3    .1    .1    .2    .3    .5    .5    .5    .6    .1    .0    .0    .0    .0
 345.  *    .1    .2    .6    .5    .5    .3    .3    .1    .1    .2    .3    .6    .5    .5    .7    .1    .0    .0    .0    .0
 350.  *    .1    .2    .6    .6    .5    .3    .3    .1    .1    .3    .4    .5    .5    .5    .8    .2    .1    .0    .0    .0
 355.  *    .1    .3    .4    .5    .6    .4    .3    .0    .1    .3    .5    .5    .5    .5    .9    .3    .1    .1    .0    .0
 360.  *    .0    .3    .4    .5    .6    .4    .3    .0    .1    .3    .5    .6    .5    .4   1.0    .4    .2    .2    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .5    .7    .9    .6    .6    .6    .5    .6    .7    .7    .7    .6    .6    .5   1.1   1.2   1.0    .8    .6    .6
 DEGR. *  185   300   290   280     0   305   275   265   225   160   110     0   225     5    10   150    30    95   115   105

1
                                                                                                                 PAGE  5
      JOB: Site 5 Olymp & La Brea (S5EXAM.DAT)                 RUN: Site 5 Existing AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
```

```
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .2    .2    .7    .5    .4    .3    .5
   5.  *    .0    .2    .2    .7    .6    .4    .4    .6
  10.  *    .0    .2    .4    .7    .7    .5    .4    .6
  15.  *    .0    .2    .4    .8    .7    .4    .5    .5
  20.  *    .0    .3    .4    .8    .7    .3    .3    .6
  25.  *    .1    .3    .5    .8    .5    .4    .4    .6
  30.  *    .1    .3    .5    .8    .4    .5    .5    .6
  35.  *    .1    .3    .5    .7    .5    .5    .5    .6
  40.  *    .1    .3    .6    .7    .4    .5    .4    .5
  45.  *    .1    .3    .6    .7    .4    .6    .5    .4
  50.  *    .1    .3    .6    .7    .4    .7    .6    .5
  55.  *    .1    .3    .6    .6    .6    .7    .6    .4
  60.  *    .1    .3    .6    .6    .6    .7    .6    .4
  65.  *    .1    .2    .6    .7    .6    .6    .5    .3
  70.  *    .2    .3    .6    .7    .6    .7    .3    .3
  75.  *    .2    .3    .5    .7    .6    .7    .3    .4
  80.  *    .1    .4    .5    .7    .7    .5    .3    .6
  85.  *    .2    .4    .4    .5    .7    .5    .4    .6
  90.  *    .2    .2    .4    .3    .4    .4    .4    .5
  95.  *    .3    .2    .3    .3    .4    .4    .5    .6
 100.  *    .4    .1    .3    .3    .4    .4    .5    .6
 105.  *    .4    .0    .1    .1    .3    .4    .5    .6
 110.  *    .5    .1    .1    .2    .3    .5    .5    .6
 115.  *    .4    .1    .1    .2    .3    .4    .6    .6
 120.  *    .4    .1    .1    .2    .4    .4    .5    .5
 125.  *    .4    .1    .1    .2    .4    .4    .5    .5
 130.  *    .4    .0    .1    .1    .4    .4    .5    .5
 135.  *    .4    .0    .1    .1    .3    .4    .4    .4
 140.  *    .3    .0    .1    .1    .3    .4    .4    .4
 145.  *    .3    .0    .1    .1    .3    .4    .3    .4
 150.  *    .3    .0    .0    .1    .3    .3    .2    .2
 155.  *    .3    .0    .0    .0    .2    .2    .1    .2
 160.  *    .3    .0    .0    .0    .2    .2    .1    .1
 165.  *    .3    .0    .0    .0    .1    .0    .0    .1
 170.  *    .3    .0    .0    .0    .0    .0    .0    .1
 175.  *    .3    .0    .0    .0    .0    .0    .0    .0
 180.  *    .3    .0    .0    .0    .0    .0    .0    .0
 185.  *    .3    .0    .0    .0    .0    .0    .0    .0
 190.  *    .3    .0    .0    .0    .0    .0    .0    .0
 195.  *    .3    .0    .0    .0    .0    .0    .0    .0
 200.  *    .3    .0    .0    .0    .0    .0    .0    .0
 205.  *    .3    .0    .0    .0    .0    .0    .0    .0
1                                                                                                                          PAGE  6
      JOB: Site 5 Olymp & La Brea (S5EXAM.DAT)                  RUN: Site 5 Existing AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .3    .0    .0    .0    .0    .0    .0    .0
 215.  *    .3    .0    .0    .0    .0    .0    .0    .0
 220.  *    .3    .0    .0    .0    .0    .0    .0    .0
 225.  *    .3    .0    .0    .0    .0    .0    .0    .0
 230.  *    .3    .0    .0    .0    .0    .0    .0    .0
 235.  *    .3    .0    .0    .0    .0    .0    .0    .0
 240.  *    .3    .0    .0    .0    .0    .0    .0    .0
 245.  *    .4    .0    .0    .0    .0    .0    .0    .0
 250.  *    .4    .0    .0    .0    .0    .0    .0    .0
 255.  *    .4    .1    .0    .0    .0    .0    .0    .0
 260.  *    .4    .1    .1    .0    .1    .0    .0    .0
 265.  *    .4    .1    .1    .2    .2    .0    .0    .0
 270.  *    .3    .1    .2    .4    .3    .0    .0    .0
 275.  *    .2    .3    .2    .4    .5    .0    .0    .0
 280.  *    .2    .3    .3    .4    .6    .0    .0    .0
 285.  *    .1    .3    .3    .5    .5    .1    .0    .0
 290.  *    .1    .3    .3    .5    .5    .1    .0    .0
 295.  *    .1    .3    .3    .5    .6    .2    .0    .0
 300.  *    .0    .3    .3    .5    .6    .2    .1    .0
 305.  *    .0    .3    .3    .5    .6    .2    .1    .0
 310.  *    .0    .3    .3    .6    .6    .3    .2    .1
 315.  *    .0    .2    .3    .6    .5    .3    .1    .1
 320.  *    .0    .2    .2    .6    .5    .3    .1    .1
 325.  *    .0    .2    .2    .6    .5    .3    .1    .1
 330.  *    .0    .2    .2    .6    .4    .3    .2    .2
 335.  *    .0    .2    .2    .6    .4    .3    .2    .2
 340.  *    .0    .2    .2    .6    .4    .4    .2    .4
 345.  *    .0    .2    .2    .6    .3    .6    .2    .5
 350.  *    .0    .2    .2    .6    .4    .5    .3    .5
 355.  *    .0    .2    .2    .6    .4    .4    .3    .4
 360.  *    .0    .2    .2    .7    .5    .4    .3    .5
 ------*------------------------------------------------
 MAX   *    .5    .4    .6    .8    .7    .7    .6    .6
 DEGR. *  110    80    40    15    10    50    50     5

 THE HIGHEST CONCENTRATION IS    1.20 PPM AT  150 DEGREES FROM REC16.
 THE 2ND HIGHEST CONCENTRATION IS    1.10 PPM AT   10 DEGREES FROM REC15.
 THE 3RD HIGHEST CONCENTRATION IS    1.00 PPM AT   30 DEGREES FROM REC17.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5EXPM.DAT)                 RUN: Site 5 Existing PM
      DATE: 03/19/2010   TIME: 10:21:35.12


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)        (VEH)
      ------------------------*--------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG  1745.   3.3    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG  1745.   3.3    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0    -500.7    1061.7 *    1045.   272. AG   143. 100.0    .0 48.0 1.22  53.1
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG  1744.   3.3    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG  1171.   3.3    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG  1171.   3.3    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0     781.2    1061.9 *      86.    91. AG   119. 100.0    .0 48.0  .64   4.4
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG  1167.   3.3    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG  1547.   3.3    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG  1547.   3.3    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG  1547.   3.3    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG  1494.   3.3    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG  1494.   3.3    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    1159.0    -217.5 *    1291.   157. AG   112. 100.0    .0 36.0 1.25  65.6
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG    53.   3.3    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG    53.   3.3    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     639.5     947.4 *      28.   156. AG    49. 100.0    .0 12.0  .60   1.4
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG  1699.   3.3    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG  1699.   3.3    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG  1699.   3.3    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG  1845.   3.3    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG  1705.   3.3    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG  1705.   3.3    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0     821.8    2727.1 *    1624.     8. AG   107. 100.0    .0 36.0 1.30  82.5
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG   140.   3.3    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG   140.   3.3    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     722.5    1848.9 *     739.     8. AG    29. 100.0    .0 12.0 1.82  37.5
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG  1698.   3.3    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG  1698.   3.3    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG  1698.   3.3    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG  1698.   3.3    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG  1698.   3.3    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG  1698.   3.3    .0 56.0
1
                                                                                                                PAGE  2
      JOB: Site 5 Olymp & La Brea (S5EXPM.DAT)                 RUN: Site 5 Existing PM
      DATE: 03/19/2010   TIME: 10:21:35.12

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*----------------------------------------------------------------------------------

       3. EB        Oly AP Q  *     100       65       2.0      1745       1154      20.50      1        3
       7. WB        Oly AP Q  *     100       54       2.0      1171       1094      20.50      1        3
      14. NB        Brea T+R Q*     100       68       2.0      1494       1422      20.50      1        3
      17. NB        Brea LT Q *     100       90       2.0        53       1490      20.50      1        3
      24. SB        Brea T+R Q*     100       65       2.0      1705       1411      20.50      1        3
      27. SB        Brea LT Q *     100       53       2.0       140        180      20.50      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)         *
         RECEPTOR             *      X          Y          Z      *
     -------------------------*-----------------------------------*
      1. SE MID S             *       873.0      736.0       5.0   *
      2. SE 164 S             *       771.0      827.0       5.0   *
      3. SE 82 S              *       719.0      893.0       5.0   *
      4. SE CNR               *       695.0      985.0       5.0   *
      5. SE 82 E              *       784.0      990.0       5.0   *
      6. SE 164 E             *       866.0      989.0       5.0   *
      7. SE MID E             *       986.0      986.0       5.0   *
      8. NE MID E             *       977.0     1089.0       5.0   *
      9. NE 164 E             *       844.0     1094.0       5.0   *
     10. NE 82 E              *       762.0     1096.0       5.0   *
     11. NE CNR               *       680.0     1105.0       5.0   *
     12. NE 82 N              *       683.0     1199.0       5.0   *
     13. NE 164 N             *       707.0     1278.0       5.0   *
     14. NE MID N             *       748.0     1407.0       5.0   *
     15. NW MID N             *       646.0     1421.0       5.0   *
     16. NW 164 N             *       592.0     1268.0       5.0   *
     17. NW 82 N              *       569.0     1188.0       5.0   *
     18. NW CNR               *       550.0     1110.0       5.0   *
     19. NW 82 W              *       462.0     1106.0       5.0   *
     20. NW 164 W             *       380.0     1107.0       5.0   *
     21. NW MID W             *       226.0     1111.0       5.0   *
     22. SW MID W             *       220.0     1007.0       5.0   *
     23. SW 164 W             *       395.0     1000.0       5.0   *
     24. SW 82 W              *       478.0      998.0       5.0   *
     25. SW CNR               *       560.0      994.0       5.0   *
     26. SW 82 S              *       594.0      911.0       5.0   *
     27. SW 164 S             *       626.0      834.0       5.0   *
     28. SW MID S             *       709.0      731.0       5.0   *
1
                                                                                                                PAGE  3
      JOB: Site 5 Olymp & La Brea (S5EXPM.DAT)                 RUN: Site 5 Existing PM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
   0.  *   .0    .2    .3    .6    .6    .3    .3    .0    .1    .3    .5    .6    .6    .5   1.0    .5    .2    .2    .0    .0
   5.  *   .0    .2    .3    .6    .5    .3    .3    .0    .0    .2    .4    .6    .5    .5   1.0    .7    .4    .3    .1    .0
  10.  *   .0    .1    .3    .6    .4    .3    .3    .0    .0    .1    .3    .4    .5    .5   1.0    .8    .7    .5    .1    .0
  15.  *   .0    .1    .2    .5    .3    .2    .3    .0    .0    .0    .3    .4    .4    .4    .9    .8    .8    .6    .1    .1
  20.  *   .0    .1    .2    .5    .3    .2    .3    .0    .0    .0    .1    .3    .3    .3   1.0   1.2    .8    .7    .1    .1
  25.  *   .0    .1    .1    .5    .3    .2    .3    .0    .0    .0    .1    .1    .2    .2    .9   1.2    .9    .8    .3    .1
  30.  *   .0    .1    .1    .5    .3    .3    .3    .0    .0    .0    .0    .1    .1    .1    .8   1.2    .8    .7    .4    .1
  35.  *   .0    .1    .1    .5    .3    .3    .3    .0    .0    .0    .0    .0    .1    .1    .7   1.0    .8    .6    .3    .1
  40.  *   .0    .1    .1    .5    .3    .3    .3    .0    .0    .0    .0    .0    .0    .1    .7   1.0    .7    .7    .2    .1
  45.  *   .0    .1    .1    .4    .3    .3    .3    .0    .0    .0    .0    .0    .0    .0    .6   1.0    .7    .7    .2    .1
  50.  *   .0    .1    .1    .4    .3    .3    .3    .0    .0    .0    .0    .0    .0    .0    .6   1.0    .7    .6    .2    .1
  55.  *   .0    .1    .1    .4    .3    .3    .3    .0    .0    .0    .0    .0    .0    .0    .6    .7    .6    .5    .2    .1
  60.  *   .0    .1    .1    .4    .2    .3    .3    .0    .0    .0    .0    .0    .0    .0    .5    .7    .7    .5    .2    .1
  65.  *   .0    .1    .1    .3    .4    .4    .4    .0    .0    .0    .0    .0    .0    .0    .5    .7    .6    .5    .2    .1
  70.  *   .0    .1    .1    .2    .4    .4    .4    .1    .0    .0    .0    .0    .0    .0    .5    .7    .6    .4    .2    .1
  75.  *   .0    .0    .1    .2    .4    .4    .4    .1    .0    .0    .0    .0    .0    .0    .4    .7    .6    .3    .2    .2
  80.  *   .0    .0    .1    .3    .4    .4    .4    .1    .1    .1    .0    .0    .0    .0    .4    .7    .6    .3    .3    .2
  85.  *   .0    .0    .1    .2    .4    .4    .4    .1    .1    .2    .1    .0    .0    .0    .4    .7    .6    .3    .2    .1
  90.  *   .0    .0    .0    .2    .3    .3    .2    .3    .3    .3    .3    .0    .0    .0    .4    .7    .6    .5    .2    .2
  95.  *   .0    .0    .0    .1    .2    .2    .2    .3    .3    .3    .4    .0    .0    .0    .4    .7    .6    .7    .2    .3
 100.  *   .0    .0    .0    .1    .2    .2    .2    .3    .3    .3    .4    .0    .0    .0    .4    .7    .6    .7    .2    .5
 105.  *   .0    .0    .0    .1    .1    .1    .1    .3    .3    .3    .4    .1    .0    .0    .4    .7    .7    .7    .4    .5
 110.  *   .1    .0    .0    .0    .1    .1    .1    .3    .3    .3    .4    .1    .0    .0    .4    .7    .7    .7    .5    .5
 115.  *   .1    .0    .0    .0    .0    .0    .0    .3    .3    .3    .4    .1    .0    .0    .4    .8    .7    .6    .6    .5
 120.  *   .1    .0    .0    .0    .0    .0    .0    .3    .3    .3    .4    .1    .0    .0    .4    .8    .8    .5    .7    .6
 125.  *   .1    .1    .0    .0    .0    .0    .0    .3    .3    .3    .5    .1    .0    .0    .5    .8    .8    .4    .5    .6
 130.  *   .2    .2    .0    .0    .0    .0    .0    .3    .2    .3    .5    .1    .0    .0    .5    .8   1.0    .6    .4    .7
 135.  *   .2    .2    .3    .0    .0    .0    .0    .2    .2    .3    .5    .1    .0    .0    .5    .8    .8    .6    .5    .6
 140.  *   .2    .2    .3    .1    .0    .0    .0    .2    .2    .3    .4    .2    .0    .0    .5    .7    .8    .6    .5    .6
 145.  *   .2    .4    .5    .1    .0    .0    .0    .2    .2    .4    .4    .2    .0    .0    .5    .8    .8    .7    .5    .6
 150.  *   .2    .4    .6    .2    .0    .0    .0    .2    .2    .4    .5    .2    .0    .0    .5   1.0    .7    .6    .5    .6
 155.  *   .4    .5    .7    .2    .1    .0    .0    .2    .2    .5    .5    .3    .0    .0    .5    .9    .9    .6    .5    .5
 160.  *   .4    .5    .7    .4    .1    .0    .0    .2    .2    .5    .6    .3    .1    .0    .7   1.0    .8    .5    .6    .5
 165.  *   .4    .6    .8    .4    .1    .1    .0    .2    .3    .6    .5    .3    .2    .1    .7   1.0    .7    .5    .5    .5
 170.  *   .5    .6    .8    .5    .1    .1    .0    .2    .3    .6    .5    .3    .2    .1    .8    .9    .6    .4    .5    .5
 175.  *   .5    .6    .9    .5    .2    .1    .1    .3    .3    .6    .6    .3    .2    .1   1.0    .8    .5    .4    .5    .5
 180.  *   .5    .6    .8    .5    .2    .1    .1    .3    .3    .6    .5    .4    .1    .2   1.1    .7    .5    .3    .5    .5
 185.  *   .5    .6    .8    .5    .2    .1    .1    .3    .3    .6    .4    .3    .1    .2   1.0    .6    .6    .3    .5    .5
 190.  *   .5    .6    .7    .4    .2    .1    .1    .3    .3    .6    .4    .3    .1    .2   1.1    .6    .4    .4    .5    .5
 195.  *   .5    .6    .7    .4    .1    .1    .1    .3    .3    .6    .5    .2    .1    .1   1.1    .6    .4    .4    .5    .5
 200.  *   .5    .5    .7    .5    .1    .1    .1    .3    .3    .6    .6    .2    .2    .2   1.0    .5    .3    .4    .5    .6
 205.  *   .5    .5    .7    .5    .1    .1    .1    .3    .3    .6    .5    .2    .2    .3   1.0    .4    .3    .4    .5    .5
1
                                                                                                                        PAGE  4
      JOB: Site 5 Olymp & La Brea (S5EXPM.DAT)                  RUN: Site 5 Existing PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-------------------------------------------------------------------------------------------------------------------------
 210.  *   .4    .4    .6    .5    .1    .1    .1    .3    .3    .6    .4    .2    .3    .3    .8    .3    .3    .4    .5    .5
 215.  *   .4    .5    .6    .5    .1    .1    .1    .3    .3    .6    .5    .5    .5    .4    .8    .2    .3    .4    .5    .5
 220.  *   .4    .5    .5    .5    .1    .1    .1    .3    .3    .6    .5    .5    .5    .5    .8    .2    .4    .4    .5    .5
 225.  *   .4    .5    .5    .4    .2    .1    .1    .3    .4    .5    .5    .6    .5    .5    .6    .1    .4    .5    .5    .5
 230.  *   .4    .5    .6    .4    .2    .1    .1    .3    .4    .6    .6    .7    .5    .6    .6    .1    .3    .5    .5    .5
 235.  *   .4    .5    .6    .4    .2    .1    .1    .3    .3    .6    .7    .7    .5    .5    .5    .1    .3    .5    .7    .6
 240.  *   .4    .5    .6    .4    .2    .1    .1    .2    .4    .7    .7    .7    .4    .5    .5    .1    .3    .5    .7    .6
 245.  *   .4    .4    .6    .4    .3    .1    .1    .2    .5    .8    .7    .7    .5    .5    .5    .1    .4    .6    .7    .6
 250.  *   .4    .4    .6    .3    .3    .1    .2    .3    .6    .6    .7    .7    .5    .5    .5    .1    .4    .7    .6    .6
 255.  *   .4    .4    .6    .5    .3    .2    .2    .4    .6    .8    .7    .8    .5    .5    .4    .1    .4    .7    .6    .6
 260.  *   .4    .5    .6    .5    .3    .3    .2    .5    .4    .8    .8    .6    .5    .4    .4    .1    .2    .6    .6    .6
 265.  *   .4    .5    .6    .7    .3    .2    .3    .5    .5    .7    .8    .6    .5    .4    .4    .1    .1    .5    .6    .6
 270.  *   .4    .5    .7    .6    .4    .3    .3    .3    .4    .6    .5    .6    .4    .4    .4    .0    .1    .4    .5    .5
 275.  *   .4    .6    .7    .8    .7    .3    .3    .3    .4    .5    .5    .5    .4    .4    .4    .0    .0    .2    .3    .3
 280.  *   .5    .6    .9    .8    .7    .4    .4    .2    .3    .4    .5    .5    .4    .4    .4    .0    .0    .2    .2    .2
 285.  *   .5    .6    .9    .7    .6    .4    .5    .0    .2    .1    .3    .5    .4    .4    .4    .0    .0    .1    .1    .1
 290.  *   .4    .6    .9    .7    .6    .6    .4    .0    .1    .1    .3    .5    .4    .4    .4    .0    .0    .0    .1    .1
 295.  *   .4    .7   1.0    .6    .6    .4    .4    .1    .1    .2    .4    .5    .4    .4    .4    .0    .0    .0    .0    .0
 300.  *   .4    .7    .9    .6    .5    .4    .3    .1    .1    .2    .4    .5    .4    .4    .4    .0    .0    .0    .0    .0
 305.  *   .4    .7    .9    .7    .5    .5    .2    .1    .1    .2    .4    .5    .4    .4    .4    .0    .0    .0    .0    .0
 310.  *   .4    .6    .9    .7    .5    .5    .3    .1    .1    .2    .4    .4    .5    .4    .4    .0    .0    .0    .0    .0
 315.  *   .3    .5    .8    .5    .6    .5    .4    .1    .1    .2    .5    .4    .5    .4    .4    .0    .0    .0    .0    .0
 320.  *   .2    .4    .6    .5    .6    .5    .4    .1    .1    .1    .5    .5    .5    .4    .4    .0    .0    .0    .0    .0
 325.  *   .1    .4    .6    .5    .6    .4    .4    .1    .1    .1    .4    .5    .5    .4    .5    .0    .0    .0    .0    .0
 330.  *   .0    .3    .6    .6    .6    .4    .4    .1    .1    .1    .4    .5    .5    .4    .5    .0    .0    .0    .0    .0
 335.  *   .1    .2    .6    .5    .6    .4    .4    .1    .2    .2    .3    .5    .5    .5    .6    .1    .0    .0    .0    .0
 340.  *   .1    .1    .5    .5    .6    .4    .4    .1    .2    .2    .3    .5    .5    .5    .6    .1    .0    .0    .0    .0
 345.  *   .1    .2    .5    .5    .6    .4    .4    .1    .2    .3    .3    .6    .5    .5    .6    .1    .0    .0    .0    .0
 350.  *   .1    .2    .5    .7    .6    .4    .3    .1    .2    .3    .4    .6    .5    .5    .7    .2    .1    .0    .0    .0
 355.  *   .1    .2    .4    .6    .6    .4    .3    .0    .1    .3    .5    .6    .5    .6    .9    .3    .1    .1    .0    .0
 360.  *   .0    .2    .3    .6    .6    .3    .3    .0    .1    .3    .5    .6    .6    .5   1.0    .5    .2    .2    .0    .0
 ------*-------------------------------------------------------------------------------------------------------------------------
 MAX   *   .5    .7   1.0    .8    .7    .6    .5    .5    .6    .8    .8    .8    .6    .6   1.1   1.2   1.0    .8    .7    .7
 DEGR. *  170   295   295   275   275   290   285   260   250   245   260   255     0   230   180    20   130    25   120   130

1
                                                                                                                        PAGE  5
      JOB: Site 5 Olymp & La Brea (S5EXPM.DAT)                  RUN: Site 5 Existing PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
```

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                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .7    .7    .8    .6    .5    .3    .7
   5.  *    .0    .7    .7    .8    .7    .6    .5    .6
  10.  *    .0    .7    .8    .8    .7    .6    .6    .5
  15.  *    .0    .7    .8    .9    .9    .6    .5    .6
  20.  *    .0    .7    .8    .9    .8    .4    .4    .6
  25.  *    .1    .8    .8   1.0    .7    .4    .5    .6
  30.  *    .1    .8    .8    .9    .8    .4    .5    .6
  35.  *    .1    .8    .8    .9    .6    .5    .5    .6
  40.  *    .1    .8    .8    .8    .5    .6    .6    .6
  45.  *    .1    .9    .8    .8    .5    .6    .6    .4
  50.  *    .1    .9    .8    .8    .4    .6    .6    .5
  55.  *    .1    .9    .9    .8    .6    .5    .6    .5
  60.  *    .1    .9    .8    .6    .6    .5    .6    .5
  65.  *    .1    .8    .7    .6    .6    .5    .5    .5
  70.  *    .1    .9    .7    .8    .6    .6    .5    .4
  75.  *    .2    .9    .7    .7    .7    .6    .4    .5
  80.  *    .1    .9    .6    .6    .7    .6    .4    .6
  85.  *    .1    .7    .6    .5    .5    .6    .5    .6
  90.  *    .2    .7    .5    .3    .6    .5    .5    .5
  95.  *    .4    .5    .3    .3    .6    .5    .5    .6
 100.  *    .5    .3    .4    .3    .4    .5    .5    .6
 105.  *    .5    .2    .3    .3    .4    .5    .5    .6
 110.  *    .5    .2    .1    .2    .3    .5    .5    .7
 115.  *    .7    .1    .1    .2    .3    .5    .6    .6
 120.  *    .8    .1    .1    .2    .4    .5    .5    .5
 125.  *    .7    .1    .1    .2    .4    .5    .5    .5
 130.  *    .7    .1    .1    .1    .5    .5    .5    .5
 135.  *    .6    .1    .1    .1    .5    .5    .5    .4
 140.  *    .6    .0    .1    .1    .4    .5    .4    .4
 145.  *    .5    .0    .1    .1    .3    .4    .3    .4
 150.  *    .5    .0    .1    .1    .3    .4    .3    .3
 155.  *    .5    .0    .0    .1    .2    .3    .2    .2
 160.  *    .5    .0    .0    .0    .2    .2    .1    .2
 165.  *    .5    .0    .0    .0    .2    .2    .1    .1
 170.  *    .5    .0    .0    .0    .0    .0    .0    .1
 175.  *    .5    .0    .0    .0    .0    .0    .0    .0
 180.  *    .5    .0    .0    .0    .0    .0    .0    .0
 185.  *    .5    .0    .0    .0    .0    .0    .0    .0
 190.  *    .5    .0    .0    .0    .0    .0    .0    .0
 195.  *    .5    .0    .0    .0    .0    .0    .0    .0
 200.  *    .5    .0    .0    .0    .0    .0    .0    .0
 205.  *    .5    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
      JOB: Site 5 Olymp & La Brea (S5EXPM.DAT)                  RUN: Site 5 Existing PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .5    .0    .0    .0    .0    .0    .0    .0
 215.  *    .5    .0    .0    .0    .0    .0    .0    .0
 220.  *    .5    .0    .0    .0    .0    .0    .0    .0
 225.  *    .5    .0    .0    .0    .0    .0    .0    .0
 230.  *    .5    .0    .0    .0    .0    .0    .0    .0
 235.  *    .6    .0    .0    .0    .0    .0    .0    .0
 240.  *    .6    .0    .0    .0    .0    .0    .0    .0
 245.  *    .6    .0    .0    .0    .0    .0    .0    .0
 250.  *    .6    .2    .1    .1    .0    .0    .0    .0
 255.  *    .6    .2    .1    .1    .1    .0    .0    .0
 260.  *    .6    .3    .3    .4    .3    .0    .0    .0
 265.  *    .5    .5    .4    .5    .5    .0    .0    .0
 270.  *    .5    .6    .7    .6    .6    .1    .0    .0
 275.  *    .2    .8    .9    .8    .9    .1    .1    .0
 280.  *    .2   1.0    .9   1.0    .9    .3    .1    .0
 285.  *    .1   1.0   1.0   1.0    .9    .3    .1    .1
 290.  *    .1   1.0   1.0   1.0    .8    .3    .1    .1
 295.  *    .0   1.0   1.0   1.0    .8    .2    .1    .1
 300.  *    .0    .9    .8    .8    .8    .3    .2    .1
 305.  *    .0    .8    .8    .8    .7    .3    .1    .1
 310.  *    .0    .8    .8    .8    .7    .3    .1    .2
 315.  *    .0    .8    .8    .8    .6    .3    .1    .2
 320.  *    .0    .8    .7    .7    .6    .3    .2    .2
 325.  *    .0    .7    .6    .7    .6    .2    .3    .2
 330.  *    .0    .7    .6    .7    .5    .2    .3    .5
 335.  *    .0    .7    .7    .7    .5    .3    .3    .4
 340.  *    .0    .7    .7    .7    .5    .3    .3    .4
 345.  *    .0    .7    .7    .7    .4    .5    .3    .5
 350.  *    .0    .7    .7    .7    .5    .4    .3    .6
 355.  *    .0    .7    .7    .7    .6    .4    .3    .5
 360.  *    .0    .7    .7    .8    .6    .5    .3    .7
 ------*------------------------------------------------
 MAX   *    .8   1.0   1.0   1.0    .9    .6    .6    .7
 DEGR. *  120   280   285    25    15     5    10   110

 THE HIGHEST CONCENTRATION IS    1.20 PPM AT   20 DEGREES FROM REC16.
 THE 2ND HIGHEST CONCENTRATION IS    1.10 PPM AT  180 DEGREES FROM REC15.
 THE 3RD HIGHEST CONCENTRATION IS    1.00 PPM AT   25 DEGREES FROM REC24.
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5NBAM.DAT)                  RUN: Site 5 No Build AM
      DATE: 03/19/2010   TIME: 10:48:39.32


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   1574.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   1574.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0    -293.1    1055.8 *     837.   272. AG     29. 100.0    .0 48.0 1.18  42.5
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   1611.    .9    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   2014.    .9    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   2014.    .9    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0    1341.2    1048.5 *     646.    91. AG     24. 100.0    .0 48.0 1.08  32.8
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   2122.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   2059.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   2059.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   2059.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   1961.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   1961.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    1845.4   -1844.0 *    3056.   157. AG     23. 100.0    .0 36.0 1.70 155.3
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG     98.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG     98.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     653.7     915.8 *      63.   156. AG     10. 100.0    .0 12.0  .82   3.2
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   2119.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   2119.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   2119.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   2322.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   2165.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   2165.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1071.7    4459.6 *    3374.     8. AG     22. 100.0    .0 36.0 1.71 171.4
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    157.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    157.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     746.3    2008.9 *     901.     8. AG      6. 100.0    .0 12.0 1.99  45.8
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   2117.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   2117.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   2117.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   2117.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   2117.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   2117.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5NBAM.DAT)                  RUN: Site 5 No Build AM
      DATE: 03/19/2010   TIME: 10:48:39.32

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       66       2.0      1574       1112       4.10     1        3
       7. WB        Oly AP Q  *     100       54       2.0      2014       1105       4.10     1        3
      14. NB        Brea T+R Q*     100       69       2.0      1961       1423       4.10     1        3
      17. NB        Brea LT Q *     100       88       2.0        98       1490       4.10     1        3
      24. SB        Brea T+R Q*     100       66       2.0      2165       1408       4.10     1        3
      27. SB        Brea LT Q *     100       54       2.0       157        190       4.10     1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5NBAM.DAT)                  RUN: Site 5 No Build AM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-----------------------------------------------------------------------------------------------------------------------
   0.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
   5.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  10.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .3    .1    .1    .1    .0    .0
  15.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0
  25.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .1    .0    .0
  30.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0
  35.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *   .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *   .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  55.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0
  60.  *   .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  65.  *   .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  70.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  75.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  80.  *   .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *   .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *   .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
  95.  *   .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
 100.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 105.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 110.  *   .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 115.  *   .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 120.  *   .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 125.  *   .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 130.  *   .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .1    .1    .2
 135.  *   .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .1    .1    .2
 140.  *   .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .1    .2    .1    .1    .2
 145.  *   .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .1    .1    .2    .1    .1    .2
 150.  *   .1    .0    .1    .0    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .2
 155.  *   .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .1    .1    .2    .0    .2    .2
 160.  *   .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .1    .1    .2    .0    .2    .2
 165.  *   .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .1    .1    .1    .0    .2    .2
 170.  *   .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .0    .2    .2
 175.  *   .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .0    .2    .2
 180.  *   .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .1    .2    .2
 185.  *   .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .1    .2    .2
 190.  *   .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .0    .2    .2
 195.  *   .0    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .1    .1    .0    .0    .2    .2
 200.  *   .0    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .1    .1    .0    .0    .0    .2    .2
 205.  *   .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .1    .1    .0    .0    .0    .2    .2
1
                                                                                                                     PAGE   4
      JOB: Site 5 Olymp & La Brea (S5NBAM.DAT)                 RUN: Site 5 No Build AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*-----------------------------------------------------------------------------------------------------------------------
 210.  *   .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
 215.  *   .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .1    .2    .2
 220.  *   .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 225.  *   .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .1    .0    .1    .1    .0    .0    .2    .2    .2
 230.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 235.  *   .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 240.  *   .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 245.  *   .1    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 250.  *   .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 255.  *   .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 260.  *   .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 265.  *   .1    .1    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .1    .1    .1
 270.  *   .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 275.  *   .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .1
 280.  *   .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1
 285.  *   .1    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *   .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *   .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *   .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *   .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 310.  *   .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 315.  *   .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 320.  *   .0    .0    .2    .0    .0    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *   .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 360.  *   .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 ------*-----------------------------------------------------------------------------------------------------------------------
 MAX   *   .1    .2    .2    .1    .2    .2    .1    .2    .2    .2    .2    .1    .1    .1    .3    .2    .2    .2    .2    .2
 DEGR. * 130   175   235    55    60    60    45    90    90   100   100     0     0     0    10    30    75    35   155   130

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                                                                                                                     PAGE   5
      JOB: Site 5 Olymp & La Brea (S5NBAM.DAT)                 RUN: Site 5 No Build AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
```

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                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .1    .1
   5.  *    .0    .1    .1    .1    .0    .0    .1    .1
  10.  *    .0    .1    .1    .1    .1    .0    .1    .1
  15.  *    .0    .1    .1    .1    .0    .0    .1    .1
  20.  *    .0    .1    .1    .1    .0    .1    .0    .1
  25.  *    .0    .1    .1    .1    .0    .1    .0    .1
  30.  *    .0    .1    .1    .1    .0    .1    .0    .1
  35.  *    .0    .1    .1    .1    .1    .1    .0    .1
  40.  *    .0    .1    .1    .1    .0    .0    .0    .1
  45.  *    .0    .1    .1    .1    .0    .0    .0    .1
  50.  *    .0    .1    .1    .1    .0    .0    .0    .1
  55.  *    .0    .1    .1    .1    .0    .0    .0    .1
  60.  *    .0    .1    .1    .1    .0    .1    .0    .1
  65.  *    .0    .1    .1    .1    .0    .1    .0    .0
  70.  *    .0    .1    .1    .1    .0    .1    .0    .1
  75.  *    .0    .1    .1    .0    .0    .1    .0    .2
  80.  *    .0    .1    .1    .0    .0    .1    .0    .2
  85.  *    .1    .1    .1    .0    .0    .0    .0    .2
  90.  *    .1    .1    .0    .0    .0    .0    .1    .2
  95.  *    .1    .1    .0    .0    .0    .0    .1    .2
 100.  *    .1    .0    .0    .0    .0    .0    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .1    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .1    .1    .2
 130.  *    .2    .0    .0    .0    .0    .0    .1    .2
 135.  *    .2    .0    .0    .0    .0    .0    .0    .1
 140.  *    .2    .0    .0    .0    .0    .0    .0    .1
 145.  *    .2    .0    .0    .0    .0    .0    .0    .1
 150.  *    .2    .0    .0    .0    .0    .0    .0    .1
 155.  *    .2    .0    .0    .0    .0    .0    .0    .1
 160.  *    .2    .0    .0    .0    .0    .0    .0    .0
 165.  *    .2    .0    .0    .0    .0    .0    .0    .0
 170.  *    .2    .0    .0    .0    .0    .0    .0    .0
 175.  *    .2    .0    .0    .0    .0    .0    .0    .0
 180.  *    .2    .0    .0    .0    .0    .0    .0    .0
 185.  *    .2    .0    .0    .0    .0    .0    .0    .0
 190.  *    .2    .0    .0    .0    .0    .0    .0    .0
 195.  *    .2    .0    .0    .0    .0    .0    .0    .0
 200.  *    .2    .0    .0    .0    .0    .0    .0    .0
 205.  *    .2    .0    .0    .0    .0    .0    .0    .0
1                                                                                                                               PAGE  6
      JOB: Site 5 Olymp & La Brea (S5NBAM.DAT)                  RUN: Site 5 No Build AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .2    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .1    .1    .1    .1    .0    .0    .0
 270.  *    .1    .1    .1    .1    .1    .0    .0    .0
 275.  *    .1    .2    .1    .1    .1    .0    .0    .0
 280.  *    .1    .2    .1    .1    .1    .0    .0    .0
 285.  *    .0    .2    .1    .1    .1    .0    .0    .0
 290.  *    .0    .2    .1    .1    .1    .0    .0    .0
 295.  *    .0    .2    .1    .1    .1    .0    .0    .0
 300.  *    .0    .2    .1    .1    .1    .0    .0    .0
 305.  *    .0    .2    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .0    .0    .0    .1
 340.  *    .0    .1    .1    .1    .0    .0    .0    .1
 345.  *    .0    .1    .1    .1    .0    .0    .0    .1
 350.  *    .0    .1    .1    .1    .0    .0    .1    .1
 355.  *    .0    .1    .1    .1    .0    .0    .1    .1
 360.  *    .0    .1    .1    .1    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .2    .2    .1    .1    .1    .1    .1    .2
 DEGR. *  115   275     0     0    10    20     0    75

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  175 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  235 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5NBPM.DAT)                 RUN: Site 5 No Build PM
      DATE: 03/19/2010   TIME: 10:59:15.30


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)        (VEH)
      ------------------------*----------------------------------------*--------------------------------------------------------------
       1. EB        Oly AP    *   354.0    1033.0    -378.0    1053.0 *    732.  272. AG  2302.    .8    .0 56.0
       2. EB        Oly AP    *   353.0    1037.0     623.0    1030.0 *    270.   91. AG  2302.    .8    .0 68.0
       3. EB        Oly AP Q  *   544.0    1032.0   -2188.0    1109.6 *   2733.  272. AG    29. 100.0    .0 48.0 1.72 138.8
       4. EB        Oly DP    *   624.0    1024.0    1617.0    1000.0 *    993.   91. AG  2212.    .8    .0 56.0
       5. WB        Oly AP    *   891.0    1065.0    1622.0    1047.0 *    731.   91. AG  1456.    .8    .0 56.0
       6. WB        Oly AP    *   890.0    1060.0     630.0    1066.0 *    260.  271. AG  1456.    .8    .0 68.0
       7. WB        Oly AP Q  *   695.0    1064.0     821.3    1061.0 *    126.   91. AG    25. 100.0    .0 48.0  .83   6.4
       8. WB        Oly DP    *   628.0    1073.0    -378.0    1100.0 *   1006.  272. AG  1502.    .8    .0 56.0
       9. NB        Brea AP   *  1230.0     261.0    1042.0     547.0 *    342.  327. AG  2217.    .8    .0 56.0
      10. NB        Brea AP   *  1042.0     547.0     981.0     616.0 *     92.  319. AG  2217.    .8    .0 56.0
      11. NB        Brea AP   *   981.0     616.0     795.0     761.0 *    236.  308. AG  2217.    .8    .0 56.0
      12. NB        Brea T+R  *   795.0     760.0     706.0     856.0 *    131.  317. AG  2174.    .8    .0 56.0
      13. NB        Brea T+R  *   706.0     856.0     653.0     980.0 *    135.  337. AG  2174.    .8    .0 56.0
      14. NB        Brea T+R Q*   657.0     972.0    2078.0   -2395.2 *   3655.  157. AG    22. 100.0    .0 36.0 1.82 185.7
      15. NB        Brea LT   *   777.0     742.0     686.0     845.0 *    137.  319. AG    43.    .8    .0 32.0
      16. NB        Brea LT   *   686.0     845.0     625.0     981.0 *    149.  336. AG    43.    .8    .0 32.0
      17. NB        Brea LT Q *   628.0     973.0     639.6     947.2 *     28.  156. AG    10. 100.0    .0 12.0  .73   1.4
      18. NB        Brea DP   *   653.0     978.0     638.0    1130.0 *    153.  354. AG  2520.    .8    .0 56.0
      19. NB        Brea DP   *   638.0    1130.0     658.0    1238.0 *    110.   10. AG  2520.    .8    .0 56.0
      20. NB        Brea DP   *   658.0    1238.0     933.0    2002.0 *    812.   20. AG  2520.    .8    .0 56.0
      21. SB        Brea AP   *   644.0    1336.0     884.0    2016.0 *    721.   19. AG  2660.    .8    .0 56.0
      22. SB        Brea T+R  *   644.0    1337.0     606.0    1228.0 *    115.  199. AG  2472.    .8    .0 56.0
      23. SB        Brea T+R  *   606.0    1228.0     588.0    1103.0 *    126.  188. AG  2472.    .8    .0 56.0
      24. SB        Brea T+R Q*   590.0    1120.0    1118.7    4785.7 *   3704.    8. AG    20. 100.0    .0 36.0 1.67 188.1
      25. SB        Brea LT   *   665.0    1326.0     629.0    1221.0 *    111.  199. AG   188.    .8    .0 32.0
      26. SB        Brea LT   *   629.0    1221.0     612.0    1105.0 *    117.  188. AG   188.    .8    .0 32.0
      27. SB        Brea LT Q *   614.0    1118.0     794.5    2333.7 *   1229.    8. AG     6. 100.0    .0 12.0 2.38  62.4
      28. SB        Brea DP   *   588.0    1102.0     600.0     989.0 *    114.  174. AG  2401.    .8    .0 56.0
      29. SB        Brea DP   *   600.0     989.0     650.0     854.0 *    144.  160. AG  2401.    .8    .0 56.0
      30. SB        Brea DP   *   650.0     854.0     723.0     758.0 *    121.  143. AG  2401.    .8    .0 56.0
      31. SB        Brea DP   *   723.0     758.0     938.0     583.0 *    277.  129. AG  2401.    .8    .0 56.0
      32. SB        Brea DP   *   938.0     583.0    1029.0     479.0 *    138.  139. AG  2401.    .8    .0 56.0
      33. SB        Brea DP   *  1029.0     479.0    1184.0     227.0 *    296.  148. AG  2401.    .8    .0 56.0
1
                                                                                                                PAGE  2
      JOB: Site 5 Olymp & La Brea (S5NBPM.DAT)                 RUN: Site 5 No Build PM
      DATE: 03/19/2010   TIME: 10:59:15.30

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       66       2.0       2302       1115       4.10      1        3
       7. WB        Oly AP Q  *     100       56       2.0       1456       1100       4.10      1        3
      14. NB        Brea T+R Q*     100       68       2.0       2174       1423       4.10      1        3
      17. NB        Brea LT Q *     100       92       2.0         43       1490       4.10      1        3
      24. SB        Brea T+R Q*     100       61       2.0       2472       1412       4.10      1        3
      27. SB        Brea LT Q *     100       51       2.0        188        176       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-----------------------------------*
      1. SE MID S             *       873.0      736.0       5.0   *
      2. SE 164 S             *       771.0      827.0       5.0   *
      3. SE 82 S              *       719.0      893.0       5.0   *
      4. SE CNR               *       695.0      985.0       5.0   *
      5. SE 82 E              *       784.0      990.0       5.0   *
      6. SE 164 E             *       866.0      989.0       5.0   *
      7. SE MID E             *       986.0      986.0       5.0   *
      8. NE MID E             *       977.0     1089.0       5.0   *
      9. NE 164 E             *       844.0     1094.0       5.0   *
     10. NE 82 E              *       762.0     1096.0       5.0   *
     11. NE CNR               *       680.0     1105.0       5.0   *
     12. NE 82 N              *       683.0     1199.0       5.0   *
     13. NE 164 N             *       707.0     1278.0       5.0   *
     14. NE MID N             *       748.0     1407.0       5.0   *
     15. NW MID N             *       646.0     1421.0       5.0   *
     16. NW 164 N             *       592.0     1268.0       5.0   *
     17. NW 82 N              *       569.0     1188.0       5.0   *
     18. NW CNR               *       550.0     1110.0       5.0   *
     19. NW 82 W              *       462.0     1106.0       5.0   *
     20. NW 164 W             *       380.0     1107.0       5.0   *
     21. NW MID W             *       226.0     1111.0       5.0   *
     22. SW MID W             *       220.0     1007.0       5.0   *
     23. SW 164 W             *       395.0     1000.0       5.0   *
     24. SW 82 W              *       478.0      998.0       5.0   *
     25. SW CNR               *       560.0      994.0       5.0   *
     26. SW 82 S              *       594.0      911.0       5.0   *
     27. SW 164 S             *       626.0      834.0       5.0   *
     28. SW MID S             *       709.0      731.0       5.0   *
1
                                                                                                                PAGE  3
      JOB: Site 5 Olymp & La Brea (S5NBPM.DAT)                 RUN: Site 5 No Build PM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .0    .0    .0
  10.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .2    .3    .1    .1    .0    .0
  30.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .3    .1    .2    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  95.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
 150.  *    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
 155.  *    .1    .0    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .1    .1
 160.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 165.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 170.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .1    .0    .1    .1
 175.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 180.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 185.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 190.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 195.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .2    .1    .0    .0    .1    .1
 200.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
 205.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
1
                                                                                                                 PAGE  4
      JOB: Site 5 Olymp & La Brea (S5NBPM.DAT)                  RUN: Site 5 No Build PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 215.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 220.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 225.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 230.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 235.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .1    .1
 240.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 245.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 250.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .2    .2    .2
 255.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 260.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 265.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 270.  *    .1    .1    .2    .1    .0    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 275.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0
 280.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 285.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .1    .2    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .2    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .2    .3    .2    .2    .2    .2
 DEGR. *  130   165   225   190     0     0     0    90   230   120   255     0     0     0     0    25    50    30   240   240

1
                                                                                                                 PAGE  5
      JOB: Site 5 Olymp & La Brea (S5NBPM.DAT)                  RUN: Site 5 No Build PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
```

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                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .2    .2    .2    .1    .0    .1    .2
   5.  *    .0    .2    .2    .2    .1    .0    .1    .2
  10.  *    .0    .2    .2    .2    .1    .1    .1    .1
  15.  *    .0    .2    .2    .2    .1    .1    .1    .1
  20.  *    .0    .2    .2    .2    .2    .1    .1    .1
  25.  *    .0    .2    .2    .2    .1    .1    .1    .1
  30.  *    .0    .2    .2    .2    .2    .1    .0    .1
  35.  *    .0    .2    .2    .2    .2    .1    .0    .1
  40.  *    .0    .2    .2    .2    .1    .1    .0    .1
  45.  *    .0    .2    .2    .2    .1    .1    .0    .0
  50.  *    .0    .2    .2    .2    .1    .1    .0    .2
  55.  *    .0    .2    .2    .2    .1    .1    .0    .1
  60.  *    .0    .2    .2    .2    .0    .1    .0    .1
  65.  *    .0    .2    .2    .2    .0    .1    .0    .1
  70.  *    .0    .2    .2    .2    .0    .1    .0    .1
  75.  *    .0    .2    .2    .1    .0    .1    .0    .1
  80.  *    .0    .2    .2    .1    .1    .1    .1    .2
  85.  *    .0    .2    .2    .1    .1    .1    .1    .2
  90.  *    .0    .1    .1    .0    .1    .1    .1    .1
  95.  *    .1    .1    .0    .0    .0    .1    .1    .2
 100.  *    .1    .0    .0    .0    .0    .1    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .1    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .1    .1    .1    .2
 130.  *    .1    .0    .0    .0    .1    .1    .1    .2
 135.  *    .1    .0    .0    .0    .1    .1    .1    .1
 140.  *    .1    .0    .0    .0    .1    .0    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .1
 150.  *    .1    .0    .0    .0    .0    .0    .0    .1
 155.  *    .1    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1                                                                                                                             PAGE  6
      JOB: Site 5 Olymp & La Brea (S5NBPM.DAT)                 RUN: Site 5 No Build PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .2    .0    .0    .0    .0    .0    .0    .0
 265.  *    .2    .2    .1    .1    .1    .0    .0    .0
 270.  *    .2    .2    .1    .1    .1    .0    .0    .0
 275.  *    .0    .2    .2    .1    .2    .0    .0    .0
 280.  *    .0    .2    .2    .1    .2    .0    .0    .0
 285.  *    .0    .2    .2    .2    .2    .0    .0    .0
 290.  *    .0    .2    .2    .2    .2    .0    .0    .0
 295.  *    .0    .2    .1    .2    .2    .0    .0    .0
 300.  *    .0    .2    .1    .2    .2    .0    .0    .0
 305.  *    .0    .2    .1    .2    .2    .0    .0    .0
 310.  *    .0    .2    .1    .2    .2    .0    .0    .0
 315.  *    .0    .2    .1    .2    .2    .0    .0    .0
 320.  *    .0    .2    .1    .2    .2    .0    .0    .0
 325.  *    .0    .2    .1    .2    .2    .0    .0    .0
 330.  *    .0    .2    .1    .2    .2    .0    .0    .1
 335.  *    .0    .2    .1    .2    .1    .0    .0    .1
 340.  *    .0    .2    .2    .2    .1    .0    .0    .1
 345.  *    .0    .2    .2    .2    .1    .0    .1    .1
 350.  *    .0    .2    .2    .2    .1    .0    .1    .1
 355.  *    .0    .2    .2    .2    .1    .0    .1    .1
 360.  *    .0    .2    .2    .2    .1    .0    .1    .2
 ------*------------------------------------------------
 MAX   *    .2    .2    .2    .2    .2    .1    .1    .2
 DEGR. *  115     0     0     0    20    10     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   25 DEGREES FROM REC16.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  165 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  225 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5M1AM.DAT)                 RUN: Site 5 MOS 1 AM
      DATE: 03/19/2010   TIME: 11:22:51.01


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*---------------------------------------*-------------------------------------------------------------
       1. EB        Oly AP    *   354.0    1033.0    -378.0    1053.0 *    732.   272. AG   1576.    .8    .0 56.0
       2. EB        Oly AP    *   353.0    1037.0     623.0    1030.0 *    270.    91. AG   1576.    .8    .0 68.0
       3. EB        Oly AP Q  *   544.0    1032.0    -303.6    1056.1 *    848.   272. AG     29. 100.0    .0 48.0 1.18  43.1
       4. EB        Oly DP    *   624.0    1024.0    1617.0    1000.0 *    993.    91. AG   1595.    .9    .0 56.0
       5. WB        Oly AP    *   891.0    1065.0    1622.0    1047.0 *    731.    91. AG   1928.    .9    .0 56.0
       6. WB        Oly AP    *   890.0    1060.0     630.0    1066.0 *    260.   271. AG   1928.    .9    .0 68.0
       7. WB        Oly AP Q  *   695.0    1064.0    1123.6    1053.7 *    429.    91. AG     24. 100.0    .0 48.0 1.04  21.8
       8. WB        Oly DP    *   628.0    1073.0    -378.0    1100.0 *   1006.   272. AG   2087.    .8    .0 56.0
       9. NB        Brea AP   *  1230.0     261.0    1042.0     547.0 *    342.   327. AG   2062.    .8    .0 56.0
      10. NB        Brea AP   *  1042.0     547.0     981.0     616.0 *     92.   319. AG   2062.    .8    .0 56.0
      11. NB        Brea AP   *   981.0     616.0     795.0     761.0 *    236.   308. AG   2062.    .8    .0 56.0
      12. NB        Brea T+R  *   795.0     760.0     706.0     856.0 *    131.   317. AG   1961.    .8    .0 56.0
      13. NB        Brea T+R  *   706.0     856.0     653.0     980.0 *    135.   337. AG   1961.    .8    .0 56.0
      14. NB        Brea T+R Q*   657.0     972.0    1789.3   -1711.1 *   2912.   157. AG     22. 100.0    .0 36.0 1.64 147.9
      15. NB        Brea LT   *   777.0     742.0     686.0     845.0 *    137.   319. AG    101.    .8    .0 32.0
      16. NB        Brea LT   *   686.0     845.0     625.0     981.0 *    149.   336. AG    101.    .8    .0 32.0
      17. NB        Brea LT Q *   628.0     973.0     655.6     911.5 *     67.   156. AG     10. 100.0    .0 12.0  .85   3.4
      18. NB        Brea DP   *   653.0     978.0     638.0    1130.0 *    153.   354. AG   2113.    .8    .0 56.0
      19. NB        Brea DP   *   638.0    1130.0     658.0    1238.0 *    110.    10. AG   2113.    .8    .0 56.0
      20. NB        Brea DP   *   658.0    1238.0     933.0    2002.0 *    812.    20. AG   2113.    .8    .0 56.0
      21. SB        Brea AP   *   644.0    1336.0     884.0    2016.0 *    721.    19. AG   2347.    .8    .0 56.0
      22. SB        Brea T+R  *   644.0    1337.0     606.0    1228.0 *    115.   199. AG   2200.    .8    .0 56.0
      23. SB        Brea T+R  *   606.0    1228.0     588.0    1103.0 *    126.   188. AG   2200.    .8    .0 56.0
      24. SB        Brea T+R Q*   590.0    1120.0    1091.0    4593.6 *   3510.     8. AG     22. 100.0    .0 36.0 1.74 178.3
      25. SB        Brea LT   *   665.0    1326.0     629.0    1221.0 *    111.   199. AG    147.    .8    .0 32.0
      26. SB        Brea LT   *   629.0    1221.0     612.0    1105.0 *    117.   188. AG    147.    .8    .0 32.0
      27. SB        Brea LT Q *   614.0    1118.0     729.1    1892.9 *    783.     8. AG      6. 100.0    .0 12.0 1.84  39.8
      28. SB        Brea DP   *   588.0    1102.0     600.0     989.0 *    114.   174. AG   2118.    .8    .0 56.0
      29. SB        Brea DP   *   600.0     989.0     650.0     854.0 *    144.   160. AG   2118.    .8    .0 56.0
      30. SB        Brea DP   *   650.0     854.0     723.0     758.0 *    121.   143. AG   2118.    .8    .0 56.0
      31. SB        Brea DP   *   723.0     758.0     938.0     583.0 *    277.   129. AG   2118.    .8    .0 56.0
      32. SB        Brea DP   *   938.0     583.0    1029.0     479.0 *    138.   139. AG   2118.    .8    .0 56.0
      33. SB        Brea DP   *  1029.0     479.0    1184.0     227.0 *    296.   148. AG   2118.    .8    .0 56.0
1
                                                                                                                        PAGE  2
      JOB: Site 5 Olymp & La Brea (S5M1AM.DAT)                 RUN: Site 5 MOS 1 AM
      DATE: 03/19/2010   TIME: 11:22:51.01

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)    (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       66       2.0      1576       1111       4.10      1         3
       7. WB        Oly AP Q  *     100       54       2.0      1928       1106       4.10      1         3
      14. NB        Brea T+R Q*     100       68       2.0      1961       1422       4.10      1         3
      17. NB        Brea LT Q *     100       88       2.0       101       1490       4.10      1         3
      24. SB        Brea T+R Q*     100       66       2.0      2200       1404       4.10      1         3
      27. SB        Brea LT Q *     100       54       2.0       147        191       4.10      1         3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-----------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                        PAGE  3
      JOB: Site 5 Olymp & La Brea (S5M1AM.DAT)                 RUN: Site 5 MOS 1 AM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .3    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
  95.  *    .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 130.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
 135.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .1    .1    .2
 140.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .1    .2    .1    .1    .2
 145.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .2
 150.  *    .1    .0    .1    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .2
 155.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .1    .1    .2    .0    .2    .2
 160.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .1    .1    .2    .0    .2    .2
 165.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .2
 170.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 175.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 180.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .1    .2    .2
 185.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .0    .2    .2
 190.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 195.  *    .0    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .1    .1    .0    .0    .2    .2
 200.  *    .0    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .1    .1    .0    .0    .0    .2    .2
 205.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .1    .1    .0    .0    .0    .2    .2
1
                                                                                                                       PAGE  4
      JOB: Site 5 Olymp & La Brea (S5M1AM.DAT)                  RUN: Site 5 MOS 1 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
 215.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .1    .2    .2
 220.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 225.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 230.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 235.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 240.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 245.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 250.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 255.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 260.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 265.  *    .1    .1    .1    .0    .0    .0    .0    .1    .2    .0    .1    .0    .0    .1    .1    .0    .0    .1    .1    .1
 270.  *    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .1    .0    .1    .1    .0    .0    .1    .1    .1
 275.  *    .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .1
 280.  *    .1    .1    .2    .1    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1
 285.  *    .1    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .0    .0    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .1    .1    .1    .1    .2    .2    .2    .2    .1    .1    .1    .3    .2    .2    .2    .2    .2
 DEGR. *  130   175   235    55    45    45    45    95    95   100   100     0     0     0    10    30    70    35   155   130

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                                                                                                                       PAGE  5
      JOB: Site 5 Olymp & La Brea (S5M1AM.DAT)                  RUN: Site 5 MOS 1 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
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                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .1    .1
   5.  *    .0    .1    .1    .1    .0    .0    .1    .1
  10.  *    .0    .1    .1    .1    .1    .0    .1    .1
  15.  *    .0    .1    .1    .1    .0    .0    .1    .1
  20.  *    .0    .1    .1    .1    .0    .1    .0    .1
  25.  *    .0    .1    .1    .1    .0    .1    .0    .1
  30.  *    .0    .1    .1    .1    .0    .1    .0    .1
  35.  *    .0    .1    .1    .1    .1    .1    .0    .1
  40.  *    .0    .1    .1    .1    .0    .0    .0    .1
  45.  *    .0    .1    .1    .1    .0    .0    .0    .0
  50.  *    .0    .1    .1    .1    .0    .0    .0    .1
  55.  *    .0    .1    .1    .1    .0    .0    .0    .0
  60.  *    .0    .1    .1    .1    .0    .1    .0    .0
  65.  *    .0    .1    .1    .1    .0    .1    .0    .0
  70.  *    .0    .1    .1    .1    .0    .1    .0    .1
  75.  *    .0    .1    .1    .0    .0    .1    .0    .1
  80.  *    .0    .1    .1    .0    .0    .1    .0    .2
  85.  *    .1    .1    .1    .0    .0    .0    .0    .2
  90.  *    .1    .1    .0    .0    .0    .0    .1    .1
  95.  *    .1    .1    .0    .0    .0    .0    .1    .2
 100.  *    .1    .0    .0    .0    .0    .0    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .1    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .1    .1    .2
 130.  *    .2    .0    .0    .0    .0    .0    .1    .2
 135.  *    .2    .0    .0    .0    .0    .0    .0    .1
 140.  *    .2    .0    .0    .0    .0    .0    .0    .1
 145.  *    .2    .0    .0    .0    .0    .0    .0    .1
 150.  *    .2    .0    .0    .0    .0    .0    .0    .1
 155.  *    .2    .0    .0    .0    .0    .0    .0    .1
 160.  *    .2    .0    .0    .0    .0    .0    .0    .0
 165.  *    .2    .0    .0    .0    .0    .0    .0    .0
 170.  *    .2    .0    .0    .0    .0    .0    .0    .0
 175.  *    .2    .0    .0    .0    .0    .0    .0    .0
 180.  *    .2    .0    .0    .0    .0    .0    .0    .0
 185.  *    .2    .0    .0    .0    .0    .0    .0    .0
 190.  *    .2    .0    .0    .0    .0    .0    .0    .0
 195.  *    .2    .0    .0    .0    .0    .0    .0    .0
 200.  *    .2    .0    .0    .0    .0    .0    .0    .0
 205.  *    .2    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                              PAGE  6
      JOB: Site 5 Olymp & La Brea (S5M1AM.DAT)                  RUN: Site 5 MOS 1 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .2    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .1    .1    .1    .1    .0    .0    .0
 270.  *    .1    .1    .1    .1    .1    .0    .0    .0
 275.  *    .1    .2    .1    .1    .1    .0    .0    .0
 280.  *    .0    .2    .1    .1    .1    .0    .0    .0
 285.  *    .0    .2    .1    .1    .1    .0    .0    .0
 290.  *    .0    .2    .1    .1    .1    .0    .0    .0
 295.  *    .0    .2    .1    .1    .1    .0    .0    .0
 300.  *    .0    .2    .1    .1    .1    .0    .0    .0
 305.  *    .0    .2    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .0    .0    .0    .1
 340.  *    .0    .1    .1    .1    .0    .0    .0    .1
 345.  *    .0    .1    .1    .1    .0    .0    .0    .1
 350.  *    .0    .1    .1    .1    .0    .0    .1    .1
 355.  *    .0    .1    .1    .1    .0    .0    .1    .1
 360.  *    .0    .1    .1    .1    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .2    .2    .1    .1    .1    .1    .1    .2
 DEGR. *  115   275     0     0    10    20     0    80

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  175 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  235 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 5 Olymp & La Brea (S5M1PM.DAT)                  RUN: Site 5 MOS 1 PM
      DATE: 03/19/2010   TIME: 11:57:35.38


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =    4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =    .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   2330.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   2330.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0   -2147.3    1108.5 *    2692.   272. AG     29. 100.0    .0 48.0 1.69 136.8
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   2181.    .8    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   1459.    .8    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   1459.    .8    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0     821.7    1061.0 *     127.    91. AG     25. 100.0    .0 48.0  .83   6.4
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   1529.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   2190.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   2190.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   2190.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   2143.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   2143.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    1808.8   -1757.2 *    2962.   157. AG     21. 100.0    .0 36.0 1.57 150.5
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG     47.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG     47.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     642.1     941.6 *      34.   156. AG     10. 100.0    .0 12.0  .80   1.7
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   2562.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   2562.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   2562.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   2702.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   2515.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   2515.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1120.2    4796.2 *    3714.     8. AG     20. 100.0    .0 36.0 1.65 188.7
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    187.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    187.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     803.8    2396.1 *    1292.     8. AG      6. 100.0    .0 12.0 2.60  65.6
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   2409.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   2409.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   2409.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   2409.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   2409.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   2409.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5M1PM.DAT)                  RUN: Site 5 MOS 1 PM
      DATE: 03/19/2010   TIME: 11:57:35.38

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       65       2.0      2330       1113       4.10      1        3
       7. WB        Oly AP Q  *     100       56       2.0      1459       1098       4.10      1        3
      14. NB        Brea T+R Q*     100       64       2.0      2143       1423       4.10      1        3
      17. NB        Brea LT Q *     100       92       2.0        47       1490       4.10      1        3
      24. SB        Brea T+R Q*     100       60       2.0      2515       1411       4.10      1        3
      27. SB        Brea LT Q *     100       51       2.0       187        161       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5M1PM.DAT)                  RUN: Site 5 MOS 1 PM

       MODEL RESULTS
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        REMARKS : In search of the angle corresponding to
                  the maximum concentration, only the first
                  angle, of the angles with same maximum
                  concentrations, is indicated as maximum.

  WIND ANGLE RANGE:   0.-360.

  WIND  * CONCENTRATION
  ANGLE *      (PPM)
  (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
  ------*------------------------------------------------------------------------------------------------------------------------
    0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
    5.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .0    .0    .0
   10.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
   15.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
   20.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .1    .0    .0
   25.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .2    .3    .1    .2    .0    .0
   30.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .3    .1    .2    .0    .0
   35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .3    .1    .2    .0    .0
   40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
   45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
   50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
   55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
   60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
   65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
   70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
   75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
   80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
   85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
   90.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
   95.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
  105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
  110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
  115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
  120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
  125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
  130.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
  135.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
  140.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
  145.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
  150.  *    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
  155.  *    .1    .0    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
  160.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
  165.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
  170.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .1    .0    .1    .1
  175.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .1    .0    .1    .1
  180.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
  185.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
  190.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
  195.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .2    .0    .0    .0    .1    .1
  200.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .2    .0    .0    .0    .1    .1
  205.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
1
                                                                                                                       PAGE  4
      JOB: Site 5 Olymp & La Brea (S5M1PM.DAT)                RUN: Site 5 MOS 1 PM

  WIND  * CONCENTRATION
  ANGLE *      (PPM)
  (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
  ------*------------------------------------------------------------------------------------------------------------------------
  210.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
  215.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
  220.  *    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
  225.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
  230.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
  235.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .1    .2
  240.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
  245.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
  250.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .2    .2    .2
  255.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
  260.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
  265.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
  270.  *    .1    .1    .2    .1    .0    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .2    .2
  275.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0
  280.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
  285.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
  290.  *    .1    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
  295.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
  300.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
  305.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
  310.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
  315.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  320.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  325.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  330.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  340.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  345.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
  350.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
  355.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
  360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
  ------*------------------------------------------------------------------------------------------------------------------------
  MAX   *    .1    .2    .2    .2    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .2    .3    .2    .2    .2    .2
  DEGR. *  130   165   225   195     0     0     0    90   230   120   255     0     0     0     5    25    50    25   240   235

1
                                                                                                                       PAGE  5
      JOB: Site 5 Olymp & La Brea (S5M1PM.DAT)                RUN: Site 5 MOS 1 PM

        MODEL RESULTS
        -------------

        REMARKS : In search of the angle corresponding to
                  the maximum concentration, only the first
```

```
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
  0.  *    .0    .2    .2    .2    .1    .0    .1    .2
  5.  *    .0    .2    .2    .2    .1    .1    .1    .2
 10.  *    .0    .2    .2    .2    .1    .1    .1    .1
 15.  *    .0    .2    .2    .2    .1    .1    .1    .1
 20.  *    .0    .2    .2    .2    .2    .1    .1    .1
 25.  *    .0    .2    .2    .2    .2    .1    .1    .1
 30.  *    .0    .2    .2    .2    .2    .1    .0    .0
 35.  *    .0    .2    .2    .2    .2    .1    .0    .0
 40.  *    .0    .2    .2    .2    .2    .1    .0    .0
 45.  *    .0    .2    .2    .2    .1    .1    .0    .0
 50.  *    .0    .2    .2    .2    .1    .1    .0    .1
 55.  *    .0    .2    .2    .2    .1    .1    .0    .1
 60.  *    .0    .2    .2    .2    .0    .1    .0    .1
 65.  *    .0    .2    .2    .2    .0    .1    .0    .1
 70.  *    .0    .2    .2    .2    .0    .1    .0    .1
 75.  *    .0    .2    .2    .1    .0    .1    .0    .1
 80.  *    .0    .2    .2    .1    .1    .1    .1    .1
 85.  *    .0    .2    .2    .1    .1    .1    .1    .1
 90.  *    .0    .1    .1    .0    .0    .1    .1    .1
 95.  *    .1    .1    .0    .0    .0    .1    .1    .1
100.  *    .1    .0    .0    .0    .0    .1    .1    .1
105.  *    .1    .0    .0    .0    .0    .1    .1    .1
110.  *    .1    .0    .0    .0    .0    .1    .1    .2
115.  *    .2    .0    .0    .0    .0    .1    .1    .2
120.  *    .2    .0    .0    .0    .0    .1    .1    .2
125.  *    .2    .0    .0    .0    .1    .1    .1    .2
130.  *    .1    .0    .0    .0    .1    .1    .1    .2
135.  *    .1    .0    .0    .0    .1    .1    .1    .1
140.  *    .1    .0    .0    .0    .1    .0    .0    .1
145.  *    .1    .0    .0    .0    .0    .0    .0    .1
150.  *    .1    .0    .0    .0    .0    .0    .0    .1
155.  *    .1    .0    .0    .0    .0    .0    .0    .1
160.  *    .1    .0    .0    .0    .0    .0    .0    .0
165.  *    .1    .0    .0    .0    .0    .0    .0    .0
170.  *    .1    .0    .0    .0    .0    .0    .0    .0
175.  *    .1    .0    .0    .0    .0    .0    .0    .0
180.  *    .1    .0    .0    .0    .0    .0    .0    .0
185.  *    .1    .0    .0    .0    .0    .0    .0    .0
190.  *    .1    .0    .0    .0    .0    .0    .0    .0
195.  *    .1    .0    .0    .0    .0    .0    .0    .0
200.  *    .1    .0    .0    .0    .0    .0    .0    .0
205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE  6
     JOB: Site 5 Olymp & La Brea (S5M1PM.DAT)                 RUN: Site 5 MOS 1 PM

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
------*------------------------------------------------
210.  *    .1    .0    .0    .0    .0    .0    .0    .0
215.  *    .1    .0    .0    .0    .0    .0    .0    .0
220.  *    .1    .0    .0    .0    .0    .0    .0    .0
225.  *    .1    .0    .0    .0    .0    .0    .0    .0
230.  *    .1    .0    .0    .0    .0    .0    .0    .0
235.  *    .2    .0    .0    .0    .0    .0    .0    .0
240.  *    .2    .0    .0    .0    .0    .0    .0    .0
245.  *    .2    .0    .0    .0    .0    .0    .0    .0
250.  *    .2    .0    .0    .0    .0    .0    .0    .0
255.  *    .2    .0    .0    .0    .0    .0    .0    .0
260.  *    .2    .0    .0    .0    .0    .0    .0    .0
265.  *    .2    .2    .1    .1    .1    .0    .0    .0
270.  *    .2    .2    .2    .1    .1    .0    .0    .0
275.  *    .0    .2    .2    .1    .2    .0    .0    .0
280.  *    .0    .2    .2    .1    .2    .0    .0    .0
285.  *    .0    .2    .2    .2    .2    .0    .0    .0
290.  *    .0    .2    .2    .2    .2    .0    .0    .0
295.  *    .0    .2    .2    .2    .2    .0    .0    .0
300.  *    .0    .2    .1    .2    .2    .0    .0    .0
305.  *    .0    .2    .1    .2    .2    .0    .0    .0
310.  *    .0    .2    .1    .2    .2    .0    .0    .0
315.  *    .0    .2    .1    .2    .2    .0    .0    .0
320.  *    .0    .2    .1    .2    .2    .0    .0    .0
325.  *    .0    .2    .1    .2    .2    .0    .0    .0
330.  *    .0    .2    .1    .2    .1    .0    .0    .1
335.  *    .0    .2    .2    .2    .1    .0    .0    .1
340.  *    .0    .2    .2    .2    .1    .0    .0    .1
345.  *    .0    .2    .2    .2    .1    .0    .1    .1
350.  *    .0    .2    .2    .2    .1    .0    .1    .1
355.  *    .0    .2    .2    .2    .1    .0    .1    .1
360.  *    .0    .2    .2    .2    .1    .0    .1    .2
------*------------------------------------------------
MAX   *    .2    .2    .2    .2    .2    .1    .1    .2
DEGR. *  115     0     0     0    20     5     0     0

THE HIGHEST CONCENTRATION IS     .30 PPM AT   25 DEGREES FROM REC16.
THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  165 DEGREES FROM REC2 .
THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  225 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5M2AM.DAT)                  RUN: Site 5 MOS 2 AM
      DATE: 03/19/2010   TIME: 12:16:43.70


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2    *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*-----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   1580.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   1580.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0     -90.0    1050.0 *     634.   272. AG     28. 100.0    .0 48.0 1.11  32.2
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   1583.    .9    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   1900.    .9    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   1900.    .9    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0     917.8    1058.7 *     223.    91. AG     23. 100.0    .0 48.0  .98  11.3
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   2025.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   2071.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   2071.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   2071.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   1950.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   1950.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    1777.1   -1682.2 *    2881.   157. AG     22. 100.0    .0 36.0 1.63 146.3
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG    121.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG    121.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     744.5     713.7 *     284.   156. AG     10. 100.0    .0 12.0 1.16  14.4
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   2119.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   2119.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   2119.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   2342.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   2204.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   2204.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1111.7    4737.3 *    3655.     8. AG     22. 100.0    .0 36.0 1.80 185.7
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    138.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    138.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     724.5    1862.2 *     752.     8. AG      6. 100.0    .0 12.0 1.86  38.2
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   2166.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   2166.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   2166.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   2166.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   2166.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   2166.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5M2AM.DAT)                  RUN: Site 5 MOS 2 AM
      DATE: 03/19/2010   TIME: 12:16:43.70

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE  EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)   (gm/hr)
      ------------------------*---------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       64       2.0      1580       1110       4.10      1        3
       7. WB        Oly AP Q  *     100       52       2.0      1900       1103       4.10      1        3
      14. NB        Brea T+R Q*     100       68       2.0      1950       1423       4.10      1        3
      17. NB        Brea LT Q *     100       89       2.0       121       1490       4.10      1        3
      24. SB        Brea T+R Q*     100       67       2.0      2204       1409       4.10      1        3
      27. SB        Brea LT Q *     100       58       2.0       138        196       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5M2AM.DAT)                  RUN: Site 5 MOS 2 AM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND   * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .3    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
  95.  *    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .2    .2    .0    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 130.  *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
 135.  *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
 140.  *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .1    .2    .0    .1    .2
 145.  *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .2
 150.  *    .1    .0    .1    .0    .0    .0    .0    .1    .1    .2    .0    .0    .0    .0    .1    .1    .2    .0    .1    .2
 155.  *    .1    .0    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .2    .0    .0    .2
 160.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .1    .1    .2    .0    .0    .1
 165.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 170.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .1    .2
 175.  *    .1    .2    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 180.  *    .1    .2    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 185.  *    .1    .2    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 190.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 195.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1
 200.  *    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .0    .0    .0    .1    .1
 205.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .1    .1    .0    .0    .0    .1    .1
1
                                                                                                                PAGE  4
      JOB: Site 5 Olymp & La Brea (S5M2AM.DAT)                  RUN: Site 5 MOS 2 AM

 WIND   * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
 215.  *    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
 220.  *    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .0    .1    .1    .0    .0    .1    .2    .2
 225.  *    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2    .1    .1    .0    .1    .1    .0    .0    .2    .2    .2
 230.  *    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 235.  *    .0    .0    .2    .0    .0    .0    .0    .1    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 240.  *    .0    .0    .2    .0    .0    .0    .0    .1    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 245.  *    .1    .0    .2    .0    .0    .0    .0    .1    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 250.  *    .1    .0    .2    .0    .0    .0    .0    .1    .2    .1    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 255.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 260.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .1    .1    .1
 265.  *    .1    .0    .1    .0    .0    .0    .0    .0    .2    .0    .1    .0    .0    .1    .1    .0    .0    .1    .1    .1
 270.  *    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .1    .1    .0    .0    .1    .1    .1
 275.  *    .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .1
 280.  *    .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 285.  *    .1    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .1    .1    .1    .1    .2    .2    .2    .2    .1    .1    .1    .3    .2    .2    .2    .2    .2
 DEGR. *   130   175   235    55    45    45    45   255   160   100   105     0     0     0    10    30    70    35   175   130

1
                                                                                                                PAGE  5
      JOB: Site 5 Olymp & La Brea (S5M2AM.DAT)                  RUN: Site 5 MOS 2 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
```

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                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .1    .1
   5.  *    .0    .1    .1    .1    .1    .0    .1    .1
  10.  *    .0    .1    .1    .1    .1    .0    .1    .1
  15.  *    .0    .1    .1    .1    .1    .1    .1    .1
  20.  *    .0    .1    .1    .1    .0    .1    .1    .1
  25.  *    .0    .1    .1    .1    .0    .1    .0    .1
  30.  *    .0    .1    .1    .1    .1    .1    .0    .1
  35.  *    .0    .1    .1    .1    .1    .1    .0    .1
  40.  *    .0    .1    .1    .1    .1    .1    .0    .1
  45.  *    .0    .1    .1    .1    .1    .0    .0    .0
  50.  *    .0    .1    .1    .1    .0    .0    .0    .1
  55.  *    .0    .1    .1    .1    .0    .0    .0    .0
  60.  *    .0    .1    .1    .1    .0    .1    .0    .0
  65.  *    .0    .1    .1    .1    .0    .1    .0    .1
  70.  *    .0    .1    .1    .1    .0    .1    .0    .1
  75.  *    .0    .1    .1    .0    .0    .1    .0    .1
  80.  *    .0    .1    .1    .0    .0    .1    .0    .2
  85.  *    .0    .1    .1    .0    .0    .0    .0    .2
  90.  *    .1    .1    .0    .0    .0    .0    .1    .1
  95.  *    .1    .1    .0    .0    .0    .0    .1    .2
 100.  *    .1    .0    .0    .0    .0    .1    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .1    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .1    .1    .2
 130.  *    .2    .0    .0    .0    .0    .0    .1    .2
 135.  *    .2    .0    .0    .0    .0    .0    .0    .1
 140.  *    .2    .0    .0    .0    .0    .0    .0    .1
 145.  *    .2    .0    .0    .0    .0    .0    .0    .1
 150.  *    .2    .0    .0    .0    .0    .0    .0    .1
 155.  *    .2    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .2    .0    .0    .0    .0    .0    .0    .0
 175.  *    .2    .0    .0    .0    .0    .0    .0    .0
 180.  *    .2    .0    .0    .0    .0    .0    .0    .0
 185.  *    .2    .0    .0    .0    .0    .0    .0    .0
 190.  *    .2    .0    .0    .0    .0    .0    .0    .0
 195.  *    .2    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                         PAGE  6
      JOB: Site 5 Olymp & La Brea (S5M2AM.DAT)                  RUN: Site 5 MOS 2 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .1    .0    .0    .0    .0    .0    .0    .0
 260.  *    .1    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .0    .0    .0    .0    .0    .0    .0
 270.  *    .1    .1    .1    .1    .1    .0    .0    .0
 275.  *    .1    .2    .1    .1    .1    .0    .0    .0
 280.  *    .0    .2    .1    .1    .1    .0    .0    .0
 285.  *    .0    .2    .1    .1    .1    .0    .0    .0
 290.  *    .0    .2    .1    .1    .1    .0    .0    .0
 295.  *    .0    .2    .1    .1    .1    .0    .0    .0
 300.  *    .0    .2    .1    .1    .1    .0    .0    .0
 305.  *    .0    .2    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .0    .0    .0    .0
 335.  *    .0    .1    .1    .1    .0    .0    .0    .1
 340.  *    .0    .1    .1    .1    .0    .0    .0    .1
 345.  *    .0    .1    .1    .1    .0    .0    .0    .1
 350.  *    .0    .1    .1    .1    .0    .0    .1    .1
 355.  *    .0    .1    .1    .1    .0    .0    .1    .1
 360.  *    .0    .1    .1    .1    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .2    .2    .1    .1    .1    .1    .1    .2
 DEGR. *  115   275     0     0     5    15     0    80

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  175 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  235 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 5 Olymp & La Brea (S5M2PM.DAT)                  RUN: Site 5 MOS 2 PM
      DATE: 03/19/2010   TIME: 12:25:06.55


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   2286.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   2286.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0   -2374.1    1114.9 *    2919.   272. AG     30. 100.0    .0 48.0 1.83 148.3
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   2151.    .8    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   1487.    .8    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   1487.    .8    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0     835.2    1060.6 *     140.    91. AG     25. 100.0    .0 48.0  .86   7.1
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   1533.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   2206.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   2206.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   2206.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   2161.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   2161.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    1833.1   -1814.8 *    3025.   157. AG     21. 100.0    .0 36.0 1.58 153.7
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG     45.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG     45.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     640.8     944.6 *      31.   156. AG     10. 100.0    .0 12.0  .76   1.6
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   2567.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   2567.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   2567.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   2684.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   2495.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   2495.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1087.7    4571.0 *    3487.     8. AG     19. 100.0    .0 36.0 1.59 177.1
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    189.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    189.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     806.8    2416.3 *    1313.     8. AG      5. 100.0    .0 12.0 2.63  66.7
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   2412.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   2412.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   2412.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   2412.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   2412.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   2412.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5M2PM.DAT)                  RUN: Site 5 MOS 2 PM
      DATE: 03/19/2010   TIME: 12:25:06.55

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       68       2.0      2286       1117       4.10      1        3
       7. WB        Oly AP Q  *     100       57       2.0      1487       1101       4.10      1        3
      14. NB        Brea T+R Q*     100       64       2.0      2161       1423       4.10      1        3
      17. NB        Brea LT Q *     100       92       2.0        45       1490       4.10      1        3
      24. SB        Brea T+R Q*     100       59       2.0      2495       1412       4.10      1        3
      27. SB        Brea LT Q *     100       50       2.0       189        158       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5M2PM.DAT)                  RUN: Site 5 MOS 2 PM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .0    .0    .0
  10.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .2    .3    .1    .2    .0    .0
  30.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .3    .1    .2    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  95.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .2
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
 150.  *    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
 155.  *    .1    .0    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .1    .0    .1    .1
 160.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 165.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 170.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .1    .0    .1    .1
 175.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 180.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 185.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 190.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 195.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .2    .0    .0    .0    .1    .1
 200.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
 205.  *    .1    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
1
                                                                                                                     PAGE  4
      JOB: Site 5 Olymp & La Brea (S5M2PM.DAT)                 RUN: Site 5 MOS 2 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 215.  *    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 220.  *    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 225.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 230.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 235.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .1    .2
 240.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 245.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 250.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .2    .2    .2
 255.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 260.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 265.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 270.  *    .1    .1    .2    .1    .0    .1    .1    .0    .0    .0    .2    .1    .1    .1    .1    .0    .0    .1    .2    .2
 275.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0
 280.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 285.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .1    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .2    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .2    .3    .2    .2    .2    .2
 DEGR. *  130   165   225   190     0     0     0    90   210   110   255     0     0     0    10    25    50    25   240   125

1
                                                                                                                     PAGE  5
      JOB: Site 5 Olymp & La Brea (S5M2PM.DAT)                 RUN: Site 5 MOS 2 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
```

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                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .2    .2    .2    .1    .0    .1    .2
   5.  *    .0    .2    .2    .2    .1    .1    .1    .2
  10.  *    .0    .2    .2    .2    .1    .1    .1    .1
  15.  *    .0    .2    .2    .2    .1    .1    .1    .1
  20.  *    .0    .2    .2    .2    .1    .1    .1    .1
  25.  *    .0    .2    .2    .2    .1    .1    .1    .1
  30.  *    .0    .2    .2    .2    .1    .1    .0    .0
  35.  *    .0    .2    .2    .2    .1    .1    .0    .0
  40.  *    .0    .2    .2    .2    .1    .1    .0    .0
  45.  *    .0    .2    .2    .2    .1    .1    .0    .0
  50.  *    .0    .2    .2    .2    .1    .1    .0    .1
  55.  *    .0    .2    .2    .2    .1    .1    .0    .1
  60.  *    .0    .2    .2    .2    .0    .1    .0    .1
  65.  *    .0    .2    .2    .2    .0    .1    .0    .1
  70.  *    .0    .2    .2    .2    .0    .1    .0    .1
  75.  *    .0    .2    .2    .1    .0    .1    .0    .1
  80.  *    .0    .2    .2    .1    .1    .1    .1    .1
  85.  *    .0    .2    .2    .0    .1    .1    .1    .1
  90.  *    .0    .1    .1    .0    .0    .1    .1    .1
  95.  *    .1    .1    .0    .0    .0    .1    .1    .1
 100.  *    .1    .0    .0    .0    .0    .1    .1    .1
 105.  *    .1    .0    .0    .0    .0    .1    .1    .1
 110.  *    .2    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .1    .1    .1    .2
 130.  *    .1    .0    .0    .0    .1    .1    .1    .2
 135.  *    .1    .0    .0    .0    .1    .1    .1    .1
 140.  *    .1    .0    .0    .0    .1    .0    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .1
 150.  *    .1    .0    .0    .0    .0    .0    .0    .1
 155.  *    .1    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                              PAGE  6
      JOB: Site 5 Olymp & La Brea (S5M2PM.DAT)                  RUN: Site 5 MOS 2 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .2    .0    .0    .0    .0    .0    .0    .0
 265.  *    .2    .2    .1    .1    .1    .0    .0    .0
 270.  *    .2    .2    .1    .1    .1    .0    .0    .0
 275.  *    .0    .2    .2    .1    .2    .0    .0    .0
 280.  *    .0    .2    .2    .1    .2    .0    .0    .0
 285.  *    .0    .2    .2    .2    .2    .1    .0    .0
 290.  *    .0    .2    .2    .2    .2    .1    .0    .0
 295.  *    .0    .2    .1    .2    .2    .0    .0    .0
 300.  *    .0    .2    .1    .2    .2    .0    .0    .0
 305.  *    .0    .2    .1    .2    .2    .0    .0    .0
 310.  *    .0    .2    .1    .2    .2    .0    .0    .0
 315.  *    .0    .2    .1    .2    .2    .0    .0    .0
 320.  *    .0    .2    .1    .2    .2    .0    .0    .0
 325.  *    .0    .2    .1    .2    .2    .0    .0    .0
 330.  *    .0    .2    .1    .2    .2    .0    .0    .1
 335.  *    .0    .2    .1    .2    .1    .0    .0    .1
 340.  *    .0    .2    .2    .2    .1    .0    .0    .1
 345.  *    .0    .2    .2    .2    .1    .0    .1    .1
 350.  *    .0    .2    .2    .2    .1    .0    .1    .1
 355.  *    .0    .2    .2    .2    .1    .0    .1    .1
 360.  *    .0    .2    .2    .2    .1    .0    .1    .2
 ------*------------------------------------------------
 MAX   *    .2    .2    .2    .2    .2    .1    .1    .2
 DEGR. *  110     0     0     0   275     5     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   25 DEGREES FROM REC16.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  165 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  225 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5B1AM.DAT)                  RUN: Site 5 Build 1 AM
      DATE: 03/19/2010   TIME: 12:37:37.10


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *   LENGTH  BRG TYPE     VPH   EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*---------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   1590.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   1590.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0    -335.0    1057.0 *     879.   272. AG     29. 100.0    .0 48.0 1.19  44.7
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   1612.    .9    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   1948.    .9    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   1948.    .9    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0    1287.6    1049.8 *     593.    91. AG     24. 100.0    .0 48.0 1.08  30.1
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   2060.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   2040.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   2040.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   2040.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   1944.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   1944.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    1769.0   -1662.9 *    2860.   157. AG     22. 100.0    .0 36.0 1.63 145.3
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG     96.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG     96.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     652.5     918.4 *      60.   156. AG     10. 100.0    .0 12.0  .81   3.0
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   2107.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   2107.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   2107.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   2343.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   2185.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   2185.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1082.1    4532.0 *    3447.     8. AG     22. 100.0    .0 36.0 1.73 175.1
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    158.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    158.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     747.9    2019.5 *     911.     8. AG      6. 100.0    .0 12.0 2.00  46.3
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   2142.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   2142.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   2142.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   2142.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   2142.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   2142.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5B1AM.DAT)                  RUN: Site 5 Build 1 AM
      DATE: 03/19/2010   TIME: 12:37:37.10

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       66       2.0      1590       1112       4.10      1        3
       7. WB        Oly AP Q  *     100       55       2.0      1948       1106       4.10      1        3
      14. NB        Brea T+R Q*     100       68       2.0      1944       1422       4.10      1        3
      17. NB        Brea LT Q *     100       88       2.0        96       1490       4.10      1        3
      24. SB        Brea T+R Q*     100       66       2.0      2185       1408       4.10      1        3
      27. SB        Brea LT Q *     100       54       2.0       158        189       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5B1AM.DAT)                  RUN: Site 5 Build 1 AM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*--------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .3    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  55.  *    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0
  60.  *    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
  95.  *    .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 130.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
 135.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
 140.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .1    .2    .0    .1    .2
 145.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .2
 150.  *    .1    .0    .1    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .2
 155.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .1    .1    .2    .0    .2    .2
 160.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .1    .1    .2    .0    .1    .2
 165.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .1    .1    .1    .0    .1    .2
 170.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 175.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 180.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .0    .2    .2
 185.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .0    .2    .2
 190.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .0    .2    .2
 195.  *    .0    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .1    .1    .0    .0    .2    .2
 200.  *    .0    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2
 205.  *    .0    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2
1
                                                                                                                        PAGE  4
      JOB: Site 5 Olymp & La Brea (S5B1AM.DAT)                  RUN: Site 5 Build 1 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*--------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
 215.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .1    .2    .2
 220.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 225.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 230.  *    .0    .1    .1    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 235.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 240.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 245.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 250.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 255.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 260.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 265.  *    .1    .0    .1    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0    .1    .1    .0    .0    .1    .1    .1
 270.  *    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .1    .0    .1    .1    .0    .0    .1    .1    .1
 275.  *    .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .1
 280.  *    .1    .1    .2    .1    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1
 285.  *    .1    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .0    .0    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 ------*--------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .1    .2    .2    .1    .2    .2    .2    .2    .1    .1    .1    .3    .2    .2    .2    .2    .2
 DEGR. *   130   175   235    55    60    55    45    90    95   100   100     0     0     0    10    30    70    35   155   130

1
                                                                                                                        PAGE  5
      JOB: Site 5 Olymp & La Brea (S5B1AM.DAT)                  RUN: Site 5 Build 1 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
```

```
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .1    .1
   5.  *    .0    .1    .1    .1    .0    .0    .1    .1
  10.  *    .0    .1    .1    .1    .1    .0    .1    .1
  15.  *    .0    .1    .1    .1    .0    .1    .1    .1
  20.  *    .0    .1    .1    .1    .0    .1    .0    .1
  25.  *    .0    .1    .1    .1    .0    .1    .0    .1
  30.  *    .0    .1    .1    .1    .1    .1    .0    .1
  35.  *    .0    .1    .1    .1    .1    .1    .0    .1
  40.  *    .0    .1    .1    .1    .1    .0    .0    .1
  45.  *    .0    .1    .1    .1    .0    .0    .0    .0
  50.  *    .0    .1    .1    .1    .0    .0    .0    .1
  55.  *    .0    .1    .1    .1    .0    .0    .0    .0
  60.  *    .0    .1    .1    .1    .0    .1    .0    .0
  65.  *    .0    .1    .1    .1    .0    .1    .0    .0
  70.  *    .0    .1    .1    .1    .0    .1    .0    .1
  75.  *    .0    .1    .1    .0    .0    .1    .0    .1
  80.  *    .0    .1    .1    .0    .0    .1    .0    .2
  85.  *    .1    .1    .1    .0    .0    .0    .0    .2
  90.  *    .1    .1    .0    .0    .0    .0    .1    .1
  95.  *    .1    .1    .0    .0    .0    .0    .1    .2
 100.  *    .1    .0    .0    .0    .0    .1    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .1    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .1    .1    .2
 130.  *    .2    .0    .0    .0    .0    .0    .1    .2
 135.  *    .2    .0    .0    .0    .0    .0    .0    .1
 140.  *    .2    .0    .0    .0    .0    .0    .0    .1
 145.  *    .2    .0    .0    .0    .0    .0    .0    .1
 150.  *    .2    .0    .0    .0    .0    .0    .0    .1
 155.  *    .2    .0    .0    .0    .0    .0    .0    .1
 160.  *    .2    .0    .0    .0    .0    .0    .0    .0
 165.  *    .2    .0    .0    .0    .0    .0    .0    .0
 170.  *    .2    .0    .0    .0    .0    .0    .0    .0
 175.  *    .2    .0    .0    .0    .0    .0    .0    .0
 180.  *    .2    .0    .0    .0    .0    .0    .0    .0
 185.  *    .2    .0    .0    .0    .0    .0    .0    .0
 190.  *    .2    .0    .0    .0    .0    .0    .0    .0
 195.  *    .2    .0    .0    .0    .0    .0    .0    .0
 200.  *    .2    .0    .0    .0    .0    .0    .0    .0
 205.  *    .2    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  6
      JOB: Site 5 Olymp & La Brea (S5B1AM.DAT)                  RUN: Site 5 Build 1 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .2    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .1    .1    .1    .1    .0    .0    .0
 270.  *    .1    .1    .1    .1    .1    .0    .0    .0
 275.  *    .1    .2    .1    .1    .1    .0    .0    .0
 280.  *    .0    .2    .1    .1    .1    .0    .0    .0
 285.  *    .0    .2    .1    .1    .1    .0    .0    .0
 290.  *    .0    .2    .1    .1    .1    .0    .0    .0
 295.  *    .0    .2    .1    .1    .1    .0    .0    .0
 300.  *    .0    .2    .1    .1    .1    .0    .0    .0
 305.  *    .0    .2    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .0    .0    .0    .1
 340.  *    .0    .1    .1    .1    .0    .0    .0    .1
 345.  *    .0    .1    .1    .1    .0    .0    .0    .1
 350.  *    .0    .1    .1    .1    .0    .0    .1    .1
 355.  *    .0    .1    .1    .1    .0    .0    .1    .1
 360.  *    .0    .1    .1    .1    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .2    .2    .1    .1    .1    .1    .1    .2
 DEGR. *  115   275     0     0    10    15     0    80

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  175 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  235 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                   PAGE  1

      JOB: Site 5 Olymp & La Brea (S5B1PM.DAT)                  RUN: Site 5 Build 1 PM
      DATE: 03/19/2010   TIME: 12:47:08.38


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   2260.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   2260.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0   -1969.6    1103.4 *    2515.   272. AG     29. 100.0    .0 48.0 1.64 127.7
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   2168.    .8    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   1438.    .8    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   1438.    .8    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0     817.7    1061.1 *     123.    91. AG     25. 100.0    .0 48.0  .82   6.2
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   1541.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   2204.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   2204.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   2204.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   2163.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   2163.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    2065.8   -2366.3 *    3623.   157. AG     22. 100.0    .0 36.0 1.81 184.1
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG     41.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG     41.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     638.5     949.5 *      26.   156. AG     10. 100.0    .0 12.0  .69   1.3
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   2518.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   2518.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   2518.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   2672.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   2483.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   2483.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1103.9    4683.1 *    3600.     8. AG     20. 100.0    .0 36.0 1.63 182.9
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    189.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    189.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     796.1    2344.2 *    1240.     8. AG      6. 100.0    .0 12.0 2.39  63.0
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   2347.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   2347.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   2347.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   2347.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   2347.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   2347.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5B1PM.DAT)                  RUN: Site 5 Build 1 PM
      DATE: 03/19/2010   TIME: 12:47:08.38

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       65        2.0      2260        1115       4.10      1        3
       7. WB        Oly AP Q  *     100       56        2.0      1438        1099       4.10      1        3
      14. NB        Brea T+R Q*     100       68        2.0      2163        1423       4.10      1        3
      17. NB        Brea LT Q *     100       92        2.0        41        1490       4.10      1        3
      24. SB        Brea T+R Q*     100       60        2.0      2483        1409       4.10      1        3
      27. SB        Brea LT Q *     100       51        2.0       189         176       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5B1PM.DAT)                  RUN: Site 5 Build 1 PM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND   * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .0    .0    .0
  10.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .2    .3    .1    .2    .0    .0
  30.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .3    .1    .2    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  95.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
 150.  *    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 155.  *    .1    .0    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 160.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 165.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 170.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .1    .0    .1    .1
 175.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 180.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 185.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 190.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 195.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .2    .0    .0    .0    .1    .1
 200.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
 205.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
1
                                                                                                                PAGE  4
      JOB: Site 5 Olymp & La Brea (S5B1PM.DAT)                  RUN: Site 5 Build 1 PM

 WIND   * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 215.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 220.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 225.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 230.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 235.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .1    .2
 240.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 245.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .2    .2    .2
 250.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .2    .2    .2
 255.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 260.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 265.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 270.  *    .1    .1    .2    .1    .0    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .2    .2
 275.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0
 280.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 285.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .1    .2    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .2    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .2    .3    .2    .2    .2    .2
 DEGR. *  130   165   225   190     0     0     0    90   235   120   255     0     0     0     5    25    50    25   240   235

1
                                                                                                                PAGE  5
      JOB: Site 5 Olymp & La Brea (S5B1PM.DAT)                  RUN: Site 5 Build 1 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
```

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                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .2    .2    .2    .1    .0    .1    .2
   5.  *    .0    .2    .2    .2    .1    .0    .1    .2
  10.  *    .0    .2    .2    .2    .1    .1    .1    .1
  15.  *    .0    .2    .2    .2    .1    .1    .1    .1
  20.  *    .0    .2    .2    .1    .0    .1    .1    .1
  25.  *    .0    .2    .2    .2    .1    .1    .1    .1
  30.  *    .0    .2    .2    .2    .1    .1    .0    .1
  35.  *    .0    .2    .2    .2    .1    .1    .0    .1
  40.  *    .0    .2    .2    .2    .1    .1    .0    .1
  45.  *    .0    .2    .2    .2    .1    .1    .0    .0
  50.  *    .0    .2    .2    .2    .1    .1    .0    .1
  55.  *    .0    .2    .2    .2    .1    .1    .0    .1
  60.  *    .0    .2    .2    .2    .0    .1    .0    .1
  65.  *    .0    .2    .2    .2    .0    .1    .0    .1
  70.  *    .0    .2    .2    .2    .0    .1    .0    .1
  75.  *    .0    .2    .2    .1    .0    .1    .0    .1
  80.  *    .0    .2    .2    .1    .1    .1    .0    .2
  85.  *    .0    .2    .2    .0    .1    .1    .1    .2
  90.  *    .0    .1    .1    .0    .0    .1    .1    .1
  95.  *    .1    .1    .0    .0    .0    .1    .1    .2
 100.  *    .1    .0    .0    .0    .0    .1    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .1    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .1    .1    .2
 130.  *    .1    .0    .0    .0    .1    .1    .1    .2
 135.  *    .1    .0    .0    .0    .1    .0    .1    .1
 140.  *    .1    .0    .0    .0    .1    .0    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .1
 150.  *    .1    .0    .0    .0    .0    .0    .0    .1
 155.  *    .1    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                     PAGE  6
      JOB: Site 5 Olymp & La Brea (S5B1PM.DAT)                  RUN: Site 5 Build 1 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .2    .0    .0    .0    .0    .0    .0    .0
 265.  *    .2    .2    .1    .1    .1    .0    .0    .0
 270.  *    .2    .2    .1    .1    .1    .0    .0    .0
 275.  *    .0    .2    .2    .1    .1    .0    .0    .0
 280.  *    .0    .2    .2    .1    .2    .0    .0    .0
 285.  *    .0    .2    .2    .2    .2    .0    .0    .0
 290.  *    .0    .2    .2    .2    .2    .0    .0    .0
 295.  *    .0    .2    .1    .2    .2    .0    .0    .0
 300.  *    .0    .2    .1    .2    .2    .0    .0    .0
 305.  *    .0    .2    .1    .2    .2    .0    .0    .0
 310.  *    .0    .2    .1    .2    .2    .0    .0    .0
 315.  *    .0    .2    .1    .2    .2    .0    .0    .0
 320.  *    .0    .2    .1    .2    .2    .0    .0    .0
 325.  *    .0    .2    .1    .2    .2    .0    .0    .0
 330.  *    .0    .2    .1    .2    .1    .0    .0    .1
 335.  *    .0    .2    .1    .2    .1    .0    .0    .1
 340.  *    .0    .2    .2    .2    .0    .0    .0    .1
 345.  *    .0    .2    .2    .2    .0    .0    .1    .1
 350.  *    .0    .2    .2    .2    .1    .0    .1    .1
 355.  *    .0    .2    .2    .2    .1    .0    .1    .1
 360.  *    .0    .2    .2    .2    .1    .0    .1    .2
 ------*------------------------------------------------
 MAX   *    .2    .2    .2    .2    .2    .1    .1    .2
 DEGR. *  115     0     0     0   280    10     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   25 DEGREES FROM REC16.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  165 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  225 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5B2AM.DAT)                 RUN: Site 5 Build 2 AM
      DATE: 03/19/2010   TIME: 12:56:42.57


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   1548.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   1548.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0    -230.3    1054.0 *     775.   272. AG     29. 100.0    .0 48.0 1.16   39.4
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   1564.    .9    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   1925.    .9    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   1925.    .9    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0    1113.2    1054.0 *     418.    91. AG     24. 100.0    .0 48.0 1.04   21.3
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   2025.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   2059.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   2059.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   2059.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   1959.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   1959.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    1789.3   -1711.1 *    2912.   157. AG     22. 100.0    .0 36.0 1.64  147.9
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG    100.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG    100.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     654.9     913.0 *      66.   156. AG     10. 100.0    .0 12.0  .84    3.3
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   2119.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   2119.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   2119.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   2326.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   2184.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   2184.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1102.8    4675.2 *    3592.     8. AG     22. 100.0    .0 36.0 1.78  182.5
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    142.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    142.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     724.4    1861.3 *     751.     8. AG      6. 100.0    .0 12.0 1.82   38.2
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   2150.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   2150.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   2150.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   2150.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   2150.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   2150.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5B2AM.DAT)                 RUN: Site 5 Build 2 AM
      DATE: 03/19/2010   TIME: 12:56:42.57

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*-------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       66       2.0      1548       1111       4.10      1        3
       7. WB        Oly AP Q  *     100       54       2.0      1925       1105       4.10      1        3
      14. NB        Brea T+R Q*     100       68       2.0      1959       1423       4.10      1        3
      17. NB        Brea LT Q *     100       88       2.0       100       1490       4.10      1        3
      24. SB        Brea T+R Q*     100       67       2.0      2184       1409       4.10      1        3
      27. SB        Brea LT Q *     100       55       2.0       142        191       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5B2AM.DAT)                 RUN: Site 5 Build 2 AM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .3    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  55.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
  95.  *    .0    .0    .0    .0    .0    .1    .0    .1    .2    .1    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 130.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
 135.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
 140.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .1    .2    .0    .1    .2
 145.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .2
 150.  *    .1    .0    .1    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .2
 155.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .1    .1    .2    .0    .1    .2
 160.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .1    .1    .2    .0    .1    .1
 165.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 170.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .1    .2
 175.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 180.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .0    .2    .2
 185.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .0    .2    .1    .0    .0    .2    .2
 190.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 195.  *    .0    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1
 200.  *    .0    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .1    .1    .0    .0    .0    .1    .1
 205.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .1    .1    .0    .0    .0    .1    .1
1
                                                                                                                  PAGE  4
     JOB: Site 5 Olymp & La Brea (S5B2AM.DAT)                 RUN: Site 5 Build 2 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
 215.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
 220.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 225.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .1    .1    .0    .1    .1    .0    .0    .2    .2    .2
 230.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 235.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 240.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 245.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 250.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 255.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 260.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 265.  *    .1    .1    .1    .0    .0    .0    .0    .1    .2    .0    .1    .0    .0    .1    .1    .0    .0    .1    .1    .1
 270.  *    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .1    .0    .1    .1    .0    .0    .1    .1    .1
 275.  *    .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .1
 280.  *    .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 285.  *    .1    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .1    .1    .1    .1    .2    .2    .2    .2    .1    .1    .1    .3    .2    .2    .2    .2    .2
 DEGR. *  130   175   235    60    50    45    45   100    95   100   100     0     0     0    10    30    70    35   175   130

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                                                                                                                  PAGE  5
     JOB: Site 5 Olymp & La Brea (S5B2AM.DAT)                 RUN: Site 5 Build 2 AM

      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
```

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                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .1    .1
   5.  *    .0    .1    .1    .1    .1    .0    .1    .1
  10.  *    .0    .1    .1    .1    .1    .0    .1    .1
  15.  *    .0    .1    .1    .1    .1    .1    .1    .1
  20.  *    .0    .1    .1    .1    .0    .1    .0    .1
  25.  *    .0    .1    .1    .1    .0    .1    .0    .1
  30.  *    .0    .1    .1    .1    .1    .1    .0    .1
  35.  *    .0    .1    .1    .1    .1    .1    .0    .1
  40.  *    .0    .1    .1    .1    .1    .1    .0    .1
  45.  *    .0    .1    .1    .1    .0    .0    .0    .0
  50.  *    .0    .1    .1    .1    .0    .0    .0    .1
  55.  *    .0    .1    .1    .1    .0    .0    .0    .0
  60.  *    .0    .1    .1    .1    .0    .1    .0    .0
  65.  *    .0    .1    .1    .1    .0    .1    .0    .0
  70.  *    .0    .1    .1    .1    .0    .1    .0    .1
  75.  *    .0    .1    .1    .0    .0    .1    .0    .1
  80.  *    .0    .1    .1    .0    .0    .1    .0    .2
  85.  *    .0    .1    .1    .0    .0    .0    .0    .2
  90.  *    .1    .1    .0    .0    .0    .0    .1    .1
  95.  *    .1    .1    .0    .0    .0    .0    .1    .2
 100.  *    .1    .0    .0    .0    .0    .1    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .1    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .1    .1    .2
 130.  *    .2    .0    .0    .0    .0    .0    .1    .2
 135.  *    .2    .0    .0    .0    .0    .0    .0    .1
 140.  *    .2    .0    .0    .0    .0    .0    .0    .1
 145.  *    .2    .0    .0    .0    .0    .0    .0    .1
 150.  *    .2    .0    .0    .0    .0    .0    .0    .1
 155.  *    .2    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .2    .0    .0    .0    .0    .0    .0    .0
 175.  *    .2    .0    .0    .0    .0    .0    .0    .0
 180.  *    .2    .0    .0    .0    .0    .0    .0    .0
 185.  *    .2    .0    .0    .0    .0    .0    .0    .0
 190.  *    .2    .0    .0    .0    .0    .0    .0    .0
 195.  *    .2    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                PAGE  6
      JOB: Site 5 Olymp & La Brea (S5B2AM.DAT)                 RUN: Site 5 Build 2 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .1    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .0    .0    .1    .0    .0    .0    .0
 270.  *    .1    .1    .1    .1    .1    .0    .0    .0
 275.  *    .1    .2    .1    .1    .1    .0    .0    .0
 280.  *    .0    .2    .1    .1    .1    .0    .0    .0
 285.  *    .0    .2    .1    .1    .1    .0    .0    .0
 290.  *    .0    .2    .1    .1    .1    .0    .0    .0
 295.  *    .0    .2    .1    .1    .1    .0    .0    .0
 300.  *    .0    .2    .1    .1    .1    .0    .0    .0
 305.  *    .0    .2    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .0    .0    .0    .1
 340.  *    .0    .1    .1    .1    .0    .0    .0    .1
 345.  *    .0    .1    .1    .1    .0    .0    .0    .1
 350.  *    .0    .1    .1    .1    .0    .0    .1    .1
 355.  *    .0    .1    .1    .1    .0    .0    .1    .1
 360.  *    .0    .1    .1    .1    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .2    .2    .1    .1    .1    .1    .1    .2
 DEGR. *  115   275     0     0     5    15     0    80

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  175 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  235 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5B2PM.DAT)                 RUN: Site 5 Build 2 PM
      DATE: 03/19/2010   TIME: 13:03:17.54


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   2284.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   2284.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0   -2260.0    1111.7 *    2805.   272. AG     29. 100.0    .0 48.0 1.77 142.5
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   2172.    .8    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   1465.    .8    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   1465.    .8    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0     822.9    1060.9 *     128.    91. AG     25. 100.0    .0 48.0  .83    6.5
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   1487.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   2140.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   2140.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   2140.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   2098.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   2098.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    1976.4   -2154.3 *    3393.   157. AG     22. 100.0    .0 36.0 1.76 172.4
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG     42.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG     42.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     639.0     948.4 *      27.   156. AG     10. 100.0    .0 12.0  .71    1.4
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   2479.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   2479.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   2479.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   2654.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   2470.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   2470.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1117.2    4775.4 *    3693.     8. AG     20. 100.0    .0 36.0 1.67 187.6
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    184.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    184.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     788.3    2291.4 *    1186.     8. AG      6. 100.0    .0 12.0 2.33   60.3
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   2405.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   2405.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   2405.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   2405.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   2405.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   2405.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5B2PM.DAT)                 RUN: Site 5 Build 2 PM
      DATE: 03/19/2010   TIME: 13:03:17.54

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       67       2.0      2284       1117       4.10      1        3
       7. WB        Oly AP Q  *     100       56       2.0      1465       1100       4.10      1        3
      14. NB        Brea T+R Q*     100       68       2.0      2098       1423       4.10      1        3
      17. NB        Brea LT Q *     100       92       2.0        42       1490       4.10      1        3
      24. SB        Brea T+R Q*     100       61       2.0      2470       1414       4.10      1        3
      27. SB        Brea LT Q *     100       51       2.0       184        176       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z        *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5B2PM.DAT)                 RUN: Site 5 Build 2 PM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

WIND ANGLE RANGE:   0.-360.

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
  0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
  5.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .0    .0    .0
 10.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
 15.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
 20.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .1    .0    .0
 25.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .2    .3    .1    .1    .0    .0
 30.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .3    .1    .2    .0    .0
 35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
 40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
 45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
 50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
 55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
 60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
 65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
 70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 90.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 95.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .0
130.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
135.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
140.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
145.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
150.  *    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
155.  *    .1    .0    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .1    .1
160.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
165.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
170.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .1    .0    .1    .1
175.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
180.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
185.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
190.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
195.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .2    .1    .0    .0    .1    .1
200.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
205.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
1
                                                                                                              PAGE  4
     JOB: Site 5 Olymp & La Brea (S5B2PM.DAT)                  RUN: Site 5 Build 2 PM

WIND  * CONCENTRATION
ANGLE *      (PPM)
(DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
------*------------------------------------------------------------------------------------------------------------------------
210.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
215.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
220.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
225.  *    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
230.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
235.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
240.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
245.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
250.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .2    .2    .2
255.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
260.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
265.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
270.  *    .1    .1    .2    .1    .0    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
275.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0
280.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
285.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
290.  *    .1    .2    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
295.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
300.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
305.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
310.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
315.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
320.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
325.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
330.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
340.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
345.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
350.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
355.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
------*------------------------------------------------------------------------------------------------------------------------
MAX   *    .1    .2    .2    .1    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .2    .3    .2    .2    .2    .2
DEGR. *  130   165   230     0     0     0     0    90   225   115   255     0     0     0     0    25    50    30   240   240

1
                                                                                                              PAGE  5
     JOB: Site 5 Olymp & La Brea (S5B2PM.DAT)                  RUN: Site 5 Build 2 PM

      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
```

```
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .2    .2    .2    .1    .0    .1    .2
   5.  *    .0    .2    .2    .2    .1    .0    .1    .2
  10.  *    .0    .2    .2    .2    .1    .1    .1    .1
  15.  *    .0    .2    .2    .2    .1    .1    .1    .1
  20.  *    .0    .2    .2    .2    .1    .1    .1    .1
  25.  *    .0    .2    .2    .2    .1    .1    .1    .1
  30.  *    .0    .2    .2    .2    .1    .1    .0    .1
  35.  *    .0    .2    .2    .2    .1    .1    .0    .1
  40.  *    .0    .2    .2    .2    .1    .1    .0    .1
  45.  *    .0    .2    .2    .2    .1    .1    .0    .0
  50.  *    .0    .2    .2    .2    .1    .1    .0    .2
  55.  *    .0    .2    .2    .2    .1    .1    .0    .1
  60.  *    .0    .2    .2    .2    .0    .1    .0    .1
  65.  *    .0    .2    .2    .2    .0    .1    .0    .1
  70.  *    .0    .2    .2    .2    .0    .1    .0    .1
  75.  *    .0    .2    .2    .1    .0    .1    .0    .1
  80.  *    .0    .2    .2    .1    .1    .1    .1    .2
  85.  *    .0    .2    .2    .0    .1    .1    .1    .2
  90.  *    .0    .1    .1    .0    .0    .1    .1    .1
  95.  *    .1    .1    .0    .0    .0    .1    .1    .2
 100.  *    .1    .0    .0    .0    .0    .1    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .2    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .1    .1    .1    .2
 130.  *    .1    .0    .0    .0    .1    .1    .1    .2
 135.  *    .1    .0    .0    .0    .1    .1    .1    .1
 140.  *    .1    .0    .0    .0    .1    .0    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .1
 150.  *    .1    .0    .0    .0    .0    .0    .0    .1
 155.  *    .1    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                               PAGE  6
      JOB: Site 5 Olymp & La Brea (S5B2PM.DAT)                  RUN: Site 5 Build 2 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .2    .0    .0    .0    .0    .0    .0    .0
 265.  *    .2    .2    .1    .1    .1    .0    .0    .0
 270.  *    .2    .2    .1    .1    .1    .0    .0    .0
 275.  *    .0    .2    .2    .1    .2    .0    .0    .0
 280.  *    .0    .2    .2    .1    .2    .0    .0    .0
 285.  *    .0    .2    .2    .2    .2    .0    .0    .0
 290.  *    .0    .2    .2    .2    .2    .0    .0    .0
 295.  *    .0    .2    .1    .2    .2    .0    .0    .0
 300.  *    .0    .2    .1    .2    .2    .0    .0    .0
 305.  *    .0    .2    .1    .2    .2    .0    .0    .0
 310.  *    .0    .2    .1    .2    .2    .0    .0    .0
 315.  *    .0    .2    .1    .2    .2    .0    .0    .0
 320.  *    .0    .2    .1    .2    .2    .0    .0    .0
 325.  *    .0    .2    .1    .2    .2    .0    .0    .0
 330.  *    .0    .2    .1    .2    .2    .0    .0    .1
 335.  *    .0    .2    .1    .2    .1    .0    .0    .1
 340.  *    .0    .2    .2    .2    .1    .0    .0    .1
 345.  *    .0    .2    .2    .2    .1    .0    .1    .1
 350.  *    .0    .2    .2    .2    .1    .0    .1    .1
 355.  *    .0    .2    .2    .2    .1    .0    .1    .1
 360.  *    .0    .2    .2    .2    .1    .0    .1    .2
 ------*------------------------------------------------
 MAX   *    .2    .2    .2    .2    .2    .1    .1    .2
 DEGR. *  110     0     0     0   275    10     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   25 DEGREES FROM REC16.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  165 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  230 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5B3AM.DAT)                  RUN: Site 5 Build 3 AM
      DATE: 03/19/2010   TIME: 13:12:26.96


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2    *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*-------------------------------------*-----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   1555.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   1555.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0    -272.9    1055.2 *     817.   272. AG     29. 100.0    .0 48.0 1.18  41.5
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   1559.    .9    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   1904.    .9    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   1904.    .9    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0    1001.7    1056.7 *     307.    91. AG     24. 100.0    .0 48.0 1.01  15.6
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   2050.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   2016.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   2016.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   2016.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   1911.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   1911.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    1741.2   -1597.1 *    2788.   157. AG     23. 100.0    .0 36.0 1.62 141.7
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG    105.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG    105.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     653.9     915.4 *      63.   156. AG     10. 100.0    .0 12.0  .80   3.2
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   2084.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   2084.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   2084.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   2342.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   2195.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   2195.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1115.0    4760.0 *    3678.     8. AG     22. 100.0    .0 36.0 1.81 186.8
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    147.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    147.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     732.5    1915.8 *     807.     8. AG      6. 100.0    .0 12.0 1.88  41.0
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   2124.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   2124.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   2124.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   2124.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   2124.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   2124.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5B3AM.DAT)                  RUN: Site 5 Build 3 AM
      DATE: 03/19/2010   TIME: 13:12:26.96

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE  EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*------------------------------------------------------------------------------

       3. EB        Oly AP Q  *     101       67       2.0       1555       1111       4.10      1        3
       7. WB        Oly AP Q  *     101       54       2.0       1904       1104       4.10      1        3
      14. NB        Brea T+R Q*     101       69       2.0       1911       1424       4.10      1        3
      17. NB        Brea LT Q *     101       88       2.0        105       1490       4.10      1        3
      24. SB        Brea T+R Q*     101       68       2.0       2195       1406       4.10      1        3
      27. SB        Brea LT Q *     101       57       2.0        147        197       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)          *
         RECEPTOR             *       X          Y          Z       *
     -------------------------*-------------------------------------*
       1. SE MID S            *       873.0      736.0       5.0    *
       2. SE 164 S            *       771.0      827.0       5.0    *
       3. SE 82 S             *       719.0      893.0       5.0    *
       4. SE CNR              *       695.0      985.0       5.0    *
       5. SE 82 E             *       784.0      990.0       5.0    *
       6. SE 164 E            *       866.0      989.0       5.0    *
       7. SE MID E            *       986.0      986.0       5.0    *
       8. NE MID E            *       977.0     1089.0       5.0    *
       9. NE 164 E            *       844.0     1094.0       5.0    *
      10. NE 82 E             *       762.0     1096.0       5.0    *
      11. NE CNR              *       680.0     1105.0       5.0    *
      12. NE 82 N             *       683.0     1199.0       5.0    *
      13. NE 164 N            *       707.0     1278.0       5.0    *
      14. NE MID N            *       748.0     1407.0       5.0    *
      15. NW MID N            *       646.0     1421.0       5.0    *
      16. NW 164 N            *       592.0     1268.0       5.0    *
      17. NW 82 N             *       569.0     1188.0       5.0    *
      18. NW CNR              *       550.0     1110.0       5.0    *
      19. NW 82 W             *       462.0     1106.0       5.0    *
      20. NW 164 W            *       380.0     1107.0       5.0    *
      21. NW MID W            *       226.0     1111.0       5.0    *
      22. SW MID W            *       220.0     1007.0       5.0    *
      23. SW 164 W            *       395.0     1000.0       5.0    *
      24. SW 82 W             *       478.0      998.0       5.0    *
      25. SW CNR              *       560.0      994.0       5.0    *
      26. SW 82 S             *       594.0      911.0       5.0    *
      27. SW 164 S            *       626.0      834.0       5.0    *
      28. SW MID S            *       709.0      731.0       5.0    *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5B3AM.DAT)                  RUN: Site 5 Build 3 AM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

  WIND ANGLE RANGE:   0.-360.

  WIND  * CONCENTRATION
  ANGLE *      (PPM)
  (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
  ------*------------------------------------------------------------------------------------------------------------------------
    0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
    5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
   10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .3    .1    .1    .1    .0    .0
   15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
   20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0
   25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .1    .0    .0
   30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0
   35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
   40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
   45.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
   50.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
   55.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0
   60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
   65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
   70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
   75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
   80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
   85.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
   90.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
   95.  *    .0    .0    .0    .0    .0    .1    .0    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2    .0    .1    .1
  100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
  105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
  110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
  115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
  120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
  125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
  130.  *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
  135.  *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
  140.  *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .1    .2    .0    .1    .2
  145.  *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .2
  150.  *    .1    .0    .1    .0    .0    .0    .0    .1    .1    .2    .0    .0    .0    .0    .1    .1    .2    .0    .1    .2
  155.  *    .1    .0    .1    .1    .0    .0    .0    .2    .1    .1    .0    .0    .0    .0    .1    .1    .2    .0    .2    .2
  160.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .1    .1    .2    .0    .1    .1
  165.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .2
  170.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
  175.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
  180.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
  185.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
  190.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
  195.  *    .0    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .1    .1    .0    .0    .1    .2
  200.  *    .0    .1    .1    .1    .0    .0    .0    .2    .1    .1    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2
  205.  *    .0    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2
 1
                                                                                                                          PAGE  4
      JOB: Site 5 Olymp & La Brea (S5B3AM.DAT)                 RUN: Site 5 Build 3 AM

  WIND  * CONCENTRATION
  ANGLE *      (PPM)
  (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
  ------*------------------------------------------------------------------------------------------------------------------------
  210.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
  215.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
  220.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .1    .1    .0    .0    .2    .2    .2
  225.  *    .1    .1    .1    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
  230.  *    .0    .1    .1    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
  235.  *    .0    .0    .1    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
  240.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
  245.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
  250.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
  255.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
  260.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
  265.  *    .1    .0    .1    .0    .0    .0    .0    .1    .2    .0    .1    .0    .0    .1    .1    .0    .0    .1    .1    .1
  270.  *    .1    .0    .1    .0    .0    .0    .0    .1    .1    .0    .0    .1    .0    .1    .1    .0    .0    .1    .1    .1
  275.  *    .1    .0    .1    .0    .0    .1    .1    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .1
  280.  *    .1    .0    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .0    .1
  285.  *    .1    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
  290.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
  295.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  300.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
  305.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
  310.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
  315.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
  320.  *    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  325.  *    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
  355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
  360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
  ------*------------------------------------------------------------------------------------------------------------------------
  MAX   *    .1    .1    .2    .1    .1    .1    .1    .2    .2    .2    .2    .1    .1    .1    .3    .2    .2    .2    .2    .2
  DEGR. *  130   160   240    60    50    45    45   155   100   100   105     0     0     0    10    30    70    35   155   130

 1
                                                                                                                          PAGE  5
      JOB: Site 5 Olymp & La Brea (S5B3AM.DAT)                 RUN: Site 5 Build 3 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
```

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                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .1    .1
   5.  *    .0    .1    .1    .1    .1    .0    .1    .1
  10.  *    .0    .1    .1    .1    .1    .0    .1    .1
  15.  *    .0    .1    .1    .1    .1    .0    .1    .1
  20.  *    .0    .1    .1    .1    .0    .1    .0    .1
  25.  *    .0    .1    .1    .1    .0    .1    .0    .1
  30.  *    .0    .1    .1    .1    .0    .1    .0    .1
  35.  *    .0    .1    .1    .1    .1    .1    .0    .1
  40.  *    .0    .1    .1    .1    .0    .0    .0    .1
  45.  *    .0    .1    .1    .1    .0    .0    .0    .1
  50.  *    .0    .1    .1    .1    .0    .0    .0    .1
  55.  *    .0    .1    .1    .1    .0    .0    .0    .1
  60.  *    .0    .1    .1    .1    .0    .1    .0    .0
  65.  *    .0    .1    .1    .1    .0    .1    .0    .0
  70.  *    .0    .1    .1    .1    .0    .1    .0    .1
  75.  *    .0    .1    .1    .0    .0    .1    .0    .1
  80.  *    .0    .1    .1    .0    .0    .1    .0    .2
  85.  *    .1    .1    .1    .0    .0    .0    .0    .2
  90.  *    .1    .1    .0    .0    .0    .0    .1    .2
  95.  *    .1    .1    .0    .0    .0    .0    .1    .2
 100.  *    .1    .0    .0    .0    .0    .0    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .2    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .1    .1    .2
 130.  *    .2    .0    .0    .0    .0    .0    .1    .2
 135.  *    .2    .0    .0    .0    .0    .0    .0    .1
 140.  *    .2    .0    .0    .0    .0    .0    .0    .1
 145.  *    .2    .0    .0    .0    .0    .0    .0    .1
 150.  *    .2    .0    .0    .0    .0    .0    .0    .1
 155.  *    .2    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .2    .0    .0    .0    .0    .0    .0    .0
 170.  *    .2    .0    .0    .0    .0    .0    .0    .0
 175.  *    .2    .0    .0    .0    .0    .0    .0    .0
 180.  *    .2    .0    .0    .0    .0    .0    .0    .0
 185.  *    .2    .0    .0    .0    .0    .0    .0    .0
 190.  *    .2    .0    .0    .0    .0    .0    .0    .0
 195.  *    .2    .0    .0    .0    .0    .0    .0    .0
 200.  *    .2    .0    .0    .0    .0    .0    .0    .0
 205.  *    .2    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                 PAGE  6
      JOB: Site 5 Olymp & La Brea (S5B3AM.DAT)                 RUN: Site 5 Build 3 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .2    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .1    .1    .1    .1    .0    .0    .0
 270.  *    .1    .1    .1    .1    .1    .0    .0    .0
 275.  *    .1    .2    .1    .1    .1    .0    .0    .0
 280.  *    .0    .2    .1    .1    .1    .0    .0    .0
 285.  *    .0    .2    .1    .1    .1    .0    .0    .0
 290.  *    .0    .2    .1    .1    .1    .0    .0    .0
 295.  *    .0    .2    .1    .1    .1    .0    .0    .0
 300.  *    .0    .2    .1    .1    .1    .0    .0    .0
 305.  *    .0    .2    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .0    .0    .0    .1
 340.  *    .0    .1    .1    .1    .0    .0    .0    .1
 345.  *    .0    .1    .1    .1    .0    .0    .0    .1
 350.  *    .0    .1    .1    .1    .0    .0    .1    .1
 355.  *    .0    .1    .1    .1    .0    .0    .1    .1
 360.  *    .0    .1    .1    .1    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .2    .2    .1    .1    .1    .1    .1    .2
 DEGR. *  110   275     0     0     5    20     0    80

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  240 DEGREES FROM REC3 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  155 DEGREES FROM REC8 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5B3PM.DAT)                  RUN: Site 5 Build 3 PM
      DATE: 03/19/2010   TIME: 13:32:02.42


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W   V/C QUEUE
                              *   X1        Y1        X2        Y2    *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.  272. AG  2253.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.   91. AG  2253.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0   -2280.1    1112.2 *    2825.  272. AG    30. 100.0    .0 48.0 1.80 143.5
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.   91. AG  2174.    .8    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.   91. AG  1458.    .8    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.  271. AG  1458.    .8    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0     821.3    1061.0 *     126.   91. AG    25. 100.0    .0 48.0  .83   6.4
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.  272. AG  1491.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.  327. AG  2233.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.  319. AG  2233.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.  308. AG  2233.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.  317. AG  2192.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.  337. AG  2192.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    2102.4   -2453.0 *    3718.  157. AG    22. 100.0    .0 36.0 1.83 188.8
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.  319. AG    41.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.  336. AG    41.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     638.5     949.5 *      26.  156. AG    10. 100.0    .0 12.0  .69   1.3
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.  354. AG  2555.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.   10. AG  2555.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.   20. AG  2555.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.   19. AG  2623.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.  199. AG  2428.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.  188. AG  2428.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1077.2    4498.1 *    3413.    8. AG    20. 100.0    .0 36.0 1.60 173.4
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.  199. AG   195.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.  188. AG   195.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     803.8    2396.1 *    1292.    8. AG     5. 100.0    .0 12.0 2.44  65.6
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.  174. AG  2347.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.  160. AG  2347.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.  143. AG  2347.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.  129. AG  2347.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.  139. AG  2347.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.  148. AG  2347.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5B3PM.DAT)                  RUN: Site 5 Build 3 PM
      DATE: 03/19/2010   TIME: 13:32:02.42

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*---------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       68       2.0      2253       1121       4.10      1        3
       7. WB        Oly AP Q  *     100       56       2.0      1458       1101       4.10      1        3
      14. NB        Brea T+R Q*     100       68       2.0      2192       1423       4.10      1        3
      17. NB        Brea LT Q *     100       92       2.0        41       1490       4.10      1        3
      24. SB        Brea T+R Q*     100       60       2.0      2428       1411       4.10      1        3
      27. SB        Brea LT Q *     100       50       2.0       195        176       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5B3PM.DAT)                  RUN: Site 5 Build 3 PM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .0    .0    .0
  10.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .2    .3    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .3    .1    .2    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  95.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
 150.  *    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 155.  *    .1    .0    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .2    .0    .1    .1
 160.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 165.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 170.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .1    .0    .1    .1
 175.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 180.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 185.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 190.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 195.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .2    .0    .0    .0    .1    .1
 200.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
 205.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
1
                                                                                                                         PAGE  4
     JOB: Site 5 Olymp & La Brea (S5B3PM.DAT)                 RUN: Site 5 Build 3 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 215.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 220.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 225.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 230.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 235.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .1    .1
 240.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 245.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 250.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .2    .2    .2
 255.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 260.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 265.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 270.  *    .1    .1    .2    .1    .0    .1    .1    .0    .0    .0    .2    .1    .1    .1    .1    .0    .0    .1    .2    .2
 275.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0
 280.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 285.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .1    .2    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .2    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .2    .3    .2    .2    .2    .2
 DEGR. *  130   160   225   190     0     0     0    90   230   120   255     0     0     0    10    25    55    30   240   240

1
                                                                                                                         PAGE  5
     JOB: Site 5 Olymp & La Brea (S5B3PM.DAT)                 RUN: Site 5 Build 3 PM

      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
```

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                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .2    .2    .2    .1    .0    .1    .2
   5.  *    .0    .2    .2    .2    .1    .0    .1    .2
  10.  *    .0    .2    .2    .2    .1    .1    .1    .1
  15.  *    .0    .2    .2    .2    .1    .1    .1    .1
  20.  *    .0    .2    .2    .1    .0    .1    .1    .1
  25.  *    .0    .2    .2    .2    .1    .1    .1    .1
  30.  *    .0    .2    .2    .2    .1    .1    .0    .1
  35.  *    .0    .2    .2    .2    .1    .1    .0    .1
  40.  *    .0    .2    .2    .2    .1    .1    .0    .1
  45.  *    .0    .2    .2    .2    .1    .1    .0    .0
  50.  *    .0    .2    .2    .2    .1    .1    .0    .1
  55.  *    .0    .2    .2    .2    .1    .1    .0    .1
  60.  *    .0    .2    .2    .2    .0    .1    .0    .1
  65.  *    .0    .2    .2    .2    .0    .1    .0    .1
  70.  *    .0    .2    .2    .2    .0    .1    .0    .1
  75.  *    .0    .2    .2    .1    .0    .1    .0    .1
  80.  *    .0    .2    .2    .1    .1    .1    .0    .2
  85.  *    .0    .2    .2    .0    .1    .1    .1    .2
  90.  *    .0    .1    .1    .0    .0    .1    .1    .1
  95.  *    .1    .1    .0    .0    .0    .1    .1    .2
 100.  *    .1    .0    .0    .0    .0    .1    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .2    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .1    .1    .2
 130.  *    .1    .0    .0    .0    .1    .1    .1    .2
 135.  *    .1    .0    .0    .0    .1    .0    .1    .1
 140.  *    .1    .0    .0    .0    .1    .0    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .1
 150.  *    .1    .0    .0    .0    .0    .0    .0    .1
 155.  *    .1    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1                                                                                                                             PAGE  6
      JOB: Site 5 Olymp & La Brea (S5B3PM.DAT)                  RUN: Site 5 Build 3 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .2    .0    .0    .0    .0    .0    .0    .0
 265.  *    .2    .2    .1    .1    .1    .0    .0    .0
 270.  *    .2    .2    .1    .1    .1    .0    .0    .0
 275.  *    .0    .2    .2    .1    .1    .0    .0    .0
 280.  *    .0    .2    .2    .1    .2    .0    .0    .0
 285.  *    .0    .2    .2    .2    .2    .0    .0    .0
 290.  *    .0    .2    .2    .2    .2    .1    .0    .0
 295.  *    .0    .2    .1    .2    .2    .0    .0    .0
 300.  *    .0    .2    .1    .2    .2    .0    .0    .0
 305.  *    .0    .2    .1    .2    .2    .0    .0    .0
 310.  *    .0    .2    .1    .2    .2    .0    .0    .0
 315.  *    .0    .2    .1    .2    .2    .0    .0    .0
 320.  *    .0    .2    .1    .2    .2    .0    .0    .0
 325.  *    .0    .2    .1    .2    .2    .0    .0    .0
 330.  *    .0    .2    .1    .2    .2    .0    .0    .1
 335.  *    .0    .2    .1    .2    .1    .0    .0    .1
 340.  *    .0    .2    .2    .1    .0    .0    .0    .1
 345.  *    .0    .2    .2    .1    .0    .0    .1    .1
 350.  *    .0    .2    .2    .2    .1    .0    .1    .1
 355.  *    .0    .2    .2    .2    .1    .0    .1    .1
 360.  *    .0    .2    .2    .2    .1    .0    .1    .2
 ------*------------------------------------------------
 MAX   *    .2    .2    .2    .2    .2    .1    .1    .2
 DEGR. *  110     0     0     0   280    10     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   25 DEGREES FROM REC16.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  160 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  225 DEGREES FROM REC3 .
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1                        CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                    PAGE  1

      JOB: Site 5 Olymp & La Brea (S5B4AM.DAT)                  RUN: Site 5 Build 4 AM
      DATE: 03/19/2010   TIME: 14:33:37.21


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W   V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)           (G/MI)  (FT) (FT)       (VEH)
      ------------------------*--------------------------------------*------------------------------------------------------------
       1. EB       Oly AP    *    354.0    1033.0    -378.0    1053.0 *    732.   272. AG  1578.    .8    .0 56.0
       2. EB       Oly AP    *    353.0    1037.0     623.0    1030.0 *    270.    91. AG  1578.    .8    .0 68.0
       3. EB       Oly AP Q  *    544.0    1032.0     134.3    1043.6 *    410.   272. AG    27. 100.0    .0 48.0 1.05  20.8
       4. EB       Oly DP    *    624.0    1024.0    1617.0    1000.0 *    993.    91. AG  1606.    .9    .0 56.0
       5. WB       Oly AP    *    891.0    1065.0    1622.0    1047.0 *    731.    91. AG  1912.    .9    .0 56.0
       6. WB       Oly AP    *    890.0    1060.0     630.0    1066.0 *    260.   271. AG  1912.    .9    .0 68.0
       7. WB       Oly AP Q  *    695.0    1064.0     887.6    1059.4 *    193.    91. AG    22. 100.0    .0 48.0  .94   9.8
       8. WB       Oly DP    *    628.0    1073.0    -378.0    1100.0 *   1006.   272. AG  2025.    .8    .0 56.0
       9. NB       Brea AP   *   1230.0     261.0    1042.0     547.0 *    342.   327. AG  2060.    .8    .0 56.0
      10. NB       Brea AP   *   1042.0     547.0     981.0     616.0 *     92.   319. AG  2060.    .8    .0 56.0
      11. NB       Brea AP   *    981.0     616.0     795.0     761.0 *    236.   308. AG  2060.    .8    .0 56.0
      12. NB       Brea T+R  *    795.0     760.0     706.0     856.0 *    131.   317. AG  1957.    .8    .0 56.0
      13. NB       Brea T+R  *    706.0     856.0     653.0     980.0 *    135.   337. AG  1957.    .8    .0 56.0
      14. NB       Brea T+R Q*    657.0     972.0    1785.2   -1701.4 *   2902.   157. AG    22. 100.0    .0 36.0 1.64 147.4
      15. NB       Brea LT   *    777.0     742.0     686.0     845.0 *    137.   319. AG   103.    .8    .0 32.0
      16. NB       Brea LT   *    686.0     845.0     625.0     981.0 *    149.   336. AG   103.    .8    .0 32.0
      17. NB       Brea LT Q *    628.0     973.0     727.1     752.3 *    242.   156. AG    10. 100.0    .0 12.0 1.16  12.3
      18. NB       Brea DP   *    653.0     978.0     638.0    1130.0 *    153.   354. AG  2099.    .8    .0 56.0
      19. NB       Brea DP   *    638.0    1130.0     658.0    1238.0 *    110.    10. AG  2099.    .8    .0 56.0
      20. NB       Brea DP   *    658.0    1238.0     933.0    2002.0 *    812.    20. AG  2099.    .8    .0 56.0
      21. SB       Brea AP   *    644.0    1336.0     884.0    2016.0 *    721.    19. AG  2294.    .8    .0 56.0
      22. SB       Brea T+R  *    644.0    1337.0     606.0    1228.0 *    115.   199. AG  2148.    .8    .0 56.0
      23. SB       Brea T+R  *    606.0    1228.0     588.0    1103.0 *    126.   188. AG  2148.    .8    .0 56.0
      24. SB       Brea T+R Q*    590.0    1120.0    1105.5    4694.4 *   3611.     8. AG    22. 100.0    .0 36.0 1.82 183.5
      25. SB       Brea LT   *    665.0    1326.0     629.0    1221.0 *    111.   199. AG   146.    .8    .0 32.0
      26. SB       Brea LT   *    629.0    1221.0     612.0    1105.0 *    117.   188. AG   146.    .8    .0 32.0
      27. SB       Brea LT Q *    614.0    1118.0     740.4    1969.3 *    861.     8. AG     7. 100.0    .0 12.0 2.03  43.7
      28. SB       Brea DP   *    588.0    1102.0     600.0     989.0 *    114.   174. AG  2114.    .8    .0 56.0
      29. SB       Brea DP   *    600.0     989.0     650.0     854.0 *    144.   160. AG  2114.    .8    .0 56.0
      30. SB       Brea DP   *    650.0     854.0     723.0     758.0 *    121.   143. AG  2114.    .8    .0 56.0
      31. SB       Brea DP   *    723.0     758.0     938.0     583.0 *    277.   129. AG  2114.    .8    .0 56.0
      32. SB       Brea DP   *    938.0     583.0    1029.0     479.0 *    138.   139. AG  2114.    .8    .0 56.0
      33. SB       Brea DP   *   1029.0     479.0    1184.0     227.0 *    296.   148. AG  2114.    .8    .0 56.0
1
                                                                                                                PAGE  2
      JOB: Site 5 Olymp & La Brea (S5B4AM.DAT)                  RUN: Site 5 Build 4 AM
      DATE: 03/19/2010   TIME: 14:33:37.21

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *    (SEC)   (SEC)     (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB       Oly AP Q  *     100       62       2.0      1578       1106       4.10      1        3
       7. WB       Oly AP Q  *     100       50       2.0      1912       1101       4.10      1        3
      14. NB       Brea T+R Q*     100       68       2.0      1957       1422       4.10      1        3
      17. NB       Brea LT Q *     100       90       2.0       103       1490       4.10      1        3
      24. SB       Brea T+R Q*     100       68       2.0      2148       1409       4.10      1        3
      27. SB       Brea LT Q *     100       60       2.0       146        202       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*------------------------------------*
      1. SE MID S             *       873.0      736.0       5.0   *
      2. SE 164 S             *       771.0      827.0       5.0   *
      3. SE 82 S              *       719.0      893.0       5.0   *
      4. SE CNR               *       695.0      985.0       5.0   *
      5. SE 82 E              *       784.0      990.0       5.0   *
      6. SE 164 E             *       866.0      989.0       5.0   *
      7. SE MID E             *       986.0      986.0       5.0   *
      8. NE MID E             *       977.0     1089.0       5.0   *
      9. NE 164 E             *       844.0     1094.0       5.0   *
     10. NE 82 E              *       762.0     1096.0       5.0   *
     11. NE CNR               *       680.0     1105.0       5.0   *
     12. NE 82 N              *       683.0     1199.0       5.0   *
     13. NE 164 N             *       707.0     1278.0       5.0   *
     14. NE MID N             *       748.0     1407.0       5.0   *
     15. NW MID N             *       646.0     1421.0       5.0   *
     16. NW 164 N             *       592.0     1268.0       5.0   *
     17. NW 82 N              *       569.0     1188.0       5.0   *
     18. NW CNR               *       550.0     1110.0       5.0   *
     19. NW 82 W              *       462.0     1106.0       5.0   *
     20. NW 164 W             *       380.0     1107.0       5.0   *
     21. NW MID W             *       226.0     1111.0       5.0   *
     22. SW MID W             *       220.0     1007.0       5.0   *
     23. SW 164 W             *       395.0     1000.0       5.0   *
     24. SW 82 W              *       478.0      998.0       5.0   *
     25. SW CNR               *       560.0      994.0       5.0   *
     26. SW 82 S              *       594.0      911.0       5.0   *
     27. SW 164 S             *       626.0      834.0       5.0   *
     28. SW MID S             *       709.0      731.0       5.0   *
1
                                                                                                                PAGE  3
      JOB: Site 5 Olymp & La Brea (S5B4AM.DAT)                  RUN: Site 5 Build 4 AM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .3    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
  95.  *    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .2    .2    .0    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 130.  *    .1    .0    .0    .0    .0    .0    .0    .1    .0    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 135.  *    .1    .0    .0    .0    .0    .0    .0    .1    .0    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
 140.  *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .2
 145.  *    .1    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .1
 150.  *    .1    .0    .1    .0    .0    .0    .0    .1    .1    .2    .0    .0    .0    .0    .1    .1    .2    .0    .1    .1
 155.  *    .1    .0    .1    .1    .0    .0    .0    .1    .1    .2    .0    .0    .0    .0    .1    .1    .2    .0    .0    .2
 160.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .1    .1    .2    .0    .0    .1
 165.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .2    .1    .1    .0    .0    .1
 170.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .0    .2
 175.  *    .1    .2    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 180.  *    .1    .2    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .2    .1    .0    .0    .1    .1
 185.  *    .1    .2    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .2    .1    .0    .0    .1    .1
 190.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .1    .2
 195.  *    .0    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1
 200.  *    .0    .1    .1    .1    .0    .0    .0    .1    .1    .1    .0    .0    .0    .1    .1    .0    .0    .0    .0    .1
 205.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .1    .0    .0    .0    .1    .1    .0    .0    .0    .0    .1
1
                                                                                                                         PAGE  4
      JOB: Site 5 Olymp & La Brea (S5B4AM.DAT)                 RUN: Site 5 Build 4 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .1    .2
 215.  *    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
 220.  *    .1    .1    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .0    .1    .1    .0    .0    .1    .2    .2
 225.  *    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 230.  *    .1    .1    .1    .0    .0    .0    .0    .1    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 235.  *    .0    .0    .2    .0    .0    .0    .0    .1    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 240.  *    .0    .0    .2    .0    .0    .0    .0    .1    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 245.  *    .1    .0    .2    .0    .0    .0    .0    .1    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .1
 250.  *    .1    .0    .2    .0    .0    .0    .0    .1    .2    .1    .0    .1    .0    .1    .1    .0    .0    .1    .1    .1
 255.  *    .1    .0    .2    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0    .1    .1    .0    .0    .1    .1    .1
 260.  *    .1    .0    .1    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0    .1    .1    .0    .0    .1    .1    .1
 265.  *    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .1    .0    .0    .1    .1    .0    .0    .1    .1    .1
 270.  *    .1    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .1    .1    .0    .0    .1    .1    .1
 275.  *    .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .1
 280.  *    .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 285.  *    .1    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .0    .0    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .1    .1    .1    .1    .1    .2    .2    .2    .1    .1    .1    .3    .2    .2    .2    .2    .2
 DEGR. *  130   175   235    55    45    45    45    85   160   105   105     0     0     0    10    30    80    35   215   135

1
                                                                                                                         PAGE  5
      JOB: Site 5 Olymp & La Brea (S5B4AM.DAT)                 RUN: Site 5 Build 4 AM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
```

```
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .1    .1
   5.  *    .0    .1    .1    .1    .1    .0    .1    .1
  10.  *    .0    .1    .1    .1    .1    .0    .1    .1
  15.  *    .0    .1    .1    .1    .1    .0    .1    .1
  20.  *    .0    .1    .1    .1    .0    .1    .0    .1
  25.  *    .0    .1    .1    .1    .0    .1    .0    .1
  30.  *    .0    .1    .1    .1    .0    .1    .0    .1
  35.  *    .0    .1    .1    .1    .0    .1    .0    .1
  40.  *    .0    .1    .1    .1    .0    .0    .0    .1
  45.  *    .0    .1    .1    .1    .0    .0    .0    .0
  50.  *    .0    .1    .1    .1    .0    .0    .0    .1
  55.  *    .0    .1    .1    .1    .0    .0    .0    .0
  60.  *    .0    .1    .1    .1    .0    .1    .0    .0
  65.  *    .0    .1    .1    .1    .0    .1    .0    .0
  70.  *    .0    .1    .1    .0    .0    .1    .0    .1
  75.  *    .0    .1    .1    .0    .0    .1    .0    .1
  80.  *    .0    .1    .1    .0    .0    .1    .0    .2
  85.  *    .0    .1    .1    .0    .0    .0    .0    .2
  90.  *    .1    .1    .0    .0    .0    .0    .1    .1
  95.  *    .1    .1    .0    .0    .0    .0    .1    .2
 100.  *    .1    .0    .0    .0    .0    .0    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .1    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .1    .1    .2
 130.  *    .2    .0    .0    .0    .0    .0    .1    .2
 135.  *    .2    .0    .0    .0    .0    .0    .0    .1
 140.  *    .2    .0    .0    .0    .0    .0    .0    .1
 145.  *    .2    .0    .0    .0    .0    .0    .0    .1
 150.  *    .2    .0    .0    .0    .0    .0    .0    .1
 155.  *    .2    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .2    .0    .0    .0    .0    .0    .0    .0
 175.  *    .2    .0    .0    .0    .0    .0    .0    .0
 180.  *    .2    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .0    .0    .0    .0    .0    .0    .0    .0
 205.  *    .0    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
      JOB: Site 5 Olymp & La Brea (S5B4AM.DAT)                  RUN: Site 5 Build 4 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .1    .0    .0    .0    .0    .0    .0    .0
 245.  *    .1    .0    .0    .0    .0    .0    .0    .0
 250.  *    .1    .0    .0    .0    .0    .0    .0    .0
 255.  *    .1    .0    .0    .0    .0    .0    .0    .0
 260.  *    .1    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .0    .0    .0    .0    .0    .0    .0
 270.  *    .1    .0    .0    .1    .1    .0    .0    .0
 275.  *    .1    .1    .1    .1    .1    .0    .0    .0
 280.  *    .0    .1    .1    .1    .1    .0    .0    .0
 285.  *    .0    .2    .1    .1    .1    .0    .0    .0
 290.  *    .0    .2    .1    .1    .1    .0    .0    .0
 295.  *    .0    .2    .1    .1    .1    .0    .0    .0
 300.  *    .0    .2    .1    .1    .1    .0    .0    .0
 305.  *    .0    .2    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .0    .0    .0    .0
 335.  *    .0    .1    .1    .1    .0    .0    .0    .1
 340.  *    .0    .1    .1    .1    .0    .0    .0    .1
 345.  *    .0    .1    .1    .1    .0    .0    .0    .1
 350.  *    .0    .1    .1    .1    .0    .0    .1    .1
 355.  *    .0    .1    .1    .1    .0    .0    .1    .1
 360.  *    .0    .1    .1    .1    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .2    .2    .1    .1    .1    .1    .1    .2
 DEGR. *  115   285     0     0     5    20     0    80

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  175 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  235 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 5 Olymp & La Brea (S5B4PM.DAT)                 RUN: Site 5 Build 4 PM
      DATE: 03/19/2010   TIME: 14:02:36.33


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*--------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   2244.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   2244.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0   -2155.3    1108.7 *    2700.   272. AG     29. 100.0    .0 48.0 1.74 137.2
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   2159.    .8    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   1464.    .8    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   1464.    .8    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0     822.9    1060.9 *     128.    91. AG     25. 100.0    .0 48.0  .83   6.5
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   1507.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   2251.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   2251.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   2251.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   2208.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   2208.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    2126.8   -2510.8 *    3780.   157. AG     22. 100.0    .0 36.0 1.85 192.0
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG     43.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG     43.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     639.6     947.2 *      28.   156. AG     10. 100.0    .0 12.0  .73   1.4
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   2548.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   2548.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   2548.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   2648.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   2466.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   2466.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1115.7    4765.1 *    3683.     8. AG     20. 100.0    .0 36.0 1.66 187.1
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    182.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    182.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     785.1    2270.3 *    1165.     8. AG      6. 100.0    .0 12.0 2.30  59.2
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   2393.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   2393.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   2393.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   2393.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   2393.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   2393.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5B4PM.DAT)                 RUN: Site 5 Build 4 PM
      DATE: 03/19/2010   TIME: 14:02:36.33

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       67        2.0      2244       1116       4.10      1        3
       7. WB        Oly AP Q  *     100       56        2.0      1464       1101       4.10      1        3
      14. NB        Brea T+R Q*     100       68        2.0      2208       1423       4.10      1        3
      17. NB        Brea LT Q *     100       92        2.0        43       1490       4.10      1        3
      24. SB        Brea T+R Q*     100       61        2.0      2466       1413       4.10      1        3
      27. SB        Brea LT Q *     100       51        2.0       182        176       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *           COORDINATES (FT)           *
         RECEPTOR             *      X          Y          Z         *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0       5.0    *
      2. SE 164 S             *       771.0      827.0       5.0    *
      3. SE 82 S              *       719.0      893.0       5.0    *
      4. SE CNR               *       695.0      985.0       5.0    *
      5. SE 82 E              *       784.0      990.0       5.0    *
      6. SE 164 E             *       866.0      989.0       5.0    *
      7. SE MID E             *       986.0      986.0       5.0    *
      8. NE MID E             *       977.0     1089.0       5.0    *
      9. NE 164 E             *       844.0     1094.0       5.0    *
     10. NE 82 E              *       762.0     1096.0       5.0    *
     11. NE CNR               *       680.0     1105.0       5.0    *
     12. NE 82 N              *       683.0     1199.0       5.0    *
     13. NE 164 N             *       707.0     1278.0       5.0    *
     14. NE MID N             *       748.0     1407.0       5.0    *
     15. NW MID N             *       646.0     1421.0       5.0    *
     16. NW 164 N             *       592.0     1268.0       5.0    *
     17. NW 82 N              *       569.0     1188.0       5.0    *
     18. NW CNR               *       550.0     1110.0       5.0    *
     19. NW 82 W              *       462.0     1106.0       5.0    *
     20. NW 164 W             *       380.0     1107.0       5.0    *
     21. NW MID W             *       226.0     1111.0       5.0    *
     22. SW MID W             *       220.0     1007.0       5.0    *
     23. SW 164 W             *       395.0     1000.0       5.0    *
     24. SW 82 W              *       478.0      998.0       5.0    *
     25. SW CNR               *       560.0      994.0       5.0    *
     26. SW 82 S              *       594.0      911.0       5.0    *
     27. SW 164 S             *       626.0      834.0       5.0    *
     28. SW MID S             *       709.0      731.0       5.0    *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5B4PM.DAT)                 RUN: Site 5 Build 4 PM

       MODEL RESULTS
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       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
                 angle, of the angles with same maximum
                 concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .0    .0    .0
  10.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .2    .3    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .3    .1    .2    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  95.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
 150.  *    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
 155.  *    .1    .0    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .1    .1
 160.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 165.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 170.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .1    .0    .1    .1
 175.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 180.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 185.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 190.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 195.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .2    .1    .0    .0    .1    .1
 200.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
 205.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
1
                                                                                                                        PAGE  4
      JOB: Site 5 Olymp & La Brea (S5B4PM.DAT)                RUN: Site 5 Build 4 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 215.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 220.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 225.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 230.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 235.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .1    .1
 240.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 245.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 250.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .2    .2    .2
 255.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 260.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 265.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 270.  *    .1    .1    .2    .1    .0    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 275.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0
 280.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 285.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .1    .2    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .2    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .2    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .2    .3    .2    .2    .2    .2
 DEGR. *   130   160   225   190     0     0     0    90   225   115   255     0     0     0     0    25    50    30   240   240

1
                                                                                                                        PAGE  5
      JOB: Site 5 Olymp & La Brea (S5B4PM.DAT)                RUN: Site 5 Build 4 PM

       MODEL RESULTS
       -------------

       REMARKS : In search of the angle corresponding to
                 the maximum concentration, only the first
```

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                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .2    .2    .2    .1    .0    .1    .2
   5.  *    .0    .2    .2    .2    .1    .0    .1    .2
  10.  *    .0    .2    .2    .2    .1    .1    .1    .1
  15.  *    .0    .2    .2    .2    .0    .1    .1    .1
  20.  *    .0    .2    .2    .1    .1    .1    .1    .1
  25.  *    .0    .2    .2    .2    .1    .1    .1    .1
  30.  *    .0    .2    .2    .2    .1    .1    .0    .1
  35.  *    .0    .2    .2    .2    .1    .1    .0    .1
  40.  *    .0    .2    .2    .2    .1    .1    .0    .1
  45.  *    .0    .2    .2    .2    .1    .1    .0    .0
  50.  *    .0    .2    .2    .2    .1    .1    .0    .2
  55.  *    .0    .2    .2    .2    .1    .1    .0    .1
  60.  *    .0    .2    .2    .2    .0    .1    .0    .1
  65.  *    .0    .2    .2    .2    .0    .1    .0    .1
  70.  *    .0    .2    .2    .2    .0    .1    .0    .1
  75.  *    .0    .2    .2    .1    .0    .1    .0    .1
  80.  *    .0    .2    .2    .1    .1    .1    .1    .2
  85.  *    .0    .2    .2    .0    .1    .1    .1    .2
  90.  *    .0    .1    .1    .0    .0    .1    .1    .1
  95.  *    .1    .1    .0    .0    .0    .1    .1    .2
 100.  *    .1    .0    .0    .0    .0    .1    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .2    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .1    .1    .2
 130.  *    .1    .0    .0    .0    .1    .1    .1    .2
 135.  *    .1    .0    .0    .0    .1    .1    .1    .1
 140.  *    .1    .0    .0    .0    .1    .0    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .1
 150.  *    .1    .0    .0    .0    .0    .0    .0    .1
 155.  *    .1    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                               PAGE  6
      JOB: Site 5 Olymp & La Brea (S5B4PM.DAT)                 RUN: Site 5 Build 4 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .1    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .2    .0    .0    .0    .0    .0    .0    .0
 265.  *    .2    .2    .1    .1    .1    .0    .0    .0
 270.  *    .2    .2    .1    .1    .1    .0    .0    .0
 275.  *    .0    .2    .2    .1    .1    .0    .0    .0
 280.  *    .0    .2    .2    .1    .2    .0    .0    .0
 285.  *    .0    .2    .2    .2    .2    .0    .0    .0
 290.  *    .0    .2    .2    .2    .2    .0    .0    .0
 295.  *    .0    .2    .1    .2    .2    .0    .0    .0
 300.  *    .0    .2    .1    .2    .2    .0    .0    .0
 305.  *    .0    .2    .1    .2    .2    .0    .0    .0
 310.  *    .0    .2    .1    .2    .2    .0    .0    .0
 315.  *    .0    .2    .1    .2    .2    .0    .0    .0
 320.  *    .0    .2    .1    .2    .2    .0    .0    .0
 325.  *    .0    .2    .1    .2    .2    .0    .0    .0
 330.  *    .0    .2    .1    .2    .2    .0    .0    .1
 335.  *    .0    .2    .1    .2    .1    .0    .0    .1
 340.  *    .0    .2    .1    .1    .0    .0    .0    .1
 345.  *    .0    .2    .2    .1    .0    .0    .1    .1
 350.  *    .0    .2    .2    .2    .1    .0    .1    .1
 355.  *    .0    .2    .2    .2    .1    .0    .1    .1
 360.  *    .0    .2    .2    .2    .1    .0    .1    .2
 ------*------------------------------------------------
 MAX   *    .2    .2    .2    .2    .2    .1    .1    .2
 DEGR. *  110     0     0     0   280    10     0     0

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   25 DEGREES FROM REC16.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  160 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  225 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                     PAGE  1

      JOB: Site 5 Olymp & La Brea (S5B5AM.DAT)                  RUN: Site 5 Build 5 AM
      DATE: 03/19/2010   TIME: 14:28:45.17


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *        LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF      H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.  272. AG   1549.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.   91. AG   1549.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0    -230.3    1054.0 *     775.  272. AG     29. 100.0    .0 48.0 1.16  39.4
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.   91. AG   1559.    .9    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.   91. AG   1904.    .9    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.  271. AG   1904.    .9    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0    1061.4    1055.2 *     367.   91. AG     24. 100.0    .0 48.0 1.03  18.6
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.  272. AG   2022.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.  327. AG   2042.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.  319. AG   2042.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.  308. AG   2042.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.  317. AG   1944.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.  337. AG   1944.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    1825.0   -1795.7 *    3004.  157. AG     23. 100.0    .0 36.0 1.69 152.6
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.  319. AG     98.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.  336. AG     98.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     653.7     915.8 *      63.  156. AG     10. 100.0    .0 12.0  .82   3.2
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.  354. AG   2105.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.   10. AG   2105.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.   20. AG   2105.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.   19. AG   2303.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.  199. AG   2153.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.  188. AG   2153.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1065.7    4418.3 *    3332.    8. AG     22. 100.0    .0 36.0 1.70 169.3
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.  199. AG    150.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.  188. AG    150.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     735.3    1934.9 *     826.    8. AG      6. 100.0    .0 12.0 1.90  42.0
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.  174. AG   2112.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.  160. AG   2112.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.  143. AG   2112.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.  129. AG   2112.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.  139. AG   2112.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.  148. AG   2112.    .8    .0 56.0
1
                                                                                                                 PAGE  2
      JOB: Site 5 Olymp & La Brea (S5B5AM.DAT)                  RUN: Site 5 Build 5 AM
      DATE: 03/19/2010   TIME: 14:28:45.17

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*--------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100        66       2.0      1549       1111       4.10      1        3
       7. WB        Oly AP Q  *     100        54       2.0      1904       1106       4.10      1        3
      14. NB        Brea T+R Q*     100        69       2.0      1944       1424       4.10      1        3
      17. NB        Brea LT Q *     100        88       2.0        98       1490       4.10      1        3
      24. SB        Brea T+R Q*     100        66       2.0      2153       1408       4.10      1        3
      27. SB        Brea LT Q *     100        54       2.0       150        190       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)          *
         RECEPTOR             *      X          Y          Z       *
     -------------------------*------------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                 PAGE  3
      JOB: Site 5 Olymp & La Brea (S5B5AM.DAT)                  RUN: Site 5 Build 5 AM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  10.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .3    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .2    .1    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0
  35.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  55.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
  95.  *    .0    .0    .0    .0    .0    .1    .0    .1    .2    .1    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0    .0    .1    .2    .2    .0    .1    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .2    .2    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .1
 130.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
 135.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .2    .2    .0    .1    .2
 140.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .2    .0    .0    .0    .1    .1    .2    .0    .1    .2
 145.  *    .1    .0    .0    .0    .0    .0    .0    .2    .1    .2    .1    .0    .0    .0    .1    .1    .2    .0    .1    .2
 150.  *    .1    .0    .1    .0    .0    .0    .0    .2    .1    .2    .0    .0    .0    .0    .1    .1    .2    .0    .1    .2
 155.  *    .1    .0    .1    .1    .0    .0    .0    .2    .1    .1    .0    .0    .0    .0    .1    .1    .2    .0    .1    .2
 160.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .1    .1    .2    .0    .1    .1
 165.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 170.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .1    .2
 175.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 180.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 185.  *    .1    .2    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 190.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .0    .0    .0    .2    .1    .0    .0    .2    .2
 195.  *    .0    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1
 200.  *    .0    .1    .1    .1    .0    .0    .0    .2    .1    .1    .0    .0    .0    .1    .1    .0    .0    .0    .1    .1
 205.  *    .0    .1    .1    .1    .0    .0    .0    .2    .2    .1    .0    .0    .0    .1    .1    .0    .0    .0    .1    .1
1
                                                                                                                       PAGE  4
     JOB: Site 5 Olymp & La Brea (S5B5AM.DAT)                RUN: Site 5 Build 5 AM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
 215.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .0    .2    .2
 220.  *    .1    .0    .1    .1    .0    .0    .0    .2    .2    .2    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 225.  *    .1    .1    .1    .1    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 230.  *    .0    .1    .1    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 235.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 240.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 245.  *    .0    .0    .2    .0    .0    .0    .0    .2    .2    .2    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 250.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .0    .1    .0    .1    .1    .0    .0    .2    .2    .2
 255.  *    .1    .0    .2    .0    .0    .0    .0    .2    .2    .1    .0    .0    .0    .1    .1    .0    .0    .2    .2    .2
 260.  *    .1    .0    .1    .0    .0    .0    .0    .2    .2    .1    .1    .0    .0    .1    .1    .0    .0    .2    .2    .2
 265.  *    .1    .0    .1    .0    .0    .0    .0    .1    .2    .0    .1    .0    .0    .1    .1    .0    .0    .1    .1    .1
 270.  *    .1    .1    .1    .0    .0    .0    .0    .1    .1    .0    .0    .1    .0    .1    .1    .0    .0    .1    .1    .1
 275.  *    .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .1
 280.  *    .1    .1    .2    .0    .0    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 285.  *    .1    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .1    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .1    .2    .1    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .1    .1    .1    .1    .2    .2    .2    .2    .1    .1    .1    .3    .2    .2    .2    .2    .2
 DEGR. *  130   175   235    60    50    45    45   105    95   100   105     0     0     0    10    30    80    35   175   130

1
                                                                                                                       PAGE  5
     JOB: Site 5 Olymp & La Brea (S5B5AM.DAT)                RUN: Site 5 Build 5 AM

      MODEL RESULTS
      -------------

      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
```

```
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .1    .1    .1    .0    .0    .1    .1
   5.  *    .0    .1    .1    .1    .0    .0    .1    .1
  10.  *    .0    .1    .1    .1    .1    .0    .1    .1
  15.  *    .0    .1    .1    .1    .0    .0    .1    .1
  20.  *    .0    .1    .1    .1    .0    .1    .0    .1
  25.  *    .0    .1    .1    .1    .0    .1    .0    .1
  30.  *    .0    .1    .1    .1    .0    .1    .0    .1
  35.  *    .0    .1    .1    .1    .0    .1    .0    .1
  40.  *    .0    .1    .1    .1    .0    .0    .0    .1
  45.  *    .0    .1    .1    .1    .0    .0    .0    .1
  50.  *    .0    .1    .1    .1    .0    .0    .0    .1
  55.  *    .0    .1    .1    .1    .0    .0    .0    .1
  60.  *    .0    .1    .1    .1    .0    .1    .0    .1
  65.  *    .0    .1    .1    .1    .0    .1    .0    .0
  70.  *    .0    .1    .1    .1    .0    .1    .0    .1
  75.  *    .0    .1    .1    .0    .0    .1    .0    .2
  80.  *    .0    .1    .1    .0    .0    .0    .0    .2
  85.  *    .0    .1    .1    .0    .0    .0    .0    .2
  90.  *    .1    .1    .0    .0    .0    .0    .1    .2
  95.  *    .1    .1    .0    .0    .0    .0    .1    .2
 100.  *    .1    .0    .0    .0    .0    .0    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .1    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .0    .1    .2
 130.  *    .2    .0    .0    .0    .0    .0    .1    .2
 135.  *    .2    .0    .0    .0    .0    .0    .0    .1
 140.  *    .2    .0    .0    .0    .0    .0    .0    .1
 145.  *    .2    .0    .0    .0    .0    .0    .0    .1
 150.  *    .2    .0    .0    .0    .0    .0    .0    .1
 155.  *    .2    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .2    .0    .0    .0    .0    .0    .0    .0
 175.  *    .2    .0    .0    .0    .0    .0    .0    .0
 180.  *    .2    .0    .0    .0    .0    .0    .0    .0
 185.  *    .2    .0    .0    .0    .0    .0    .0    .0
 190.  *    .2    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                            PAGE  6
      JOB: Site 5 Olymp & La Brea (S5B5AM.DAT)                  RUN: Site 5 Build 5 AM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .2    .0    .0    .0    .0    .0    .0    .0
 215.  *    .2    .0    .0    .0    .0    .0    .0    .0
 220.  *    .2    .0    .0    .0    .0    .0    .0    .0
 225.  *    .2    .0    .0    .0    .0    .0    .0    .0
 230.  *    .2    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .1    .0    .0    .0    .0    .0    .0    .0
 265.  *    .1    .0    .0    .1    .0    .0    .0    .0
 270.  *    .1    .1    .1    .1    .1    .0    .0    .0
 275.  *    .1    .2    .1    .1    .1    .0    .0    .0
 280.  *    .0    .2    .1    .1    .1    .0    .0    .0
 285.  *    .0    .2    .1    .1    .1    .0    .0    .0
 290.  *    .0    .2    .1    .1    .1    .0    .0    .0
 295.  *    .0    .2    .1    .1    .1    .0    .0    .0
 300.  *    .0    .2    .1    .1    .1    .0    .0    .0
 305.  *    .0    .2    .1    .1    .1    .0    .0    .0
 310.  *    .0    .1    .1    .1    .1    .0    .0    .0
 315.  *    .0    .1    .1    .1    .1    .0    .0    .0
 320.  *    .0    .1    .1    .1    .1    .0    .0    .0
 325.  *    .0    .1    .1    .1    .1    .0    .0    .0
 330.  *    .0    .1    .1    .1    .1    .0    .0    .0
 335.  *    .0    .1    .1    .1    .0    .0    .0    .1
 340.  *    .0    .1    .1    .1    .0    .0    .0    .1
 345.  *    .0    .1    .1    .1    .0    .0    .0    .1
 350.  *    .0    .1    .1    .1    .0    .0    .1    .1
 355.  *    .0    .1    .1    .1    .0    .0    .1    .1
 360.  *    .0    .1    .1    .1    .0    .0    .1    .1
 ------*------------------------------------------------
 MAX   *    .2    .2    .1    .1    .1    .1    .1    .2
 DEGR. *  115   275     0     0    10    20     0    75

 THE HIGHEST CONCENTRATION IS     .30 PPM AT   10 DEGREES FROM REC15.
 THE 2ND HIGHEST CONCENTRATION IS     .20 PPM AT  175 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS     .20 PPM AT  235 DEGREES FROM REC3 .
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1                         CAL3QHC: LINE SOURCE DISPERSION MODEL - VERSION 2.2, JUNE 2000                   PAGE  1

      JOB: Site 5 Olymp & La Brea (S5B5PM.DAT)                 RUN: Site 5 Build 5 PM
      DATE: 03/19/2010   TIME: 14:29:03.35


       SITE & METEOROLOGICAL VARIABLES
       -------------------------------
       VS =    .0 CM/S       VD =    .0 CM/S       Z0 = 321. CM
        U =  1.0 M/S         CLAS =   4  (D)     ATIM =  60. MINUTES     MIXH =  1000. M   AMB =   .0 PPM

       LINK VARIABLES
       --------------
         LINK DESCRIPTION     *         LINK COORDINATES (FT)          *    LENGTH  BRG TYPE   VPH    EF     H   W    V/C QUEUE
                              *   X1        Y1        X2        Y2     *     (FT)  (DEG)            (G/MI)  (FT) (FT)       (VEH)
      ------------------------*----------------------------------------*----------------------------------------------------------
       1. EB        Oly AP    *    354.0    1033.0    -378.0    1053.0 *     732.   272. AG   2222.    .8    .0 56.0
       2. EB        Oly AP    *    353.0    1037.0     623.0    1030.0 *     270.    91. AG   2222.    .8    .0 68.0
       3. EB        Oly AP Q  *    544.0    1032.0   -2092.4    1106.9 *    2637.   272. AG     29. 100.0    .0 48.0 1.72 134.0
       4. EB        Oly DP    *    624.0    1024.0    1617.0    1000.0 *     993.    91. AG   2166.    .8    .0 56.0
       5. WB        Oly AP    *    891.0    1065.0    1622.0    1047.0 *     731.    91. AG   1455.    .8    .0 56.0
       6. WB        Oly AP    *    890.0    1060.0     630.0    1066.0 *     260.   271. AG   1455.    .8    .0 68.0
       7. WB        Oly AP Q  *    695.0    1064.0     820.5    1061.0 *     125.    91. AG     25. 100.0    .0 48.0  .82   6.4
       8. WB        Oly DP    *    628.0    1073.0    -378.0    1100.0 *    1006.   272. AG   1515.    .8    .0 56.0
       9. NB        Brea AP   *   1230.0     261.0    1042.0     547.0 *     342.   327. AG   2226.    .8    .0 56.0
      10. NB        Brea AP   *   1042.0     547.0     981.0     616.0 *      92.   319. AG   2226.    .8    .0 56.0
      11. NB        Brea AP   *    981.0     616.0     795.0     761.0 *     236.   308. AG   2226.    .8    .0 56.0
      12. NB        Brea T+R  *    795.0     760.0     706.0     856.0 *     131.   317. AG   2196.    .8    .0 56.0
      13. NB        Brea T+R  *    706.0     856.0     653.0     980.0 *     135.   337. AG   2196.    .8    .0 56.0
      14. NB        Brea T+R Q*    657.0     972.0    2110.6   -2472.3 *    3738.   157. AG     22. 100.0    .0 36.0 1.84 189.9
      15. NB        Brea LT   *    777.0     742.0     686.0     845.0 *     137.   319. AG     30.    .8    .0 32.0
      16. NB        Brea LT   *    686.0     845.0     625.0     981.0 *     149.   336. AG     30.    .8    .0 32.0
      17. NB        Brea LT Q *    628.0     973.0     636.1     955.1 *      20.   156. AG     10. 100.0    .0 12.0  .68   1.0
      18. NB        Brea DP   *    653.0     978.0     638.0    1130.0 *     153.   354. AG   2530.    .8    .0 56.0
      19. NB        Brea DP   *    638.0    1130.0     658.0    1238.0 *     110.    10. AG   2530.    .8    .0 56.0
      20. NB        Brea DP   *    658.0    1238.0     933.0    2002.0 *     812.    20. AG   2530.    .8    .0 56.0
      21. SB        Brea AP   *    644.0    1336.0     884.0    2016.0 *     721.    19. AG   2640.    .8    .0 56.0
      22. SB        Brea T+R  *    644.0    1337.0     606.0    1228.0 *     115.   199. AG   2446.    .8    .0 56.0
      23. SB        Brea T+R  *    606.0    1228.0     588.0    1103.0 *     126.   188. AG   2446.    .8    .0 56.0
      24. SB        Brea T+R Q*    590.0    1120.0    1086.1    4559.7 *    3475.     8. AG     20. 100.0    .0 36.0 1.61 176.5
      25. SB        Brea LT   *    665.0    1326.0     629.0    1221.0 *     111.   199. AG    194.    .8    .0 32.0
      26. SB        Brea LT   *    629.0    1221.0     612.0    1105.0 *     117.   188. AG    194.    .8    .0 32.0
      27. SB        Brea LT Q *    614.0    1118.0     804.0    2397.0 *    1293.     8. AG      6. 100.0    .0 12.0 2.46  65.7
      28. SB        Brea DP   *    588.0    1102.0     600.0     989.0 *     114.   174. AG   2332.    .8    .0 56.0
      29. SB        Brea DP   *    600.0     989.0     650.0     854.0 *     144.   160. AG   2332.    .8    .0 56.0
      30. SB        Brea DP   *    650.0     854.0     723.0     758.0 *     121.   143. AG   2332.    .8    .0 56.0
      31. SB        Brea DP   *    723.0     758.0     938.0     583.0 *     277.   129. AG   2332.    .8    .0 56.0
      32. SB        Brea DP   *    938.0     583.0    1029.0     479.0 *     138.   139. AG   2332.    .8    .0 56.0
      33. SB        Brea DP   *   1029.0     479.0    1184.0     227.0 *     296.   148. AG   2332.    .8    .0 56.0
1
                                                                                                                PAGE  2
      JOB: Site 5 Olymp & La Brea (S5B5PM.DAT)                 RUN: Site 5 Build 5 PM
      DATE: 03/19/2010   TIME: 14:29:03.35

       ADDITIONAL QUEUE LINK PARAMETERS
       --------------------------------
         LINK DESCRIPTION     *    CYCLE    RED     CLEARANCE  APPROACH  SATURATION   IDLE   SIGNAL   ARRIVAL
                              *    LENGTH   TIME    LOST TIME    VOL     FLOW RATE   EM FAC   TYPE     RATE
                              *     (SEC)   (SEC)    (SEC)      (VPH)      (VPH)    (gm/hr)
      ------------------------*---------------------------------------------------------------------------------
       3. EB        Oly AP Q  *     100       67       2.0      2222       1117       4.10      1        3
       7. WB        Oly AP Q  *     100       56       2.0      1455       1101       4.10      1        3
      14. NB        Brea T+R Q*     100       68       2.0      2196       1423       4.10      1        3
      17. NB        Brea LT Q *     100       93       2.0        30       1490       4.10      1        3
      24. SB        Brea T+R Q*     100       60       2.0      2446       1410       4.10      1        3
      27. SB        Brea LT Q *     100       51       2.0       194        176       4.10      1        3

       RECEPTOR LOCATIONS
       ------------------
                              *          COORDINATES (FT)         *
         RECEPTOR             *      X          Y          Z      *
     -------------------------*-------------------------------------*
      1. SE MID S             *       873.0      736.0        5.0   *
      2. SE 164 S             *       771.0      827.0        5.0   *
      3. SE 82 S              *       719.0      893.0        5.0   *
      4. SE CNR               *       695.0      985.0        5.0   *
      5. SE 82 E              *       784.0      990.0        5.0   *
      6. SE 164 E             *       866.0      989.0        5.0   *
      7. SE MID E             *       986.0      986.0        5.0   *
      8. NE MID E             *       977.0     1089.0        5.0   *
      9. NE 164 E             *       844.0     1094.0        5.0   *
     10. NE 82 E              *       762.0     1096.0        5.0   *
     11. NE CNR               *       680.0     1105.0        5.0   *
     12. NE 82 N              *       683.0     1199.0        5.0   *
     13. NE 164 N             *       707.0     1278.0        5.0   *
     14. NE MID N             *       748.0     1407.0        5.0   *
     15. NW MID N             *       646.0     1421.0        5.0   *
     16. NW 164 N             *       592.0     1268.0        5.0   *
     17. NW 82 N              *       569.0     1188.0        5.0   *
     18. NW CNR               *       550.0     1110.0        5.0   *
     19. NW 82 W              *       462.0     1106.0        5.0   *
     20. NW 164 W             *       380.0     1107.0        5.0   *
     21. NW MID W             *       226.0     1111.0        5.0   *
     22. SW MID W             *       220.0     1007.0        5.0   *
     23. SW 164 W             *       395.0     1000.0        5.0   *
     24. SW 82 W              *       478.0      998.0        5.0   *
     25. SW CNR               *       560.0      994.0        5.0   *
     26. SW 82 S              *       594.0      911.0        5.0   *
     27. SW 164 S             *       626.0      834.0        5.0   *
     28. SW MID S             *       709.0      731.0        5.0   *
1
                                                                                                                PAGE  3
      JOB: Site 5 Olymp & La Brea (S5B5PM.DAT)                 RUN: Site 5 Build 5 PM

       MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
   0.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
   5.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .0    .0    .0
  10.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  15.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .1    .1    .1    .0    .0
  20.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .2    .2    .1    .1    .0    .0
  25.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .2    .3    .1    .1    .0    .0
  30.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .3    .1    .2    .0    .0
  35.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  40.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  45.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .2    .0    .0
  50.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .1    .1    .0    .0
  55.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  60.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  65.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .1    .0    .0
  70.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  75.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  80.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  85.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  90.  *    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
  95.  *    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .0
 100.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 105.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 110.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 115.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 120.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 125.  *    .0    .0    .0    .0    .0    .0    .0    .1    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 130.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 135.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .0    .0    .1
 140.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .1    .0    .0    .0    .1    .2    .2    .1    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .1    .0    .1
 150.  *    .1    .0    .1    .0    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .0    .1
 155.  *    .1    .0    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .2    .2    .0    .1    .1
 160.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 165.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1
 170.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .1    .0    .1    .1
 175.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 180.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 185.  *    .1    .2    .1    .1    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 190.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .0    .0    .0    .0    .2    .1    .0    .0    .1    .1
 195.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .2    .0    .0    .0    .1    .1
 200.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
 205.  *    .1    .2    .1    .2    .0    .0    .0    .0    .0    .1    .1    .0    .0    .1    .1    .0    .0    .0    .1    .1
1
                                                                                                                        PAGE  4
     JOB: Site 5 Olymp & La Brea (S5B5PM.DAT)                 RUN: Site 5 Build 5 PM

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC1  REC2  REC3  REC4  REC5  REC6  REC7  REC8  REC9  REC10 REC11 REC12 REC13 REC14 REC15 REC16 REC17 REC18 REC19 REC20
 ------*------------------------------------------------------------------------------------------------------------------------
 210.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 215.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .0    .1    .1
 220.  *    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 225.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 230.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .0    .1    .1    .0    .0    .1    .1    .1
 235.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .1    .2
 240.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 245.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 250.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .1    .1    .1    .1    .1    .1    .0    .0    .2    .2    .2
 255.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 260.  *    .1    .1    .2    .0    .0    .0    .0    .0    .1    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 265.  *    .1    .1    .2    .0    .0    .0    .0    .0    .0    .0    .2    .1    .1    .1    .1    .0    .0    .2    .2    .2
 270.  *    .1    .1    .2    .1    .0    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .1    .2    .2
 275.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0
 280.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 285.  *    .1    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 290.  *    .1    .2    .2    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 295.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 300.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 305.  *    .0    .1    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 310.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 315.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 320.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 325.  *    .0    .0    .2    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 330.  *    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 335.  *    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 340.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 345.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .0
 350.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .0    .0    .0    .0    .0
 355.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
 360.  *    .0    .0    .0    .0    .1    .1    .1    .0    .0    .0    .0    .1    .1    .1    .1    .1    .0    .0    .0    .0
 ------*------------------------------------------------------------------------------------------------------------------------
 MAX   *    .1    .2    .2    .2    .1    .1    .1    .1    .1    .1    .2    .1    .1    .1    .2    .3    .2    .2    .2    .2
 DEGR. *  130   160   225   190     0     0     0    90   230   120   255     0     0     0    10    25    55    30   240   235

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                                                                                                                        PAGE  5
     JOB: Site 5 Olymp & La Brea (S5B5PM.DAT)                 RUN: Site 5 Build 5 PM

      MODEL RESULTS
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      REMARKS : In search of the angle corresponding to
                the maximum concentration, only the first
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                angle, of the angles with same maximum
                concentrations, is indicated as maximum.

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
   0.  *    .0    .2    .2    .2    .1    .0    .1    .2
   5.  *    .0    .2    .2    .2    .1    .0    .1    .1
  10.  *    .0    .2    .2    .2    .1    .1    .1    .1
  15.  *    .0    .2    .2    .2    .0    .1    .1    .1
  20.  *    .0    .2    .2    .1    .0    .1    .1    .1
  25.  *    .0    .2    .2    .1    .1    .1    .1    .1
  30.  *    .0    .2    .2    .2    .1    .1    .0    .1
  35.  *    .0    .2    .2    .2    .1    .1    .0    .1
  40.  *    .0    .2    .2    .2    .1    .1    .0    .1
  45.  *    .0    .2    .2    .2    .1    .1    .0    .0
  50.  *    .0    .2    .2    .2    .1    .1    .0    .1
  55.  *    .0    .2    .2    .2    .1    .1    .0    .1
  60.  *    .0    .2    .2    .2    .0    .1    .0    .1
  65.  *    .0    .2    .2    .2    .0    .1    .0    .1
  70.  *    .0    .2    .2    .2    .0    .1    .0    .1
  75.  *    .0    .2    .2    .1    .0    .1    .0    .1
  80.  *    .0    .2    .2    .1    .1    .1    .0    .2
  85.  *    .0    .2    .2    .0    .1    .1    .1    .2
  90.  *    .0    .1    .1    .0    .0    .1    .1    .1
  95.  *    .1    .1    .0    .0    .0    .1    .1    .2
 100.  *    .1    .0    .0    .0    .0    .1    .1    .2
 105.  *    .1    .0    .0    .0    .0    .1    .1    .2
 110.  *    .2    .0    .0    .0    .0    .1    .1    .2
 115.  *    .2    .0    .0    .0    .0    .1    .1    .2
 120.  *    .2    .0    .0    .0    .0    .1    .1    .2
 125.  *    .2    .0    .0    .0    .0    .1    .1    .2
 130.  *    .1    .0    .0    .0    .1    .1    .1    .2
 135.  *    .1    .0    .0    .0    .1    .0    .1    .1
 140.  *    .1    .0    .0    .0    .1    .0    .0    .1
 145.  *    .1    .0    .0    .0    .0    .0    .0    .1
 150.  *    .1    .0    .0    .0    .0    .0    .0    .1
 155.  *    .1    .0    .0    .0    .0    .0    .0    .1
 160.  *    .1    .0    .0    .0    .0    .0    .0    .0
 165.  *    .1    .0    .0    .0    .0    .0    .0    .0
 170.  *    .1    .0    .0    .0    .0    .0    .0    .0
 175.  *    .1    .0    .0    .0    .0    .0    .0    .0
 180.  *    .1    .0    .0    .0    .0    .0    .0    .0
 185.  *    .1    .0    .0    .0    .0    .0    .0    .0
 190.  *    .1    .0    .0    .0    .0    .0    .0    .0
 195.  *    .1    .0    .0    .0    .0    .0    .0    .0
 200.  *    .1    .0    .0    .0    .0    .0    .0    .0
 205.  *    .1    .0    .0    .0    .0    .0    .0    .0
1
                                                                                                                             PAGE  6
      JOB: Site 5 Olymp & La Brea (S5B5PM.DAT)                 RUN: Site 5 Build 5 PM

 WIND ANGLE RANGE:   0.-360.

 WIND  * CONCENTRATION
 ANGLE *      (PPM)
 (DEGR)* REC21 REC22 REC23 REC24 REC25 REC26 REC27 REC28
 ------*------------------------------------------------
 210.  *    .1    .0    .0    .0    .0    .0    .0    .0
 215.  *    .1    .0    .0    .0    .0    .0    .0    .0
 220.  *    .1    .0    .0    .0    .0    .0    .0    .0
 225.  *    .1    .0    .0    .0    .0    .0    .0    .0
 230.  *    .1    .0    .0    .0    .0    .0    .0    .0
 235.  *    .2    .0    .0    .0    .0    .0    .0    .0
 240.  *    .2    .0    .0    .0    .0    .0    .0    .0
 245.  *    .2    .0    .0    .0    .0    .0    .0    .0
 250.  *    .2    .0    .0    .0    .0    .0    .0    .0
 255.  *    .2    .0    .0    .0    .0    .0    .0    .0
 260.  *    .2    .0    .0    .0    .0    .0    .0    .0
 265.  *    .2    .2    .1    .1    .1    .0    .0    .0
 270.  *    .2    .2    .1    .1    .1    .0    .0    .0
 275.  *    .0    .2    .2    .1    .1    .0    .0    .0
 280.  *    .0    .2    .2    .1    .2    .0    .0    .0
 285.  *    .0    .2    .2    .2    .2    .0    .0    .0
 290.  *    .0    .2    .2    .2    .2    .0    .0    .0
 295.  *    .0    .2    .1    .2    .2    .0    .0    .0
 300.  *    .0    .2    .1    .2    .2    .0    .0    .0
 305.  *    .0    .2    .1    .2    .2    .0    .0    .0
 310.  *    .0    .2    .1    .2    .2    .0    .0    .0
 315.  *    .0    .2    .1    .2    .2    .0    .0    .0
 320.  *    .0    .2    .1    .2    .2    .0    .0    .0
 325.  *    .0    .2    .1    .2    .2    .0    .0    .0
 330.  *    .0    .2    .1    .2    .2    .0    .0    .1
 335.  *    .0    .2    .1    .2    .1    .0    .0    .1
 340.  *    .0    .2    .1    .1    .0    .0    .0    .1
 345.  *    .0    .2    .2    .1    .0    .0    .1    .1
 350.  *    .0    .2    .2    .2    .1    .0    .1    .1
 355.  *    .0    .2    .2    .2    .1    .0    .1    .1
 360.  *    .0    .2    .2    .2    .1    .0    .1    .2
 ------*------------------------------------------------
 MAX   *    .2    .2    .2    .2    .2    .1    .1    .2
 DEGR. *  110     0     0     0   280    10     0     0

 THE HIGHEST CONCENTRATION IS      .30 PPM AT   25 DEGREES FROM REC16.
 THE 2ND HIGHEST CONCENTRATION IS      .20 PPM AT  160 DEGREES FROM REC2 .
 THE 3RD HIGHEST CONCENTRATION IS      .20 PPM AT  225 DEGREES FROM REC3 .
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